ABSTRACT

Title of Document: THE EFFECTS OF INTERACTIONS AND INDIVIDUAL CHARACTERISTICS ON EGRESS DOWN STAIRS

Bryan Lawrence Hoskins, Ph.D., 2011

Directed By: Professor James A. Milke,
Department of Fire Protection Engineering

For high-rise building evacuations, travel on stairs accounts for a large portion of the total egress time. Previous research has typically focused on the relationship between speed and density, with the results being relatively poor for predicting how long an individual requires to descend the stairs.

In this dissertation, methods for measuring fundamental variables for determining speed and density are presented. The inverse of speed (normalized time) is shown to be more conservative for prediction methods. Furthermore, the interactions between individuals and flow units and the characteristics of individuals provide a deeper understanding of the flow dynamics and lead to more accurate predictions than relying on density alone.

Rather than all of the occupants behaving in a uniform manner, flow units form where all of the occupants in them descend at the same rate. The first persons in flow units were found to be engaging in five different types of behavior that set the pace for their followers. There are also flow states identified that previous researchers have not identified.

How occupants interacted with one another was also found to vary based on individual characteristics. The behavior of individuals was not random, but appeared to be based on variables like gender and exit lane. These characteristics, in turn, were found to influence their descent rate.

These findings are then applied to a blind data set and the actual observations are accurately predicted. This allowed equations to be presented that are representative of the flow dynamics.

THE EFFECTS OF INTERACTIONS AND INDIVIDUAL CHARACTERISTICS ON EGRESS DOWN STAIRS

By

Bryan Lawrence Hoskins

Dissertation submitted to the Faculty of the Graduate School of the
University of Maryland, College Park, in partial fulfillment
of the requirements for the degree of
Doctor of Philosophy
2011

Advisory Committee:
Professor James A. Milke, Chair
Professor James Wallace
Associate Professor André Marshall
Associate Professor Arnaud Trouvé
Associate Professor Elise Miller-Hooks

Acknowledgements

There are many individuals who have made it possible for me to complete my PhD. My advisor, Dr. James A. Milke, has given me an immeasurable amount of time, effort, and support starting during my undergraduate years and continuing through my graduate years. Without his help, I would not be where I am today. I also want to thank my committee members for their guidance on my dissertation and other assistance that they have given me over the years.

I am especially grateful for the help of the National Institute of Standards and Technology (NIST) in allowing me to spend nearly two years going through the videos that I have used for the data in my dissertation as well as helping me to learn some of the finer details of conducting research. I want to give special thanks to my supervisor, Mr. Jason Averill, for all of his guidance and assistance and Mr. Rick Peacock for always being willing to listen when I was stuck on some issue and for his help on a variety of issues. I am most grateful for all of the time, help, and advice that Dr. Erica Kuligowski has given me. Not only was she extremely helpful with the technical issues that I was dealing with, but she also helped me find my place in the field. I learned more from her than I ever imagined was possible.

Finally, I want to thank all of my family, friends, and teachers for their support and encouragement over the years. I want to give special thanks to my parents, grandparents, aunts and uncles. Last but not least, I want to thank my brother for everything over the years.

Table of Contents

List of Tables

List of Figures

Chapter 1: Introduction

Building evacuations can be required in the event of a fire, severe weather, or other emergency. When the evacuation is required, the egress system needs to be designed to enable the people to reach a point of safety before conditions within the building become untenable. In order to design the egress system to meet the expected objectives, the designer needs to be able to accurately predict how long it will take to evacuate the building. In order to do this, they need to know what variables lead to the amount of time that people require. How each individual interacts with his or her surroundings and fellow building occupants will determine how long that individual needs to safely exit the building. Then, the combination of the response of all of the individuals will result in the total egress time for the building.

There are currently dozens of simulation models available for the designer to choose from, but the models are not well validated (Kuligowski, Peacock, and Hoskins, 2010). More data and a better understanding of the fundamental principles guiding egress behavior needs to be developed (Averill, 2011). In order for any calculation method to be effective, data needs to be collected that contains the relevant variables, or specifically controls for selected variables.

This study focuses on the movement of building occupants on a critical egress component, the stair. The objective is to determine the fundamental principles that determine the amount of time that each individual requires for egress while a part of a total building evacuation. This will be accomplished by developing a mathematical model built from actual evacuation data using key variables identified by others as well as new variables developed based on behaviors observed during fire drills.

1.1 Egress System Design

When designing an egress system, the system designer theoretically considers the number of occupants in a building, the egress components available, and the potential hazards within the building. The designer then conducts an evacuation analysis to determine if the proposed egress system will meet the stated goals for the system.

In an evacuation analysis, the Required Safe Egress Time (RSET) needs to be calculated in order to determine how long it will take for all occupants to safely exit the building. The Available Safe Egress Time (ASET) needs to be determined to see how long tenable conditions are present. The fundamental requirement for an egress system is that RSET is less than ASET.

RSET is the sum of:

- the time until the occupant is aware of the need to evacuate
- the time until the occupant actually starts to move towards an exit (pre-evacuation time)
- the time required to reach safety

RSET will vary for each individual. The characteristics of the individual, his or her interactions with the physical aspects of the building, and his or her interactions with other people will determine the RSET for that individual. It is from these characteristics and interactions that the RSET value is determined rather than from homogeneous or average conditions. For the entire building, the RSET value is that of the last individual to leave. Thus, subpopulations that require more safe egress time need to be accounted for.

ASET is determined based on the exposure of an individual to the smoke and/or heat of the fire or the structural strength of the building. ASET can be determined based on loss of visibility, carbon monoxide concentration, heat exposure, or any other tenability criteria set by the designer. ASET values can be set for each area within the building and for the building as a whole. For example, in an atrium, the ASET value for people on the upper floors from exposure to smoke or heat is less than that for people on the lower floors due to smoke filling.

From a life safety perspective, it is more important to consider those occupants that will be the slowest movers. While a stair can be considered a relatively safe area in terms of fire, there is still the potential for smoke to enter the stair or structural collapse. In the event of an evacuation from a weather event or an explosion, time is very important even for those occupants that are within the stair.

1.2 Egress Systems

Egress systems consist of the means by which occupants travel from their initial location to their final destination, typically outside of the building. The egress system is comprised of several egress components (doorways, corridors, stairs, ramps, and similar features). A typical egress path for a person in a multi-story building will consist of the occupant walking from the room that they are in, passing thru a doorway into a corridor, walking along the corridor, passing thru a doorway into the stairs, walking down the stairs, and exiting the building at the bottom of the stairs.

As the individual moves from one point to another, their speed may change. Some of this change will be caused by the physical nature of the component; people generally walk faster on level ground than they do on stairs (Fruin, 1971). Other changes in speed will be brought about due to interactions with other people; people tend to walk faster in isolation than they do in crowded areas (Fruin, 1971).

At points where groups of people converge together or where the type of egress component changes, movement speeds will change and queues can form. Also, if an individual is slower than the people around them, the people behind that person are either forced to decrease their speed or maneuver around the individual. In all of these cases, the decisions by individuals will determine how long they require to safely egress from the building. Their choices and actions can then slow the people that are near them.

The movement on stairs is critical for determining the amount of time required to safely evacuate the building. For example, the Life Safety Code (NFPA, 2009) requires the maximum travel distance to an exit in a new business occupancy that is fully sprinklered to be 91 m. Assuming an approximate travel distance of 8.2 m per floor in a stair (Galbreath, 1969), travel distance in stairs is greater than the maximum travel distance to reach the stair for buildings taller than 11 stories. Even for buildings less than 11 stories, occupants located closer to the stair may travel further in the stair than outside of it. Furthermore, because the stair shaft is required to be fire rated and means of egress cannot have occupants move to a less safe location (NFPA, 2009), the stair tends to be one of the last components in any egress system with multiple components directing occupants to it. Because the stairs are a major component in the egress system, an error in estimating the movement on stairs will lead to an error in the overall evacuation time.

1.3 Calculation Methods

There are two basic types of methods used to calculate RSET. The first are algebraic equations. The second are computer simulations.

1.3.1 Algebraic Equations

Algebraic equations are relatively simple and can be determined using just a pencil, piece of paper, and calculator. They were developed before the computer simulations and are used as the basis of the computer simulations.

The algebraic equations were developed before the computer models and tend to be simpler in terms of number of variables. The computer models are more time and variable intensive, so, in theory, they could produce a more accurate result if they are developed based on the principles determining the flow dynamics.

1.3.1.1 Algebraic Equations- Total Building Evacuation

Some of the first correlations for egress times on stairs come from the work of Pauls (1980). He found that the total egress time from buildings was a linear function of egress width and total building population. He proposed that, when the normalized population was less than 800 persons per meter of effective width (the egress width minus a boundary layer), the total evacuation time could be calculated by:

$$t = 2.00 + 0.0117 \cdot p \qquad (1.1)$$

where:

t=total evacuation time (minutes)
p=population per meter of effective stair width (persons/m)

This equation was based on his study of 56 office buildings. With 6 exceptions for buildings above 15 stories, he found that the expected total egress times were within one minute of the observed egress times. All of the drills were approximately 3 to 10 minutes in length. While Pauls claimed a net error of 0.2%, the absolute value of the errors was larger (original from page 268 of Pauls (1980) is shown in Figure 1.1).

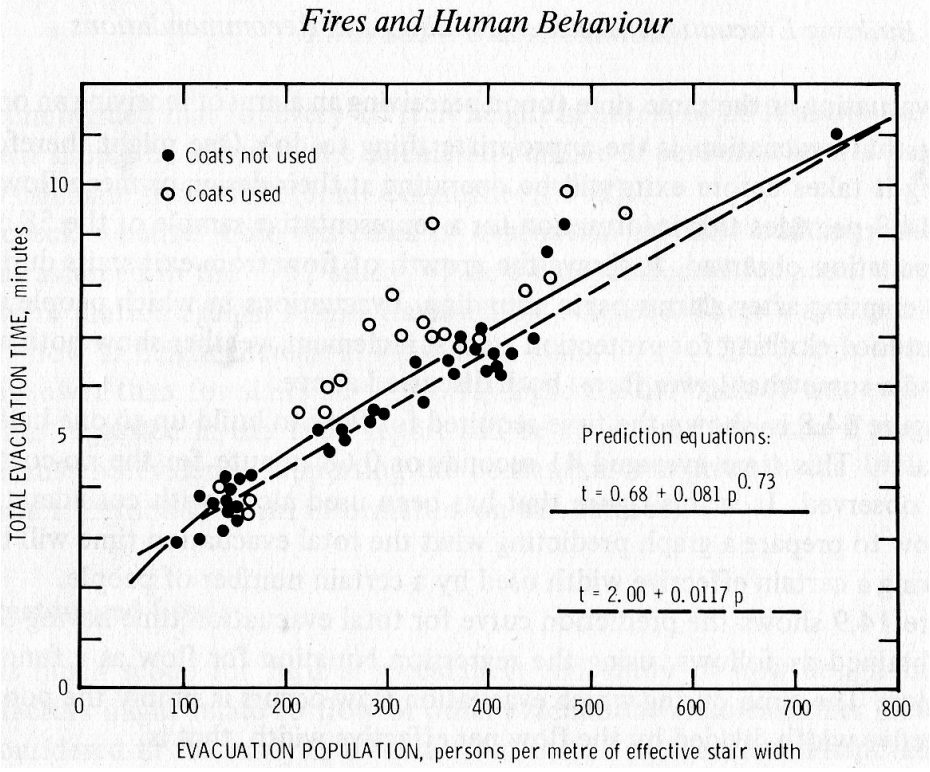

Figure 1.1: Evacuation Time from Pauls's Experiments

This equation is still presented in handbooks to be used when calculating total egress times from buildings (Fahy, 2008; Proulx, 2008).

1.3.1.2 Algebraic Equations- Movement Speed

Based on the work of Pauls and others, Gwynne and Rosenbaum (2008) present an estimate that occupants' speed could be based on effective stair width, density, and the riser and tread dimensions. If the density is below 0.538 persons/m^2, then it is assumed that the individuals will move at their natural pace. When the density is above 3.77 persons/m^2, it is assumed that no movement occurs. In between these two ranges, they proposed that the speed could be calculated by:

$$s = k - a \cdot k \cdot D \quad (1.2)$$

where:

s=slope speed (m/s)
k=constant depending on type of egress component
a=0.266
D=density (persons/m^2)

1.3.1.3 Limitations of Algebraic Equations

The algebraic equations provide a first order estimate of the individual movement speeds and do not consider several factors involving individual behaviors or the interactions of people with their environment. First, they only look at the average behavior. This ignores the fact that individuals can have characteristics that prevent them from moving at the speed of the rest of the population. Conversely, some individuals may choose to pass others and move at a faster speed. Second, the density is an average measurement. In mass population movements, clusters (platoons) will form (Templer, 1975) and this will lead to many individuals not experiencing "average" conditions. Third, it does not account for the pace that previous occupants were descending at.

1.3.2 Computer Simulations

Several evacuation models have been developed to determine RSET values. These models use different methods in how they view occupants as well as different variables that they consider. Thus, the models can range from versions akin to the algebraic equations to models that attempt to capture the movement and decisions that the individual makes that determine their RSET value. This review is not considered to be exhaustive of all the models that are currently available. A comprehensive review is provided by Kuligowski, Peacock, and Hoskins (2010). Instead, the review included in this document will focus on the different types of evacuation models in order to understand where the field currently stands.

1.3.2.1 Computer Simulations- Model Types

Evacuation models can be movement, behavior, or partial behavior models (Francis and Saunders, 1979). These labels refer to what actions the individuals consider as they move through the building.

The movement models are primarily concerned with how occupants move. This is accomplished by treating all of the occupants like fluid particles that move from a point of origin to a final destination. These models are best at identifying areas where flow problems might be found. Basically, they solve a series of algebraic equations in an efficient manner. Generally, individual actions are ignored and all occupants start to move at the same time. The occupants make no decisions and movement speeds are either specified by the user or are based on density (or other physical

properties) alone. Like the algebraic equations, these models provide a simplified estimate of egress times.

The behavior models consider each occupant individually. The occupants can be assigned tasks (firefighting, assisting others, etc.) to perform before they start to evacuate. These models are best for occupancies where a staff member and/or other occupants are expected to perform duties rather than, or in advance of, evacuating. An example would be a health care facility where staff needs to assist patients in evacuating. Because individuals are assigned tasks to do, the model design requires an understanding of the decision process of individuals as well as how they interact with other people in the building.

The partial behavior models allow an individual occupant to respond to their surroundings. These models can account for interactions and individual characteristics. Each occupant makes decisions about the path that they follow based on their natural movement speed, knowledge of egress paths, and things encountered after starting to evacuate. This can include interactions with other simulated occupants, being able to "see" signage, encountering smoke, etc. In order for the models to accurately and consistently reproduce behavior, data needs to be collected and analyzed in order to determine the key variables and the magnitude of their impact rather than using theory and altering coefficients that provide global rather than local agreement. As will be discussed in Chapter 2, few researchers have considered what these variables are, let alone what their magnitude is. Without understanding these fundamental human movement principles, the simulation models cannot provide accurate predictions over a large range of scenarios.

How the decisions are represented in the partial behavior models depends on the model design. Like the movement models, occupants are primarily trying to reach a designated point of safety. However the individual occupants are not simply moving like a fluid. In some of these models, individuals are given unique characteristics. Usually little, if any, guidance is provided about what these unique values should be. Understanding individual actions is very important for the partial behavior models because each occupant makes decisions based on their interactions with other occupants and the environment.

1.3.2.2 Computer Simulations- Perspectives

The model can have either a global or individual perspective (Kuligowski, Peacock, and Hoskins, 2010). These labels refer to what level of knowledge is obtained about the individuals.

If the model has an individual perspective, the location of each occupant is known at all times. The behavior and partial behavior models must have an individual perspective because each individual is making decisions. Using models with an individual perspective, it is possible to follow one individual through their entire egress path and determine how conditions change for that individual throughout the

egress scenario. Only in these models is it possible to consider interactions and individual characteristics.

A global perspective model assumes all occupants have the same characteristics and the flow of occupants is homogeneous. The global perspective models do not track each individual through the entire egress process. The movement models have this perspective. The output from these models can include results such as total evacuation time and density maps that may vary with time. The global perspective is less time and data intensive, so those models provide less detailed information.

Along with how the program views the occupants, there can be differences in how the simulated occupants view the building. The simulated occupants can have an individual knowledge of the building by only knowing the paths that they are programmed to know or have discovered during the egress process. This is only possible in models that allow individuals to make decisions about their own egress paths.

If the simulated occupants have a global perspective, then they know about all egress paths in advance and which will be their best path to follow. A global perspective of all exits allows for an optimum egress time to be calculated.

1.3.2.3 Computer Simulations- Behavior

Kuligowski, Peacock, and Hoskins (2010) classify the models accounting for behavior as being in one of five categories. Some models do not include any behavior at all. A second group of models accounts for behavior by using implicit rules that alter the movement throughout the entire evacuation. In some models, rather than having implicit behaviors that are present throughout the evacuation, the behaviors are conditional on things that the occupant encounters. The fourth group of models considers behavior in a manner where the model attempts to mimic human intelligence. This can be accomplished for the partial behavioral models with an individual perspective where the occupant responds to the conditions that they experience. The final type of models treats behavior in a probabilistic manner. With multiple runs of the simulation it is possible to determine a possible range of scenarios.

When the models do account for different behaviors, the different values should be based on actual data. This requires identifying the characteristics that are common to slower moving populations rather than assuming that all occupants are equally likely to be slower moving. It also requires an understanding how occupants interact with each other and the building rather than assuming that all occupants are acting independently.

1.3.2.4 Computer Simulations- Features

Models can have special features, e.g. the ability to include fire effects and user defined attributes. One example is the pre-evacuation time. The pre-evacuation time

is usually user defined and can be combined with the time required for occupant notification to give the total time of fire development before individuals start the egress process. These times can be incorporated either globally or individually.

In the global case, no occupants start to move until a specified time has passed. In essence, this global perspective is a safety factor applied to the entire population. In models with fire effects included and occupants not being allowed to move for a period of time, the occupants may be exposed to less tenable conditions as they move through the building than they would experience if they started to move immediately. In models without fire effects, the global pre-evacuation time is no different than adding a safety factor at the end of the analysis.

An individual perspective on pre-evacuation time involves each individual (or group), delaying his or her egress by a probabilistic distribution defined by the user. This leads to individuals starting to use the egress components at different times.

Other special features include the ability to block exits, have counterflow, change occupants speeds based on fire effects or toxicity, include groups, and use elevators for evacuation. Models can have combinations of these features.

1.3.2.5 Computer Simulations- Modeling Non-Homogeneous Populations

To account for some of the variability between subpopulations and the average movement speed, some computer models account for a range of speeds within the occupants. This is accounted for by a distribution of movement speeds or user defined speeds for different individuals or groups. As will be shown in Chapter 2, the previous studies involving movement speeds on stairs did not provide distributions or bounding equations for this purpose.

1.4 Data Sources

In order to develop the algebraic equations or validate the models, data points need to be collected. Data can come from five different types of research. A study can look at behavior of general population on stairs during a fire drill, during normal use, or during a real fire; be a compilation of others' research; or examine a controlled laboratory situation.

1.4.1 Fire Drill

By observing fire drills, the researcher is able to pre-position recording equipment and staff in order to best observe the evacuation. Drills stress the egress system by requiring large portions of the building to be evacuated at the same time. Building occupants can interpret a fire drill as an actual emergency (Khristy, 1985), so the behavior is similar to what would be seen during an actual fire for occupants remote from the effects of the fire. Examples of researchers that have observed fire drills include Pauls (1980) and Proulx (1995).

1.4.2 Normal Use

Observing normal use conditions is similar to observing fire drills with respect to the ease of observation. Unlike during drills, there is no indication of an emergency. These studies have typically been conducted in locations where people are expected to move with some urgency. Examples include transit stations (e.g., London Transport Board, 1958) and theaters (e.g., National Bureau of Standards, 1935). Fruin (1971) and Templer (1975) also collected normal use data.

1.4.3 Real Fires

Unlike data collected during fire drills or normal use, data collected during real fires do not require any assumptions about behavior being similar to real events. Unfortunately, there is no known data publicly available that systematically records movement on stairs during a real fire. Instead, researchers have interviewed survivors after the fact. There are two main limitations to this approach. First, it assumes that a person's memory is perfect (or can be adjusted by the researcher to match known facts). Second, it is naturally biased to only include those individuals that survived the fire and are willing to discuss their experiences. Examples of this type of study include Galea and Blake (2004) and Averill, et al. (2005).

1.4.4 Compiled Works

Compiled studies collect the works of others and attempt to find similarities and general guidance from multiple sources. They do not collect any data for their analysis. Thus, in theory, they eliminate the bias that might be present in a particular study. However they are ultimately only as valid as the sources they used. Both Predtechenskii and Milinskii (1978) and Gwynne and Rosenbaum (2008) are examples of compiled works.

1.4.5 Laboratory Study

Laboratory studies are conducted under controlled conditions. The researcher is interested in specific details and the subjects are instructed on exactly how to behave; there is no sense of emergency or other "real" effect. Examples of this type of study include Templer (1975), Frantzich (1996), and Boyce, et al., (1999).

1.5 Current Understanding of Movement on Stairs: Level of Service

From all five types of data sources, the proper variables need to be extracted in order to accurately assess how people move while on stairs. Previous research examining individual movement speed on stairs during building evacuations focused on a limited number of physical characteristics of the building (at most, researchers considered engineering variables like stair width and tread dimensions, but some failed to even note these characteristics[1]) and the density that was observed. Assuming individuals

[1] See Chapter 2 for a detailed discussion on what various authors considered.

ignore most of their physical environment and others in the building does not explain most of the variation found in actual egress scenarios (Peacock, Averill, and Kuligowski, 2009). As will be discussed more in Chapter 2, these other variables are often not mentioned, looked at qualitatively, or not properly controlled for.

As was shown with Equation 1.2, movement speed on stairs can vary from a free-flow condition to a complete stoppage. The approach in that equation is that, for a given stair, the only population dynamics that influence movement speed on the stairs is the density. The level of service concept, proposed by Fruin (1971), defines six different cases relating the density to the flow conditions. These levels are shown in Figure 1.2 using images from pages 81 and 83 of Fruin (1971).

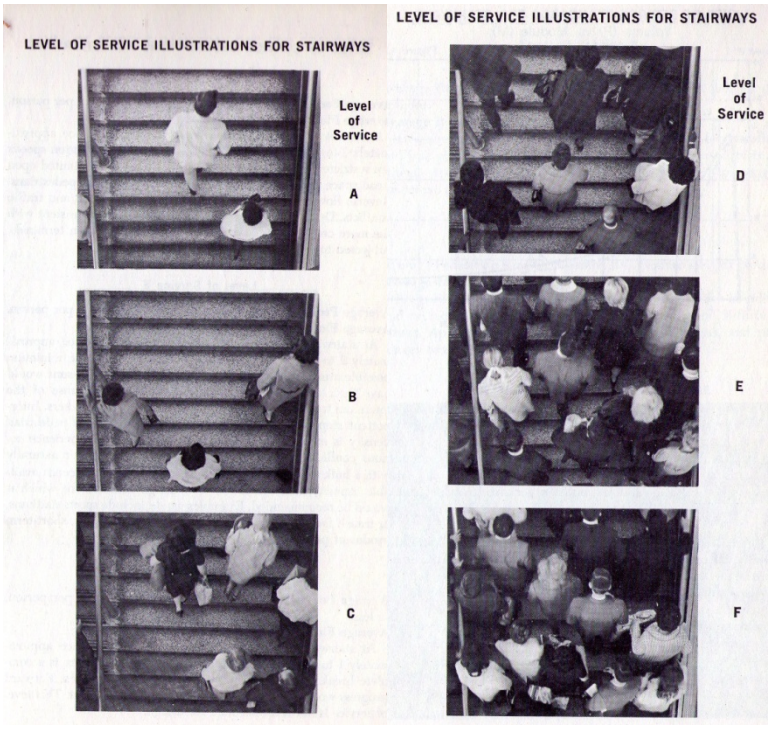

Figure 1.2: Fruin's Level of Service

Fruin labeled the cases by different letters and qualitatively described the types of behavior present for each quantitatively defined level.

- Level A: >3.25 m^2/person on level surfaces, >1.86 m^2/person on stairs- occupants can move at their own speed and the presence of other people has no effect on the egress time.
- Level B: 2.32 to 3.25 m^2/person on level ground, 1.39 to 1.86 m^2/person on stairs- occupants can move freely when with the main flow direction; the bulk flow will slow down when counter flows are present.
- Level C: 1.39 to 2.32 m^2/person on level ground, 0.93 to 1.39 m^2/person on stairs- the ability for the occupant to walk at the desired speed is restricted.

- Level D: 0.93 to 1.39 m^2/person on level ground, 0.65 to 0.93 m^2/person on stairs- the walking speeds of most occupants are reduced and passing other occupants is limited.
- Level E: 0.46 to 0.93 m^2/person on level ground, 0.37 to 0.65 m^2/person on stairs- occupants have to move at the speed of the slowest member since passing is severely limited.
- Level F: <0.46 m^2/person on level ground, <0.37 m^2/person on stairs- occupants are in contact with one another and movement is reduced to shuffling; this level is not recommended for design.

1.6 Variable Types

Based on isolated studies or research in other fields, a selection of other variables that can be visually observed has been identified that potentially determine movement speeds on stairs. Five different classes of variables affect the speed of individual occupants. These classes are merely groupings of characteristics. In some instances, it may be possible for a variable to belong to more than one class.

1.6.1 Engineering Variables

The first class is engineering variables. They describe the physical environment and can be recorded in advance. They are true for the entire population, not just certain individuals.

1.6.1.1 Stair Width

The original building codes relied upon exit lanes to determine the capacity of an egress component (Pauls, 1980). This assumption was driven by the fact that each individual needed a given amount of physical space and that people traveled in columns. Thus, the number of units of that physical space across the width of the component determined how many people could use it.

With the work of Pauls (1980), the building codes shifted to using the linear proportionality concept. Rather than accounting for whole people, components could accommodate fractions of people. The linear proportionality concept enables the designer to design for a continuous population size rather than as a step function.

1.6.1.2 Riser Height and Tread Depth

In stairs, the riser height and tread depth can alter the speed at which individuals move. In the Gwynne and Rosenbaum speed equation presented earlier (Equation 1.2), a different k-value is assigned for each combination of riser height and tread depth.

Over several centuries, ideal relationships between riser height and tread depth (often with unknown origins) have been suggested that were claimed to allow individuals to most efficiently use stairs. Templer (1975) provided some examples. These

calculations have ranged from simple linear relationships to more complex formulas. Examples include:

$$R + T = 43.2cm \tag{1.3}$$

$$2 \cdot R + T = 64.8cm \tag{1.4}$$

$$R \cdot T = 484cm^2 \tag{1.5}$$

$$\frac{R}{T} = \tan\left(3.1 \cdot \left(R - 7.6\right)\right) \tag{1.6}$$

$$R = 22.9 - \sqrt{7 \cdot \left(T - 20.3\right) \cdot \left(T - 5.1\right)} \tag{1.7}$$

$$T = 12.7 + \sqrt{\frac{\left(22.9 - R\right)^2}{7} + 58.1} \tag{1.8}$$

where:

R=riser height (cm)
T=tread depth (cm)

The stair riser height can have an impact on individual movement speeds within stairs. A steep riser height can slow the individual down due to either fatigue or fear of falling (Templer, 1975). Conversely, since the individual is required to make fewer steps, the average vertical speed will increase (Templer, 1975). For normal stride patterns, steeper risers (16.0-22.6 cm) are preferred for ascent and shallower ones (11.7-18.3 cm) for descent (Templer, 1975).

The tread depth can alter the occupant's speed in two ways. First, if the tread depth is very narrow, the occupant will move more slowly as they takes extra caution to ensure that their foot is safely on the tread (Fruin, 1971). In fact, the actual stride pattern can change (Templer, 1975). In stair descent, the individual ensures that the ball of the foot lands on the tread. If the tread is not large enough to place the entire foot in line with the direction of motion, the individual will place their foot at an angle so that it will fit. This is a less natural movement and it will cause the individual to move at a slower pace (Templer, 1975). Based on average shoe and foot sizes for the 95th percentile of the population, tolerance of heel to nosing, and the comfortable toe overlap, the minimum tread depth on stairs should be 27.9 cm (Templer, 1975). If the tread depth is too long, then the person may slow down as an intermediary step is required and individuals hesitate before taking either the first or last step as well as having to shift his or her gait between the two different styles (Templer, 1975).

1.6.1.3 Time and Location

An evacuation with occupants having just been woken up could lead to slower movement speeds (Khristy, 1985). Rather than combining data in this situation with those when occupants are fully awake, the appropriate analysis would compare the

two scenarios for differences in movement speeds. As for seasonal effects, Pauls (1980) found that the average total evacuation time in cold or wet weather was greater than in the warm and dry conditions.

The location refers to both the type of building that is being evacuated and its location. Different types of buildings have different types of people present. The physical location could cause differences if there are differences based on culture (Galea, et al., 2010).

1.6.1.4 Integrity of Egress Route

The integrity of an egress route consists of the physical conditions present within the egress route that could alter movement speed. These features can be inherent to the building or brought about by the emergency at hand. If conditions within the egress route become untenable, individuals may choose to change their egress paths and find another, more desirable option.

One component of the integrity of the egress route is the lighting level (Wright, et al., 2001). Associated with decreased lighting can be the presence of fire smoke. Individuals decrease their movement speed in smoke (Jin, 1976). While some individuals will move through smoke further than the visibility distance, others will turn back (Bryan, 1977). Also, as individuals are exposed to the heat and products of incomplete combustion, physical capabilities are decreased which can decrease movement speeds (Jin, 1976).

The third integrity of egress route issue comes from objects that block the egress path. While all egress paths are supposed to be kept free of physical obstructions, this is not always true in reality (Kratchman, 2007).

1.6.2 Characteristic Variables

The second class of variables is characteristic variables. This information is inherent to the individual and does not change at any point during the egress scenario.

1.6.2.1 Age and Gender

For studies that look at the population under normal or drill conditions, the exact genders and ages are not known. Gender is determined based on secondary sex characteristics and age is approximated based on physical features and placed into an appropriate range.

Gender can play a role in movement speeds in a few ways. First, some studies have found that the average male movement speed is greater than the average female speed (e.g., Fruin, 1971). Thus, if these findings are accurate, men move faster than women on stairs. Second, both men and women prefer to have more personal space when around men (Fruin, 1971). Third, a difference in speeds could be caused by

differences in footwear or clothing associated with a particular gender or age group (Templer, 1978).

On the other hand, studies have found that gender is not statistically significant in determining egress speed. Templer (1975) studied individuals in isolation and Proulx (1995) observed individuals during a drill.

For age, the very old and the very young move more slowly than the average population (Fruin, 1971, Proulx, 1995).

1.6.2.2 Pre-Evacuation Time

Six different steps have been found to determine the amount of time that an occupant requires before the occupant safely exits a building (Bryan, 2008). The first four steps are always part of the pre-evacuation time while the last two can be depending on the actions that are chosen. How an individual approaches the six steps depends on the mental and physical characteristics of the individual. The first step is recognition. In this step, the occupant becomes aware of cues (smoke, flames, alarm, etc.) and realizes that this represent a potential threatening situation. Until the occupant realizes that there is a potential threat, he or she will not consider doing anything other than his or her normal activities. The second step is validation. Here the occupant seeks additional information in order to make sure that the initial indications are correct. If the occupant is not convinced that there is a threat, he or she will return to his or her normal activities until more recognition has occurred. If the occupant's concerns are validated, he or she will then proceed to the next step. The third step is definition. For this step, the occupant combines all of the cues to determine the extent, nature, and severity of the threat. The fourth step is evaluation. The occupant determines what the possible responses for the given scenario are. This could be evacuating, defending in place, or any other behavior that the occupant thinks is required. For example, during a winter egress scenario, occupants that choose to evacuate are likely to consider the outside weather and thus dress accordingly. While performing the chosen action, the occupant is also continuing the first three steps if more information has become available. The fifth step is commitment. Here, the occupant carries out the plan from the previous step. In this step, the occupant will begin to leave the building, head to a secure location to wait for rescue, or attempt to fight the fire. The final step is reassessment. For this step, the occupant determines that the previous ideas did not reach the desired result. For example, the chosen egress path could be obstructed or the fire was too large to be extinguished. This then requires the occupant to develop new strategies based on the new information that has been acquired.

In actual fires, individuals that took more time to start leaving the building seemed to move faster and be more aggressive (Tubbs and Meacham, 2007). As the perceived risk increased, the individuals felt a more pressing need to get out of the building quickly. Thus, if this is the case, longer pre-evacuation times will lead to occupants moving faster.

1.6.2.3 Body Size

Not all people are the same size (Kendik, 1986). In addition to the physical area that people occupy, individuals tend to want a buffer area that other people are not to enter (Fruin, 1971). Pauls, Fruin, and Zuppan (2005) have suggested that the changing population demographics will alter the movement speeds on stairs.

1.6.3 Mobility Variables

The third class is mobility variables. While similar to characteristic variables, these could change for the individual during the egress scenario. In most instances, no change will probably occur, but there is the potential that this variable could change for the individual during the egress process.

1.6.3.1 Encumbrances

Encumbrances may include personal possessions that occupants carry because they did not want to leave the item(s) behind or simply they had something in hand when they started the egress process and did not want to delay their evacuation in order to return the item to some other area. Proulx (1995) and Fruin (1971) found that occupants carrying objects moved at the same speed as other occupants while Peacock, Hoskins, and Kuligowski (2011) found that occupants carrying objects moved slower than others.

1.6.3.2 Fatigue

The location of origin can help to determine how far the individual has traveled. While several studies (i.e., Pauls and Jones, 1980; Khisty, 1985) indicated that fatigue is not an issue in building evacuations, this was based on speed only and other variables could have been counteracting the fatigue effects. One study (Pauls and Jones, 1980) actually found a slight increase in movement speed as the individuals descended. On the other hand, Peacock, Averill, and Kuligowski (2009) and Proulx, et al., (1999) both reported fatigue being present. While not based on any known data, the Joint Committee (1952) recommended that, for stairs only serving one floor, the movement speeds be decreased for longer travel distances.

1.6.3.3 Groups

Multiple authors have identified groups forming during evacuations (i.e., Jones and Hewitt, 1985 and Shields, Boyce, and McConnell, 2009). The groups stay together once evacuation has started (Proulx, 1995) and move no faster than their slowest member (Sime, 1994). Even in the work environment, potentially 90% of the population evacuated in groups (Galea and Blake, 2004). During an evacuation, groups may stay together throughout the evacuation or move together only for a portion of the evacuation, breaking apart before completing the evacuation (Galea and Blake, 2004).

Gates et al. (2005) found that larger groups tended to move more slowly than smaller groups when crossing intersections. They also found that large waiting groups tended to break into smaller groups when crossing. When groups got significantly large, it was hard to distinguish between the smaller groups.

Groups are smaller units that have some connection to one another and, at least temporarily, can be said to be moving together. Related to groups are platoons. Platoons are short bursts of people; a continuous string of individuals that may or may not have any connection to one another aside from being together as the density temporarily increases. Platoons can have a significant impact on the instantaneous flow rate (Templer, 1975).

Groups can cause the local density to be much greater than the average density. In studies of movement speeds in New York City, Pushkarev and Zupan (1975) found that platoons tended to have durations between 5-50s for travel on sidewalks and up stairs from subway stations (no data was collected for travel descending stairs). On sidewalks, on average, 35 to 84% of pedestrians were in platoons. For stairs, the values increased to 75 to 95%. They proposed that the platoon flow could be calculated by:

$$f_p = 0.22 + f_a \tag{1.9}$$

where:

f_p=platoon flow (persons/m-s)
f_a=average flow (persons/m-s)

After studying more than 700 platoons at four sites in West London, Robertson (1969) found that platoons would spread in time exponentially.

1.6.4 Position Variables

The fourth class will be position variables. These variables are expected to change in the course of the drill and will cause variations among individuals' movement speeds as they progress down the building. These variables can change based on how the individual responds to changes in the environment throughout the egress process.

1.6.4.1 Density

In terms of egress systems, density is usually calculated based on the number of individuals within a given floor area (i.e., London Transport Board, 1958 and Pauls, 1980). However Predtechenskii and Milinskii (1978) calculated density based on the fraction of area occupied by people. The density of an individual depends on his or her proximity to other people. Depending on how the researcher chose to determine this variable, it could involve the people ahead of the individual over a defined area or both the people ahead of and behind the individual.

In the middle of the 20th century, Hall (1966) interviewed adult subjects, primarily middle-class, with business or professional occupations, native to the northeastern seaboard of the United States. He found that there were different distances that people were willing to tolerate between themselves and other depending on the situation. The first distance, intimate distance (within 46 cm), is not generally tolerated in public with exceptions like crowded subways. The second distance, personal distance (46-122 cm), is the distance where people can still touch one another, but are comfortable with other people within this distance under many public situations. The third distance, social distance (122-366 cm), is the distance at which many people will converse. Finally, the fourth distance, public distance (over 366 cm) is the distance that public figures maintain when addressing the public. Hall did warn that these distances would vary depending on the cultural norms of the people involved.

1.6.4.2 Exit Lanes

The handrails in most stairs used for egress tend to be along either edge of the stair. Thus, individuals that are using the handrails will be found near the edges of the stairs. This type of behavior has been identified in previous studies (i.e., Templer, 1975 and Pauls, 1980). One exit lane will be an inner lane that provides an individual the ability to travel the shortest distance. Another lane will be the outer lane and the individual in that lane would travel a longer distance on the landings.

Exit lanes can also form as a social protocol. For example, on escalators and moving walkways in the United States, people tend to stand on the right and individuals that are walking are allowed to be on the left (Fruin, 1971). Based on stair erosion, studies of individuals in isolation, and studies of large groups, the stay on the right tendency has been seen to occur on stairs as well in the United States (Templer, 1975). The main exceptions tend to be when moving to the left is more convenient or provides a shorter path, but, even in these instances, some individuals stay to the right (Templer, 1975).

Also, if an egress component is used for multidirectional flow, each population tends to split the space into lanes so that each can move past one another (Templer, 1975). While egress from buildings in the case of an alarm tends to have all components experiencing a unidirectional flow, counterflows can occur if emergency personnel are attempting to enter the building.

1.6.5 Interaction Variables

The final class will be interaction variables. These variables are activities that individuals engage in that could not be studied by observing subjects in isolation.

1.6.5.1 Merging

Merging occurs any time that two or more egress paths combine into one path, e.g. at a stair landing where one path is coming from the floor above and one path is coming

from the stair door. Each individual can choose to follow directly behind the person ahead of them and not allow anyone from the other path in, allow one person in so that occupants from each path are uniformly mixed, or allow multiple individuals from the other path to enter ahead of them. The exact manner in which merging occurs is not well understood (Galea, Sharp, Lawrence, 2008).

Merging behavior can arise from social protocols. For example, when leaving an airplane under normal conditions, people tend to allow all people from the rows ahead of them to enter the aisle ahead of them. Even under emergency conditions, the row of origin appears to be more important than if the person is on an aisle (Galea, et al., no date).

1.6.5.2 Passing

Passing behavior can be caused by one of two scenarios. The first is when an individual is behind someone in an egress component. They then move ahead of the slower individual. The second possible cause of passing is when an individual steps aside to allow several people to pass.

1.6.5.3 Counterflow

Counterflow occurs when there is two-directional flow on the stairs. Under normal-use conditions (e.g., at a mass transit station), this can occur as some people are trying to exit as others are trying to enter (i.e., Daly, McGrath, and Annesley, 1991 and Lee and Lam, 2006). In a building evacuation, in addition to the occupants that are trying to exit, others (e.g., firefighters) can be attempting to move in the opposite direction (i.e., Peacock, Averill, and Kuligowski, 2009 and Kratchman, 2007). The egress component is then split between the two populations.

1.6.5.4 Congestion

Congestion occurs when the occupant has to slow down or stop due to the inability to move at their free-flow speed. This is seen directly in the Level of Service concept proposed by Fruin (1971) and Equation 1.2.

1.7 Research Needs

Aside from the need for more data (Averill, 2011), systematic research needs to consider variables beyond the primarily density related research that has been conducted previously (Peacock, Averill, and Kuligowski, 2009). Variables discussed in Section 1.6 should be considered quantitatively and interactions between the variables should be controlled. Also, other variables that have not previously been identified need to be included that account for how occupants actually behave on stairs while evacuating a building. Ideally, video footage can be used rather than having to rely on people's memories or perceptions. The research for this dissertation will examine many of the variables identified in previous studies and develops new ones based on the data from video footage that has been collected.

The fundamental principles guiding the RSET values need to be better understood. The behavior of individuals needs to be considered. At the same time, the actions of the individuals while a part of the larger group need to be included because people behave differently in groups than they do in isolation (Chertkoff and Kushigian, 1999). This better understanding of the fundamentals can then be applied to the dozens of simulation tools currently available.

1.8 Summary

During an emergency, occupants can be required to evacuate from a building. The egress system needs to be designed to efficiently to allow occupants to reach a safe location in a timely manner. The ability to design the system to meet these requirements is dependent on the quality of the design criteria.

The methods for predicting movement speeds on stairs range from simple algebraic equations to more complex computer simulations. The data used in these models tends to be based on either averages or applying data collected from individuals in isolation to members of the larger populations.

These models are then used to predict the egress time for a given scenario. The predictions are needed to establish an RSET value that is less than the ASET value for a given fire scenario. For tall buildings, this requires an understanding of how people actually move while on the stairs.

Five classes of variables that have been found to play a role in movement speed have been identified. These variables account for the individual characteristics of occupants and how they interact with the building and other occupants.

Despite the existence of numerous variables that affect people movement, calculations typically rely on only density for predicting movement speed. In order to more accurately predict movement speeds on stairs, other variables need to be considered. Even when some additional variables are included, the models are still not very accurate (Peacock, Averill, and Kuligowski, 2009). There are other important considerations that the field has not yet identified. Some of those variables will be identified with this research.

Chapter 2: Previous Studies of Movement Speeds Down Stairs

Several authors have previously conducted studies that looked at movement speeds and human behavior while descending stairs. However, when estimating the movement speed of people, these authors tended to concentrate on the general characteristics of the entire population rather than those of the individuals. The previous studies tended to only consider average values for all observations or individuals in isolation.

Six general types of experiments have been conducted. The first type used observations from fire drills. The second type made observations during normal use. Accounts from people in actual fires are the third type. The fourth type of reported values saw authors combine data from the previous categories to develop their own movement speed calculations. In order to isolate certain key variables, a fifth type of study has examined movement speeds under laboratory conditions. Finally, a group of studies that have used subsets of the data used in this research are included.

Detailed descriptions of the studies are available in Appendix A. This chapter focuses on the speeds that the different authors observed and the key variables that they indicated play a role in movement speeds down stairs. For each of the studies presented, as much data as was possible from the authors' descriptions was given with respect to the physical conditions and interactions of the building and stairs as well as the occupants. Unless otherwise noted, all comments that give explanations for effects are from the authors of the studies.

2.1 Movement Speed Measurements

Speed was determined in the different studies by how long it took individuals to travel a known distance. While the time component of the movement speed is relatively consistent, the distance measurement is not. When the authors described how they calculated it, several different methods were used. In some instances (i.e., Kagawa, Kose, and Morishita, 1985 and Shields, Boyce, and McConnell, 2009) times were given on a per floor basis. However most of the authors instead calculated speed based on a measured distance within the stairs.

When descending stairs in a high-rise building, travel distance in stairs needs to include both travel on landings and treads. The differences in the studies regarding travel distance stemmed from which components were included and, if included, how the travel distance was calculated.

2.1.1 Landing Calculation

Some authors (i.e., London Transport Board, 1958 and Frantzich, 1994) chose to ignore travel on landings. These studies involved only occupants while they were on the treads. Other authors (i.e., Predtechenskii and Milinskii, 1978 and Peacock,

Hoskins, and Kuligowski, 2011) chose to calculate travel distance by assuming that the travel distance on the landing would be twice the stair width. Unfortunately, many other authors (i.e., Pauls and Jones, 1980 and Galea, et al., 2009) did not indicate whether landings were included or not or, if included, how the distance was calculated. The known method used in each study is shown in Table 2.1.

2.1.2 Treads Calculation

All of the studies included occupants traveling along the treads. As with the landings, two different methods were used. First, (i.e., Pauls, 1980 and Daly, McGrath, and Annesley, 1991) travel distance was along the slope of the stairs. Second, (i.e., Fruin, 1971 and Templer, 1992) travel distance was only calculated in the horizontal direction. In many instances, (i.e., Khisty, 1985 and Proulx, 1995) the authors did not indicate which method they used. The known method used for each study is also shown in Table 2.1.

2.1.3 Combined Travel Distance Calculation Method

Of the 42 references involving movement speeds on stairs, only 22 reported how travel distance was calculated for at least one component. The methods used by the different authors are shown in Table 2.1. The remaining 20 references did not indicate how travel distance was calculated on either the landings or treads and thus are not included in the table.

Table 2.1: Travel Distance Calculation Method

Study Type	Study	Landing Method	Treads Method
Compiled	Predtechenskii and Melinskii (1978)	Linear Path	Slope
Real Fires	Galea and Blake (2004)	Linear Path	Slope
Fire Drills	Kratchman (2007)	Linear Path	Slope
Data Subsets	Blair (2010)	Linear Path	Slope
Data Subsets	Peacock, et al. (2011)	Linear Path	Slope
Compiled	Galbreath (1969)	Linear Path	Horizontal
Laboratory	Frantzich (1994)	Not Considered	Slope
Fire Drills	Kagawa, et al. (1985)	Not Considered	Not Considered
Real Fires	Shields, et al. (2009)	Not Considered	Not Considered
Normal Use	London Transport Board (1958)	Not Considered	Not Provided
Fire Drills	Pauls (1971)	Not Provided	Slope
Fire Drills	Pauls and Jones (1980)	Not Provided	Slope
Fire Drills	Pauls (1980)	Not Provided	Slope
Normal Use	Daly, et al. (1991)	Not Provided	Slope
Laboratory	Frantzich (1996)	Not Provided	Slope
Laboratory	Boyce, et al. (1999)	Not Provided	Slope
Compiled	Gwynne and Rosenbaum (2008)	Not Provided	Slope
Normal Use	Ye, et al. (2008)	Not Provided	Slope
Real Fires	Galea, et al. (2009)	Not Provided	Slope
Normal Use	Fruin (1971)	Not Provided	Horizontal
Compiled	Templer (1992)	Not Provided	Horizontal
Laboratory	Fujiyama and Tyler (2004)	Not Provided	Horizontal

2.2 Observed Movement Speeds

With nearly half of the references not providing details about how the travel distance was calculated, direct comparisons between different studies need to be done with caution. As can be seen in Table 2.2, there is a range of movement speeds that have been observed or predicted by different authors (with known horizontal speeds converted to slope speeds based on stair dimensions).

Table 2.2: Observed Movement Speeds

Study Type	Study	Average Speed	Minimums or Maximums
Fire Drill	Pauls (1971)	0.61 to 0.81 m/s	
Fire Drill	Pauls and Jones (1980)	0.44 to 0.66 m/s	0.23 m/s (min)
Fire Drill	Pauls (1980)	0.50 m/s	
Fire Drill	Khisty (1985)		0.64 m/s (norm) 0.70 m/s (drill)
Fire Drill	Kagawa, et al. (1985)	16 s/flr	
Fire Drill	Proulx (1995)	0.52 to 0.62 m/s	
Fire Drill	Proulx, et al. (1995)	0.95 to 1.07 m/s	
Fire Drill	Proulx, et al. (1996)	0.75 to 1.2 m/s	
Fire Drill	Shields, et al. (1997)	0.33 to 1.1 m/s	
Fire Drill	Proulx, et al. (1999)		0.39 to 1.30 m/s
Fire Drill	Kratchman (2007)	0.70 to 0.80 m/s	
Fire Drill	Proulx, et al. (2007)	0.40 to 0.66 m/s	0.17 to 1.87 m/s
Fire Drill	Hostikka (2007)	0.64 m/s	0.5 to 1.5 m/s
Fire Drill	Peacock, et al. (2009)	0.40 to 0.83 m/s	
Normal Use	NBS (1935)	0.45 to 0.65 m/s	
Normal Use	London Transport Board (1958)	0.67 to 0.98 m/s	
Normal Use	Fruin (1971)	0.56 to 1.10 m/s	
Normal Use	Daly, et al. (1991)	0.56 to 0.67 m/s	
Normal Use	Tanaboriboon and Guyano (1991)	0.58 to 0.62 m/s	0.39 to 0.89 m/s
Normal Use	Lee and Lam (2006)	0.48 to 0.65 m/s	0.29 to 0.93 m/s
Normal Use	Ye, et al. (2008)		0.5 to 1.2 m/s
Real Fires	Galea and Blake (2004)	0.2 to 0.7 m/s	
Real Fires	Averill, et al. (2005)	0.2 m/s	
Real Fires	Shields, et al. (2009)	43 to 150 s/flr	
Real Fires	Galea, et al. (2009)	0.29 m/s	
Compiled	Melinek and Booth (1975)	0.5 m/s	
Compiled	Predtechenskii and Milinskii (1978)	0.18 to 0.27 m/s	
Compiled	Templer (1992)	0.45 m/s (horiz)	
Compiled	Smith (1995)		0.1 to 0.9 m/s
Compiled	Proulx (2008)	0.5 m/s	0.76* m/s
Laboratory	Frantzich (1994)	1.0 m/s	0.3 to 1.3 m/s
Laboratory	Frantzich (1996)	0.69 to 0.72 m/s	2.27 m/s (max)
Laboratory	Boyce, et al. (1999)	0.13 to 0.70 m/s	0.11 to 1.10 m/s
Laboratory	Wright, et al. (2001)	0.30 to 0.42 m/s	
Laboratory	Fujiyama and Tyler (2004)	0.60 to 1.30 m/s	

*Indicates value is an average

The average values from Table 2.2 are shown in Figure 2.1. In the instances where speeds were given on a per floor basis, the distance per floor was assumed to be 8 m (Galbreath, 1969). For the horizontal speed, the tread depth and riser height were assumed to be 0.2794 m and 0.1778 m respectively (Pauls, 1984).

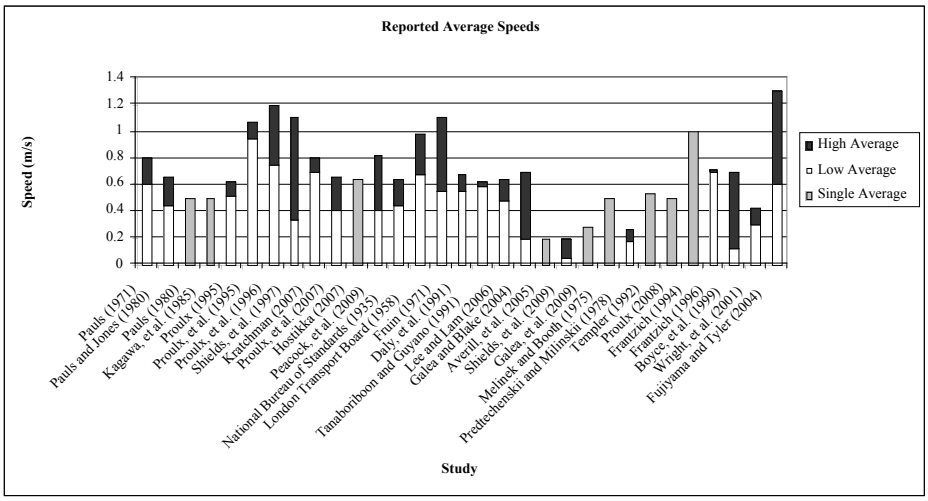

Figure 2.1: Average Speeds in References

There is no one value that authors consistently report for the average speed. While Melinek and Booth (1975), Pauls (1980), and Proulx (2008) recommended using 0.5 m/s, none of the studies where data was actually collected[2] reported averages (or ranges of averages) that fell completely with 20% of this recommended value. Individual data points will lie even further away from this value than averages do.

2.3 Density Measurements

Many of the authors have determined relationships between movement speed and density to better predict movement speeds. As was the case with travel distance, authors have used a variety of methods to calculate density.

Some studies (i.e., Proulx, 1995 and Shields, Boyce, and McConnell, 2009) ignored density entirely. Predtechenskii and Milinskii (1978) calculated density based on the fraction of floor space occupied by individuals. For the other authors that were interested in density (i.e., Galbreath, 1969 and Gwynne and Rosenbaum, 2008), density was calculated based on the number of persons per unit area of floor space. The area used was either on the treads or a combination of treads and landings, yet another variation across studies. The methods used for each component were not consistent to complicate matters even more.

[2] Excluding the compiled studies that only gave rules of thumb or generalized findings

2.3.1 Fluctuations in Density

Most authors did not indicate how they handled whether density was static or dynamic. With two exceptions average values (whether for the entire evacuation or over short durations) were assigned to all occupants. Blair (2010) assumed that the density for occupants was a variable for each individual, and could be calculated based on the number of people in the entire area over multiple floors. Peacock, Hoskins, and Kuligowski (2011) also assumed that density changed with each individual, but the density within a single camera view held constant over multiple floors.

2.3.2 Landing Area

Very few authors provided any information about how they calculated landing areas. Some authors (i.e., Kratchman, 2007 and Proulx, et al., 2007) chose to only use treads. Pauls (1971) used an effective area to account for occupants not normally being in the corners, but no other details were provided. Blair (2010) calculated the area based on the total area of the landings. The methods of authors that indicated how landing areas were calculated are shown in Table 2.3.

2.3.3 Tread Area

As with the landings, many authors did not state how the area of treads was calculated. While some may have chosen to not include treads, with one exception, the other authors that described their method accounted for the horizontal surface of the treads. Kratchman (2007) used the area of the slope of the treads. There was also a difference between whether an effective area should be used (e.g., Pauls 1980 and Daly, McGrath, and Annesley, 1991), accounting for a boundary layer people left to the edge of the stair, or the total width (e.g., Joint Committee, 1952 and London Transport Board, 1958). When known, the method used in each study is provided in Table 2.3.

Table 2.3: Total Area Calculation Methods

Study Type	Study	Landing Area	Tread Area
Fire Drill	Pauls (1971)	Effective	Total
Data Subsets	Blair (2010)	Total	Effective
Compiled	Galbreath (1969)	Total	Total
Data Subsets	Peacock, et al. (2011)	Total	Total
Fire Drill	Kratchman (2007)	Not Considered	Effective
Normal Use	Tanaboriboon and Guyano (1991)	Not Considered	Not Considered
Fire Drill	Proulx (1995)	Not Considered	Not Considered
Fire Drill	Proulx, et al. (1995)	Not Considered	Not Considered
Fire Drill	Proulx, et al. (1996)	Not Considered	Not Considered
Laboratory	Boyce, et al. (1999)	Not Considered	Not Considered
Laboratory	Wright, et al. (2001)	Not Considered	Not Considered
Laboratory	Fujiyama and Tyler (2004)	Not Considered	Not Considered
Real Fires	Galea and Blake (2004)	Not Considered	Not Considered
Real Fires	Averill, et al. (2005)	Not Considered	Not Considered
Normal Use	Lee and Lam (2006)	Not Considered	Not Considered
Real Fires	Shields, et al. (2009)	Not Considered	Not Considered
Fire Drill	Proulx, et al. (2007)	Not Considered	Not Provided
Fire Drill	Pauls (1980)	Not Provided	Effective
Normal Use	Daly, et al. (1991)	Not Provided	Effective
Compiled	Gwynne and Rosenbaum (2008)	Not Provided	Effective
Compiled	Joint Committee (1952)	Not Provided	Total
Normal Use	London Transport Board (1958)	Not Provided	Total

2.3.4 Combined Landing and Tread Areas

Only 22 of the 42 references provided information about how density was calculated. And, within this subset, the information provided by half of the studies was that they did not measure it. Only four authors that included landings gave any indication as to how it was calculated. Ten authors (including the four that gave information about landing areas) included information in their studies that indicated how they measured areas on the treads.

2.4 Observed Densities

As shown in Table 2.3, a majority of the authors did not clearly indicate how density was measured. Table 2.4 shows the density values reported by the different authors.

Table 2.4: Observed Densities

Study Type	Study	Average Density	Reported Minimums or Maximums
Fire Drill	Pauls and Jones (1980)	1.38 persons/m^2	
Fire Drill	Pauls (1980)		2.0 persons/m^2 (optimum)
Fire Drill	Khisty (1985)	1.38 persons/m^2 (normal) 1.40 persons/m^2 (emergency)	
Fire Drill	Kagawa, et al. (1985)		< 3.0 persons/m^2
Fire Drill	Proulx, et al. (1999)	1.00 to 2.05 persons/m^2	
Fire Drill	Proulx, et al. (2007)	1.56 to 1.60 persons/m^2	2.30 persons/m^2
Fire Drill	Hostikka (2007)		0.5 to 2.5 persons/m^2
Normal Use	National Bureau of Standards (1935)	1.3 to 2.6 persons/m^2	2.8 persons/m^2 (maximum)
Normal Use	London Transport Board (1958)		1.6 persons/m^2 (optimum)
Normal Use	Fruin (1971)	0.72 to 1.08 persons/m^2	0.54 persons/m^2 (end of free-flow) 2.70 persons/m^2 (maximum)
Compiled	Melinek and Booth (1975)	2.2 persons/m^2	
Compiled	Predtechenskii and Milinskii (1978)		0.01 to 0.92 m^2/m^2
Compiled	Smith (1995)		< 4.0 persons/m^2
Compiled	Proulx (2008)		0.54 to 3.2 persons/m^2
Compiled	Gwynne and Rosenbaum (2008)		0.54 to 3.8 persons/m^2
Data Subsets	Blair (2010)	0.886 to 1.329 persons/m^2	0.019 to 3.653 persons/m^2

The range of densities reported in the different references are shown in Figure 2.2 with average or optimum values shown where the authors did not provide the complete range of values.

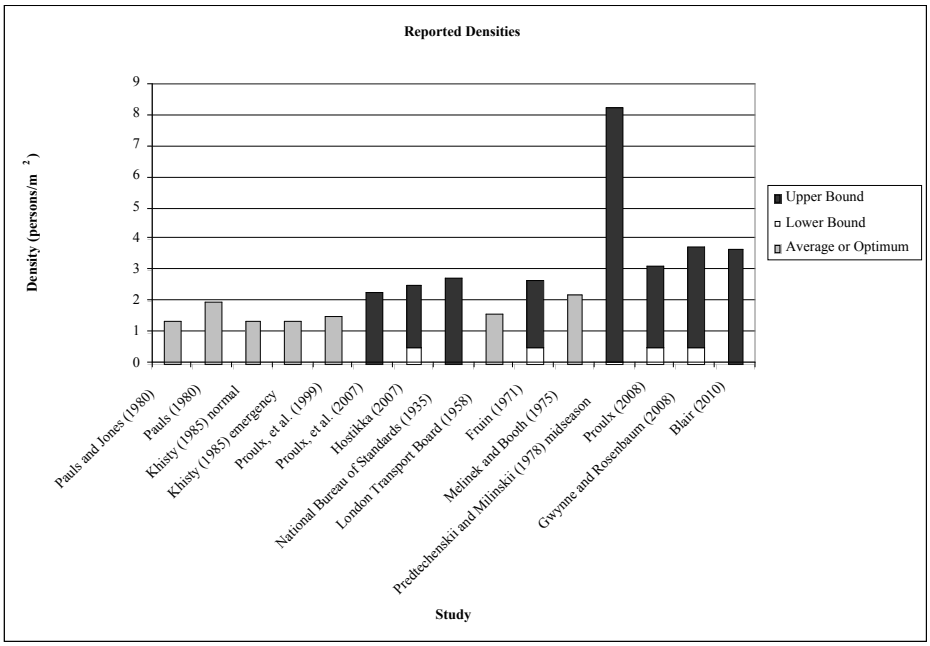

Figure 2.2: Reported Densities in References

As was the case with velocities, there was little agreement between the authors as to what characteristic densities are. This was evident in the reported average values as well as in the minimum, maximum, and optimum values.

2.5 Equations

Despite differences in the reported movement speeds and densities, many of the authors have provided data or proposed equations to predict movement speeds based on density. These equations are shown in Table 2.5.

Table 2.5: Movement Speed Formulas

Study Type	Study	Formula	
Fire Drill	Pauls (1980)	$s = 1.08 - 0.29 \cdot D$	(2.1)
Fire Drill	Khisty (1985)	$s = 0.864 - 0.187 \cdot D$ (normal)	(2.2)
		$s = 0.798 - 0.177 \cdot D$ (emergency)	(2.3)
Fire Drill	Shields, et al. (1997)	$s = 1.27 - 0.30 \cdot D$ (ahead of wheelchair)	(2.4)
		$s = 1.69 - 0.05 \cdot D$ (behind wheelchair text)	(2.5)
		$s = 1.69 - 0.50 \cdot D$ (behind wheelchair graph)	(2.6)
Normal Use	Fruin (1971a)	$s = 0.650 - 0.097 \cdot D$	(2.7)
Normal Use	Daly, et al. (1991)	$s = \frac{1}{1.5 + 0.3 \cdot (f/1.14)^{2.7}}$ *	(2.8)
Normal Use	Ye, et al. (2008)	$s = 0.996 - 0.159 \cdot D$ *	(2.9)
Compiled	Predtechenskii and Milinskii (1978)	$s = (112 \cdot d^4 - 380 \cdot d^3 + 434 \cdot d^2 - 217 \cdot d + 57) \cdot (0.775 + 0.44 \cdot e^{(-0.39 \cdot d)} \cdot \sin(5.61 \cdot d - 0.224))$	(2.10)
		$s = 1.0308 \cdot x^2 - 1.7867 \cdot x + 0.86$ (normal)*	(2.11)
		$s = 0.0159 \cdot x^2 - 0.2443 \cdot x + 1.04$ (emergency)*	(2.12)
Compiled	Pauls (1984)	$s = 1.08 - 0.29 \cdot \left(\frac{1}{((b - \delta)/P) \cdot y} \right)$	(2.13)
Compiled	Smith (1995)	$s = 0.9 - 0.13 \cdot D$ *	(2.14)
Compiled	Gwynne and Rosenbaum (2008)	$s = k - 0.266 \cdot k \cdot D$	(2.15)

*Portions of the equations extrapolated from other information in the text

where:

s=speed (m/s)
D=density (persons/m^2)
d=density (m^2/ m^2)
f=specific flow (persons/m-s)
k=1.00 (m/s) for 19.0 cm riser, 25.4 cm tread
=1.08 (m/s) for 17.8 cm riser, 27.9 cm tread
=1.16 (m/s) for 16.5 cm riser, 30.5 cm tread
=1.23 (m/s) for 16.5 cm riser, 33.0 cm tread
b=stair width (m)
δ=boundary layer (m)
P=population (persons)
y=depth (m)

All of the equations for movement speed based on density are shown in Figure 2.3.

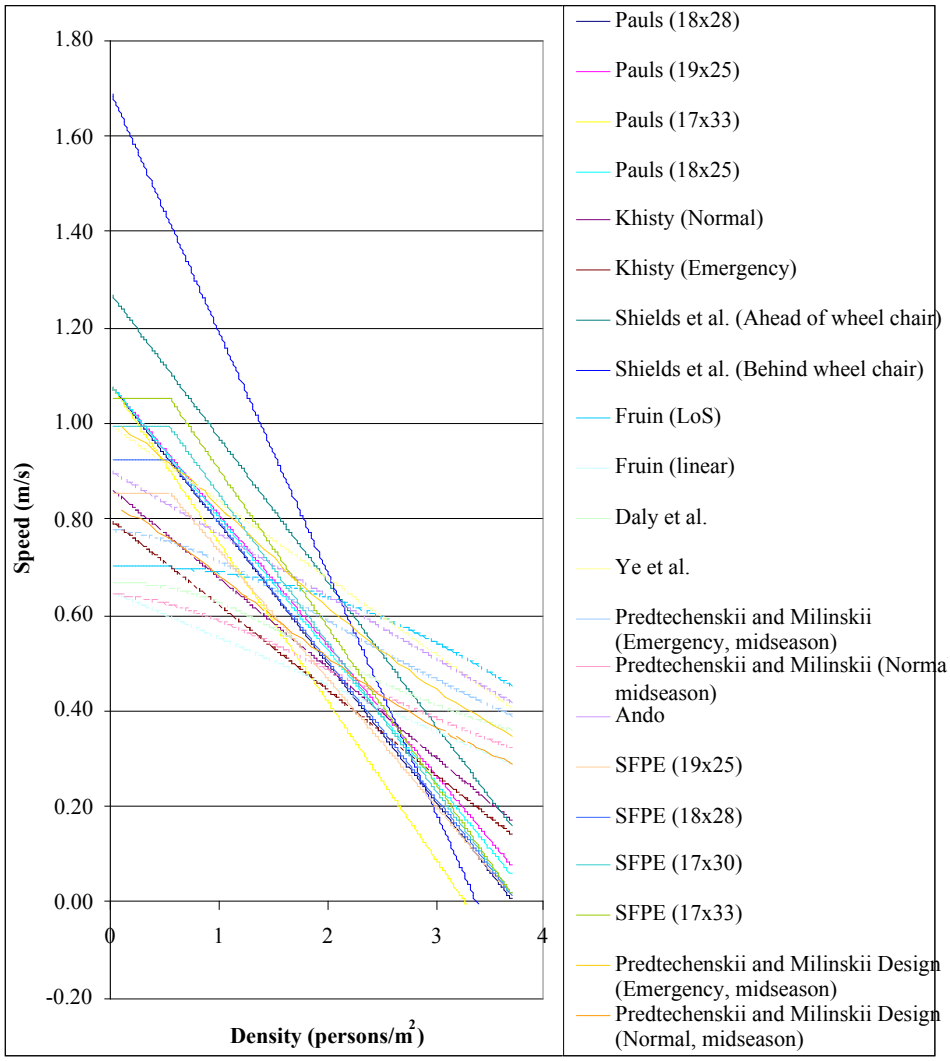

Figure 2.3: Movement Speed Equations Based on Density

Even for densities where the different equations are the closest to converging, there is still a range of predicted speeds that is greater than 0.3 m/s. Other variables not accounted for in the formulas could explain the wide variation in proposed equations.

2.6 Additional Variables

In some of the referenced studies, authors reported other variables that were present. In some instances, the authors stated that these other variables could explain some of the variation in the data. All of the variables that the different authors identified are discussed in the following section.

2.6.1 Perception of Drill

The behavior of occupants under drill conditions could be different than how they would behave under real fire emergencies. If differences exist, this could impact movement speeds.

Early researchers believed that there was a difference in movement speeds based on a sense of urgency. The National Bureau of Standards (1935) found that occupants at a transit station moved faster than those at a theater. However other variables were not controlled. The Joint Committee (1952) stated that occupants would behave in an urgent manner during an actual emergency, but this was not quantified. Predtechenskii and Milinskii (1978) assumed that movement speeds near a fire would be greater than those further away (where speeds would be similar to normal movement speeds).

Later researchers conducted surveys of drill participants to determine what perceptions those people had as well as how the individuals that thought it was a drill behaved compared to those that thought it was an actual emergency. Khisty (1985), in exit interviews with a random sample of at least 10% of the occupants after each drill, found that 80% of occupants thought that the drills were real incidents. Thus, for those individuals, their behavior under drill conditions would be the same as under a real emergency with remote cues. Proulx, Kaufman, and Pineau (1996) surveyed participants in two fire drills and asked them about their perceptions of the drill as well as actions that they undertook. In the first drill, 21.2% believed that it was an actual emergency and, in the second drill, 23.2% believed it was an actual emergency. When comparing reported actions between the occupants that believed it was not a drill and those that did, there were no statistical differences in actions taken in the first building. In the second building, the occupants that thought it was an actual emergency were statistically more likely to save files and turn off their computers.

2.6.2 Stair Width

Two different authors (Khisty, 1985 and Frantzich, 1996) found that the width of the stairs did not alter movement speeds. Khisty (1985) also stated that localized

constrictions similarly did not alter movement speeds, but no description was given to define what was meant by a localized constriction.

2.6.3 Stair Conditions

There were three types of conditions within the stairs that were identified by authors as causing changes in movement speed. The first were environmental factors in real fire events that slowed down occupants or forced them to choose an alternate route. The second type of condition relates to changing densities. Finally, the riser height and tread depth were found to alter movement speeds.

Galea and Blake (2004) and Shields, Boyce, and McConnell (2009) reported that water in the stairs hindered movement speed. Furthermore, Shields, Boyce, and McConnell found that strong odors made people leave the stair.

During some evacuations (i.e., Pauls and Jones, 1980; Kagawa, Kose, and Morishita, 1985; Blair, 2010), densities increased at intermediary floors and decreased at lower floors. The authors did not provide explanations as to what caused the density to increase on certain floors and not on others. These increases in density corresponded to locations at which the movement speeds decreased.

As for movement speeds changing due to tread dimensions, Predtechenskii and Milinskii (1978) stated that speeds on very steep stairs were less than those on more gradual inclines. Pauls (1984) theorized that movement speeds would change (within certain limits) depending on the riser height and tread depth. These assumptions were used to develop the equations presented by Gwynne and Rosenbaum (2008).

2.6.4 Exit Selection

Typically, occupants were found to use a well-known egress path (Pauls, 1980; Proulx, 1995; Proulx, Kaufman, and Pineau, 1996; Shields, et al., 1997). While Proulx, et al. (1995) reported occupants using the nearest exit, they did not indicate if there was a difference in familiarity between the exits. In some instances this led to an unequal usage of the different stairs as closer stairs were bypassed. The more commonly used stairs then had slower movement speeds than the lighter used stairs.

2.6.5 Weather

In most studies, the effects of weather were not considered. Two studies did make observations about the effects of weather on movement speeds. In the first, during cold or wet weather, occupants wearing coats were found to have a decrease in flow of approximately 6% (Pauls, 1980). On the other hand, one drill observed by Proulx, et al. (1995) was conducted during winter weather and the speeds were slower, but not significantly slower, than those drills conducted during warmer weather.

2.6.6 Groups

In some studies, groups formed and changed composition as occupants descended (i.e., Galea and Blake, 2004). Galea and Blake found that most (88% and 90%) of the occupants they studied from the World Trade Center evacuation traveled in groups. Other authors also identified groups being present in their studies.

Two different types of groups were identified in the different studies. The first were groups that formed due to either the building evacuation plan or by occupants staying with previous acquaintances (i.e., Pauls, 1971; Kagawa, Kose, and Morishita, 1985). In residential settings, occupants were found to evacuate in small groups with large spaces between groups (Proulx, 1995; Proulx, et al., 1995). The second types of groups formed spontaneously as occupants descended. Both types can be seen in a single evacuation (i.e., Shields, Boyce, and McConnell, 2009). Some authors (Kratchman, 2007) indicated groups being present, but did not indicate how they formed.

Proulx et al. (1995) reported that occupants traveling in groups moved slower than individuals by themselves (1.00 compared to 1.18 m/s) and that the speed of the groups was at the speed of their slowest member. Unfortunately, the authors did not explain how they reached this conclusion that the speed was of the slowest member rather than the group dynamics causing the slowest people to go faster than they usually would, but still slower than the average person.

2.6.7 Occupant Spacing

As occupants descended the stairs, some authors indicated patterns in how they were spaced. Pauls (1971) and Kagawa, Kose, and Morishita (1985) found that occupants tended to walk down in a staggered file or two abreast with an open tread between pairs. Thus, the minimum spacing was one person per tread when two exit lanes were available. Similarly, Fruin (1971) found that occupants tended to be 4 to 5 treads apart during normal movement and that the maximum density (where the flow came to a stop) was when there was one person on every other tread. Proulx, et al., (2007) observed occupants at higher densities moving in a staggered file as had Pauls (1971) and Kagawa, Kose, and Morishita (1985). At lighter densities, Proulx, et al. (2007) found that occupants tended to stay to the right. The staying to one side phenomenon was also found by Galea and Blake (2004) for able-bodied occupants in the World Trade Center. One study (Peacock, Hoskins, and Kuligowski, 2011) used a multiple regression model and found that which side of the stair occupants were on was significant in determining their movement speed.

One author attempted to quantify the line-of-travel distance between occupants. Frantzich (1996) found that the minimum interpersonal spacing was usually 0.37 m (free-flow speed was possible at this distance), but, when instructed to be as close to the person ahead as possible, the minimum spacing was 0.25 m.

Aside from the spacing between occupants, how they were spaced on a tread was also observed by some authors. Occupants were found to leave a boundary layer, but to also stay near the handrails while descending stairs (Pauls, 1980). Previous work (i.e., London Transport Board, 1958 and Joint Committee, 1952) had included the entire width of the steps, in terms of exit lanes, when calculating the density.

2.6.8 Gender

Studies were divided as to whether or not movement speeds were significantly different depending on gender. Proulx, et al. (1995) found gender to not be significant in movement speed in two of three buildings, but males were statistically faster in the third building. In only one building in one study (Proulx, Kaufman, and Pineau, 1996) were females found to be statistically faster, but, for the other building in the study, males had a greater, but not significantly so, average speed. Kratchman (2007) found that males moved faster, but the difference was not significant. Hostikka, et al. (2007) and Peacock, Averill, and Kuligowski (2009) found that there was no difference in movement speed based on gender.

On the other hand, Fruin (1971) found that males moved faster than females. And Peacock, Hoskins, and Kuligowski (2011) found that males moved statistically faster than females when other variables were controlled for.

In some instances, gender was also found to influence occupants' behavior. Pauls and Jones (1980) found that there was a "ladies first" deference as occupants entered from a given floor. Proulx, Kaufman, and Pineau (1996) found that females in one building required less pre-evacuation time. Kratchman (2007) found that females were nearly three times more likely to be carrying objects than were males.

2.6.9 Age

The exact age ranges that authors used varied from one study to another. In some instances (i.e., Proulx, Kaufman, and Pineau, 1996) speeds were not found to be dependent on age. There were other authors that did find differences in movement speed based on age.

Proulx (1995) found that very young and very old occupants tended to move slower than the other occupants and Proulx, et al. (1995) found that seniors moved significantly slower than other age groups. Similarly, Fruin (1971) found that speed decreased for older occupants.

Fujiyama and Tyler (2004) reported that older and younger subjects, when asked to descend at a normal pace, did not move at statistically different speeds. However, when the subjects were asked to descend as quickly as possible, the younger subjects went statistically faster.

Proulx (1995) also found differences in behavior based on age. Specifically, older individuals tended to begin their evacuation sooner. However Proulx, et al. (1995)

found that seniors were not significantly different than the rest of the population in two buildings and required more time in the third.

2.6.10 Carrying

Two studies attempted to quantify the change in movement speed based on whether the occupants were carrying items or not. Proulx (1995) found that occupants carrying items tended to move at the same speed as other occupants. However the author noted that they tended to behave in a more cautious manner. Peacock, Hoskins, and Kuligowski (2011) used a multiple regression model and found that occupants carrying items went significantly slower than those that were not when the other variables were held constant.

2.6.11 Handrail Use

Using handrails, in at least two studies, was found to impact how occupants used the stairs. Proulx, et al. (2007) observed 70 to 90% of occupants on the upper floors using handrails (the percentage decreased lower in the building). The use of handrails caused occupants to progress in single-file. Boyce, Shields, and Silcock (1999) found that 94% of unassisted disabled subjects used the handrail.

In one study that attempted to quantify how handrail use alters movement speed, Peacock, Hoskins, and Kuligowski (2011) found no difference in movement speeds between occupants that used or did not use handrails.

2.6.12 Fatigue

Some authors suggested that fatigue was present (i.e., Shields, et al., 1997) and others suggested that it was not (i.e., Khisty, 1985). However none of the authors explained how they reached this conclusion.

In other instances, fatigue was determined based on general observations. Proulx, et al. (1999) stated that occupants that exited below the main floors of their study moved faster in part due to less fatigue, but this was not quantified. Galea and Blake (2004) reported some instances of fatigue and that this was typically caused by footwear. Galea, et al. (2009) reported occupants stopping when their companions needed to stop due to fatigue.

Quantification of how fatigue would slow down occupants was based on both assumptions by the authors and by statistical analysis. The Joint Committee (1952) believed that occupants would slow down by 8% for every 3.05 m (above 6.10 m) if occupants did not have to slow down due to merging flows. Peacock, Averill, and Kuligowski (2009) found that travel distance was significant when they used a multiple regression model to predict movement speeds. On the other hand, Peacock, Hoskins, and Kuligowski (2011) found that travel distance was not significant in predicting movement speed.

2.6.13 Body Size

Most studies did not consider the effect of body size on movement speed. The two that did, (Fujiyama and Tyler, 2004 and Galea, et al., 2009) found no differences in speed based on body mass index.

2.6.14 Pre-Evacuation Time

No studies have looked directly at pre-evacuation time and movement speeds on stairs. Five studies, (Proulx, 1995; Proulx et al., 1995; Proulx, Kaufman, and Pineau, 1996; Proulx, et al., 2007 and Shields, et al., 1997) reported pre-evacuation times that varied from 0.6 to 9.7 minutes depending on the building being studied. Proulx (1995), Proulx, et al. (1995), Proulx, Kaufman, and Pineau (1996), and Shields, et al. (1997) measured the time after the alarm to when occupants left their apartment, office, or room. The three articles written by Proulx referred to this time as the "time to start". Proulx, et al. (2007) observed when occupants entered the stairs and assumed that time to start or pre-evacuation time (the authors stating that the two terms were equivalent) would be 10 to 15 s less than this value.

None of the studies made a connection between pre-evacuation time and movement speed. However Proulx, Kaufman, and Pineau (1996) found that women had shorter times than men in the building where women moved faster, but the authors did not provide the decreased pre-evacuation time as a possible reason for the greater speeds.

In their regression model for predicting movement speeds, Peacock, Averill, and Kuligowski (2009) found that pre-evacuation time was significant. However, in the regression model by Peacock, Hoskins, and Kuligowski (2011), pre-evacuation time was not significant. In both instances, pre-evacuation time was measured based on when occupants entered the stairs.

2.6.15 Passing

The studies disagreed as to how and whether passing would take place. Pauls (1980) found that occupants would pass slower or disabled occupants as they descended. He claimed that these occupants did not alter the overall flow since occupants, once past the slower moving occupant, were able to fill any gaps in the flow that had been created. However Shields, et al. (1997) found that occupants were unwilling to pass a wheelchair user being assisted down the stairs despite there being approximately 40 cm to do so and Proulx, et al. (2007) found that occupants using the handrail or with disabled occupants ahead of them were not passing slower moving occupants.

If occupants did pass, there was further disagreement as to whether it was the slower individuals being passed or the faster individuals passing that changed their path. Shields, Boyce, and McConnell (2009) found that some interviewees had engaged in passing behavior while others had allowed others to pass them. In one instance, a group of people formed behind a slower moving occupant and chose not to pass. Kratchman (2007) observed occupants engaging in passing behavior, with faster

moving individuals moving to the outside. Lee and Lam (2006) observed some individuals weaving through the crowd and passing other individuals. On the other hand, Hostikka, et al. (2007) observed that passing behavior occurred when slower moving individuals moved to the side to allow others to pass them. Galea and Blake (2004) reported able-bodied occupants staying to one side to allow injured occupants to pass using the other side of the stair. Galea, et al. (2009) reported occupants stopping to allow others to pass them. Other studies (i.e., Frantzich, 1996; Ye, et al., 2008) observed some occupants engaging in passing behavior, but did not indicate how the dynamics occurred.

2.6.16 Merging

Three different types of merging are possible. In the first, occupants in the stairs defer to occupants entering the stairs (Pauls and Jones, 1980; Proulx, Kaufman, and Pineau, 1996 and Shields, Boyce, and McConnell, 2009). In the second, occupants on the floors defer to those already in the stair (Hostikka, et al., 2007). The third type is where neither defers and the occupants on the floor and already in the stair split evenly. Kagawa, Kose, and Morishita (1985) had occupants report (from different floors) that there were instances where the occupants in the stairs would not let occupants from the floors enter and that there were instances where occupants entering from the floor caused severe disruptions to the flow in the stairs. As occupants merged into the stair, the flow would slow down or become stagnant (Proulx, et al., 2007).

2.6.17 Counterflow

Some early research (London Transport Board, 1958) indicated that counterflow did not have an impact on movement speed. More recent studies (i.e., Galea and Blake, 2004; Kratchman, 2007; Lee and Lam, 2006; Peacock, Averill, and Kuligowski, 2009) have found the opposite to be true. Furthermore, Daly, McGrath, and Annesley (1991), when adjusting flows based on factors developed for level surfaces, found that the flows on the stairs were still less than expected when counterflow was present. As for the dynamics of counterflow, Kratchman (2007) noted that, to accommodate the counterflow, occupants were observed to move to the right.

2.7 Summary

All of the studies previously presented made observations about movement speeds down stairs. The methods used in calculating these speeds were not consistent and the values varied by large amounts. In an effort to explain the disparity between different observations, several authors found that movement speed was dependent on density. Once again, the method for calculating this variable was not consistent. Multiple equations were developed where speed decreased with density, but the values predicted by the different equations for specific densities are dissimilar. Some authors then attempted to examine if other variables were responsible for the differences in movement speeds.

Chapter 3: Methods

The research in this study analyzes the movement speeds of individuals on stairs in high-rise office buildings during egress drills conducted by the National Institute of Standards and Technology (NIST). These drills took place during different times of the year and in different geographic areas of the United States.

The analysis of the buildings was conducted in several phases in order to build an understanding of the underlying principles. The first phase of the building analysis focuses on a single building in which the significance of several variables can be explored due to long travel distances and low density. The second phase focuses on buildings in which the density is greater.

3.1 Drill Data

Systematic video footage of stairwell evacuations during actual fire emergencies is not known to exist. Thus the decision was made to use fire drill data. While no known studies have looked at how movement speeds differ between actual emergencies and drills, Proulx, Kaufman, and Pineau (1996) found that, during a drill, the only difference in actions between individuals that thought it was a drill and those that thought it was an actual emergency was that those who thought it was an actual emergency were more likely to save files and shut down their computers. Those actions require more time and thus the occupants were not feeling a need to evacuate as quickly as they possibly could.

Predtechenskii and Milinskii (1978) stated that occupants, once removed from the immediate effects of the fire, moved at normal speeds. Furthermore, Averill, et al. (2005) and Shields, Boyce, and McConnell (2009), when studying evacuations during an actual emergency found that occupants were altruistic and patient. There were no indications that occupants were behaving differently than drills described by other authors (i.e., Galea, et al., 2009). Thus, there are no known differences in behavior whether during a drill or an actual emergency evacuation.

3.2 Building Selection

The data in this study comes from Kuligowski and Peacock (2010). Multiple buildings from across the United States were selected in order to not have the findings limited to one region of the United States. All of the drills were conducted during normal working hours to ensure that a relatively large population was present. Furthermore, they were all conducted in high-rise office buildings. These buildings consisted of primarily adult populations that were working at or visiting the building at the time of the drills; this resulted in few observations of very young or very old individuals. This restriction precluded the observation of occupants in their residences as well.

As noted in the previous chapter, most of the previous studies of people movement on stairs have dealt with working and/or adult populations. Thus, the results from this current study can be directly compared to the previous works. Also, because the previous studies have not examined individual variables (as defined in Chapter 1), restricting the data to a more homogeneous sample will limit the interference from other variables. Once a baseline of how to predict individual descent rates has been established, then other population groups can be examined to see if they behave in similar ways.

3.3 Egress Component Selection

This study will focus on only one component involving people walking down stairs. Some of the NIST data contains segments where individuals walked down stairs as well as along transfer corridors. For consistency across the data, these segments are excluded from the analysis because it is not possible to split the times between the two components.

Two different density levels are studied. The first will be a lower density case where the stairs are, on average, Level of Service either A or B as defined by Fruin (1971). These are situations where individuals tend to be able to move at their own basic pace (or at the pace of another individual that they have adequate room to pass, but choose not to). However platoons can form that create higher densities for a limited number of occupants. This phase of the analysis will allow an examination of data when individuals are not impeded to the point of being forced to stop on the stairs. Next, stairs with a higher density, Level of Service D or E being observed, are used to demonstrate that the significant variables from the simplified case are important in the more complex case.

3.4 Experimental Set-Up

For the buildings approximately up to 30 stories in height, cameras were usually placed at every other level starting from the level of discharge. Cameras captured the landing area and, typically, three treads leading to and from the landing. All of the drills were held on the workweek during normal working hours.

Building 6 was used for the initial analysis. It was a 61 story building (57 occupied levels) on the west coast of the United States. There were multiple transfer corridors and places where occupants could change which stair they were using. Cameras were typically placed every six floors in four stairs (with two of the stairs having a landing that could be viewed by a single camera on some levels). There were 30 cameras used for data collection.

For the three buildings used in the primary analysis, the riser heights were 17.8 cm and the tread depths were 27.9 cm in Buildings 4 and 5 and 27.3 cm in Building 8. Building 4 was located on the west coast, was 24 stories tall, and had cameras located on every other floor, with two instances where cameras failed to work properly. With

two stairwells observed within the building, this resulted in twenty-one cameras that provided data. Building 5 was also located on the west coast, but it was only 10 stories tall. There were two stairwells observed using a total of ten cameras for collecting data. Building 8 was 30 stories tall (numbered to 31 and omitting 13) and was located in the eastern part of the United States. Thirty cameras were used in two stairwells, but one of the cameras failed to work properly resulting in twenty-nine cameras with usable data.

In compliance with the Institutional Review Board (IRB) at NIST, the videos were recorded in mosaic mode to prevent identification of individuals. Figure 3.1 shows a comparison of a normal image and one that has a mosaic filter applied to it.

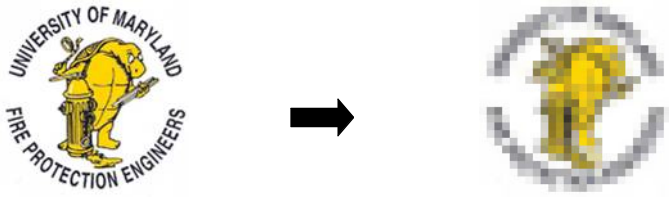

Figure 3.1: Image in Regular and Mosaic

As can be seen, fine details of an individual's appearance cannot be seen. However, it is possible to determine if the individual is carrying something, their gender, and a limited number of additional individual variables.

Video cameras were clamped onto the underside of the stairways. For each landing that was being observed, one camera was typically placed to capture a minimum of three treads descending to the landing and three treads descending from the landing. In order to synchronize the cameras, a stopwatch was recorded at the start of each recording. This stopwatch time, along with the alarm sounding from the video, were used to provide a common reference for all of the cameras. When data was extracted, the local time from the videos was adjusted to the global, synchronized time. Thus, it was possible to determine the time difference from when a person was recorded on the first camera to when he or she was observed on the second camera.

The width and depth of the treads as well as the riser height were measured and recorded before each drill. Also, whether the stair was sinistral or dextral was recorded.

The data was extracted by hand from the videos and released to the public in excel spreadsheets. Consistency checks were made to ensure that the different NIST staff extracting the data applied consistent definitions for all of the variables. The author, while an intern at NIST, personally extracted the data for multiple sets of data as well as augmented, checked, and fixed (when needed) the data that was collected by others.

3.5 Data Collection

Five types of evacuation variables have been mentioned previously. For most of the variables, there is a significant lack of data with which to build algorithms. Variables from all types are examined.

3.5.1 Travel Distance and Area

Before predicting movement speed, the method used to measure speed needs to be established. For stairs, the time component of speed is based on the difference in clock time from one observation to the next. However, for the travel distance, as shown in the previous chapter, different authors have used different methods. Because the exact path that an individual takes from one observation to the next might not lie in a straight line, it is important to determine an average travel distance that will be constant for all occupants.

As shown in the previous chapter, there are two basic types of calculations for speeds on stair treads that have been performed. The first uses the horizontal component of the speed. From an overhead camera, it is possible to measure this distance without any additional calculations or considerations. The occupants are assumed to be traveling in a straight line while descending the treads. The speed is simply the horizontal travel distance divided by the difference in the enter and exit times. The main flaw with this method is that it is very dependent on the tread dimensions in that people will move slower in the horizontal dimension when descending stairs that have a greater vertical dimension (Templer, 1975). The second method is to measure the length of travel along the slope of the treads. This method accounts for differences in tread dimensions, but cannot be directly obtained from video footage. To calculate the speed, the distance along the slope needs to be calculated and then divided by the difference between the enter and exit times. With this method as well, occupants are assumed to be traveling in a straight line.

For calculating travel distance, Gwynne and Rosenbaum (2008) gave factors for calculating the distance occupants move on the stair treads when converting from a horizontal component to the slope. The table simply used trigonometric relationships between the two values to determine the factors. They also mentioned that the travel distance on the landings has to be added to this value. In order to determine how long it will take individuals to descend within a building, the landings cannot be ignored. However Gwynne and Rosenbaum (2008) do not give a recommendation on how to calculate that distance.

3.5.1.1 Travel Distance- Linear Method

Predtechenskii and Milinskii (1978) suggest that travel distance for two flights of stairs with two landings (a dogleg stair) can be calculated by:

$$L = \frac{2 \cdot L'}{\cos(\alpha)} + 4 \cdot b \qquad (3.1)$$

where:

L=travel distance
L'=horizontal projection of the length of the inclined path
α=angle of inclination to the horizontal
b=width of the stairs

Equation 3.1 is shown in Figure 3.2.

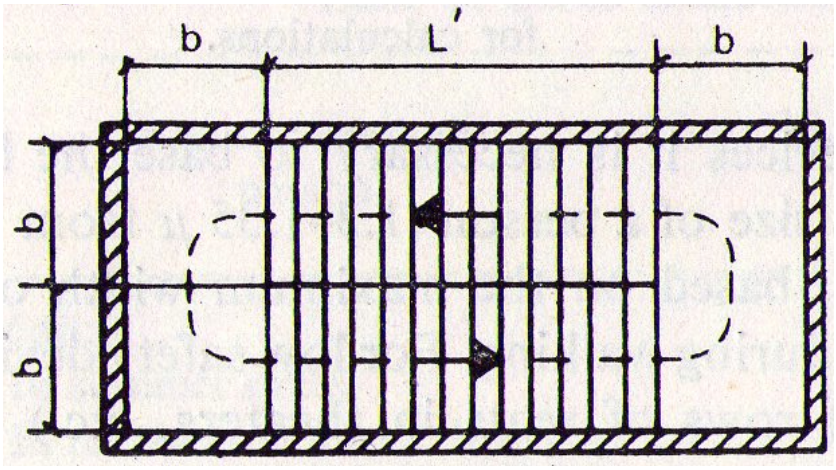

Figure 3.2: Predtechenskii and Milinskii Travel Path

In this case, the L' term and the cosine term are the same trigonometric relationship specified by Gwynne and Rosenbaum and the b term arises from the distance traveled on the landings. The assumed path is that an individual occupant is traveling down the middle of the stairs, walks out onto the landing in a straight line for half of the width of the stairs, make a 90º turn, and then descends. Thus, the distance on a given landing is 2*b and, for a single floor, there are two sets of stairs and landings. Figure 3.2 shows rounded corners on the travel path, but the calculation assumes a sharp turn. If the stairs are wide enough for two exit lanes, then the midpoint assumptions mean that, under heavy density conditions, the width of the stair is maintained on the landing with individual occupants maintaining the same horizontal distance as they had during the travel period on the stair treads. In other words, a pair of occupants would walk onto the landing and make 90º turns so that they maintained the same spacing on the landing as they had on the treads.

This travel distance calculation is commonly used for calculations of travel distance (i.e., Galbreath, 1969 and Peacock, Hoskins, and Kuligowski, 2011). While the assumption is that it is the average path that the occupants will take, Predtechenskii and Milinskii did not explain if this calculation was based on observing actual stair behavior or if it was based on an engineering judgment.

3.5.1.2 Travel Distance- Arc Method

As part of his dissertation, Templer (1975) observed the path that individuals followed while descending stairs. An observer hidden from view traced the path that individuals in isolation followed while descending stairs.

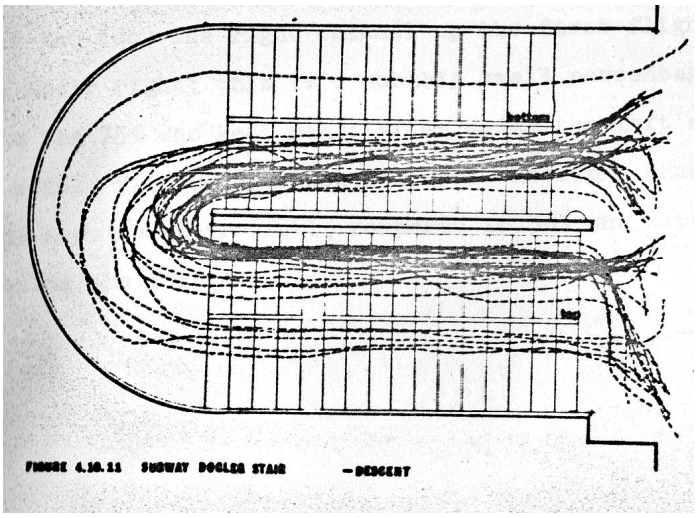

Figure 3.3: 25 Individuals Descending from 6th Avenue

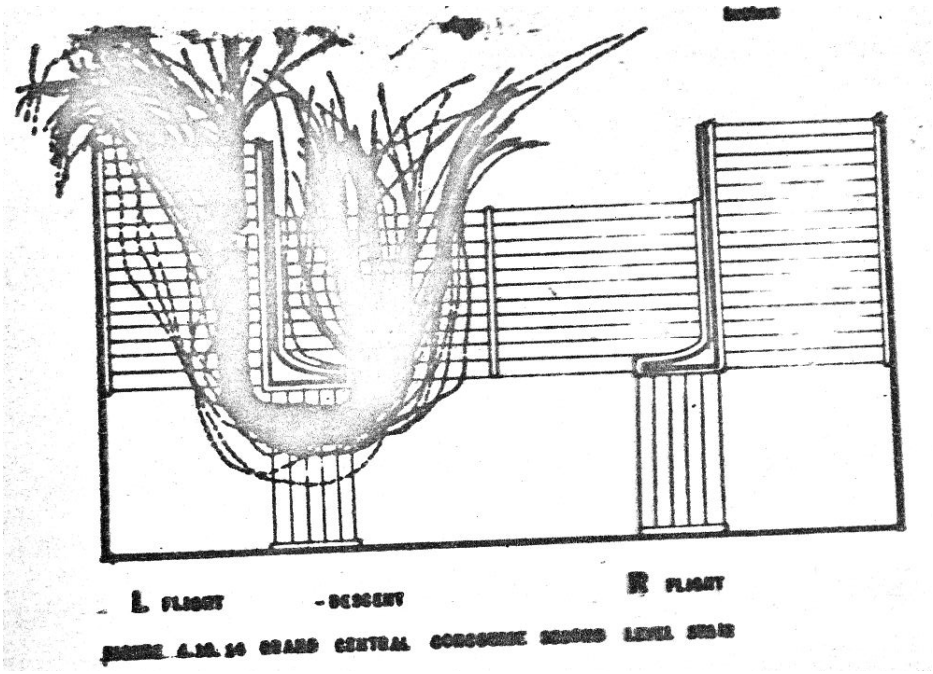

Figure 3.4: 50 Individuals Descending a Sinistral Stair at Grand Central Station

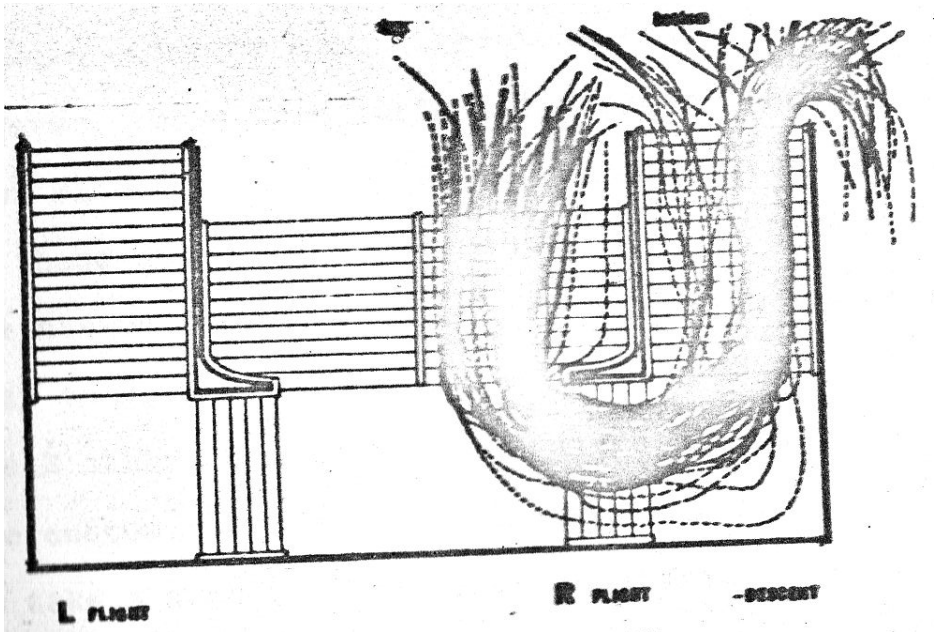

Figure 3.5: 50 Individuals Descending a Dextral Stair at Grand Central Station

Figure 3.3 illustrates the paths of 25 individuals descending a stair from 6th Avenue to a subway station in New York City. Figure 3.4 and Figure 3.5 are each paths of 50 individuals from a matching pair of stairs descending from the main concourse of Grand Central Station in New York City. The specific route chosen seems to be a combination of the custom, in the United States, to stay to the right as well as individuals' desires to take the shortest possible route.

In these observations, occupants were not making 90º turns or even the slightly rounded corners in Figure 3.2; instead, they were walking along an arc. The dextral stair (descending in the counter clockwise direction) has a larger arc than the sinistral stairs (descending in the clockwise direction), but the same (individuals that start on the outside of the stair stay on the outside) would be the case if the Predtechensii and Milinskii (1978) approach were applied.

In a single evacuation of a 30-story high rise building, Hyun-seung, Jun-ho, and Won-hwa (2011) recorded the paths taken by individuals on a sinistral stair. Generally speaking, occupants walked in an arc on the landing and the authors assumed that the path on the landing could be calculated as a semi-circle with an appropriate radius. Occupants were classified as being in an inner (A), middle (B), or outer (C) zone. The zones were defined by arcs of 0, b/3, 2*b/3, and b (where b was adjusted to account for the internal handrail). The authors did not state if any occupants went outside of the outer zone or, if they did, if these occupants were placed in zone C or just not counted. During the drill, 1,057 occupants were observed in zone A, 1,118 in zone B, and 1,588 in zone C. On the higher floors, the zones were used in approximately equal percentages while lower in the building zone C became more likely. When comparing multiple calculations for travel distance on landings, the result that most closely matched the experimental results was the weighted average of

the respective zones. Due to the larger number of zone C occupants, this value was beyond the arc from the midpoint of the stairs (approximately 0.58*b). However the authors did not give an indication as to what caused the shift from equal distribution to favoring the outer lane.

3.5.1.3 Travel Distance- Arc Method Formula

The work by Templer (1975) was collected under single occupant conditions and it is possible that people behave differently as the density increases. However the occupants on the upper floors in the work by Hyun-seung, Jun-ho, and Won-hwa (2011) were not staying to the outside even when multiple people were present. Without an understanding of what caused the behavior to change, more research needs to be conducted to determine if these effects are universal or a function of the characteristics of this particular experiment.

There are some general trends that can be supposed from these studies. Primarily, it appears that occupants maintain formation and travel in an arc rather than on straight-line segments on landings as is shown in Figure 3.6.

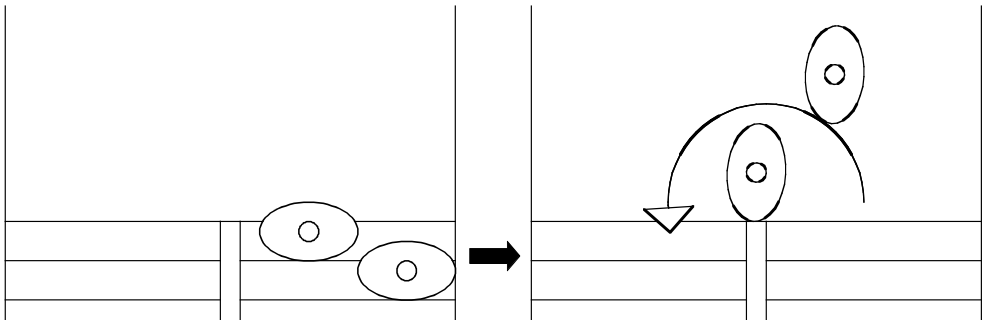

Figure 3.6: Travel Path on Landings

When occupants are alone, Templer (1975) found that they tend to stay to the right and/or take the shortest path. On sinistral stairs, this could lead to a path that is along the inner half of the stairs, but this was not found by Hyun-seung, Jun-ho, and Won-hwa (2011). For a dextral stair, some occupants would be on the inner half while others would stay on the outer half, thus the path followed is more likely to be further from the centerline. However, as density increases, there will be occupants in each exit lane leading to the arc from a central point being the average travel distance. Thus, the assumption will be made that the midpoint of the stairs is the central arc since the assumption is that the entire stair is used uniformly in a higher density situation. Using the middle distance would also be consistent with the Predtechenskii and Milinskii (1978) calculation.

An occupant on the inside would maintain the boundary layer that they had to the stair wall while descending the treads. Assuming that the inner edge of the first flight of stairs and the second flight of stairs were the same, the path would be a semicircle as shown in Figure 3.7.

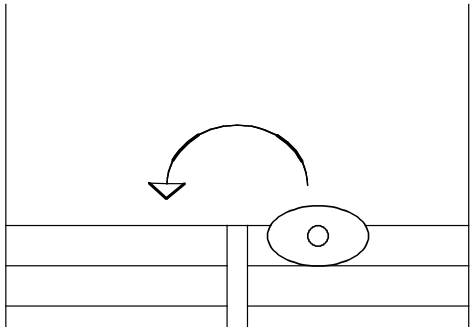

Figure 3.7: Semicircular Path

For a person on the outside lane, the path would also be a semicircle except the radius would be the initial distance of that person to the inner side of the stair. For the average path, the occupant would be at a radius of b/2. For the case where the newel is nonzero (Hyun-seung, Jun-ho, and Won-hwa (2011) assumed a zero thickness newel), a linear section equal to the length of the newel should be included.

Using a similar approach as Predtechenskii and Milinskii (1978), the travel distance for descending one floor (two landings) can be given by:

$$L = \frac{2 \cdot L'}{\cos(\alpha)} + \pi \cdot b + 2 \cdot n \qquad (3.2)$$

where:

L=travel distance
L'=horizontal projection of the length of the inclined path
α=angle of inclination to the horizontal
b=width of the stairs
n=newel width

Equation 3.2 is the travel distance along the arc for the middle of the stairs. Under all conditions, this will be a slightly shorter distance than was found using the previous method. Except for the landing, all distances are the same since Equation 3.1 should have a newel term in it. The landing distance is reduced by the ratio of $\pi/4$.

3.5.1.4 Density

By redefining the paths that individuals follow, the expected locations of individuals will be similarly adjusted. As was previously mentioned, most researchers have found a relationship between speed and density. Even more so than was done with travel distance, a variety of methods have been used to determine density. Unfortunately, some researchers did not explain how they calculated this variable.

Predtechenskii and Milinskii (1978) calculated a dimensionless area and related it to speed. This was based on the horizontal area occupied by people over the possible

horizontal area. For researchers that used a density with units, it was based on a population per unit of floor area (i.e., Pauls, 1980). While the number of people to count is relatively trivial after an area has been established, determining what area to use is more complicated since locations that are rarely, if ever, used by occupants should not be included in the calculation.

Two different methods have been used to define the area of occupants while they are descending stairs. The first method observed occupants while they were only on the treads (i.e., Kratchman, 2007). They defined the area of the treads and counted the number of people that were on the stairs. In some instances (i.e., Pauls, 1980), a boundary layer was applied so that only the area that was actually used by the occupants was counted. For the second method, other authors used observations that included the landings. Pauls (1971) adjusted the area based on people not using the corners of the landing, but he did not show his method for doing so. Blair (2010) calculated the density based on the entire area of stairs and landing over multiple floors between observations. Peacock, Hoskins, and Kuligowski (2011) used only the area within a single camera view (a single landing and a few stairs ascending to and descending from the landing). In both of the latter cases, they used the entire area of the landing. To be consistent with the Predtechenskii and Milinskii (1978) travel distance calculation, the area of the landings should be a rectangle with dimensions equal to $2*b^2$ (or less if boundary layers are applied) since the path of travel is, theoretically, along the centerline of where occupants are located. If the unused area of the landings is sufficiently large, it would make it appear as if the correlations found by the first method are over predicting movement speeds.

Based on the same procedures that led to the new proposed travel distance, a new method for determining the area on landings needs to be developed. Occupants will follow the path on the landing as they had while on the stairs. For occupants on the inside of the stair, there is the same tendency to stay away from the newel. Under heavy density conditions, individuals will maintain the boundary layer that they had with the individuals in the inner lane. On the treads, a boundary layer ∂ is applied to each wall and ∂ is then applied to the area on the landing. Thus, the area on a single landing for the density calculation should be:

$$A = \frac{\pi}{2} \cdot \left((b - \partial)^2 - (\partial)^2 \right) + (n \cdot d) \cdot (b - 2 \cdot \partial) \qquad (3.3)$$

where:

A=area
b=width of stairs
∂=boundary layer
n=number of steps
d=tread depth

This is the area in which occupants are actually expected to use and is illustrated in Figure 3.8.

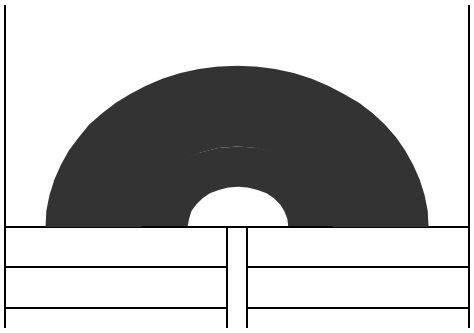

Figure 3.8: Theoretical Area Used

Even under higher density situations, occupants stayed in the same formation as they had been on the treads when on the landings as shown in Figure 3.9.

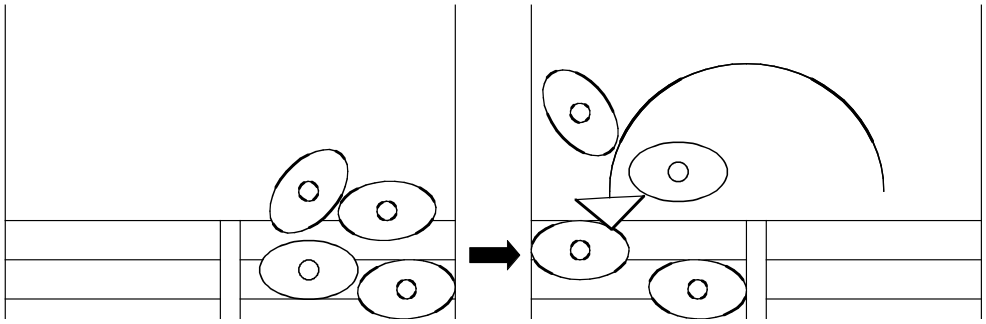

Figure 3.9: High Density Travel Paths

3.5.2 Effective Movement Speed and Normalized Descent Time

As mentioned previously, the local, effective movement speed was determined by the amount of time it took an individual to proceed from one video camera view to the next video camera view. The synchronization of the cameras is needed for this variable. The travel path was determined by use of Equation 3.2.

However, in the analysis presented in Chapter 4, the inverse of speed (a normalized time) is used. The use of time rather than speed is a better fit for the intended use of the data, the method used to collect the data, and, most importantly, the mathematics used to analyze the data in both this study as well as previous works.

For the intended use of the data, as stated in Chapter 1, the goal is to predict RSET where the "T" stands for time. An egress system designer will divide the distance by the speed in order to calculate the time required. Both methods are equivalent in this regard and the change is only a semantic one for this issue. However, when calculating time, coefficients with time in the numerator are more intuitive.

Similarly, the data used in this study and in previous studies observed how long it took occupants to travel a known distance. Time was the variable for the population and the distance was controlled. Once again, the change from the effective speed to

the inverse of speed is merely a semantic change in many respects, but the change aligns the meaning of the coefficients with the methods used to collect the data. The numerical component is the change in the numerator when the denominator is equal to 1, a fixed value. In this case, the distance was fixed and it was the time that was varied.

The instance where the change in speed to the inverse of speed is not semantic is in terms of the mathematics used in interpreting the data. For speed, an individual that travels faster than predicted by X% will travel X% further over a set period of time. With the inverse of speed, the differences between the over and under prediction are the amount of time gained or lost to cover a set distance.

With the inverse of speed, a curve fit similar to the one done by Pauls (1980) or any of the other linear equations presented in Chapter 2, an overestimation in the time by Y and an underestimation by Y would cause the same error. However, when measuring speed over a known distance, an overestimation of time for one occupant and an underestimation for another do not cancel out as shown in Equation 3.4 and its simplified form, Equation 3.5.

$$\frac{L}{t - E_f} - \frac{L}{t} = \frac{L}{t} - \frac{L}{t + E_s} \tag{3.4}$$

$$\frac{1}{E_s} = \frac{1}{E_f} - \frac{2}{t} \tag{3.5}$$

where:

L=length
t=predicted time to travel L
E_f=the amount of time a faster occupant did not need
E_s=the amount of additional time a slower occupant needed

Equation 3.4 is comparing the error in the speed for an occupant that is moving faster than predicted to the equal error of an occupant that is moving slower. Because E_f and E_s are both positive numbers by definition, any possible value of E_f will cause a greater error than the equivalent time for E_s. The effect becomes larger as E_f increases and, if E_f is greater than t/2, then no possible value for E_s will be able to cause a comparable error.

For curve fitting lines, the mathematical techniques create a best fit by minimizing the square of the errors. Thus, when previous researchers have curve fit lines to data, the occupants traveling faster were more influential in shaping the curve.

From a life safety perspective, this is not ideal. If occupants are able to exit in less time than is expected, there are no negative ramifications. On the other hand, if occupants require more time than is expected, the results can be disastrous. Thus

equal (or even greater) weight should be given to the slower population rather than less weight. Thus, the normalized time will be used in the subsequent analysis.

3.5.3 Component Width

The width of the stairs was recorded for each individual building based on the measurements collected earlier. For all buildings, this variable ranged from 1.12 to 1.38 m. The effective width was determined by subtracting a 0.15 cm boundary layer from each side except when the handrails projected into the effective width as recommended by Pauls (1980). This value was used in Equation 3.2 for determining the travel distance and normalized time.

3.5.4 Riser Height and Tread Depth

Code requirements and standard practice do not allow these variables to differ by a large amount in most buildings. As with the stair width, this information was collected previously. The values were found to range from 17.78 to 20.00 cm for the riser height and from 25.40 to 27.94 cm for the tread depth as shown in Table 3.1. The riser height and tread depth were used to calculate the first component in Equation 3.2.

Table 3.1: Riser Heights and Tread Depths

Building	Riser Height (cm)	Tread Depth (cm)
4	17.78	27.94
5	17.78	27.94
6	20.00	25.40
7	19.05	25.40
8	17.78	27.30

3.5.5 Time and Location

The variables related to the set up of the drills were controlled to eliminate potential variables between buildings. The drills were conducted in the afternoon and all of the buildings reported conducting regular drills. All of the buildings were office occupancies. The drills were conducted across the country with buildings 4, 5, and 6 being on the west coast and buildings 7 and 8 on the east coast.

3.5.6 Age and Gender

The buildings were office facilities, so both genders were represented in approximately equal numbers. Thus, gender was included in the data analysis phase. Since the videos were recorded in mosaic mode and detailed personal information of each participant was not collected, it was not possible to approximate age from the videos.

When reviewing the video recordings, each individual was classified as male or female based on secondary sex characteristics as identified during the data extraction phase. This information was recorded on a spreadsheet that contains all observations. An "F" was used for any individual identified as being female and an "M" was used for any individual identified as being male.

3.5.7 Floor of Origin

The floor of origin was recorded for each individual. For the buildings where the cameras were located on every other floor, individuals entering on the floor with the video camera could be seen on the video and were recorded as such; for individuals that were not observed to be entering on a floor with a video camera, they were assigned a location of origin as the floor directly above the one on which they were first observed. For instances where cameras were not located on every other floor, the occupants seen entering on the floor with the video camera were recorded as such; for the occupants that entered on other floors, the middle floor of the floors between cameras was recorded as the location of origin. Each time that the individual was observed, recorded along with the movement speed was the distance traveled since that individual entered the stair.

3.5.8 Pre-Observation Time

Like the floor of origin, this variable was recorded based on when the individual first appeared on a camera. For the occupants that entered on an unobserved floor, the time required to travel to the camera within the stair is included. Furthermore, this definition of pre-observation time includes movement on the floor of origin towards the exit. The authors in Chapter 2 that looked at pre-evacuation time did not include that movement, so these times are greater than would have been reported in those studies. This variable is included more as a measure of delay than an attempt to quantify the time that people required to prepare to evacuate.

3.5.9 Body Size

Body size was a binary variable based on whether the individual occupied more or less than half of the stair width. The image of the individual was visually inspected to see if he or she appeared to be occupying more than half of the egress width. For each individual, this was recorded in the spreadsheet as either a blank (less than half of the egress width) or an "x" (more than half the egress width).

3.5.10 Physical Impairments

With very few exceptions, no physical impairments were observed in the videos collected by NIST. It is very possible that there were individuals that had impairments that did not have physical manifestations that could be observed on the videos. Thus, this variable had to be excluded from the analysis.

3.5.11 Footwear

With the videos in mosaic mode, it was not possible to visually determine what style of footwear each individual was wearing. While audio cues were used, this method was not considered reliable enough for inclusion in this study.

3.5.12 Encumbrances

Encumbrances were noted for each individual at all observations and were recorded as a categorical variable. For each observation, it was recorded as to whether the individual was wearing the encumbrance, had the encumbrance on a shoulder, had the encumbrance in their hands, or if the individual was assisting another occupant. Furthermore, it was recorded if the individual was using his or her right or left hand or shoulder. If the encumbrance variable was found to vary for the individual, the videos were reviewed to verify this change.

3.5.13 Flow Units

To account for interactions, the occupants were subdivided based on behaviors relative to one another. Platoons were identified based on individuals that were within four tread lengths of each other (see the next section for more details on this). Flow units were then identified based on individuals in the same platoon for the adjacent pair of observations. If occupants were engaging in passing behavior, flow units were defined based on whether they were passing or being passed. If occupants were allowing individuals from the floor to enter into the stair, this created another set of flow units.

3.5.14 Effective Density

Density was calculated using two different methods. The first method calculated the number of people per unit area as discussed in Section 3.1.5.4 to calculate the effective density. Specifically, the number of occupants in the observation area on a given floor when the person entered the observation area was recorded. This number was divided by Equation 3.3 to calculate the density on that landing. The same procedure was repeated for the subsequent landing. These two values were then averaged to calculate the density that the individual experienced when traveling between the two floors.

The second method was approximated by the distance from the occupant to the individual ahead of them. This was described as the number of open treads to the individual immediately ahead, up to three treads. If the distance was greater than three open treads, the variable was recorded as a ".". The tread left open assumption corresponds with the intimate distance proposed by Hall (1966) that is a distance that is typically socially unacceptable for Americans. Even outside of the United States this value was found to be the minimum interpersonal spacing by Frantzich (1996). One to two treads beyond this falls within the personal distance that is not socially acceptable for interactions, but is acceptable for the impersonal act of walking down

stairs. Three treads beyond the intimate zone is the start of the social distance and, as such, was initially assumed to be where the pull of others will start to diminish. Also, each occupant having four treads or fewer corresponds to Levels of Service of C and greater (Fruin, 1971). For those levels of service, occupants are not supposed to have extreme difficulty passing and are greatly influenced by the speed of people ahead of them.

For analysis purposes, the distance between individuals had to be determined for the time between the two video camera observations. Each observation was classified as having one or fewer open treads to the next occupant, two open treads to the next occupant, three open treads to the next occupant, or more than three open treads to the next person. If the occupant was at three or fewer treads to the next occupant on both cameras and the two values were different, the smaller value was used in the analysis.

3.5.15 Handrail Use

Handrail use was recorded for each individual at each observation. However, on several cameras, it was not possible to clearly see the outer handrail. In order to avoid large errors associated with the true negatives, this variable will be excluded from analysis.

3.5.16 Exit Lanes

Each occupant was classified as being in the inner exit lane, in the middle of the stair, or in the outer exit lane. Occupants in the inner lane were recorded with an "I"; those in the outer lane were recorded with an "O". If the individual was walking such that their body was crossing the centerline of the stairwell, the person was recorded as "M". Also, if the individual shifted within a single camera view from one position on the stair to a different one, a "/" was included between the sequential designations of positions.

For analysis purposes, the second value on the upper floor and first value on the lower floor were used if the individual changed locations on a given floor. If the individual was in either the inner or outer lane on one video camera and in the middle on the other video camera, the inner or outer lane designation was used. If the individual was in the inner lane for one observation and the outer lane for the other observation, then the individual was recorded as being in the middle.

3.5.17 Counterflow

In Building 4, Stair A and Building 5, Stair B firefighters ascended the stairs during the evacuation. The occupants that they passed were recorded with a binary variable indicating that they experienced counter flow for that portion of their evacuation.

3.5.18 Allowed Entering

Merging behavior was recorded based on if the occupant allowed a different occupant to enter the flow ahead of them. The difference in occupants between individuals from one camera to the next was used if those individuals were within the maximum tread spacing mentioned previously. The two videos were compared and recorded in the spreadsheet the number of individuals that entered in front of the individual in question. This variable was then used in determining flow units as previously mentioned.

3.5.19 Passing

Two different forms of passing were observed. The first was passing where an individual overtook another occupant. The second was when several occupants passed another individual(s). As with merging, this variable was used in defining flow units.

3.6 Data Classification

After the data was extracted from the videos and recorded in spreadsheet form, the data was analyzed in order to be able to predict which individual variables are significant in determining an individual's descent rate.

The first sets of data will be four stairwells from Building 6. Only those variables that are found to be significant for this population, along with the variables that involve interactions with other individuals will then be used when analyzing the other buildings.

The goal of the analysis phase is to construct a model that will accurately predict individual descent rates. The data used will be what was collected in the previous phases. While many variables exist for each individual, this data is not assumed to be everything that is needed for a complete understanding of an individual's descent rate. For example, unseen variables like heart and breathing problems are expected to influence an individual's descent rate. Prior activity (someone just waking up or coming back from the gym) might cause an individual to move differently. There are countless other, unmeasured, influences that will play a role in the actual descent rate.

With a perfect model not being possible, the goal is thus to predict, with a reasonable degree of accuracy, the descent rate of an individual. Also, the model should be as simple as possible so that the results can be more readily applied to future situations.

3.7 Statistical Analysis

Five different types of statistical analyses tools are used in Chapter 4 to analyze the data. Each of the methods is best suited for the applications in which they are used. In all instances, the 95% confidence level is used to determine whether a value is

significant or not. However, in some instances, other confidence levels will be noted when a value is barely significant or not.

3.7.1 t-test

When comparing whether two sample populations have the same mean, a t-test is used. The t-statistic is calculated by:

$$t = \frac{\overline{x_1} - \overline{x_2}}{\left(\frac{{s_1}^2}{n_1} + \frac{{s_2}^2}{n_2} \right)^{0.5}} \tag{3.6}$$

where:

t=test statistic
$\overline{x}$=population mean
s=population standard deviation
n=population size
_1 or _2=population group

and the degrees of freedom are calculated by rounding down:

$$\mathrm{df} = \left(\frac{{s_1}^2}{n_1} + \frac{{s_2}^2}{n_2} \right) \Bigg/ \left(\frac{\left(\frac{{s_1}^2}{n_1} \right)^2}{n_1 - 1} + \frac{\left(\frac{{s_2}^2}{n_2} \right)^2}{n_2 - 1} \right) \tag{3.7}$$

where:

df=degrees of freedom
s=population standard deviation
n=population size
_1 or _2=population group

Using the t-value and degrees of freedom, the p-value is calculated from its location on the t-distribution.

3.7.2 χ^2-test

A χ^2-test is used to compare if the observed population counts match the expected values. The expected values are the denominator in equation 3.8. The test statistic is calculated by:

$$\chi^2 = \sum_i \frac{(A_i - R_i \cdot A_t)^2}{R_i \cdot A_t} \tag{3.8}$$

where:

χ^2=test statistic
A_i=actual count of observations with given set of characteristics
R_i=ratio of all observation with main characteristic
A_t=actual count of observations with secondary characteristic

The degrees of freedom are equal to one less than the number of main characteristic levels. Using the χ^2-value and degrees of freedom, the p-value is calculated from its location on the χ^2-distribution.

3.7.3 Partial F-test

The partial F-test is used to test whether a reduced regression model is statically different than the full model. The desire is to have a reduced model that contains as few variables as possible, but still sufficiently explains the observed data.

The F-statistic is calculated by:

$$F = \frac{(RSS_R - RSS_F)/(p_F - p_R)}{RSS_F/(n - p_F)} \tag{3.9}$$

where:

F=F-statistic
RSS=residual sum of squares from regression model
p=number of parameters
n=number of data points
$_R$=reduced model
$_F$=full model

3.7.4 Multiple Regression

Multiple regression modeling uses least squares to determine the linear combination of the independent variables that best explains the dependent variable. The coefficients are determined by the combination of coefficients that lead to the squares of the differences between the actual and predicted values of the dependent variable being closest to 0. The equation is of the form:

$$y = \beta_0 + \sum \beta_i \cdot x_{ij} + \varepsilon \tag{3.10}$$

where:

y=dependent variable
β=coefficient
x=independent variable
ε=error

Multiple regression is used to determine the effect of each independent variable on the dependent variable when the other variables are held constant. The significance level of the coefficients is the probability that the given coefficient is not zero.

3.7.5 R^2

The R^2 analysis is used to determine how much of the error can be explained by the model. It is calculated by:

$$R^2 = 1 - \frac{\sum \left(y_i - \hat{y}_i\right)^2}{\sum \left(y_i - \bar{y}\right)^2} \tag{3.11}$$

where:

R^2=measure of error explained
y_i=observed value
$\hat{y}_i$ =predicted value
$\bar{y}$ =average value of y

3.8 Summary

Data collected by NIST was used for this study. The travel distance and area were determined based on paths that matched observe behavior on stairs rather than the paths that had been used in previous studies. Five different classifications of variables were extracted from the data. Each data point was calculated based on the observations between two adjacent video camera locations.

The analysis will divide the data into two sets. The first set will involve the tallest building in which data was collected that had a low density. This set will serve as a method for identifying the variables that are the most significant without the interactions that could occur in the higher density situations. The second set will contain all of the buildings and will be used as a more general understanding of individual movement on stairs.

Chapter 4: Data Analysis

The data analysis consists of two primary sections. The first primary section analyzes occupants in a building where the mean effective density was below Level C (Fruin, 1971). Qualitative and quantitative observations are made about patterns in the data. The second primary section examines occupants in buildings with higher densities. The knowledge gained from the first section as well as additional qualitative and quantitative observations is used to understand the human movement principles. From here, a model for predicting descent times is developed and applied to data from a different evacuation.

The raw data used in the analysis is available in Appendix B and all of the calculated values are available in Appendix C.

4.1 Light Effective Density Case

For the light effective density condition, four stairs from Building 6 of the NIST data were selected. The west coast building was 62- stories tall and 607 occupants were seen a total of 2,518 times. There were multiple transfer corridors in each stair and only those sections for which the occupants did not use a transfer corridor were included in the analysis. This resulted in 595 usable data points. Of these data points, 199 were in Stair 5, 158 were in Stair 5A, 97 were in Stair 6, and 141 were in Stair 6A. The stairs were 1.05 m-wide and there were typically 22 steps (25.4 cm tread depth, 20.0 cm riser height) between floors.

Because the effective density was light, there were no queues or other effects found under heavy flow conditions. The data can be treated as being similar to that from a laboratory experiment where small platoons of people are asked to descend the stairs together. This allows for key variables to be studied in isolation and to see the individual dynamics that are present during evacuations.

4.1.1 Traditional Methods

As a baseline case, the traditional speed versus density methods will be presented for Building 6. The SFPE Handbook (2008) equation (Equation 2.15) will be applied to the data as well as a curve fit to match the data.

4.1.1.1 Description of the Data

The effective density was calculated based on the mean number of people within the landing area when the occupant entered the landing for both the upstream and downstream cameras. For the 595 data points, the effective density ranged from 0.35 to 2.25 persons/m^2 with a mean of 1.01 persons/m^2 and a standard deviation of 0.48 persons/m^2.

The effective speeds were based on the times between exiting each landing. The minimum effective speed was 0.32 m/s and the maximum was 1.17 m/s. The mean was 0.61 m/s with a standard deviation of 0.12 m/s. It should be noted that the mean effective normalized descent time was 1.71 s/m, which is greater than inverse of the mean effective speed (1.65 s/m). The standard deviation for this value is 0.32 s/m.

4.1.1.2 SFPE Handbook Equation

In order to use the SFPE Handbook (2008) equation (Equation 2.15) for predicting effective movement speed, the k-value for the stairs is needed. Unfortunately, the riser height and tread depth (20.0 cm and 25.4 cm respectively) do not match any of the provided k-values. Pauls (1984) proposed that the ratio of the effective width divided by the total population could be adjusted by 1% for every for every 0.5 cm tread depth decrease or riser height increase, up to 10% for either value. He then provided four examples that are in the SFPE Handbook (2008). Even though Pauls (1984) explicitly said not to use his method for calculating speed based on riser height and tread depth, Nelson and MacLennan (1995) used the values to develop the values in the Second Edition of the SFPE Handbook (the equations are unchanged in later editions). Thus, to be consistent with the methodology, the same procedure is used here. The resulting equation is:

$$s = \begin{cases} 0.85 & D < 0.54 \\ 0.98 - 0.26 \cdot D & 0.54 \le D \le 3.7 \\ 0 & D > 3.7 \end{cases} \quad (4.1)$$

where:

s=effective speed (m/s)
D=effective density (persons/m^2)

Differences in how the area and travel distance are calculated could cause substantial differences between the reference equation and the data due to measurement methods alone (see Appendix D). Unfortunately, the SFPE Handbook (2008) does not provide guidance on how to include landings, so the assumption is made that the methods used elsewhere in the dissertation can be used with the equation. The accuracy of this assumption is unknown. Figure 4.1 shows equation 4.1 and the data from Building 6.

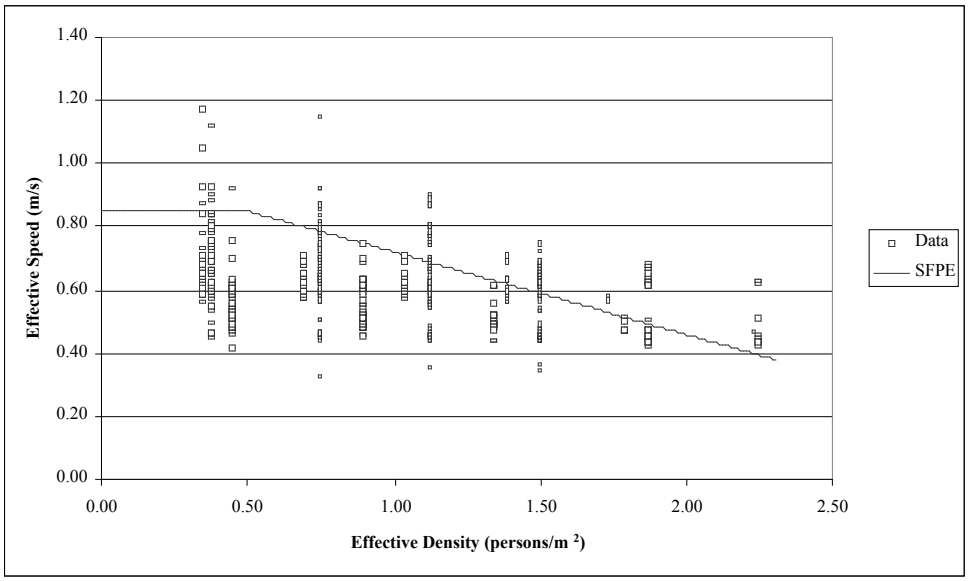

Figure 4.1: Effective Speed vs. Effective Density- SFPE Curve

The modified SFPE equation passes through the data, but the scatter is rather large. Figure 4.2 compares the predicted values with the actual values.

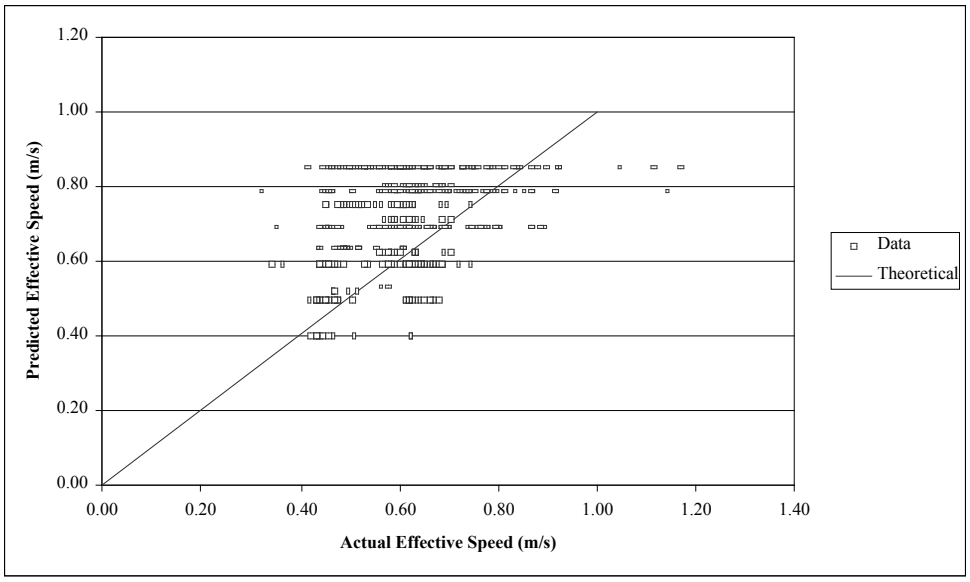

Figure 4.2: Predicted vs. Actual Values Predicted by the Modified SFPE Curve

The values predicted by the SFPE curve do not seem to follow the theoretical trend line. In fact, the R^2 value for this equation is –1.12, indicating that the correlation is less accurate than assuming all occupants travel at the mean effective speed of all observations in Building 6.

4.1.1.3 Effective Speed Equation Fit to Data

To account for potential differences in the measurement methods, because Building 6 is taller than the range of data used to develop the SFPE Handbook (2008) curve, and there is some belief that the population is now slower than it used to be, there could be an inherent difference between the equation and the data that are not related to just the terms in the equation. While there is no proof that any of these, or other differences between the data used to develop the equation and this building exist, an equation will be developed using the approach followed by Pauls (1980) to demonstrate the best possible fit of that style of equation for the effective speed and effective density for this building's occupants. The equation is developed using the regression line that is developed by least squares. The equation comprised of the linear trend line that fits the data is:

$$s = 0.69 - 0.085 \cdot D \tag{4.2}$$

where:

s=effective speed (m/s)
D=effective density (persons/m^2)

Equation 4.2 is plotted against the data in Figure 4.3 and the predicted effective speed values for this curve are plotted against the observed values in Figure 4.4.

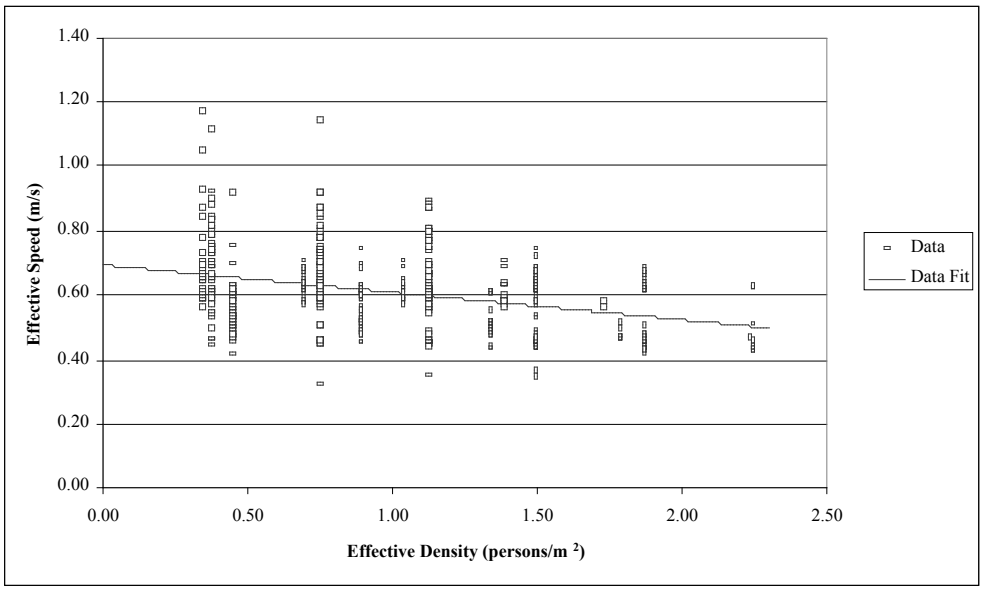

Figure 4.3: Effective Speed vs. Effective Density- Fitted Curve

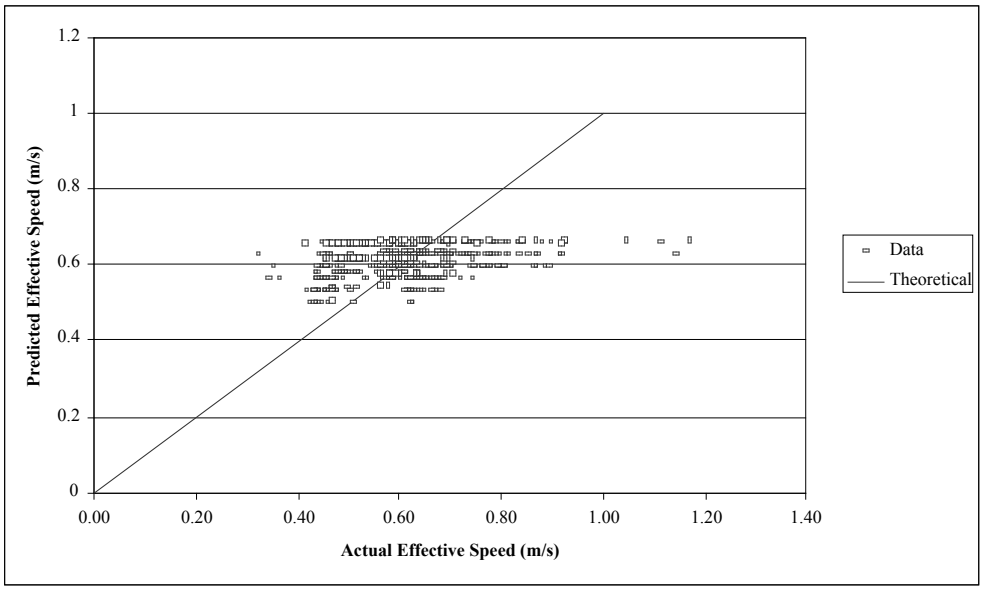

Figure 4.4: Predicted vs. Actual Values Predicted by the Effective Speed Curve

As was the case with the modified SFPE curve, the trend line passes through the data, but the predicted values do not appear to be linearly related to the actual values. In fact, the R^2 value is 0.12. Because Equation 4.2 is the best possible fit to the data, no other linear relationship between effective speed and effective density will provide a better R^2 value for this data. Thus, 88% of the error is explained by variables other than effective density.

4.1.1.4 Effective Normalized Descent Time Equation Fit to Data

As was discussed in Chapter 3, the normalized time will be used in the analysis of the data. For a comparison of equivalent values, the methods used in Section 4.1.1.3 are used to analyze the data when the inverse of effective speed is used as the dependent variable.

For the effective normalized descent time, the linear equation that best matches the data using least squares is:

$$t = 1.46 + 0.24 \cdot D \qquad (4.3)$$

where:

t=effective normalized descent time (s/m)
D=effective density (persons/m^2)

Equation 4.3 is graphed along with the data in Figure 4.5 and the predicted versus actual measurements are shown in Figure 4.6.

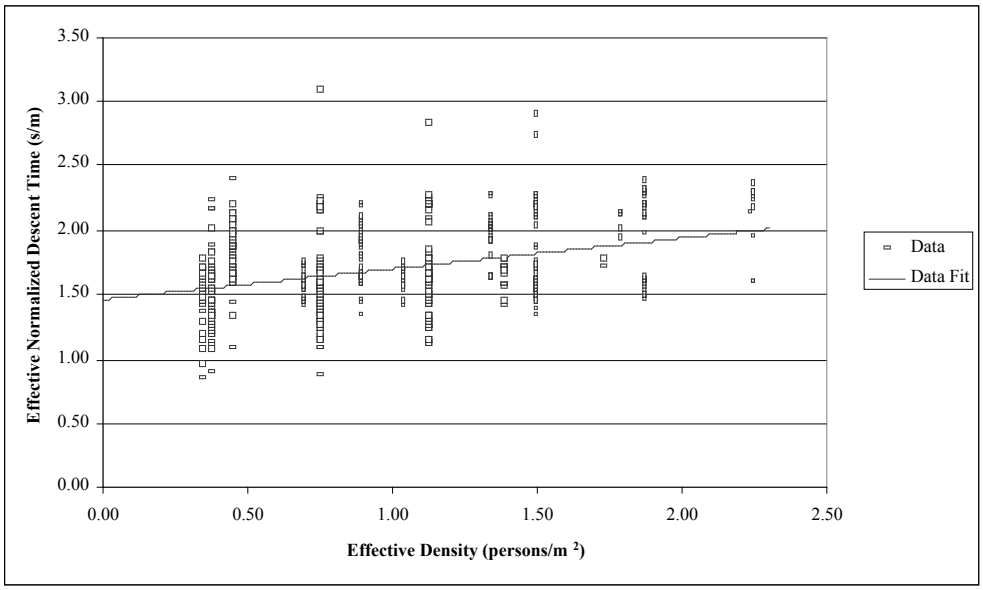

Figure 4.5: Effective Normalized Descent Time vs. Effective Density- Fitted Curve

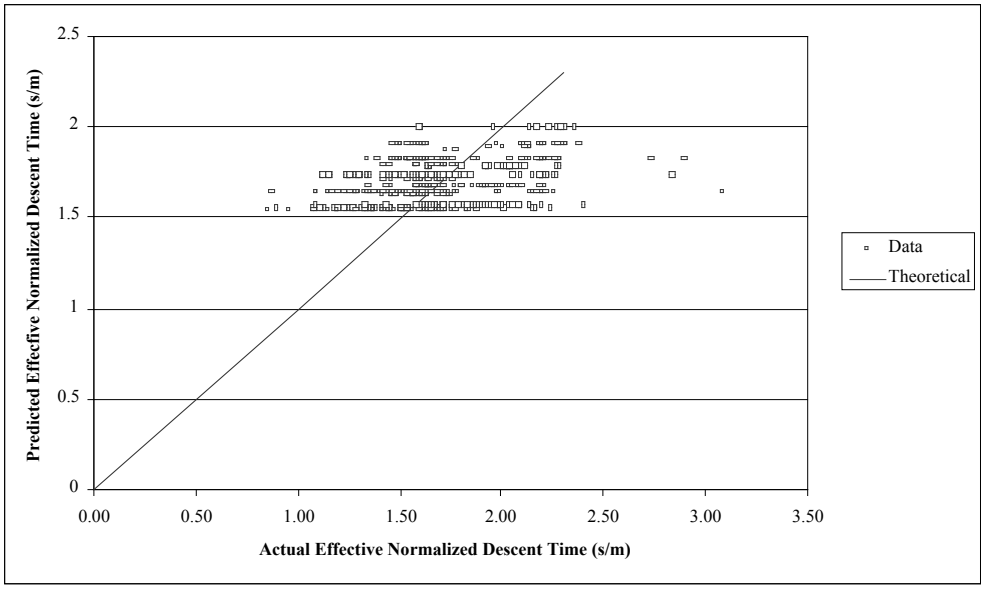

Figure 4.6: Predicted vs. Actual Values Predicted by the Effective Normalized Descent Time Curve

As expected, Figure 4.5 and Figure 4.6 show the same basic trends as does Figure 4.3 and Figure 4.4. The only readily discernable difference is the exact numbers. There is a very minor improvement in the R^2 value, being 0.13 for this method.

4.1.2 Variables and Effective Normalized Descent Times

As was shown in Section 4.1.1.4, only accounting for effective density provides a relatively poor prediction of effective normalized descent times. Other variables that provide better predictive power are needed. This section of the analysis will examine different variables with most other variables held constant. This will aide in the ability to identify some patterns within the data.

4.1.2.1 Flow Units

The occupants tended to descend in nonrandom clusters. This can be seen in a few ways. First, visual inspection of the data for a given floor shows that occupants are not evenly spread out over the duration of the evacuation; there appear to be clusters that are together. These are platoons similar to the ones seen by Pushkarev and Zupan (1975). This effect can be seen in Figure 4.7 where each data point represents the time that an occupant exited floor 20 in stair 5.

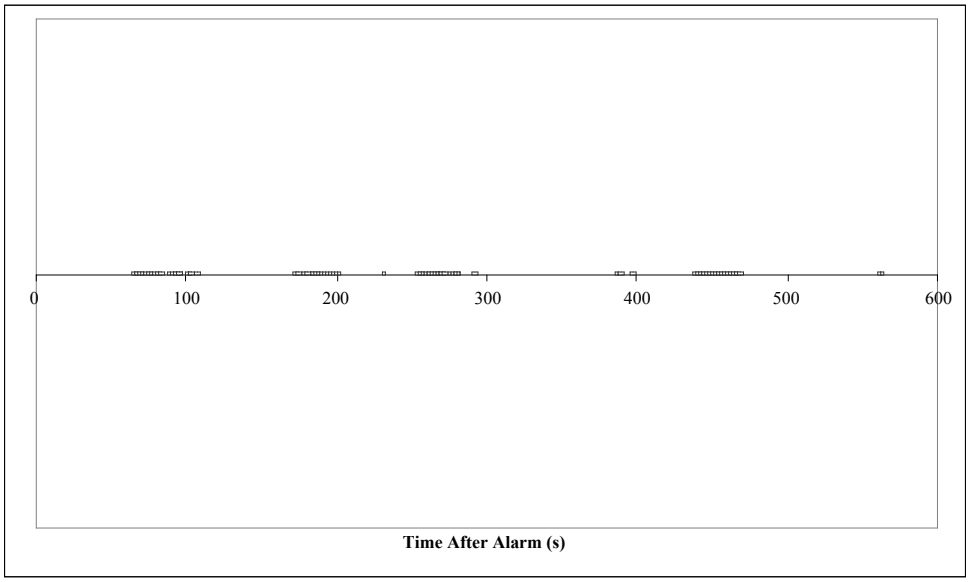

Figure 4.7: Occupant Platoons on Floor 20 in Stair 5 of Building 6

In Figure 4.7, there are several clear clusters of individuals as they descend. While some of the clusters do not maintain cohesiveness as they descend, others clearly do.

For example, the first five occupants seen in Building 6, Stair 5, Floor 20 are all within 13 s of each other and they maintain the same order and exit the building within 13 s of each other despite the fact that they never encounter another occupant as they descend (the last person to exit the building before them did so nearly 2 min before they did). In other words, they can travel at their free speed for the entire evacuation. Qualitatively, similar patterns were noted on all of the stairs, on all floors, and for multiple clusters on all floors.

Based on the qualitative observations that occupants were not randomly distributed and that some of these occupants remained together as they descended, a quantification of the clusters (flow units) was defined. A new flow unit was defined for any instance where there was a gap between occupants of at least four open treads (different platoons), where occupants passed other occupants, or where occupants allowed other occupants to enter the flow between them and other people that they had been in a previous flow unit with. Because of the light effective density within the stair, it was assumed that the first occupant in each flow unit was setting the pace for the other members of the flow unit. Thus, the first person in the flow unit is considered differently from the subsequent members of the flow unit. This resulted in 248 first persons in flow units being identified. Of these, 149 were in flow units by themselves. For the remaining 99 flow units, the maximum number of followers was 35 persons, with a mean of 3.51 persons, and a standard deviation of 4.47 persons.

The effective normalized descent times of the first persons in flow units is plotted against the effective normalized descent times of the followers in Figure 4.8. The line on the graph is the proposed theoretical relationship between followers and first persons in flow units. Specifically, each member of the flow unit is descending at the same rate as the first person in their flow unit. The R^2 value for this theoretical prediction is 0.99.

Due to the strong relationship between the effective normalized descent times of followers and first persons in flow units, all subsequent analysis of the other variables will consider both the entire population as well as for just the first persons in flow units. This will limit the analysis to only those occupants that are perceived to be setting the pace for others.

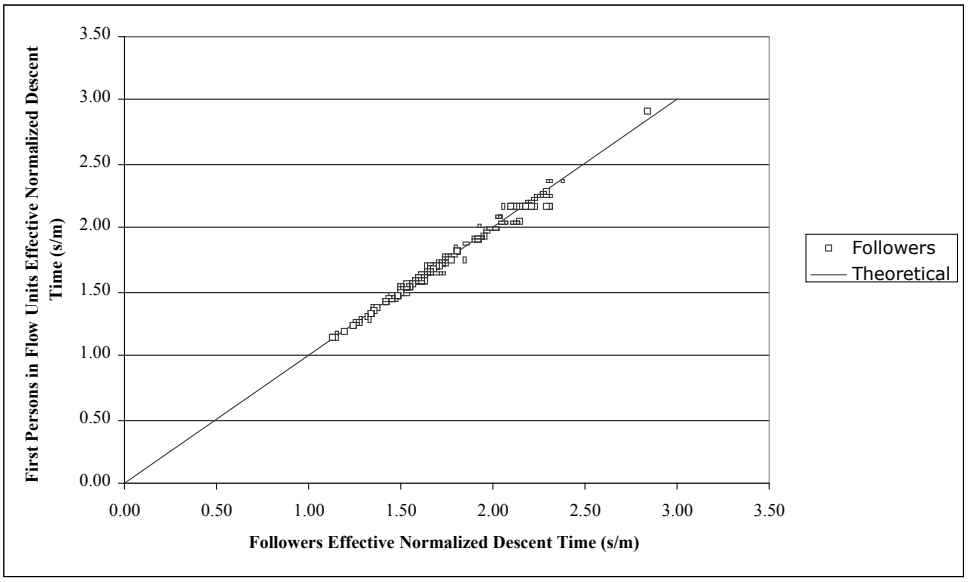

Figure 4.8: Predicted Effective Normalized Descent Time of Followers

4.1.2.2 Categorical Variables

As shown in Appendix C, the effective normalized descent times for the different levels of the number of open treads were significant at the 95% confidence level. When the values are controlled for just the first persons in flow units, then the effective normalized descent times for the different levels of gender were also significant.

4.1.2.3 Effective Stair Travel Distance

For effective stair travel distance, in order to control for some of the interpersonal variations, the descent times for first persons in flow units that were recorded on two consecutive sets of observations, without transfer hallways, were compared. Of the 42 instances where there were paired sets of effective normalized descent times for the first persons in flow units, 30 of the first persons in flow units had slower observed times at the observation made lower in the building. The differences in their effective normalized descent times are plotted against the distance between the two observation points as shown in Figure 4.9.

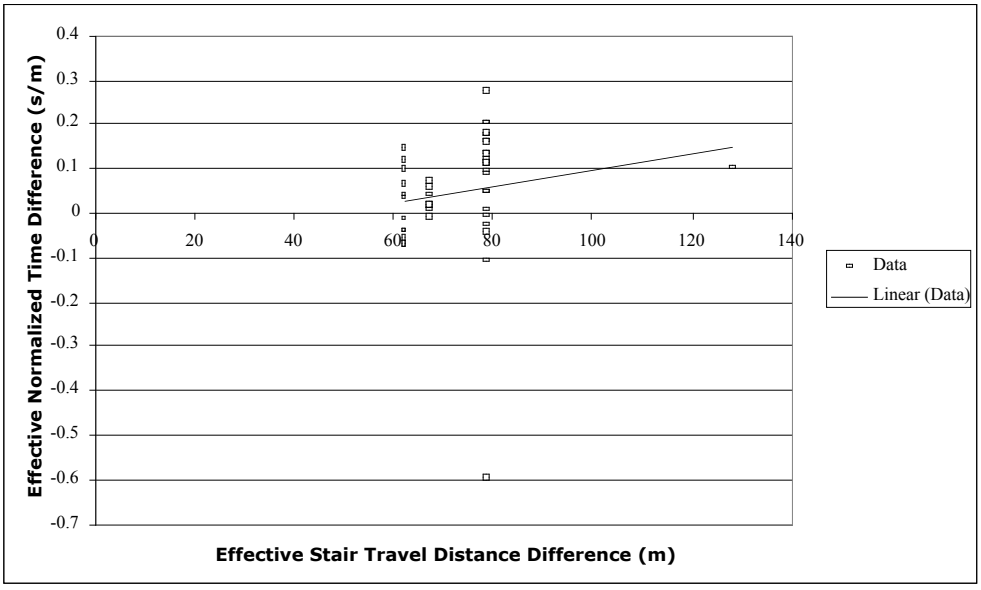

Figure 4.9: Difference in Effective Normalized Descent Time Based on Effective Stair Travel Distance

A paired t-test was conducted based on the null hypothesis that the mean effective normalized descent time difference for these first persons in flow units was unchanged between the first and second observation (including the one outlier). This resulted in a p-value of 0.02, so first persons in flow units required a statistically greater amount of time to descend as they traveled further.

4.1.2.4 Pre-Observation Time

To eliminate any effects from effective stair travel distance, the effective normalized descent time based only on pre-observation times of first persons of flow units for only for the first observation of them is shown in Figure 4.10.

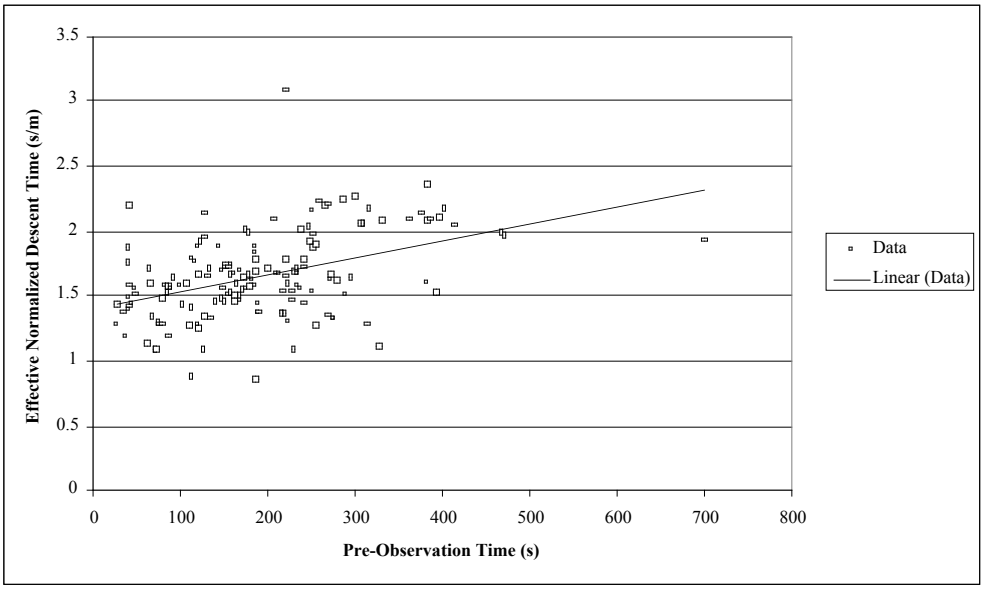

Figure 4.10: Effective Normalized Descent times, First Persons in Flow Units 1st Seen, Pre-Observation Time

The linear equation that best matches the data is:

$$t = 1.39 + 0.0013 \cdot p \qquad (4.4)$$

where:

t=effective normalized descent time (s/m)
p=pre-observation time (s)

The R^2 value for Equation 4.3 is 0.19. While this value is much smaller than that found for predicting followers' effective normalized descent times, it is greater than any of the values relating effective density to either effective speed or descent time.

4.1.3 Relationships between Variables

Several of the variables were categorical in nature (first person in flow unit/follower, number of open treads, gender, carrying, body size, and exit lane). A χ^2-test will be used when comparing the actual values with the expected values for each combination of categorical variables. For the continuous data, t-tests were used to compare the means of the different subpopulations. These values are shown in Appendix C.

4.1.3.1 First Persons in Flow Units and Followers

There were 248 first persons in flow units and 348 followers. The number of first persons in flow units and followers with the different categorical characteristics and the expected values are shown in Table 4.1.

Table 4.1: First Persons in Flow Units and Followers Actual and Expected Counts

Variable	1st Persons (Actual)	1st Persons (Expected)	Followers (Actual)	Followers (Expected)
< 2 Open Treads	24	74.2	154	103.8
2 Open Treads	50	90.4	167	126.6
3 Open Treads	54	33.3	26	46.7
> 3 Open Treads	120	50.0	0	70.0
p-value	$4.7*10^{-35}$*		$4.8*10^{-28}$*	
Female	159	133.8	162	187.2
Male	89	114.2	185	159.8
p-value	0.0013*		0.0066*	
Carrying	112	110.0	152	154.0
Not Carrying	136	138.0	195	193.0
p-value	0.80		0.83	
Large	10	6.7	6	9.3
Not Large	238	241.3	341	337.7
p-value	0.19		0.27	
Inner	135	112.1	134	156.9
Middle	51	54.6	80	76.4
Outer	62	81.3	133	113.7
p-value	0.0087*		0.034*	

*Significant based on 95% confidence level

The spacing between occupants does lead to significantly different results than the expected values. At three or three or more open treads, more occupants are first persons in flow units than is expected and, at the closer spacings, occupants are more likely to be followers. Further details about the relationship between treads and first persons in flow units are shown in Appendix C where the first person in flow units are observed more than expected for distances more than two open treads and followers are observed more than expected for two or fewer open treads.

Also, first persons in flow units were more likely to be female while males were more likely to be followers. However first persons in flow units and followers were not statistically different with respect to carrying items or body size. The exit lanes were significant with more first persons in flow units being expected in the inner lane and more followers than expected in the middle and outer lanes. As shown in Appendix C, the inner lane has statistically more first persons in flow units than expected, the

outer lane has more followers than expected, and the middle sees no statistical difference.

The first persons in flow units had a mean effective stair travel distance of 130.3 m (standard deviation 99.2 m) and the followers had a mean effective stair travel distance of 131.2 m (standard deviation 84.2 m). A t-test resulted in a p-value of 0.90, so the two values are not statistically different. Similarly, first persons in flow units had a mean pre-observation time of 195 s (standard deviation 99.0 s) and the followers had a mean of 200.5 s (standard deviation 98.9 s). A t-test resulted in a p-value of 0.50, so first persons in flow units and followers had the same statistical pre-observation time.

4.1.3.2 Categorical and Continuous Variables

As shown in Appendix C, many of the categorical variables had significantly greater observed values than expected values. When the analysis was conducted by separating the first persons in flow units and follower populations, only the relationships between gender and carrying items (females being more likely to be carrying and males not to be carrying), less than two open treads followers were more likely to be carrying objects, and followers in the outer lane being more likely to be male and not carrying objects remained significant.

4.1.4 Modeling Data

The final step in analyzing the light effective density case is using regression modeling to test the change in the dependent variable (effective normalized descent time) with changes in each of the independent variables when all other variables are held constant. Because of the strong relationship between followers' effective normalized descent times and first persons in flow units' descent times, the followers are excluded from the analysis; they are not assumed to not be setting the pace for the flow unit. SPSS Version 12.0.1 was used for conducting the analysis.

The coefficients in the models for the continuous variables (effective stair travel distance and pre-observation time) are interpreted as the change in the dependent variable (for effective normalized descent time, the number of s/m) for a change of one unit in the independent variable. For example, Equation 4.3 is a regression equation relating the effective normalized descent time with a continuous variable, effective density. The coefficient for effective density was 0.24, so an increase in the effective density by 1 persons/m^2 would result in the expected effective normalized descent time increasing by 0.24 s.

For the categorical variables (i.e., gender or number of open treads), one level is excluded from the model and the coefficients on the other levels are interpreted as the change for that level from the reference level; it does not matter mathematically which level is selected as the reference level. For example, the reference level for exit lane is the occupants in the middle. The occupants in the middle would have an expected descent time of the constant plus all additional independent variables

coefficients that apply. An occupant in the inner lane (with the other independent variables being held constant) would have an expected effective normalized descent time equal to the occupant in the middle plus the coefficient for being in the inner lane. The reference levels for the different variables are shown in Table 4.2.

Table 4.2: Reference Levels of Categorical Variables

Variable	Reference Level
Open Treads	> 3
Gender	Male
Carrying	Not Carrying
Body Size	Not Large
Exit Lane	Middle
Flow Type	Uniform
Stair	5

Flow type is a variable that was developed based on observations of the heavy effective density conditions and is defined and explained in Section 4.2.2.3. Only five observations were made of first persons in flow units not in the uniform flow type. The stair variable (a categorical variable separating the population by the stair that they were in) was included to see if occupants in the sinistral stair (Stair 6) had different effective normalized descent times than the occupants in the dextral stairs.

4.1.4.1 Stairs Included

The first model includes the stair variable. As shown in Section 3.7.4, the regression formula is of the form:

$$y = \beta_0 + \sum \beta_i \cdot x_{ij} + \varepsilon \qquad (4.5)$$

where:

y=dependent variable
β=coefficient
x=independent variable
ε=error

The coefficients of this model are shown in Table 4.4 with the definitions of the different terms for all regression models in Table 4.3.

Table 4.3: Definitions of Terms in Regression Models

Term	Meaning
Const.	Values for all levels of the variables
S5a, S6, S6a	Values for the non-reference levels of the stair variable
Female	Values for the non-reference levels of the gender variable
Carrying	Values for the non-reference levels of the carrying variable
Large	Values for the non-reference levels of the body size variable
< 2, 2, or 3 Open Treads	Values for the non-reference levels of the open treads variable
Lane Flow	Values for the non-reference levels of the flow type variable
Inner or Outer Lane	Values for the non-reference levels of the exit lane variable
Travel Distance	Values for the effective stair travel distance variable
Pre-Obs. Time	Values for the pre-observation time variable
B	The coefficient determined by SPSS to provide the best linear fit to the data when all other levels of the variables are controlled
Std. Err.	The standard error for B
Beta	The B coefficient normalized by SPSS
t	The t-test statistic for the coefficient
Sig.	The p-value of the coefficient

Table 4.4: Stairs Model Coefficients

	Unstandard. Coefficients		Standard. Coefs.	T	Sig.	95% Confidence Interval for B	
	B	Std. Err.	Beta			Lower Bound	Upper Bound
Const.	1.236	.068		18.087	.000*	1.101	1.370
S5a	-.017	.049	-.023	-.352	.725	-.114	.079
S6	.042	.051	.052	.822	.412	-.059	.143
S6a	.228	.052	.279	4.339	.000*	.124	.331
Female	.210	.042	.308	5.030	.000*	.127	.292
Carrying	-.025	.041	-.038	-.610	.543	-.105	.055
Large	.366	.093	.222	3.946	.000*	.183	.549
< 2 Open Treads	.145	.067	.127	2.154	.032*	.012	.278
2 Open Treads	.120	.048	.148	2.480	.014*	.025	.215
3 Open Treads	.043	.047	.055	.912	.362	-.050	.135
Lane Flow	.336	.130	.146	2.591	.010*	.080	.591
Inner Lane	-.016	.047	-.024	-.336	.737	-.107	.076
Outer Lane	-.004	.054	-.006	-.083	.934	-.110	.101
Travel Distance	.000	.000	.089	1.581	.115	.000	.001
Pre-Obs. Time	.001	.000	.186	3.149	.002*	.000	.001

*Significant based on 95% confidence level

For this model, SPSS calculated the F-statistic as 7.671 and the model is significant at the 95% confidence level. The R^2 value for the model is 0.32. Several of the variables were found to be significant at the 95% confidence level. Specifically, when all other variables were controlled:

- Female that were the first person in a flow unit required 0.210 more s/m than comparable males
- First persons in flow units within two open treads to the previous occupant required 0.145 more s/m than those further than three open treads to the previous occupant
- First persons in flow units with two open treads to the previous occupant required 0.120 more s/m to descend than occupants spaced more than three open treads from the nearest occupant
- First persons in flow units in the lane flow required 0.336 s/m more than those in the uniform flow

- For every 1 s of pre-observation time a first person in flow units required, their effective normalized descent time increased by 0.001 s/m.

There was also one stair (Stair 6a) that the first persons in flow units were requiring significantly greater effective normalized descent times. This cannot be explained by the direction that the stair turns because Stair 6a is a dextral stair as were Stair 5 and Stair 5a. All of the stairs have the same dimensions, and, because the significant decrease in effective normalized descent time is not caused by the direction that the stair turns, some characteristics of the occupants must explain what is happening. A possible explanation is provided by the previous flow unit variable developed in Section 4.2.2.5 for the heavy effective density condition. Because the effect of the different stairs does not appear to stem from differences in the physical conditions of the stairs, that variable will be excluded from the subsequent analysis.

4.1.4.2 Stairs Excluded

For the case where the stairs are combined, the coefficients for the regression model are shown in Table 4.5.

Table 4.5: Light Effective Density Model Coefficients

	Unstandard. Coefficients.		Standard. Coefs.	t	Sig.	95% Confidence Interval for B	
	B	Std. Err.	Beta			Lower Bound	Upper Bound
Const.	1.260	.069		18.384	.000*	1.125	1.395
Female	.223	.043	.327	5.131	.000*	.137	.308
Carrying	-.029	.042	-.045	-.693	.489	-.113	.054
Large	.390	.096	.236	4.047	.000*	.200	.580
<2 Open Treads	.131	.069	.114	1.885	.061	-.006	.267
2 Open Treads	.100	.049	.123	2.019	.045*	.002	.197
3 Open Treads	.054	.049	.068	1.097	.274	-.043	.150
Lane Flow	.279	.135	.121	2.069	.040*	.013	.544
Inner Lane	-.035	.048	-.054	-.725	.469	-.130	.060
Outer Lane	-.002	.056	-.003	-.036	.972	-.112	.108
Travel Distance	.000	.000	.093	1.586	.114	.000	.001
Pre-Obs. Time	.001	.000	.235	4.062	.000*	.000	.001

*Significant based on 95% confidence level

As was the case with the previous model, SPSS calculated that the model was significant at the 95% confidence level (F-statistic was 6.91) and the R^2 value was 0.25. The findings of the model are:

- Females that were the first person in a flow unit required 0.223 s/m more than comparable males
- Large occupants that were the first person in a flow unit required 0.390 s/m more than comparable occupants that were not large
- First persons in flow units with less than two open treads to the previous occupant required 0.131 s/m more than first persons in flow units with more than three open treads at the 90% confidence level
- First persons in flow units with two open treads to the previous occupant required 0.100 s/m more than first persons in flow units with more than three open treads
- First persons in flow units in the lane flow required 0.279 s/m more than first persons in flow units in the uniform flow
- First persons in flow units required 0.001 s/m more for every 1 s of pre-observation time

4.1.4.3 Overall Predictions

The final regression model was significant at the 95% confidence level and a majority of the variables were found to be significant. Combining the first persons in flow units and the followers results in an R^2 value of 0.66. This value is approximately five times better than the method of just using effective density. These predictions are shown in Figure 4.11.

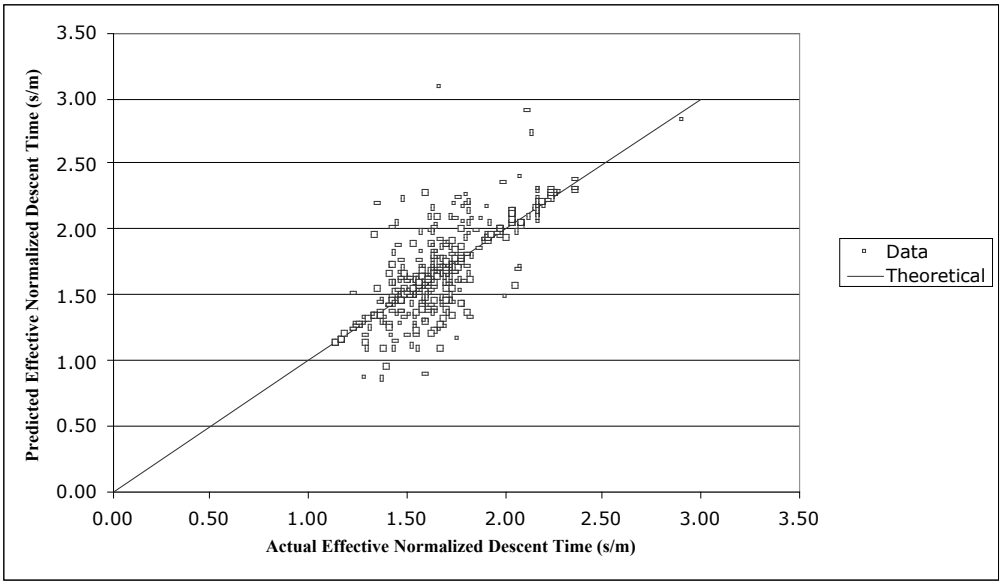

Figure 4.11: Predicted vs. Actual Values from Models

4.2 Heavy Effective Density Case

The light effective density case is used as a screening method to identify several key variables that are important for predicting effective normalized descent time. The concept of first persons in flow units and followers as well as the inclusion of several other variables resulted in predictions that were more accurate than the normal method of relying on just effective density. These variables, and other variables that are developed to account for the dynamics in heavy effective density situations, will now be used to develop regression models for a more diverse set of building evacuations.

4.2.1 Description of Buildings

Three different buildings (Buildings 4, 5, and 8 from the NIST data), each with two stairs, were included in this the heavy effective density analysis. Buildings 4 and 5 were located on the west coast of the United States while Building 8 was on the east coast of the United States. The building heights varied with Building 5 being 10 stories, Building 4 being 24 stories, and Building 8 being 30 stories. Building 8 had the widest stairs of the group (1.38 m), Building 4 had the narrowest stairs (1.12 m), and Building 5 was in between (1.27 m). All three buildings had riser heights of 17.8 cm and Buildings 4 and 5 had tread depths of 27.9 cm, but the tread depth in Building 8 was only 27.3 cm. The buildings also varied as to the number of steps per story. In Building 4 it was typically 20 steps per story, in Building 5 it was 22 steps per story, and in Building 8 it was 18 steps per story. With the exception of Stair 8S, all of the stairs are dextral stairs. All of these properties are shown in Table 4.6.

Table 4.6: Heavy Effective Density Buildings

Characteristic	Building 4	Building 5	Building 8
Location	West Coast	West Coast	East Coast
Building Height (stories)	24	10	30
Steps per Story (typical)	20	22	18
Stair Width (m)	1.12	1.27	1.38
Riser Height (cm)	17.8	17.8	17.8
Tread Depth (cm)	27.9	27.9	27.3
Direction of Turn	Dextral/Dextral	Dextral/Dextral	Sinistral/Dextral
Persons Observed	622	807	1203
# of Observations	3439	2492	9712
# of Data Points	2818	1685	7369

Also shown in Table 4.6 are the number of occupants observed in each building, the total number of observations in each building (where an observation is defined as an occupant descending the stairs identified on a single camera), and the number of data points (where a data point is determined when an occupant is identified on two consecutive floors). In Building 4, 622 occupants were observed 3,439 times which resulted in 2,818 data points. For Building 5, these numbers were 807, 2,492, and 1,685, respectively. While there were more occupants in Building 5 than Building 4, Building 4 had more observations and data points due to the greater height of the building. A majority of the data came from Building 8 where 1,203 occupants were observed 9,712 times, generating 7,369 data points. In total, there were 11,872 data points available for analysis.

4.2.2 Variables

All of the variables presented in Section 4.1.2 were included in this analysis. Additionally, the counterflow variable discussed in Chapters 2 and 3 was included due to firefighters ascending Stair 4A and 5B. Counterflow was defined as an occupant that was passed by a firefighter ascending the stair in the time interval between when they exited the upper floor and the lower floor. In addition to these variables, other variables were identified based on the dynamics observed within the flow.

4.2.2.1 Variables from Light Effective Density Analysis

As was the case previously, the dependent variable is the effective normalized descent time. For the independent variables, gender, carrying objects, body size, exit lane, and effective stair travel distance are all determined for the heavy effective density case as they were for the light effective density case. There were slight modifications made to the other variables.

The number of open treads categories was reduced to three (less than two open treads, two open treads, or more than two open treads) based on the findings in Section 4.1. Specifically, in Section 4.1.4.2, the effective normalized descent times of first persons in flow units with three open treads to the previous occupant were not statistically different than those that had more than three open treads. Also, occupants that left three open treads were found to be more likely to be first persons in flow units. Due to these similarities, all occupants that left three open treads or more were classified as first persons in flow units.

Five different types of first persons in flow units were identified (Section 4.2.2.4) and, depending on the flow type (Section 4.2.2.3), the followers could engage in passing (or being passed) behavior when following the first person in a flow unit who was similarly engaged.

Finally, a slight modification was made to the pre-observation time variable as described in Section 4.2.2.6. This was done in order to treat differently those occupants that appeared to have additional responsibilities other than just exiting the building.

4.2.2.2 Shoulder-to-Shoulder

When defining first persons in flow units and followers, those occupants engaging in passing behavior is one of the methods to identify flow units. One potential shortcoming to this method is when two occupants exit at basically the same instant. These occupants can be described as descending shoulder-to-shoulder. Pauls (1980) and others observed this type of behavior in evacuations.

Because the line designating the edge of the observation area is arbitrary and the exact stride patterns of the two occupants could be slightly different, the one recorded as being in the lead could depend on the selection of the line. One tread in either direction could lead to the other occupant being recorded as being ahead and thus the pass is not a real dynamic occurring between these two occupants.

Because these individuals are not truly acting differently than those around them, they should not be classified as first persons in flow units because that would introduce errors into the analysis (first persons in flow units are assumed to be behaving differently and thus why they are considered first persons in flow units). Thus, a screening tool needed to be developed to determine the time gap that signifies shoulder-to-shoulder descending.

Occupants that have no open treads between them and the previous occupant can be said to be descending shoulder-to-shoulder. This value is not provided in the NIST data. However this is equivalent to those occupants that are within one tread of one another. The amount of time required to travel one tread can be approximated from the NIST data based on those occupants that are recorded as being two or three treads apart. The difference in the two time gaps can be used to determine the amount of time to travel one tread.

Due to no instances of lane flow (see Section 4.2.2.3), Building 4 was selected to determine this value. There were 1,567 observations of occupants with two open treads to the previous occupant and 625 observations of occupants with three open treads to the previous occupant. For those with two open treads, the mean time to the previous occupant was 1.73 s (standard deviation 0.38 s). Similarly, for those with three open tread to the previous occupant the mean time was 2.05 s (standard deviation of 0.40 s).

As a crude approximation, a gap of 0.32 s is used to designate occupants that are walking shoulder-to-shoulder. When the time gap is less than this value, the occupants are not considered to be engaging in passing behavior.

4.2.2.3 Flow Type

There were two basic types of flows that were identified. The first is a uniform flow where all of the occupants are moving as a single flow unit regardless of what lane they are in. The second is a lane flow where the occupants in the two lanes are moving independently of one another (as if they were two separate flows). Lane flow is designated any time when a first person in a flow unit and follower in one lane pass their counterpart first person in flow unit/follower in the other lane. The changes between the types of flow appear to be dependent on the first persons in flow units. For an example of how this is seen within the data, see Appendix E.

4.2.2.4 Types of First Persons in Flow Units

Five different types of first persons in flow units were identified based on the reason that they were identified as first persons in flow units. Each type represents a different set of actions that are expected to play a role in determining the effective normalized descent time of the first persons in flow units.

The first type of first persons in flow units is for first persons that engage in passing behavior. Passing is defined as an occupant that was behind one or more occupants when exiting the upper floor and then being ahead of those occupants when exiting the lower floor (with exceptions for occupants that are shoulder-to-shoulder). Exceptions were also made for instances where a single first person in a flow unit was passed by multiple other first persons in flow units. In this instance, none of the first persons in flow units were designated as engaging in passing behavior; the passed individual most likely exited the stair and thus was not truly being passed. Passing behavior was observed for both the uniform flow and the lane flow.

The second type of first persons in flow units is first persons that are being passed. These first persons in flow units are the counterparts to the first persons in flow units engaging in passing behavior; they are ahead of one or more occupants when exiting the upper floor and are then behind them when exiting the lower floor (with exceptions based on being shoulder-to-shoulder). Again, these first persons in flow units can be present in both the uniform and lane flows.

The third type of first person in flow units is first persons that are allowing other people to enter the flow. Allowing occupants to enter is defined based on two occupants being in the same platoon when exiting the upper floor and exiting the lower floor and an occupant that entered the stairs after the upper floor is between them. In the lane flow type, allowing occupants to enter the flow is only seen to occur with occupants in the outer lane. For the uniform flow type, allowing occupants to enter the flow is seen to occur for occupants in all exit lanes.

The fourth type of first persons in flow units is first persons that experience congestion. This occurs in two different manners. First, the first person in the flow unit belongs to one platoon when exiting the upper floor and then is behind other occupants in a new platoon when exiting the lower floor. They are classified as first

persons in flow units over that segment because no one was setting the pace for them the entire distance and thus they could not be said to following someone else. Second, the first person in a flow unit is experiencing congestion when the transition from lane flow back to uniform flow happens. In both instances, the first person in a flow unit is not able to fully choose their own descent rate for the entire duration of the descent from the upper floor to the lower floor; the occupants ahead of them inhibit their descent rate.

The fifth type of first person in a flow unit is first persons that are free to choose their own descent rate as they descend from the upper floor to the lower floor. When they reach the lower floor, the occupants ahead of them are more than two open treads away.

Each first person in a flow unit is categorized into one of the five first persons in flow units types. In the event that more than one applied, preference was given to being passed, passing, and allowing other occupants to enter the flow. This resulted in 826 first persons in flow units being classified as ones that were passing, 988 that were passed, 278 that allowed other occupants to enter the flow, 1,299 that experienced congestion, and 1,572 that experienced free-flow conditions.

4.2.2.5 Previous Flow Unit

Except for some of the first persons in flow units experiencing free-flow conditions, all of the other first persons in flow units were having their descent rate shaped in part by the other occupants that were around them. The first persons in flow units that are experiencing congestion cannot move any faster once they are behind other occupants, the first persons in flow units that allow other occupants to enter the flow are previously moving at the descent rate of the occupants ahead of them; even those occupants that are passing or are being passed could be inhibited by the other occupants in the stairs.

Just as the followers have their descent times related to the first person in their flow unit, the different first persons in flow units experience the same issue to a limited extent. To account for this, the effective normalized descent time for a preceding flow unit will be used to predict the effective normalized descent times of each first person in a flow unit. In most instances, the effective normalized descent time that will be used is the one for the preceding flow unit. The exception is if the preceding flow unit was engaging in passing or being passed behavior. In these instances, the previous flow unit is defined as the closest flow unit not engaging in one of these actions.

4.2.2.6 Security and Floor Wardens

In some buildings there were occupants that did not start in the stairs until very late in the egress processes. Most of the last occupants appeared to be building staff (either floor wardens or security officers) that were assumed to be performing other duties aside from evacuating. In Section 4.1.4.2, first persons in flow units that were

observed later were found to require more effective normalized descent time than first persons in flow units that left earlier when all other variables were held constant. Because of the light effective density, a possible explanation is that occupants that require more time to descend were self-selecting to evacuate later. If this is true, then the security and floor wardens that are leaving later need to be excluded because their motivation for leaving later is different than the other occupants that chose to start later for personal reasons.

To account for this difference, the pre-observations time was considered to be a continuous variable for the first ten minutes after the alarm sounded. For the occupants that required more than ten minutes until they were first seen in the stairs, they were recorded as having no pre-observation time and were instead recorded as belonging to a categorical variable of late starters.

4.2.3 Characteristics of First Persons in Flow Units

As was the case in Section 4.1, the followers will be considered separately from the first persons in flow units. The comparisons in this section will use χ^2-tests to compare the characteristics of the first persons in flow units from a given type to the rest of the first persons in flow units in order to determine if certain types of individuals are more or less inclined to become a particular type of first persons in flow units. The details are available in Appendix C.

4.2.3.1 Passing First Persons in Flow Units

First persons in flow units that are engaging in passing behavior are more likely to be carrying objects than first persons in flow units that are not carrying anything. Also, first persons in flow units that engaged in passing behavior were recorded as being in the inner lane far more than expected (and recorded less than expected in the outer lane).

4.2.3.2 Passed First Persons in Flow Units

Due to the complimentary nature of passing and being passed, the actual and expected counts are expected to mirror those for the first persons in flow units that were passed. Gender was significant, with more females that were the first person in a flow unit being passed than comparable males (the opposite trend was seen for passing behavior, but it was not significant). For passing first persons in flow units, carrying and not carrying had been significant. While it was not significant for first persons in flow units that were passed, the trend was not complimentary (carrying was once again more likely). First persons in flow units that were large were less likely to be passed than was expected. As for exit lane, first persons in flow units in the middle and outer lane were more likely to be passed than was expected. This finding compliments the finding in Section 4.2.3.1 that passing first persons in flow units were located on the inner lane.

The mean effective stair travel distance for first persons in flow units that were passed were 58.94 m (with a standard deviation of 54.98 m). For all other first persons in flow units, the mean value was 68.65 m (with a standard deviation of 60.51 m). The p-value from a t-test was $1.2*10^{-6}$. Thus, the null hypothesis that the mean effective stair travel distance for first persons in flow units that were passed and the other first persons in flow units was the same is rejected at the 95% confidence level.

4.2.3.3 Allowed Entering First Persons in Flow Units

The third type of first persons in flow units that were typically surrounded by other occupants was first persons that allowed other occupants to enter the flow. The only value that is significantly different than expected is that there were more first persons in flow units not carrying objects that allowed people to enter the flow.

The mean effective stair travel distance for first persons in flow units that allowed occupants to enter the flow was 29.56 m (with a standard deviation of 33.87 m). For the other first persons in flow units, the means were 68.93 m (with a standard deviation of 60.04 m). The p-values from a t-test was $3.0*10^{-52}$, so the first persons in flow units that allowed occupants to enter the flow had statistically less effective stair travel distance.

4.2.3.4 Experienced Congestion First Persons in Flow Units

First persons in flow units that experienced congestion were the ones that had their descent rates impeded by flow units ahead of them, but they did not perform any behaviors relative to the other occupants. None of the actual values are statistically different than the expected counts. These first persons in flow units were not able to be distinguished from the rest of the first persons in flow units.

4.2.3.5 Free-Flow First Persons in Flow Units

The final type of first persons in flow units is one where they experienced free-flow conditions. There were more males (and less females) than expected that were free-flow first persons in flow units. Also, there were more first persons in flow units not carrying things than was expected; this corresponds to the findings in Section 4.1.2.2 where men were found to be less likely to be carrying items. There were more free-flow first persons in flow units than expected in the outer lane (and fewer in the inner lane). The findings regarding gender and exit lane contradict what was found in Section 4.1.3.1. This contradiction will be discussed more in Chapter 5.

The mean effective stair travel distances for those first persons in flow units that experience free-flow conditions and those that did not were 78.73 m (with a standard deviation of 63.96 m) and 61.15 m (with a standard deviation of 56.58 m). For the pre-observation times, the values were 245.69 s (with a standard deviation of 273.58 s) and 165.21 s (with a standard deviation of 120.07 s). The p-values from t-tests were $2.1*10^{-20}$ for effective stair travel distance and $4.1*10^{-28}$ for pre-observation time. Thus, in both instances, the values were statistically greater.

4.2.4 Characteristics of First Followers

As is seen in Appendix E, occupants generally stayed in their lanes. The exception came in 7B where two occupants passed a slower moving occupant. They are classified as first persons in flow units. This raises the question as to whether there are different types of occupants that choose to become first persons in flow units or not.

The hypothesis is that any differences between those individuals that are first persons in flow units and the ones that are not would be most evident for the first follower in each flow unit; the followers located much further back might not have the opportunity to behave differently while the person immediately behind the first person in a flow unit could choose to follow the first person in the flow unit or not.

To determine if there are any differences between the first followers and their first persons in flow units, χ^2-tests are conducted to determine what, if any, differences there are between the two populations. These values are shown in Table 4.7.

Table 4.7: First Persons in Flow Units and First Follower Pairs Actual and Expected Counts

Variable	1st Persons (Actual)	1st Persons (Expected)	Followers (Actual)	Followers (Expected)	p-value
Female	1152	1148.5	1145	1148.5	0.884
Male	893	896.5	900	896.5	0.869
Carrying	1377	1348.0	1319	1348.0	0.264
Not Carrying	668	697.0	726	697.0	0.120
Large	138	127.5	117	127.5	0.188
Not Large	1907	1917.5	1928	1917.5	0.735
Inner	526	600.0	674	600.0	$1.93*10^{-5}$*
Middle	241	258.5	276	258.5	0.124
Outer	1278	1186.5	1095	1186.5	$1.72*10^{-4}$*

*Significant based on 95% confidence level

The only relationships that are significant were that there were more first persons in flow units in the outer lane (and more followers in the inner lane) than expected. This corresponds to the findings in Section 4.2.3.5.

4.2.4.1 Gender Relationship between First Persons in Flow Units and First Followers

In Table 4.7, the gender ratio between the first followers and the first persons in flow units was shown to not be significant. However, in both Sections 4.1.3 and 4.2.3.5, significant differences for first persons in flow units based on gender were identified.

A possible explanation is that there is some relationship between the gender of the first persons in flow units and first followers. To determine if this was the case, first persons in flow units and first followers were divided into four possible combinations (female first person in flow unit with female follower, female first person in flow unit with male follower, male first person in flow unit with female follower, and male first person in flow unit with male follower). These values are shown in Table 4.8.

Table 4.8: First Persons in Flow Units and First Followers by Gender Actual and Expected Counts

Variable	Female 1st Person (Actual)	Female 1st Person (Expected)	Male 1st Person (Actual)	Male 1st Person (Expected)	p-value
Female First Follow	714	645.0	431	500.0	$3.94*10^{-5}$*
Male First Follow	438	507.0	462	393.0	$3.54*10^{-6}$*
p-value	$4.22*10^{-5}$*		$3.30*10^{-6}$*		

*Significant based on 95% confidence level

Considering the pairings of first persons in flow units and first followers, female-female and male-male combinations occurred more often than expected while female-male and male-female combinations occurred less often than expected.

Taking this a step further, the actual and expected counts for the different variables of the followers, when the data is sorted by the gender of the first persons in flow units are shown in Table 4.9 for the female first persons in flow units and in Table 4.10 for the male first persons in flow units.

Table 4.9: Female First Persons in Flow Units and First Follower Pairs Actual and Expected Counts

Variable	Female (Actual)	Female (Expected)	Male (Actual)	Male (Expected)	p-value
Carrying	566	472.9	197	290.1	$3.8*10^{-12}$*
Not Carrying	148	241.1	241	147.9	$2.4*10^{-22}$*
Large	28	31.0	22	19.0	0.38
Not Large	686	683.0	416	419.0	0.85
Inner	245	234.3	133	143.7	0.26
Middle	79	84.9	58	52.1	0.30
Outer	390	394.8	247	242.2	0.69
Uniform Flow	472	502.7	339	308.3	0.027*
Lane Flow	242	211.3	99	129.7	$6.3*10^{-4}$*

*Significant based on 95% confidence level

Table 4.10: Male First Persons in Flow Units and First Follower Pairs Actual and Expected Counts

Variable	Female (Actual)	Female (Expected)	Male (Actual)	Male (Expected)	p-value
Carrying	355	268.3	201	287.7	$1.9*10^{-23}$*
Not Carrying	76	162.7	261	174.3	$3.5*10^{-21}$*
Large	24	32.3	43	34.7	0.042*
Not Large	407	398.7	419	427.3	0.52
Inner	136	142.9	160	153.1	0.42
Middle	62	67.1	77	71.9	0.39
Outer	233	221.1	225	236.9	0.26
Uniform Flow	325	333.0	365	357.0	0.54
Lane Flow	106	98.0	97	105.0	0.26

*Significant based on 95% confidence level

For carrying items, regardless of the gender of the first person in a flow unit, female followers were more likely to be carrying items while male followers were more likely to not be carrying items. As for body size, there were more large male followers than female followers that were behind a male first person in a flow unit at the 95% confidence level, but not at the 99% confidence level; no other values were significant. For the flow type, female followers (compared to male followers) were

more likely to be behind female first persons in flow units than was expected for the lane flow situation.

4.2.4.2 Following Distance Relationship by Gender

Building upon Section 4.2.4.1, the relationship between the gender of the first follower and the first person in a flow unit also leads to differences in the following distance. The actual and expected counts are shown in Table 4.11.

Table 4.11: First Person in a Flow Units and First Follower Pairs Spacing Actual and Expected Counts

Variable	< 2 Open Treads (Actual)	<2 Open Treads (Expected)	2 Open Treads (Actual)	2 Open Treads (Expected)	p-value
Female First Persons in Flow Units					
Female	626	603.3	82	104.7	0.016*
Male	348	370.7	87	64.3	0.0022*
Male First Persons in Flow Units					
Female	355	341.9	74	87.1	0.11
Male	355	368.1	107	93.9	0.13
Female Followers					
Female	626	610.9	82	97.1	0.098
Male	355	370.1	74	58.9	0.034*
Male Followers					
Female	348	340.9	87	94.1	0.41
Male	355	362.1	107	99.9	0.42

*Significant based on 95% confidence level

At the 95% confidence level, there were more female followers within one tread of female first persons in flow units and fewer male followers within one tread when the reference population was female first persons in flow units. When examining the followers behind male first persons in flow units, the actual and expected counts for both female and male followers were not statistically different than the expected values with a 95% confidence level. When looking at the spacing for female followers behind either gender first person in a flow unit, females were observed less frequently being one open tread behind male first persons in flow units as would have been expected. For male followers, there were no differences in their spacing behind either male or female first persons in flow units.

4.2.4.3 Effective Normalized Descent by Gender

Female first persons in flow units with female first followers had a mean effective normalized descent time of 2.27 s/m (standard deviation 1.02 s/m) and those with male first followers had a mean effective normalized descent time of 2.12 s/m (standard deviation 1.07 s/m). For male first persons in flow units, the female and

male first followers had mean effective normalized descent times of 2.38 s/m (standard deviation 1.37 s/m) and 2.09 s/m (standard deviation 1.23 s/m) respectively. For first persons in flow units of both genders, when the first followers were females, t-tests found the mean effective normalized descent time to be statistically greater than when the first followers were male.

4.2.5 Modeling Data

For the purpose of predicting the effective normalized descent time, three different models are developed based on the findings of the previous sections. First, as was done in Section 4.1.2.1, the followers' effective normalized descent time is determined based on the values of the first person in their flow unit. Second, a regression model is used to develop an equation for the free-flow first persons in flow units. Finally, a separate regression model is developed for the first persons in flow units with interactions based on their change in descent rate from the previous first person in a flow unit as discussed in Section 4.2.2.5. All of these values are then combined to look at the overall accuracy of the methods.

Before analyzing the data, the data set was reduced from 11,872 to 11,844 data points. There were 28 occupants that were observed leaving the stairs or being passed by many occupants and then being seen either with either a new object or losing an object (i.e., not having a jacket and then having one or carrying papers and then no longer having them). For the occupants that left the stair, their effective normalized descent time over that section is removed because their times are not representative of movement on stairs, but are instead dependent on the location they went to on the floor. Thus, the unreliable data points, 0.2% of the sample, were not included in the analysis.

4.2.5.1 Followers

The 6,909 followers' effective normalized descent times are theorized to be the same as the effective normalized descent time of the first person in their flow unit. These values are shown in Figure 4.12.

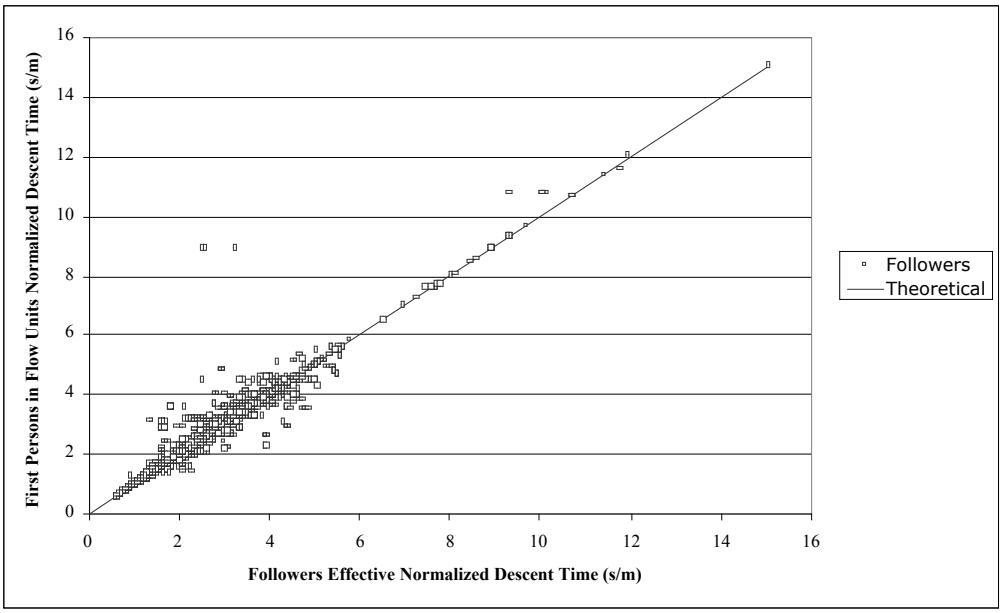

Figure 4.12: Predicted Effective Normalized Descent Times of Followers

The R^2 value of the followers, when the predicted effective normalized descent time is the same as the first person in their flow unit, is 0.93.

4.2.5.2 Free-Flow First Persons in Flow Units

The effective normalized descent times of the 1,567 free-flow first persons in flow units was calculated using a regression model as had been done in Section 4.1.4.2. The reference levels for the categorical variables are the same as shown in Table 4.2 with the addition of the security and floor warden reference level being those that required less than 600 s to be first seen in the stairs and counterflow as not experiencing it. As defined in Section 4.2.2.5, the effective normalized descent time of the previous flow unit was included for those occupants that had a preceding flow unit by subtracting that value from the effective normalized descent time. For those occupants that did not, a dummy variable was included to account for them not having a time from the previous flow unit. The coefficients of the model are shown in Table 4.12.

Table 4.12: Free-Flow First Persons in Flow Units Full Model Coefficients

	Unstandard. Coefficients.		Standard Coefs.	t	Sig.	95% Confidence Interval for B	
	B	Std. Err.	Beta			Lower Bound	Upper Bound
Const.	-.004	0.028		-.166	.869	-.059	.049
Female	.051	.018	.069	2.875	.004*	.016	.086
Carrying	.000	.018	.000	-.005	.996	-.036	.036
Large	.031	.033	.021	.933	.351	-.034	.097
Lane Flow	.006	.100	.001	.064	.949	-.190	.203
Inner Lane	-.012	.028	-.012	-.432	.666	-.066	.042
Outer Lane	.031	.022	.040	1.443	.149	-.011	.074
Travel Distance	.000	.000	.010	.424	.672	.000	.000
Pre-Obs. Time	.000	.000	-.117	-4.743	.000*	.000	.000
> 600 s Pre-Obs.	-.153	.030	-.128	-5.087	.000*	-.212	-.094
Counter	-.010	.036	-.007	-.303	.762	-.082	.060
First Seen	1.019	.054	.430	18.779	.000*	.912	1.125

*Significant based on 95% confidence level

Due to the apparent insignificance of the carrying, body size, flow type, counter flow, travel distance, and inner lane variables, a reduced model was determined with those coefficients excluded. Those coefficients are shown in Table 4.13.

Table 4.13: Free-Flow First Persons in Flow Units Reduced Model Coefficients

	Unstandard. Coefficients.		Standard Coefs.	t	Sig.	95% Confidence Interval for B	
	B	Std. Err.	Beta			Lower Bound	Upper Bound
Const.	-.003	.020		-.147	.883	-.043	.037
Female	.051	.017	.068	3.017	.003*	.018	.084
Outer Lane	.036	.017	.046	2.082	.038*	.002	.070
Pre-Obs. Time	.000	.000	-.118	-4.800	.000*	.000	.000
> 600 s Pre-Obs.	-.155	.029	-.130	-5.266	.000*	-.213	-.097
First Seen	1.013	.053	.428	19.031	.000*	.909	1.118

*Significant based on 95% confidence level

All of the variables are found to be significant. Comparing the full and reduced model, the F-statistic is 0.228, which results in a p-value of 0.968. Thus, it is a valid reduced model. The predicted and actual values are shown in Figure 4.13.

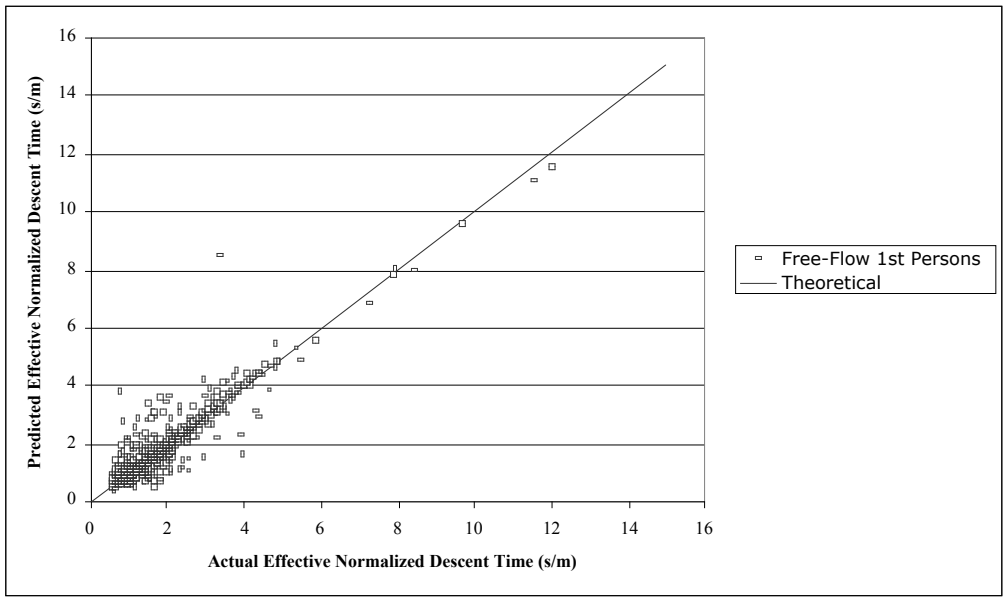

Figure 4.13: Predicted vs. Actual Values for Free-Flow First Persons in Flow Units

4.2.5.3 First Persons in Flow Units with Interactions

There were 3,368 first persons in flow units that were not free-flow first persons in flow units. For these first persons in flow units the full regression model looked at all of the independent variables crossed with the different first persons in flow units types (with first persons in flow units experiencing congestion being the reference case). For the crossed variables, only those variables that would contain at least 10% of the total population were included. Thus, all crosses with allowing occupants to enter, being large, counterflow, and not starting until after 600 s were excluded. Also, the two open tread crosses had the same issue, so those were grouped with the less than two open tread crosses. The final set of crosses that fell below 10% were for the first persons in flow units in the middle. The reference values for the crosses between exit lane and passing or being passed were modified to have being in the middle included with one of the crosses in line with the findings in Sections 4.2.3.1 and 4.2.3.2. Being passed crossed with exit lane included the inner lane and middle for the reference level. For passing crossed with exit lane the outer lane and being in the middle were included in the reference level. The dependent variable was the difference between the first persons in flow units' effective normalized decent time and the effective normalized descent time of the previous first person in a flow unit as defined in Section 4.2.2.5. These values are shown in Table 4.14.

Table 4.14: First Persons in Flow Units Other Than Free-Flow Full Model Coefficients

	Unstandard. Coefs.		Standard. Coefs.	t	Sig.	95% Confidence Interval for B	
	B	Std. Err.	Beta			Lower Bound	Upper Bound
Const.	.072	.030		2.366	.018*	.012	.131
Pass	-.152	.060	-.220	-2.523	.012*	-.270	-.034
Passed	.311	.052	.465	5.932	.000*	.208	.414
Allow Entering	.120	.021	.108	5.730	.000*	.079	.161
Female	-.001	.016	-.002	-.070	.944	-.033	.030
Carrying	.002	.017	.003	.109	.913	-.031	.035
Large	.008	.022	.006	.364	.716	-.036	.052
< 2 Open Treads	-.031	.028	-.046	-1.102	.271	-.086	.024
2 Open Treads	-.020	.029	-.027	-.710	.478	-.077	.036
Lane Flow	.008	.029	.013	.289	.773	-.048	.065
Inner Lane	-.020	.018	-.031	-1.089	.276	-.056	.016
Outer Lane	.020	.016	.033	1.229	.219	-.012	.052
Travel Distance	.000	.000	-.084	-3.201	.001*	-.001	.000

	Unstandard. Coefs.		Standard. Coefs.	t	Sig.	95% Confidence Interval for B	
	B	Std. Err.	Beta			Lower Bound	Upper Bound
Pre-Obs. Time	.000	.000	-.061	-2.398	.017*	.000	.000
Counter.	-.016	.070	-.004	-.225	.822	-.153	.121
> 600 s	-.269	.055	-.086	-4.878	.000*	-.377	-.161
Pre-Obs. Pass and Female	.010	.027	.012	.376	.707	-.043	.064
Pass and Carrying	-.018	.030	-.023	-.600	.548	-.077	.041
Pass and Treads	.138	.056	.196	2.458	.014*	.028	.248
Pass and Lane Flow	-.008	.036	-.008	-.217	.828	-.078	.062
Pass and Inner Lane	.034	.026	.040	1.319	.187	-.017	.085
Pass and Travel Distance	.000	.000	-.038	-1.211	.226	-.001	.000
Pass and Pre-Obs.	.000	.000	-.081	-2.246	.025*	-.001	.000
Passed and Female	.041	.027	.052	1.518	.129	-.012	.094
Passed and Carrying	.009	.028	.012	.326	.744	-.046	.065
Passed and Treads	-.159	.046	-.231	-3.458	.001*	-.249	-.069
Passed and Lane Flow	-.057	.035	-.065	-1.633	.103	-.126	.012
Passed and Outer Lane	.002	.025	.003	.080	.937	-.047	.052
Passed and Travel Distance	.000	.000	-.027	-.893	.372	-.001	.000
Passed and Pre-Obs.	.000	.000	.022	.587	.557	.000	.000

*Significant based on 95% confidence level

Many of the terms appeared to be insignificant, so a reduced model was tested that eliminated the variables that were not significant or did not cause a significant change in the F-statistic. The coefficients of this model are shown in Table 4.15.

Table 4.15: First Persons in Flow Units Other Than Free-Flow Reduced Model Coefficients

	Unstandard. Coefficients		Standard. Coefs.	t	Sig.	95% Confidence Interval for B	
	B	Std. Err.	Beta			Lower Bound	Upper Bound
Const.	.044	.014		3.093	.002*	.016	.071
Pass	-.133	.050	-.193	-2.656	.008*	-.232	-.035
Passed	.339	.037	.505	9.170	.000*	.266	.411
Allow Entering	.113	.020	.101	5.618	.000*	.073	.152
Outer Lane	.029	.011	.049	2.717	.007*	.008	.050
Travel Distance	-.001	.000	-.110	-6.339	.000*	-.001	.000
Pre-Obs. Time	.000	.000	-.052	-2.606	.009*	.000	.000
> 600 s Pre-Obs.	-.261	.055	-.083	-4.760	.000*	-.368	-.153
Pass and Treads	.110	.048	.157	2.312	.021*	.017	.204
Pass and Pre-Obs.	.000	.000	-.093	-2.793	.005*	-.001	.000
Passed and Female	.046	.020	.058	2.264	.024*	.006	.085
Passed and Treads	-.189	.036	-.274	-5.190	.000*	-.260	-.117
Passed and Lane Flow	-.049	.020	-.056	-2.475	.013*	-.088	-.010

*Significant based on 95% confidence level

All of the variables were significant in the reduced model. The different first persons in flow units types were significant as were being in the outer lane, effective stair travel distance, pre-observation time, and requiring more than 600 s of pre-observation time. For the interaction terms, passing and being within three treads, passing and pre-observation time, being passed and gender, being passed and being within three treads, and being passed and flow type were all significant. The F-statistic comparing the reduced and full model is 0.401, which results in a p-value of 0.99. Thus, the reduced model is valid. The actual and predicted values for all of the first persons in flow units not being free-flow first persons in flow units are shown in Figure 4.14. The R^2 value for these first persons in flow units is 0.86.

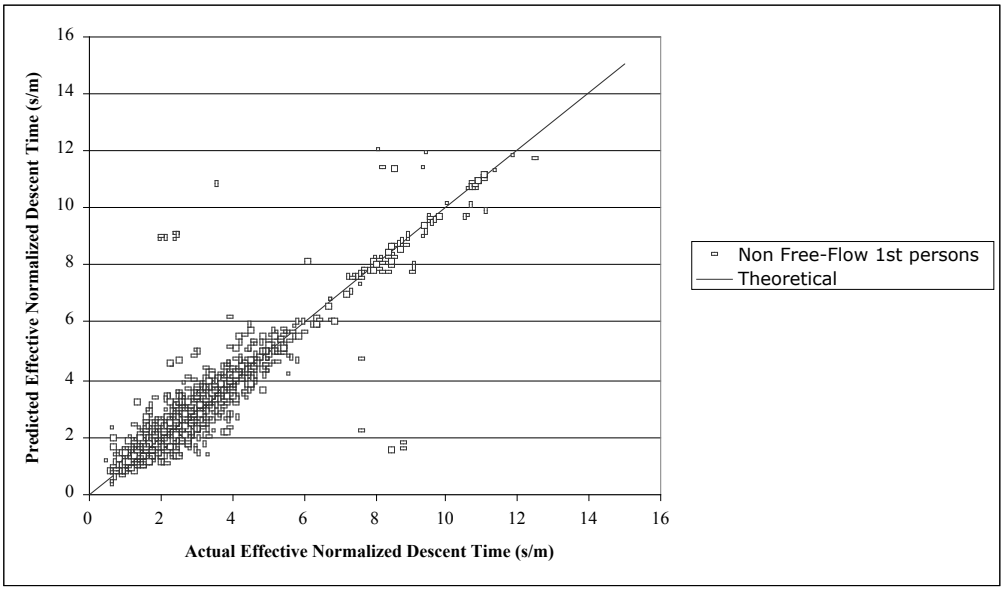

Figure 4.14: Predicted vs. Actual Values for Non Free-Flow First Persons in Flow Units

4.2.5.4 All Occupants

When all three types of occupants are combined, the actual and predicted values are shown in Figure 4.15.

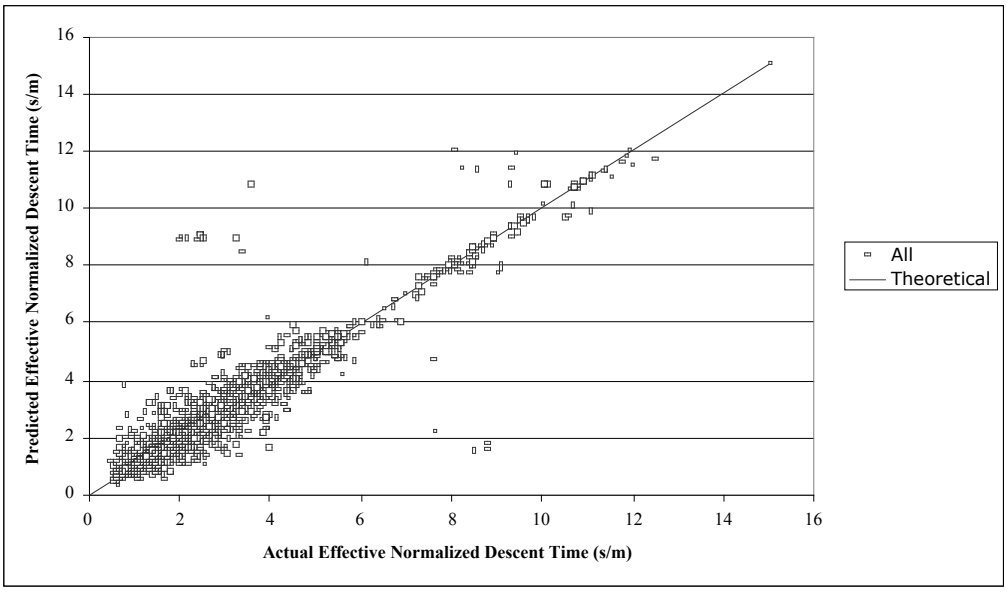

Figure 4.15: Predicted vs. Actual Values for all Occupants

The R^2 value for all occupants is 0.90.

4.3 Blind Application of Models

The previous sections developed equations based on data that was collected and then applied to that same data to demonstrate the accuracy of the models. While this will demonstrate internal consistency, it does not demonstrate how accurate methods are if applied to other data. In this section, an equation relating just effective normalized descent time to effective density[3] and the model equation will be applied to data not used to generate either.

The stair selected for this analysis is Stair 3 in Building 7 from the NIST data set. The spring 2008 drill had test conditions similar to the other buildings previously used (regular working hours, before lunch). The 18-story building was located on the east coast of the United States. Cameras were placed on Floors 5 (discharge level), 7, 9, 11, 13, 15, and 17. The stairs were 1.12 m-wide, with 16 or 19 steps per level, and were 19.0 cm high by 25.4 cm deep. A total of 312 people were observed 1,319 times and there was a resulting 1,007 data points.

The effective normalized decent times varied from 0.75 to 6.71 s/m. The mean effective normalized descent time was 2.48 s/m with a standard deviation of 1.11 s/m. This mean value was less than the one from the stairs described in Section 4.2.

As was shown in Chapter 1, previous researchers have claimed that there are combinations of treads and risers that allow occupants to more easily descend stairs. This was confirmed with work by Templer (1975) and is seen in the SFPE Handbook (2008) in the form of k-values for different riser height and tread depth combinations. However, the SFPE Handbook (2008) does not provide a method for calculating k-values for stair dimensions other than the four that they provide. In this case, the k-value is 1.00 (compared to 1.08 for the previous data).

Three k-values will be used to compare the accuracy of the effective density equation. The first k-value will assume that it is one for all stair configurations; essentially, this means that the different riser heights and tread depths can change the travel distance, but there is no other change in effective normalized descent time. This was the method used by Pauls (1980) that was a primary source for developing the SFPE Handbook (2008) equation.

The second k-value will use the method described by Pauls (1984). In this case, 1/k is increased by 1% from 1.08 for every 0.5 cm increase in tread depth from 28 cm or 0.5 cm decrease in riser height from 18 cm (where each change is a maximum at 10%). Because k is proportional to speed, 1/k is proportional to the effective normalized descent time. With Building 7, the effective normalized descent time would be 1.07 times the values from the previous analysis.

[3] As mentioned previously, the methods used to calculate area and travel distance in the SFPE Handbook are unknown. To ensure that the comparisons are fair, an equation similar to the SFPE Handbook equation is presented.

The third k-value is developed based on the assumption that the time to descend a floor is constant. Proulx (2008), Kagawa, Kose, and Morishita (1985), and Melinek and Booth (1975) all give similar values for the time to descend one floor. Figure 4.16 shows the specific flow equations from the SFPE Handbook (where the effective specific flow is the effective speed multiplied by the effective density) and the equation that relate the descent speeds to the 17.8 cm riser height and 27.9 cm tread depth case for the 19.0 cm riser height, 25.4 cm tread depth case.

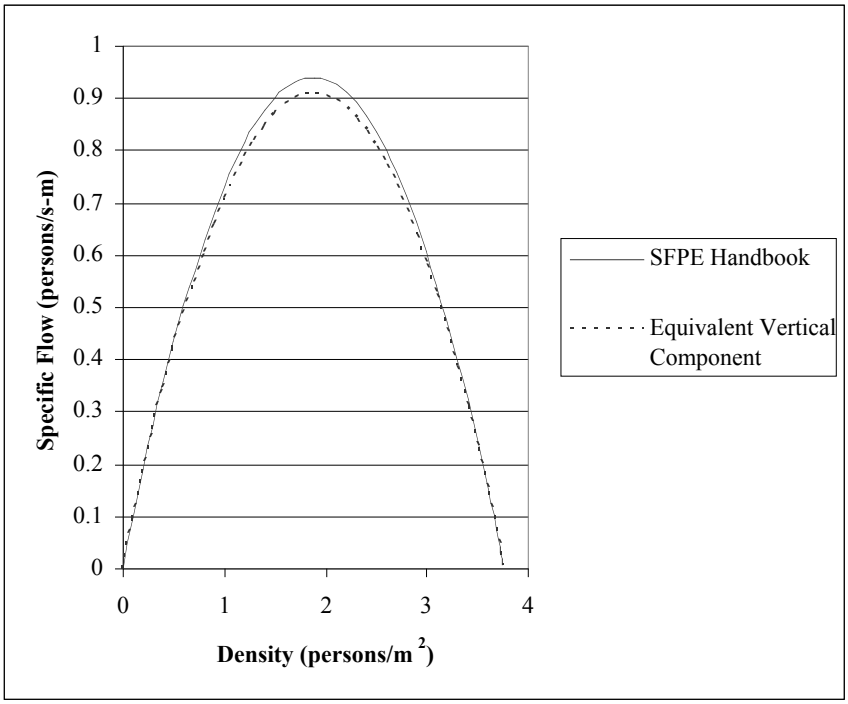

Figure 4.16: SFPE Handbook and Constant Vertical Descent Time Prediction

The curve produced nearly matches the SFPE Handbook (2008) equations (less than 4% difference). Because the SFPE Handbook (2008) does not provide a method for determining k-values, this alternate method will be tested that could then be tested and subsequently applied to a wider range of stair dimensions. In this case, the effective normalized descent times would be 1.12 times the values from the previous analysis.

4.3.1 Effective Density Equation

From the data used in Section 4.2, the equation that provides the best linear fit between effective normalized descent time and density is:

$$t = 0.97 + 0.76 \cdot D \qquad (4.6)$$

where:

t=effective normalized descent time (s/m)
D=effective density (persons/m^2)

This equation will be used to test the different k-values for the relationship between stair dimensions, effective normalized descent time, and density.

4.3.1.1 No k-value

When no k-value is applied, Equation 4.5 results in a predicted mean effective normalized descent time of 2.40 s/m (standard deviation of 0.52 s/m). The R^2 value for this model is 0.34. The actual and predicted values are shown in Figure 4.17.

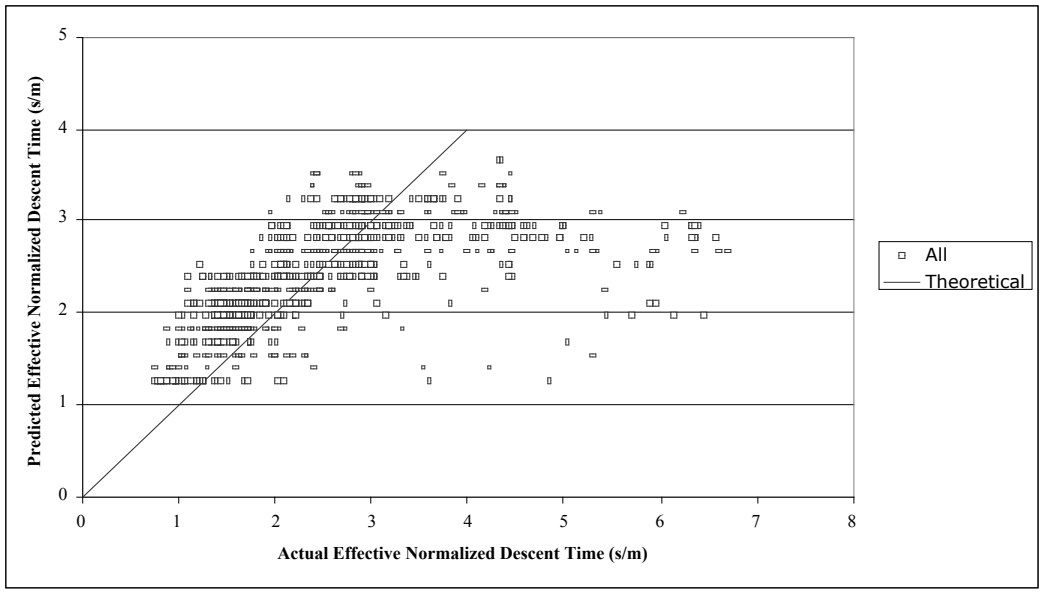

Figure 4.17: Predicted vs. Actual Values for No k-value Data Set

With the exception of the occupants that were caught in the queue, the equation tends to overestimate the effective normalized descent time.

4.3.1.2 Pauls (and SFPE Handbook) Method

Applying a coefficient of 1.07 to Equation 4.5 results in a predicted mean effective normalized descent time of 2.57 s/m (standard deviation of 0.56 s/m). The R^2 is again 0.34. As shown in Figure 4.18, this equation provides a more conservative estimate for the occupants.

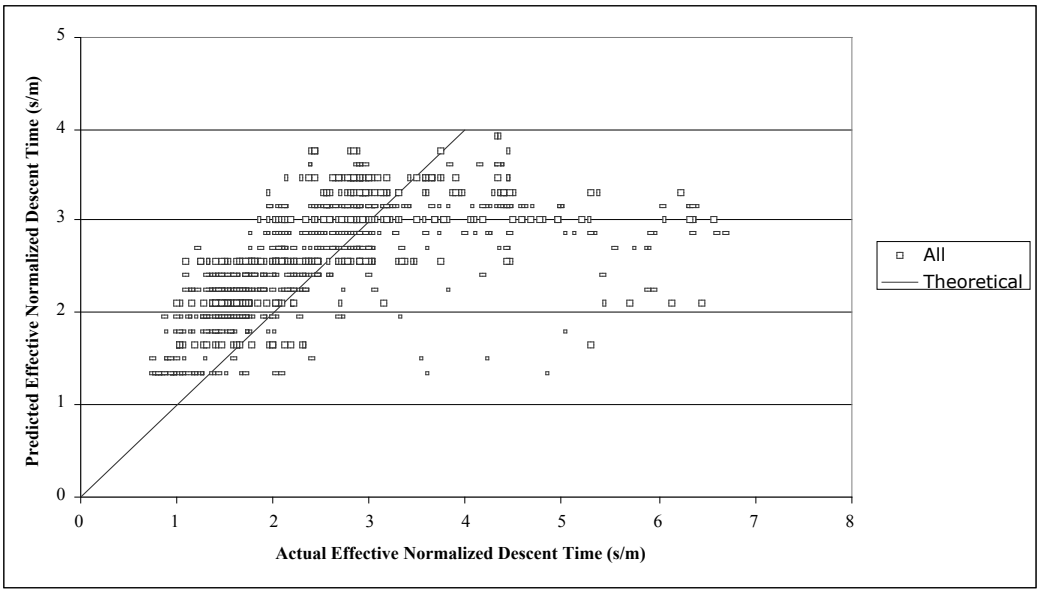

Figure 4.18: Predicted vs. Actual Values for Pauls k-value Data Set

4.3.1.3 Equivalent Time per Floor

For the final k-value, multiplying Equation 4.5 by 1.12 results in a predicted mean effective descent time of 2.68 s/m (standard deviation of 0.58 s/m). The R^2 value was slightly less than the other k-values; it was 0.32. However it was also the most conservative with more of the data point lying above the theoretical prediction line (see Figure 4.19).

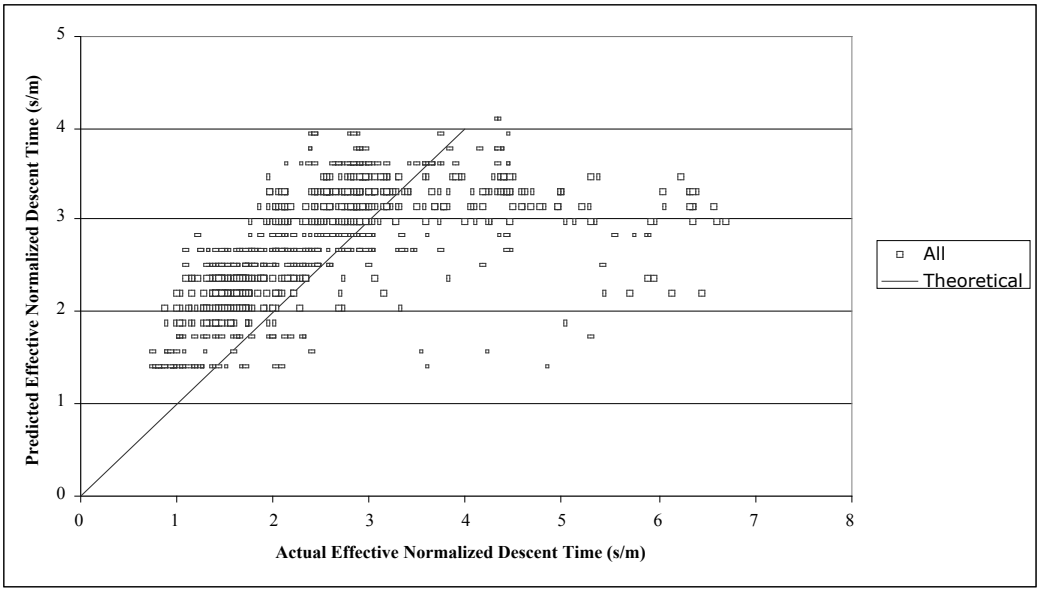

Figure 4.19: Predicted vs. Actual Values for Equivalent Descent k-value Data Set

4.3.2 Model Equations

When the predictions developed in Section 4.2.5 are applied to the data from Building 7, Stair 3, the R^2 value is 0.88. This is within 3% of the R^2 value for the data on which the models were developed. As was the case with the observations used to initially develop the models, most of the data lies along the prediction line with some outliers (due primarily to queuing). The predicted values plotted against the actual values are shown in Figure 4.20.

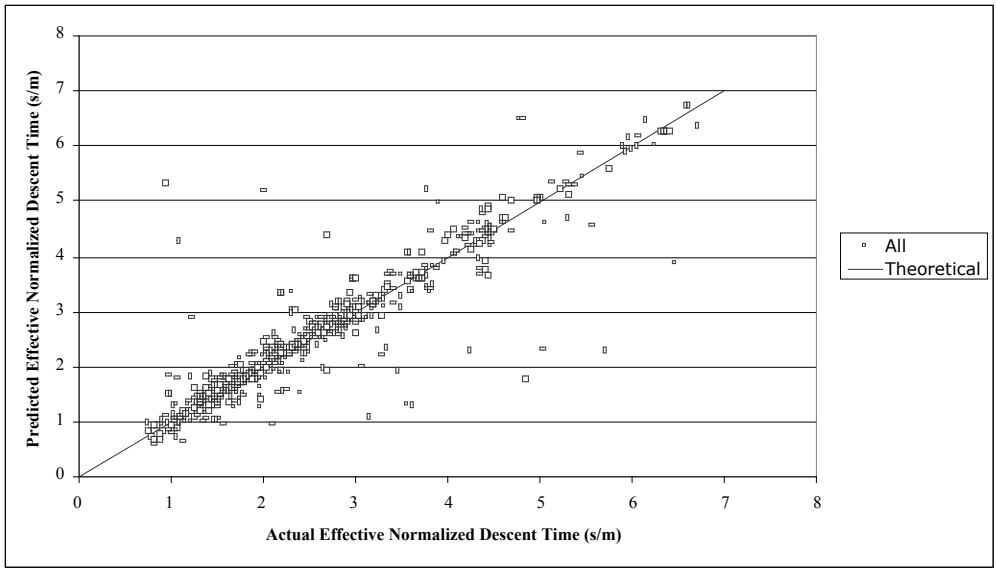

Figure 4.20: Predicted vs. Actual Values for Blind Data Set

4.4 Summary

While previous studies involving people descending stairs focused on speed and density, this relationship was shown to be a relatively poor predictor and biased towards faster moving individuals. To account for the bias towards the faster individuals, the inverse of speed was used. To improve the accuracy of the models, two types of analysis were conducted. The first focused on light density conditions where it was possible to isolate variables without the dynamics of a crowded evacuation. For the second, more crowded evacuations were observed.

For the first analysis section, occupants were observed to be traveling in flow units and the followers were descending at the same basic rate as the first person. By controlling for these first persons, it was then possible to observe some of the effects that were being masked (e.g., gender being significant). A regression model was applied that accounted for nearly two-thirds of the error.

The variables identified in the light density case were then applied to six stairs with heavier densities. In addition, new variables were developed (i.e., flow type, first person in flow unit type, and previous flow unit). When these variables were used to

develop a regression model, the resulting numerical models explained approximately 90% of the error.

In the final section, these results were applied to a blind data set. The density equation (with various k-values applied) explained approximately one third of the error. The numerical models developed in Section 4.2.5 explained 88% of the error.

Chapter 5: Discussion

In Chapter 4, data was presented that looked at a simple building (in terms of the evacuation dynamics) and then preceded to examine more complex evacuations. From this complex set of data, predictions were made for the evacuation from a blind set of data. In this chapter, the implications of these various findings will be discussed in greater detail in this chapter.

5.1 Using Effective Normalized Descent Time in Place of Effective Speed

As shown in Chapter 3, the predictions for effective speed are more sensitive to individuals that are moving fast rather than those that are moving slow. The data from Buildings 4, 5, and 8 can be used to demonstrate the difference for actual data.

5.1.1 Effective Speed

The equation relating effective speed and effective density that best fits the data from Section 4.2 is:

$$s = 0.86 - 0.19 \cdot D \tag{5.1}$$

where:

s=effective speed (m/s)
D=effective density (persons/m^2)

The equation and data are shown in Figure 5.1.

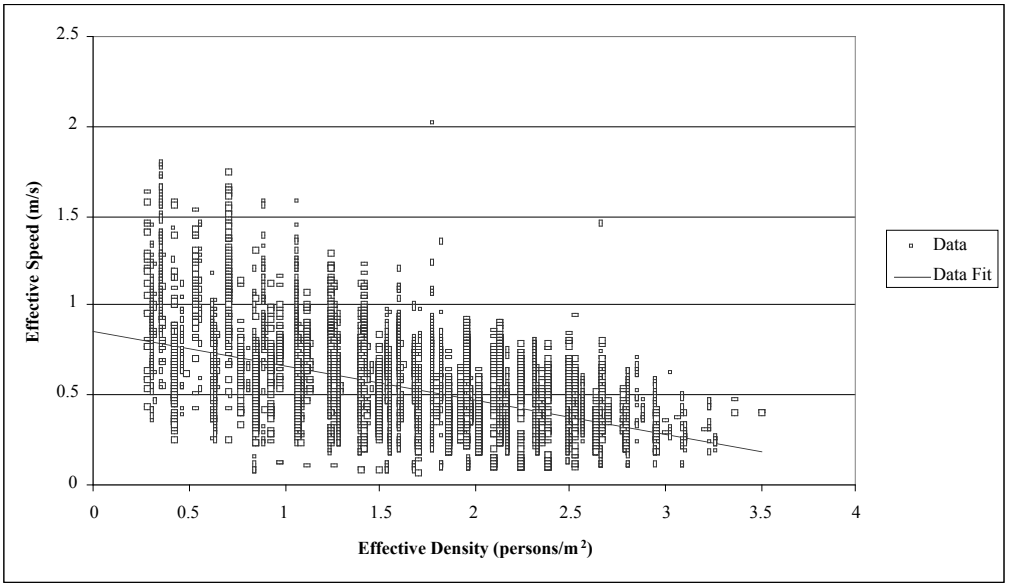

Figure 5.1: Effective Speed and Effective Density

The R^2 value for this correlation is 0.26.

5.1.2 Effective Normalized Descent Time

Recall that the equation for predicting effective normalized descent time based on effective density was:

$$t = 0.97 + 0.76 \cdot D \tag{5.2}$$

where:

t=effective normalized descent time (s/m)
D=effective density (persons/m^2)

and that the R^2 value was 0.15. Graphically, this is shown in Figure 5.2.

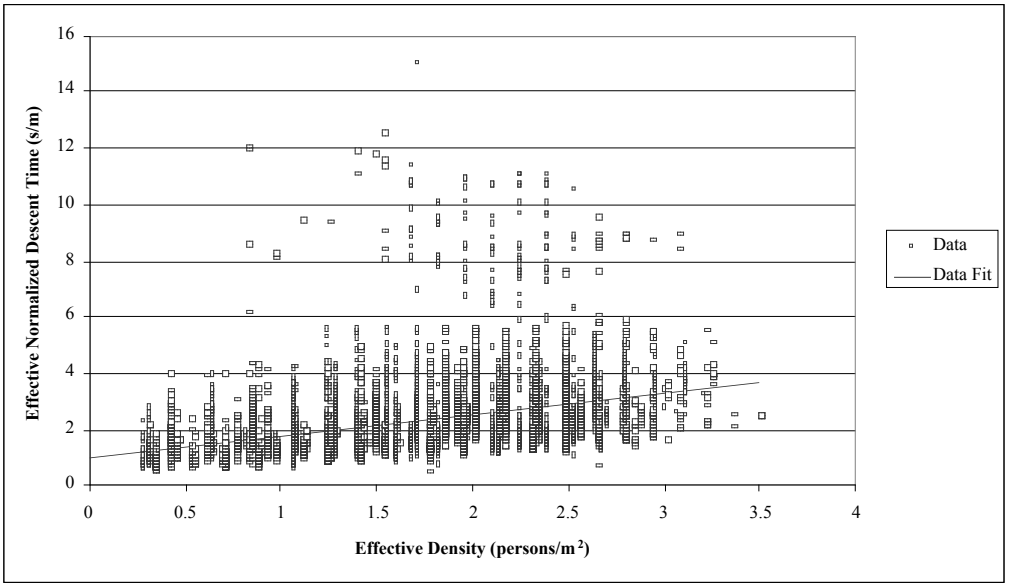

Figure 5.2: Effective Normalized Descent Time and Effective Density

5.1.3 Comparisons of Means

The mean value of the effective normalized descent time was 2.28 s/m (with a standard deviation of 1.16 s/m). The inverse value is 0.44 m/s. The mean effective speed was 0.53 m/s (with a standard deviation of 0.22 m/s). Thus, the mean effective speed is 120% of the inverse of the mean normalized time. The cause of this disparity (and the cause of the smaller R^2 for the normalized time) is that the occupants that require much more time have a relatively small change in effective speed compared to those occupants that require more time.

5.1.4 Implications

As shown in Equation 3.5, the methods based on effective speed are always going to be more sensitive to the faster moving occupants. When the goal is to ensure that all occupants can make it out in a timely manner, calculations involving descent time allow for better consideration of the slower occupants. While speed has traditionally been the dependent variable for similar types of studies (see Chapter 2), it is for this reason that the effective normalized descent time has been used in the previous analysis.

5.2 Using Number of Treads in Place of Density

Just as previous studies have used speed as the dependent variable, density has been the independent variable. In this analysis, the number of open treads to the next occupant was used. Both density and the number of open treads account for the spacing to other occupants, but they do so in different ways. Density assumes that all of the people in a given area influence how fast an occupant can move and conditions are homogeneous. However the variables that were newly introduced in this study (see Section 5.5.1 and Section 5.5.2) found that this was not the case.

In the lane flow condition, two occupants that have the same effective density (one in the inner lane and one in the outer lane) move at different descent rates (Section 5.5.2) because, by definition, the occupants in one lane are passing occupants in the other lane. Thus, the descent rate is determined based on the interactions and characteristics of the first person in the flow unit rather than a measurement of the number of persons in the observation area. The regression equations (Section 4.2) demonstrated that the interactions and individual characteristics of the first persons were determining the descent rate even during uniform flow.

It is from these first persons in flow units that many of the findings were derived. As will be discussed subsequently (Section 5.4), the exclusion of considering flow units potentially led to discrepancies in the referenced studies. In this study, when occupants left three open treads between themselves and other occupants, they had more control over their own descent time. At two treads or less, the followers simply moved at the descent rate of the first person in their flow unit. In other words, the number of open treads appears to be a way to capture how occupants are interacting in a meaningful way while the traditional density measurement does not.

Slower first persons in flow units can collect more people behind them than faster moving ones can simply because more people can catch up to their flow unit from behind. This leads to a greater density behind the slower moving occupant (and the occupants behind them moving at the same slower rate). The occupants maintained a spacing between one another (with the qualitative minimum usually being staggered file or shoulder to should with an open tread), but the first persons in flow units were setting the pace for everyone else rather than the speed being set by the number of

people in the observation area. Thus, the first persons are influencing both the descent rate and the density.

The number of open treads and effective density should be used as independent variables under two very different circumstances. For a sophisticated computer model with an individual perspective that is considering many variables, the spacing based on the number of open treads is a more appropriate means of determining the descent time. When used in conjunction with the other variables described in this study, the predictive power of the open treads is much stronger than relying on effective density alone. On the other hand, for a simple algebraic equation, the number of open treads is not as well suited as an independent variable because of the lack of the other flow dynamics in the equations. Effective density can instead be used as a proxy that incorporates many of the variables that are present.

5.3 Flow Units

One of the most important findings of this research was dividing the occupants into flow units. The studies in the literature treated each occupant as an individual. While it was recognized that others around the individual would make a difference (with respect to density), all other interactions were not considered.

In Section 4.1, some of the flow units could easily be seen as plotting exit times showed clearly defined platoons. If all occupants were acting independently, this would not be seen. Instead, the occupants would be randomly scattered throughout the evacuation period.

While the data in Section 4.2 did not have as lengthy of separations between platoons, it was still relatively easy to identify where the different flow units were located. The interactions became more significant as they led to different types of flows occurring.

In Section 4.1, predicting the followers effective normalized descent time based on the effective normalized descent time of the first person in their flow unit resulted in an R^2 value of 0.99. Even for the more complex conditions in Section 4.2, the R^2 value was 0.93 (including some outliers caused by queuing). Thus, the followers were not freely choosing their own descent time but were instead dependant on others.

As will be discussed more in Section 5.4, some levels of variables were significant when looking at the entire population and not significant when controlled for first persons in flow units and followers (or the other way around). By separating the population into different flow units, it became possible to eliminate many of the masking characteristics from the followers; treating followers the same as first persons in flow units prevented the true dynamics from being seen because the followers were not acting independently.

Followers need to be considered differently than the first persons in flow units for making predictions about effective normalized descent times (or effective speeds). The adoption of flow units into sophisticated computer models will allow for a more accurate representation of the evacuation. This effect was found to be far stronger than the effect of effective density. Ignoring the fact that there are slow moving flow units would lead to estimates that are not conservative. From a life safety perspective, accounting for these flow units will make it more possible that all occupants are provided with an adequate level of safety.

5.4 Literature Variables

Seven variables that were mentioned in the literature (gender, carrying items, body size, exit lane, fatigue, pre-observation time, and counterflow) were studied in this research. Discussion will be provided regarding the findings from the research as well as how those findings align with the previous research.

5.4.1 Gender

The previous studies were divided as to whether gender was significant (e.g., Fruin, 1971) or not (e.g., Peacock, Averill, and Kuligowski, 2009) in determining movement speed. Proulx, et al. (1995) found that it was significant in one case, but not in others. These sources did not provide any explanations as to why there were contradictory findings.

In this study, comparisons were made based on gender while controlling other important variables. In Building 6, 54% of the data points were for occupants identified as being female. Similarly, in the buildings from Section 4.2, 55% of the data points were for occupants identified as being female. For all of the comparisons, the expected counts for a given gender are calculated based on these percentages.

5.4.1.1 Effective Normalized Descent Time

In Building 6, when looking at all occupants, there were no statistical differences between the descent times of men and women. However, when looking at just first persons in flow units, females required more effective normalized descent time. This was also apparent in the regression model for the first persons in flow units in Building 6 and the free-flow first persons in flow units in the other buildings. As shown previously, the followers had the same effective normalized descent times as the first person in their flow unit. While the raw data that the other researchers used is not available, a likely explanation is that the studies that found no significance based on gender had a larger percentage of followers than those that did.

While females that were first persons in flow units experiencing free-flow conditions required more effective normalized descent time than their male counterparts, when controlling for the other variables in the regression equation, the only type of first person in a flow unit that gender was significant for determining the effective normalized descent time was for first persons in flow units that were passed; the first

persons in flow units that were passing, allowing other occupants to enter, or experiencing congestion did not have different effective normalized descent times based on gender. Female followers were able to move at the same descent rate as males that were the first persons in flow units. Across all buildings, for the instances where the interactions dominated, there were typically no differences based on gender. For the situations where individual effects dominated, males descended faster than females.

Based on this research, it cannot be concluded whether the cause of females requiring more descent time was a result of physiological factors or if it was the result of other factors (e.g., wearing high heels). Regardless of the cause, algebraic equations and computer models should account for this difference in descent time based on gender.

5.4.1.2 First Persons in Flow Units and First Follower Pairs

The combinations of first persons in flow units and followers based on gender were not random. For both males and females, the first persons in flow units and first follower pairs were more likely to be of the same gender rather than opposite genders. Social effects or followers staying with people that have similar descent times could cause this.

Aside from not being random as to whom they were following, the spacing between the first followers and the first persons in flow units was dependent on the gender of each person. Females that were first persons in flow units had female followers that stayed closer to them than male followers. Female followers left more distance to males that were the first persons in flow units than comparable females. For males that were the first persons in flow units and male followers, none of the spacings based on gender were significantly different than expected in the χ^2 tests. Fruin (1971) noted this type of behavior with regard to tests involving elevators. For the elevators, it was found that males left the same (larger) spacing regardless of the gender of others while females would have the larger spacing around men, but a smaller spacing when around other females.

Also, when comparing the first persons in flow units and the first followers, females with males as their first follower descended at a faster rate than those with females as their first follower. Similarly, males with male first followers descended at a faster rate than those with female first followers. It would appear from this finding that the opposite gender pairings of first persons in flow units and first followers occur when the first person in the flow unit is similar to the opposite gender (faster females followed by males and slower males followed by females).

For the different density equations presented in Chapter 2, none of the authors mentioned accounting for the genders of the different occupants. With female-female pairings, the density would be higher than any of the others because females followed other females closer than any other pairing. As such, the curves would be less conservative when applied to the other pairings. Because these pairings were found to occur more often than was expected, this shift is more likely to have occurred.

Especially in sophisticated computer models, this decrease in spacing based on gender (and the prevalence of gender pairs) should be incorporated when there are other distinctions made based on gender.

5.4.1.3 Differences in First Persons in Flow Units Gender Based on Effective Density

In Building 6, the first persons in flow units were more likely to be female while in Building 4, 5, and 8 combined, the free-flow first persons in flow units were more likely to be male (see Appendix C). A possible explanation for this is the relationship between the first persons in flow units and follower pairs and the other first persons in flow units types. In Building 6, the females that were first persons in flow units entered the stairs and were able to proceed freely. In the other buildings, the comparable first persons in flow units were being passed and were thus not free-flow first persons in flow units; this corresponds to females that were first persons in flow units being passed more than expected. On the other hand, the males that were first persons in flow units did not have this same interaction with the different type of first persons in flow units and thus their proportion of free-flow first persons in flow units increased.

5.4.1.4 Different Characteristics

After controlling for first persons in flow units and followers, the only characteristic that was different was carrying items. It was consistently found that women were more likely to be carrying items. This is consistent with Kratchman (2007). All of the other categorical variables considered in Chapter 4 were the same based on gender.

5.4.1.5 Implications

Many of the findings regarding gender are complimentary to the previous findings. First, the findings regarding gender are another demonstration that occupants are not randomly entering the stairs and the gender pairings could be indicative of underlying group dynamics. By understanding how these flow units form and move, it will be possible to better model how occupants will behave in an actual event. Second, the effective normalized descent times of females that were first persons in flow units are longer. The contradictions in previous research likely come from not properly separating out the first persons in flow units from the followers before looking at the differences in speed based on gender.

For sophisticated models that apply different characteristics to each occupant, gender should be included to account for the longer effective normalized descent times found for female free-flow and passed leaders. These same models should also take into account the difference in spacings based on gender (and the fact that gender seems to play a role in the flow units within the stairs). Even for developing algebraic

equations, a more conservative approach would be to exclude female-female pairings that would tend to lead to higher observed densities.

5.4.2 Carrying

Proulx (1995) had found that occupants carrying items moved at the same speed as other occupants. Peacock, Hoskins, and Kuligowski (2011) found that occupants carrying items moved slower than others. As was the case with gender, no consistent finding had been made.

In the analysis in Chapter 4, carrying items was not seen to be significant in predicting effective normalized descent time no matter what methods were used. From this work, it could be interpreted that carrying items do not affect descent time, but there are several limitations in how the variable was measured. First, there was no differentiation based on what was carried. Thus, a cell phone in one hand was considered to be the same as a heavy bag. By not being able to differentiate carrying items based on the size and weight of the object carried (or the strength of the person carrying it), the occupants that were truly slowed down due to the object that they were carrying would be washed out by the other data points. Second, there was no differentiation made based on how the item was carried. For example, a backpack that did not prevent the ability to hold onto the handrail was treated the same as a large box requiring both hands (and a forward shifted center of gravity). Third, there was no way of controlling for how routine it was for the individual to carry that item. Someone that was used to descending a stair while carrying a particular item might respond differently than someone that did not normally have that item.

Form this study, no guidance can be provided on how to incorporate occupants that carry items or whether such a designation is meaningful or not. However the methodology used here is aligned with the previous research that found that carrying objects did not significantly change the expected speed (or effective normalized descent time).

5.4.3 Body Size

Pauls, Fruin, and Zuppan (2005) stated that the population being more obese would lead to a slowing down of the population. If this were true, then the larger individuals would be shown to be moving slower than the rest of the population. Previous research (e.g., Galea, et al., 2009) has not found this effect. For another effect from body size, Kendik (1986) and Predtechenskii and Milinskii (1978) based density on body size. Larger occupants would lead to fewer persons per unit area, so the equations that were developed in the past would over predict speeds if these assumptions are true.

In Building 6, the first persons in flow units with a large body size required a statistically greater amount of effective normalized descent time in the regression model, but the effective normalized descent times were not different between large occupants (or first persons in flow units) and the other occupants (or first persons in

flow units). However, in the other buildings, the effective normalized descent time of the large occupants that were first persons in flow units was not significant in the regression models. One possible explanation for this discrepancy is that there were only sixteen large individuals in Building 6. With so few observations, each individual would have significant influence on the coefficient. Thus, the findings of this study are more in line with Galea, et al. (2009) rather than Pauls, Fruin, and Zuppan (2005).

One finding of note was that large occupants that were first persons in flow units were less likely to be passed than the other first persons in flow units. From this, it appears as if they can limit the flow around them. Because they were found to descend at the same rate as other occupants, this would not appear to alter the descent time. While on average they do not appear to be slower, some large individuals will be, as seen in Building 6. In this case, it would lead to other occupants requiring more time to descend.

5.4.4 Exit Lane

There were two different effects observed with respect to exit lanes. The first effect was the difference in effective normalized descent times based on exit lane. The second effect was the difference in usage of the exit lanes.

5.4.4.1 Effective Normalized Descent Time

The importance of which lane an occupant is in is emphasized when the occupants are engaging in lane flow rather than uniform flow (see Section 5.5.2). In the case of lane flow, the descent times in the two lanes can be considerably different. For the uniform flow, the exit lane should not make a difference.

This is why there were different results in Section 4.1 and Section 4.2. In Section 4.1, exit lane was found to not be significantly different for determining effective normalized descent time for the entire population, for the first persons in flow units, or when included in the regression model. However, in Section 4.2, where lane flow was taking place, the lane was significant for all different types of first persons in flow units, whether they were in the lane flow condition or not. A better understanding of what causes lane flow could indicate that there are more first persons in flow units engaging in it than were identified here (which would explain why the lane was significant even when the first persons in flow units was not identified as being engaged in lane flow). For example, it could be that the slower moving first persons in flow units choose to stay to the outside to allow faster flow units to pass on the inside. This was seen by passing first persons in flow units being more likely to be in the inner lane and passed first persons in flow units more likely in the outer lane.

5.4.4.2 Exit Lane Usage

There was another way that the exit lane varied from Section 4.1 to Section 4.2. In Section 4.1, first persons in flow units were more likely to be in the inner lane. However, in Section 4.2, the free-flow first persons in flow units were more likely to be in the outer lane. Examining the data from pairs of stairs in each section can provide a more detailed analysis.

For both stairs in Building 8 and stairs 6 and 6a in Building 6 the two stairs had the same dimensions. In each case, one of the stairs was a sinistral stair and the other was a dextral stair. The actual and expected values are shown in Table 5.1 for the free-flow first persons in flow units in the data from Section 4.2 and all of the first persons in flow units in Section 4.1.

Table 5.1: Actual and Expected Counts for Exit Lanes

Variable	Inner (Act)	Inner (Exp)	Middle (Act)	Middle (Exp)	Outer (Act)	Outer (Exp)
8S	111	68.0	38	28.1	48	100.9
8N	75	118.0	39	48.9	228	175.1
p-value	$5.8*10^{-11}$*		0.020*		$3.9*10^{-11}$*	
6-6	32	27.8	9	11.5	13	14.7
6-6a	21	25.2	13	10.5	15	13.3
p-value	0.25		0.28		0.53	

*Significant based on 95% confidence level

Templer (1975) stated that there are two tendencies for people while on the stairs as shown in Chapter 3. Building 8 saw the first persons in flow units stay to the right. In the dextral stair, this was the outer lane and in the sinistral stair it was the inner lane. The other situation is that people stay to the inside. In Building 6, both the sinistral and dextral stair saw first persons in flow units stay to the inside.

In the buildings in Section 4.2, the occupants stayed to the right. In the building in Section 4.1, occupants stayed to the inside. It is not clear if it was the different effective density levels or some other factor (i.e., Building 6 was the tallest building) that led to the first persons in flow units choosing to instead remain on the inside of the stair.

For sophisticated computer models, the outward shift of occupants in dextral stairs should be assumed. The shift to the inner lane seen in Building 6 would lead to shorter travel distances and thus assuming an outward shift would be more conservative. Also, as will be discussed more in Section 5.5.2, using an average value for the different lanes is not appropriate. For the more sophisticated models, the dynamics of the different lanes can be included. For the algebraic equations, the values should be based on the occupants in the outer lane. In this case, not

accounting for the faster inner lane occupants will make the equations more conservative from a life safety perspective.

5.4.5 Fatigue

While previous studies have stated that fatigue was present, this was seldom quantified. Building 6 provided an excellent opportunity to observe if fatigue was present. Not only is the building taller than most in the literature, but the lack of crowding provides evidence as to whether the assumption by Joint Committee (1952) that uninterrupted flows cause occupants to slow down is true or not.

When first persons in flow units were observed at two locations in Building 6 where they did not have to move through transfer corridors, the effective normalized descent time was slower at the second observation area. These observations were typically six floors apart and the slower effective normalized descent times were present after six stories, well within the heights of the other buildings.

The regression model in Building 6 also found effective stair travel distance to be significant when the other variables in the regression model were controlled. On the other hand, effective stair travel distance was not significant in the buildings in Section 4.2.

The data from this study agrees with the previous research. Specifically, it appears as if the assumption made by the Joint Committee (1952) has merit. For occupants that are able to freely descend, they slow down as they travel. In the cases of higher effective density, slowing down or stopping leads to each individual not experiencing a measurable change in effective normalized descent time.

To be conservative, estimates of descent time should account for any fatigue that happens. If the building experiences queuing, fatigue is not expected to play as large of a role.

5.4.6 Pre-Observation Time

Previous research involving pre-evacuation time has focused on the fact that it exists and how it influences when people enter the stair. There was little consideration given as to whether there was a difference in descent times for the occupants that started earlier compared to those that started later. For example, Proulx, Kaufman, and Pineau (1996) found that females descended faster and they found that females required less pre-evacuation time (but they did not connect the two findings).

If increasing pre-observation times led to greater effective normalized descent times, when the other variables are controlled for, then it would indicate that slower moving occupants are either slower to enter the stair or choose to wait longer so as to not hinder the evacuation of others. If instead the increasing pre-observation time has the opposite effect on the effective normalized descent time, then that would indicate that the delay is causing the occupants to experience a greater sense of urgency.

The results in this study were internally contradicting. In Building 6, for longer pre-observation time, more normalized descent was required. In the other buildings, the opposite effect was found; the longer that the occupants waited to start, the smaller their effective normalized descent time was. Further research is needed in order to understand why the results were different between the different buildings. Two possible explanations are that either the height of Building 6 made the slower occupants choose to wait longer because it was viewed as a more significant undertaking or that the increasing numbers of people meant that the occupants that entered the stair later were able to join with a pre-existing flow unit and matched its descent rate (which was faster than they would go in isolation).

5.4.7 Counterflow

Unlike some of the previous studies mentioned in Chapter 2, occupants experiencing counterflow did not descend at a statistically slower rate in this study. While it is possible that counterflow is not significant, the methods used to calculate the effective normalized descent time inherently make it appear to be so even if it is actually significant. The methods used based each flow unit's effective normalized descent time on that of the preceding flow unit. If the first person in the first flow unit were slowed by the counterflow, all subsequent first persons in flow units would be slowed due to the relationship to that flow unit. Thus, for all of those other first persons in flow units, it would appear as if counterflow was not significant and this would eliminate any of the effects seen with the first person in the first flow unit. Even considering just the data for the first person in the first flow unit that experienced counterflow would not be sufficient due to the possibility that the entire stair was slowed, even though the previous first person in a flow unit had been able to exit the observation area shortly before the firefighters arrived. Thus, the results in this study involving counterflow should not be interpreted to mean that counterflow does not significantly alter descent times.

5.5 Newly Developed Variables

Several of the variables that had been identified by previous research were found to be significant in determining the effective normalized descent times. Even with using effective normalized descent time instead of effective speed and number of open treads instead of effective density, there were other variables that needed to be developed that explained phenomena that were observed within the data. Most of these variables were directly related to defining flow units within the flow.

5.5.1 Occupant Types

Unlike the previous methods that treated each individual as acting individually, the data showed that occupants were actually functioning within flow units. There were five different types of first persons in flow units and followers that were identified.

5.5.1.1 Passing First Persons in Flow Units

As mentioned in Chapter 2, previous studies had observed occupants engaging in passing behavior. In this study, flow units were identified as engaging in passing behavior and all of the followers were said to be requiring the same effective normalized descent time as the first person in their flow unit.

The most significant difference between passing first persons in flow units and other first persons in flow units was that the passing ones tended to be on the inside lane. They were taking the shortest path and were thus able to move ahead of the other occupants. If the passing first persons in flow units were able to move beyond all of the other occupants in the stair, then they required the least amount of time to descend. However, if they were still within three open treads of other occupants, their descent times were comparable to first persons in flow units that experienced congestion.

As discussed in Section 5.4.6, a decrease in descent time with increasing pre-observation time would be indicative of a sense of urgency. The passing first persons in flow units had an even greater decrease in effective normalized descent time for a given pre-observation time (above and beyond the decrease associated with just being a passing first person in a flow unit). Thus, these first persons in flow units appear to have a greater sense of urgency than the other first persons in flow units do.

There were no differences in effective stair travel distance between the passing first persons in flow units and the other first persons in flow units. The urgency appeared to be something inherent to the individual or was based on the experiences on the floors before entering the stair. Once inside the stair, the urgency appeared to remain fixed.

5.5.1.2 Passed First Persons in Flow Units

The passed first persons in flow units were the counterparts to the passing first persons in flow units. While the passing first persons in flow units were on the inside, the passed first persons in flow units were on the outside. The passed first persons in flow units also complimented the passing first persons in flow units in another way. For the passed first persons in flow units that were within three open treads, their effective normalized descent times were closer to those first persons in flow units that experienced congestion.

In addition, the passed first persons in flow units were more likely to be female. It is not known from this study if the cause of more females being passed was the slower descent rate of females (as discussed in Section 5.4.1) or if there were social factors at play. However, in the regression model for the non free-flow first person in flow units, gender was only significant for the passed first persons in flow units. It was also found that the passed first persons in flow units that were engaging in lane flow had smaller effective normalized descent times than the comparable passed first persons in flow units that were engaged in uniform flow.

The passed first persons in flow units had greater increases in their effective normalized descent time than any of the other first persons in flow units. They were the slowest occupants. When they were experiencing more interactions with others, they tended to have a descent time greater than the other first persons in flow units, but closer to them. There was not the same indication of a lack of urgency as had been seen with the passing first persons in flow units. However they did have a statistically smaller effective stair travel distance than the other first persons in flow units. This could be indicative of an initial slow movement rate as attempting to enter the flow. Once fully established, those slower occupants were then able to keep pace with the rest of the flow units.

The passed first persons in flow units should be included in sophisticated computer models. From a conservative life safety point of view, the slowest individuals need to be accounted for.

5.5.1.3 Allowed Entering First Persons in Flow Units

There were fewer first persons in flow units that allowed other occupants to enter the flow than any other type of first persons in flow units. The characteristics of these first persons in flow units were not statistically different than any of the other first persons in flow units, with the exceptions being that they were more likely to not be carrying objects and they had a shorter effective stair travel distance. The shorter effective stair travel distance is likely due to most occupants entering the stair near the beginning of the drill, so only in the early stage of the drill do occupants have an opportunity to allow other occupants to enter.

The first persons in flow units who allowed other occupants to enter the flow required more effective normalized descent time than the other comparable first persons in flow units except for those that were passed. Because they allowed occupants to enter ahead of them, they are considered to have weaker social bonds with the other people ahead of them than some of the other first persons in flow units.

While the occupants allowing other occupants to enter the flow that were first persons in flow units are not different than the other first persons in flow units, it is not possible from the data to know who chose not to let other occupants to enter the flow. The difference between those individuals and the first persons in flow units that allowed other occupants to enter the flow would be a more meaningful comparison. Despite this limitation, it is still possible to take into account that allowing other occupants to enter the flow causes the people in the stair to take longer to descend.

5.5.1.4 Experienced Congestion First Persons in Flow Units

The first persons in flow units that experienced congestion were not statistically different than any of the other comparable first persons in flow units. This was expected because they were defined as first person in flow units based on being right behind the other types of first persons in flow units; random people were following

ones where something happened. It was for this reason that these first persons in flow units were selected as the reference level for the regression equation.

When all other variables are controlled for, these first persons in flow units require more effective normalized descent time than the flow unit ahead of them. This, in part, explains why they are first persons in flow units rather than followers of the previous flow unit.

5.5.1.5 Free-Flow First Persons in Flow Units

The free-flow first persons in flow units were the ones thought to be able to choose their own pace. For the data in Section 4.2, the free-flow first persons in flow units were disproportionately male (see Section 5.4.1), not carrying objects (probably related to being male as shown in Section 5.4.1.4), and in the outer lane (see Section 5.4.4). These findings contradict what was found in Building 6. This is possibly due, in part, to the different effective density conditions.

Of additional interest was the average pre-observation times and effective stair travel distances being greater than the other first persons in flow units. By default, the first person on most floors was in a free-flow flow unit and none have to be at the end. Predtechenskii and Milinskii (1978) describe the flow shape in corridors (and the logic would apply to stairs as well) as being cigar shaped: there are a few lone individuals at the start, then a solid mass of people, and finally a few lone individuals. Based on these averages, the front end of the "cigar" appears to contain fewer people than the back end. This is yet another indication that the flow is not as uniform as the algebraic equations assume that it is.

Controlling for the other variables found that females and those in the outer lane required more effective normalized descent time. This is consistent with the previous findings. Also, as was the case with the other first persons in flow units, there was a relationship between increasing pre-observation time and decreasing effective normalized descent time.

Even though these first persons in flow units were thought to be able to choose their own pace, they still had it related to the flow unit ahead of them. These occupants seeing similar conditions ahead as the previous flow unit and responding in a similar manner possibly cause this. For example, if there were very few people in the stairs, then both these first persons in flow units and the previous first person in a flow unit were able to go at a pace that was natural. If instead they saw congestion, they chose to stay further back and not crowd the people ahead. In either case they were selecting their own pace even though it was similar to the decisions made by previous first persons in flow units under similar conditions.

5.5.1.6 First Followers

As discussed in Section 5.3, followers simply went at the pace of the first person in their flow unit. The first followers were singled out because they were assumed to be

the ones that had an option not to follow. When compared with their corresponding first persons in flow units, the followers were more likely to be in the inner lane with the first persons in flow units in the outer lane. By choosing to stay with the first persons in the flow units (and occupying both lanes), the subsequent occupants were required to slow down.

The finding previously discussed related to the gender of the first follower in relationship to the first person in their flow unit; the same gender pairings were far more common than the mixed gender pairings. The characteristics of these followers were typically consistent with the previous findings, with the exceptions being that there were more large males than females behind male first persons in flow units and that the female followers of female first persons in flow units were more likely to be present during lane flow (and males more present during uniform flow). During lane flow, occupants could, in theory, switch lanes and join a different flow unit. Thus, it appears as if the female followers are more inclined to remain with female first persons in flow units than any of the other gender pairings.

The gender pairings were also different based on the following distances (see Section 5.4.1.2). As with the flow type, the difference seems to have been that the female-female pairings behaved differently than the other three. In this instance, the females were generally closer than were the other pairings.

5.5.1.7 Implications

Previous research has treated all occupants as contributing equally to the flow. This does not appear to be the case as there are some first persons in flow units that are setting the pace for the followers behind them. Thus, when taking average values for effective normalized descent time (or effective speed), the number of people that happen to be in a given flow unit will weight that particular first person in a flow unit's descent rate and cause the standard deviation to change.

A more accurate representation of the data for predictive purposes should only look at those individuals that are actually setting the pace. Even within this, further consideration should be given to the types of first persons in flow units. For example, taking the average of a passing first person in a flow unit and a passed first person in a flow unit would not be representative of the flow; it would underestimate the time required by the slower occupant. From a life safety perspective, this is not a conservative approach. By looking at the different first persons in flow units types, the algebraic equations could be determined based on the slower moving populations. For the more sophisticated computer models, incorporating the different first persons in flow units types would allow for the dynamics of the flow to more accurately match reality.

For the first followers, as mentioned in Section 5.4.1.5, the differences in spacings can be used to get effective density relationships that are more representative. The computer models can also use the information to create the nonrandom grouping of occupants that are seen in actual evacuations.

5.5.2 Flow Type

As shown in the example in Appendix E, lane flow typically sees faster occupants passing on the inside lane. Lane flow tends to occur during the slowest effective normalized descent times and it was one of the variables used to define flow units.

The exact cause of the shifts between lane flow and uniform flow are not known. In Building 6, very little lane flow took place. That could have been caused by the light effective density and thus being no opportunity for the dynamics to develop. In Building 4 there were no instances of lane flow. In that building, occupants were in queues at various locations, so it was not caused by a lack of effective density. One possible explanation is that the building had the smallest stair width and thus, even though some occupants were recorded as walking shoulder-to-shoulder, there was not sufficient width for the lane flow to develop. In Building 5 and Building 8 there were many instances of lane flow observed.

As an example of the effect that lane flow can have over the course of an evacuation time, 26 occupants that exited floor 14 in Stair N of Building 8 are shown with their exit lane designation on level 14, their exit lane designation on level 4, and the time required for them to descend that distance are shown in Table 5.2.

Table 5.2: Effects of Flow Type

Occupant	Floor 14 Lane	Floor 4 Lane	Descent Time (s)
350	Outer	Outer	301.17
352	Outer	Outer	301.70
321	Inner	Inner	276.41
354	Outer	Outer	301.47
324	Inner	Inner	278.11
362	Outer	Outer	308.21
325	Inner	Outer	277.64
365	Outer	Outer	307.44
326	Inner	Outer	277.81
367	Outer	Outer	308.17
329	Inner	Inner	274.85
368	Outer	Outer	302.87
369	Outer	Outer	303.00
330	Inner	Inner	274.51
370	Outer	Outer	302.07
331	Inner	Inner	274.58
373	Outer	Outer	301.50
332	Inner	Inner	273.51
374	Outer	Outer	301.34
335	Inner	Inner	273.30
371	Outer	Outer	300.97
341	Inner	Inner	273.34
375	Outer	Outer	300.90
376	Outer	Outer	300.91
380	Outer	Outer	308.81
342	Inner	Inner	270.27

All of the occupants that started in the outer lane required more than 300 s to descend these floors while those that started in the inner lane required less than 280 s. In this instance, the lane flow caused the descent times to increase by approximately 10%. Any occupant in the outer lane could have chosen to move to the inner lane to descend faster, but none did so until late in the evacuation (when some occupants in the outer lane went to the inner lane, but descended in uniform flow rather than lane flow). Because all of these occupants were together initially, they would be described as having the same densities using the methods of previous studies. Clearly, there are two distinct clusters in this case that are moving based on different dynamics. Using an average value does not accurately reflect what is happening because the population is not homogenous.

As has been mentioned previously, algebraic equations should be calculated based on the subpopulations that are requiring the most time to descend. In this instance, the values should be based on the occupants in the outer lane during lane flow. For the computer models, this dynamic could be included.

5.5.3 Previous Flow Unit

The final variable to be developed was the concept of the previous flow unit. As was mentioned in Section 5.5.1.5, even the free-flow first persons in flow units that were able to freely choose their descent time had their time related to the flow unit ahead of them. For the other first persons in flow units, the previous flow unit was included directly in the dependent variable of the regression model as the calculation was how much more (or less) effective normalized descent time the first persons in flow units required than the previous first person in a flow unit. In many ways, it is very similar to the relationship between first persons in flow units and followers (although far more complicated). Thus, one slow individual near the start of the evacuation can have long lasting effects on the rest of the evacuation. It was, in part, the inclusion of this variable that caused the R^2 value to increase from the models in Section 4.1 to those in Section 4.2.

5.6 Method Comparisons

Two different methods have been presented in this study. The first method is the traditional use of density as the only independent variable. For the second, the flow dynamics were taken into account. In both instances, the models developed in Section 4.2 were subsequently applied to a blind data set. With no connections between Building 7 and the other buildings, the data is as independent from the previous buildings as would be any other office building in the United States.

5.6.1 k-Values

All three k-value methods (using no k-value, the k-value method proposed by Pauls (1984), and the equivalent vertical descent value) all gave somewhat similar results with the equivalent descent being the most conservative, but also the least accurate.

For the most part, the occupants were descending at a faster rate than the different methods predicted. Because the methodologies were identical, the cause of this shift cannot be explained due to differences in methodologies. Two possible explanations for the shift are that the dynamics caused by differences in first persons in flow units (as identified in the previous sections) led to building effects or that the method of calculating density is not transferable to buildings with different stair dimensions.

5.6.2 Individuals Compared to Effective Density

The traditional method for predicting how long people require to descend stairs relies on only using density as the dependent variable. For the blind data set, the equation only had an R^2 of 0.34 (and that value was greater than for the data used to derive the equation). In this study, individual effects as well as flow dynamics were included. For the blind data set, using the regression model from Section 4.2, the R^2 value was 0.88, over 2.5 times better. Thus, using the models developed in Chapter 4 will result in much better accuracy in predicted effective normalized descent times.

5.7 Application of Results

In this research, the need for a better understanding of how people move on stairs was described based on the work of previous researchers. In many instances, the previous work was inconsistent or not thoroughly examined. To address these issues, this research was conducted using data from actual evacuation drills in high-rise office buildings. The different characteristics of the occupants were analyzed and models for predicting descent times were created using many of the variables identified in the literature as well as newly developed ones.

The question then becomes how the field can use this information. There are three general answers to this question. First, the computer egress models can incorporate the findings. Second, the algebraic equations can be adjusted to better represent the populations. Third, egress systems can be better designed based upon the results.

5.7.1 Computer Models

The main goal of the work was to gain insight into the important interactions and characteristics of individuals as they descended the stairs rather than to develop an algebraic equation that could be placed into a handbook. This was underlying many of the decisions that were made with regards to the selection of variables. In addition, dynamics were identified that could be used to better represent how occupants actually use stairs.

5.7.1.1 Definition of Variables

Many of the variables were centered around a given individual and their interactions with others rather than being based on global values. Thus, rather than a more global effective density, the occupants were classified as being in a given exit lane and having a following distance to the occupant ahead of them. It is also where the concept of flow type originated. In developing (or refining) a model with an individual perspective, these considerations can replace the global concept of density. As has been shown, just applying effective density gives a rather crude approximation of the individual movement that is occurring. The other variables led to a better match of the blind data to the predictions.

The other aspect of the analysis that lends itself to computer models is the iterative approach that seems to be required. The descent time of the first persons and the followers in flow units is tied to the flow units ahead of them. As the models with an individual perspective calculate how far an occupant travels, the values for the other occupants can be used based on the relationships demonstrated in Section 4.2. Also, fatigue could be added iteratively based on whether an occupant becomes part of a queue or not (see Section 5.7.1.3).

5.7.1.2 Flow Dynamics

For the models that assume that all occupants randomly enter the stair and then move as if they were a fluid, several of the flow dynamics could be implemented to more accurately reflect what is happening. Rather than being randomly located in the stairs, occupants form flow units descend at the pace of the first person in the flow unit. The occupants tend to form lanes and the flow rate in each lane can be different.

Consideration can also be given to the fact that the occupants do not enter and behave randomly. Flow units typically have a first person and first follower with the same gender. Along with these pairings, there appears to be a difference in the spacing between occupants based on their gender and the gender of the occupant ahead of them. For the models that include buffer zones between occupants, this information could be used to have the buffer zone adjusted conditionally; a female following another female would require less of a buffer zone.

For the flow models that are sensitive to the body size for determining density, the findings in this study did not indicate a difference in spacing based on body size. Thus, based on this research, the models should not adjust their equations based on body size.

5.7.1.3 Incorporation of Human Movement Principles

The findings from this dissertation are most suited for partial behavioral models with an individual perspective. The simulated occupants' individual characteristics as well as their interactions with the building and other simulated occupants can be used to determine their descent rate.

Rather than relying on density alone, this research focused on how the interpersonal spacing influenced descent rates implicitly by its inclusion in the definition of flow units. Based on their interactions with the other simulated occupants, simulated occupants can be classified as a first person or follower. This designation can be determined by their maximum travel rate, their interactions with other occupants, and psychological factors like their desire to evacuate the building.

Conditional, probabilistic, or artificial intelligence behaviors can be applied based on the attributes of the simulated occupants. In general, for models used in the United States, simulated occupants can have a preference to move to the right. In lighter density scenarios, they can be allowed to move to the inside. For simulated occupants engaging in passing behavior, they can be made more likely to be on the inside.

Furthermore, how simulated occupants interact with each other can be modified based on the gender of the surrounding simulated occupants. If the other occupant has the same gender, then the simulated occupant is more likely to become a follower. If not, then the simulated occupant would be more likely to still act independently. These pairings should also include smaller interpersonal spacings when the two simulated occupants are female.

Finally, there can be differences based on the location of the simulated occupants within the stair. The occupants in the outer lane would move at a slower rate than those in the inner lane. The lane flow type could be used when the occupants in the two lanes do not have a social connection that is causing them to stay together.

5.7.1.4 Methods for Application

Simulation models with an individual perspective need to account for the individual effects and interactions that were found to strongly influence the effective normalized descent time of occupants. The regression models developed in Chapter 4 can be used to set the descent rate of all occupants.

The proposed equations are the regression models from Section 4.2 with three changes to reflect the findings in Section 4.1. All of the changes lead to more conservative (larger effective normalized descent times). Specifically, effective travel distance is included with a coefficient of $3.2*10^{-4}$, the coefficient for pre-observation time is increased to $7.7*10^{-4}$, and the coefficient for gender in the free-flow condition is increased from 0.05 to 0.22. The results are shown in Figure 5.3.

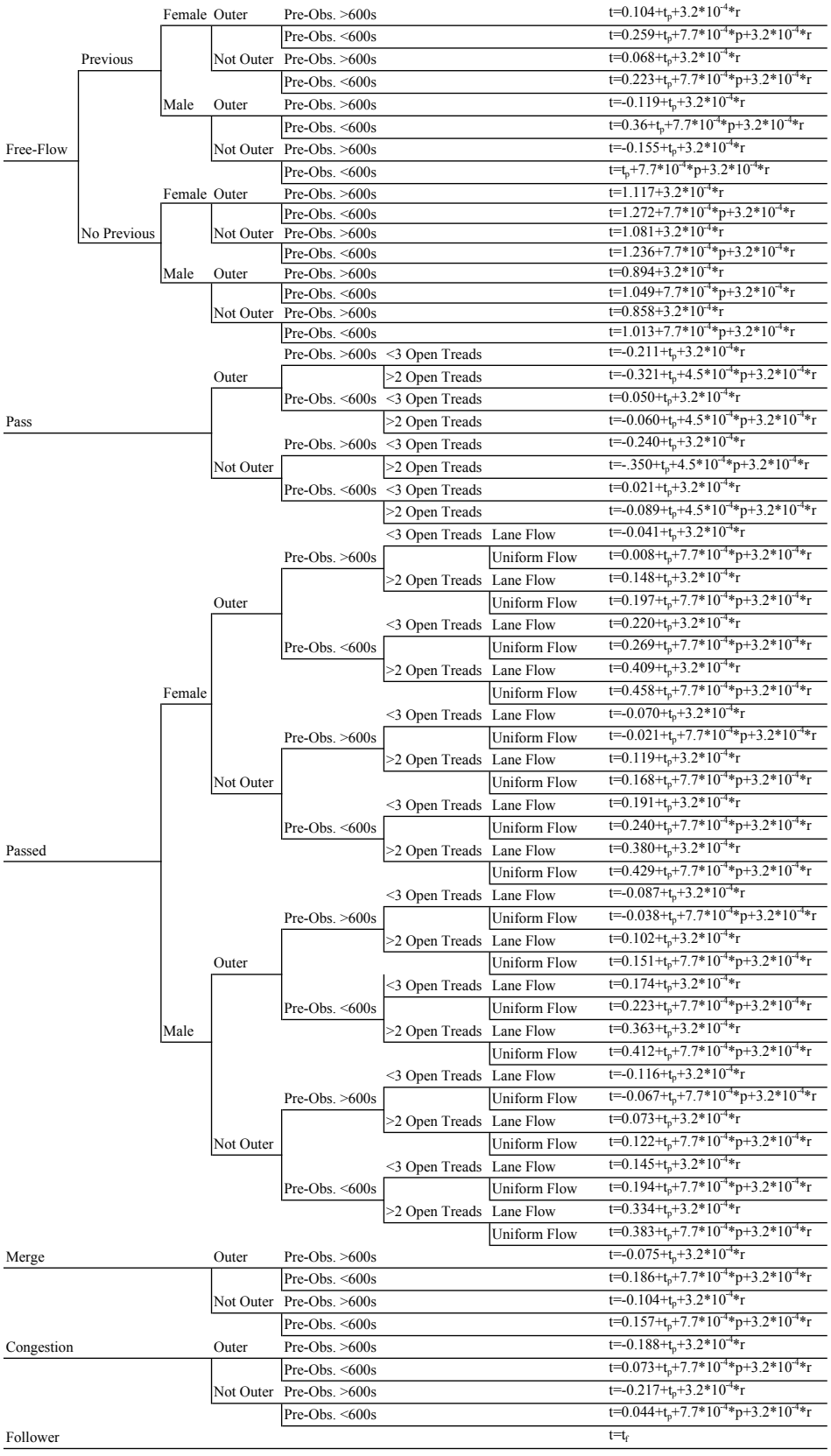

Figure 5.3: Decision Tree for Effective Normalized Descent Times

where:

t=effective normalized descent time (s/m)
t_p=effective normalized descent time of the first person in the previous flow unit (s/m)
p=pre-observation time (s)
r=effective travel distance in stairs (m)
t_f=effective normalized descent time of the first person in flow unit (s/m)

The equations in Figure 5.3, when applied to the blind data, result in an R^2 of 0.85. Model developers can use the equations to iteratively calculate the effective normalized descent rate of the simulated occupants.

5.7.2 Algebraic Equations

While not an initial goal of this research, several findings were made that directly relate to the future development of algebraic equations. These findings relate both to the variables that are used and the data that is used to develop them.

5.7.2.1 Effective Normalized Descent Time

In egress modeling, the goal is to determine ASET. The data that has been collected in the reference studies recorded the amount of time required to travel a known distance. Thus, the data that was collected was time and the final outcome is time. There does not appear to be any need to have an equation that calculates values based on the inverse of time (as all of the previous studies in Chapter 2 did).

None of the references in Chapter 2 looked at effective normalized descent time. When they used a comparable variable, it was always speed. As shown in Chapter 3, this will always lead to calculations that are more sensitive to the faster occupants than the slower ones. From a life safety perspective, this is not a conservative answer. Rather than focusing on speed, future equations could be developed that predict the effective normalized descent time (as is done in Section 5.7.2.2 and Section 5.7.2.3). Not only will these models be inherently more conservative but they will also be consistent with how the data was collected and applied.

5.7.2.2 Slower Populations

All of the calculations provided in Chapter 2 for predicting speed were calculated based on treating each individual as an equally valid data point and the equation then determined by minimizing the error from each data point and the predicted values. There are two problems with this approach. First, not all data points are equally valid. A follower is going at the same rate as the first person in the flow unit and including the followers is basically equivalent to applying a heavier weight to the first person in their flow unit. Second, the average value does not account for the dynamics that actually lead to some occupants going much slower than would be expected (for example, those occupants in the outer lane).

Equation 5.2 was developed to be similar to the previously developed ones and thus includes all of these flaws. This equation should not be used. For a single equation, it should be developed based on some of the slowest occupants. In Section 4.2, the categorical variables associated with slower normalized descent times were the first persons in flow units that were female, in the outer lane, and were passed. An equation developed relating effective normalized descent times to effective density for just the 410 first persons in flow with these characteristics in the data from Section 4.2 is:

$$t = 1.93 + 0.51 \cdot D \tag{5.3}$$

where:

t=effective normalized descent time (s/m)
D=effective density (persons/m^2)

Because Equation 5.3 is derived using only slower subpopulations, when applied to the entire population, the results are more conservative than assuming that the effective normalized descent time is the mean value for all occupants. For cases where the egress system designer wants to rely on a single equation, Equation 5.3 is more sensitive to slower moving populations than the SFPE Handbook (2008) equation.

Equation 5.3 should only be applied for cases where the effective density and the effective normalized descent time are calculated the in the same manner as was done in this study. Also, the tread depth and riser height should match those in this study, or the equation should be adjusted by an appropriate factor. Finally, the building heights should be within the range of 10 to 30 stories.

5.7.2.3 Range of Equations

Equation 5.3 should be applied when a single answer is desired. Due to the uncertainty surrounding the relationship between effective normalized descent time and density (even the best-fit regression lines had R^2 values less than 0.4), the egress system designer might desire to be able to bound the solution in order to know the shortest or longest probable egress times. Equation 5.3 does not provide any insight as to the minimum or maximum expected values. Two equations that bound over 96% of the first persons in flow units (with approximately two thirds of the data outside the bounds being from queues) developed using the data from Section 4.2 are:

$$t = 0.30 + 0.35 \cdot D \tag{5.4}$$

$$t = 1.93 + 1.67 \cdot D \tag{5.5}$$

where:

t=effective normalized descent time (s/m)
D=effective density (persons/m^2)

Due to the fact that queues are not well described by these equations, they should not be applied in situations where queues are expected. In Building 7, Stair 3 (despite some limited queuing), 97% of data points fell within this range as shown in Figure 5.4.

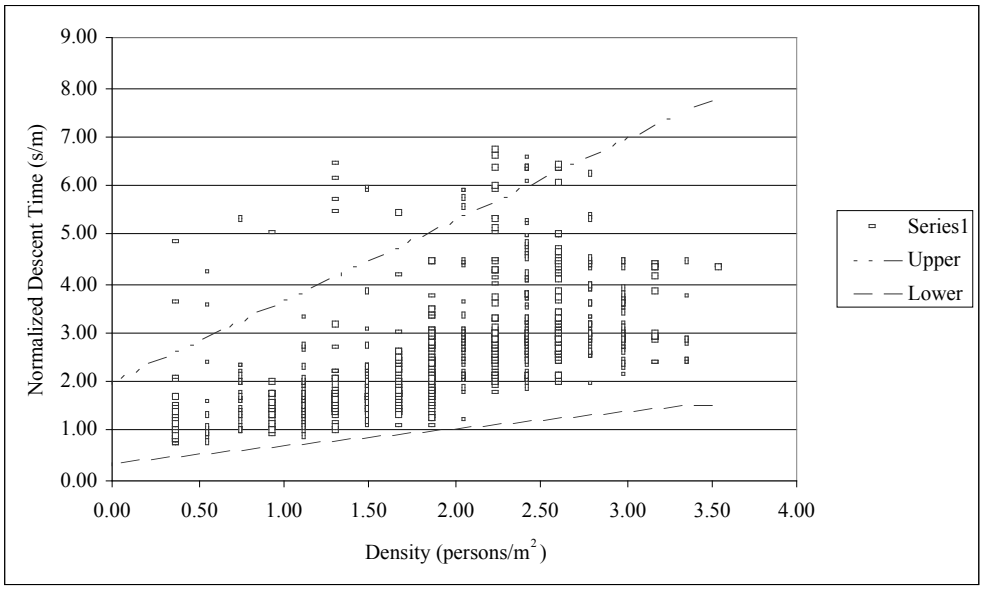

Figure 5.4: Building 7, Stair 3 Bounding Equations

5.7.3 Egress Systems

One of the main findings of this research indicates a direct improvement that can be made for egress systems. Followers moved at the same rate as the first person in their flow unit. The rate at which the first persons in flow units descended was also based on the previous flow unit. Thus, allowing the individuals that will require the most time to descend the option of using alternate means of egress, such as elevators, is expected to allow the occupants in the stairs to descend faster, as well as providing a means of egress for individuals that could not otherwise use the stairs.

Also, based on the large occupants that were first persons in flow units being less likely to be passed, it could be that wider stairs are needed for occupants to use them as efficiently as is expected. However how much additional width would be needed cannot be determined from these results.

Finally, occupants were found to stay to the right while descending in heavy density conditions and occupants in the outer lane required more effective normalized descent time. Based on these findings, the use of sinistral stairs would lead to faster effective normalized descent times.

5.8 Summary

The implications of the variables and dynamics identified previously were demonstrated to make a difference when the effects were observed on a larger population. Beyond this, the findings were refined in order to be applied in practice.

While it had previously been shown (see Chapter 3) that the inverse of the mean effective normalized decent time would always be less than the mean speed, this was explicitly shown by using the data from Section 4.2. In this instance, the value was 20% less.

Next, the different variables that determine the flow were examined. The emphasis was on understanding how the flow was characterized. Rather than being a uniform collection of individuals with a homogenous density, the number of open treads, lane, gender, flow unit, flow type, first persons in flow units types, and the effective normalized descent time of the previous flow unit were all important factors to consider. For the different variables, there were two types of observations made. The first type looked at how some sub populations were different than others. For example, the data from Section 4.1 showed a trend of first persons in flow units staying to the inside while the data from Section 4.2 showed a trend of first persons in flow units staying to the right. The second type looked at how different variables altered the effective normalized descent times. For example, one instance of lane flow conditions led to a 10% decrease in the effective normalized descent times of occupants that were initially together.

The final sections focused on how these findings could be applied to other data sets, as was done with the Building 7, Stair 3 data. Using the equations that accounted for the individual effects and interactions, the results were much more accurate than the methods that relied on density alone. Equations to use in computer models based on these methods were provided. Next, an algebraic equation was developed that took into account slower moving subpopulations. This equation is similar to the current SFPE Handbook equation, but is sensitive to the slower moving occupants that are setting the pace rather than treating all individuals as being completely equal; it is a more conservative approach. Then, a set of equations that bounded the data were also provided for egress system designers that want to be able to know what range of descent times will be seen in a different building. Finally, potential modifications to egress system design, based on the previous findings, were recommended.

All of the studies cited in Chapter 2 focused on homogenous conditions that caused everyone to behave in the same manner. In this work, that assumption was found to be flawed. The dynamics observed showed that individual characteristics and the effects of others were far more pronounced in determining the effective normalized descent rate.

Chapter 6: Conclusions

In this study, the first principles of movement down stairs during egress were examined in detail. This better understanding led to far more accurate predictions on blind data than the traditional density relationship. This chapter will focus on how all of the previous work can be applied.

6.1 Findings

The field can use the findings in this study in at least five different ways. First, measurement methods for collecting high-quality data were proposed. Second, human movement principles for descending stairs were developed. Third, modifications to the algebraic equations were implemented based on the movement principles. Fourth, equations for use in simulation models were provided. Fifth, changes to egress systems and associated codes can be made based on how stairs are used for evacuations.

6.1.1 Measurement Methods

In the current version of the SFPE Handbook, Gwynne and Rosenbaum (2008) state that the travel distance on the landing has to be included and only that the density should be measured in persons per unit area. Predtechenskii and Milinskii (1978) provided a travel distance on the landing, but it was not stated how it was developed. They also did not say how the area of the landing should be calculated.

This lack of details about how to take measurements of fundamental variables (travel distance and area are both used in all of the equations for movement speed in Chapter 2) can lead to faulty conclusions. For example, Kratchman (2007) and Blair (2010) used different area measurements than were used by Pauls (1980). In both cases, their area was larger and this led to them calculating lighter densities than Pauls (1980) would have done with the same observations. This led to the appearance that the older equation was an upper bound.

For some of the simulation models, the developers implement the equations that are provided in the literature. If someone measured the area in the same manner as Kratchman (2007), but used the equations developed by Pauls (1980), this misunderstanding of measurement methods would lead to over predictions.

Even when measurement methods have been provided, there are no known sources that attempted to have the equations match how people actually use stairs. On top of this, there are no generally agreed upon methods for calculating area on landings. Rather than applying multiple ad hoc methods, there should be a standard measurement method or, alternatively, known conversion factors between methods.

In this study, a new travel distance calculation (Equation 3.2) was presented that is representative of how stairs are actually used. Also, an equation for the area including landings (Equation 3.3) was similarly proposed. These equations can now be used to standardize measurements from one study to the next, unlike current practice. Even if other researchers want to use other measurement methods, they can supply conversion factors from their method to this one.

6.1.2 Human Movement Principles for Descending Stairs

The primary focus of this work was to develop the theory underlying people descending stairs. The studies in Chapter 2 primarily focused on density and all occupants were assumed to be moving in a homogeneous manner.

This type of behavior is not what is observed in actual evacuations. For example, Shields, et al. (1997) found that there was sufficient room for occupants to pass a slower individual, but they chose not to. When Peacock, Averill, and Kuligowski (2009) used a regression model for their data, the model (which also included other variables) only explained 13% of the error. They called upon the field to develop the theory that would explain much of the unaccounted for error.

In addition to standardizing the measurement methods to reduce errors between different estimates, the different dynamics occurring within the flow were identified. Accounting for these dynamics explained 85% of the error in this study.

The most basic finding was that there were flow units that moved at the pace of the first person in them. The spacing to other occupants (more than two open treads) and actions (passing, being passed, allowing other occupants to enter, experiencing congestion, or being in free-flow conditions) defined the flow units. The actions of this first person helped determine how fast the entire flow unit could descend. In addition to their behaviors, the first persons in flow units had their effective normalized descent time influenced by the previous flow unit, their gender, and their location within the stair (exit lane).

Aside from the first persons in flow units setting the pace, the flow was not homogenous in terms of how it operated. There were two different types of flows (lane and uniform). Furthermore, same gender pairings of the first two people in flow units were more common than mixed pairings. Also, in most buildings, occupants tended to stay to the right.

With a better understanding of how people actually use stairs, future studies can exclude observations that are not meaningful. For example, the studies in Chapter 2 provided conflicting results as to whether gender was significant or not in predicting speed. By separating out followers and first persons in flow units that were directly interacting with other flow units, there was a consistent difference.

Understanding the human movement principles can also allow for experiments to be conducted that focus on how occupants are actually using the stairs. For example,

when studying merging behavior, understanding lane flow can allow the merging effects to only be accounted for in the outer lane (if the occupants in the inner lane continue moving as they were before).

In addition to helping the research community, the principles can be used in model development. Direct methods of doing this will be discussed in Section 6.1.3 and Section 6.1.4.

6.1.3 Algebraic Equations

The equations in Chapter 2 for predicting movement speed calculated speed based on only density. The density was a homogenous measure and average values (for both the speed and density) were normally used. When it was provided, the travel distance on the landing was calculated by the method of Predtechenskii and Milinskii (1978).

As shown in Equation 3.5, an equation based on speed will always be more sensitive to faster moving people than slower moving ones. In both the data used in Section 4.1 and Section 4.2 (and would be the case with any other data set), the inverse of the mean normalized time will always be less than the mean speed. From a life safety perspective, this is not conservative.

Assuming a homogenous density is also not conservative. Based on the human movement principles, there are known subpopulations that will descend slower than others. Depending on the fraction of the different subpopulations used to develop the equations, the accuracy of the predictions could vary significantly. If the goal is to design a system for every day use, not accounting for slower moving populations will not have as big of an impact as a system that does not allow some people to safely evacuate before the building collapses or the stairs become untenable.

Another shortcoming of many of the equations is that they provide only a single answer. This leads to safety factors being applied because the system designer cannot tell the authority having jurisdiction what are the expected ranges of actual performance. If the safety factor is too small, then the system could easily fail in the event of an actual emergency. If the safety factor is too big, then the building owner is not able to use their building as they could safely do. Even with a deterministic approach it is possible to provide guidance on the expected variability. For a performance based design approach, bounding equations would allow for the egress system designer to quantify why they are choosing the safety factor that they are using.

The research in this study addresses all of these issues. All of the equations are calculated based on effective normalized descent time (with the measurement method provided so that they can be applied consistent with how they were developed). For the case where the egress system designer wants only a single value, Equation 5.3 addresses the concern of the homogeneous values; it was developed using only the slowest subpopulation. This provides an equation that does not suffer from the effects of the homogenous population assumption and instead incorporates, indirectly,

the human movement principles. Finally, to be able to design a system with appropriate safety factor (although extremely long queues are not accounted for), Equation 5.4 and Equation 5.5 can be used as an upper and lower bound.

These equations can be used in practice (or a model) where the designer would currently use an equation like those presented in Chapter 2 for predicting speed. The methods can also be used by the research community to develop equations if the researchers choose to use a different measurement method.

6.1.4 Simulation Models

The simulation models that are based on the hydraulic analogy use algebraic equations similar to the ones in Chapter 2 for calculating speed based on density. For models with an individual perspective, the methods are more complicated.

For the hydraulic models, the same shortcomings that exist for the algebraic equations are present and can be solved in the same manner. For more sophisticated hydraulic models, distributions can be used (no distributions are provided in the studies presented in Chapter 2). Equation 5.4 can be used as a lower bound. No simulation should see faster descents than presented in that equation. While the model developer could choose to use Equation 5.5 as an upper bound, having slower descent times would be more conservative.

For the simulation models with an individual perspective, the human movement principles can be incorporated. For example, in Building 8, it was found that over 70% of the first persons in flow units experiencing free-flow conditions stayed to the right. Especially in dextral stairs, model developers could have designated exit lanes (which would also be used for lane flow) and have the probability of someone in free-flow conditions staying to the right be at that level. There could also be factors based on the nonrandom entry in the stairs. For the models that have occupants being attracted to one another, the same gender attractions should be 1.25 times stronger than the opposite gender attractions based on the findings of the first person in the flow unit and the first follower. The attraction forces can also be limited to only simulated occupants that are within two or fewer open treads to the simulated occupant ahead of them. The paths on the landings can also be shown (and calculated) as an arc to match how people actually use the stairs.

Aside from qualitatively matching the look of the flow, the descent rates can be made to better match the quantitative observations. Figure 5.3 can be used rather than the current equations that are based on only density or untested theory.

6.1.5 Egress System and Code Changes

The codes and egress system design usually revolve around the physical attributes of the stair. Because the focus of this research was on developing the human movement principles, there was relatively little attention paid to some of the physical attributes.

With that being said, there were two findings that can be directly applied to match how occupants use stairs in practice.

High-rise buildings today typically rely on only stairs for evacuating nearly all occupants. Based on the current calculation methods, this is a reasonable practice. While having stairs available for all occupants to use, the findings in this study strongly indicate that alternative means of egress should be considered.

A slow moving person causes their entire flow unit to move slowly. This causes the next flow unit to move slower and the trend continues further back. Proulx, et al. (2007) and Shields, et al. (1997) both noted occupants staying behind slower individuals in evacuations that they observed. In the buildings discussed in Section 4.2, the flow out the exit doors was not coming to a stop. Nor was the flow coming to a stop just to let more people enter the stair. By allowing the slower moving occupants to have a different means of egress, the findings in this study indicate that all subsequent occupants will be able to descend faster.

Furthermore, in Building 6, fatigue was present as occupants descended (even before they had descended the height of the smallest building in the study). Especially if the slower moving occupants are removed (reducing queues in the other buildings) fatigue would be expected.

Based on the findings in this study, having slower moving occupant use elevators for egress should lead to faster descent times for them as well as faster descent times (even faster than those brought about by the reduced density) for the occupants that are still using the stairs.

A second proposed code change relates to the direction that the stair turns. While it could be a United States cultural issue, there was a noted tendency of people to stay to the right during the evacuation. In a dextral stair, this causes occupants to shift to the outside and travel further as they evacuate. A new code requirement to address this should be that, for stairs that are being used for emergency evacuation only, only sinistral stairs should be used. In this way, the egress system could be made to better fit how people actually use it.

6.1.6 Summary of Findings

The main goal of this study was to identify the flow dynamics that could explain much of the error that Peacock, Averill, and Kuligowski (2009) found with a regression model using the theory that existed about human movement on stairs. Based on an in depth analysis of several proposed variables and the development of others, much of that error has been explained and the results were duplicated on a blind data set.

The work and methods used can benefit the field in many ways. By developing equations based on how stairs are actually used, measurements can now be made more accurately (and consistently) between different researchers. Future researchers

can use the principles to properly design experiments and analyze their data. The proposed algebraic equations do not suffer from the less conservative methods used to develop the current ones. Simulation models can use the human movement principles to both qualitatively and quantitatively match what is seen in evacuations. Finally, egress systems can be designed to better serve how occupants will actually use them.

6.2 Future Research

While many advances were made during this study, it is only one step towards a better understanding of how people actually behave during evacuations. There are many opportunities to examine the variables more closely or to determine the broader applicability of the findings.

6.2.1 Travel Distance and Area

The equations that were developed to calculate the travel distance and area are qualitatively accurate. Because no one else has used these equations previously, it could be that additional effective factors need to be applied for them to match the way that they are actually used.

6.2.2 Open Treads

The number of open treads was used to determine the occupants that were first persons in flow units and as a measure of the spacing between occupants. This is a dynamic variable that was given a static value. Because it was developed in the process of this study, there is a very limited understanding about how sensitive it is. Future research could examine more closely how the spacing interacts with other variables. For example, there could be minimum spacings needed for allowing other occupants to enter the flow.

6.2.3 Gender

While there were several sections that examined the role of gender, these initial findings can be investigated further. While the variable is based on secondary sex characteristics, it could be that the difference in effective normalized descent times was caused by clothing or some other factor.

6.2.4 Carrying

Carrying objects was treated as a binary variable in this study. Future research could examine the effects caused by he types of items carried, how they are being carried, and how this carrying interacts with other variables (e.g., is the item on the same side as the handrail).

6.2.5 Flow Type

Because flow types were first documented as part of this research, there are many unanswered questions about them. Some unknown effect(s) causes the flow to oscillate between lane flow and uniform flow (and prevented lane flow from occurring in Building 4). Understanding this will lead to a better understanding of who is actually leading the flow units. Finally, this study assumed that the effect was the same for sinistral and dextral stairs and that there was no difference between the passing occurring by the occupants in the inner or outer lane. Both of these assumptions need to be examined more closely.

6.2.6 Exit Lane

In Section 4.1, occupants were observed to move to the inside of the stair for both sinistral and dextral stairs. In Section 4.2, the occupants shifted to the outside in the dextral stairs. What causes this shift, and under what conditions it occurs, needs to be studied in order to accurately represent both the travel distance and area.

6.2.7 Fatigue

Fatigue was calculated indirectly by looking at effective stair travel distance and its impact. In Section 4.1, fatigue was significant. However that was not the case in Section 4.2. There could be a minimum travel distance before which fatigue is not present and/or there could be an effect based on density (assuming that most occupants in the high effective density case were not able to reach their normal descent rate and thus did not start to experience fatigue).

6.2.8 Pre-Observation Time

Pre-observation time led to different conclusions in Section 4.1 and Section 4.2. When and how pre-observation time interacts with descent times needs to be better understood.

6.2.9 Queues

In the data from Section 4.2, queuing was observed. These queues led to some occupants having much different times than were expected. Future research could focus on when and how queues form. Based on the flow always being continuous at the exit, it appears that the queue formed as occupants slowed to keep a space between themselves and those ahead of them, but this was not possible to obtain from the spreadsheets because the queues were not initiated within the camera view.

6.2.10 First Persons in Flow Units Definitions

The different types of first persons in flow units were defined for the first time in this research. Future research could refine the methods used to classify first persons in flow units. In this study, the definitions were based on behavior and spacing. There

could be more types of first persons in flow units than were identified here or there could be better methods for identifying which occupants are first persons in flow units. Because of how important the flow units were determined to be, a better definition of first persons in flow units would allow the predictions to be more accurate.

6.2.11 Merging

The only consideration allotted to merging behavior was to identify certain first persons in flow units that allowed other occupants to enter the flow. Future research could consider both those occupants that allow merging and those that do not, including if there is a minimum number of open treads required and if it affects one lane more than another. This can be combined with research on the ratio of flows from the stairs to provide a better understanding of how the merging alters the flow in the stairs.

6.2.12 Counterflow

Due to the way that the previous flow unit variable was defined, the effect of counterflow was masked. It could be that there is an actual decrease in descent rate when counterflow is present. There have been relatively few studies have looked at this variable before, so the influence of it is unknown. Future research should look at how the effects of counterflow alter the flow. For example, it causes a lane shift if the occupants are using the entire width of the stairs. It is possible that the flow immediately fills the entire stair or that the occupants stay to one side. Also, there could be a difference in which side experiences counterflow if the stay to the right pattern persists on both sinistral and dextral stairs.

6.2.13 Handrails

The effects of handrails were not included in this study because the outside rail could not be seen in many of the videos. Future research could investigate the relationship between handrail use and effective normalized descent time. Also, there could be interactions between first persons in flow units (or other variables) and handrails.

6.2.14 Age and Fitness

The buildings observed were office buildings, so there were not expected to be many occupants that were either very young or very old. However there could have been differences based on either age or fitness that were not accounted for. This is an area that needs to be investigated further. Some of these populations could descend at slower rates, so they should be included when developing models or equations that are to be applied to a wider range of buildings.

6.2.15 k-Values

The prediction model for the heavy effective density case and the blind data set used to test the validity of the model had a different stair dimension. While three different methods for calculating k-values were tested, more testing needs to be done to determine which method(s) are most appropriate for a wider variety of stair sizes. The results in this instance were inconclusive as to what the appropriate method should be.

6.2.16 Stair Width

Based on the finding that first persons in flow units with large body size were not being passed as often as expected, future research should examine what stair width is wide enough to accommodate occupants as the stairs are used in practice. This should be combined with studies on counterflow to account for a similar time when the system is placed under maximum demand.

6.2.17 Other Egress Components

While the current study looked at movement down stairs, egress paths can include other components like corridors or upward movement on stairs. The interaction dynamics are expected to be seen in these other components as well, but research is needed to verify this assumption.

6.2.18 Other Occupancies

The study was intentionally restricted to office buildings in the United States. Most of the studies in Chapter 2 were conducted using adult populations similar to office workers (either in office building evacuations or commuters during the peak period). While this makes the findings comparable to those studies, it does not provide definitive insight into other occupancies. Thus, data should be collected from different occupancies to determine if the flow dynamics are the same.

6.2.19 Removal of Slow Occupants

Based on the findings with first persons in flow units, the removal of slower occupants to other egress components (like elevators) should cause the average effective normalized descent time in the stairs to increase. If true, this could be used to improve egress systems in buildings.

6.2.20 Use of Other Analysis Methods

The analysis methods in this dissertation focused on the interactions and individual characteristics of occupants. Additional analysis techniques from other fields (i.e., car-following from transportation engineering) could provide additional insight into methods for calculating descent rates on stairs.

Car-following theory describe the interactions between adjacent cars in a single lane of traffic (Brackstone and McDonald, 1999). In this theory, subsequent cars accelerate to match the changes in speed of the previous cars or attempt to keep a safe spacing. There is some delay in the rate at which the second driver can respond. If this is also seen in movement on stairs, it will lead to slight differences between the different followers over short distances. For studies examining distances less than several floors, this phenomenon could be present.

6.3 Summary

The traditional methods for predicting movement on stairs relied on density in order to predict speed. This method resulted in relatively low R^2 values as well as it being sensitive to faster moving occupants. The previous research in this area had not clearly demonstrated what other variables were needed in order to better understand why people descended at the rate that they do. The intent of this research was to identify the individual characteristics and interactions that influence people while descending stairs.

To address the sensitivity for the faster moving occupants, the inverse of speed (effective normalized descent time) was used. For the heavy density case, this resulted in a 20% greater mean descent time. From a life safety perspective, this is the conservative approach.

While using density as the only independent variable can be applied for simple algebraic equations, the results in this study indicated that it was slower moving occupants that allow more occupants to collect behind them rather than the other way around. Instead of density, the spacing between occupants was used to define relationships between occupants.

The variables that were consistently found to be important were the ones related to the first persons in the flow units; the followers basically descended at the same rate as the person that they were following. The type of flow (lane or uniform) as well as actions taken by the first person (passing, being passed, allowing entering, experiencing congestion, or being in free-flow conditions) were all found to be important. In addition to these effects, some characteristics of the first persons that were significant were gender of the occupant and the lane that the occupant was in. Furthermore, the interactions with both the building and other occupants were significant.

When the methods were applied to a blind data set, the predictive capabilities of the numerical models were nearly as accurate as the results from the data from which the models were developed. Thus, the findings appear to be applicable to similar buildings.

For sophisticated computer models that have an individual perspective, using the equations in this study that account for the individual characteristics, interactions, and

flow dynamics should lead to more accurate predictions than relying on density alone. For the algebraic equations, new equations based on both slower subpopulations and the range of data were developed.

The findings in this dissertation are an important step in understanding egress behavior on stairs. By properly accounting for those individuals that are setting the pace of the evacuation, egress systems can be designed in accordance with how they are actually used.

Appendix A: Details of Previous Studies

Several authors have previously conducted studies that looked at movement speeds and human behavior while descending stairs. However these authors tended to pay very little attention to the individual characteristics that determine movement speeds of individuals within a larger group. The previous studies have instead looked at some general issues rather than the individual characteristics; average values for all observations or individuals in isolation tended to be the focus of the studies. A few general types of experiments have been conducted. The first type used observations from fire drills. The second type made observations during normal use. Accounts from people in actual fires is the third type. The fourth type of reported values saw authors combined data from the previous categories to develop their own movement speed calculations. In order to isolate certain key variables, a fifth type of study has studied movement speeds under laboratory conditions. Finally, a group of studies that have used subsets of the data used in this research are included.

For each of the studies presented, as much data as was possible from the authors' descriptions was given with respect to the physical conditions and interactions of the building and stairs as well as the occupants. Unless otherwise noted, all comments that give explanations for effects are from the authors of the studies.

A.1 Fire Drill Studies

When an emergency evacuation is required, the egress system needs to be able to accommodate the people in the building at that time. No known systematic observations of movement speeds have been made under actual fire conditions. For ethical reasons, intentional fire experiments are not possible. Thus, for systematic analysis that can be preplanned, drill data has to be used.

It is unknown how accurate drill data for movement speeds is compared to speeds in actual emergencies. The only indication comes from indirect sources. In real fires, interviews with victims after the fact indicate that people, once remote from the fire, tend to behave normally and in an altruistic manner (i.e., Keating, 1982). Also, the initial reactions of people not receiving fire cues can have significant delays in starting the egress process (i.e., Chertkoff and Kushigian, 1999; Kuligowski and Hoskins, 2011). These are actions that are typically associated with fire drills.

Studies have been identified where the authors observed actual fire drills and were able to observe the evacuation speeds. These measurements were made in some instances by having observers move with the occupants and in other instances by using videotape evidence.

A.1.1 Pauls- BC Hydro Building

Pauls (1971) observed the evacuation of the BC Hydro Building on June 26, 1969. The drill was pre-announced and 910 occupants used two 1.19 m stairs with 17.8 cm riser heights and 25.4 cm tread depths. An additional 35 occupants that could not walk down the stairs were able to use elevators for egress. Occupants were originally located on floors 1 to 21 over a total of 17,500 m^2 of floor space. Occupants on a given floor reported to the exit and waited there until being instructed to enter the stair; the protocol was for the lower floors to be evacuated first. Occupants tended to evacuate in groups with the spacing being two abreast or in a staggered file. People moving within the main flow made observations. For a few selected instances, the author was able to estimate the average descent speed and these values ranged from 0.61 to 0.81 m/s. No information was provided about the basis for these calculations. The average discharge rate was 0.7 persons/s with a peak flow of 1.2 persons/s.

For calculating the density (for the flow calculation) an adjusted horizontal area was used to account for people not using the corners of the landings; the entire width of the stairs was used. Aside from the two flow values, the author did not give any indication of the density. Travel distance was measured long the slope of the stair, but the path on the landings was not defined.

A.1.2 Pauls and Jones

Pauls and Jones (1980) studied two different office buildings. The comparison between the two unannounced evacuations focused on total evacuation versus phased evacuation. Both buildings were medium-sized, high-rise, government office buildings located in Ottawa, Canada. Conversely, the plan configuration was markedly different and the building used for total evacuation had nearly four times the effective stair width.

The building used for the total evacuation had 32,500 m^2 of office space over 14 floors. There were five 1.14 m-wide dogleg stairs. The riser height and tread depth were not provided. The drill was conducted on a cool October 1972 day with 1,453 able-bodied people using four of the five stairs and 73 people that were disabled or assisting the disabled occupants using the center stair. Seventeen observers collected data with five at ground level and one moving person every five stories for each of the four stairs used by able-bodied occupants. The observers had tape recorders to provide data on human behavior, densities, and movement speeds.

In this study, occupants already in the stairs deferred to people entering from lower floors. Above the seventh floor, the movement speeds, measured along the slope of the stairs, varied due to the stairs being used at a significantly greater density. The slowest recorded speed was 0.23 m/s. Below the seventh floor, the average speed was 0.44 m/s. On the last floor, the mean speed was 0.66 m/s with an average density of 1.38 persons/m^2.

The building used for the phased evacuation had 30,800 m^2 of office space over 20 floors. There were only two dogleg exit stairs that were 1.04 m wide. The drill was conducted in May 1971. The phased evacuation was designed to evacuate the fire floor first, the two adjacent floors second, and then the other floors starting from the top of the building. Observers moved with other occupants on floors 3, 4, 12, 14, and 21 and others were positioned on the ground and second floors in fixed positions. The observers followed the same procedures as the total evacuation drill.

During the drill, unclear instructions over the public address system caused several floors to evacuate out of sequence. While the authors did not provide movement speeds, the observers during steady-state conditions descended at approximately the same rate as those in the total evacuation study under steady-state conditions.

A.1.3 Pauls- Multiple Buildings

From the late 1960s to the 1970s, Pauls (1980) conducted 58 total evacuations from high-rise office buildings. The stairs had widths that ranged from 0.91 to 1.52 m. The variation of riser heights and tread dimensions were not provided, but mention was made of the maximum tread depth, 27.9 cm, and at least one stair with a tread depth of 22.9 cm. Also, the exact heights of buildings were not given, but buildings 18 to 20 stories were described as being very tall. Typically, people stayed near the sides of the stairs in a staggered file, but left a space between themselves and the wall.

Based on these observations, the author developed a formula to calculated the expected flow on a stair:

$$F = 0.206 \cdot (b - 0.3) \cdot \left(\frac{P}{b - 0.3} \right)^{0.27} \qquad \text{(A.1)}$$

where:

F= flow (persons/s)
P= population (persons)
b= width of stairs (m)

In Equation A.1, the -0.3 term is to account for the space (a boundary layer) that people left between themselves and the wall.

Pauls noted that individual characteristics could alter the total time required for evacuation. He identified 20 of the 58 cases as being ones where individuals required coats due to cold or wet weather. In these evacuations, the flows dropped by 6%. Also, individuals tended to more frequently use stairs for evacuations that they used under normal conditions and those buildings with more training tended to have higher flows. He also found that disabled occupants slowed the flow in their general vicinity, but had no noticeable effect on the overall flow.

In order to calculate total evacuation times, he proposed using:

$$t = 2.00 + 0.117 \cdot p \quad \text{(A.2)}$$

$$t = 0.70 + 0.133 \cdot p \quad \text{(A.3)}$$

where:

t= time (minutes)
p= evacuation population per meter of effective width

Equation A.2 was to be used when p < 800 persons/meter of effective width and Equation A.3 was to be used when p > 800 persons/meter of effective width. Pauls also found that movement speed was dependent on density:

$$s = 1.08 - 0.29 \cdot D \quad \text{(A.4)}$$

where:

s= speed (m/s)
D= density (persons/m^2)

The speed was the speed along the slope of the stair. To calculate the horizontal component, the author said to multiply the speed by 0.9. There was also no indication as to how the travel distances on the landings were calculated.

Furthermore, the author concluded that the optimum evacuation conditions occurred when the density was 2.0 p/m^2 and the speed was 0.5 m/s. However he did not explain how density was to be calculated. A figure in the chapter showed an overhead camera shot of occupants only on treads. If that figure is representative of the data that he collected, then the density was for the treads only, but it is not stated whether this was the case or not.

While not stated, Equation 4 makes several assumptions as to the nature of speed on stairs. One is that the relationship between speed and density is a linear relationship. The equation also implies that an individual in isolation will travel at 1.08 m/s and that, at a density of 3.7 people/m^2, all movement will stop.

For calculating the flow, Pauls suggested using:

$$f = 1.26 \cdot D - 0.33 \cdot D^2 \quad \text{(A.5)}$$

where:

f= specific flow (persons/m-s)
D= density (persons/m^2)

If the theory relating specific flow, speed, and density was completely accurate without any other effects, then Equation A.5 would be Equation A.4 multiplied by the density. Thus, at least for the data collected by Pauls, there appears to possibly be some nonlinear interaction between flow, speed, and density.

A.1.4 Khisty

Khisty (1985) observed 21 unannounced fire drills and normal use in dormitories 3 to 12 stories in height on the Washington State University, Pullman campus during 1983 and 1984. Drills were conducted at all hours of the day with the latest one at 11 p.m. Exit interviews with a random sample of at least 10% of the occupants after each drill found that 80% of occupants thought that the drills were real incidents. Thus, for those individuals, their behavior under drill conditions would be the same as under a real emergency with remote cues.

In this study, scissor stairs were most common, occurring in 19 of the 21 buildings. The risers varied from 16.5 to 19.0 cm with tread heights from 27.9 to 30.5 cm. The width of the stairs varied from 1.22 to 2.13 m. As expected for a dormitory, about 99% of the occupants were between 18 to 30 years old. Time-lapse photography at 18 frames per second was used to record the drills. Observers also moved within the flow to collect data.

Movement speed was calculated based on the number of frames between two marked locations a known distance apart. The author did not indicate if the speed was calculated for the slope or horizontal component. The density was calculated based on the number of individuals within the area between the two marked locations, but the author did not indicate if that was an effective area or if it was of just the treads, landings, or a combination of the two. The flows were calculated by multiplying the density by the speed.

During the emergency evacuation, the mode and median of density were 1.96 and 1.40 persons/m^2 respectively. Comparatively, under normal conditions, the mode and median of density were 1.66 and 1.38 persons/m^2 respectively. The highest recorded speeds were 0.635 and 0.696 m/s for normal and emergency conditions respectively. Flows were also seen to increase under emergency conditions. The maximum specific flow increased from 0.898 to 0.998 persons/m-s.

Equations were provided for movement speeds down stairs for both normal and emergency conditions.

$$s = 0.864 - 0.187 \cdot D \qquad \text{(A.6)}$$

$$s = 0.798 - 0.177 \cdot D \qquad \text{(A.7)}$$

where:

s= speed (m/s)
D= density (persons/m^2)

Equation A.6 is for normal conditions and Equation A.7 is for emergency conditions.

Several variables did not seem to decrease the speeds or flows. These included the stair width and localized constrictions; a description of the constrictions was not provided. Also, fatigue was not observed, but how this was determined was not stated.

A.1.5 Kagawa, Kose, and Morishita

Kagawa, Kose, and Morishita (1985) recorded a fire drill in a 53 story high-rise office building in Tokyo, Japan on September 4, 1984 at 14:30. Approximately 1500 individuals, 20% of the building population, participated in the drill and used the two 1.20 m-wide emergency stairs. The occupants had been notified in advance about the drill.

Four pairs of video cameras were used to monitor the flow through selected doors on the east stair. An unspecified number of additional cameras were used to monitor the general flow. Research staff with cameras also moved with the last person on selected floors.

The first individuals exited the building 42 seconds after the initial alarm. Most of the occupants were outside of the building within 16 minutes. The flow was not uniform but consisted of groups moving as platoons and occupants were either in a staggered file or should-to-shoulder with an open tread to the preceding person. Generally speaking, the observers had an initial delay after first entering the stairs and then descended approximately one story every 16 seconds. Each story was approximately 3.65 m high. While not provided in the article, based on these numbers, the approximate vertical travel speed was 0.23 m/s. No values were given for the horizontal or slope components.

Stagnation of the flow was reported in several locations with people on some of the lower floors commenting in questionnaires that the people from above would not let them enter the flow; but people in the stairs from other floors commented that the people from the lower floors disrupted the flow. Even at the stagnation points, the density did not exceed 3 persons/m^2. The authors anticipated a higher density, but attributed the decrease to the fact that it was a drill. It was not indicated if this density included landings and, if so, what area was used for the landings.

A.1.6 Proulx

Proulx (1995) videotaped fire drills in four similar apartment buildings in four different Canadian cities. All of the buildings were 6 to 7 stories high and were 6 to 11 years old at the time of the fire drill.

The drills were conducted between 18:45 to 19:30 on weekday evenings in the late summer and early fall of 1993. For all four drills, the weather was sunny and warm. The occupants were given a memo a week in advance notifying them that a drill would be conducted, but the exact day and time of the drill were not indicated.

The pre-evacuation times in the buildings averaged 2.5 minutes, 8.4 minutes, 9.7 minutes, and 3.1 minutes. The difference between pre-evacuation times appeared to be related to the ability of occupants to hear the alarm according to the author. There were no statistically significant differences in pre-evacuation times based on gender or age.

Once occupants started to evacuate, the average travel time in all four buildings was between 1.1 minutes and 1.3 minutes. The difference between buildings was not statistically significant. The average speed on the stairs, when it could be measured, ranged from 0.52 m/s to 0.62 m/s. The author did not state if the speeds were along the slope or the horizontal component nor was there any indication for how the travel distance on the landings was calculated. The speeds did include the time when individuals stopped for a rest or to look into hallways. The average time to descend one floor varied from 9.6 to 20.6 s.

Children between the ages of 2 to 5 years old and the elderly had average speeds of 0.45 and 0.43 m/s respectively. This was slower than the rest of the population, but the elderly occupants tended to leave earlier, thus making their total evacuation times similar to younger adults. People carrying children tended to move at the same average speed as the rest of the population, but they were also more cautious in their movements.

During the evacuations, occupants tended to use stairs that they used on a regular basis even if other stairs were closer to their apartment. The stairs were never crowded during the drill (the density was not reported), but many occupants traveled in groups.

A.1.7 Proulx, Latour, Maclaurin, Pineau, Hoffman, and Laroche

Proulx, et al. (1995) recorded evacuations from three high-rise buildings in Canada in 1994. The first two drills (one building in Montreal and the other in Calgary) occurred on weekdays between 18:30 and 19:00 in the summer and fall during sunny and warm conditions. The third building was in Gloucester drill was conducted on a Saturday morning in December between 10:30 and 11:00. The weather for that day was below freezing and snowing.

For all of the drills, cameras were placed in corridors as well as in both stairwells (each building had exactly two). No dimensions were given for the stairs nor were the methods used to calculate travel distance. Speed calculations were based on the total travel distance in the stair and the time required to travel that distance.

Occupants tended to travel in groups and use the nearest stairwell. The groups were described to be moving at the speed of the slowest member and the stairs were described as not being crowded. Occupants were deemed to have a limitation if they were slow and elderly, using a mobility device, carrying things, or assisting other occupants.

The occupants were also grouped according to age, as estimated from the video recordings. The first group was children under 2 years old that had to be carried. The second group was children between 3 to 5 years old that needed assistance on the stairs. The third group was children from ages 6 to 12 years old that did not need assistance, but were typically with an adult. The fourth group was teenagers who may have evacuated without an adult. The fifth group was described as young adults (less than 40 years old). The sixth group was older adults (between 40 to 64 years old). The final group was seniors.

The building in Montreal had fourteen floors and 244 apartments. The occupants received a memo four days before the drill informing them that a drill would be taking place and that it would be videotaped. It was also noted that the manual normally given to all residents instructed them that, in the case of a fire, they were to wait on their balconies. The drill only lasted five minutes (a previously unknown feature of the system was an automatic silencing of the alarm after five minutes). The average pre-evacuation time of thirty-one occupants was 90 s. There were no significant differences based on gender, age, or limitation. For descending stairs, the average speed was 1.07 m/s. Fourteen men averaged 1.14 m/s and fifteen women averaged 1.00 m/s, but the difference was not significant. The speeds for the different age groups were not statistically significant, but only three of the groups (children six to twelve and the two adult groups) had more than one person. For those three groups, seven children average 1.30 m/s, eight young adults averaged 1.00 m/s, and thirteen older adults averaged 1.03 m/s. Occupants with limitations traveled at an average speed of 0.88 m/s, also not statistically different, but the authors attributed that in part to only three such individuals being identified. Groups traveled slightly slower than individuals (nineteen group members averaged 1.00 m/s while ten individuals averaged 1.18 m/s).

The Calgary building was also fourteen floors in height and it had 117 apartments. Once again, occupants received a memo four days before the drill. The alarm sounded for 17.5 minutes. While the elevators were supposed to be recalled, they were not and some occupants used them during their evacuation. Thirty-three occupants had pre-evacuation times that averaged 168 s. Based on gender or age categories with at least five individuals recorded, none of the differences were significant. The nine occupants with limitations required a significantly greater average pre-evacuation time (334 s compared to 106 s). The overall average speed on stairs for twenty-eight occupants was 1.05 m/s. Women moved slightly faster, but the difference was not significant. Nearly all of the movement speeds were from young adults (19 out of 28) with no other group having more than five individuals. Eight occupants with limitations were moving at an average speed of 0.61 m/s (compared to an average of 1.22 m/s for the other twenty occupants).

The Gloucester building was twelve floors tall and had 213 apartments. The drill lasted approximately 20 minutes. During the drill, ninety-three occupants required an average of 319 s for pre-evacuation time. For all gender, age, and limitation comparisons (where the category had at least five observations), only seniors had a

statistically different time (in this case, they required more time). The average speed for seventy-six occupants was 0.95 m/s. For descending stairs, men moved statistically faster (1.05 m/s) than women (0.86 m/s). The authors stated that a greater proportion of women being older might have caused this. Based on age, six teenagers averaged 1.28 m/s, thirty young adults averaged 1.12 m/s, twenty-one older adults averaged 0.95 m/s, and eighteen seniors averaged 0.56 m/s. All of these speeds (with the exception of teenagers and younger adults) were statistically different. Twenty-one occupants with limitations averaged a statistically slower speed of 0.57 m/s (compared with 1.09 m/s for the fifty-five occupants without a limitation).

When comparing the three buildings, the average descent speeds were not statistically significant. However the Gloucester building did have a slower speed and the authors attributed this to the colder weather. The authors then combined the populations from the three buildings and found that men (average speed 1.07 m/s) and women (average speed 0.90 m/s) were not statistically significant at their chosen 95% confidence level. However the p-value was 0.06 and that indicates that the speeds were statistically different at the 94% confidence level. Based on age groups, seven children between 6 and 12 years old averaged 1.30 m/s, seven teenagers averaged 1.16 m/s, fifty-six young adults averaged 1.13 m/s, thirty-nine older adults averaged 0.96 m/s, and twenty seniors averaged 0.56 m/s. Seniors were statistically slower than all other groups and the two adult groups were statistically different. Finally, across all three buildings, thirty-two occupants with limitations averaged a statistically slower 0.61 m/s when compared to occupants without limitations who averaged 1.11 m/s.

A.1.8 Proulx, Kaufman, and Pineau

Proulx, Kaufman, and Pineau (1996) observed evacuation drills in two government office buildings in Canada during the fall of 1995. The weather was overcast with temperatures of 19 and 13 ºC. Both buildings were in Ontario (London and Ottawa) and the drills were initiated between 14:00 and 14:15.

Video cameras were located in corridors and in the stairs. The travel distances (in both buildings) changed between floors, but these values (and how they were calculated) were not provided. Movement speeds were based on the total travel distance in the stair and the time required to descend to the exit. Occupants were categorized based on gender and two age groups were also identified (between 20 to 40 years old and between 40 to 65 years old; all occupants were placed into one of the two groups).

For the London drill, the building had seven occupied floors. The drill lasted for approximately 14 minutes and there were 165 occupants present. Of these occupants, 133 used one of three stairs that was available; the side stair (near the main hall) was used by 66.2% of occupants, the rear stair was used by 22.6% of occupants, and the front stair was used by 11.3% of occupants. Occupants were found to use the more familiar stair rather than the closest stair. For ninety-two occupants, the average pre-evacuation time was 36 s with women requiring statistically less time (30 s compared

to 44 s for men). There was no difference in times based on age. The mean speed for all occupants was 0.78 m/s with the side stair users averaging 0.75 m/s, the rear stair users averaging 0.76 m/s, and the front stair users averaging 0.97 m/s. The rear stair had a smaller width, thus creating a higher density with fewer people. For gender, women traveled at 0.81 m/s and men at 0.72 m/s (the result was statistically significant). The authors noted that this contradicted previous research and they could not explain the reason that this building was different. One possible explanation (not stated in the report) was that women had a shorter pre-evacuation time; they would thus experience a decrease in density, which can lead to faster movement speeds. There were no differences in speed based on age. In a post-evacuation survey, 21.2% of occupants reported believing that it was an actual event and not a drill. The actions of these individuals were not statistically different from occupants that thought it was a drill.

The building in Ottawa had seven full levels and 502 occupants. For this building, the drill lasted approximately 20 minutes. As with the previous drill, occupants used the familiar stairs with 46.1% using the southeast stair (leading to the main entrance), 26.0% using the northwest stair (leading to the secondary entrance), 14.2% using the southwest stair, and 13.7% using the northeast stair. The average pre-evacuation time for 161 occupants was 63 s. The average speed on the stairs was 0.93 m/s with the southeast stair users having an average speed of 0.82 m/s, northwest stair users having an average speed of 0.92 m/s, southwest stair users having an average speed of 1.1 m/s, and northeast stair users having an average speed of 1.2 m/s. The number of people entering the stair appeared to alter the speed of occupants descending to that level. Men had a statistically faster average speed (0.96 m/s) than women (0.90 m/s). The difference in speeds based on age was not statistically significant. Questionnaires were again provided after the drill and 23.2% reported interpreting the alarm as an actual fire rather than a drill. The only activity that these occupants were more likely to do than other occupants was saving files and turning off their computers. While not stated by the authors, these were not activities that indicate that occupants thinking it was a real event were being more urgent; if anything these activities increased pre-evacuation times.

A.1.9 Shields, Boyce, Silcock, and Dunne

Shields, et al. (1997) observed an unannounced drill in an educational building (the main Jordanstown Campus Building of the University of Ulster) during the morning of May 4, 1995. There were 276 persons on the five levels of the building. Two stairs were located within the building with 77% of the population using one stair. The large unequal usage arose from occupants using the more familiar stair rather than the closest stair.

Pre-evacuation time varied depending on where the occupant was located. All office workers had left their room of origin within 144 s. In rooms used for academic purposes, the pre-evacuation time was up to 197 s.

During the evacuation, a wheelchair user was assisted down the stairs. This caused congestion on the stairway, but no one tried to pass the wheelchair party despite there being approximately 40 cm to do so. People behind the wheelchair had an average movement speed of 0.33 m/s and those ahead of the wheelchair had average speeds of 1.1 m/s. The authors noted that the average speeds, based on density, were greater than Pauls had found in his study. Their theory for the cause of this difference was that their building was smaller in height and the difference in speeds could come from fatigue. The authors presented two regression formulas to describe the movement speeds of occupants.

$$s = 1.27 - 0.30 \cdot D \quad \text{(A.8)}$$

$$s = 1.69 - 0.05 \cdot D \quad \text{(A.9)}$$

where:

s= speed (m/s)
D= density (persons/m^2)

Equation A.8 was for the population ahead of the wheelchair user and Equation A.9 was for the population behind the wheelchair user. However the graph of the data in the article showed the line associated with Equation A.9 having a steeper slope and values that are approximately:

$$s = 1.69 - 0.50 \cdot D \quad \text{(A.10)}$$

Thus, either the graph or the written equation was in error.

A.1.10 Proulx, Tiller, Kyle, and Creak

Proulx, et al. (1999), as part of a study on photoluminescent markings, recorded occupants in four stairs during a building evacuation drill. The building was a 13-story government office building in Ottawa. The drill was conducted at 13:45 on a day with light snow falling.

The emergency evacuation plan called for the fire floor and the floors above and below to be evacuated first with all other occupants waiting on their floor for instruction. The selected fire floor was the tenth floor and instructions to begin evacuating were not given until 6 minutes after the initial alarm. The building had four stairs located at the corners of the building. One stair had only the photoluminescent markings. A second stair had reduced emergency lighting and photoluminescent markings. The third stair had only reduced emergency lighting. The final stair had normal emergency lighting.

Video cameras were placed at the stair doors for the floors that were to evacuate, at the landing between the fifth and sixth floor in all stairs, and at the exit doors for all four stairs. There were 457 occupants observed during the drill and the average time

occupants needed to reach the exit door was 72 s. The drill was completed within 15 minutes of the initial alarm.

A total of 392 occupants exited from the three floors. In the stair with only the photoluminescent markings, 144 occupants were observed. The average speed of these occupants was 0.57 m/s with a range of speeds from 0.39 to 1.13 m/s. There were 65 occupants in the stair with reduced emergency lighting and photoluminescent markings. The speeds in this stair varied from 0.64 to 1.30 m/s with an average speed of 0.72 m/s. For the stair with only reduced emergency lighting, 82 occupants had speeds from 0.41 to 1.14 m/s and an average speed of 0.70 m/s. In the control stair with normal emergency lighting, there were 101 occupants. Their speeds varied between 0.45 to 0.84 m/s with an average speed of 0.61 m/s. The travel distance in each stair varied, but the authors did not state how they calculated the travel distance or what any of the stair dimensions were.

Based on the control stair having occupants with the second slowest speed (and the order of the average speeds corresponding to the order of the number of occupants), the authors concluded that the difference in speeds was based on the density rather than the photoluminescent markings. Also, counterflow was present in the stair with only the photoluminescent markings.

Density was calculated for the average conditions in each stair during the busiest three minutes of the drill. The densities were 2.05 persons/m^2 (photoluminescent markings stair), 1.00 persons/m^2 (reduced emergency lighting and photoluminescent markings stair), 1.23 persons/m^2 (reduced emergency lighting stair), and 1.30 persons/m^2 (normal emergency lighting stair). How the area used to calculate these values was calculated was not provided.

There were also 30 occupants that left from lower floors despite not being instructed to do so. While the exact speeds were not reported, the authors described these occupants as moving faster since they did not have any density or fatigue issues.

A.1.11 Kratchman

Kratchman (2007) studied two different stairs in a 6-story high-rise building during an evacuation drill on a morning in June 2005 at 9:47. A total of 269 occupants were recorded on videotapes located within the stairwells. One stair was 1.44 m wide and the other was 1.54 m wide. The riser height and tread depths were 20.3 cm and 28.3 cm respectively.

One stair experienced counterflow conditions as firefighters proceeded up the stairs and the other only had unidirectional flow. In the stair without counterflow, the mean speed was 0.80 m/s. For the counterflow case, this value was decreased to 0.70 m/s. These speeds were measured along the slope of the stairs. The travel path on the landing assumed that individuals traveled in straight lines from midpoint to midpoint of each flight of stairs.

In this study, density was measured by counting the number of people over a known area of stair treads in a snapshot every 10 s and assuming that value was constant over the 10 s period. Rather than using the entire buffer zone of 0.3 m recommended by Pauls, the author assumed a buffer zone of 0.13 m accounting for just the handrail projection. Also, rather than using the horizontal area to calculate the density, the author used the area of the sloped surface along the treads. Thus, for the densities to be compared to work done by Pauls, the density in the 1.44 m-wide stair needs to be multiplied by 1.42 and in the 1.54 m-wide stair by 1.40. Also, the reference values that the author used to show that the speeds were less than predicted at a given velocity were for stairs with a smaller riser and tread height. In the Gwynne and Rosenbaum section later in this appendix (Section A.4.9), the reference choice will be shown to be inappropriate based on the assumptions of the reference. For reasons discussed in that later section, the choice might be appropriate in reality, but the author did not present the data in this manner.

When her data is adjusted based on the modifications to density, the data are more in line with the previous findings, but still predict slightly slower speeds. In the speed versus density graphs, nearly all speeds, even at very low densities, were less than the average speed reported earlier in the thesis. The author did not note or explain why occupants in the selected segment that was graphed appeared to be moving slower than the average people across all density values. Since the travel distance used to calculate the speeds on these graphs was different that other places in the thesis, there is probably an error in one of the two the calculation methods. If the actual speeds were in line with the average speed reported earlier in her thesis (and the density adjusted appropriately), then the speeds fall well within the range of the previously cited works.

While it was not statistically significant, occupants in the stair with counterflow sped up as they descended. The author indicated that this might have been caused by a decrease in counterflow at the lower levels. In the stair without counterflow, speeds generally did not increase from the initial speed and there was a decrease in speed when the stair became more crowded at a middle level. During the counterflow, occupants descending moved to the right (inner) exit lane.

Occupants were seen engaging in activities that were not accounted for in the equations (socializing, group behavior, reentry, stopping to let firefighters pass, etc.). Men had a slightly greater average speed than women, but the difference was not statistically significant.

During the evacuation, nearly half of the population was carrying items with women being nearly three times more likely to be carrying an item than men. The primary cause for this discrepancy came from over half of the women carrying a purse or briefcase while less than 3% of men did so. Passing behavior was observed with the faster individual moving to the outer exit lane.

A.1.12 Proulx, Bénichou, Hum, and Restivo

Proulx, et al. (2007) used a single fire drill to collect data based on different photoluminsecent coatings in a 13-story office building in Ottawa, Canada. Approximately 4000 occupants were in the building during the drill that started at 10:35 am on October 5, 2006 and 1191 were recorded in the studied stairs. Four of the six windowless stairs in the building were observed during the six-minute duration of the drill.

All four of the stairs had widths of 1.1 m, but no information was reported about the riser height and tread depth. Overhead images of the stair treads were to calculate density. They had similar densities that ranged from 1.56 to 1.60 persons/m^2 during the busiest five minutes of the drill and the maximum density, when the occupants were at a standstill, was 2.30 persons/m^2. The speeds for descent ranged from 0.17 to 1.87 m/s. However how the travel distance was calculated was not provided. The mean speed in three of the four stairs was between 0.57 to 0.66 m/s. While one stairwell had a slower mean speed, 0.40 m/s, this was attributed to individuals with mobility impairments in the stairs rather than the photo-luminescent coatings.

Most occupants required between 1 to 5.5 minutes to enter the stair. Once in the stair, they tended to stay to the right or form a staggered file at higher densities and to slow down as they descended. The authors attributed this to the merging of additional people from the floors into the stair. Stagnation in the flow was observed near the merging areas. Handrail use also appeared to cause individuals to progress single-file and thus move at the speed of the slowest individual. No passing behavior was observed to overtake individuals using the handrails. At the higher floors, between 70 to 90% of occupants were using handrails. This decreased to 30 to 60% near the level of discharge. The authors provided two explanations: the lighting was better at the lower level which made the occupants feel safer and thus not hold the handrail or the occupants were starting to button their coats in preparation for going outside.

A.1.13 Hostikka, Paloposki, Rinne, Saari, Korhonen, and Heliövaara

Hostikka, et al. (2007), as part of a larger study, observed the evacuation of 281 occupants from a 7-story office building in November 2006. The building occupants were told what day the drill would occur, but not the time of the drill. There were four egress paths usually available, but two of the more commonly used exits were blocked using cold smoke.

Occupants were observed using both video cameras and radio frequency identification (RFID) tags. Only occupants that worked on floors 5 and 6 (82 occupants) were given the RFID tags and these readings were only collected in one of two usable stairs. Only about 60% of the expected RFID tags were read and the lower floors saw higher percentages of RFID tags read than the upper floors.

Queues formed under two different scenarios. First, slower individuals moved to the side to let people from higher floors pass them. Second, one group stopped to let occupants from lower levels enter the stair.

From video images, the flow rates on the lower floors were reported to range from 0.80 to 0.83 persons/m-s. Of the occupants with RFID tags, 44 were recorded on consecutive floors for a total of 97 data points. The movement speeds were calculated based on the difference in times between two RFID readers a known distance apart. The exact means of calculating this distance was not provided and there was no mention of whether the dimensions were effective or total. The density that corresponded to these speeds was approximated by using the flow values from the video data. For densities less than 0.5 persons/m^2, the data was scattered with most observations falling between 0.5 to 1.5 m/s. For densities between 0.5 to 2.5 persons/m^2, the velocity decreased linearly from approximately 0.75 to 0.5 m/s. The median value of a fitted curve was 0.64 m/s. Also, men and women were found to travel at the same speeds.

A.1.14 Peacock, Averill, and Kuligowski

Peacock, Averill, and Kuligowski (2009) collected data from three high-rise buildings that ranged in height from 6 to 18 stories. Typically, 100 to 300 persons used the stairs during the evacuations. The stairs varied in width from 0.91 to 2.24 m. The riser heights varied from 18.6 to 20.3 cm with tread depths of 25.4 to 28.3 cm (typographical errors corrected from published paper).

The average speeds in the different buildings varied from 0.40 to 0.83 m/s. While not stated in the publication, these speeds were the slope component. Occupants that started higher in the buildings tended to have slower speeds and the average speed in the six-story building was the greatest and in the 18-story building it was the least. In the six-story building, the occupants in the stair with firefighter counterflow tended to move more slowly than the stair without counter flow. The 18-story building saw the occupants in the stair with firefighter counterflow move at a faster speed, but that was assumed to be related to the lower level of congestion in that stair.

A multiple regression analysis based on the variables of counterflow, delay time, distance traveled, stair width, density, and gender was conducted. How some of these variables were defined was not specified in the paper, but it is believed that counterflow was a binary variable for each observation of each individual, delay time and distance traveled were based on the initial appearance on a camera, stair width was the total width, and the density calculation used the entire area of the landing and treads. Gender was found to not be predictive and the other variables accounted for only 13% of the variance.

A.2 Normal-Use Studies

Similar to fire drills, observations made under normal-use conditions can be used as a basis for predicting movement speeds during emergency evacuations. Most of these

studies involve observations made in mass transit or other public facilities. The assumption is that the occupants are primarily concerned with getting to their final destination. Even more so than was the case with the fire drill studies, these studies do not involve fire cues and it is unknown how close actual behavior in an emergency evacuation would be to this data.

A.2.1 National Bureau of Standards

The National Bureau of Standards (1935) observed stairwells under normal, drill, and laboratory conditions; most were normal conditions. Occupant counts were made once the stairwell was filled. At this point, either one individual that could be observed from start to finish or an audible clue (a second researcher that moved with the flow gave a whistle upon entering) started the timing and counting of people that passed the end point. Once the designated person passed the endpoint, the timing and counting ceased.

The report gave the number of people discharged per unit width per unit time and the area per person by dividing the known area by the number of people that were counted. In the discussion here, those numbers are converted back to a velocity using the same assumptions as the authors.

The first stair was at a theater. It was 1.90 m wide with a 19.1 cm riser and 28.6 cm tread. The average discharge rate was 0.601 persons/m-s with a maximum rate of 0.711 persons/m-s. These values corresponded to densities of 1.33 persons/m^2 and 1.86 persons/m^2. For all of the values in this report, the authors were assumed to have used the total width of the stair and to have only used paths along stair treads. If these assumptions are correct, then the discharge rate and density values were 0.714 and 0.844 persons/m-s and 1.58 and 2.21 persons/m^2 respectively. Thus, the speed was approximately 0.452 m/s for average conditions.

The second stair was 1.52 m wide and located at a transit station. The riser height was 18.4 cm and the tread depth was 30.5 cm. The average and maximum discharge rates were much greater than the theater, 1.04 and 1.53 persons/m-s respectively (1.30 and 1.91 persons/m-s for assumed effective width), and the authors attributed this to greater motivation on the part of the observed people to exit the transit station. The densities were also increased as the average density was 2.20 persons/m^2 and the maximum density was 2.83 persons/m^2 (2.74 and 3.53 persons/m^2 for assumed effective width). The average speed was thus 0.473 m/s.

The third stair was a controlled test at the National Bureau of Standards where people were assembled at the top of the stair and instructed to descend naturally without attempting to run. It was 0.914 m wide and had 17.8 cm risers and 29.2 cm treads. The average discharge rate was 1.70 persons/m-s and the maximum specific flow was 1.86 persons/m-s (2.53 and 2.77 persons/m-s with assumed effective width). The average and maximum densities were 2.63 persons/m^2 (3.92 persons/m^2 with assumed effective area). This corresponds to an average speed of 0.646 m/s.

While the three stairs were under different types of occupancies, there did not appear to be a relationship between movement speed and density. While it occurred in a controlled situation, the highest density was where the movement speed was the greatest.

In addition to the stairs where densities were provided, eight other stairs were presented with just the flow rates. These stairs were from a variety of building types as well as experimental conditions.

The first building with just a flow rate was an office building during a fire drill. The stair was 2.22 m wide with a riser height of 17.8 cm and tread depth of 30.5 cm. The average flow was 1.26 people/m-s (only higher average flow recorded was in the controlled test previously mentioned) and the maximum flow was 1.31 persons/m-s.

A second office building had a stair 2.20 m wide with a riser height of 16.5 cm and a tread depth of 30.5 cm. The average and maximum reported flows were 0.77 and 0.98 persons/m-s. Next, a pair of stairs at two different office buildings had widths of 1.83 and 1.68 m. The riser heights were both 17.8 cm. The tread depth in one building was 27.9 cm and it was 26.7 cm in the other. In both buildings, the average and maximum flows were 0.77 and 0.93 persons/m-s. A fourth office building had a 1.26 m-wide stair with a riser height of 20.3 cm and the tread depth was 28.6 cm. The average and maximum flows were 0.93 and 0.98 persons/m-s. A final office building had a 1.22 m-wide stair with a riser height of 19.0 cm and a tread depth of 29.2 cm. The average reported flow was 0.71 persons/m-s and the maximum flow was 0.77 persons/m-s.

Some observations were also made at transit stations. At one, the stair was 1.83 m with a riser height of 17.8 cm and a tread depth of 29.2 cm. The average flow was 0.93 persons/m-s and the maximum flow was 0.98 persons/m-s. A second station had a 1.52 m-wide stair. The riser height and tread depth were 18.4 and 30.5 cm respectively. The average and maximum flows were 0.98 and 1.09 persons/m-s.

Finally, they reported some flow values found by Illinois Central Railway. The first stair was 1.68 m wide with a riser height and tread depth of 17.8 and 27.8 cm respectively. The average flow was 1.04 persons/m-s. A second stair was 1.22 m wide with a riser height of 17.8 cm and tread depth of 29.2 cm. The average flow on that stair was 1.59 persons/m-s. For two other locations, no stair dimensions were given and the flows were reported as 0.98 and 1.09 persons/m-s.

A.2.2 London Transport Board

The London Transport Board (1958) observed passengers in nine London subway stations. Observations were made by one of three methods. First, to calculate the flow, a researcher recorded the amount of time required for 50 passengers to pass a designated point. The shortest three times were used to calculate the flow. While not stated by the authors, only using the shortest times would serve to give higher estimates of flow than if all values were used. Second, two researchers stood a

known distance apart within a crowd. Upon a signal, both researchers started their stopwatches and the one in the upstream position started to move with the flow. The number of passengers to pass the stationary observer were counted and combined with the time and known distance to calculate speed and density. Third, during off-peak times, passengers were recorded walking a known distance in a given time to get the free speeds. The stairs were 1 to 2 m wide and had between 19 to 23 uninterrupted steps or two sets of 12 steps. No details were given about the tread dimensions or the number of observations. The free flow speed was 0.98 m/s. At conditions of maximum flow, the speed was 0.67 m/s. The authors did not indicate if this was the horizontal component or the slope component of the speed. At maximum flow conditions, the flow was 1.1 persons/m-s and the density was 1.6 persons/m^2 (both of these values are assumed to be based on the total width, but the authors do not indicate if this is the case or not).

The authors noted that, for stairs less than 1.22 m, occupants exited proportional to exit lanes 0.53 m wide and, above this threshold, it was proportional to the entire width. This was partially based on a 1.8 m wide stair observed both before and after a handrail was installed down the middle of it. After the handrail was installed, the flow rate dropped to 81% of its original value. The authors attributed this to there previously being three exit lanes and that was reduced to two. If that theory were correct, the flow should have decreased to 67% rather than 81%.

The authors also found that the flow rate was approximately a constant for most densities studied. As density increased, speed was found to proportionally decrease. Also, the introduction of counterflow was not observed to alter the total flow.

A.2.3 Fruin

Fruin (1971), as part of his work on pedestrian planning, noted that energy use on stairs was 10 to 15 times greater for ascent and about one third more for descent than walking on level ground. In addition, the human body tended to sway, resulting in exit lanes of 0.762 m.

For downward travel, movement speeds had a bimodality that the author said indicated that there are two different normal speeds depending on unknown variables. Furthermore, there was a significant difference in speed based on gender and a slightly less decrease in speed based on age.

On an indoor stair with a 17.8 cm riser and 28.6 cm tread, men under 30 years old had an average slope component of speed of 0.975 m/s. For men between the ages of 30 to 50 years, men over 50 years old, women under 30 years old, women between 30 to 50 years old, and women over 50 years old, the average slope movement speeds were 0.814 m/s, 0.670 m/s, 0.700 m/s, 0.598 m/s, and 0.556 m/s. On an outdoor stair with a 15.2 cm riser and 30.5 cm tread all ages and genders saw their average speed increase generally by a factor between 1.1 to 1.2. For men, the average speeds were 1.10, 0.957, and 0.706 m/s for the age groups from youngest to oldest. The three female age groups, in the same order, had average speeds of 0.790, 0.766, and 0.664

m/s. These values are presented in Table A.1. It appears that the observations were made for only travel on the treads.

Table A.1: Fruin's Recorded Descent Speeds

Stair Dimensions (cm)	Gender	Age (years)	Speed (m/s)
17.8 by 28.6	Male	<30	0.975
		30 to 50	0.814
		>50	0.670
	Female	<30	0.700
		30 to 50	0.598
		>50	0.556
15.2 by 30.5	Male	<30	1.10
		30 to 50	0.957
		>50	0.706
	Female	<30	0.790
		30 to 50	0.766
		>50	0.664

Based on energy expenditure, the author recommended that the maximum riser height should be 17.8 cm. The author did not indicate the densities present during these surveys, but he did provide some guidance for the relationships between speed and density.

Fruin divided the different stair density conditions into six levels of service. Level A was 0.54 persons/m^2 or less in which individuals can freely choose their own speed and pass slower individuals. Level B was 0.54 to 0.72 persons/m^2 in which individuals can freely choose their own speed, but passing slower individuals is difficult. Level C was 0.72 to 1.08 persons/m^2 in which some individuals are restricted in choosing their own speed and cannot pass slower individuals. Level D was 1.08 to 1.54 persons/m^2 in which most individuals are restricted in choosing their own speed. Level E was 1.54 to 2.70 persons/m^2 in which movement speed is severely restricted and intermittent stoppages occur. Level F was 2.70 persons/m^2 or more in which most individuals are stopped; this level of service was not recommended for design under any condition.

A graph, without an accompanying equation, showed an asymptote to the slope speed for densities less than 0.54 persons/m^2 of approximately 0.7 m/s. At higher densities, the speed decreased nonlinearly.

In a separate article Fruin (1971a) used a stadium stair to provide an equation for movement speeds down stairs.

$$s = 0.650 - 0.097 \cdot D \quad \text{(A.11)}$$

where:

s= speed (m/s)
D= density (persons/m^2)

The author described four to five treads per person as being the normal spacing on the steps and this was Level of Service C. The maximum density was found to be approximately one person every other tread which equated to being Level of Service F. It was not stated whether this was the horizontal or slope speed or how the density was calculated.

A.2.4 Daly, McGrath, and Annesley

Daly, McGrath, and Annesley (1991) observed passengers descending stairs (and using other components) at eight London Underground stations from November 6 to 14, 1989. Observations were made during both the peak period as well as the inter-peak period. All stairs that were observed had two-way flow conditions and 796 passengers were observed descending the stairs (compared to 496 ascending the stairs). Due to the two-way conditions, the authors made adjustments to the required capacity, but the adjustments were the same as those recommended for level surfaces. Even with these adjustments, the authors noted that the capacities were at or below the expected capacity of 1.14 persons/m-s in all but one observation site. While not stated by the authors, the difference in gait and the more narrow stairs (than many level components) could lead to even minor counterflows having a more significant impact on the flow (Fruin 1971); this is potentially supported by the finding that the flows were not as great as expected.

The authors did not report the tread dimensions, the number of flights of stairs observed (they did say that, for components including stairs that observations were made at multiple stations and/or on multiple days), or the observed density ranges. They did state that the slant length varied from 5.99 to 9.34 m (thus the assumption was that the speeds reported are along the slope, but this, too, was not explicitly stated) and that the effective width of the stair ranged from 1.13 to 1.80 m after adjusting for boundary layer effects (0.31 m for either a hard edge or handrail).

Based on a curve fit and a base equation form that was used for all types of components studied, the authors proposed that speeds descending stairs (up to the capacity value of 1.14 persons/m-s) could be calculated by:

$$s = \frac{1}{t_0/L + (C/L)\cdot(f/1.14)^{2.7}} \quad \text{(A.12)}$$

where:

s= speed (m/s)
L= travel distance (m)
t_0= free flow travel time (s)
C= model derived constant (s)
f= specific flow (persons/m-s)

The free speed was found to be 0.67 m/s with a speed at capacity (1.14 persons/m-s) to be 0.56 m/s. Using these values in Equation A.12, t_0/L is approximately 1.5 and C/L is approximately 0.3.

The authors made the implicit assumption that people change their movement speeds even with very small changes in density from the free-flow conditions. If reality is closer to the assumption made by Fruin, that up to a certain density people can move at their free-flow speed, then the equation will artificially adjust to fit data from both regimes; this would lead to under predictions at lower speeds and over predictions at higher speeds.

A.2.5 Tanaboriboon and Guyano

Tanaboriboon and Guyano (1991) studied four different descending stairs in Bangkok, Thailand. The observations were made under normal use conditions and no consideration was given to the density that corresponded to a given speed. The authors did not indicate if the speed values were for horizontal or slope speeds.

The first stair had a 20 cm riser and 30 cm tread, was 1.20 m wide, and the observation length was 5.00 m. The authors observed 205 individuals with speeds ranging from 0.388 to 0.874 m/s with a mean speed of 0.583 m/s.

The second stair had a smaller riser, 15 cm, and the same tread width, 30 cm, as the first stair. It was 3.00 m wide and the observation length was also 5.00 m. The authors observed 307 individuals with speeds ranging from 0.435 to 0.820 m/s with a mean speed of 0.598 m/s.

The third stair had a 14 cm riser and 30 cm tread, was 1.20 m wide, and the observation length was 5.40 m. The authors observed 140 individuals. The minimum speed observed was 0.440 m/s and the maximum was 0.815 m/s. The mean speed was 0.610 m/s.

The final stair had the smallest riser, 13 cm, and a 30 cm tread like all of the other stairs. It was 1.40 m wide, and the observation length was 4.50 m. The authors observed 215 individuals with speeds ranging from 0.459 to 0.893 m/s with a mean speed of 0.620 m/s.

A.2.6 Lee and Lam

Lee and Lam (2006) used video recordings of stairs in Hong Kong mass transit railway stations on the last two Fridays of January and the first three Fridays of February in 2001. Observations were made using a handheld video camera on a tripod during the morning peak (8:00 to 10:00), afternoon off-peak (14:00 to 16:00), and evening peak (17:30 to 19:30) hours. The observation area was delineated using tape on the ground and the precision of the data was 0.04 s.

Their observations were part of a larger study that was intended to provide a better understanding of route selection by occupants in a congested station. The study examined both the unidirectional and bidirectional flow cases for ascending and descending stairs.

The stair had an effective width of 1.94 m with a riser height of 16 cm and a tread depth of 31 cm. Observations were recorded over a length of 5.58 m with the data extraction process being automated. When the stairs were at the peak capacity, the average descending speed ranged from 0.48 to 0.65 m/s. The first number corresponded with a heavy counterflow while the second number was under a unidirectional flow. The authors did not state whether the speed was for the horizontal or slope component of speed.

Within the average flows, some individuals were moving faster as they weaved through the other people. Others went slower than the average flow as well. For descending the stairs, the individual speeds varied from 0.38 to 0.92 m/s and 0.29 to 0.93 m/s for the unidirectional and heavy counter flow cases respectively.

This study is one of the few that has attempted to examine the speeds of individuals within the average flow. No consideration was given as to why individuals chose to go at a speed different than the average nor if there were characteristics that distinguished these individuals from the general population.

A.2.7 Ye, Chen, Yang, and Wu

Ye, et al. (2008) made videotape observations of people descending stairs from 8:00 to 10:00 a.m. in one subway station in Shanghai, China from October to November 2006. The stair had 15 cm risers, 30 cm treads, and was 3.05 m wide. Observations were made over a length of 3.35 m as measured along the slope.

The authors calculated density by using 15 s intervals and averaging three points within the interval; rather than calculating the speed of all individuals, the authors only calculated the speeds of three individuals within a given crowd that did not engage in passing behavior. Thus, the values were more representative of the bulk flow rather than individual flow. This resulted in 410 data points. However the authors did not state if they used the horizontal component of density or if they used the slope length to determine the area. They also did not state if they used the effective or total area.

Speeds primarily fell between 0.5 to 1.2 m/s for densities up to 1.7 persons/m^2. Based on their observations, the authors recommended a calculation for the flow per meter:

$$f = 0.996 \cdot D - 0.159 \cdot D^2 \quad \text{(A.13)}$$

where:

f= specific flow (persons/m-s)
D= density (persons/m^2)

While not provided by the authors, with the assumption that the specific flow is the speed multiplied by the density, Equation A.13 can be used to determine the free-flow speed and maximum density as was done for Equation A.4. In this case, the free-flow speed would be 0.996 m/s and the maximum density 6.30 persons/m^2.

A.3 Post-Incident Studies

In order to better understand how behavior is different in an actual emergency in comparison to drills and normal use, some studies have been conducted that surveyed victims of actual fires. These studies relied on individuals' ability to recall all of their actions during the emergency. In most cases, the authors did not ask respondents to estimate their movement speed. In only a few known studies have the authors attempt to estimate the movement speeds of individuals descending stairs. In these estimates, the exact times were not known and other variables (like density) were either approximated or not collected in combination with the speed values.

A.3.1 Galea and Blake

Galea and Blake (2004) gathered over 250 accounts from the public record of survivors from the World Trade Center collapse. Relying on the public record meant that the survey was not scientific and the accounts tended to be from occupants higher in the building. The information related to 3,291 experiences of 260 occupants.

In Tower 1, the stairs were reported to be crowded below the 44th floor and slow moving between the 44th and 76th floors. In Tower 2, the floors between the 44th and 78th floor were, at least initially, crowded. Below the 44th floor, the flow was fast moving. Occupants typically traveled in groups (90% in Tower 1, 88% in tower 2), but the groups changed size during the evacuation, both gaining and losing members.

Occupants typically reported able-bodied individuals using one exit lane while the other exit lane was reserved for injured occupants (and those assisting them). Water was reported in the stairs and the authors believed that it could have hindered the evacuation. There were some reports of fatigue, typically caused by the nature of footwear worn by some female occupants. Counterflow was also reported as a hindrance to movement down the stairs.

A total of twenty-nine accounts provided enough time cues to estimate descent times, but even this group usually gave an approximate time (or a range of times). Only eight accounts (four in each tower) gave specific initial and final times and did not have extraneous actions. Eight accounts in Tower 1 and three accounts in Tower 2 gave either small ranges of times or had extraneous actions. The final five accounts from both towers were not reliable due to wide time ranges or extraneous actions. In Tower 1, occupants were estimated to travel at 29 to 33 s/floor (approximately between 0.25 to 0.41 m/s). Occupants in Tower 2 were estimated to travel at a faster speed of 20 to 29 s/floors (approximately between 0.2 to 0.7 m/s). The m/s calculations were based on occupants traveling down the middle of the stars, making 90º turns, walking half the stair width onto the landing, and then mirroring this path.

A.3.2 Averill, Mileti, Peacock, Kuligowski, Groner, Proulx, Reneke, and Nelson

Averill et al. (2005) conducted 368 telephone interviews with survivors of the World Trade center collapse. In each tower there were two 1.1 m-wide stairs and one 1.4 m-wide stair. Individuals were observed to be altruistic. Some individuals left the stair that they started in due to instructions or deteriorating conditions within the stairs and some women removed their high-heeled shoes. Counterflows were present in some of the stairwells as emergency personnel ascended towards the fire floors. In Tower I, the average movement speed was 0.2 m/s for the entire time in the stairs. This included any rest periods and stopping due to overcrowding in the stairs.

A.3.3 Shields, Boyce, and McConnell

Shields, Boyce, and McConnell (2009) used data collected from interviews from six World Trade Center survivors that had self-identified mobility impairments prior to September 11, 2001. For five of the six occupants, the authors were able to describe the activities and movement speeds (in terms of floors) as they descended.

Participant A, initially on the 64th floor of Tower 1, had recently had knee surgery, had discomfort descending the stairs, and needed to use the handrail for support. While she descended, she allowed others to merge into the flow and deferred to firefighters climbing the stairs. Her speed was also decreased when she encountered water in the stairs. She still managed to descend at the pace of 46 s/floor.

Participant B suffered from hypertension. He was initially located on the 63rd floor of Tower 1 and immediately started herding other people towards the exits. In the stair he experienced some crowding, merging of flows, and deferential treatment towards injured occupants and firefighters ascending the stairs. His rate of descent was approximately 43 s/floor.

Participant C needed an air cast for his injured ankle and was using crutches to move around. During his evacuation from the 54th floor of Tower 1 he did not have a shoe on his injured foot. He entered the stair with thirteen other individuals from his floor and they encountered crowding and merging as they descended. Once again,

deferential treatment was shown to allow more injured occupants to pass as well as firefighters. He ended up separating from his group and passing people as he descended. As was the case with Participant A, his descent rate was approximately 46 s/floor.

Participant D was initially on the 17th floor of Tower 1. She had multiple mobility impairments and descended immediately with several colleagues. They descended single-file, even though the stair was empty when they entered, so that anyone that attempted to come up the stair could pass them. Around the 10th floor, the person with her offered her part of his shirt to block out the strong smell of jet fuel in the stair. They then had to ascending up three levels due to further passage in that stair being impossible; the second stair had the same result of starting to descend before having to return to a higher floor and change stairs. While descending she required an average of 150 s/floor (including the time needed to ascend and change stairs).

Participant E required canes for moving. She started on the 20th floor of Tower 1 and recruited three colleagues to act as crowd control (so she would not be knocked over) while descending the stairs; one walked behind her, one next to her, and one in front of her. They had to stop every few floors to allow some of her helpers (they had asthma) stop and recover. As they descended, they allowed other people to pass them, but a group formed behind them that refused to pass (one even walked down to her, gave her some water, and then got back in line behind her). They also experienced some crowding as they descended at approximately 75 s/floor.

A.3.4 Galea, Hulse, Day, Siddiqui, and Sharp

Galea et al. (2009) interviewed survivors of the World Trade Center collapse (129 from Tower 1 and 125 from Tower 2). From these accounts, they attempted to approximate the density that was present for each floor, but they did not indicate how the area was calculated. Speeds were calculated along the slope of the stairs, but no direct mention was given about how the travel distance on the landing was measured.

From the accounts of thirty interviewees from Tower 1, estimates of movement speeds down the stairs were approximated. After attempting to eliminate known stops and other identifiable issues, the average adjusted speed was 0.29 m/s. Subgroups of the population, based on body mass index, found no differences in movement speeds. The authors indicated that there was a possibility that the number of stops required by most occupants while descending masked this variable.

From the total survey, not just the interviewees used for the movement speed calculation, the authors found that 86% of interviewees had to stop in the stairs during their descent. Congestion was the most common cause of stopping, followed by allowing others to pass and fatigue; usually a companion that needed to rest.

A.4 Compiled Studies

Rather than conducting their own studies, some authors have attempted to develop their own movement speed values for descending stairs based upon the works of other authors or their own perceptions. The sources reported here also include an instance where the authors present the results from another author that was not published in English.

A.4.1 Joint Committee

The Joint Committee (1952) examined different codes and studies from the United Kingdom, Canada, and the United States and looked at the complete situation with respect to the built environment in relation to fire. From these, they made a list of recommendations for all aspects of building design.

For stairs, they recommended that values should be determined from the perspective of 0.53 m-wide units of width. The width used was the entire width and no boundary layer was suggested. Their logic was that, at a basic level, people would walk down stairs as moving files. With a small increase in width, an additional file of people could not be added and there was no data supporting the fact that there would be a linear increase in discharge rate. However the authors did not explain how they determined that 0.53 m was the correct value for an exit lane.

In addition to comments about how people would be in lanes, the authors stated that, from everyday observations, slightly wider stairs seemed to allow greater movement speeds. They could not find this supported in the data of others, so they recommended more testing be undertaken to determine if small increases in width led to higher speeds. However they did add that, if the stair width was only slightly deficient, and the addition of another unit would be unduly expensive, small increases in width could be used to provide adequate means of egress.

The authors found a wide variation in the current data (from 0.60 to 3.4 persons/m-s). The highest rates were reported in a French study where the subjects (firemen) were told to hurry. They cautioned that these speeds were not expected in most crowds and that, in one test where a subject fell, the speed was then the same as the normal tests.

Based on all of the different codes and studies, they assumed that people in an emergency would behave in an urgent manner and thus recommended that flow rates be 0.94 to 1.41 persons/m-s (in terms of 0.53 m-wide exit lanes).

For a stair serving only one floor, the authors believed that fatigue would cause occupants to slow down and that the flow should be calculated based on an increase of 8% for every 3.05 m above 6.10 m. They did not state what led to this conclusion.

A.4.2 Galbreath

Galbreath (1969) used the work of the Joint Committee and London Transport Board to develop an equation for the time required to complete an evacuation.

$$T = \frac{N + n}{r \cdot u} \tag{A.14}$$

where:

T=time
N=persons above the first floor
n=persons per floor
or area of stairs divided by 0.3 m^2/person (whichever is less)
r=rate of discharge with r_{max}=2.5 persons/m-s
u=number of 0.56 m exit lanes

The equation could be used with any sets of units since there are no empirical constants in the equation.

The author also estimated that a typical stair would have a travel path of 8.2 m per floor. This consisted of a pair stair flights that were 1.9 m long and four lengths of the stair width (1.1 m). The area of the stair shaft was said to be 9.2 m^2. The area was taken by using the length of travel while on the treads.

Using the typical stair dimensions, number of persons/floor (60, 120, 240), and number of levels (15, 20, 30, 40, 50), the author calculated total evacuation times that ranged from 9 to 131 minutes.

A.4.3 Melinek and Booth

Melinek and Booth (1975), based on the work of Fruin, the London Transport Board, and Togawa made several recommendation for calculating stair movement. They recommend a normal capacity of 1.1 persons/m-s and an unimpeded movement speed of 0.5 m/s. Furthermore, they state that the normal time for an unimpeded crowd to descend one story is 16 s.

A.4.4 Predtechenskii and Milinskii

Predtechenskii and Milinskii (1978) reported that research at the Institute of Architecture of the Russian Academy of Arts (VAKh) found that the speed for descending stairs varied from 0.183 to 0.267 m/s. It is not clear if this was the speed along the slope or the vertical component. The speed was inversely proportional to the density. VAKh recommended using 0.167 m/s for design purposes.

In their list of design parameters (for slope speeds), Predtechenskii and Milinskii recommend using values for every density from 0.01 to 0.92 m^2/m^2 under emergency,

normal, and comfortable conditions. The emergency speeds were developed based on the assumption that the 75th percentile speed would be the average under emergency conditions; no measurements under emergency conditions were recorded. For emergency design, the values range from 0.098 to 0.991 m/s. For example, a normal recommended speed of 0.167 m/s corresponds to a density of approximately 0.59 m^2/m^2 with an emergency speed of 0.202 m/s.

The authors also stated, without citing any studies or data, that movement speeds are at a maximum when nearest to a fire and then decrease to normal speeds once far away from the fire.

To calculate the length of travel down stairs, they proposed two equations:

$$L = \frac{2 \cdot L'}{\cos(\alpha)} + 4 \cdot b \qquad \text{(A.15)}$$

$$L = L' \cdot \left(\frac{3}{\cos(\alpha)} + 1 \right) + 4 \cdot b \qquad \text{(A.16)}$$

where:

L=actual distance traveled (m)
L'=horizontal projection of path on stairs (m)
α=angle of inclination to the horizontal (degrees)
b=width of stairs and depth of landing (m)

Equation A.15 is valid for one story with two flights of stairs. Equation A.16 is to be used for one story with three flights of stairs.

Speeds decreased as density increased. These observations were made under normal use and most of the observations were at lighter densities since densities nearing the maximum were very rare. They proposed equation for descending stairs was:

$$s = \left(112 \cdot d^4 - 380 \cdot d^3 + 434 \cdot d^2 - 217 \cdot d + 57 \right) \cdot \left(0.775 + 0.44 \cdot e^{(-0.39 \cdot d)} \cdot \sin(5.61 \cdot d - 0.224) \right) \Big/ 60 \qquad \text{(A.17)}$$

where:

s=speed (m/s)
d=density (m^2/m^2)

The equation is valid for descending stairs with d<0.92 m^2/m^2. These curves were described to fit well with the experimental data. In emergency conditions, the equation was multiplied by 1.21. According to the authors, if the staircase is steep, the emergency condition multipliers should not be used and might even need to be reduced below normal conditions speeds. The design values that the authors provide

do not match this equation and they do not explain how those values were determined.

Similar to Fruin's level of service, the authors proposed different movement behavior based on density. At densities less than 0.05 m^2/m^2, people can overtake slower individuals and engage in passing behavior. Up to 0.15 m^2/m^2, individuals are still engaged in streamline, unidirectional flow, but passing is not readily possible. At higher densities, interactions with other individuals start to determine the movement speed. Up to approximately 0.4 m^2/m^2, individuals can maintain a natural rhythm in their movement. By 0.75 m^2/m^2, contact has become so prevalent that the individuals are moving as a single unit.

The authors recommended that flights of stairs should not have more than 18 steps, the width of the stairs between handrails should be greater than 1.1 m and less than 2.4 m, the slope should be less than 30º, and the treads should be 15 cm by 30 cm.

A.4.5 Pauls

In an article by Pauls (1984), no new data was presented. Instead the author presented a base equation:

$$\frac{(b-\delta)}{P} = 8.040 \cdot t^{-1.37} \qquad \text{(A.18)}$$

where:

b= width of the stairwell (m)
∂= boundary layer (m)
P= population in the stair (persons)
t= time (s)

This equation is an alternate form of Equation A.1 with the constant value changed slightly.

Based on the author's opinion, not on data (the author specifically stated not to use his values without additional analysis), recommendations were made on how to adjust the $(b-\delta)/P$ value for different riser heights and tread depths. First, 1%, up to a maximum of 10% was to be subtracted for every 0.5 cm that the tread depth was greater than 28 cm. Second, 1% was to be added for every 0.5 cm that the tread depth was less than 28 cm. Third, 1%, up to a maximum of 10% was to be subtracted for every 0.5 cm that the riser height was less than 18 cm. Fourth, 1% was to be added for every 0.5 cm that the riser height was greater than 18 cm.

Equation A.4 can thus be rewritten as:

$$s = 1.08 - 0.29 \cdot \left(\frac{1}{((b - \delta)/P) \cdot y} \right) \quad \text{(A.19)}$$

where:

s= speed (m/s)
b= width of the stairwell (m)
∂= boundary layer (m)
P= population in the stair (persons)
y= length of area (m)

A.4.6 Templer

In his book that dealt with safe stair design, Templer (1992) stated that the average horizontal speed on stairs was 0.45 m/s. How this value was determined was not provided.

A.4.7 Ando

Smith (1995) compiled the work of many previous authors and specifically gave details about work done by Ando in Japan. Ando used extensive (in the words of Smith) observations of passengers in subway stations that were unaware that they were being videotaped. According to Ando, density would reach stagnation when it was 4 persons/m^2. For movement down stairs, he proposed a linear decrease in speed from approximately 0.9 to 0.1 m/s as density increases from 0 to 6 persons/m^2. There was no indication whether this was the horizontal or slope component of speed. While not provided, this would result in an equation of approximately:

$$s = 0.9 - 0.13 \cdot D \quad \text{(A.20)}$$

where:

s= speed (m/s)
D= density (persons/m^2)

A.4.8 Proulx

Proulx (2008) primarily reported the equations that Pauls (1980) had determined from his original research. The author provided reference values for minimum, moderate, optimum and crush values. Those values are presented in Table A.2.

Table A.2: Crowd Movement Parameters from Proulx

Condition	Density (persons/m2)	Speed (m/s)	Specific Flow (persons/m-s)
Minimum	<0.54	0.76	<0.27
Moderate	1.1	0.61	0.77
Optimum	2.0	0.48	0.98
Crush	3.2	<0.20	<0.66

Under moderate conditions on a 1.22 m-wide stair, each individual would occupy 1 to 2 treads, have a speed of 0.5 m/s, and descend approximately one floor every 15 seconds. This is similar to the values found by Kagawa, Kose, and Morishita (1985) and level of service C from Fruin (1971) mentioned previously.

A.4.9 Gwynne and Rosenbaum

Based on the work of Fruin, Pauls, and Predtechenskii and Milinskii, Gwynne and Rosenbaum (2008) proposed calculating stair movement speeds for densities between 0.54 to 3.8 persons/m^2 (they did not specify what area should be used to calculate the density or what standard conditions would be) by:

$$s = k - a \cdot k \cdot D \tag{A.21}$$

where:

s= speed along the path of travel (m/s)
k= 1.00 (m/s) for 19.0 cm riser, 25.4 cm tread
= 1.08 (m/s) for 17.8 cm riser, 27.9 cm tread
= 1.16 (m/s) for 16.5 cm riser, 30.5 cm tread
= 1.23 (m/s) for 16.5 cm riser, 33.0 cm tread
a= 0.266 (m^2/person)
D= density (persons/m^2)

For situations where the density was less than 0.54 persons/m^2, the speed was assumed to be the speed at 0.54 persons/m^2. The authors also stated that the specific flow rate could be calculated by:

$$f = s \cdot D \tag{A.22}$$

where:

f= specific flow (persons/m-s)
s= speed (m/s)
D= density (persons/m^2)

Based on the work of Pauls, Fruin, and Predtechenskii and Milinskii, it was possible to determine how the authors developed this equation. The lower limit on Equation A.21 came directly from the Level of Service concept introduced by Fruin (1971). It was the boundary between Level A and Level B. Level B was where the very first

interactions with other individuals are said to occur. Thus, the free speed was the speed at Level A.

With a 17.8 cm riser height and 27.9 cm tread depth, Equation A.21 is Equation A.4. Thus, the equation relied most heavily on the work of Pauls (1980). The highest density Pauls used in developing his model was approximately 2.5 persons/m^2. The upper bound on Equation A.21 is 3.8 persons/m^2 (where the speed becomes 0). Because fitting a curve to data developed the equation, extreme caution should be used when going beyond the data range in which the data was collected. Nowhere did the authors mention this limitation nor did they mention that the equation loses accuracy above 15 stories (as stated by Pauls (1980)). Also, Equation A.4 was developed using data with densities less than 0.54 persons/m^2. Since Gwynne and Rosenbaum assumed that speeds less than this limit behaved differently than those above the limit, Equation A.21 should have been determined with those values being excluded.

The other way that Equation A.21 differs from Equation A.4 is the introduction of factors for different stair geometries. As mentioned in Section A.1.3, Pauls had a range of stair geometries in his study. While a stair with a riser height of 17.8 cm and tread depth of 27.9 cm was a common stair, it was not the only stair configuration in his study. For proper model development, Equation A.4 should have been recalculated using only a single, common stair dimension. After that, other stair geometries could have been tested to develop the correction factors for the equation.

The development of the k factors appears to have been determined using the suggestion of Pauls (1984) for four rules for adjusting the $(b-\delta)/P$ ratio. As shown in Equation A.18 this ratio is inversely related to density. The authors assumed that the horizontal spacing between people was a constant, so the adjustment factor is applied to the default k value of 1.08 m/s. In the absence of data, other reasonable explanations could result in similar k values.

Ideally, Gwynne and Rosenbaum (2008) would limit the equation to the data range over which it was developed including, the stair geometries, and clearly state that the k factors are not based on data and/or present information for how k factors might be determined for unique stair geometries. If that was the case, then other researchers, like Kratchman (2007) mentioned previously, could apply that equation with an understanding of what it means. Under the current formation, and without guidance on how the k factors should be determined, authors like Kratchman will apply the incorrect k factor (in her case it should have been approximately 1.03 using the method of Pauls (1984)) to their analysis.

A.5 Laboratory Studies

In order to better understand selected variables, some authors have conducted controlled laboratory studies. In these studies, the authors asked the participants to behave in ways such that they could observe specific variables. This often led to

conditions that were beyond what the authors expected would be found in real-world situations.

A.5.1 Frantzich- Laboratory and Field

Frantzich (1994) conducted a study that was divided into two parts. The first part consisted of students on a campus stair. The second part looked at a stair in a theater.

For the first part of the study, students were videotaped ascending and descending a 1.3 m wide stair with 27 cm tread depth and 17 cm riser height under controlled conditions. The stair was open on one side with only a handrail, while the other side consisted of a wall and handrail. The subjects knew each other and were instructed to walk at normal speeds rather than to act as if it was an emergency evacuation. All speed measurements were based on the slope of the stair. Individuals descended at 1.0 m/s. For groups, the movement speed varied from 0.82 to 0.91 m/s with densities ranging from 2.2 to 2.5 persons/m^2. The density was measured by using markers on the stairs, but it was not indicated if the area was effective or total or if the area was calculated along the slope or horizontal.

For the second part of the study (a normal use condition), the general population after a performance in a theater; the subjects were unaware that they were being recorded on videotape and ranged in age from 15 to 70 years. The stair was open on one side with a handrail while the other side had a wall with a handrail. It was 2.25 m wide with a tread depth of 30 cm and a riser height of 15 cm. The movement speed varied from 0.3 to 1.3 m/s, with the speed increasing as the density decreased.

A.5.2 Frantzich- Laboratory

In a study by Frantzich (1996), subjects were students that ranged in age from 20 to 30 years old without any known movement disabilities. The study looked at both ascending and descending movement speeds. Four different stair configurations were used. The first, base case, used a 1.3 m wide stair. The three alternates were: using a 0.9 m wide stair; having two stationary individuals force the flow to move around them, thus increasing the density; and having slower individuals in the stair that were passed. For all configurations, the density was varied from individuals in isolation to large groups. Individuals were recorded on videotapes and the movement speeds were calculated based on the change in shoulder position every 0.25 s. Observations were made along the treads only and the speeds were measured along the slope of the stairs.

The primary stair used in the investigation had a tread depth of 28.0 cm and a riser height of 17.5 cm. The steps were made of brick and the stair was open on one side with a handrail. The other side consisted of a concrete wall and a handrail.

The more narrow stair used in the investigation had a tread depth of 22.5 cm and a riser height of 20.5 cm; this stair had a steeper slope than the wider stair. The steps

were made of steel and the stair was open on one side with a handrail. The other side consisted of a gypsum wall and a handrail.

In the trials without any obstructions, the minimal interpersonal spacing was found to be 0.37 m. While not directly stated, it appears that the author was defining this based on the horizontal distance between people rather than along the slope. For the case where the stair width was reduced, the interpersonal spacing was decreased to 0.25 m. Individuals for the case with obstructions were instructed to be as close to the person ahead of them as was possible. Thus, the interpersonal spacing in that trial could be less than would ever be found in an actual evacuation. The movement of individuals near the walls was the same as individuals that were located elsewhere in the stair.

For descending the 1.3 m wide stair without obstructions, the movement speed varied from 0.27 to 1.09 m/s with a mean speed of 0.69 m/s (standard deviation of 0.15 m/s). For the 0.9 m wide stair, the speed varied from 0 to 2.27 m/s with a mean speed of 0.72 m/s and a standard deviation of 0.27 m/s.

The distribution of speeds on either stair size in either direction was approximately normal in this investigation. When comparing the two stairs, the stair width was not significant in determining the movement speed. The author reported that the speeds only decreased slightly as the interpersonal spacing increased.

Based on the results from the 1.3 m wide stair, 0.9 m wide stair, and the interpersonal spacing for the restricted width case, the author proposed that the speed on stairs was a constant (approximately 0.7 m/s for descending) for interpersonal spacing greater than 0.37 m. For interpersonal spacing greater than 0.25 m and less than 0.37 m, the movement speed would increase linearly from 0 m/s to the steady-state value. Interpersonal spacing less than 0.25 m was considered an impossibility and thus the speed would be 0 m/s.

For passing behavior, individuals moved to the side to overtake the slower individual ahead of them.

A.5.3 Boyce, Shields, and Silcock

Boyce, Shields, and Silcock (1999) had volunteers with and without disabilities from five day centers in the United Kingdom use different egress components. For stairs, occupants first ascended and then descended stairs after a five-minute rest. No information was provided about the number of steps or stair dimensions, but the speed was measured along the slope of the stairs.

Forty-two subjects were able to participate in the stair portion of the experiment. Of these, eight did not have a disability, four needed assistance from another person, and thirty had a disability, but were able to use the stairs without the assistance from another person. The disabled subjects that needed assistance were evenly split between men and women and were all over 75 years old. In the disabled, but not

needing additional assistance group, twenty were men and ten were women with ages from 25 to 85 years old.

The authors noted a few common characteristics about the subjects. First, 94% of the unassisted subjects used the handrails while descending. Second, subjects tended to choose the shortest path while on the stairs, unless they had very little strength in the arm that would be on the handrail side. Third, subjects with locomotion disabilities took up more space descending the stairs than ascending the stairs (this was said to be caused by the ergonomics of stairway movement, but the effect was not quantified).

The eight subjects without disabilities had an average descending speed of 0.70 m/s with a range of speeds from 0.45 to 1.10 m/s. The thirty disabled subjects that were not assisted by another person had a mean speed of 0.33 m/s with a range from 0.11 to 0.70 m/s. Within this group, nineteen subjects did not use a mobility aid and had an average speed of 0.36 m/s and their speeds ranged from 0.13 to 0.70 m/s. Nine subjects used a walking stick and had a mean speed of 0.32 m/s and their speeds were between 0.11 and 0.49 m/s. One subject on crutches and one subject that used a rollator had speeds of 0.22 and 0.16 m/s respectively. For the four assisted subjects, the average speed was 0.13 m/s and the range of speeds was 0.11 to 0.23 m/s.

A.5.4 Wright, Cook, Webber

Wright, Cook, and Webber (2001) conducted a laboratory study in which eighteen subjects walked along a smoke-filled egress path under six different lighting conditions. There were seven men and eleven women that ranged in age from 23 to 63 years old (average age 46 years old).

The subjects walked through artificial smoke that varied in mean optical density from 1.1 to 1.2 m^{-1}. The subjects traveled on a landing, down a flight of stairs, and then through two corridors. No dimensions were provided for the stair or if the speeds were in the horizontal or slope directions. The different lighting conditions were normal lighting, emergency lighting, electroluminescent wayguidance system, miniature incandescent wayguidance system, and two light emitting diode wayguidance systems. The order that occupants proceeded through the different lighting systems was randomized. Under normal and emergency lighting, the average speeds were approximately 0.3 m/s. The other four systems had average speeds that ranged from approximately 0.35 to 0.42 m/s.

A.5.5 Fujiyama and Tyler

Fujiyama and Tyler (2004) had subjects ascend and descend four sets of stairs, with a rest period between flights, inside buildings of University College London. The first stair had 12 steps with a riser height of 18.5 cm and a tread depth of 23.0 cm. The second stair also had 12 steps with 17.5 cm and 25.0 cm riser height and tread depth, respectively. For the third stair, there were 15 steps with a riser height of 15.7 cm and a tread depth of 26.7 cm. Finally, the fourth stair had 9 steps and their dimensions were 15.2 cm by 33.2 cm for the riser height and tread depth, respectively.

There were 18 subjects, 6 men and 12 women, between 60 to 81 years old and an additional 15 subjects, 7 men, 8 women, between the ages of 25 to 60 years old. On each set of stairs, the subjects were asked to ascend and descend the stairs twice. For descending the first flight of stairs, occupants were asked to move at their normal pace. For the second set, the occupants were asked to move at their fast pace.

In all cases, the speeds are given in terms of the speed along the slope. The younger group had average, normal speeds that ranged from 0.76 to 0.96 m/s and the older group had comparable speeds of 0.60 to 0.88 m/s. The speeds increased as the slope of the stairs decreased. With the exception of one descending stair, the differences between the two groups were not significant for the normal speeds.

For fast descending of the stairs, the young group had average speeds from 1.12 to 1.30 m/s and the older group averaged 0.80 to 1.11 m/s. For the set of stairs with the least amount of slope, the difference between the two groups was significant at the 0.05 level. For the set of stairs with the greatest slope, the difference was significant at the 0.001 level. For the two intermediary stairs, the difference was significant at the 0.01 level. All of their calculated speeds are shown in Table A.3.

Table A.3: Fujiyama and Tyler's Movement Speeds

Speed Type	Stair Dimension (cm)	Old	Young
Normal	18.5 by 23.0	0.60	0.76
	17.5 by 25.0	0.71	0.79
	15.7 by 26.7	0.74	0.86
	15.2 by 33.2	0.88	0.96
Fast	18.5 by 23.0	0.80	1.12
	17.5 by 25.0	0.85	1.12
	15.7 by 26.7	0.97	1.25
	15.2 by 33.2	1.11	1.30

The authors also collected a limited amount of physiological data on the participants. The height and weight of the subjects were not found to have a high correlation with movement speed on stairs.

A.6 Subsets of Data Studies

The final group is studies that have used subsets of the data used in this research. Many of the specific details are not provided here since they are presented in greater detail when discussing this current study. Instead, the focus will be on some of the methodological differences between the studies and current work.

A.6.1 Blair

Blair (2010) used eight of the stairs in four of the buildings (4a, 4b, 5a, 5b, 7-1, 7-3, 7-7, and 8S) to perform bivariate correlations with the data. Observations were made between adjacent cameras, typically two floors apart, with the travel distance determined using a travel distance that assumed occupants traveled down the middle of the stair with the distance on a landing being twice the stair width. Also, transfer corridors were included and occupants were assumed to have the same travel speed as when on the stairs. Density was calculated over the entire area between floors including the entire landing area. This assumed that the density was uniform over all floors and that the entire area of the stairs and landings was used uniformly. These assumptions led to reported density values that were at least 110% of the values that would have been produced using the methods of previous researchers.

Typically, occupants that started early, or started late, had faster movement speeds than those in the middle. There was a corresponding density pattern that could explain these results. The slope of the density versus speed calculation was similar to that of Equation A.21, but that curve was found to be an upper bound on the data. In making comparisons to Equation A.21, seven of the eight stairs had dimensions with k values that were listed. The final stair, from Stair 8S, the author used 1.08 because of the same 18 cm riser height. However, due to the smaller treads, the k value should have been 1.03 using Pauls's estimates.

A.6.2 Peacock, Hoskins, and Kuligowski

Peacock, Hoskins, and Kuligowski (2011) used a multiple regression model to predict movement speeds down stairs in nine stairwells in four different buildings (4a, 4b, 5a, 5b, 7-1, 7-3, 7-7, 7-12, and 8S). The main independent variables were stair, gender, carrying objects, exit lane, handrail use, pre-evacuation time, density, and travel distance. Travel distance was determined using the Predtechenskii and Milinskii method. Speeds were calculated from one camera to the next one, typically two floors below it in the building. Transfer corridors were included in the travel distance in some instances. Density was calculated by accounting for the entire landing area and the number of people within that area and it was assumed that this density was constant from the upper camera to the lower one.

Of these variables, only handrail use, travel distance, and pre-evacuation time were not significant. Due to the similarities of the buildings, the finding that stair was significant is likely caused by unaccounted variables and is not a real effect. The model accounted for 21% of the variation within the data. Interaction variables were examined and effects involving density and the stair were significant.

Appendix B: Data

Appendix B contains the data used for all of the analysis. The different columns can be interpreted as:

St: 0=Building 6, Stair 5
1=Building 6, Stair 5a
2 or 3=Building 6, Stair 6
4 or 5=Building 6, Stair 6a
6=Building 8, Stair S
7=Building 8, Stair N
8=Building 4, Stair A
9=Building 4, Stair B
10=Building 5, Stair A
11=Building 5, Stair B
12=Building 7, Stair 3

ID: The numbers before the decimal point are the unique personal identification number for each occupant in the given stair. The numbers after the decimal points are the same for all occupants between a given set of cameras in each building.

Gen: 0=Male
1=Female

Follow Gend: .=First person in flow unit
0=Same as first person in flow unit
1=Different than first person in flow unit

Carry: 0=Not carrying anything
1=Carrying item

Large: 0=Not large
1=Large

Trds: .=More than three open treads to previous occupant
1, 2, or 3=Number of open treads to previous occupant

Grp: The unique personal identification number for the first person in the flow unit (without the camera set indication).

Flow Type: 0=Uniform flow
1=Lane flow

Den: The effective density (persons/m^2).

Lane: 0=Middle
1=Outer Lane
2=Inner Lane

Dist: The effective travel distance while in the stair (m).

Pre-Obs: The pre-observation time (s).

Speed: The effective speed (m/s).

Norm Time: The effective normalized descent time (s/m)

First Per Spd: The effective speed of the first person in the flow unit (m/s).

1^{st} Per Time: The effective normalized time of the first person in the flow unit (s/m).

1st Per: 0=Not a first person in flow unit
1=First person in flow unit

1st Per Type: For all buildings except Building 6, the classification of the first person in the flow units.
0=Free-flow
1=Congestion
2=Pass
3=Passed
4=Allowed enter

1st Follow: For all buildings except Buildings 6 and 7:
0=Not the first follower in a flow unit
1=First follower in a flow unit

Prev Grp Time: For the first persons in flow units, the effective normalized descent time of the previous flow unit (s/m).

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
0	4.1	0	.	0	0	3	4	0	0.37	2	2.29
0	5.1	1	.	1	0	.	5	0	0.75	1	2.29
0	6.1	1	.	1	0	3	6	0	0.37	1	2.29
0	7.1	0	1	0	0	.	6	0	0.37	2	2.29
0	8.1	1	.	0	0	1	8	0	0.75	1	2.29
0	9.1	1	.	0	0	2	9	0	0.75	1	2.29
0	10.1	1	.	0	0	1	10	0	0.75	1	2.29
0	13.1	0	.	1	0	3	13	0	0.37	2	2.29
0	16.1	0	.	1	0	3	16	0	0.75	2	2.29
0	17.1	0	.	0	0	3	17	0	0.37	2	2.29
0	18.1	1	.	1	0	3	18	0	0.37	2	140.36
0	19.1	1	0	1	0	2	18	0	0.75	2	140.36
0	20.1	0	1	0	0	2	18	0	1.12	2	140.36
0	21.1	0	0	0	0	1	18	0	1.12	1	140.36
0	22.1	0	0	0	0	1	18	0	1.12	2	140.36
0	24.1	0	.	0	0	.	24	0	0.37	1	140.36
0	25.1	0	0	0	0	1	24	0	0.75	2	140.36
0	26.1	0	0	0	0	2	24	0	1.12	1	140.36
0	27.1	0	0	1	0	1	24	0	1.50	0	140.36
0	28.1	0	0	0	0	2	24	0	1.50	2	140.36
0	29.1	0	0	0	0	2	24	0	1.50	1	140.36
0	30.1	1	.	1	0	2	30	0	0.75	2	36.05
0	31.1	1	.	1	0	3	31	0	0.37	2	36.05
0	32.1	0	1	0	0	1	31	0	1.12	1	36.05
0	33.1	1	.	0	0	3	33	0	0.37	2	140.36
0	34.1	0	1	0	0	1	33	0	0.75	1	140.36
0	35.1	0	0	0	0	1	33	0	1.12	0	140.36
0	36.1	0	0	0	0	.	33	0	1.50	2	140.36
0	37.1	1	.	1	0	3	37	0	1.12	0	36.05
0	38.1	1	0	1	0	2	37	0	1.12	0	36.05
0	39.1	1	.	1	0	.	39	0	0.37	2	36.05
0	40.1	1	.	1	0	1	40	0	0.75	1	36.05
0	41.1	1	.	1	0	3	41	0	0.37	2	140.36
0	42.1	1	.	1	0	3	42	0	0.75	0	140.36
0	43.1	1	.	0	0	3	43	0	0.75	0	140.36
0	44.1	0	1	0	0	2	43	0	0.75	2	140.36
0	45.1	1	1	1	0	1	43	0	1.12	0	140.36
0	46.1	1	.	0	0	3	46	0	0.37	2	140.36
0	47.1	1	0	1	0	1	48	0	0.37	1	140.36
0	48.1	1	.	0	0	1	48	0	0.75	2	140.36
0	49.1	0	1	0	0	2	48	0	1.12	2	140.36
0	50.1	1	1	0	0	1	48	0	1.50	1	140.36
0	51.1	1	0	1	0	.	48	0	1.12	2	140.36
0	52.1	0	.	0	0	2	52	0	1.12	0	140.36
0	53.1	1	.	0	0	.	53	0	1.12	2	140.36
0	54.1	1	.	0	0	2	54	0	0.75	2	140.36
0	55.1	0	1	0	0	2	54	0	1.50	1	140.36
0	56.1	1	1	1	0	1	54	0	1.50	1	140.36
0	57.1	1	0	1	0	1	54	0	0.37	2	140.36
0	58.1	0	.	0	0	3	58	0	1.12	2	140.36

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
0	4.1	25.15	0.78	1.28	0.78	1.28	1			
0	5.1	26.96	0.70	1.43	0.70	1.43	1			
0	6.1	34.56	0.73	1.37	0.73	1.37	1			
0	7.1	39.07	0.74	1.34	0.73	1.37	0			
0	8.1	39.87	0.72	1.40	0.72	1.40	1			
0	9.1	41.17	0.70	1.42	0.70	1.42	1			
0	10.1	42.61	0.69	1.45	0.69	1.45	1			
0	13.1	48.01	0.66	1.51	0.66	1.51	1			
0	16.1	111.24	1.14	0.87	1.14	0.87	1			
0	17.1	86.15	0.84	1.19	0.84	1.19	1			
0	18.1	67.97	0.62	1.61	0.62	1.61	1			
0	19.1	73.8	0.61	1.63	0.62	1.61	0			
0	20.1	76.01	0.61	1.63	0.62	1.61	0			
0	21.1	79.14	0.62	1.61	0.62	1.61	0			
0	22.1	80.78	0.63	1.60	0.62	1.61	0			
0	24.1	84.15	0.58	1.73	0.58	1.73	1			
0	25.1	88.65	0.58	1.72	0.58	1.73	0			
0	26.1	85.82	0.58	1.73	0.58	1.73	0			
0	27.1	90.79	0.59	1.70	0.58	1.73	0			
0	28.1	89.89	0.58	1.73	0.58	1.73	0			
0	29.1	87.52	0.58	1.74	0.58	1.73	0			
0	30.1	185.52	0.56	1.78	0.56	1.78	1			
0	31.1	183.78	0.55	1.83	0.55	1.83	1			
0	32.1	187.32	0.56	1.80	0.55	1.83	0			
0	33.1	98.6	0.57	1.76	0.57	1.76	1			
0	34.1	96.39	0.57	1.74	0.57	1.76	0			
0	35.1	99.9	0.57	1.75	0.57	1.76	0			
0	36.1	102.73	0.57	1.76	0.57	1.76	0			
0	37.1	221.15	0.56	1.78	0.56	1.78	1			
0	38.1	222.72	0.56	1.79	0.56	1.78	0			
0	39.1	231.69	0.59	1.68	0.59	1.68	1			
0	40.1	233.03	0.58	1.71	0.58	1.71	1			
0	41.1	168	0.69	1.46	0.69	1.46	1			
0	42.1	169.97	0.59	1.68	0.59	1.68	1			
0	43.1	174.14	0.60	1.67	0.60	1.67	1			
0	44.1	176.34	0.60	1.67	0.60	1.67	0			
0	45.1	179.84	0.60	1.68	0.60	1.67	0			
0	46.1	183.25	0.60	1.68	0.60	1.68	1			
0	47.1	186.28	0.62	1.63	0.62	1.61	0			
0	48.1	188.45	0.62	1.61	0.62	1.61	1			
0	49.1	190.39	0.62	1.62	0.62	1.61	0			
0	50.1	192.12	0.62	1.62	0.62	1.61	0			
0	51.1	194.26	0.61	1.63	0.62	1.61	0			
0	52.1	196.83	0.61	1.65	0.61	1.65	1			
0	53.1	184.78	0.56	1.78	0.56	1.78	1			
0	54.1	252.68	0.70	1.43	0.70	1.43	1			
0	55.1	250.71	0.68	1.47	0.70	1.43	0			
0	56.1	254.19	0.69	1.46	0.70	1.43	0			
0	57.1	255.89	0.69	1.45	0.70	1.43	0			
0	58.1	220.65	0.55	1.82	0.55	1.82	1			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
0	59.1	1	.	1	0	3	59	0	0.37	2	140.36
0	60.1	0	.	0	0	2	60	0	1.50	2	140.36
0	61.1	0	.	0	0	2	61	0	1.50	2	140.36
0	62.1	1	1	1	0	2	61	0	1.50	2	140.36
0	63.1	1	0	1	0	1	61	0	1.50	1	140.36
0	64.1	0	1	0	0	1	61	0	1.87	2	230.38
0	65.1	1	1	1	0	1	61	0	1.87	1	230.38
0	66.1	0	1	0	0	1	61	0	2.25	2	230.38
0	67.1	0	0	1	0	2	61	0	2.25	0	140.36
0	68.1	0	0	0	0	2	61	0	1.87	0	230.38
0	69.1	1	1	1	0	1	61	0	1.50	2	140.36
0	70.1	1	0	1	0	1	61	0	1.50	2	140.36
0	71.1	1	0	0	0	1	61	0	1.50	1	140.36
0	72.1	0	.	1	0	.	72	0	1.50	2	140.36
0	73.1	0	.	0	0	3	73	0	0.37	2	140.36
0	74.1	1	.	0	0	3	74	0	0.75	2	36.05
0	75.1	1	0	1	0	2	76	0	0.75	0	140.36
0	76.1	1	.	0	0	3	76	0	0.37	1	140.36
0	77.1	1	.	1	0	3	77	0	1.12	2	140.36
0	78.1	0	1	0	0	1	81	0	1.12	1	309.15
0	79.1	1	1	1	0	2	81	0	0.75	0	309.15
0	80.1	0	0	1	0	2	81	0	1.12	2	309.15
0	81.1	0	.	0	0	3	81	0	0.37	1	309.15
0	82.1	1	.	1	0	2	82	0	0.75	2	309.15
0	83.1	1	0	1	0	2	84	0	0.75	2	309.15
0	84.1	1	.	0	0	.	84	0	0.75	2	309.15
0	85.1	0	1	0	0	1	84	0	1.12	1	309.15
0	86.1	0	.	1	0	2	86	0	1.12	2	230.38
0	87.1	1	1	1	0	2	86	0	1.12	2	390.96
0	88.1	0	.	0	1	1	88	0	1.12	1	390.96
0	89.1	1	0	1	0	1	88	0	1.50	2	390.96
0	90.1	1	1	1	0	2	88	0	1.12	0	390.96
0	91.1	0	1	0	0	1	88	0	1.87	1	390.96
0	92.1	0	.	1	0	2	92	0	1.50	1	140.36
0	93.1	1	.	1	0	2	93	0	1.50	1	309.15
0	94.1	1	.	1	0	3	94	0	0.37	2	390.96
0	95.1	0	.	0	0	2	95	0	0.75	2	390.96
0	96.1	1	.	1	1	2	96	0	1.50	2	309.15
0	97.1	1	0	1	0	2	98	0	1.12	2	309.15
0	98.1	1	.	0	1	.	98	0	1.50	2	309.15
0	99.1	0	.	0	0	.	99	0	0.37	0	36.05
0	100.1	1	1	0	0	.	99	0	0.75	1	36.05
0	101.1	1	.	1	0	3	101	0	1.12	1	2.29
0	102.1	1	.	0	0	1	102	0	0.75	2	36.05
0	103.1	0	1	1	0	.	102	0	0.37	1	36.05
0	104.1	0	.	0	0	3	104	0	0.37	1	2.29
0	105.1	0	.	0	0	3	105	0	0.37	2	140.36
0	106.1	0	0	0	0	2	105	0	0.75	1	140.36
0	107.1	0	0	0	0	1	105	0	1.12	1	140.36
0	108.1	0	.	0	0	.	108	0	1.12	0	140.36

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
0	59.1	249.51	0.60	1.66	0.60	1.66	1			
0	60.1	257.49	0.64	1.56	0.64	1.56	1			
0	61.1	259.36	0.64	1.57	0.64	1.57	1			
0	62.1	260.86	0.64	1.57	0.64	1.57	0			
0	63.1	261.83	0.64	1.57	0.64	1.57	0			
0	64.1	107.57	0.64	1.57	0.64	1.57	0			
0	65.1	110.57	0.63	1.59	0.64	1.57	0			
0	66.1	111.74	0.62	1.60	0.64	1.57	0			
0	67.1	267.76	0.63	1.60	0.64	1.57	0			
0	68.1	129.76	0.62	1.60	0.64	1.57	0			
0	69.1	274.34	0.62	1.61	0.64	1.57	0			
0	70.1	276.24	0.62	1.61	0.64	1.57	0			
0	71.1	275.41	0.62	1.61	0.64	1.57	0			
0	72.1	270.2	0.62	1.62	0.62	1.62	1			
0	73.1	287.99	0.61	1.65	0.61	1.65	1			
0	74.1	456.39	0.73	1.37	0.73	1.37	1			
0	75.1	383.01	0.60	1.67	0.60	1.66	0			
0	76.1	381.21	0.60	1.66	0.60	1.66	1			
0	77.1	393.46	0.59	1.71	0.59	1.71	1			
0	78.1	148.92	0.62	1.61	0.62	1.61	0			
0	79.1	147.41	0.62	1.61	0.62	1.61	0			
0	80.1	151.02	0.62	1.62	0.62	1.61	0			
0	81.1	145.71	0.62	1.61	0.62	1.61	1			
0	82.1	143.64	0.63	1.60	0.63	1.60	1			
0	83.1	155.49	0.64	1.56	0.64	1.57	0			
0	84.1	157.26	0.64	1.57	0.64	1.57	1			
0	85.1	159.73	0.64	1.57	0.64	1.57	0			
0	86.1	281.01	0.70	1.43	0.70	1.43	1			
0	87.1	125.43	0.70	1.42	0.70	1.43	0			
0	88.1	128.27	0.67	1.49	0.67	1.49	1			
0	89.1	131.9	0.66	1.50	0.67	1.49	0			
0	90.1	130.53	0.67	1.49	0.67	1.49	0			
0	91.1	132.77	0.67	1.50	0.67	1.49	0			
0	92.1	463.33	0.67	1.50	0.67	1.50	1			
0	93.1	169.67	0.54	1.86	0.54	1.86	1			
0	94.1	162.27	0.81	1.23	0.81	1.23	1			
0	95.1	164.97	0.64	1.56	0.64	1.56	1			
0	96.1	174.97	0.37	2.74	0.37	2.74	1			
0	97.1	172.94	0.35	2.84	0.34	2.90	0			
0	98.1	168.1	0.34	2.90	0.34	2.90	1			
0	99.1	110.61	0.79	1.27	0.79	1.27	1			
0	100.1	112.54	0.78	1.28	0.79	1.27	0			
0	101.1	120.55	0.80	1.25	0.80	1.25	1			
0	102.1	119.82	0.78	1.28	0.78	1.28	1			
0	103.1	118.75	0.75	1.33	0.78	1.28	0			
0	104.1	127.79	0.75	1.34	0.75	1.34	1			
0	105.1	61.79	0.80	1.25	0.80	1.25	1			
0	106.1	64.13	0.80	1.25	0.80	1.25	0			
0	107.1	63.29	0.80	1.26	0.80	1.25	0			
0	108.1	70.97	0.80	1.25	0.80	1.25	1			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
0	109.1	1	.	0	0	.	109	0	1.12	2	140.36
0	110.1	0	.	0	0	.	110	0	0.75	2	140.36
0	18.2	1	.	1	0	.	18	0	1.12	2	61.59
0	19.2	1	.	1	0	2	19	0	1.12	2	61.59
0	20.2	0	.	0	0	.	20	0	1.12	0	61.59
0	21.2	0	.	0	0	1	21	0	0.75	0	61.59
0	22.2	0	0	0	0	2	21	0	0.75	2	61.59
0	24.2	0	.	0	0	3	24	1	0.75	0	61.59
0	25.2	0	0	0	0	1	24	1	1.50	2	61.59
0	26.2	0	.	0	0	2	26	1	0.75	1	61.59
0	27.2	0	0	1	0	1	24	1	1.87	2	61.59
0	28.2	0	0	0	0	1	24	1	1.50	0	61.59
0	29.2	0	0	0	0	2	26	1	1.12	1	61.59
0	33.2	1	.	0	0	.	33	0	0.75	2	61.59
0	34.2	0	1	0	0	1	33	0	0.37	1	61.59
0	35.2	0	0	0	0	1	33	0	1.12	0	61.59
0	36.2	0	0	0	0	.	33	0	1.12	2	61.59
0	41.2	1	.	1	0	3	41	0	0.75	0	61.59
0	42.2	1	.	1	0	2	42	0	0.75	0	61.59
0	43.2	1	.	0	0	3	43	0	0.75	2	61.59
0	44.2	0	1	0	0	2	43	0	0.75	0	61.59
0	45.2	1	1	1	0	1	43	0	1.12	1	61.59
0	46.2	1	.	0	0	2	46	0	1.50	2	61.59
0	47.2	1	.	1	0	2	47	0	1.50	0	61.59
0	48.2	1	0	0	0	1	47	0	1.50	0	61.59
0	49.2	0	1	0	0	2	47	0	1.12	2	61.59
0	50.2	1	1	0	0	1	47	0	1.12	1	61.59
0	51.2	1	0	1	0	2	47	0	1.12	0	61.59
0	52.2	0	1	0	0	2	47	0	1.12	2	61.59
0	53.2	1	.	0	0	2	53	0	1.50	2	61.59
0	54.2	1	1	0	0	2	59	0	0.75	2	61.59
0	55.2	0	1	0	0	2	59	0	1.50	1	61.59
0	56.2	1	0	1	0	1	59	0	1.50	1	61.59
0	57.2	1	0	1	0	1	59	0	0.37	2	61.59
0	58.2	0	.	0	0	3	58	0	1.12	2	61.59
0	59.2	1	.	1	0	3	59	0	0.37	2	61.59
0	60.2	0	1	0	0	2	59	0	1.50	1	61.59
0	61.2	0	0	0	0	2	59	0	1.50	2	61.59
0	62.2	1	1	1	0	2	59	0	1.50	2	61.59
0	63.2	1	0	1	0	1	59	0	1.50	1	61.59
0	64.2	0	1	0	0	1	59	0	1.87	2	151.61
0	65.2	1	1	1	0	1	59	0	1.50	1	151.61
0	66.2	0	1	0	0	1	59	0	1.87	2	151.61
0	67.2	0	0	1	0	2	59	0	1.50	2	61.59
0	68.2	0	0	0	0	2	59	0	1.12	2	151.61
0	69.2	1	1	1	0	1	59	0	1.12	2	61.59
0	70.2	1	0	1	0	1	59	0	1.50	2	61.59
0	71.2	1	0	0	0	1	59	0	1.12	1	61.59
0	72.2	0	.	1	0	.	72	0	1.50	2	61.59
0	73.2	0	.	0	0	3	73	0	0.37	2	61.59

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
0	109.1	66.16	0.77	1.30	0.77	1.30	1			
0	110.1	72.37	0.77	1.29	0.77	1.29	1			
0	18.2	67.97	0.75	1.34	0.75	1.34	1			
0	19.2	73.8	0.77	1.29	0.77	1.29	1			
0	20.2	76.01	0.78	1.29	0.78	1.29	1			
0	21.2	79.14	0.78	1.29	0.78	1.29	1			
0	22.2	80.78	0.78	1.28	0.78	1.29	0			
0	24.2	84.15	0.66	1.52	0.66	1.52	1			
0	25.2	88.65	0.67	1.50	0.66	1.52	0			
0	26.2	85.82	0.64	1.57	0.64	1.57	1			
0	27.2	90.79	0.66	1.50	0.66	1.52	0			
0	28.2	89.89	0.65	1.53	0.66	1.52	0			
0	29.2	87.52	0.63	1.59	0.64	1.57	0			
0	33.2	98.6	0.63	1.58	0.63	1.58	1			
0	34.2	96.39	0.61	1.63	0.63	1.58	0			
0	35.2	99.9	0.62	1.61	0.63	1.58	0			
0	36.2	102.73	0.62	1.61	0.63	1.58	0			
0	41.2	168	0.67	1.50	0.69	1.46	1			
0	42.2	169.97	0.65	1.55	0.65	1.55	1			
0	43.2	174.14	0.64	1.56	0.64	1.56	1			
0	44.2	176.34	0.64	1.56	0.64	1.56	0			
0	45.2	179.84	0.65	1.53	0.64	1.56	0			
0	46.2	183.25	0.63	1.58	0.63	1.58	1			
0	47.2	186.28	0.59	1.69	0.59	1.69	1			
0	48.2	188.45	0.60	1.66	0.59	1.69	0			
0	49.2	190.39	0.60	1.67	0.59	1.69	0			
0	50.2	192.12	0.60	1.67	0.59	1.69	0			
0	51.2	194.26	0.60	1.67	0.59	1.69	0			
0	52.2	196.83	0.60	1.67	0.59	1.69	0			
0	53.2	184.78	0.53	1.88	0.53	1.88	1			
0	54.2	252.68	0.65	1.54	0.65	1.54	0			
0	55.2	250.71	0.65	1.54	0.65	1.54	0			
0	56.2	254.19	0.65	1.54	0.65	1.54	0			
0	57.2	255.89	0.65	1.54	0.65	1.54	0			
0	58.2	220.65	0.60	1.66	0.60	1.66	1			
0	59.2	249.51	0.65	1.54	0.65	1.54	1			
0	60.2	257.49	0.65	1.54	0.65	1.54	0			
0	61.2	259.36	0.65	1.55	0.65	1.54	0			
0	62.2	260.86	0.65	1.55	0.65	1.54	0			
0	63.2	261.83	0.65	1.54	0.65	1.54	0			
0	64.2	107.57	0.64	1.56	0.65	1.54	0			
0	65.2	110.57	0.65	1.54	0.65	1.54	0			
0	66.2	111.74	0.65	1.54	0.65	1.54	0			
0	67.2	267.76	0.65	1.54	0.65	1.54	0			
0	68.2	129.76	0.66	1.50	0.65	1.54	0			
0	69.2	274.34	0.67	1.50	0.65	1.54	0			
0	70.2	276.24	0.67	1.50	0.65	1.54	0			
0	71.2	275.41	0.66	1.51	0.65	1.54	0			
0	72.2	270.2	0.61	1.63	0.61	1.63	1			
0	73.2	287.99	0.66	1.51	0.66	1.51	1			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
0	75.2	1	0	1	0	2	76	0	0.75	0	61.59
0	76.2	1	.	0	0	3	76	0	0.37	1	61.59
0	77.2	1	.	1	0	3	77	0	0.37	1	61.59
0	78.2	0	1	0	0	1	81	0	1.12	1	230.38
0	79.2	1	1	1	0	2	81	0	0.75	2	230.38
0	80.2	0	0	1	0	2	81	0	1.50	2	230.38
0	81.2	0	.	0	0	3	81	0	0.37	1	230.38
0	82.2	1	.	1	0	2	82	0	1.50	0	230.38
0	83.2	1	0	1	0	2	84	0	1.50	2	230.38
0	84.2	1	.	0	0	.	84	0	1.50	2	230.38
0	85.2	0	1	0	0	1	84	0	1.50	1	230.38
0	86.2	0	1	1	0	2	84	0	1.50	0	151.61
0	87.2	1	1	1	0	2	84	0	1.50	0	312.19
0	88.2	0	1	0	1	1	84	0	1.50	1	312.19
0	89.2	1	0	1	0	1	84	0	0.75	2	312.19
0	90.2	1	1	1	0	.	84	0	1.12	0	312.19
0	91.2	0	1	0	0	1	84	0	1.50	1	312.19
0	92.2	0	0	1	0	2	84	0	1.12	1	61.59
0	93.2	1	0	1	0	1	84	0	1.50	1	230.38
0	94.2	1	.	1	0	3	94	0	0.37	2	312.19
0	95.2	0	.	0	0	2	95	0	0.75	2	312.19
0	96.2	1	0	1	1	1	84	0	1.87	2	230.38
0	97.2	1	0	1	0	2	84	0	1.50	2	230.38
0	98.2	1	1	0	1	2	84	0	1.50	2	230.38
0	105.2	0	.	0	0	3	105	0	0.37	2	61.59
0	106.2	0	0	0	0	1	105	0	1.12	0	61.59
0	107.2	0	0	0	0	1	105	0	0.75	1	61.59
0	108.2	0	.	0	0	3	108	0	0.75	2	61.59
0	109.2	1	1	0	0	.	105	0	1.12	2	61.59
0	110.2	0	.	0	0	2	110	0	0.75	0	61.59
0	78.4	0	1	0	0	1	81	0	1.50	1	47.30
0	79.4	1	1	1	0	2	81	0	1.12	2	47.30
0	80.4	0	.	1	0	2	80	0	1.50	2	47.30
0	81.4	0	.	0	0	2	81	0	0.75	1	47.30
0	82.4	1	.	1	0	1	82	0	0.37	1	47.30
0	83.4	1	0	1	0	1	84	0	1.12	1	47.30
0	84.4	1	.	0	0	.	84	0	1.12	0	47.30
0	85.4	0	1	0	0	2	84	0	0.75	0	47.30
0	87.4	1	.	1	0	3	87	0	0.37	2	129.11
0	88.4	0	.	0	1	3	88	0	0.75	2	129.11
0	89.4	1	0	1	0	2	88	0	1.12	2	129.11
0	90.4	1	1	1	0	.	88	0	0.75	2	129.11
0	91.4	0	1	0	0	1	88	0	1.12	1	129.11
0	93.4	1	0	1	0	1	98	0	0.75	1	47.30
0	94.4	1	.	1	0	3	94	0	0.37	2	47.30
0	95.4	0	1	0	0	.	94	0	0.75	2	47.30
0	96.4	1	0	1	1	2	98	0	1.12	2	47.30
0	97.4	1	0	1	0	.	98	0	1.12	2	47.30
0	98.4	1	.	0	1	.	98	0	0.37	0	47.30
1	5.1	1	.	1	0	3	5	0	0.37	0	81.21

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
0	75.2	383.01	0.63	1.59	0.62	1.61	0			
0	76.2	381.21	0.62	1.61	0.62	1.61	1			
0	77.2	393.46	0.65	1.53	0.65	1.53	1			
0	78.2	148.92	0.66	1.52	0.66	1.52	0			
0	79.2	147.41	0.66	1.52	0.66	1.52	0			
0	80.2	151.02	0.65	1.53	0.66	1.52	0			
0	81.2	145.71	0.66	1.52	0.66	1.52	1			
0	82.2	143.64	0.65	1.55	0.65	1.55	1			
0	83.2	155.49	0.63	1.59	0.63	1.59	0			
0	84.2	157.26	0.63	1.59	0.63	1.59	1			
0	85.2	159.73	0.63	1.59	0.63	1.59	0			
0	86.2	281.01	0.61	1.63	0.63	1.59	0			
0	87.2	125.43	0.61	1.63	0.63	1.59	0			
0	88.2	128.27	0.61	1.63	0.63	1.59	0			
0	89.2	131.9	0.62	1.62	0.63	1.59	0			
0	90.2	130.53	0.62	1.62	0.63	1.59	0			
0	91.2	132.77	0.62	1.62	0.63	1.59	0			
0	92.2	463.33	0.61	1.64	0.63	1.59	0			
0	93.2	169.67	0.62	1.60	0.63	1.59	0			
0	94.2	162.27	0.55	1.83	0.55	1.83	1			
0	95.2	164.97	0.64	1.55	0.64	1.55	1			
0	96.2	174.97	0.62	1.61	0.63	1.59	0			
0	97.2	172.94	0.62	1.62	0.63	1.59	0			
0	98.2	168.1	0.62	1.60	0.63	1.59	0			
0	105.2	61.79	0.88	1.13	0.88	1.13	1			
0	106.2	64.13	0.89	1.12	0.88	1.13	0			
0	107.2	63.29	0.87	1.15	0.88	1.13	0			
0	108.2	70.97	0.92	1.09	0.92	1.09	1			
0	109.2	66.16	0.89	1.13	0.88	1.13	0			
0	110.2	72.37	0.92	1.09	0.92	1.09	1			
0	78.4	148.92	0.59	1.71	0.59	1.70	0			
0	79.4	147.41	0.59	1.70	0.59	1.70	0			
0	80.4	151.02	0.58	1.73	0.58	1.73	1			
0	81.4	145.71	0.59	1.70	0.59	1.70	1			
0	82.4	143.64	0.53	1.88	0.53	1.88	1			
0	83.4	155.49	0.54	1.85	0.57	1.75	0			
0	84.4	157.26	0.57	1.75	0.57	1.75	1			
0	85.4	159.73	0.56	1.77	0.57	1.75	0			
0	87.4	125.43	0.92	1.08	0.92	1.08	1			
0	88.4	128.27	0.47	2.14	0.47	2.14	1			
0	89.4	131.9	0.87	1.15	0.47	2.14	0			
0	90.4	130.53	0.87	1.15	0.47	2.14	0			
0	91.4	132.77	0.87	1.15	0.47	2.14	0			
0	93.4	169.67	0.59	1.69	0.59	1.70	0			
0	94.4	162.27	0.66	1.51	0.66	1.51	1			
0	95.4	164.97	0.66	1.50	0.66	1.51	0			
0	96.4	174.97	0.61	1.64	0.59	1.70	0			
0	97.4	172.94	0.59	1.70	0.59	1.70	0			
0	98.4	168.1	0.59	1.70	0.59	1.70	1			
1	5.1	35.81	0.84	1.19	0.84	1.19	1			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
1	6.1	1	.	1	0	3	6	0	0.75	1	81.21
1	7.1	1	.	0	0	.	7	0	0.75	2	81.21
1	8.1	1	.	1	0	1	8	0	1.50	2	81.21
1	9.1	1	0	0	0	1	7	0	1.12	1	81.21
1	10.1	1	0	1	0	2	7	0	1.50	1	81.21
1	11.1	0	1	0	0	1	7	0	1.87	1	81.21
1	12.1	1	1	1	0	.	7	0	1.50	1	81.21
1	13.1	1	0	1	0	1	7	0	1.50	0	81.21
1	14.1	1	0	1	0	2	7	0	1.50	1	81.21
1	15.1	1	0	0	0	2	7	0	1.50	1	81.21
1	16.1	0	1	1	0	2	7	0	1.87	1	81.21
1	17.1	1	1	0	1	2	7	0	1.87	0	81.21
1	18.1	0	1	0	0	2	7	0	1.87	2	81.21
1	19.1	1	1	1	0	1	7	0	1.87	0	81.21
1	20.1	1	.	0	0	.	20	0	0.75	2	81.21
1	22.1	1	.	1	0	2	22	0	1.12	2	81.21
1	23.1	1	0	0	0	.	22	0	0.75	2	81.21
1	24.1	0	1	1	0	1	22	0	1.12	1	81.21
1	25.1	1	1	1	0	2	22	0	1.12	0	81.21
1	30.1	0	.	1	1	3	30	0	0.37	2	81.21
1	31.1	1	1	1	0	2	30	0	0.75	0	81.21
1	32.1	0	1	0	0	2	30	0	1.12	2	81.21
1	33.1	0	.	0	0	1	33	0	1.12	0	81.21
1	34.1	1	.	0	0	2	34	0	1.12	2	81.21
1	35.1	1	.	0	0	.	35	0	1.12	2	81.21
1	36.1	0	.	0	0	3	36	0	0.37	2	81.21
1	37.1	0	0	0	0	2	36	0	0.75	0	81.21
1	38.1	1	.	0	0	3	38	0	0.37	1	81.21
1	39.1	1	.	1	0	.	39	0	0.75	2	81.21
1	40.1	1	.	0	0	3	40	0	0.37	2	81.21
1	41.1	0	.	0	0	2	41	0	0.75	1	81.21
1	42.1	1	1	1	0	2	43	0	1.12	0	81.21
1	43.1	0	.	0	0	1	43	0	1.12	0	81.21
1	44.1	1	.	1	0	2	44	0	1.87	2	81.21
1	45.1	1	0	1	0	1	44	0	1.50	1	81.21
1	46.1	0	1	0	0	1	44	0	1.50	0	81.21
1	47.1	1	1	0	0	2	44	0	1.50	2	81.21
1	48.1	0	1	0	0	1	44	0	1.87	1	81.21
1	49.1	0	0	0	0	1	44	0	1.50	2	81.21
1	50.1	1	1	1	0	2	44	0	1.50	2	81.21
1	51.1	1	.	1	0	2	51	0	1.12	2	81.21
1	52.1	0	.	0	0	2	52	0	1.50	1	81.21
1	53.1	0	.	0	0	2	53	0	0.75	1	81.21
1	54.1	0	1	0	0	.	57	0	0.75	1	81.21
1	55.1	1	1	0	0	1	57	0	1.12	2	81.21
1	56.1	0	.	0	0	3	56	0	1.12	1	81.21
1	57.1	1	.	1	0	3	57	0	0.37	2	81.21
1	58.1	0	1	0	0	2	56	0	1.12	0	81.21
1	59.1	1	.	0	0	2	59	0	1.12	0	81.21
1	60.1	1	.	1	0	1	60	0	0.75	0	81.21

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
1	6.1	39.84	0.67	1.48	0.67	1.48	1			
1	7.1	42.15	0.63	1.58	0.63	1.58	1			
1	8.1	46.22	0.64	1.56	0.64	1.56	1			
1	9.1	43.45	0.62	1.61	0.63	1.58	0			
1	10.1	45.05	0.62	1.62	0.63	1.58	0			
1	11.1	46.75	0.62	1.60	0.63	1.58	0			
1	12.1	49.49	0.63	1.58	0.63	1.58	0			
1	13.1	50.69	0.63	1.59	0.63	1.58	0			
1	14.1	52.09	0.62	1.60	0.63	1.58	0			
1	15.1	53.93	0.62	1.61	0.63	1.58	0			
1	16.1	55.56	0.62	1.62	0.63	1.58	0			
1	17.1	57	0.62	1.62	0.63	1.58	0			
1	18.1	58.16	0.61	1.63	0.63	1.58	0			
1	19.1	59.3	0.61	1.64	0.63	1.58	0			
1	20.1	66.37	0.63	1.59	0.63	1.59	1			
1	22.1	64.1	0.58	1.71	0.58	1.71	1			
1	23.1	69.01	0.60	1.66	0.58	1.71	0			
1	24.1	70.64	0.60	1.66	0.58	1.71	0			
1	25.1	72.01	0.60	1.66	0.58	1.71	0			
1	30.1	140.45	0.69	1.46	0.69	1.46	1			
1	31.1	142.48	0.69	1.45	0.69	1.46	0			
1	32.1	145.08	0.69	1.45	0.69	1.46	0			
1	33.1	146.42	0.67	1.48	0.67	1.48	1			
1	34.1	150.76	0.69	1.45	0.69	1.45	1			
1	35.1	148.99	0.64	1.56	0.64	1.56	1			
1	36.1	161.53	0.69	1.45	0.69	1.45	1			
1	37.1	163.47	0.68	1.46	0.69	1.45	0			
1	38.1	173.68	0.50	2.02	0.50	2.02	1			
1	39.1	177.92	0.50	1.99	0.50	1.99	1			
1	40.1	215.69	0.73	1.38	0.73	1.38	1			
1	41.1	218.56	0.74	1.36	0.74	1.36	1			
1	42.1	224.56	0.76	1.31	0.77	1.30	0			
1	43.1	222.39	0.77	1.30	0.77	1.30	1			
1	44.1	227.73	0.68	1.47	0.68	1.47	1			
1	45.1	225.16	0.67	1.48	0.68	1.47	0			
1	46.1	229.17	0.68	1.47	0.68	1.47	0			
1	47.1	231.34	0.67	1.48	0.68	1.47	0			
1	48.1	232.84	0.67	1.49	0.68	1.47	0			
1	49.1	234.54	0.67	1.48	0.68	1.47	0			
1	50.1	237.54	0.69	1.46	0.68	1.47	0			
1	51.1	240.75	0.69	1.44	0.69	1.44	1			
1	52.1	236.14	0.64	1.55	0.64	1.55	1			
1	53.1	251.96	0.51	1.98	0.51	1.98	1			
1	54.1	254.86	0.47	2.15	0.46	2.16	0			
1	55.1	255.63	0.46	2.16	0.46	2.16	0			
1	56.1	258.8	0.45	2.23	0.45	2.23	1			
1	57.1	249.65	0.46	2.16	0.46	2.16	1			
1	58.1	262.03	0.45	2.22	0.45	2.23	0			
1	59.1	265.7	0.46	2.19	0.46	2.19	1			
1	60.1	269.01	0.45	2.20	0.45	2.20	1			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
1	61.1	1	0	1	0	2	60	0	0.75	2	81.21
1	62.1	1	0	1	0	2	60	0	1.12	0	81.21
1	63.1	1	0	1	0	1	60	0	1.12	0	81.21
1	69.1	1	.	1	0	2	69	0	0.37	2	81.21
1	70.1	1	0	0	0	1	69	0	0.75	0	81.21
1	71.1	1	0	0	0	1	69	0	1.12	1	81.21
1	72.1	1	0	0	0	1	69	0	1.50	2	81.21
1	73.1	0	1	0	0	1	69	0	1.87	1	81.21
1	74.1	0	0	0	0	1	69	0	1.50	0	81.21
1	75.1	0	0	0	0	1	69	0	1.87	1	81.21
1	76.1	0	0	0	0	1	69	0	1.87	2	81.21
1	77.1	1	1	0	0	1	69	0	2.25	1	81.21
1	78.1	1	.	1	0	1	78	0	1.50	2	81.21
1	79.1	0	0	0	0	1	78	0	1.50	1	81.21
1	80.1	0	1	0	0	2	78	0	1.12	1	81.21
1	81.1	0	0	0	0	1	78	0	1.50	2	81.21
1	82.1	0	0	0	0	1	78	0	2.25	2	81.21
1	83.1	0	0	0	0	1	78	0	1.87	1	81.21
1	84.1	0	0	0	0	1	78	0	1.50	0	81.21
1	85.1	1	.	1	0	2	85	0	0.37	2	81.21
1	86.1	0	1	1	0	1	85	0	0.75	1	81.21
1	87.1	1	1	1	0	2	56	0	0.75	2	81.21
1	88.1	0	0	1	0	2	85	0	1.12	1	81.21
1	89.1	1	1	1	0	1	85	0	1.50	2	81.21
1	90.1	0	1	0	0	2	85	0	1.50	1	81.21
1	91.1	0	0	0	0	1	85	0	1.50	2	81.21
1	92.1	1	1	0	0	2	85	0	1.50	2	81.21
1	93.1	1	1	0	0	1	85	0	1.50	2	163.37
1	94.1	0	1	0	0	2	85	0	1.50	1	163.37
1	95.1	0	1	0	0	1	85	0	1.50	1	163.37
1	96.1	1	1	0	0	1	85	0	1.50	1	81.21
1	97.1	1	0	0	0	1	85	0	1.50	1	81.21
1	98.1	1	0	1	0	2	85	0	1.50	2	81.21
1	99.1	1	0	0	0	1	85	0	1.12	2	81.21
1	100.1	0	1	0	0	2	85	0	1.50	2	163.37
1	101.1	0	0	1	0	1	85	0	1.87	1	163.37
1	102.1	0	0	0	0	2	85	0	1.12	2	81.21
1	103.1	1	1	0	0	1	85	0	1.50	2	208.28
1	104.1	1	0	0	0	1	85	0	1.87	1	163.37
1	105.1	1	0	0	0	1	85	0	1.50	2	208.28
1	106.1	1	0	1	0	1	85	0	1.12	0	208.28
1	107.1	1	0	1	0	1	85	0	1.87	1	208.28
1	108.1	0	1	0	0	1	85	0	1.50	1	81.21
1	109.1	1	1	1	0	1	85	0	1.50	2	208.28
1	110.1	1	0	1	0	2	85	0	1.50	1	208.28
1	111.1	0	1	0	0	1	85	0	1.87	2	208.28
1	112.1	1	0	1	0	1	85	0	1.87	2	81.21
1	113.1	0	1	0	0	1	85	0	1.50	1	81.21
1	114.1	0	0	0	0	1	85	0	1.87	0	81.21
1	115.1	1	1	0	0	1	85	0	1.87	2	81.21

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
1	61.1	271.01	0.46	2.20	0.45	2.20	0			
1	62.1	273.98	0.46	2.19	0.45	2.20	0			
1	63.1	275.21	0.45	2.20	0.45	2.20	0			
1	69.1	285.89	0.45	2.24	0.45	2.24	1			
1	70.1	286.39	0.44	2.26	0.45	2.24	0			
1	71.1	289.46	0.44	2.26	0.45	2.24	0			
1	72.1	289.89	0.45	2.23	0.45	2.24	0			
1	73.1	291.1	0.44	2.28	0.45	2.24	0			
1	74.1	292.83	0.44	2.27	0.45	2.24	0			
1	75.1	294.27	0.44	2.27	0.45	2.24	0			
1	76.1	296.2	0.44	2.29	0.45	2.24	0			
1	77.1	295.77	0.43	2.31	0.45	2.24	0			
1	78.1	300.84	0.44	2.26	0.44	2.26	1			
1	79.1	302.21	0.44	2.28	0.44	2.26	0			
1	80.1	300.64	0.44	2.27	0.44	2.26	0			
1	81.1	303.44	0.44	2.28	0.44	2.26	0			
1	82.1	306.08	0.44	2.27	0.44	2.26	0			
1	83.1	305.04	0.44	2.28	0.44	2.26	0			
1	84.1	308.58	0.44	2.26	0.44	2.26	0			
1	85.1	315.72	0.46	2.17	0.46	2.17	1			
1	86.1	317.62	0.46	2.19	0.46	2.17	0			
1	87.1	260.43	0.45	2.22	0.45	2.23	0			
1	88.1	319.29	0.46	2.20	0.46	2.17	0			
1	89.1	321.19	0.46	2.18	0.46	2.17	0			
1	90.1	323.36	0.45	2.21	0.46	2.17	0			
1	91.1	324.76	0.45	2.20	0.46	2.17	0			
1	92.1	327.77	0.45	2.21	0.46	2.17	0			
1	93.1	73.8	0.45	2.21	0.46	2.17	0			
1	94.1	85.08	0.45	2.21	0.46	2.17	0			
1	95.1	84.48	0.46	2.18	0.46	2.17	0			
1	96.1	332.97	0.46	2.18	0.46	2.17	0			
1	97.1	339.48	0.45	2.20	0.46	2.17	0			
1	98.1	342.51	0.46	2.19	0.46	2.17	0			
1	99.1	338.08	0.46	2.20	0.46	2.17	0			
1	100.1	86.88	0.46	2.18	0.46	2.17	0			
1	101.1	88.19	0.45	2.20	0.46	2.17	0			
1	102.1	348.09	0.45	2.20	0.46	2.17	0			
1	103.1	89.89	0.46	2.20	0.46	2.17	0			
1	104.1	91.62	0.45	2.20	0.46	2.17	0			
1	105.1	91.72	0.46	2.19	0.46	2.17	0			
1	106.1	121.78	0.49	2.06	0.46	2.17	0			
1	107.1	88.62	0.46	2.19	0.46	2.17	0			
1	108.1	356.69	0.46	2.18	0.46	2.17	0			
1	109.1	125.26	0.48	2.10	0.46	2.17	0			
1	110.1	123.52	0.48	2.10	0.46	2.17	0			
1	111.1	127.22	0.48	2.10	0.46	2.17	0			
1	112.1	368.74	0.47	2.12	0.46	2.17	0			
1	113.1	370.44	0.47	2.12	0.46	2.17	0			
1	114.1	372.21	0.48	2.10	0.46	2.17	0			
1	115.1	373.34	0.47	2.13	0.46	2.17	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
1	116.1	0	1	1	1	2	85	0	1.87	0	81.21
1	117.1	1	.	1	0	2	117	1	1.12	2	81.21
1	118.1	0	0	0	0	1	85	0	1.87	1	163.37
1	119.1	0	0	1	0	2	85	0	1.87	1	81.21
1	120.1	0	0	1	0	1	85	0	2.25	2	81.21
1	121.1	0	0	0	0	1	85	0	2.25	2	81.21
1	122.1	1	.	0	0	1	122	1	1.87	1	286.88
1	123.1	1	0	0	0	1	122	1	2.25	1	286.88
1	124.1	0	.	0	0	1	124	1	2.25	0	81.21
1	125.1	1	.	1	0	1	125	0	1.50	0	81.21
1	126.1	1	0	1	0	1	124	1	2.25	1	81.21
1	127.1	1	1	0	0	1	132	0	1.12	0	81.21
1	128.1	0	0	0	0	1	124	1	1.87	1	81.21
1	129.1	1	1	1	0	1	132	0	2.25	2	208.28
1	130.1	1	1	0	0	1	124	1	1.87	2	81.21
1	131.1	1	0	0	0	1	132	0	0.75	2	81.21
1	132.1	1	.	0	0	1	132	0	0.75	2	81.21
1	133.1	0	1	0	0	1	132	0	1.50	1	81.21
1	134.1	0	1	0	0	1	132	0	1.87	2	81.21
1	135.1	0	.	1	0	3	135	0	0.37	2	208.28
1	136.1	1	.	1	0	.	136	0	0.75	2	81.21
1	137.1	0	0	1	0	1	85	0	1.87	2	81.21
1	138.1	1	.	1	0	3	138	0	0.37	2	380.26
1	139.1	1	.	1	0	2	139	0	0.75	2	380.26
1	140.1	1	.	1	0	3	140	0	0.37	2	380.26
1	141.1	1	.	1	0	.	141	0	0.75	0	380.26
1	142.1	0	.	0	0	3	142	0	0.37	2	380.26
1	143.1	0	.	0	0	.	143	0	0.75	0	380.26
1	144.1	0	0	0	0	2	143	0	1.12	1	380.26
1	145.1	0	.	0	0	.	145	0	0.75	1	380.26
1	146.1	0	0	0	0	2	143	0	1.12	1	380.26
1	147.1	0	0	0	0	2	148	0	1.12	2	380.26
1	148.1	0	.	0	0	.	148	0	1.12	1	380.26
1	122.3	1	.	0	0	3	122	0	0.37	0	36.30
1	123.3	1	0	0	0	1	122	0	0.75	2	36.30
1	138.3	1	.	1	0	3	138	0	0.37	0	129.69
1	139.3	1	.	1	0	2	139	0	0.75	2	129.69
1	140.3	1	.	1	0	3	140	0	0.37	0	129.69
1	141.3	1	.	1	0	.	141	0	0.75	2	129.69
1	142.3	0	.	0	0	3	142	0	0.37	2	129.69
1	143.3	0	0	0	0	2	145	0	0.75	2	129.69
1	144.3	0	0	0	0	1	145	0	1.12	2	129.69
1	145.3	0	.	0	0	3	145	0	0.75	1	129.69
1	146.3	0	.	0	0	2	146	0	1.50	2	129.69
1	147.3	0	0	0	0	1	148	0	0.75	0	129.69
1	148.3	0	.	0	0	3	148	0	0.37	1	129.69
1	138.4	1	.	1	0	3	138	0	0.37	1	62.33
1	139.4	1	.	1	0	2	138	0	0.75	0	62.33
1	140.4	1	.	1	0	3	140	0	0.37	0	62.33
1	141.4	1	0	1	0	.	140	0	0.75	2	62.33

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
1	116.1	374.51	0.46	2.18	0.46	2.17	0			
1	117.1	396.1	0.48	2.10	0.48	2.10	1			
1	118.1	186.92	0.43	2.31	0.46	2.17	0			
1	119.1	380.75	0.43	2.30	0.46	2.17	0			
1	120.1	386.56	0.45	2.24	0.46	2.17	0			
1	121.1	385.16	0.44	2.29	0.46	2.17	0			
1	122.1	111.77	0.51	1.98	0.51	1.98	1			
1	123.1	113.04	0.51	1.96	0.51	1.98	0			
1	124.1	383.45	0.42	2.36	0.42	2.36	1			
1	125.1	414.02	0.49	2.04	0.49	2.04	1			
1	126.1	391.5	0.44	2.30	0.42	2.36	0			
1	127.1	405.48	0.46	2.19	0.46	2.17	0			
1	128.1	383.22	0.42	2.38	0.42	2.36	0			
1	129.1	220.52	0.46	2.18	0.46	2.17	0			
1	130.1	389.73	0.43	2.32	0.42	2.36	0			
1	131.1	404.61	0.46	2.16	0.46	2.17	0			
1	132.1	401.24	0.46	2.17	0.46	2.17	1			
1	133.1	407.18	0.47	2.14	0.46	2.17	0			
1	134.1	407.91	0.45	2.20	0.46	2.17	0			
1	135.1	436.13	1.12	0.90	1.12	0.90	1			
1	136.1	221.23	0.32	3.09	0.32	3.09	1			
1	137.1	377.05	0.45	2.21	0.46	2.17	0			
1	138.1	187.72	0.70	1.42	0.70	1.42	1			
1	139.1	189.49	0.70	1.43	0.70	1.43	1			
1	140.1	256.02	0.75	1.33	0.75	1.33	1			
1	141.1	259.09	0.76	1.32	0.76	1.32	1			
1	142.1	269.6	0.82	1.23	0.82	1.23	1			
1	143.1	276.48	0.81	1.23	0.81	1.23	1			
1	144.1	277.88	0.81	1.24	0.81	1.23	0			
1	145.1	274.91	0.81	1.23	0.81	1.23	1			
1	146.1	280.31	0.81	1.24	0.81	1.23	0			
1	147.1	323.99	0.78	1.28	0.80	1.26	0			
1	148.1	328.19	0.80	1.26	0.80	1.26	1			
1	122.3	111.77	0.71	1.41	0.71	1.41	1			
1	123.3	113.04	0.70	1.42	0.71	1.41	0			
1	138.3	187.72	0.73	1.36	0.73	1.36	1			
1	139.3	189.49	0.72	1.38	0.72	1.38	1			
1	140.3	256.02	0.76	1.32	0.76	1.32	1			
1	141.3	259.09	0.74	1.36	0.74	1.36	1			
1	142.3	269.6	0.73	1.37	0.73	1.37	1			
1	143.3	276.48	0.74	1.35	0.74	1.35	0			
1	144.3	277.88	0.74	1.35	0.74	1.35	0			
1	145.3	274.91	0.74	1.35	0.74	1.35	1			
1	146.3	280.31	0.72	1.39	0.72	1.39	1			
1	147.3	323.99	0.84	1.20	0.84	1.18	0			
1	148.3	328.19	0.84	1.18	0.84	1.18	1			
1	138.4	187.72	0.73	1.37	0.73	1.37	1			
1	139.4	189.49	0.73	1.37	0.73	1.37	1			
1	140.4	256.02	0.79	1.27	0.79	1.27	1			
1	141.4	259.09	0.79	1.26	0.79	1.27	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
1	142.4	0	.	0	0	3	142	0	0.37	2	62.33
1	143.4	0	0	0	0	2	145	0	0.75	0	62.33
1	144.4	0	0	0	0	1	145	0	1.12	2	62.33
1	145.4	0	.	0	0	3	145	0	0.37	1	62.33
1	146.4	0	.	0	0	3	145	0	0.37	1	62.33
1	147.4	0	0	0	0	1	147	0	0.37	2	62.33
1	148.4	0	.	0	0	3	148	0	0.37	1	62.33
2	48.1	1	.	0	0	2	48	0	0.45	0	25.86
2	49.1	0	1	0	0	2	48	0	0.89	2	25.86
2	58.1	1	.	1	0	3	58	0	0.45	2	106.25
2	65.1	1	.	0	0	.	65	0	0.89	1	106.25
2	83.1	1	0	1	0	2	176	0	0.89	0	271.76
2	84.1	1	0	1	0	2	176	0	0.89	0	271.76
2	96.1	1	.	0	0	.	96	0	0.45	2	342.63
2	97.1	1	0	0	0	1	96	0	0.89	1	342.63
2	98.1	1	0	0	0	1	96	0	1.34	2	342.63
2	99.1	1	0	0	0	1	96	0	0.89	1	342.63
2	115.1	1	.	1	0	3	115	0	0.45	2	342.63
2	116.1	1	.	1	0	3	116	0	0.45	0	342.63
2	117.1	1	.	1	0	3	117	0	0.45	2	342.63
3	128.1	1	1	0	0	2	129	0	0.89	2	60.84
3	129.1	0	.	0	0	3	129	0	0.45	1	60.84
3	130.1	0	.	0	0	3	130	0	0.45	1	91.88
3	131.1	1	1	1	0	1	130	0	0.89	1	91.88
3	136.1	1	.	1	0	3	136	0	0.45	2	133.26
3	137.1	0	1	1	0	2	136	0	0.89	1	133.26
3	138.1	1	1	1	0	.	136	0	0.89	0	133.26
3	139.1	1	0	0	0	2	136	0	0.89	0	133.26
3	140.1	1	0	0	0	2	136	0	0.89	0	133.26
3	141.1	0	1	0	0	2	136	0	0.89	1	133.26
3	150.1	1	.	1	0	.	150	0	0.89	2	195.32
3	160.1	1	.	1	0	3	160	0	0.45	2	133.26
3	161.1	1	.	0	0	3	161	0	0.45	2	133.26
3	162.1	1	.	0	0	.	162	0	0.45	0	133.26
3	163.1	1	0	0	0	2	162	0	0.89	0	133.26
3	164.1	1	0	0	0	2	162	0	0.89	0	133.26
3	165.1	0	.	0	1	3	165	0	0.45	1	133.26
3	166.1	1	.	1	0	3	166	0	0.45	2	133.26
3	167.1	1	.	1	0	.	167	0	0.45	1	133.26
3	168.1	1	0	1	0	2	167	0	0.89	1	133.26
3	169.1	0	1	1	0	.	167	0	0.89	2	91.88
3	170.1	0	0	1	0	2	167	0	0.89	1	91.88
3	171.1	1	1	1	0	.	172	0	1.34	2	133.26
3	172.1	0	.	0	0	3	172	0	0.89	2	71.19
3	174.1	0	.	0	0	3	174	0	0.45	2	133.26
3	175.1	0	0	0	0	2	174	0	0.89	0	133.26
3	176.1	1	.	0	0	3	176	0	0.45	1	133.26
3	177.1	0	1	0	0	.	176	0	0.89	2	133.26
3	178.1	1	1	1	0	.	176	0	0.89	0	133.26
3	179.1	0	.	0	0	.	179	0	0.89	1	257.39

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
1	142.4	269.6	0.74	1.36	0.74	1.36	1			
1	143.4	276.48	0.75	1.34	0.75	1.33	0			
1	144.4	277.88	0.75	1.34	0.75	1.33	0			
1	145.4	274.91	0.75	1.33	0.75	1.33	1			
1	146.4	274.91	0.75	1.33	0.74	1.34	1			
1	147.4	323.99	0.83	1.20	0.83	1.20	0			
1	148.4	328.19	0.90	1.11	0.90	1.11	1			
2	48.1	208.31	0.60	1.67	0.60	1.67	1			
2	49.1	210.95	0.60	1.66	0.60	1.67	0			
2	58.1	164.3	0.63	1.59	0.63	1.59	1			
2	65.1	233.13	0.60	1.67	0.60	1.67	1			
2	83.1	78.07	0.52	1.92	0.53	1.90	0			
2	84.1	79.44	0.52	1.92	0.53	1.90	0			
2	96.1	167.03	0.55	1.81	0.55	1.81	1			
2	97.1	165.19	0.55	1.81	0.55	1.81	0			
2	98.1	168.46	0.55	1.80	0.55	1.81	0			
2	99.1	169	0.55	1.81	0.55	1.81	0			
2	115.1	154.88	0.56	1.78	0.56	1.78	1			
2	116.1	157.95	0.54	1.86	0.54	1.86	1			
2	117.1	156.62	0.55	1.83	0.55	1.83	1			
3	128.1	137.74	0.74	1.34	0.75	1.33	0			
3	129.1	134.07	0.75	1.33	0.75	1.33	1			
3	130.1	102.1	0.70	1.44	0.70	1.44	1			
3	131.1	103.47	0.70	1.44	0.70	1.44	0			
3	136.1	106.14	0.63	1.60	0.63	1.60	1			
3	137.1	115.45	0.63	1.58	0.63	1.60	0			
3	138.1	118.25	0.63	1.59	0.63	1.60	0			
3	139.1	121.49	0.63	1.59	0.63	1.60	0			
3	140.1	125.52	0.63	1.59	0.63	1.60	0			
3	141.1	127.06	0.63	1.59	0.63	1.60	0			
3	150.1	188.02	0.69	1.46	0.69	1.46	1			
3	160.1	152.25	0.58	1.72	0.58	1.72	1			
3	161.1	130.7	0.61	1.65	0.61	1.65	1			
3	162.1	132.73	0.58	1.71	0.58	1.71	1			
3	163.1	151.05	0.59	1.70	0.58	1.71	0			
3	164.1	135.1	0.58	1.71	0.58	1.71	0			
3	165.1	154.85	0.58	1.72	0.58	1.72	1			
3	166.1	160.53	0.60	1.68	0.60	1.68	1			
3	167.1	156.72	0.60	1.66	0.60	1.66	1			
3	168.1	158.46	0.60	1.66	0.60	1.66	0			
3	169.1	223.12	0.60	1.66	0.60	1.66	0			
3	170.1	223.69	0.60	1.66	0.60	1.66	0			
3	171.1	199.8	0.52	1.93	0.50	2.01	0			
3	172.1	238.67	0.50	2.01	0.50	2.01	1			
3	174.1	251.65	0.53	1.87	0.53	1.87	1			
3	175.1	249.75	0.54	1.86	0.53	1.87	0			
3	176.1	256.02	0.53	1.90	0.53	1.90	1			
3	177.1	258.29	0.53	1.90	0.53	1.90	0			
3	178.1	260.79	0.52	1.92	0.53	1.90	0			
3	179.1	81.18	0.49	2.04	0.49	2.04	1			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
3	180.1	1	.	0	0	3	180	0	0.45	1	257.39
3	181.1	1	.	1	0	3	181	0	0.45	2	133.26
3	182.1	0	1	0	0	2	183	0	0.89	2	257.39
3	183.1	1	.	0	0	3	183	0	0.45	0	257.39
3	184.1	0	0	0	0	1	183	0	1.34	1	133.26
3	185.1	0	0	1	0	1	183	0	1.34	0	133.26
3	186.1	0	0	0	0	1	183	0	1.34	1	133.26
3	187.1	0	0	0	0	1	183	0	1.79	2	133.26
3	190.1	0	0	1	0	2	183	0	1.34	2	195.32
3	191.1	0	0	0	0	2	183	0	1.34	0	257.39
3	208.1	1	.	1	0	2	208	0	0.89	1	323.41
3	209.1	1	.	0	0	3	209	0	0.45	2	323.41
3	210.1	1	.	1	0	3	210	0	0.45	2	323.41
3	211.1	0	.	1	0	2	211	0	0.89	1	395.82
2	77.2	0	1	0	0	1	80	0	0.35	2	25.86
2	78.2	0	0	0	0	2	80	0	0.69	1	25.86
2	79.2	0	0	0	0	2	80	0	1.39	1	25.86
2	80.2	1	.	1	0	1	80	0	1.04	0	25.86
2	83.2	1	0	1	0	2	84	0	0.69	2	87.93
2	84.2	1	.	1	0	3	84	0	0.35	2	87.93
2	96.2	1	.	0	0	3	96	0	0.35	2	158.80
2	97.2	1	0	0	0	1	96	0	0.69	1	158.80
2	98.2	1	0	0	0	1	96	0	1.39	2	158.80
2	99.2	1	0	0	0	2	96	0	1.04	1	158.80
2	115.2	1	.	1	0	3	115	0	0.35	2	158.80
2	116.2	1	.	1	0	.	116	0	0.69	0	158.80
2	117.2	1	.	1	0	3	117	0	0.35	2	158.80
3	150.2	1	.	1	0	1	150	0	0.35	1	25.86
3	179.2	0	.	0	0	3	179	0	0.35	0	87.93
3	180.2	1	.	0	0	3	180	0	0.69	0	87.93
3	182.2	0	1	0	0	2	183	0	0.69	2	87.93
3	183.2	1	.	0	0	.	183	0	0.69	2	87.93
3	190.2	0	.	1	0	2	190	0	0.35	2	25.86
3	191.2	0	.	0	0	3	191	0	0.35	2	87.93
3	208.2	1	.	1	0	3	208	0	0.35	1	153.94
3	209.2	1	.	0	0	.	209	0	0.69	2	153.94
3	210.2	1	.	1	0	.	210	0	0.69	2	153.94
3	211.2	0	.	1	0	3	211	0	0.35	2	226.36
2	83.3	1	0	1	0	2	84	0	0.35	2	25.86
2	84.3	1	.	1	0	2	84	0	0.69	2	25.86
2	96.3	1	.	0	0	3	96	0	0.35	2	96.73
2	97.3	1	0	0	0	1	96	0	0.69	1	96.73
2	98.3	1	0	0	0	1	96	0	1.39	2	96.73
2	99.3	1	0	0	0	2	96	0	1.04	1	96.73
2	115.3	1	.	1	0	3	115	0	0.35	2	96.73
2	116.3	1	0	1	0	2	117	0	0.69	0	96.73
2	117.3	1	.	1	0	3	117	0	0.35	2	96.73
3	179.3	0	.	0	0	2	179	0	1.04	1	25.86
3	180.3	1	.	0	0	3	180	0	0.69	0	25.86
3	182.3	0	1	0	0	2	183	0	0.69	2	25.86

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
3	180.1	84.85	0.50	1.99	0.50	1.99	1			
3	181.1	206.17	0.48	2.09	0.48	2.09	1			
3	182.1	90.22	0.50	1.98	0.50	1.98	0			
3	183.1	88.65	0.50	1.98	0.50	1.98	1			
3	184.1	289.72	0.50	1.99	0.50	1.98	0			
3	185.1	290.96	0.50	2.00	0.50	1.98	0			
3	186.1	291.46	0.50	2.02	0.50	1.98	0			
3	187.1	292.69	0.50	2.01	0.50	1.98	0			
3	190.1	313.68	0.50	2.01	0.50	1.98	0			
3	191.1	187.05	0.50	2.02	0.50	1.98	0			
3	208.1	226.36	0.62	1.61	0.62	1.61	1			
3	209.1	233.63	0.54	1.87	0.54	1.87	1			
3	210.1	236.17	0.53	1.87	0.53	1.87	1			
3	211.1	228.96	0.53	1.89	0.53	1.89	1			
2	77.2	170.34	0.59	1.70	0.61	1.63	0			
2	78.2	172.14	0.58	1.73	0.61	1.63	0			
2	79.2	174.37	0.58	1.72	0.61	1.63	0			
2	80.2	173.11	0.61	1.63	0.61	1.63	1			
2	83.2	78.07	0.63	1.60	0.62	1.60	0			
2	84.2	79.44	0.62	1.60	0.62	1.60	1			
2	96.2	167.03	0.71	1.42	0.71	1.42	1			
2	97.2	165.19	0.71	1.41	0.71	1.42	0			
2	98.2	168.46	0.71	1.42	0.71	1.42	0			
2	99.2	169	0.70	1.42	0.71	1.42	0			
2	115.2	154.88	0.69	1.44	0.69	1.44	1			
2	116.2	157.95	0.68	1.48	0.68	1.48	1			
2	117.2	156.62	0.64	1.56	0.64	1.56	1			
3	150.2	188.02	0.69	1.44	0.69	1.44	1			
3	179.2	81.18	0.65	1.55	0.65	1.55	1			
3	180.2	84.85	0.64	1.56	0.64	1.56	1			
3	182.2	90.22	0.62	1.61	0.62	1.62	0			
3	183.2	88.65	0.62	1.62	0.62	1.62	1			
3	190.2	313.68	0.78	1.29	0.78	1.29	1			
3	191.2	187.05	1.05	0.95	1.05	0.95	1			
3	208.2	226.36	0.92	1.08	0.92	1.08	1			
3	209.2	233.63	0.69	1.46	0.69	1.46	1			
3	210.2	236.17	0.69	1.46	0.69	1.46	1			
3	211.2	228.96	0.87	1.15	0.87	1.15	1			
2	83.3	78.07	0.65	1.53	0.68	1.48	0			
2	84.3	79.44	0.68	1.48	0.68	1.48	1			
2	96.3	167.03	0.68	1.47	0.68	1.47	1			
2	97.3	165.19	0.69	1.46	0.68	1.47	0			
2	98.3	168.46	0.69	1.45	0.68	1.47	0			
2	99.3	169	0.69	1.46	0.68	1.47	0			
2	115.3	154.88	0.66	1.51	0.66	1.51	1			
2	116.3	157.95	0.65	1.53	0.65	1.53	0			
2	117.3	156.62	0.65	1.53	0.65	1.53	1			
3	179.3	81.18	0.63	1.58	0.63	1.58	1			
3	180.3	84.85	0.64	1.57	0.64	1.57	1			
3	182.3	90.22	0.64	1.57	0.64	1.56	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
3	183.3	1	.	0	0	.	183	0	0.69	2	25.86
3	191.3	0	.	0	0	3	191	0	0.35	2	25.86
3	211.3	0	.	1	0	3	211	0	0.35	2	164.29
3	211.4	0	.	1	0	3	211	0	0.45	2	36.21
4	29.1	1	.	1	0	3	29	0	0.45	2	85.56
4	30.1	1	0	0	0	1	32	0	0.89	0	106.25
4	31.1	1	0	1	0	2	32	0	1.34	1	106.25
4	32.1	1	.	1	0	3	32	0	0.45	1	106.25
4	33.1	1	.	0	0	1	33	0	0.45	2	95.90
4	34.1	1	0	0	0	.	32	0	0.89	0	106.25
4	35.1	0	1	0	0	1	32	0	0.89	1	106.25
4	36.1	0	0	0	0	2	32	0	1.34	0	106.25
4	37.1	1	0	1	0	1	32	0	0.89	2	106.25
4	38.1	0	0	0	0	2	32	0	1.34	1	106.25
4	39.1	0	0	0	0	2	32	0	0.89	1	106.25
4	40.1	0	0	0	0	.	32	0	0.89	1	106.25
4	41.1	1	1	1	0	2	32	0	0.89	2	106.25
4	42.1	1	0	1	0	2	32	0	1.34	2	106.25
4	43.1	1	0	1	0	2	32	0	1.34	0	106.25
4	44.1	0	1	0	0	2	32	0	0.89	0	106.25
4	66.1	0	.	0	0	.	66	0	0.45	1	147.63
4	67.1	1	.	1	0	3	67	0	0.45	0	147.63
4	68.1	1	1	1	0	2	66	0	0.89	2	147.63
4	69.1	0	1	0	0	2	66	0	0.89	1	106.25
4	70.1	0	0	0	0	2	66	0	0.89	1	209.69
4	71.1	0	0	0	0	2	66	0	0.89	1	147.63
4	72.1	0	.	0	0	1	72	0	0.45	2	209.69
4	73.1	0	.	0	0	3	73	0	0.89	1	147.63
4	74.1	0	.	0	0	.	74	0	0.45	0	209.69
4	75.1	0	0	0	0	2	74	0	0.89	2	209.69
4	76.1	0	.	0	0	.	76	0	0.89	2	209.69
4	81.1	1	.	1	0	3	81	0	0.45	2	147.63
4	82.1	1	0	0	0	2	81	0	0.89	0	147.63
4	86.1	0	.	0	0	2	86	0	0.89	1	147.63
4	87.1	1	.	1	0	3	87	0	0.45	2	106.25
4	89.1	1	.	0	0	.	89	0	0.89	0	147.63
4	90.1	1	.	0	0	.	90	0	0.89	0	147.63
4	91.1	1	0	1	0	.	90	0	0.45	0	147.63
4	92.1	1	.	1	0	.	92	0	0.45	1	147.63
4	93.1	1	.	0	0	.	93	0	0.89	1	147.63
4	94.1	0	.	0	0	.	94	0	0.89	0	147.63
4	95.1	1	.	0	0	3	95	0	0.45	1	147.63
4	100.1	1	.	1	0	2	100	0	0.89	2	271.76
4	101.1	1	.	0	0	3	101	0	0.45	0	271.76
4	102.1	0	1	1	0	1	103	0	1.34	0	271.76
4	103.1	1	.	1	0	3	103	0	0.45	1	271.76
4	104.1	0	0	1	0	.	103	0	1.34	2	271.76
4	105.1	0	0	1	0	2	103	0	0.89	2	271.76
4	106.1	0	0	0	0	2	103	0	1.34	0	342.63
4	107.1	0	0	0	0	2	103	0	1.34	1	342.63

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
3	183.3	88.65	0.64	1.56	0.64	1.56	1			
3	191.3	187.05	1.17	0.85	1.17	0.85	1			
3	211.3	228.96	0.84	1.19	0.84	1.19	1			
3	211.4	228.96	0.92	1.09	0.92	1.09	1			
4	29.1	39.67	0.57	1.76	0.57	1.76	1			
4	30.1	91.86	0.61	1.65	0.61	1.64	0			
4	31.1	92.89	0.61	1.65	0.61	1.64	0			
4	32.1	91.42	0.61	1.64	0.61	1.64	1			
4	33.1	39.04	0.53	1.87	0.53	1.87	1			
4	34.1	95.16	0.61	1.65	0.61	1.64	0			
4	35.1	98.5	0.61	1.63	0.61	1.64	0			
4	36.1	97.56	0.61	1.64	0.61	1.64	0			
4	37.1	96.49	0.60	1.65	0.61	1.64	0			
4	38.1	100.5	0.61	1.65	0.61	1.64	0			
4	39.1	102.5	0.61	1.64	0.61	1.64	0			
4	40.1	105.07	0.61	1.63	0.61	1.64	0			
4	41.1	106.1	0.61	1.64	0.61	1.64	0			
4	42.1	107.94	0.61	1.64	0.61	1.64	0			
4	43.1	109.41	0.61	1.64	0.61	1.64	0			
4	44.1	111.11	0.61	1.63	0.61	1.64	0			
4	66.1	180.88	0.61	1.63	0.61	1.63	1			
4	67.1	177.41	0.60	1.66	0.61	1.63	1			
4	68.1	183.12	0.61	1.64	0.61	1.63	0			
4	69.1	247.21	0.61	1.64	0.61	1.63	0			
4	70.1	215.58	0.61	1.63	0.61	1.63	0			
4	71.1	212.01	0.62	1.60	0.61	1.63	0			
4	72.1	219.15	0.61	1.64	0.61	1.64	1			
4	73.1	211.88	0.60	1.67	0.60	1.67	1			
4	74.1	217.92	0.62	1.62	0.62	1.62	1			
4	75.1	222.55	0.61	1.63	0.62	1.62	0			
4	76.1	228.13	0.62	1.62	0.62	1.62	1			
4	81.1	232.33	0.63	1.58	0.63	1.58	1			
4	82.1	239.27	0.63	1.58	0.63	1.58	0			
4	86.1	294.43	0.61	1.63	0.61	1.63	1			
4	87.1	361.59	0.48	2.09	0.48	2.09	1			
4	89.1	330.3	0.48	2.08	0.48	2.08	1			
4	90.1	306.27	0.49	2.05	0.49	2.05	1			
4	91.1	304.04	0.47	2.14	0.49	2.05	0			
4	92.1	309.41	0.49	2.06	0.49	2.06	1			
4	93.1	383.12	0.48	2.08	0.48	2.08	1			
4	94.1	386.69	0.48	2.09	0.48	2.09	1			
4	95.1	376.11	0.47	2.14	0.47	2.14	1			
4	100.1	279.04	0.51	1.97	0.51	1.97	1			
4	101.1	275.71	0.50	2.00	0.50	2.00	1			
4	102.1	280.71	0.49	2.04	0.48	2.08	0			
4	103.1	273.07	0.48	2.08	0.48	2.08	1			
4	104.1	282.38	0.49	2.02	0.48	2.08	0			
4	105.1	284.31	0.49	2.04	0.48	2.08	0			
4	106.1	180.48	0.49	2.04	0.48	2.08	0			
4	107.1	182.08	0.49	2.04	0.48	2.08	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
4	108.1	0	0	1	0	2	103	0	1.34	0	342.63
4	109.1	0	0	0	0	2	103	0	1.34	1	342.63
4	110.1	1	1	1	0	2	103	0	1.34	2	342.63
4	111.1	0	1	0	0	2	103	0	1.34	1	342.63
4	112.1	1	1	0	0	2	103	0	1.34	0	342.63
4	113.1	1	.	0	0	3	113	0	0.45	0	342.63
4	114.1	0	.	1	0	2	114	0	1.34	0	342.63
5	132.1	0	.	1	0	3	132	0	0.45	1	25.86
5	135.1	0	.	1	0	2	135	0	0.89	2	71.19
5	142.1	0	.	0	0	2	142	0	0.45	1	133.26
5	143.1	1	.	1	0	3	143	0	0.45	2	91.88
5	144.1	0	1	0	0	1	145	0	0.89	1	91.88
5	145.1	1	.	1	0	1	145	0	0.45	2	91.88
5	146.1	1	1	1	0	2	145	0	1.34	1	91.88
5	147.1	1	1	0	0	1	145	0	1.34	1	91.88
5	148.1	0	0	1	0	1	145	0	1.34	2	133.26
5	149.1	0	1	1	0	2	145	0	1.34	1	91.88
5	151.1	0	0	1	0	2	145	0	1.34	1	91.88
5	152.1	0	1	1	0	2	145	0	1.79	2	91.88
5	153.1	0	0	1	0	2	145	0	1.34	0	91.88
5	154.1	1	1	1	0	.	145	0	0.89	0	25.86
5	155.1	1	.	0	0	.	155	0	0.89	0	25.86
5	156.1	1	.	1	0	.	156	0	0.45	0	133.26
5	157.1	1	.	0	0	2	157	0	0.89	2	133.26
5	173.1	1	.	0	0	3	173	0	0.45	2	133.26
5	188.1	1	.	1	0	3	188	0	0.45	2	133.26
5	189.1	1	0	1	0	1	188	0	0.89	0	133.26
5	192.1	0	1	0	0	2	188	0	1.34	0	195.32
5	193.1	1	0	1	0	2	188	0	1.34	1	195.32
5	194.1	1	1	0	0	2	188	0	1.34	0	195.32
5	195.1	1	0	1	0	2	188	0	1.34	2	195.32
5	196.1	1	0	1	0	1	188	0	1.34	2	195.32
5	197.1	1	0	0	0	2	188	0	0.89	1	195.32
5	198.1	1	0	1	0	2	188	0	1.34	2	133.26
5	199.1	1	1	1	0	1	188	0	2.23	0	133.26
5	200.1	0	1	0	0	1	188	0	1.79	0	133.26
5	201.1	0	0	1	0	1	188	0	1.79	1	91.88
5	202.1	1	1	1	0	1	188	0	1.79	0	133.26
5	203.1	0	1	1	0	2	188	0	1.79	2	133.26
5	205.1	1	.	1	0	3	205	0	0.45	0	133.26
5	206.1	1	.	1	0	.	206	0	0.45	1	133.26
5	207.1	1	0	1	0	1	206	0	0.89	2	133.26
5	212.1	0	.	0	0	3	212	0	0.45	2	133.26
5	213.1	0	0	0	0	.	212	0	0.89	0	133.26
5	214.1	0	0	0	0	2	212	0	0.89	1	133.26
5	215.1	0	1	1	0	2	113	0	0.89	0	323.41
5	216.1	1	.	0	1	3	216	0	0.45	2	323.41
5	217.1	0	0	1	0	2	114	0	1.34	0	323.41
4	70.2	0	.	0	0	3	70	0	0.35	1	25.86
4	72.2	0	0	0	0	2	74	0	1.04	0	25.86

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
4	108.1	183.61	0.49	2.04	0.48	2.08	0			
4	109.1	184.58	0.49	2.03	0.48	2.08	0			
4	110.1	186.22	0.49	2.04	0.48	2.08	0			
4	111.1	187.92	0.49	2.04	0.48	2.08	0			
4	112.1	196.63	0.49	2.04	0.48	2.08	0			
4	113.1	199.6	0.46	2.20	0.46	2.20	1			
4	114.1	203.67	0.44	2.27	0.44	2.27	1			
5	132.1	126.83	0.51	1.95	0.51	1.95	1			
5	135.1	41.64	0.46	2.19	0.46	2.19	1			
5	142.1	120.12	0.60	1.66	0.60	1.66	1			
5	143.1	119.78	0.53	1.89	0.53	1.89	1			
5	144.1	122.02	0.52	1.91	0.52	1.92	0			
5	145.1	122.19	0.52	1.92	0.52	1.92	1			
5	146.1	123.49	0.52	1.92	0.52	1.92	0			
5	147.1	146.61	0.52	1.94	0.52	1.92	0			
5	148.1	73.14	0.52	1.93	0.52	1.92	0			
5	149.1	125.26	0.52	1.93	0.52	1.92	0			
5	151.1	136.37	0.52	1.93	0.52	1.92	0			
5	152.1	132.23	0.52	1.94	0.52	1.92	0			
5	153.1	133.9	0.52	1.92	0.52	1.92	0			
5	154.1	246.15	0.52	1.92	0.52	1.92	0			
5	155.1	249.08	0.52	1.91	0.52	1.91	1			
5	156.1	111.98	0.56	1.79	0.56	1.79	1			
5	157.1	115.61	0.56	1.77	0.56	1.77	1			
5	173.1	241.77	0.58	1.72	0.58	1.72	1			
5	188.1	246.04	0.49	2.04	0.49	2.04	1			
5	189.1	244.14	0.49	2.05	0.49	2.04	0			
5	192.1	243.08	0.49	2.05	0.49	2.04	0			
5	193.1	241.01	0.49	2.05	0.49	2.04	0			
5	194.1	244.01	0.48	2.07	0.49	2.04	0			
5	195.1	245.44	0.48	2.08	0.49	2.04	0			
5	196.1	248.05	0.48	2.10	0.49	2.04	0			
5	197.1	247.21	0.48	2.10	0.49	2.04	0			
5	198.1	265.26	0.47	2.12	0.49	2.04	0			
5	199.1	270.24	0.47	2.14	0.49	2.04	0			
5	200.1	271.97	0.47	2.13	0.49	2.04	0			
5	201.1	330.73	0.47	2.14	0.49	2.04	0			
5	202.1	280.91	0.47	2.14	0.49	2.04	0			
5	203.1	274.21	0.47	2.12	0.49	2.04	0			
5	205.1	467.83	0.50	1.99	0.50	1.99	1			
5	206.1	470	0.51	1.97	0.51	1.97	1			
5	207.1	471.34	0.51	1.96	0.51	1.97	0			
5	212.1	699.3	0.52	1.93	0.52	1.93	1			
5	213.1	702.73	0.51	1.94	0.52	1.93	0			
5	214.1	704.27	0.51	1.96	0.52	1.93	0			
5	215.1	202.67	0.45	2.21	0.46	2.20	0			
5	216.1	178.84	0.42	2.41	0.42	2.41	1			
5	217.1	201.43	0.44	2.29	0.44	2.27	0			
4	70.2	215.58	0.73	1.37	0.73	1.37	1			
4	72.2	219.15	0.65	1.54	0.65	1.54	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
4	74.2	0	.	0	0	.	74	0	0.69	0	25.86
4	75.2	0	.	0	0	3	75	0	0.69	0	25.86
4	76.2	0	.	0	0	.	76	0	0.35	2	25.86
4	100.2	1	0	1	0	2	103	0	1.04	1	87.93
4	101.2	1	0	0	0	1	103	0	0.69	2	87.93
4	102.2	0	1	1	0	2	103	0	1.39	0	87.93
4	103.2	1	.	1	0	3	103	0	0.35	1	87.93
4	104.2	0	0	1	0	2	103	0	1.04	2	87.93
4	105.2	0	0	1	0	2	103	0	1.04	2	87.93
4	106.2	0	1	0	0	2	216	0	1.04	0	158.80
4	107.2	0	0	0	0	2	216	0	0.69	1	158.80
4	108.2	0	0	1	0	2	216	0	1.39	1	158.80
4	109.2	0	0	0	0	1	216	0	1.39	1	158.80
4	110.2	1	1	1	0	2	216	0	1.39	0	158.80
4	111.2	0	1	0	0	2	216	0	1.39	1	158.80
4	112.2	1	1	0	0	2	216	0	1.73	1	158.80
4	113.2	1	.	0	0	3	113	0	0.35	2	158.80
4	114.2	0	0	1	0	1	113	0	1.04	2	158.80
5	192.2	0	1	0	0	2	193	0	0.69	1	25.86
5	193.2	1	.	1	0	1	193	0	0.35	2	25.86
5	194.2	1	1	0	0	1	193	0	1.04	2	25.86
5	195.2	1	0	1	0	2	193	0	1.39	1	25.86
5	196.2	1	0	1	0	1	193	0	1.73	2	25.86
5	197.2	1	0	0	0	2	193	0	1.39	1	25.86
5	215.2	0	1	1	0	2	113	0	0.69	1	153.94
5	216.2	1	.	0	1	.	216	0	0.35	2	153.94
5	217.2	0	0	1	0	1	113	0	1.39	1	153.94
4	100.3	1	.	1	0	2	100	0	0.69	1	25.86
4	101.3	1	0	0	0	1	103	0	0.69	2	25.86
4	102.3	0	1	1	0	2	100	0	0.69	2	25.86
4	103.3	1	.	1	0	3	103	0	0.35	1	25.86
4	104.3	0	0	1	0	2	100	0	1.04	2	25.86
4	105.3	0	0	1	0	2	100	0	1.04	2	25.86
4	106.3	0	1	0	0	2	216	0	0.69	1	96.73
4	107.3	0	0	0	0	2	216	0	1.04	1	96.73
4	108.3	0	0	1	0	2	216	0	1.39	1	96.73
4	109.3	0	0	0	0	1	216	0	1.39	1	96.73
4	110.3	1	1	1	0	2	216	0	1.39	0	96.73
4	111.3	0	1	0	0	1	216	0	1.39	1	96.73
4	112.3	1	1	0	0	2	216	0	1.39	1	96.73
4	113.3	1	.	0	0	3	113	0	0.35	2	96.73
4	114.3	0	0	1	0	1	113	0	1.39	2	96.73
5	215.3	0	1	1	0	2	113	0	1.04	1	91.88
5	216.3	1	.	0	1	.	216	0	0.69	2	91.88
5	217.3	0	0	1	0	1	113	0	0.69	1	91.88
6	39.01	1	.	1	0	.	39	0	0.43	1	1.60
6	41.01	1	0	1	0	1	39	0	0.86	2	1.60
6	44.01	1	.	1	0	1	44	1	0.64	2	1.60
6	45.01	1	0	0	0	1	44	1	0.86	1	1.60
6	46.01	0	.	0	0	2	46	1	1.07	1	11.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
4	74.2	217.92	0.65	1.54	0.65	1.54	1			
4	75.2	222.55	0.63	1.59	0.63	1.59	1			
4	76.2	228.13	0.65	1.54	0.65	1.54	1			
4	100.2	279.04	0.59	1.69	0.59	1.70	0			
4	101.2	275.71	0.59	1.69	0.59	1.70	0			
4	102.2	280.71	0.59	1.69	0.59	1.70	0			
4	103.2	273.07	0.59	1.70	0.59	1.70	1			
4	104.2	282.38	0.59	1.69	0.59	1.70	0			
4	105.2	284.31	0.59	1.70	0.59	1.70	0			
4	106.2	180.48	0.58	1.72	0.58	1.71	0			
4	107.2	182.08	0.58	1.72	0.58	1.71	0			
4	108.2	183.61	0.58	1.71	0.58	1.71	0			
4	109.2	184.58	0.58	1.72	0.58	1.71	0			
4	110.2	186.22	0.58	1.72	0.58	1.71	0			
4	111.2	187.92	0.58	1.72	0.58	1.71	0			
4	112.2	196.63	0.58	1.73	0.58	1.71	0			
4	113.2	199.6	0.61	1.64	0.61	1.64	1			
4	114.2	203.67	0.61	1.64	0.61	1.64	0			
5	192.2	243.08	0.57	1.74	0.56	1.78	0			
5	193.2	241.01	0.56	1.78	0.56	1.78	1			
5	194.2	244.01	0.57	1.76	0.56	1.78	0			
5	195.2	245.44	0.57	1.76	0.56	1.78	0			
5	196.2	248.05	0.56	1.78	0.56	1.78	0			
5	197.2	247.21	0.56	1.78	0.56	1.78	0			
5	215.2	202.67	0.61	1.64	0.61	1.64	0			
5	216.2	178.84	0.58	1.71	0.58	1.71	1			
5	217.2	201.43	0.60	1.66	0.61	1.64	0			
4	100.3	279.04	0.62	1.61	0.62	1.61	1			
4	101.3	275.71	0.61	1.64	0.60	1.66	0			
4	102.3	280.71	0.62	1.61	0.62	1.61	0			
4	103.3	273.07	0.60	1.66	0.60	1.66	1			
4	104.3	282.38	0.62	1.61	0.62	1.61	0			
4	105.3	284.31	0.62	1.61	0.62	1.61	0			
4	106.3	180.48	0.64	1.57	0.64	1.57	0			
4	107.3	182.08	0.64	1.57	0.64	1.57	0			
4	108.3	183.61	0.63	1.58	0.64	1.57	0			
4	109.3	184.58	0.63	1.58	0.64	1.57	0			
4	110.3	186.22	0.64	1.57	0.64	1.57	0			
4	111.3	187.92	0.63	1.58	0.64	1.57	0			
4	112.3	196.63	0.63	1.59	0.64	1.57	0			
4	113.3	199.6	0.59	1.71	0.59	1.71	1			
4	114.3	203.67	0.59	1.69	0.59	1.71	0			
5	215.3	202.67	0.59	1.70	0.59	1.71	0			
5	216.3	178.84	0.64	1.57	0.64	1.57	1			
5	217.3	201.43	0.57	1.75	0.59	1.71	0			
6	39.01	88.52	0.61	1.64	0.61	1.64	1	0	0	.
6	41.01	90.06	0.62	1.61	0.61	1.64	0		0	.
6	44.01	96.33	0.58	1.72	0.58	1.72	1	2	0	1.64
6	45.01	98.17	0.57	1.77	0.58	1.72	0		1	.
6	46.01	103.90	0.65	1.53	0.65	1.53	1	1	0	1.64

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	47.01	1	1	1	0	1	46	1	1.29	1	1.60
6	48.01	1	0	1	0	1	46	1	1.29	2	1.60
6	51.01	1	.	1	0	.	51	0	1.07	1	1.60
6	55.01	1	.	1	0	.	55	0	0.64	2	1.60
6	56.01	1	.	1	0	3	56	0	0.64	0	1.60
6	58.01	0	.	0	0	2	58	0	0.86	2	11.80
6	62.01	1	.	1	0	.	62	0	0.64	2	32.20
6	63.01	1	0	0	0	1	62	0	0.64	1	32.20
6	64.01	1	.	1	0	1	64	0	1.29	2	32.20
6	65.01	0	.	1	0	1	65	0	2.14	2	42.40
6	66.01	1	1	0	0	1	65	0	1.93	2	42.40
6	67.01	1	1	1	0	1	75	0	1.71	0	11.80
6	68.01	1	.	1	0	1	68	1	2.14	2	32.20
6	69.01	1	0	1	0	1	68	1	1.93	2	32.20
6	70.01	1	.	1	0	1	70	1	1.93	1	32.20
6	72.01	1	0	1	0	1	70	1	2.36	1	32.20
6	74.01	1	0	0	0	1	68	1	2.14	2	32.20
6	75.01	0	.	0	0	1	75	0	1.50	1	32.20
6	79.01	1	.	1	0	1	79	0	1.71	2	1.60
6	80.01	1	.	1	0	1	80	1	1.50	1	1.60
6	81.01	0	1	0	0	1	79	0	1.71	1	32.20
6	82.01	1	1	1	0	1	79	0	1.71	2	32.20
6	83.01	0	1	0	0	1	79	0	2.14	2	32.20
6	84.01	1	1	1	0	1	79	0	1.71	1	1.60
6	85.01	1	0	1	0	1	79	1	1.50	1	1.60
6	86.01	1	.	1	0	1	86	0	2.57	1	1.60
6	87.01	1	0	1	0	1	79	1	1.71	2	32.20
6	88.01	1	0	1	0	1	86	0	1.93	2	32.20
6	89.01	0	1	0	0	1	86	0	2.36	1	1.60
6	90.01	0	.	0	0	1	90	0	2.14	1	22.00
6	91.01	1	1	1	0	1	90	0	1.71	2	32.20
6	92.01	0	1	1	0	1	90	0	1.29	1	32.20
6	93.01	1	.	1	0	1	93	0	1.07	0	1.60
6	94.01	1	.	1	0	1	94	0	0.64	1	73.00
6	95.01	1	.	1	0	1	95	0	1.07	1	73.00
6	96.01	0	1	1	0	1	95	0	1.50	2	73.00
6	97.01	1	1	0	0	1	95	0	1.71	1	62.80
6	99.01	1	0	1	0	1	95	0	1.29	1	42.40
6	100.01	1	.	1	0	1	100	0	1.29	0	32.20
6	101.01	1	.	1	0	1	101	0	1.50	1	32.20
6	102.01	1	.	1	0	2	102	0	1.50	2	32.20
6	106.01	1	.	1	0	1	106	0	1.07	2	62.80
6	107.01	1	.	1	0	1	107	0	1.71	1	1.60
6	108.01	1	.	1	0	1	108	1	1.50	2	73.00
6	109.01	1	0	1	0	1	108	1	2.14	2	73.00
6	110.01	1	0	1	0	1	108	1	1.93	2	73.00
6	111.01	1	0	1	0	1	108	1	2.14	2	73.00
6	112.01	1	.	0	0	1	112	1	1.71	1	1.60
6	113.01	1	0	0	0	1	108	1	2.14	2	73.00
6	114.01	0	1	0	0	1	112	1	1.71	1	73.00

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	47.01	105.27	0.64	1.56	0.65	1.53	0		1	.
6	48.01	106.34	0.61	1.64	0.65	1.53	0		0	.
6	51.01	95.16	0.45	2.22	0.45	2.22	1	3	0	1.64
6	55.01	117.42	0.98	1.02	0.98	1.02	1	0	0	1.53
6	56.01	118.79	0.85	1.17	0.85	1.17	1	0	0	1.02
6	58.01	118.99	0.75	1.34	0.75	1.34	1	0	0	1.17
6	62.01	88.62	0.51	1.98	0.51	1.98	1	0	0	1.34
6	63.01	89.46	0.48	2.07	0.51	1.98	0		1	.
6	64.01	92.66	0.52	1.94	0.52	1.94	1	2	0	1.98
6	65.01	63.30	0.52	1.91	0.52	1.91	1	4	0	1.98
6	66.01	64.30	0.52	1.93	0.52	1.91	0		1	.
6	67.01	128.66	0.43	2.31	0.41	2.43	0		1	.
6	68.01	97.03	0.50	2.01	0.50	2.01	1	1	0	1.91
6	69.01	98.97	0.47	2.12	0.50	2.01	0		1	.
6	70.01	91.79	0.39	2.58	0.39	2.58	1	4	0	2.01
6	72.01	93.19	0.38	2.60	0.39	2.58	0		1	.
6	74.01	100.70	0.45	2.21	0.50	2.01	0		0	.
6	75.01	90.79	0.41	2.43	0.41	2.43	1	3	0	1.91
6	79.01	138.24	0.41	2.46	0.41	2.46	1	1	0	2.71
6	80.01	135.10	0.37	2.71	0.37	2.71	1	4	0	2.58
6	81.01	101.30	0.39	2.54	0.41	2.46	0		1	.
6	82.01	102.70	0.42	2.39	0.41	2.46	0		0	.
6	83.01	103.77	0.43	2.32	0.41	2.46	0		0	.
6	84.01	142.74	0.41	2.41	0.41	2.46	0		0	.
6	85.01	145.75	0.42	2.36	0.41	2.46	0		0	.
6	86.01	147.25	0.42	2.39	0.42	2.39	1	0	1	2.46
6	87.01	110.51	0.42	2.38	0.41	2.46	0		0	.
6	88.01	112.58	0.44	2.29	0.42	2.39	0		0	.
6	89.01	146.91	0.42	2.41	0.42	2.39	0		0	.
6	90.01	110.31	0.42	2.37	0.42	2.37	1	0	0	2.39
6	91.01	115.48	0.42	2.38	0.42	2.37	0		1	.
6	92.01	118.22	0.42	2.36	0.42	2.37	0		0	.
6	93.01	160.36	0.48	2.08	0.48	2.08	1	2	0	2.37
6	94.01	68.57	0.41	2.46	0.41	2.46	1	3	0	2.37
6	95.01	69.14	0.46	2.20	0.46	2.20	1	1	0	2.37
6	96.01	69.94	0.45	2.20	0.46	2.20	0		1	.
6	97.01	71.31	0.47	2.15	0.46	2.20	0		0	.
6	99.01	103.51	0.47	2.12	0.46	2.20	0		0	.
6	100.01	134.04	0.57	1.77	0.57	1.77	1	1	0	2.20
6	101.01	136.00	0.58	1.73	0.58	1.73	1	2	0	1.77
6	102.01	135.70	0.51	1.97	0.51	1.97	1	3	0	1.77
6	106.01	46.88	0.36	2.81	0.36	2.81	1	3	0	1.77
6	107.01	175.14	0.41	2.46	0.41	2.46	1	1	0	1.77
6	108.01	74.18	0.44	2.28	0.44	2.28	1	2	0	2.46
6	109.01	75.64	0.46	2.17	0.44	2.28	0		1	.
6	110.01	78.18	0.44	2.26	0.44	2.28	0		0	.
6	111.01	79.62	0.43	2.32	0.44	2.28	0		0	.
6	112.01	176.41	0.41	2.46	0.41	2.46	1	3	0	2.46
6	113.01	83.89	0.43	2.34	0.44	2.28	0		0	.
6	114.01	72.54	0.41	2.41	0.41	2.46	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trd	Grp	Flow Type	Den	Lane	Dist
6	115.01	1	1	1	0	1	112	1	1.93	1	32.20
6	116.01	0	1	0	0	1	108	1	2.36	2	73.00
6	117.01	1	0	1	0	1	112	1	1.93	1	42.40
6	118.01	0	1	0	0	1	112	1	2.14	1	62.80
6	119.01	1	0	1	0	1	112	1	2.57	1	42.40
6	120.01	1	1	1	0	1	108	1	1.50	2	83.20
6	121.01	0	0	0	0	2	112	1	2.14	1	32.20
6	122.01	1	1	1	0	1	112	1	2.14	1	32.20
6	123.01	0	1	0	0	1	108	1	1.50	2	73.00
6	124.01	1	1	1	0	1	112	1	1.93	1	32.20
6	125.01	1	1	1	0	1	108	1	1.93	2	83.20
6	126.01	0	1	0	0	2	112	1	1.93	1	32.20
6	128.01	0	1	1	0	1	112	1	1.93	1	62.80
6	129.01	1	1	1	0	1	112	1	1.93	1	83.20
6	130.01	0	1	0	0	1	108	1	1.50	2	62.80
6	131.01	1	.	0	0	1	131	0	1.29	2	83.20
6	132.01	1	.	1	0	1	132	0	1.93	1	11.80
6	133.01	1	0	1	0	1	135	0	1.29	1	11.80
6	135.01	1	.	1	0	1	135	0	1.71	2	42.40
6	136.01	1	0	0	0	1	135	0	1.93	1	1.60
6	137.01	0	1	0	0	1	135	0	1.71	1	11.80
6	138.01	1	0	1	0	1	135	0	2.14	2	42.40
6	139.01	0	0	0	0	1	135	0	2.36	1	11.80
6	140.01	0	0	0	0	1	135	0	1.93	2	83.20
6	141.01	0	0	0	0	1	135	0	1.71	2	83.20
6	142.01	1	.	1	0	1	142	0	1.50	2	32.20
6	143.01	1	1	1	0	1	135	0	1.29	1	124.01
6	144.01	1	.	1	0	1	144	0	1.07	1	124.01
6	145.01	0	.	1	0	1	145	0	1.50	2	124.01
6	146.01	1	1	1	0	1	145	0	0.86	2	83.20
6	147.01	0	0	1	0	1	145	0	1.50	1	32.20
6	148.01	1	0	1	0	1	145	0	1.29	2	113.80
6	149.01	1	.	1	0	1	149	1	1.71	2	42.40
6	150.01	1	0	1	0	2	145	0	1.07	1	42.40
6	151.01	1	0	1	0	1	149	1	1.50	2	62.80
6	152.01	1	0	0	0	1	145	0	1.50	1	1.60
6	153.01	1	0	1	0	1	145	0	1.71	2	93.40
6	154.01	1	.	1	0	1	154	1	1.29	1	11.80
6	155.01	1	0	1	0	1	154	1	1.71	1	42.40
6	156.01	1	0	1	0	2	154	1	1.50	1	42.40
6	159.01	1	0	0	0	1	154	1	1.50	1	42.40
6	160.01	0	1	1	0	1	149	1	1.29	2	73.00
6	161.01	1	.	1	0	1	161	1	1.71	1	1.60
6	162.01	0	1	0	0	1	161	1	1.50	1	1.60
6	163.01	0	0	1	0	1	161	1	1.29	1	32.20
6	164.01	1	.	1	1	1	164	1	1.50	2	1.60
6	165.01	1	0	1	0	1	164	1	1.50	2	73.00
6	166.01	0	.	0	0	1	166	0	1.71	2	73.00
6	167.01	1	1	1	0	1	166	0	1.71	1	11.80
6	168.01	1	0	1	0	1	166	0	1.50	1	11.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	115.01	141.44	0.41	2.47	0.41	2.46	0		0	.
6	116.01	81.25	0.43	2.30	0.44	2.28	0		0	.
6	117.01	105.21	0.40	2.52	0.41	2.46	0		0	.
6	118.01	74.18	0.39	2.54	0.41	2.46	0		0	.
6	119.01	108.38	0.39	2.54	0.41	2.46	0		0	.
6	120.01	68.30	0.41	2.44	0.44	2.28	0		0	.
6	121.01	148.25	0.39	2.58	0.41	2.46	0		0	.
6	122.01	149.02	0.38	2.61	0.41	2.46	0		0	.
6	123.01	95.03	0.41	2.41	0.44	2.28	0		0	.
6	124.01	153.69	0.38	2.63	0.41	2.46	0		0	.
6	125.01	71.27	0.40	2.47	0.44	2.28	0		0	.
6	126.01	151.55	0.37	2.69	0.41	2.46	0		0	.
6	128.01	94.56	0.38	2.67	0.41	2.46	0		0	.
6	129.01	69.80	0.39	2.59	0.41	2.46	0		0	.
6	130.01	96.17	0.41	2.44	0.44	2.28	0		0	.
6	131.01	72.74	0.43	2.30	0.43	2.30	1	3	0	2.46
6	132.01	202.97	0.50	2.00	0.50	2.00	1	2	0	2.46
6	133.01	202.50	0.51	1.97	0.49	2.05	0		1	.
6	135.01	129.40	0.49	2.05	0.49	2.05	1	1	0	2.46
6	136.01	206.94	0.49	2.05	0.49	2.05	0		0	.
6	137.01	208.04	0.48	2.09	0.49	2.05	0		0	.
6	138.01	130.67	0.50	2.01	0.49	2.05	0		0	.
6	139.01	211.18	0.49	2.03	0.49	2.05	0		0	.
6	140.01	73.77	0.50	2.02	0.49	2.05	0		0	.
6	141.01	75.01	0.50	2.01	0.49	2.05	0		0	.
6	142.01	174.88	0.56	1.77	0.56	1.77	1	2	0	2.05
6	143.01	37.39	0.51	1.95	0.49	2.05	0		0	.
6	144.01	38.28	0.51	1.94	0.51	1.94	1	3	0	2.05
6	145.01	40.68	0.53	1.88	0.53	1.88	1	1	0	2.05
6	146.01	82.58	0.56	1.78	0.53	1.88	0		0	.
6	147.01	177.18	0.56	1.78	0.53	1.88	0		1	.
6	148.01	63.19	0.58	1.73	0.53	1.88	0		0	.
6	149.01	149.12	0.54	1.85	0.54	1.85	1	2	0	1.88
6	150.01	134.60	0.50	1.99	0.53	1.88	0		0	.
6	151.01	115.58	0.55	1.82	0.54	1.85	0		1	.
6	152.01	228.03	0.50	1.99	0.53	1.88	0		0	.
6	153.01	87.79	0.55	1.83	0.53	1.88	0		0	.
6	154.01	226.96	0.46	2.19	0.46	2.19	1	3	0	1.88
6	155.01	135.60	0.45	2.21	0.46	2.19	0		0	.
6	156.01	140.14	0.44	2.27	0.46	2.19	0		0	.
6	159.01	138.31	0.44	2.25	0.46	2.19	0		0	.
6	160.01	118.82	0.47	2.15	0.54	1.85	0		0	.
6	161.01	235.04	0.43	2.31	0.43	2.31	1	2	0	1.88
6	162.01	240.04	0.45	2.23	0.43	2.31	0		1	.
6	163.01	196.90	0.46	2.19	0.43	2.31	0		0	.
6	164.01	238.31	0.41	2.44	0.41	2.44	1	3	0	1.88
6	165.01	120.79	0.41	2.41	0.41	2.44	0		1	.
6	166.01	121.96	0.42	2.41	0.42	2.41	1	1	0	1.88
6	167.01	245.85	0.45	2.24	0.42	2.41	0		1	.
6	168.01	246.98	0.44	2.26	0.42	2.41	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	169.01	1	0	1	0	1	166	0	1.93	2	93.40
6	170.01	0	1	1	0	1	166	0	1.71	1	11.80
6	171.01	1	1	1	0	1	166	0	1.71	2	124.01
6	172.01	1	0	0	0	2	166	0	1.07	2	42.40
6	173.01	0	1	0	0	2	166	0	0.86	0	113.80
6	174.01	1	1	1	0	1	166	0	0.86	2	124.01
6	175.01	1	0	1	0	1	166	0	1.29	0	124.01
6	176.01	1	0	1	0	1	166	0	1.29	2	124.01
6	177.01	1	0	0	0	1	166	0	1.71	2	124.01
6	178.01	0	0	0	0	1	166	0	1.93	2	144.41
6	179.01	1	0	1	0	1	166	0	1.29	1	124.01
6	180.01	0	1	1	0	1	166	0	1.71	1	124.01
6	181.01	0	1	1	0	1	166	0	1.29	2	93.40
6	182.01	1	1	1	0	1	166	0	1.71	1	93.40
6	183.01	1	.	1	0	2	183	0	1.29	1	73.00
6	184.01	1	0	1	0	1	183	0	1.29	2	83.20
6	185.01	1	0	0	0	1	183	0	0.86	1	83.20
6	186.01	1	0	1	0	1	183	0	1.29	2	124.01
6	187.01	1	0	1	0	2	183	0	0.86	2	144.41
6	188.01	1	0	1	1	1	183	0	0.86	2	93.40
6	189.01	1	0	1	0	2	183	0	0.86	2	124.01
6	190.01	1	0	1	0	2	183	0	1.07	2	93.40
6	191.01	1	0	0	1	2	183	0	1.07	2	93.40
6	192.01	1	0	1	0	1	183	0	1.50	2	93.40
6	193.01	1	0	1	0	1	183	0	1.07	1	62.80
6	194.01	1	0	1	0	1	183	0	1.50	1	83.20
6	195.01	1	0	1	0	2	183	0	1.50	1	62.80
6	196.01	1	0	1	0	1	183	0	1.71	2	113.80
6	197.01	1	0	1	0	1	183	0	1.50	0	113.80
6	198.01	1	0	1	0	1	183	0	1.93	1	93.40
6	199.01	1	0	1	0	1	183	0	2.14	2	113.80
6	200.01	1	0	1	0	1	183	0	1.93	2	113.80
6	201.01	1	0	1	0	1	183	0	2.36	1	93.40
6	202.01	1	0	0	0	1	183	0	2.14	1	93.40
6	203.01	1	0	1	0	1	183	0	1.71	2	93.40
6	204.01	1	0	1	0	1	183	0	1.29	2	62.80
6	205.01	1	0	0	0	1	183	0	1.07	1	11.80
6	206.01	0	0	0	0	1	183	0	1.29	1	11.80
6	207.01	0	1	0	0	1	183	0	1.29	2	11.80
6	208.01	0	0	0	0	1	183	0	1.50	1	32.20
6	209.01	1	1	1	0	1	183	0	1.50	2	32.20
6	210.01	1	0	1	0	1	183	0	1.29	0	11.80
6	211.01	1	1	0	0	1	183	0	1.71	1	124.01
6	212.01	0	.	1	0	1	212	0	2.36	1	124.01
6	213.01	0	1	0	0	1	183	0	2.36	2	124.01
6	214.01	0	0	0	0	1	212	0	2.36	0	124.01
6	215.01	1	0	1	0	1	212	0	1.50	0	62.80
6	216.01	1	1	1	0	1	212	0	2.57	2	62.80
6	217.01	0	0	0	0	1	212	0	1.71	1	11.80
6	218.01	0	1	1	0	2	212	0	1.50	1	11.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	169.01	90.99	0.44	2.28	0.42	2.41	0		0	.
6	170.01	247.98	0.46	2.17	0.42	2.41	0		0	.
6	171.01	48.95	0.46	2.17	0.42	2.41	0		0	.
6	172.01	164.83	0.46	2.17	0.42	2.41	0		0	.
6	173.01	79.27	0.47	2.15	0.42	2.41	0		0	.
6	174.01	55.19	0.48	2.10	0.42	2.41	0		0	.
6	175.01	61.63	0.45	2.21	0.42	2.41	0		0	.
6	176.01	62.50	0.46	2.17	0.42	2.41	0		0	.
6	177.01	63.67	0.46	2.19	0.42	2.41	0		0	.
6	178.01	64.80	0.45	2.20	0.42	2.41	0		0	.
6	179.01	47.82	0.45	2.20	0.42	2.41	0		0	.
6	180.01	53.52	0.45	2.22	0.42	2.41	0		0	.
6	181.01	117.98	0.45	2.21	0.42	2.41	0		0	.
6	182.01	114.75	0.45	2.24	0.42	2.41	0		0	.
6	183.01	146.22	0.45	2.23	0.45	2.23	1	0	0	2.41
6	184.01	124.19	0.44	2.29	0.45	2.23	0		1	.
6	185.01	123.16	0.44	2.26	0.45	2.23	0		0	.
6	186.01	65.57	0.47	2.11	0.45	2.23	0		0	.
6	187.01	68.81	0.48	2.09	0.45	2.23	0		0	.
6	188.01	128.49	0.48	2.10	0.45	2.23	0		0	.
6	189.01	68.97	0.48	2.09	0.45	2.23	0		0	.
6	190.01	133.23	0.47	2.12	0.45	2.23	0		0	.
6	191.01	132.63	0.44	2.28	0.45	2.23	0		0	.
6	192.01	134.77	0.46	2.18	0.45	2.23	0		0	.
6	193.01	164.47	0.42	2.41	0.45	2.23	0		0	.
6	194.01	134.07	0.43	2.34	0.45	2.23	0		0	.
6	195.01	165.37	0.44	2.26	0.45	2.23	0		0	.
6	196.01	100.73	0.44	2.25	0.45	2.23	0		0	.
6	197.01	99.96	0.45	2.24	0.45	2.23	0		0	.
6	198.01	137.50	0.45	2.20	0.45	2.23	0		0	.
6	199.01	103.36	0.44	2.29	0.45	2.23	0		0	.
6	200.01	104.20	0.44	2.28	0.45	2.23	0		0	.
6	201.01	139.61	0.44	2.29	0.45	2.23	0		0	.
6	202.01	140.54	0.45	2.24	0.45	2.23	0		0	.
6	203.01	143.08	0.44	2.29	0.45	2.23	0		0	.
6	204.01	179.11	0.44	2.30	0.45	2.23	0		0	.
6	205.01	305.57	0.42	2.40	0.45	2.23	0		0	.
6	206.01	307.44	0.43	2.32	0.45	2.23	0		0	.
6	207.01	308.81	0.45	2.23	0.45	2.23	0		0	.
6	208.01	254.86	0.32	3.13	0.45	2.23	0		0	.
6	209.01	256.59	0.33	3.06	0.45	2.23	0		0	.
6	210.01	312.31	0.32	3.09	0.45	2.23	0		0	.
6	211.01	70.78	0.33	3.06	0.45	2.23	0		0	.
6	212.01	72.98	0.33	3.04	0.33	3.04	1	1	0	2.23
6	213.01	75.91	0.34	2.98	0.45	2.23	0		0	.
6	214.01	77.65	0.36	2.77	0.33	3.04	0		1	.
6	215.01	181.28	0.34	2.97	0.33	3.04	0		0	.
6	216.01	180.12	0.34	2.96	0.33	3.04	0		0	.
6	217.01	322.56	0.34	2.95	0.33	3.04	0		0	.
6	218.01	321.76	0.34	2.98	0.33	3.04	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	219.01	0	0	0	0	1	212	0	1.71	2	103.60
6	220.01	0	0	0	0	1	212	0	1.71	2	103.60
6	221.01	0	0	0	0	1	212	0	1.50	1	11.80
6	222.01	0	0	1	0	1	212	0	1.71	2	103.60
6	223.01	0	0	0	0	1	212	0	1.71	1	124.01
6	224.01	1	1	1	0	2	212	0	1.29	1	93.40
6	225.01	1	0	1	0	1	212	0	1.71	2	73.00
6	226.01	1	.	1	0	1	226	0	1.07	1	1.60
6	227.01	1	0	1	0	1	226	0	1.29	2	1.60
6	228.01	1	.	1	0	1	228	0	1.29	2	73.00
6	229.01	1	0	1	0	1	228	0	1.07	1	73.00
6	230.01	0	1	0	0	1	228	0	1.29	1	73.00
6	231.01	0	0	0	0	1	228	0	1.50	1	124.01
6	232.01	0	0	0	1	1	228	0	1.71	2	124.01
6	233.01	1	1	1	0	1	228	0	1.71	0	124.01
6	234.01	0	1	0	0	1	228	0	1.50	2	124.01
6	235.01	1	0	1	0	1	228	0	1.93	1	93.40
6	236.01	0	0	0	0	1	228	0	1.71	1	93.40
6	237.01	0	0	1	0	1	228	0	1.71	2	124.01
6	238.01	1	1	1	0	1	228	0	1.71	1	124.01
6	239.01	0	1	1	0	1	228	0	2.14	2	124.01
6	240.01	1	1	1	0	1	228	0	2.57	1	103.60
6	241.01	0	1	0	0	1	228	0	2.36	2	124.01
6	242.01	0	0	0	0	1	228	0	1.93	2	124.01
6	243.01	0	0	1	0	1	228	0	1.93	1	144.41
6	244.01	1	1	1	0	1	228	0	1.93	2	124.01
6	245.01	0	0	0	0	1	228	0	1.93	1	124.01
6	246.01	0	1	0	0	1	228	0	1.93	1	144.41
6	247.01	0	0	0	0	1	228	0	2.36	1	124.01
6	248.01	0	0	0	0	1	228	0	2.14	1	144.41
6	249.01	1	1	1	0	1	228	0	2.79	1	144.41
6	250.01	0	0	1	0	1	228	0	2.14	2	124.01
6	251.01	0	0	0	0	1	228	0	2.36	2	124.01
6	252.01	0	1	0	0	1	228	0	2.14	1	144.41
6	253.01	1	0	1	0	1	228	0	2.14	1	144.41
6	254.01	1	1	1	0	1	228	0	2.36	2	144.41
6	255.01	0	0	0	0	1	228	0	1.93	2	144.41
6	256.01	0	0	0	0	1	228	0	2.36	1	124.01
6	257.01	0	1	0	0	1	228	0	2.36	2	144.41
6	258.01	1	1	1	0	1	228	0	1.71	1	124.01
6	259.01	1	0	1	0	2	228	0	1.50	1	124.01
6	260.01	1	0	1	0	1	228	0	1.50	1	124.01
6	261.01	0	1	1	0	1	228	0	1.29	1	144.41
6	262.01	1	1	1	0	1	228	0	1.29	2	93.40
6	263.01	0	1	1	0	1	228	0	1.71	1	124.01
6	264.01	1	1	0	0	1	228	0	1.71	2	144.41
6	265.01	1	0	1	0	1	228	0	1.50	1	144.41
6	266.01	1	0	1	0	1	228	0	1.93	2	144.41
6	267.01	0	1	1	0	1	228	0	1.71	1	124.01
6	268.01	1	1	1	0	1	228	0	1.93	2	124.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	219.01	112.74	0.34	2.93	0.33	3.04	0		0	.
6	220.01	109.04	0.34	2.98	0.33	3.04	0		0	.
6	221.01	325.29	0.32	3.11	0.33	3.04	0		0	.
6	222.01	113.94	0.34	2.95	0.33	3.04	0		0	.
6	223.01	73.51	0.32	3.10	0.33	3.04	0		0	.
6	224.01	153.12	0.32	3.09	0.33	3.04	0		0	.
6	225.01	192.53	0.32	3.10	0.33	3.04	0		0	.
6	226.01	334.67	0.31	3.25	0.31	3.25	1	0	0	3.04
6	227.01	336.34	0.31	3.24	0.31	3.25	0		1	.
6	228.01	195.90	0.31	3.21	0.31	3.21	1	0	0	3.25
6	229.01	193.86	0.31	3.25	0.31	3.21	0		1	.
6	230.01	196.67	0.31	3.27	0.31	3.21	0		0	.
6	231.01	78.85	0.31	3.18	0.31	3.21	0		0	.
6	232.01	80.75	0.32	3.11	0.31	3.21	0		0	.
6	233.01	82.49	0.34	2.95	0.31	3.21	0		0	.
6	234.01	83.22	0.42	2.36	0.31	3.21	0		0	.
6	235.01	158.29	0.43	2.33	0.31	3.21	0		0	.
6	236.01	161.39	0.42	2.37	0.31	3.21	0		0	.
6	237.01	86.89	0.43	2.31	0.31	3.21	0		0	.
6	238.01	84.59	0.43	2.31	0.31	3.21	0		0	.
6	239.01	93.30	0.43	2.30	0.31	3.21	0		0	.
6	240.01	123.92	0.44	2.29	0.31	3.21	0		0	.
6	241.01	98.40	0.44	2.28	0.31	3.21	0		0	.
6	242.01	97.27	0.46	2.17	0.31	3.21	0		0	.
6	243.01	90.43	0.44	2.30	0.31	3.21	0		0	.
6	244.01	95.10	0.43	2.33	0.31	3.21	0		0	.
6	245.01	101.74	0.43	2.30	0.31	3.21	0		0	.
6	246.01	98.40	0.44	2.27	0.31	3.21	0		0	.
6	247.01	91.80	0.43	2.31	0.31	3.21	0		0	.
6	248.01	105.08	0.44	2.30	0.31	3.21	0		0	.
6	249.01	106.34	0.43	2.30	0.31	3.21	0		0	.
6	250.01	105.98	0.43	2.34	0.31	3.21	0		0	.
6	251.01	108.28	0.41	2.41	0.31	3.21	0		0	.
6	252.01	112.38	0.43	2.33	0.31	3.21	0		0	.
6	253.01	113.78	0.43	2.32	0.31	3.21	0		0	.
6	254.01	116.25	0.43	2.31	0.31	3.21	0		0	.
6	255.01	121.79	0.44	2.28	0.31	3.21	0		0	.
6	256.01	120.69	0.43	2.34	0.31	3.21	0		0	.
6	257.01	119.86	0.45	2.22	0.31	3.21	0		0	.
6	258.01	111.08	0.44	2.30	0.31	3.21	0		0	.
6	259.01	112.95	0.43	2.31	0.31	3.21	0		0	.
6	260.01	99.74	0.44	2.28	0.31	3.21	0		0	.
6	261.01	118.46	0.44	2.26	0.31	3.21	0		0	.
6	262.01	191.22	0.43	2.30	0.31	3.21	0		0	.
6	263.01	119.29	0.44	2.26	0.31	3.21	0		0	.
6	264.01	125.33	0.43	2.33	0.31	3.21	0		0	.
6	265.01	123.63	0.42	2.39	0.31	3.21	0		0	.
6	266.01	126.73	0.42	2.39	0.31	3.21	0		0	.
6	267.01	128.87	0.41	2.44	0.31	3.21	0		0	.
6	268.01	127.70	0.42	2.41	0.31	3.21	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	269.01	1	0	0	0	1	228	0	2.36	1	93.40
6	270.01	1	0	1	0	1	228	0	2.14	2	144.41
6	271.01	0	1	0	0	1	228	0	2.14	1	93.40
6	272.01	1	1	1	0	2	228	0	2.14	1	144.41
6	273.01	1	0	0	0	1	228	0	2.14	2	124.01
6	274.01	0	1	1	0	1	228	0	1.93	1	124.01
6	275.01	1	.	1	0	1	275	1	2.36	2	144.41
6	276.01	1	.	1	0	1	276	1	1.93	1	144.41
6	277.01	1	0	1	0	1	275	1	2.36	2	195.41
6	278.01	1	0	1	0	1	276	1	2.14	1	113.80
6	279.01	1	0	1	0	1	275	1	2.36	2	144.41
6	280.01	0	1	0	0	1	276	1	2.36	1	113.80
6	281.01	1	0	1	0	1	275	1	2.14	2	144.41
6	282.01	1	0	1	0	1	275	1	1.93	2	144.41
6	283.01	0	0	1	0	1	276	1	2.14	1	124.01
6	284.01	1	1	1	0	1	276	1	1.93	1	226.01
6	285.01	1	0	1	1	1	275	1	1.50	2	175.01
6	286.01	0	1	0	0	1	276	1	1.50	1	32.20
6	287.01	1	.	0	0	1	287	0	1.50	1	175.01
6	288.01	1	0	1	0	1	287	0	1.50	2	175.01
6	289.01	1	0	1	0	2	287	0	1.50	1	164.81
6	290.01	0	1	0	0	1	287	0	1.50	1	93.40
6	291.01	1	0	1	0	1	287	0	1.50	1	62.80
6	292.01	1	1	1	0	1	287	0	1.50	2	164.81
6	293.01	1	0	1	0	2	287	0	1.93	1	124.01
6	294.01	1	1	1	0	1	287	0	1.93	1	164.81
6	295.01	0	1	1	0	1	287	0	1.29	2	124.01
6	296.01	0	0	1	0	1	287	0	1.50	2	195.41
6	297.01	0	1	0	0	1	287	0	1.71	1	164.81
6	298.01	1	0	1	0	1	287	0	1.29	2	185.21
6	299.01	1	1	1	0	1	287	0	1.50	1	62.80
6	300.01	1	0	1	0	2	287	0	0.86	2	164.81
6	301.01	1	.	0	0	1	301	1	1.29	2	144.41
6	302.01	1	0	1	0	1	301	1	1.71	2	144.41
6	303.01	1	1	0	0	1	301	1	2.14	2	164.81
6	304.01	1	0	1	0	1	301	1	1.71	2	144.41
6	305.01	1	0	0	0	1	311	1	2.14	1	164.81
6	306.01	0	1	0	0	1	301	1	2.14	2	144.41
6	307.01	0	.	0	0	1	307	1	1.93	0	164.81
6	308.01	1	.	0	0	1	308	0	1.93	0	164.81
6	309.01	0	.	1	0	1	309	0	2.14	2	144.41
6	310.01	1	.	1	0	1	310	0	2.14	1	144.41
6	311.01	1	.	1	0	1	311	1	1.07	1	62.80
6	312.01	1	1	1	0	1	311	1	2.14	1	103.60
6	313.01	1	0	1	0	1	311	1	1.29	1	124.01
6	314.01	0	1	0	0	1	311	1	1.71	1	124.01
6	315.01	1	.	1	0	2	315	0	1.29	2	164.81
6	316.01	0	1	1	0	1	315	0	1.29	2	226.01
6	317.01	1	.	1	0	1	317	0	1.71	2	144.41
6	318.01	1	.	1	0	1	318	0	1.50	1	124.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	269.01	198.40	0.41	2.45	0.31	3.21	0		0	.
6	270.01	132.70	0.39	2.57	0.31	3.21	0		0	.
6	271.01	199.93	0.38	2.61	0.31	3.21	0		0	.
6	272.01	131.37	0.38	2.64	0.31	3.21	0		0	.
6	273.01	130.67	0.38	2.66	0.31	3.21	0		0	.
6	274.01	133.34	0.38	2.62	0.31	3.21	0		0	.
6	275.01	135.61	0.38	2.64	0.38	2.64	1	3	0	3.21
6	276.01	137.27	0.39	2.58	0.39	2.58	1	2	0	3.21
6	277.01	55.73	0.38	2.61	0.38	2.64	0		1	.
6	278.01	177.64	0.39	2.53	0.39	2.58	0		1	.
6	279.01	140.41	0.38	2.63	0.38	2.64	0		0	.
6	280.01	180.74	0.41	2.46	0.39	2.58	0		0	.
6	281.01	139.28	0.39	2.58	0.38	2.64	0		0	.
6	282.01	142.01	0.38	2.64	0.38	2.64	0		0	.
6	283.01	134.87	0.41	2.43	0.39	2.58	0		0	.
6	284.01	44.25	0.41	2.44	0.39	2.58	0		0	.
6	285.01	86.55	0.38	2.61	0.38	2.64	0		0	.
6	286.01	352.12	0.42	2.38	0.39	2.58	0		0	.
6	287.01	91.15	0.43	2.32	0.43	2.32	1	1	0	3.21
6	288.01	88.85	0.42	2.36	0.43	2.32	0		1	.
6	289.01	86.12	0.42	2.37	0.43	2.32	0		0	.
6	290.01	240.57	0.43	2.33	0.43	2.32	0		0	.
6	291.01	280.18	0.43	2.31	0.43	2.32	0		0	.
6	292.01	89.26	0.44	2.28	0.43	2.32	0		0	.
6	293.01	167.57	0.44	2.28	0.43	2.32	0		0	.
6	294.01	83.71	0.44	2.29	0.43	2.32	0		0	.
6	295.01	139.78	0.44	2.27	0.43	2.32	0		0	.
6	296.01	61.50	0.46	2.19	0.43	2.32	0		0	.
6	297.01	87.35	0.43	2.33	0.43	2.32	0		0	.
6	298.01	75.88	0.45	2.22	0.43	2.32	0		0	.
6	299.01	262.20	0.43	2.32	0.43	2.32	0		0	.
6	300.01	98.69	0.43	2.30	0.43	2.32	0		0	.
6	301.01	165.57	0.44	2.26	0.44	2.26	1	2	0	2.32
6	302.01	167.10	0.45	2.23	0.44	2.26	0		1	.
6	303.01	103.47	0.48	2.10	0.44	2.26	0		0	.
6	304.01	169.11	0.47	2.14	0.44	2.26	0		0	.
6	305.01	102.37	0.36	2.77	0.34	2.92	0		0	.
6	306.01	172.08	0.45	2.20	0.44	2.26	0		0	.
6	307.01	104.40	0.44	2.26	0.44	2.26	1	2	0	2.32
6	308.01	100.73	0.40	2.52	0.40	2.52	1	1	0	2.32
6	309.01	192.20	0.41	2.47	0.41	2.47	1	3	0	2.52
6	310.01	188.96	0.43	2.34	0.43	2.34	1	2	0	2.52
6	311.01	282.08	0.34	2.92	0.34	2.92	1	3	0	2.32
6	312.01	218.21	0.35	2.85	0.34	2.92	0		0	.
6	313.01	170.21	0.35	2.83	0.34	2.92	0		1	.
6	314.01	171.68	0.35	2.84	0.34	2.92	0		0	.
6	315.01	106.37	0.41	2.46	0.41	2.46	1	1	0	2.52
6	316.01	45.88	0.41	2.42	0.41	2.46	0		1	.
6	317.01	186.22	0.42	2.41	0.42	2.41	1	1	0	2.46
6	318.01	183.42	0.38	2.60	0.38	2.60	1	3	0	2.41

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	319.01	1	0	1	0	1	320	0	1.93	0	124.01
6	320.01	1	.	1	0	1	320	0	1.29	1	124.01
6	321.01	1	.	0	0	2	321	0	1.71	2	144.41
6	322.01	1	0	1	0	1	321	0	1.71	1	144.41
6	323.01	1	0	1	0	1	321	0	1.07	2	195.41
6	324.01	1	0	1	0	2	321	0	1.50	1	144.41
6	325.01	0	0	0	0	1	321	0	1.50	2	164.81
6	326.01	0	1	0	0	1	321	0	1.29	1	144.41
6	327.01	1	1	1	0	1	321	0	1.07	2	164.81
6	328.01	0	0	1	0	1	321	0	1.93	1	144.41
6	329.01	1	0	1	0	2	321	0	0.86	2	144.41
6	330.01	1	1	1	0	2	321	0	0.86	1	124.01
6	331.01	0	1	0	0	1	321	0	1.07	2	124.01
6	332.01	0	1	0	0	1	321	0	1.50	1	144.41
6	333.01	1	0	0	0	1	321	0	1.71	1	164.81
6	334.01	1	1	1	0	1	321	0	2.14	2	164.81
6	335.01	1	0	1	0	1	321	0	1.71	1	144.41
6	336.01	1	0	1	0	1	321	0	1.93	2	144.41
6	337.01	1	0	1	0	1	321	0	1.71	2	144.41
6	338.01	1	0	1	0	1	321	0	1.50	1	113.80
6	339.01	1	0	1	0	1	321	0	1.71	2	144.41
6	340.01	1	0	1	0	1	321	0	1.71	1	144.41
6	341.01	0	0	1	0	1	321	0	1.71	2	226.01
6	342.01	0	1	1	0	1	321	0	1.93	0	144.41
6	343.01	1	1	0	0	1	321	0	1.50	1	144.41
6	344.01	0	0	0	0	1	321	0	1.50	1	175.01
6	345.01	0	1	1	0	1	321	0	1.29	2	175.01
6	346.01	1	1	1	0	1	321	0	1.93	0	164.81
6	347.01	1	.	1	0	1	347	1	1.93	1	144.41
6	348.01	1	0	1	0	1	347	1	1.93	1	226.01
6	349.01	0	1	0	0	1	347	1	1.71	1	226.01
6	350.01	0	.	0	0	1	350	1	2.14	2	175.01
6	351.01	0	1	1	0	1	350	1	1.93	2	144.41
6	352.01	0	0	1	1	1	350	1	2.14	2	164.81
6	353.01	1	.	1	0	1	350	1	2.14	2	144.41
6	354.01	1	0	1	0	1	363	0	1.93	2	226.01
6	355.01	1	1	1	0	1	350	1	2.14	2	144.41
6	356.01	1	0	1	0	1	350	1	1.50	2	144.41
6	357.01	1	1	0	0	1	347	1	1.93	1	144.41
6	358.01	1	1	1	0	1	363	0	1.71	2	113.80
6	359.01	1	0	0	0	1	347	1	1.71	1	144.41
6	360.01	1	0	1	0	1	363	0	1.93	1	144.41
6	361.01	1	0	1	0	1	347	1	1.50	1	144.41
6	362.01	1	0	1	0	1	363	0	1.50	1	144.41
6	363.01	0	.	0	0	1	363	0	1.50	1	144.41
6	364.01	0	0	0	0	1	363	0	1.71	2	113.80
6	365.01	0	1	1	0	1	363	0	1.93	1	124.01
6	366.01	1	1	1	0	1	363	0	1.93	2	144.41
6	367.01	0	0	0	0	1	363	0	1.93	1	185.21
6	368.01	0	1	0	0	2	363	0	1.29	0	185.21

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	319.01	185.36	0.41	2.42	0.39	2.57	0		1	.
6	320.01	185.39	0.39	2.57	0.39	2.57	1	1	0	2.41
6	321.01	190.26	0.39	2.54	0.39	2.54	1	0	0	2.57
6	322.01	185.62	0.42	2.39	0.39	2.54	0		1	.
6	323.01	87.06	0.40	2.47	0.39	2.54	0		0	.
6	324.01	190.72	0.40	2.47	0.39	2.54	0		0	.
6	325.01	108.49	0.40	2.48	0.39	2.54	0		0	.
6	326.01	194.83	0.40	2.49	0.39	2.54	0		0	.
6	327.01	110.07	0.40	2.52	0.39	2.54	0		0	.
6	328.01	196.57	0.40	2.51	0.39	2.54	0		0	.
6	329.01	202.77	0.40	2.47	0.39	2.54	0		0	.
6	330.01	198.04	0.40	2.50	0.39	2.54	0		0	.
6	331.01	201.71	0.40	2.50	0.39	2.54	0		0	.
6	332.01	198.30	0.42	2.38	0.39	2.54	0		0	.
6	333.01	113.21	0.43	2.34	0.39	2.54	0		0	.
6	334.01	112.04	0.41	2.43	0.39	2.54	0		0	.
6	335.01	214.89	0.41	2.44	0.39	2.54	0		0	.
6	336.01	217.09	0.41	2.43	0.39	2.54	0		0	.
6	337.01	219.29	0.42	2.38	0.39	2.54	0		0	.
6	338.01	185.61	0.42	2.38	0.39	2.54	0		0	.
6	339.01	207.81	0.42	2.36	0.39	2.54	0		0	.
6	340.01	203.14	0.42	2.39	0.39	2.54	0		0	.
6	341.01	51.95	0.45	2.20	0.39	2.54	0		0	.
6	342.01	205.34	0.45	2.24	0.39	2.54	0		0	.
6	343.01	211.08	0.45	2.24	0.39	2.54	0		0	.
6	344.01	114.71	0.45	2.24	0.39	2.54	0		0	.
6	345.01	114.94	0.42	2.37	0.39	2.54	0		0	.
6	346.01	117.78	0.44	2.27	0.39	2.54	0		0	.
6	347.01	231.57	0.45	2.22	0.45	2.22	1	3	0	2.54
6	348.01	56.39	0.47	2.14	0.45	2.22	0		1	.
6	349.01	54.46	0.48	2.10	0.45	2.22	0		0	.
6	350.01	119.68	0.49	2.06	0.49	2.06	1	2	0	2.54
6	351.01	238.08	0.49	2.03	0.49	2.06	0		0	.
6	352.01	124.62	0.50	2.00	0.49	2.06	0		1	.
6	353.01	228.77	0.49	2.04	0.49	2.06	1	0	0	.
6	354.01	55.02	0.48	2.07	0.49	2.04	0		0	.
6	355.01	237.64	0.51	1.96	0.49	2.06	0		0	.
6	356.01	240.58	0.51	1.97	0.49	2.06	0		0	.
6	357.01	213.48	0.44	2.27	0.45	2.22	0		0	.
6	358.01	317.78	0.49	2.04	0.49	2.04	0		1	.
6	359.01	215.92	0.45	2.20	0.45	2.22	0		0	.
6	360.01	230.10	0.48	2.07	0.49	2.04	0		0	.
6	361.01	216.59	0.46	2.16	0.45	2.22	0		0	.
6	362.01	237.71	0.46	2.19	0.49	2.04	0		0	.
6	363.01	221.89	0.46	2.16	0.49	2.04	1	1	0	2.54
6	364.01	316.31	0.46	2.17	0.49	2.04	0		0	.
6	365.01	88.39	0.46	2.18	0.49	2.04	0		0	.
6	366.01	253.06	0.47	2.12	0.49	2.04	0		0	.
6	367.01	94.90	0.46	2.19	0.49	2.04	0		0	.
6	368.01	89.39	0.47	2.11	0.49	2.04	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	369.01	1	1	1	0	1	363	0	1.29	2	144.41
6	370.01	0	1	1	0	1	363	0	0.86	1	124.01
6	371.01	0	0	0	0	1	363	0	1.71	1	144.41
6	372.01	1	0	1	0	1	363	0	1.71	0	226.01
6	373.01	1	1	0	0	1	363	0	1.71	2	226.01
6	374.01	1	0	1	0	1	363	0	1.71	1	226.01
6	375.01	0	1	1	0	1	363	0	1.93	2	226.01
6	376.01	1	1	0	0	1	363	0	1.93	1	226.01
6	377.01	1	0	0	0	1	363	0	2.36	0	226.01
6	378.01	1	0	1	0	1	363	0	2.14	2	185.21
6	379.01	0	1	1	0	1	363	0	1.93	1	195.41
6	380.01	0	0	1	0	1	363	0	1.50	0	113.80
6	381.01	0	0	1	0	1	363	0	1.07	1	226.01
6	382.01	1	1	1	0	1	363	0	1.29	2	226.01
6	383.01	1	.	1	0	1	383	0	1.29	0	144.41
6	384.01	1	.	1	0	1	384	0	1.07	2	144.41
6	385.01	1	0	1	0	1	384	0	1.50	2	42.40
6	386.01	1	.	1	0	2	386	1	1.71	2	144.41
6	387.01	1	0	1	0	1	386	1	2.14	2	144.41
6	388.01	1	0	1	0	1	386	1	2.36	2	205.61
6	389.01	0	0	1	0	1	392	1	1.71	1	246.41
6	390.01	0	1	1	0	1	386	1	2.14	2	144.41
6	391.01	1	0	1	0	1	386	1	1.71	2	205.61
6	392.01	1	.	0	0	1	392	1	1.07	1	144.41
6	393.01	0	0	0	0	2	392	1	1.93	1	205.61
6	394.01	0	1	0	0	1	392	1	1.07	1	205.61
6	395.01	0	0	0	0	1	392	1	2.14	1	124.01
6	396.01	0	0	1	0	1	392	1	1.93	1	226.01
6	397.01	0	0	0	0	1	392	1	1.93	1	195.41
6	398.01	0	0	1	0	1	392	1	1.93	1	144.41
6	399.01	1	.	1	0	1	399	0	1.29	2	175.01
6	400.01	1	0	1	0	1	399	0	0.64	2	175.01
6	401.01	0	1	0	0	1	399	0	0.86	0	175.01
6	402.01	0	0	1	0	1	399	0	0.86	0	175.01
6	403.01	0	0	1	0	1	399	0	0.86	2	195.41
6	404.01	1	.	1	0	1	404	0	0.86	1	144.41
6	405.01	1	.	1	0	1	405	0	1.29	2	144.41
6	406.01	0	.	1	0	1	406	0	1.29	1	226.01
6	407.01	1	0	1	0	1	406	0	1.29	1	226.01
6	408.01	1	1	1	0	1	406	0	1.50	2	215.81
6	409.01	1	.	1	0	.	409	0	0.43	1	226.01
6	410.01	1	.	1	0	1	410	0	0.64	2	215.81
6	411.01	0	.	1	0	1	411	0	0.64	0	215.81
6	412.01	1	.	1	0	1	412	0	1.07	2	185.21
6	413.01	1	0	1	0	1	412	0	0.64	2	185.21
6	414.01	1	.	1	0	1	414	1	1.50	2	185.21
6	415.01	1	0	1	0	1	414	1	1.71	2	256.61
6	416.01	1	.	1	0	1	416	0	1.50	1	144.41
6	417.01	0	1	1	0	1	416	0	1.50	1	226.01
6	418.01	0	0	1	0	2	416	0	1.71	1	226.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	369.01	231.80	0.47	2.11	0.49	2.04	0		0	.
6	370.01	90.13	0.47	2.12	0.49	2.04	0		0	.
6	371.01	241.28	0.47	2.12	0.49	2.04	0		0	.
6	372.01	51.35	0.46	2.16	0.49	2.04	0		0	.
6	373.01	50.85	0.49	2.05	0.49	2.04	0		0	.
6	374.01	53.62	0.48	2.10	0.49	2.04	0		0	.
6	375.01	49.18	0.49	2.05	0.49	2.04	0		0	.
6	376.01	57.79	0.48	2.08	0.49	2.04	0		0	.
6	377.01	57.39	0.49	2.03	0.49	2.04	0		0	.
6	378.01	93.06	0.51	1.98	0.49	2.04	0		0	.
6	379.01	94.70	0.49	2.06	0.49	2.04	0		0	.
6	380.01	201.53	0.50	1.98	0.49	2.04	0		0	.
6	381.01	60.20	0.51	1.97	0.49	2.04	0		0	.
6	382.01	59.33	0.50	2.01	0.49	2.04	0		0	.
6	383.01	248.19	0.55	1.83	0.55	1.83	1	2	0	1.74
6	384.01	250.85	0.57	1.74	0.57	1.74	1	1	0	2.16
6	385.01	477.21	0.57	1.76	0.57	1.74	0		1	.
6	386.01	276.01	0.51	1.94	0.51	1.94	1	2	0	1.74
6	387.01	273.18	0.51	1.95	0.51	1.94	0		1	.
6	388.01	81.08	0.50	1.99	0.51	1.94	0		0	.
6	389.01	30.19	0.39	2.59	0.38	2.62	0		0	.
6	390.01	282.69	0.45	2.22	0.51	1.94	0		0	.
6	391.01	84.72	0.46	2.17	0.51	1.94	0		0	.
6	392.01	224.86	0.38	2.62	0.38	2.62	1	3	0	1.74
6	393.01	86.75	0.41	2.42	0.38	2.62	0		0	.
6	394.01	83.01	0.39	2.56	0.38	2.62	0		1	.
6	395.01	256.46	0.39	2.57	0.38	2.62	0		0	.
6	396.01	66.80	0.39	2.54	0.38	2.62	0		0	.
6	397.01	125.06	0.39	2.54	0.38	2.62	0		0	.
6	398.01	287.59	0.42	2.39	0.38	2.62	0		0	.
6	399.01	156.52	0.45	2.22	0.45	2.22	1	1	0	1.74
6	400.01	158.59	0.46	2.19	0.45	2.22	0		1	.
6	401.01	160.32	0.46	2.17	0.45	2.22	0		0	.
6	402.01	161.96	0.45	2.22	0.45	2.22	0		0	.
6	403.01	128.60	0.48	2.09	0.45	2.22	0		0	.
6	404.01	305.98	0.59	1.70	0.59	1.70	1	2	0	2.22
6	405.01	304.21	0.53	1.88	0.53	1.88	1	3	0	2.22
6	406.01	72.11	0.56	1.78	0.56	1.78	1	1	0	2.22
6	407.01	69.80	0.55	1.81	0.56	1.78	0		0	.
6	408.01	104.13	0.56	1.80	0.56	1.78	0		1	.
6	409.01	70.44	0.56	1.78	0.56	1.78	1	0	0	1.78
6	410.01	107.87	0.62	1.61	0.62	1.61	1	1	0	1.78
6	411.01	110.87	0.64	1.57	0.64	1.57	1	1	0	1.61
6	412.01	145.48	0.47	2.13	0.47	2.13	1	0	0	1.57
6	413.01	148.35	0.47	2.11	0.47	2.13	0		0	.
6	414.01	148.75	0.47	2.13	0.47	2.13	1	2	0	2.13
6	415.01	67.46	0.48	2.08	0.47	2.13	0		1	.
6	416.01	321.39	0.35	2.84	0.35	2.84	1	1	0	2.13
6	417.01	77.45	0.36	2.82	0.35	2.84	0		1	.
6	418.01	73.64	0.40	2.51	0.35	2.84	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	419.01	0	0	0	0	1	416	0	1.93	0	226.01
6	420.01	0	0	1	0	2	416	0	1.71	1	226.01
6	421.01	1	1	0	0	1	416	0	1.71	2	185.21
6	422.01	1	0	1	0	1	416	0	1.93	1	215.81
6	423.01	1	0	1	0	1	416	0	1.71	1	185.21
6	424.01	1	0	1	0	1	416	0	2.36	2	215.81
6	425.01	0	1	1	0	1	416	0	2.14	1	215.81
6	426.01	1	.	0	0	1	426	1	0.64	1	113.80
6	427.01	1	0	1	0	1	426	1	0.86	1	113.80
6	428.01	1	1	1	0	1	416	0	2.14	2	215.81
6	429.01	0	0	1	0	1	416	0	2.57	1	226.01
6	430.01	1	0	1	0	2	416	0	2.14	1	83.20
6	431.01	0	1	0	0	1	416	0	1.71	1	124.01
6	432.01	0	.	1	0	2	432	1	1.71	1	205.61
6	433.01	1	1	1	0	1	432	1	1.50	1	205.61
6	434.01	1	0	1	1	1	432	1	1.50	0	226.01
6	435.01	1	1	1	0	2	437	1	1.93	2	205.61
6	436.01	1	0	1	0	1	416	0	1.93	2	215.81
6	437.01	0	.	0	0	1	437	1	1.50	2	215.81
6	438.01	1	.	1	1	.	438	0	0.43	0	215.81
6	439.01	1	1	1	0	1	440	0	0.86	1	215.81
6	440.01	0	.	1	0	2	440	0	0.64	2	226.01
6	441.01	0	1	1	0	2	440	0	0.86	1	226.01
6	442.01	1	1	1	0	1	440	0	1.07	1	226.01
6	443.01	0	1	1	0	1	440	0	0.86	2	226.01
6	444.01	1	1	0	0	2	440	0	1.29	1	42.40
6	445.01	0	.	1	0	2	445	0	0.86	0	226.01
6	446.01	1	1	1	0	2	445	0	1.29	1	215.81
6	447.01	0	0	0	0	1	445	0	1.29	2	215.81
6	448.01	0	1	1	0	1	445	0	1.29	1	205.61
6	449.01	0	0	0	0	1	445	0	1.71	2	205.61
6	450.01	1	1	1	0	1	445	0	1.29	1	226.01
6	451.01	0	1	1	0	2	445	0	1.71	0	226.01
6	452.01	1	1	1	0	1	445	0	1.50	1	246.41
6	453.01	1	1	1	0	1	445	0	1.71	1	246.41
6	454.01	0	1	1	0	1	445	0	2.14	2	215.81
6	455.01	1	1	1	0	1	445	0	1.93	1	246.41
6	456.01	0	.	1	0	1	456	0	1.71	1	205.61
6	457.01	0	1	1	0	1	445	0	1.50	2	215.81
6	458.01	1	0	1	0	1	456	0	2.14	1	215.81
6	459.01	1	1	1	0	1	456	0	1.71	2	246.41
6	460.01	1	0	0	0	1	456	0	2.14	1	246.41
6	461.01	0	1	1	0	2	456	0	2.14	1	226.01
6	462.01	0	.	1	0	3	462	0	2.36	1	226.01
6	463.01	1	.	1	1	3	463	0	2.14	0	226.01
6	464.01	1	0	0	0	1	463	0	2.14	1	226.01
6	465.01	0	0	0	1	1	462	0	1.93	2	246.41
6	466.01	0	0	1	0	2	462	0	1.93	1	175.01
6	467.01	0	.	0	0	1	467	1	1.50	1	144.41
6	468.01	1	.	1	0	1	468	1	1.29	2	144.41

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	419.01	74.91	0.39	2.58	0.35	2.84	0		0	.
6	420.01	79.21	0.39	2.54	0.35	2.84	0		0	.
6	421.01	169.64	0.41	2.46	0.35	2.84	0		0	.
6	422.01	131.23	0.41	2.47	0.35	2.84	0		0	.
6	423.01	168.32	0.40	2.48	0.35	2.84	0		0	.
6	424.01	144.78	0.41	2.43	0.35	2.84	0		0	.
6	425.01	140.90	0.41	2.47	0.35	2.84	0		0	.
6	426.01	310.84	0.35	2.88	0.35	2.88	1	3	0	2.13
6	427.01	312.77	0.35	2.89	0.35	2.88	0		1	.
6	428.01	140.14	0.43	2.32	0.35	2.84	0		0	.
6	429.01	84.32	0.41	2.46	0.35	2.84	0		0	.
6	430.01	451.68	0.43	2.34	0.35	2.84	0		0	.
6	431.01	353.86	0.42	2.35	0.35	2.84	0		0	.
6	432.01	132.13	0.42	2.36	0.42	2.36	1	3	0	2.84
6	433.01	129.16	0.42	2.39	0.42	2.36	0		1	.
6	434.01	80.98	0.43	2.33	0.42	2.36	0		0	.
6	435.01	147.34	0.43	2.31	0.44	2.29	0		1	.
6	436.01	123.82	0.43	2.34	0.35	2.84	0		0	.
6	437.01	142.87	0.44	2.29	0.44	2.29	1	2	0	2.84
6	438.01	126.46	0.39	2.59	0.39	2.59	1	0	0	2.84
6	439.01	121.62	0.42	2.40	0.39	2.59	0		1	.
6	440.01	66.27	0.39	2.59	0.39	2.59	1	0	0	2.59
6	441.01	90.66	0.41	2.46	0.39	2.59	0		0	.
6	442.01	95.70	0.41	2.45	0.39	2.59	0		0	.
6	443.01	88.36	0.39	2.54	0.39	2.59	0		0	.
6	444.01	590.09	0.39	2.55	0.39	2.59	0		0	.
6	445.01	93.33	0.39	2.59	0.39	2.59	1	0	0	2.59
6	446.01	127.99	0.40	2.52	0.39	2.59	0		0	.
6	447.01	129.19	0.39	2.54	0.39	2.59	0		1	.
6	448.01	152.22	0.39	2.55	0.39	2.59	0		0	.
6	449.01	150.51	0.39	2.57	0.39	2.59	0		0	.
6	450.01	97.70	0.39	2.58	0.39	2.59	0		0	.
6	451.01	100.27	0.41	2.45	0.39	2.59	0		0	.
6	452.01	69.03	0.41	2.42	0.39	2.59	0		0	.
6	453.01	70.27	0.39	2.59	0.39	2.59	0		0	.
6	454.01	157.32	0.39	2.55	0.39	2.59	0		0	.
6	455.01	75.20	0.36	2.79	0.39	2.59	0		0	.
6	456.01	163.96	0.34	2.95	0.34	2.95	1	1	0	2.59
6	457.01	183.31	0.36	2.79	0.39	2.59	0		0	.
6	458.01	163.19	0.32	3.11	0.34	2.95	0		0	.
6	459.01	72.17	0.30	3.28	0.34	2.95	0		1	.
6	460.01	73.70	0.32	3.11	0.34	2.95	0		0	.
6	461.01	93.83	0.32	3.09	0.34	2.95	0		0	.
6	462.01	104.24	0.33	3.02	0.33	3.02	1	0	0	3.16
6	463.01	102.20	0.32	3.16	0.32	3.16	1	0	0	2.95
6	464.01	102.20	0.33	3.03	0.32	3.16	0		1	.
6	465.01	77.54	0.33	3.02	0.33	3.02	0		1	.
6	466.01	294.86	0.33	3.03	0.33	3.02	0		0	.
6	467.01	427.73	0.34	2.94	0.34	2.94	1	2	0	3.02
6	468.01	424.43	0.31	3.22	0.31	3.22	1	3	0	3.02

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	469.01	1	0	1	0	1	468	1	1.29	2	256.61
6	470.01	1	0	1	0	1	468	1	1.07	2	256.61
6	471.01	1	1	1	0	1	467	1	1.50	1	215.81
6	472.01	0	0	0	0	1	467	1	1.50	1	215.81
6	473.01	1	0	1	0	1	467	1	1.93	1	175.01
6	474.01	1	0	1	0	1	468	1	1.07	2	256.61
6	475.01	0	1	1	0	1	468	1	1.93	2	83.20
6	476.01	1	0	1	0	1	467	1	2.14	1	226.01
6	477.01	1	1	1	0	1	468	1	1.93	2	256.61
6	478.01	1	0	1	0	1	468	1	1.71	2	226.01
6	479.01	0	1	0	0	1	467	1	1.71	1	175.01
6	480.01	0	0	1	0	1	467	1	2.14	1	124.01
6	481.01	1	.	1	0	1	481	1	1.50	2	226.01
6	482.01	1	.	1	0	1	482	1	1.93	1	236.21
6	483.01	1	0	1	0	1	481	1	1.50	2	256.61
6	484.01	1	0	1	0	1	481	1	1.50	0	256.61
6	485.01	1	.	1	0	1	485	0	1.07	2	256.61
6	486.01	1	0	1	0	1	481	1	1.71	2	256.61
6	487.01	1	0	1	0	2	485	0	0.86	0	256.61
6	488.01	1	0	1	0	1	485	0	1.07	1	256.61
6	489.01	0	1	1	0	1	485	0	1.29	2	256.61
6	490.01	1	.	1	0	2	490	0	0.86	1	226.01
6	491.01	0	0	1	0	1	485	0	0.86	2	226.01
6	492.01	1	0	1	0	1	490	0	1.29	1	226.01
6	493.01	1	.	1	0	1	493	0	1.71	1	226.01
6	494.01	0	.	0	0	1	494	0	1.71	2	226.01
6	495.01	1	.	1	0	1	495	1	1.93	1	226.01
6	496.01	1	0	1	0	1	495	1	1.71	1	226.01
6	497.01	0	.	1	0	1	497	1	1.93	2	226.01
6	498.01	0	.	1	0	.	498	0	0.43	2	226.01
6	499.01	1	1	1	1	1	497	1	1.71	2	215.81
6	500.01	1	.	1	0	1	500	0	1.71	1	215.81
6	501.01	0	1	1	0	1	500	0	1.29	2	195.41
6	502.01	1	0	1	0	1	500	0	1.29	2	256.61
6	503.01	1	1	1	0	2	500	0	1.29	1	226.01
6	504.01	1	0	1	0	1	500	0	1.29	1	236.21
6	505.01	1	.	1	0	1	505	0	1.29	2	215.81
6	506.01	1	.	1	0	1	506	0	1.50	1	236.21
6	507.01	0	1	0	0	1	506	0	1.50	1	236.21
6	508.01	0	.	0	0	2	508	0	1.29	2	215.81
6	509.01	1	0	1	0	1	510	0	1.29	1	144.41
6	510.01	1	.	1	0	1	510	0	1.50	2	144.41
6	511.01	0	.	1	0	2	511	0	1.07	0	205.61
6	512.01	1	.	0	0	.	512	0	0.43	2	144.41
6	513.01	0	.	1	0	.	513	0	0.43	0	11.80
6	62.02	1	.	1	0	.	62	0	0.64	2	11.80
6	63.02	1	0	0	0	1	62	0	0.64	1	11.80
6	64.02	1	.	1	0	1	64	1	1.50	2	11.80
6	65.02	0	1	1	0	1	64	1	1.93	2	22.00
6	66.02	1	1	0	0	1	64	1	1.50	2	22.00

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	469.01	93.42	0.31	3.18	0.31	3.22	0		1	.
6	470.01	95.02	0.32	3.15	0.31	3.22	0		0	.
6	471.01	184.62	0.35	2.87	0.34	2.94	0		0	.
6	472.01	183.35	0.34	2.90	0.34	2.94	0		1	.
6	473.01	326.92	0.36	2.78	0.34	2.94	0		0	.
6	474.01	97.26	0.32	3.16	0.31	3.22	0		0	.
6	475.01	529.16	0.33	3.03	0.31	3.22	0		0	.
6	476.01	145.65	0.39	2.59	0.34	2.94	0		0	.
6	477.01	100.33	0.32	3.09	0.31	3.22	0		0	.
6	478.01	137.17	0.33	3.06	0.31	3.22	0		0	.
6	479.01	336.53	0.48	2.06	0.34	2.94	0		0	.
6	480.01	460.03	0.48	2.10	0.34	2.94	0		0	.
6	481.01	134.24	0.33	3.05	0.33	3.05	1	3	0	3.02
6	482.01	154.89	0.36	2.81	0.36	2.81	1	2	0	3.02
6	483.01	109.27	0.31	3.24	0.33	3.05	0		0	.
6	484.01	106.97	0.32	3.12	0.33	3.05	0		1	.
6	485.01	108.17	0.32	3.11	0.32	3.11	1	1	0	3.02
6	486.01	101.80	0.31	3.20	0.33	3.05	0		0	.
6	487.01	111.47	0.32	3.11	0.32	3.11	0		0	.
6	488.01	114.24	0.32	3.14	0.32	3.11	0		0	.
6	489.01	115.18	0.31	3.18	0.32	3.11	0		0	.
6	490.01	141.31	0.23	4.32	0.23	4.32	1	0	0	3.11
6	491.01	151.72	0.23	4.33	0.32	3.11	0		0	.
6	492.01	149.82	0.23	4.32	0.23	4.32	0		0	.
6	493.01	171.01	0.23	4.32	0.23	4.32	1	3	0	4.32
6	494.01	169.54	0.24	4.18	0.24	4.18	1	2	0	4.32
6	495.01	175.61	0.25	4.08	0.25	4.08	1	2	0	4.32
6	496.01	178.61	0.25	4.00	0.25	4.08	0		1	.
6	497.01	180.88	0.24	4.16	0.24	4.16	1	3	0	4.32
6	498.01	82.68	0.38	2.63	0.38	2.63	1	0	0	2.98
6	499.01	244.17	0.24	4.16	0.24	4.16	0		1	.
6	500.01	252.18	0.25	4.08	0.25	4.08	1	1	0	4.32
6	501.01	409.05	0.24	4.14	0.25	4.08	0		0	.
6	502.01	203.53	0.24	4.22	0.25	4.08	0		0	.
6	503.01	233.50	0.24	4.19	0.25	4.08	0		1	.
6	504.01	351.62	0.24	4.25	0.25	4.08	0		0	.
6	505.01	377.94	0.29	3.49	0.29	3.49	1	2	0	4.08
6	506.01	350.59	0.24	4.12	0.24	4.12	1	3	0	4.08
6	507.01	354.03	0.26	3.91	0.24	4.12	0		1	.
6	508.01	377.57	0.32	3.16	0.32	3.16	1	2	0	4.08
6	509.01	560.73	0.33	3.04	0.34	2.98	0		1	.
6	510.01	563.10	0.34	2.98	0.34	2.98	1	1	0	4.08
6	511.01	250.01	0.26	3.80	0.26	3.80	1	3	0	2.98
6	512.01	748.35	0.47	2.12	0.47	2.12	1	0	0	2.63
6	513.01	1178.05	0.82	1.22	0.82	1.22	1	0	0	2.12
6	62.02	88.62	0.54	1.84	0.54	1.84	1	0	0	.
6	63.02	89.46	0.58	1.73	0.54	1.84	0		0	.
6	64.02	92.66	0.58	1.72	0.58	1.72	1	2	0	1.84
6	65.02	63.30	0.58	1.72	0.58	1.72	0		1	.
6	66.02	64.30	0.58	1.73	0.58	1.72	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	68.02	1	.	1	0	1	68	0	1.50	1	11.80
6	69.02	1	0	1	0	1	68	0	1.29	0	11.80
6	70.02	1	.	1	0	1	70	1	1.50	1	11.80
6	72.02	1	0	1	0	1	70	1	1.71	1	11.80
6	74.02	1	.	0	0	1	74	0	1.50	2	11.80
6	75.02	0	1	0	0	1	62	0	1.07	0	11.80
6	81.02	0	.	0	0	1	81	0	1.50	1	11.80
6	82.02	1	1	1	0	1	81	0	1.50	2	11.80
6	83.02	0	.	0	0	1	83	0	1.71	1	11.80
6	87.02	1	.	1	0	1	87	0	1.29	2	11.80
6	88.02	1	.	1	0	1	88	0	1.50	2	11.80
6	90.02	0	.	0	0	1	90	0	1.50	1	1.60
6	91.02	1	.	1	0	2	91	0	1.29	2	11.80
6	92.02	0	1	1	0	2	91	0	0.86	0	11.80
6	94.02	1	.	1	0	1	94	0	0.64	1	52.60
6	95.02	1	.	1	0	1	95	0	0.86	1	52.60
6	96.02	0	1	1	0	1	95	0	1.29	0	52.60
6	97.02	1	1	0	0	2	95	0	1.29	1	42.40
6	99.02	1	0	1	0	1	95	0	1.07	0	22.00
6	100.02	1	.	1	0	1	100	0	1.07	1	11.80
6	101.02	1	0	1	0	1	100	0	1.29	1	11.80
6	102.02	1	0	1	0	1	100	0	1.07	2	11.80
6	106.02	1	.	1	0	.	106	0	0.43	2	42.40
6	108.02	1	.	1	0	1	108	0	1.29	2	52.60
6	109.02	1	1	1	0	1	108	0	2.14	2	52.60
6	110.02	1	0	1	0	1	108	0	1.71	2	52.60
6	111.02	1	0	1	0	1	108	0	2.14	2	52.60
6	113.02	1	.	0	0	1	113	1	2.14	2	52.60
6	114.02	0	1	0	0	1	108	0	1.29	1	52.60
6	115.02	1	0	1	0	1	108	0	1.71	1	11.80
6	116.02	0	.	0	0	1	116	1	1.93	2	52.60
6	117.02	1	0	1	0	1	108	0	1.93	1	22.00
6	118.02	0	.	0	0	1	118	1	1.93	1	42.40
6	119.02	1	0	1	0	1	108	0	2.36	1	22.00
6	120.02	1	1	1	0	1	116	1	1.50	2	62.80
6	121.02	0	.	0	0	1	121	1	1.93	1	11.80
6	122.02	1	1	1	0	1	121	1	1.93	1	11.80
6	123.02	0	1	0	0	1	116	1	1.29	2	52.60
6	124.02	1	1	1	0	1	121	1	1.50	1	11.80
6	125.02	1	0	1	0	1	129	0	1.50	2	62.80
6	126.02	0	1	0	0	1	121	1	1.93	1	11.80
6	128.02	0	.	1	0	2	128	1	1.71	1	42.40
6	129.02	1	.	1	0	1	129	0	1.50	1	62.80
6	130.02	0	1	0	0	1	129	0	1.07	2	42.40
6	131.02	1	1	0	0	1	129	0	0.86	2	62.80
6	135.02	1	.	1	0	1	135	1	1.07	2	22.00
6	138.02	1	0	1	0	1	135	1	1.71	2	22.00
6	140.02	0	.	0	0	1	140	0	1.50	0	62.80
6	141.02	0	.	0	0	1	141	0	1.29	2	62.80
6	142.02	1	0	1	0	1	141	0	1.29	0	11.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	68.02	97.03	0.56	1.78	0.56	1.78	1	1	0	1.84
6	69.02	98.97	0.56	1.79	0.56	1.78	0		1	.
6	70.02	91.79	0.51	1.94	0.51	1.94	1	3	0	1.84
6	72.02	93.19	0.52	1.93	0.51	1.94	0		1	.
6	74.02	100.70	0.54	1.86	0.54	1.86	1	4	0	1.78
6	75.02	90.79	0.55	1.82	0.54	1.84	0		0	.
6	81.02	101.30	0.53	1.90	0.53	1.90	1	4	0	1.86
6	82.02	102.70	0.51	1.94	0.53	1.90	0		1	.
6	83.02	103.77	0.51	1.96	0.51	1.96	1	4	0	1.90
6	87.02	110.51	0.55	1.82	0.55	1.82	1	1	0	1.96
6	88.02	112.58	0.55	1.82	0.55	1.82	1	2	0	1.82
6	90.02	110.31	0.49	2.05	0.49	2.05	1	3	0	1.82
6	91.02	115.48	0.53	1.87	0.53	1.87	1	1	0	1.82
6	92.02	118.22	0.53	1.90	0.53	1.87	0		1	.
6	94.02	68.57	0.70	1.42	0.70	1.42	1	1	0	1.87
6	95.02	69.14	0.63	1.59	0.63	1.59	1	4	0	1.42
6	96.02	69.94	0.65	1.53	0.63	1.59	0		1	.
6	97.02	71.31	0.63	1.58	0.63	1.59	0		0	.
6	99.02	103.51	0.60	1.66	0.63	1.59	0		0	.
6	100.02	134.04	0.56	1.78	0.56	1.78	1	1	0	1.59
6	101.02	136.00	0.56	1.77	0.56	1.78	0		0	.
6	102.02	135.70	0.56	1.77	0.56	1.78	0		1	.
6	106.02	46.88	0.48	2.09	0.48	2.09	1	3	0	1.59
6	108.02	74.18	0.54	1.86	0.54	1.86	1	2	0	1.78
6	109.02	75.64	0.51	1.95	0.54	1.86	0		0	.
6	110.02	78.18	0.51	1.95	0.54	1.86	0		0	.
6	111.02	79.62	0.51	1.95	0.54	1.86	0		0	.
6	113.02	83.89	0.54	1.84	0.54	1.84	1	2	0	1.78
6	114.02	72.54	0.50	2.00	0.54	1.86	0		1	.
6	115.02	141.44	0.51	1.95	0.54	1.86	0		0	.
6	116.02	81.25	0.53	1.88	0.53	1.88	1	2	0	1.78
6	117.02	105.21	0.52	1.91	0.54	1.86	0		0	.
6	118.02	74.18	0.51	1.97	0.51	1.97	1	3	0	1.78
6	119.02	108.38	0.52	1.92	0.54	1.86	0		0	.
6	120.02	68.30	0.51	1.95	0.53	1.88	0		1	.
6	121.02	148.25	0.50	1.98	0.50	1.98	1	3	0	1.78
6	122.02	149.02	0.50	1.99	0.50	1.98	0		1	.
6	123.02	95.03	0.53	1.89	0.53	1.88	0		0	.
6	124.02	153.69	0.51	1.97	0.50	1.98	0		0	.
6	125.02	71.27	0.52	1.92	0.52	1.94	0		1	.
6	126.02	151.55	0.51	1.97	0.50	1.98	0		0	.
6	128.02	94.56	0.51	1.95	0.51	1.95	1	3	0	1.78
6	129.02	69.80	0.52	1.94	0.52	1.94	1	1	0	1.78
6	130.02	96.17	0.51	1.95	0.52	1.94	0		0	.
6	131.02	72.74	0.49	2.04	0.52	1.94	0		0	.
6	135.02	129.40	0.47	2.14	0.47	2.14	1	1	0	1.94
6	138.02	130.67	0.46	2.17	0.47	2.14	0		1	.
6	140.02	73.77	0.46	2.19	0.46	2.19	1	4	0	2.14
6	141.02	75.01	0.45	2.24	0.45	2.24	1	4	0	2.19
6	142.02	174.88	0.44	2.25	0.45	2.24	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	143.02	1	1	1	0	1	141	0	1.07	2	103.60
6	144.02	1	0	1	0	1	141	0	0.86	2	103.60
6	145.02	0	1	1	0	1	141	0	1.07	2	103.60
6	146.02	1	1	1	0	1	141	0	0.86	2	62.80
6	147.02	0	0	1	0	1	141	0	1.50	1	11.80
6	148.02	1	.	1	0	1	148	0	1.29	2	93.40
6	149.02	1	0	1	0	1	153	1	1.71	2	22.00
6	150.02	1	.	1	0	2	150	0	0.86	1	22.00
6	151.02	1	.	1	0	1	151	1	1.71	0	42.40
6	153.02	1	.	1	0	1	153	1	1.93	2	73.00
6	155.02	1	.	1	0	1	155	1	1.50	1	22.00
6	156.02	1	0	1	0	1	155	1	1.71	1	22.00
6	159.02	1	0	0	0	1	155	1	1.50	1	22.00
6	160.02	0	.	1	0	1	160	1	0.86	2	52.60
6	163.02	0	.	1	0	1	163	0	1.29	1	11.80
6	165.02	1	.	1	0	2	165	0	1.29	2	52.60
6	166.02	0	.	0	0	1	166	0	1.07	2	52.60
6	169.02	1	1	1	0	1	169	0	1.50	2	73.00
6	171.02	1	0	1	0	1	171	0	1.07	2	103.60
6	172.02	1	0	0	0	1	171	0	1.07	2	22.00
6	173.02	0	1	0	0	2	171	0	0.86	0	93.40
6	174.02	1	1	1	0	1	171	0	0.86	2	103.60
6	175.02	1	0	1	0	1	171	0	1.07	0	103.60
6	176.02	1	0	1	0	1	171	0	1.29	2	103.60
6	177.02	1	0	0	0	1	171	0	1.50	2	103.60
6	178.02	0	0	0	0	1	171	0	1.93	2	124.01
6	179.02	1	0	1	0	1	171	0	1.07	1	103.60
6	180.02	0	1	1	0	1	171	0	1.50	1	103.60
6	181.02	0	1	1	0	1	171	0	1.29	0	73.00
6	182.02	1	1	1	0	1	171	0	1.50	1	73.00
6	183.02	1	.	1	0	2	183	0	0.86	1	52.60
6	184.02	1	0	1	0	2	183	0	1.29	2	62.80
6	185.02	1	0	0	0	1	183	0	0.86	1	62.80
6	186.02	1	0	1	0	1	183	0	0.86	2	103.60
6	187.02	1	0	1	0	1	183	0	0.86	2	124.01
6	188.02	1	0	1	1	1	183	0	0.86	2	73.00
6	189.02	1	0	1	0	1	183	0	0.86	2	103.60
6	190.02	1	0	1	0	1	183	0	1.07	2	73.00
6	191.02	1	0	0	1	2	183	0	1.07	2	73.00
6	192.02	1	0	1	0	1	183	0	1.71	2	73.00
6	193.02	1	0	1	0	1	183	0	1.29	1	42.40
6	194.02	1	0	1	0	1	183	0	1.07	1	62.80
6	195.02	1	0	1	0	2	183	0	1.07	1	42.40
6	196.02	1	0	1	0	1	183	0	1.50	2	93.40
6	197.02	1	0	1	0	1	183	0	1.29	0	93.40
6	198.02	1	0	1	0	1	183	0	1.71	1	73.00
6	199.02	1	0	1	0	1	183	0	2.14	2	93.40
6	200.02	1	.	1	0	1	200	0	1.93	2	93.40
6	201.02	1	.	1	0	1	201	0	1.93	1	73.00
6	202.02	1	.	0	0	1	202	0	2.14	1	73.00

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	143.02	37.39	0.44	2.26	0.45	2.24	0		1	.
6	144.02	38.28	0.44	2.26	0.45	2.24	0		0	.
6	145.02	40.68	0.45	2.24	0.45	2.24	0		0	.
6	146.02	82.58	0.44	2.28	0.45	2.24	0		0	.
6	147.02	177.18	0.44	2.28	0.45	2.24	0		0	.
6	148.02	63.19	0.47	2.11	0.47	2.11	1	2	0	2.20
6	149.02	149.12	0.49	2.05	0.48	2.10	0		1	.
6	150.02	134.60	0.45	2.20	0.45	2.20	1	1	0	2.24
6	151.02	115.58	0.46	2.18	0.46	2.18	1	2	0	2.20
6	153.02	87.79	0.48	2.10	0.48	2.10	1	2	0	2.20
6	155.02	135.60	0.42	2.40	0.42	2.40	1	3	0	2.20
6	156.02	140.14	0.42	2.37	0.42	2.40	0		0	.
6	159.02	138.31	0.42	2.38	0.42	2.40	0		1	.
6	160.02	118.82	0.45	2.23	0.45	2.23	1	1	0	2.20
6	163.02	196.90	0.43	2.32	0.43	2.32	1	2	0	2.40
6	165.02	120.79	0.42	2.40	0.42	2.40	1	4	0	2.23
6	166.02	121.96	0.41	2.42	0.41	2.42	1	3	0	2.40
6	169.02	90.99	0.40	2.48	0.40	2.48	0		1	2.40
6	171.02	48.95	0.39	2.57	0.39	2.57	0		0	2.48
6	172.02	164.83	0.39	2.57	0.39	2.57	0		1	.
6	173.02	79.27	0.38	2.62	0.39	2.57	0		0	.
6	174.02	55.19	0.38	2.63	0.39	2.57	0		0	.
6	175.02	61.63	0.38	2.62	0.39	2.57	0		0	.
6	176.02	62.50	0.39	2.59	0.39	2.57	0		0	.
6	177.02	63.67	0.38	2.62	0.39	2.57	0		0	.
6	178.02	64.80	0.38	2.61	0.39	2.57	0		0	.
6	179.02	47.82	0.39	2.57	0.39	2.57	0		0	.
6	180.02	53.52	0.39	2.59	0.39	2.57	0		0	.
6	181.02	117.98	0.39	2.59	0.39	2.57	0		0	.
6	182.02	114.75	0.39	2.59	0.39	2.57	0		0	.
6	183.02	146.22	0.39	2.59	0.39	2.59	1	1	0	2.57
6	184.02	124.19	0.39	2.57	0.39	2.59	0		1	.
6	185.02	123.16	0.39	2.58	0.39	2.59	0		0	.
6	186.02	65.57	0.38	2.64	0.39	2.59	0		0	.
6	187.02	68.81	0.37	2.67	0.39	2.59	0		0	.
6	188.02	128.49	0.38	2.63	0.39	2.59	0		0	.
6	189.02	68.97	0.38	2.61	0.39	2.59	0		0	.
6	190.02	133.23	0.39	2.59	0.39	2.59	0		0	.
6	191.02	132.63	0.39	2.57	0.39	2.59	0		0	.
6	192.02	134.77	0.39	2.59	0.39	2.59	0		0	.
6	193.02	164.47	0.39	2.55	0.39	2.59	0		0	.
6	194.02	134.07	0.39	2.58	0.39	2.59	0		0	.
6	195.02	165.37	0.40	2.50	0.39	2.59	0		0	.
6	196.02	100.73	0.40	2.51	0.39	2.59	0		0	.
6	197.02	99.96	0.40	2.50	0.39	2.59	0		0	.
6	198.02	137.50	0.40	2.50	0.39	2.59	0		0	.
6	199.02	103.36	0.40	2.49	0.39	2.59	0		0	.
6	200.02	104.20	0.40	2.51	0.40	2.51	1	3	0	2.59
6	201.02	139.61	0.41	2.44	0.41	2.44	1	2	0	2.59
6	202.02	140.54	0.40	2.47	0.40	2.47	1	1	0	2.59

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	203.02	1	0	1	0	1	202	0	1.71	2	73.00
6	204.02	1	0	1	0	1	202	0	1.29	2	42.40
6	208.02	0	.	0	0	1	208	0	1.50	1	11.80
6	209.02	1	1	1	0	1	208	0	1.29	2	11.80
6	211.02	1	.	0	0	1	211	0	1.71	1	103.60
6	212.02	0	.	1	0	1	212	0	1.93	1	103.60
6	213.02	0	.	0	0	1	213	0	2.14	2	103.60
6	214.02	0	0	0	0	1	212	0	2.14	1	103.60
6	215.02	1	.	1	0	1	215	1	1.93	1	42.40
6	216.02	1	.	1	0	1	216	1	1.71	0	42.40
6	219.02	0	1	0	0	1	216	1	1.71	2	83.20
6	220.02	0	1	0	0	1	216	1	1.93	2	83.20
6	222.02	0	1	1	0	1	216	1	1.50	2	83.20
6	223.02	0	.	0	0	1	223	1	1.93	1	103.60
6	224.02	1	.	1	0	1	224	0	1.29	1	73.00
6	225.02	1	.	1	0	1	225	0	1.50	1	52.60
6	228.02	1	.	1	0	1	228	0	1.50	2	52.60
6	229.02	1	0	1	0	1	228	0	1.50	1	52.60
6	230.02	0	1	0	0	1	228	0	1.50	1	52.60
6	231.02	0	0	0	0	1	228	0	1.50	1	103.60
6	232.02	0	0	0	1	1	228	0	1.93	2	103.60
6	233.02	1	1	1	0	1	228	0	1.50	0	103.60
6	234.02	0	1	0	0	1	228	0	1.50	2	103.60
6	235.02	1	0	1	0	1	228	0	1.93	1	73.00
6	236.02	0	0	0	0	1	228	0	1.71	1	73.00
6	237.02	0	0	1	0	1	228	0	1.71	2	103.60
6	238.02	1	1	1	0	1	228	0	1.93	1	103.60
6	239.02	0	.	1	0	1	239	1	2.14	2	103.60
6	240.02	1	.	1	0	1	240	1	2.36	1	83.20
6	241.02	0	0	0	0	1	239	1	2.14	2	103.60
6	242.02	0	.	0	0	1	242	1	1.71	0	103.60
6	243.02	0	1	1	0	1	240	1	1.71	1	124.01
6	244.02	1	.	1	0	1	244	1	1.93	2	103.60
6	245.02	0	.	0	0	1	245	1	1.93	1	103.60
6	246.02	0	.	0	0	1	246	0	1.93	1	124.01
6	247.02	0	.	0	0	1	247	1	2.14	0	103.60
6	248.02	0	0	0	0	1	246	0	1.93	1	124.01
6	249.02	1	1	1	0	1	246	0	2.57	1	124.01
6	250.02	0	0	1	0	1	246	0	2.14	2	103.60
6	251.02	0	0	0	0	1	246	0	2.79	2	103.60
6	252.02	0	1	0	0	1	246	0	2.36	1	124.01
6	253.02	1	1	1	0	1	246	0	2.14	1	124.01
6	254.02	1	0	1	0	1	246	0	2.57	2	124.01
6	255.02	0	.	0	0	1	255	0	2.36	0	124.01
6	256.02	0	.	0	0	1	256	0	2.36	0	103.60
6	257.02	0	.	0	0	1	257	0	2.79	2	124.01
6	258.02	1	.	1	0	1	258	0	2.14	1	103.60
6	259.02	1	.	1	0	1	259	0	1.93	1	103.60
6	260.02	1	.	1	0	1	260	0	2.14	1	103.60
6	261.02	0	1	1	0	1	259	0	1.93	1	124.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	203.02	143.08	0.40	2.51	0.40	2.47	0		1	.
6	204.02	179.11	0.40	2.48	0.40	2.47	0		0	.
6	208.02	254.86	0.38	2.65	0.38	2.65	1	4	0	2.47
6	209.02	256.59	0.38	2.66	0.38	2.65	0		0	.
6	211.02	70.78	0.36	2.79	0.36	2.79	1	3	0	2.65
6	212.02	72.98	0.35	2.83	0.35	2.83	1	0	0	2.65
6	213.02	75.91	0.41	2.46	0.41	2.46	1	2	0	2.65
6	214.02	77.65	0.35	2.89	0.35	2.83	0		0	.
6	215.02	181.28	0.37	2.73	0.37	2.73	1	3	0	2.83
6	216.02	180.12	0.39	2.58	0.39	2.58	1	2	0	2.83
6	219.02	112.74	0.37	2.71	0.39	2.58	0		0	.
6	220.02	109.04	0.38	2.67	0.39	2.58	0		1	.
6	222.02	113.94	0.37	2.72	0.39	2.58	0		0	.
6	223.02	73.51	0.34	2.93	0.34	2.93	1	3	0	2.83
6	224.02	153.12	0.36	2.75	0.36	2.75	1	1	0	2.83
6	225.02	192.53	0.37	2.69	0.37	2.69	1	1	0	2.75
6	228.02	195.90	0.35	2.89	0.35	2.89	1	4	0	2.69
6	229.02	193.86	0.35	2.84	0.35	2.89	0		1	.
6	230.02	196.67	0.35	2.86	0.35	2.89	0		0	.
6	231.02	78.85	0.34	2.90	0.35	2.89	0		0	.
6	232.02	80.75	0.35	2.89	0.35	2.89	0		0	.
6	233.02	82.49	0.34	2.98	0.35	2.89	0		0	.
6	234.02	83.22	0.30	3.35	0.35	2.89	0		0	.
6	235.02	158.29	0.30	3.36	0.35	2.89	0		0	.
6	236.02	161.39	0.30	3.34	0.35	2.89	0		0	.
6	237.02	86.89	0.29	3.40	0.35	2.89	0		0	.
6	238.02	84.59	0.29	3.39	0.35	2.89	0		0	.
6	239.02	93.30	0.32	3.15	0.32	3.15	1	2	0	2.89
6	240.02	123.92	0.29	3.40	0.29	3.40	1	3	0	2.89
6	241.02	98.40	0.32	3.13	0.32	3.15	0		1	.
6	242.02	97.27	0.30	3.35	0.30	3.35	1	1	0	2.89
6	243.02	90.43	0.30	3.36	0.29	3.40	0		1	.
6	244.02	95.10	0.31	3.20	0.31	3.20	1	3	0	3.35
6	245.02	101.74	0.31	3.18	0.31	3.18	1	2	0	3.35
6	246.02	98.40	0.31	3.17	0.31	3.17	1	3	0	3.35
6	247.02	91.80	0.28	3.52	0.28	3.52	1	3	0	2.89
6	248.02	105.08	0.32	3.12	0.31	3.17	0		0	.
6	249.02	106.34	0.32	3.09	0.31	3.17	0		0	.
6	250.02	105.98	0.31	3.18	0.31	3.17	0		1	.
6	251.02	108.28	0.33	3.05	0.31	3.17	0		0	.
6	252.02	112.38	0.33	3.07	0.31	3.17	0		0	.
6	253.02	113.78	0.33	3.07	0.31	3.17	0		0	.
6	254.02	116.25	0.32	3.09	0.31	3.17	0		0	.
6	255.02	121.79	0.32	3.13	0.32	3.13	1	2	0	3.35
6	256.02	120.69	0.35	2.89	0.35	2.89	1	2	0	3.35
6	257.02	119.86	0.32	3.12	0.32	3.12	1	3	0	3.35
6	258.02	111.08	0.31	3.24	0.31	3.24	1	3	0	3.35
6	259.02	112.95	0.31	3.20	0.31	3.20	1	1	0	3.21
6	260.02	99.74	0.31	3.21	0.31	3.21	1	1	0	3.35
6	261.02	118.46	0.31	3.21	0.31	3.20	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	262.02	1	1	1	0	1	259	0	1.71	2	73.00
6	263.02	0	1	1	0	1	259	0	1.71	1	103.60
6	264.02	1	1	0	0	1	259	0	1.71	2	124.01
6	265.02	1	0	1	0	1	259	0	1.50	1	124.01
6	266.02	1	0	1	0	1	259	0	1.93	2	124.01
6	267.02	0	1	1	0	1	259	0	1.50	1	103.60
6	268.02	1	1	1	0	1	259	0	1.93	2	103.60
6	269.02	1	0	0	0	1	259	0	2.14	1	73.00
6	270.02	1	0	1	0	1	259	0	2.14	2	124.01
6	271.02	0	1	0	0	1	259	0	1.71	1	73.00
6	272.02	1	1	1	0	2	259	0	1.93	1	124.01
6	273.02	1	0	0	0	1	259	0	1.93	2	103.60
6	274.02	0	1	1	0	1	259	0	1.71	1	103.60
6	275.02	1	1	1	0	1	259	0	2.14	2	124.01
6	276.02	1	0	1	0	1	259	0	1.71	1	124.01
6	277.02	1	0	1	0	1	259	0	2.14	2	175.01
6	278.02	1	0	1	0	1	259	0	2.14	1	93.40
6	279.02	1	.	1	0	1	279	1	1.93	2	124.01
6	280.02	0	.	0	0	1	280	1	2.14	1	93.40
6	281.02	1	0	1	0	1	279	1	2.14	2	124.01
6	282.02	1	0	1	0	1	279	1	1.71	2	124.01
6	283.02	0	0	1	0	1	280	1	2.14	1	103.60
6	284.02	1	1	1	0	1	280	1	1.93	1	205.61
6	285.02	1	0	1	1	1	279	1	1.29	2	154.61
6	286.02	0	1	0	0	1	280	1	1.50	1	11.80
6	287.02	1	.	0	0	1	287	1	1.50	0	154.61
6	288.02	1	.	1	0	1	288	0	1.50	2	154.61
6	289.02	1	.	1	0	2	289	0	1.71	1	144.41
6	290.02	0	1	0	0	1	289	0	1.50	1	73.00
6	291.02	1	.	1	0	1	291	0	1.71	1	42.40
6	292.02	1	.	1	0	1	292	0	1.71	2	144.41
6	293.02	1	.	1	0	1	293	0	2.14	1	103.60
6	294.02	1	.	1	0	1	294	0	2.14	1	144.41
6	295.02	0	.	1	0	1	295	0	1.50	2	103.60
6	296.02	0	.	1	0	1	296	0	1.29	2	175.01
6	297.02	0	1	0	0	1	294	0	1.50	1	144.41
6	298.02	1	0	1	0	1	298	1	1.29	2	164.81
6	299.02	1	.	1	0	1	299	0	1.50	0	42.40
6	300.02	1	0	1	0	1	298	1	1.50	2	144.41
6	301.02	1	0	0	0	1	298	1	1.71	2	124.01
6	302.02	1	0	1	0	1	298	1	1.71	2	124.01
6	303.02	1	1	0	0	1	298	1	1.93	2	144.41
6	304.02	1	0	1	0	1	298	1	1.50	2	124.01
6	305.02	1	0	0	0	1	311	1	2.36	1	144.41
6	306.02	0	1	0	0	1	298	1	1.93	2	124.01
6	307.02	0	.	0	0	1	307	1	1.93	1	144.41
6	308.02	1	0	0	0	1	311	1	1.93	1	144.41
6	309.02	0	.	1	0	1	309	1	2.14	2	124.01
6	310.02	1	.	1	0	1	310	1	1.71	1	124.01
6	311.02	1	.	1	0	1	311	1	1.50	1	42.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	262.02	191.22	0.32	3.17	0.31	3.20	0		1	.
6	263.02	119.29	0.31	3.23	0.31	3.20	0		0	.
6	264.02	125.33	0.31	3.18	0.31	3.20	0		0	.
6	265.02	123.63	0.31	3.20	0.31	3.20	0		0	.
6	266.02	126.73	0.31	3.19	0.31	3.20	0		0	.
6	267.02	128.87	0.32	3.14	0.31	3.20	0		0	.
6	268.02	127.70	0.31	3.20	0.31	3.20	0		0	.
6	269.02	198.40	0.32	3.15	0.31	3.20	0		0	.
6	270.02	132.70	0.31	3.19	0.31	3.20	0		0	.
6	271.02	199.93	0.32	3.15	0.31	3.20	0		0	.
6	272.02	131.37	0.32	3.14	0.31	3.20	0		0	.
6	273.02	130.67	0.32	3.16	0.31	3.20	0		0	.
6	274.02	133.34	0.32	3.15	0.31	3.20	0		0	.
6	275.02	135.61	0.32	3.17	0.31	3.20	0		0	.
6	276.02	137.27	0.32	3.15	0.31	3.20	0		0	.
6	277.02	55.73	0.31	3.19	0.31	3.20	0		0	.
6	278.02	177.64	0.31	3.18	0.31	3.20	0		0	.
6	279.02	140.41	0.32	3.17	0.32	3.17	1	2	0	3.20
6	280.02	180.74	0.31	3.21	0.31	3.21	1	3	0	3.20
6	281.02	139.28	0.32	3.16	0.32	3.17	0		1	.
6	282.02	142.01	0.32	3.15	0.32	3.17	0		0	.
6	283.02	134.87	0.31	3.20	0.31	3.21	0		1	.
6	284.02	44.25	0.31	3.21	0.31	3.21	0		0	.
6	285.02	86.55	0.34	2.90	0.32	3.17	0		0	.
6	286.02	352.12	0.31	3.21	0.31	3.21	0		0	.
6	287.02	91.15	0.30	3.31	0.30	3.31	1	1	0	3.20
6	288.02	88.85	0.33	3.08	0.33	3.08	1	1	0	3.31
6	289.02	86.12	0.33	3.02	0.33	3.02	1	1	0	3.08
6	290.02	240.57	0.33	3.01	0.33	3.02	0		1	.
6	291.02	280.18	0.33	3.06	0.33	3.06	1	3	0	3.02
6	292.02	89.26	0.46	2.16	0.46	2.16	1	2	0	3.02
6	293.02	167.57	0.33	3.01	0.33	3.01	1	2	0	3.02
6	294.02	83.71	0.34	2.94	0.34	2.94	1	1	0	3.02
6	295.02	139.78	0.31	3.24	0.31	3.24	1	3	0	3.02
6	296.02	61.50	0.40	2.49	0.40	2.49	1	1	0	2.94
6	297.02	87.35	0.36	2.79	0.34	2.94	0		1	.
6	298.02	75.88	0.40	2.48	0.40	2.48	0		0	2.49
6	299.02	262.20	0.28	3.63	0.28	3.63	1	3	0	2.49
6	300.02	98.69	0.41	2.46	0.40	2.48	0		1	.
6	301.02	165.57	0.41	2.46	0.40	2.48	0		0	.
6	302.02	167.10	0.41	2.42	0.40	2.48	0		0	.
6	303.02	103.47	0.43	2.31	0.40	2.48	0		0	.
6	304.02	169.11	0.41	2.44	0.40	2.48	0		0	.
6	305.02	102.37	0.40	2.47	0.37	2.69	0		0	.
6	306.02	172.08	0.41	2.45	0.40	2.48	0		0	.
6	307.02	104.40	0.40	2.48	0.40	2.48	1	1	0	2.49
6	308.02	100.73	0.40	2.48	0.37	2.69	0		0	.
6	309.02	192.20	0.43	2.33	0.43	2.33	1	2	0	2.48
6	310.02	188.96	0.41	2.44	0.41	2.44	1	3	0	2.48
6	311.02	282.08	0.37	2.69	0.37	2.69	1	3	0	2.49

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	312.02	1	1	1	0	1	311	1	1.93	1	83.20
6	313.02	1	0	1	0	1	311	1	1.50	1	103.60
6	314.02	0	1	0	0	1	311	1	1.93	1	103.60
6	315.02	1	.	1	0	1	315	1	1.50	2	144.41
6	316.02	0	.	1	0	1	316	1	1.93	2	205.61
6	317.02	1	1	1	0	1	316	1	2.14	2	124.01
6	318.02	1	.	1	0	1	318	1	1.71	1	103.60
6	319.02	1	.	1	0	2	319	0	2.14	1	103.60
6	320.02	1	0	1	0	1	318	1	1.71	1	103.60
6	321.02	1	0	0	0	1	319	0	1.71	2	124.01
6	322.02	1	0	1	0	1	319	0	1.71	1	124.01
6	323.02	1	0	1	0	1	319	0	1.50	2	175.01
6	324.02	1	0	1	0	2	319	0	1.71	1	124.01
6	325.02	0	0	0	0	1	319	0	1.71	2	144.41
6	326.02	0	1	0	0	2	319	0	1.29	1	124.01
6	327.02	1	1	1	0	1	319	0	1.29	2	144.41
6	328.02	0	0	1	0	1	319	0	1.93	1	124.01
6	329.02	1	0	1	0	2	319	0	0.86	2	124.01
6	330.02	1	1	1	0	2	319	0	0.86	1	103.60
6	331.02	0	1	0	0	1	319	0	1.07	2	103.60
6	332.02	0	1	0	0	1	319	0	1.50	1	124.01
6	333.02	1	0	0	0	1	319	0	1.71	1	144.41
6	334.02	1	1	1	0	1	319	0	1.71	2	144.41
6	335.02	1	0	1	0	1	319	0	1.50	1	124.01
6	336.02	1	0	1	0	1	319	0	1.93	2	124.01
6	337.02	1	0	1	0	2	319	0	1.93	2	124.01
6	338.02	1	0	1	0	1	319	0	1.71	1	93.40
6	339.02	1	0	1	0	1	319	0	1.93	2	124.01
6	340.02	1	0	1	0	1	319	0	1.71	1	124.01
6	341.02	0	.	1	0	1	341	0	2.14	2	205.61
6	342.02	0	1	1	0	1	319	0	1.93	1	124.01
6	343.02	1	1	0	0	1	319	0	1.50	1	124.01
6	344.02	0	0	0	0	1	319	0	1.50	1	154.61
6	345.02	0	1	1	0	1	319	0	1.50	2	154.61
6	346.02	1	.	1	0	1	346	0	2.14	2	144.41
6	347.02	1	0	1	0	1	346	0	1.93	1	124.01
6	348.02	1	.	1	0	1	348	0	2.14	1	205.61
6	349.02	0	.	0	0	1	349	1	1.93	1	205.61
6	350.02	0	.	0	0	1	350	0	2.36	2	154.61
6	351.02	0	1	1	0	1	352	1	1.93	2	124.01
6	352.02	0	.	1	1	1	352	1	1.71	2	144.41
6	353.02	1	1	1	0	1	352	1	1.93	2	124.01
6	354.02	1	0	1	0	1	352	1	2.14	2	205.61
6	355.02	1	1	1	0	1	352	1	1.71	2	124.01
6	356.02	1	0	1	0	1	352	1	1.93	2	124.01
6	357.02	1	1	0	0	1	349	1	1.93	1	124.01
6	358.02	1	0	1	0	1	352	1	1.71	2	93.40
6	359.02	1	0	0	0	1	349	1	1.93	1	124.01
6	360.02	1	1	1	0	1	349	1	1.71	1	124.01
6	361.02	1	0	1	0	1	349	1	2.14	1	124.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	312.02	218.21	0.39	2.56	0.37	2.69	0		0	.
6	313.02	170.21	0.37	2.70	0.37	2.69	0		1	.
6	314.02	171.68	0.37	2.67	0.37	2.69	0		0	.
6	315.02	106.37	0.40	2.49	0.40	2.49	1	1	0	2.48
6	316.02	45.88	0.41	2.42	0.41	2.42	1	2	0	2.49
6	317.02	186.22	0.41	2.41	0.41	2.42	0		1	.
6	318.02	183.42	0.40	2.51	0.40	2.51	1	3	0	2.49
6	319.02	185.36	0.40	2.50	0.40	2.50	1	1	0	2.49
6	320.02	185.39	0.39	2.54	0.40	2.51	0		1	.
6	321.02	190.26	0.40	2.49	0.40	2.50	0		1	.
6	322.02	185.62	0.39	2.57	0.40	2.50	0		0	.
6	323.02	87.06	0.39	2.56	0.40	2.50	0		0	.
6	324.02	190.72	0.39	2.57	0.40	2.50	0		0	.
6	325.02	108.49	0.39	2.54	0.40	2.50	0		0	.
6	326.02	194.83	0.39	2.55	0.40	2.50	0		0	.
6	327.02	110.07	0.39	2.56	0.40	2.50	0		0	.
6	328.02	196.57	0.39	2.56	0.40	2.50	0		0	.
6	329.02	202.77	0.39	2.56	0.40	2.50	0		0	.
6	330.02	198.04	0.39	2.57	0.40	2.50	0		0	.
6	331.02	201.71	0.39	2.58	0.40	2.50	0		0	.
6	332.02	198.30	0.38	2.61	0.40	2.50	0		0	.
6	333.02	113.21	0.38	2.62	0.40	2.50	0		0	.
6	334.02	112.04	0.39	2.59	0.40	2.50	0		0	.
6	335.02	214.89	0.38	2.60	0.40	2.50	0		0	.
6	336.02	217.09	0.39	2.56	0.40	2.50	0		0	.
6	337.02	219.29	0.39	2.59	0.40	2.50	0		0	.
6	338.02	185.61	0.38	2.60	0.40	2.50	0		0	.
6	339.02	207.81	0.39	2.58	0.40	2.50	0		0	.
6	340.02	203.14	0.38	2.61	0.40	2.50	0		0	.
6	341.02	51.95	0.41	2.45	0.41	2.45	1	2	0	2.50
6	342.02	205.34	0.38	2.61	0.40	2.50	0		0	.
6	343.02	211.08	0.38	2.61	0.40	2.50	0		0	.
6	344.02	114.71	0.39	2.60	0.40	2.50	0		0	.
6	345.02	114.94	0.39	2.53	0.40	2.50	0		0	.
6	346.02	117.78	0.38	2.60	0.38	2.60	1	3	0	2.50
6	347.02	231.57	0.37	2.67	0.38	2.60	0		1	.
6	348.02	56.39	0.37	2.73	0.37	2.73	1	3	0	2.50
6	349.02	54.46	0.36	2.77	0.36	2.77	1	3	0	2.50
6	350.02	119.68	0.40	2.52	0.40	2.52	1	2	0	2.50
6	351.02	238.08	0.39	2.58	0.39	2.56	0		0	.
6	352.02	124.62	0.39	2.56	0.39	2.56	1	2	0	2.50
6	353.02	228.77	0.39	2.56	0.39	2.56	0		1	.
6	354.02	55.02	0.39	2.54	0.39	2.56	0		0	.
6	355.02	237.64	0.39	2.58	0.39	2.56	0		0	.
6	356.02	240.58	0.39	2.55	0.39	2.56	0		0	.
6	357.02	213.48	0.38	2.63	0.36	2.77	0		1	.
6	358.02	317.78	0.39	2.55	0.39	2.56	0		0	.
6	359.02	215.92	0.37	2.70	0.36	2.77	0		0	.
6	360.02	230.10	0.38	2.64	0.36	2.77	0		0	.
6	361.02	216.59	0.37	2.68	0.36	2.77	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	362.02	1	0	1	0	1	349	1	1.71	1	124.01
6	363.02	0	1	0	0	1	349	1	1.50	1	124.01
6	364.02	0	0	0	0	1	365	0	1.71	2	93.40
6	365.02	0	.	1	0	1	365	0	1.93	1	103.60
6	366.02	1	1	1	0	1	365	0	1.71	1	124.01
6	367.02	0	0	0	0	1	365	0	1.71	1	164.81
6	368.02	0	1	0	0	1	365	0	1.07	2	164.81
6	369.02	1	1	1	0	1	365	0	1.07	2	124.01
6	370.02	0	1	1	0	1	365	0	1.07	1	103.60
6	371.02	0	0	0	0	1	365	0	1.71	1	124.01
6	372.02	1	1	1	0	1	365	0	1.50	0	205.61
6	373.02	1	0	0	0	1	365	0	1.71	2	205.61
6	374.02	1	0	1	0	1	365	0	1.71	1	205.61
6	375.02	0	.	1	0	1	375	0	1.50	2	205.61
6	376.02	1	.	0	0	1	376	0	1.93	1	205.61
6	377.02	1	.	0	0	1	377	0	2.14	2	205.61
6	378.02	1	.	1	0	1	378	0	1.71	1	164.81
6	379.02	0	.	1	0	1	379	0	1.71	2	175.01
6	380.02	0	.	1	0	2	380	0	2.14	0	93.40
6	381.02	0	.	1	0	1	381	0	1.50	2	205.61
6	382.02	1	1	1	0	1	381	0	1.71	0	205.61
6	383.02	1	.	1	0	1	383	0	1.50	0	124.01
6	384.02	1	.	1	0	1	384	1	1.50	2	124.01
6	385.02	1	0	1	0	1	384	1	1.93	2	22.00
6	386.02	1	.	1	0	2	386	0	1.50	2	124.01
6	387.02	1	.	1	0	1	387	1	1.71	2	124.01
6	388.02	1	.	1	0	1	388	1	1.29	2	185.21
6	389.02	0	1	1	0	1	383	0	1.29	1	226.01
6	390.02	0	1	1	0	1	388	1	1.07	2	124.01
6	391.02	1	0	1	0	1	388	1	1.29	0	185.21
6	392.02	1	.	0	0	1	392	1	1.07	1	124.01
6	393.02	0	0	0	0	2	397	1	1.29	1	185.21
6	394.02	0	1	0	0	1	392	1	1.29	1	185.21
6	395.02	0	.	0	0	1	395	1	1.50	1	103.60
6	396.02	0	0	1	0	1	395	1	1.50	1	205.61
6	397.02	0	.	0	0	2	397	1	1.50	1	175.01
6	398.02	0	0	1	0	2	397	1	1.07	1	124.01
6	399.02	1	.	1	0	2	399	0	0.64	2	154.61
6	400.02	1	.	1	0	2	400	0	0.43	2	154.61
6	401.02	0	1	0	0	2	400	0	0.64	2	154.61
6	402.02	0	.	1	0	2	402	0	0.64	0	154.61
6	403.02	0	.	1	0	1	403	0	0.86	2	175.01
6	404.02	1	.	1	0	1	404	0	1.07	0	124.01
6	405.02	1	.	1	0	1	405	0	1.50	2	124.01
6	406.02	0	1	1	0	2	404	0	1.07	1	205.61
6	407.02	1	0	1	0	1	408	0	1.07	1	205.61
6	408.02	1	.	1	0	1	408	0	1.29	2	195.41
6	409.02	1	.	1	0	1	409	0	0.64	1	205.61
6	410.02	1	.	1	0	2	410	0	0.64	2	195.41
6	411.02	0	.	1	0	1	411	0	0.64	0	195.41

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	362.02	237.71	0.38	2.62	0.36	2.77	0		0	.
6	363.02	221.89	0.37	2.68	0.36	2.77	0		0	.
6	364.02	316.31	0.40	2.48	0.39	2.55	0		1	.
6	365.02	88.39	0.39	2.55	0.39	2.55	1	1	0	2.50
6	366.02	253.06	0.40	2.48	0.39	2.55	0		0	.
6	367.02	94.90	0.39	2.56	0.39	2.55	0		0	.
6	368.02	89.39	0.39	2.60	0.39	2.55	0		0	.
6	369.02	231.80	0.39	2.58	0.39	2.55	0		0	.
6	370.02	90.13	0.39	2.58	0.39	2.55	0		0	.
6	371.02	241.28	0.39	2.55	0.39	2.55	0		0	.
6	372.02	51.35	0.40	2.50	0.39	2.55	0		0	.
6	373.02	50.85	0.39	2.59	0.39	2.55	0		0	.
6	374.02	53.62	0.40	2.47	0.39	2.55	0		0	.
6	375.02	49.18	0.44	2.28	0.44	2.28	1	2	0	2.55
6	376.02	57.79	0.40	2.47	0.40	2.47	1	3	0	2.55
6	377.02	57.39	0.38	2.60	0.38	2.60	1	3	0	2.55
6	378.02	93.06	0.47	2.13	0.47	2.13	1	2	0	2.55
6	379.02	94.70	0.43	2.34	0.43	2.34	1	3	0	2.55
6	380.02	201.53	0.45	2.24	0.45	2.24	1	1	0	2.55
6	381.02	60.20	0.45	2.21	0.45	2.21	1	1	0	2.24
6	382.02	59.33	0.46	2.15	0.45	2.21	0		1	.
6	383.02	248.19	0.42	2.37	0.42	2.37	1	3	0	2.21
6	384.02	250.85	0.44	2.28	0.44	2.28	1	2	0	2.21
6	385.02	477.21	0.46	2.17	0.44	2.28	0		1	.
6	386.02	276.01	0.44	2.27	0.44	2.27	1	1	0	2.21
6	387.02	273.18	0.44	2.28	0.44	2.28	1	3	0	2.27
6	388.02	81.08	0.48	2.10	0.48	2.10	1	3	0	2.03
6	389.02	30.19	0.43	2.35	0.42	2.37	0		1	.
6	390.02	282.69	0.49	2.05	0.48	2.10	0		0	.
6	391.02	84.72	0.49	2.04	0.48	2.10	0		1	.
6	392.02	224.86	0.37	2.73	0.37	2.73	1	3	0	2.21
6	393.02	86.75	0.48	2.09	0.49	2.03	0		1	.
6	394.02	83.01	0.38	2.61	0.37	2.73	0		1	.
6	395.02	256.46	0.46	2.16	0.46	2.16	1	2	0	2.27
6	396.02	66.80	0.46	2.19	0.46	2.16	0		1	.
6	397.02	125.06	0.49	2.03	0.49	2.03	1	1	0	2.27
6	398.02	287.59	0.52	1.93	0.49	2.03	0		0	.
6	399.02	156.52	0.59	1.70	0.59	1.70	1	1	0	2.03
6	400.02	158.59	0.59	1.69	0.59	1.69	1	1	0	1.70
6	401.02	160.32	0.59	1.69	0.59	1.69	0		1	.
6	402.02	161.96	0.60	1.67	0.60	1.67	1	1	0	1.69
6	403.02	128.60	0.67	1.50	0.67	1.50	1	1	0	1.67
6	404.02	305.98	0.63	1.60	0.63	1.60	1	1	0	1.66
6	405.02	304.21	0.60	1.66	0.60	1.66	1	0	0	1.50
6	406.02	72.11	0.64	1.57	0.63	1.60	0		1	.
6	407.02	69.80	0.68	1.47	0.66	1.52	0		1	.
6	408.02	104.13	0.66	1.52	0.66	1.52	1	1	0	1.60
6	409.02	70.44	0.56	1.79	0.56	1.79	1	3	0	1.52
6	410.02	107.87	0.59	1.70	0.59	1.70	1	0	0	1.52
6	411.02	110.87	0.56	1.80	0.56	1.80	1	0	0	1.70

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	412.02	1	.	1	0	1	412	0	1.07	2	164.81
6	413.02	1	0	1	0	1	412	0	0.86	2	164.81
6	414.02	1	0	1	0	1	412	0	1.71	2	164.81
6	415.02	1	1	1	0	1	412	0	1.71	2	236.21
6	416.02	1	0	1	0	1	412	0	1.07	1	124.01
6	417.02	0	1	1	0	1	412	0	1.29	1	205.61
6	418.02	0	0	1	0	2	412	0	1.93	1	205.61
6	419.02	0	1	0	0	1	412	0	1.71	1	205.61
6	420.02	0	0	1	0	2	412	0	1.71	1	205.61
6	421.02	1	.	0	0	1	421	1	1.71	2	164.81
6	422.02	1	0	1	0	1	423	1	1.71	1	195.41
6	423.02	1	.	1	0	1	423	1	1.71	1	164.81
6	424.02	1	0	1	0	1	421	1	2.14	2	195.41
6	425.02	0	1	1	0	1	423	1	2.14	1	195.41
6	426.02	1	.	0	0	.	426	0	0.43	1	93.40
6	427.02	1	0	1	0	1	426	0	1.07	1	93.40
6	428.02	1	.	1	0	2	428	1	1.93	0	195.41
6	429.02	0	0	1	0	1	423	1	2.36	1	205.61
6	430.02	1	.	1	0	1	430	1	1.71	1	62.80
6	431.02	0	1	0	0	1	430	1	1.93	1	103.60
6	432.02	0	0	1	0	1	430	1	2.14	1	185.21
6	433.02	1	1	1	0	1	430	1	1.93	1	185.21
6	434.02	1	0	1	1	1	430	1	1.71	0	205.61
6	435.02	1	1	1	0	2	436	1	1.93	2	185.21
6	436.02	1	.	1	0	1	436	1	1.93	2	195.41
6	437.02	0	1	0	0	1	436	1	1.71	2	195.41
6	438.02	1	.	1	1	1	438	0	0.64	2	195.41
6	439.02	1	.	1	0	1	439	0	1.07	1	195.41
6	440.02	0	.	1	0	2	440	0	0.43	2	205.61
6	441.02	0	1	1	0	2	439	0	1.07	1	205.61
6	442.02	1	.	1	0	2	442	0	1.29	1	205.61
6	443.02	0	1	1	0	1	442	0	1.07	2	205.61
6	444.02	1	1	0	0	2	442	0	1.29	1	22.00
6	445.02	0	1	1	0	2	442	0	0.86	2	205.61
6	446.02	1	1	1	0	1	442	0	1.29	1	195.41
6	447.02	0	0	0	0	1	442	0	1.29	2	195.41
6	448.02	0	1	1	0	2	442	0	1.29	1	185.21
6	449.02	0	0	0	0	1	442	0	1.71	2	185.21
6	450.02	1	1	1	0	1	442	0	1.29	1	205.61
6	451.02	0	1	1	0	2	442	0	1.71	2	205.61
6	452.02	1	1	1	0	1	442	0	1.50	1	226.01
6	453.02	1	.	1	0	1	453	1	1.71	1	226.01
6	454.02	0	.	1	0	1	454	1	1.93	2	195.41
6	455.02	1	0	1	0	1	453	1	1.71	1	226.01
6	456.02	0	.	1	0	1	456	0	1.93	1	185.21
6	457.02	0	0	1	0	1	454	1	1.93	2	195.41
6	458.02	1	0	1	0	2	456	0	2.14	1	195.41
6	459.02	1	1	1	0	1	456	0	1.93	2	226.01
6	460.02	1	0	0	0	1	456	0	2.14	1	226.01
6	461.02	0	1	1	0	2	456	0	2.36	1	205.61

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	412.02	145.48	0.46	2.19	0.46	2.19	1	1	0	1.80
6	413.02	148.35	0.46	2.17	0.46	2.19	0		1	.
6	414.02	148.75	0.47	2.14	0.46	2.19	0		0	.
6	415.02	67.46	0.46	2.19	0.46	2.19	0		0	.
6	416.02	321.39	0.46	2.18	0.46	2.19	0		0	.
6	417.02	77.45	0.46	2.15	0.46	2.19	0		0	.
6	418.02	73.64	0.45	2.21	0.46	2.19	0		0	.
6	419.02	74.91	0.46	2.19	0.46	2.19	0		0	.
6	420.02	79.21	0.46	2.19	0.46	2.19	0		0	.
6	421.02	169.64	0.46	2.17	0.46	2.17	1	2	0	2.19
6	422.02	131.23	0.45	2.21	0.45	2.21	0		1	.
6	423.02	168.32	0.45	2.21	0.45	2.21	1	3	0	2.19
6	424.02	144.78	0.46	2.17	0.46	2.17	0		1	.
6	425.02	140.90	0.45	2.20	0.45	2.21	0		0	.
6	426.02	310.84	0.35	2.87	0.35	2.87	1	3	0	1.80
6	427.02	312.77	0.35	2.84	0.35	2.87	0		1	.
6	428.02	140.14	0.46	2.17	0.46	2.17	1	1	0	2.19
6	429.02	84.32	0.46	2.17	0.45	2.21	0		0	.
6	430.02	451.68	0.47	2.14	0.47	2.14	1	2	0	2.17
6	431.02	353.86	0.47	2.14	0.47	2.14	0		1	.
6	432.02	132.13	0.47	2.13	0.47	2.14	0		0	.
6	433.02	129.16	0.46	2.17	0.47	2.14	0		0	.
6	434.02	80.98	0.45	2.22	0.47	2.14	0		0	.
6	435.02	147.34	0.43	2.31	0.44	2.29	0		0	.
6	436.02	123.82	0.44	2.29	0.44	2.29	1	3	0	2.17
6	437.02	142.87	0.43	2.31	0.44	2.29	0		1	.
6	438.02	126.46	0.41	2.45	0.41	2.45	1	2	0	2.17
6	439.02	121.62	0.36	2.80	0.36	2.80	1	1	0	2.17
6	440.02	66.27	0.36	2.81	0.36	2.81	1	3	0	2.17
6	441.02	90.66	0.36	2.76	0.36	2.80	0		1	.
6	442.02	95.70	0.36	2.77	0.36	2.77	1	1	0	2.80
6	443.02	88.36	0.36	2.80	0.36	2.77	0		1	.
6	444.02	590.09	0.37	2.74	0.36	2.77	0		0	.
6	445.02	93.33	0.36	2.76	0.36	2.77	0		0	.
6	446.02	127.99	0.36	2.76	0.36	2.77	0		0	.
6	447.02	129.19	0.36	2.75	0.36	2.77	0		0	.
6	448.02	152.22	0.36	2.77	0.36	2.77	0		0	.
6	449.02	150.51	0.36	2.78	0.36	2.77	0		0	.
6	450.02	97.70	0.36	2.79	0.36	2.77	0		0	.
6	451.02	100.27	0.35	2.86	0.36	2.77	0		0	.
6	452.02	69.03	0.35	2.86	0.36	2.77	0		0	.
6	453.02	70.27	0.35	2.84	0.35	2.84	1	3	0	2.77
6	454.02	157.32	0.36	2.77	0.36	2.77	1	2	0	2.77
6	455.02	75.20	0.36	2.79	0.35	2.84	0		1	.
6	456.02	163.96	0.36	2.80	0.36	2.80	1	0	0	2.77
6	457.02	183.31	0.37	2.69	0.36	2.77	0		1	.
6	458.02	163.19	0.35	2.84	0.36	2.80	0		0	.
6	459.02	72.17	0.37	2.67	0.36	2.80	0		1	.
6	460.02	73.70	0.35	2.82	0.36	2.80	0		0	.
6	461.02	93.83	0.35	2.82	0.36	2.80	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	462.02	0	.	1	0	2	462	0	1.71	0	205.61
6	463.02	1	.	1	1	1	463	0	1.71	2	205.61
6	464.02	1	0	0	0	1	463	0	1.93	1	205.61
6	465.02	0	0	0	1	2	462	0	1.50	2	226.01
6	466.02	0	0	1	0	2	462	0	1.50	1	154.61
6	467.02	0	1	0	0	1	462	0	1.29	1	124.01
6	468.02	1	1	1	0	1	462	0	1.29	2	124.01
6	469.02	1	1	1	0	2	462	0	1.29	2	236.21
6	470.02	1	0	1	0	2	462	0	1.07	2	236.21
6	471.02	1	1	1	0	1	462	0	1.29	1	195.41
6	472.02	0	1	0	0	1	462	0	1.29	1	195.41
6	473.02	1	.	1	0	1	473	1	1.71	1	154.61
6	474.02	1	0	1	0	1	462	0	0.86	2	236.21
6	475.02	0	0	1	0	1	462	0	1.50	2	62.80
6	476.02	1	0	1	0	1	473	1	1.93	1	205.61
6	477.02	1	0	1	0	1	462	0	1.50	2	236.21
6	478.02	1	.	1	0	2	478	1	1.50	2	205.61
6	479.02	0	1	0	0	1	473	1	1.93	1	154.61
6	480.02	0	0	1	0	1	473	1	2.14	1	103.60
6	481.02	1	0	1	0	1	478	1	1.07	2	205.61
6	482.02	1	1	1	0	1	473	1	1.93	1	215.81
6	483.02	1	0	1	0	1	478	1	1.07	2	236.21
6	484.02	1	0	1	0	2	478	1	1.29	2	236.21
6	485.02	1	0	1	0	1	478	1	1.50	2	236.21
6	486.02	1	0	1	0	1	478	1	1.50	2	236.21
6	487.02	1	0	1	0	2	478	1	1.50	2	236.21
6	488.02	1	.	1	0	1	488	0	1.50	0	236.21
6	489.02	0	1	1	0	1	488	0	1.29	2	236.21
6	490.02	1	1	1	0	1	491	0	0.43	1	205.61
6	491.02	0	.	1	0	1	491	0	0.86	2	205.61
6	492.02	1	0	1	0	1	491	0	1.29	1	205.61
6	493.02	1	0	1	0	1	491	0	1.71	1	205.61
6	494.02	0	1	0	0	1	491	0	1.50	2	205.61
6	495.02	1	.	1	0	1	495	1	1.50	1	205.61
6	496.02	1	0	1	0	1	495	1	1.29	1	205.61
6	497.02	0	.	1	0	1	497	1	1.71	2	205.61
6	498.02	0	.	1	0	.	498	0	0.64	2	205.61
6	499.02	1	1	1	1	1	497	1	1.93	2	195.41
6	500.02	1	.	1	0	1	500	0	1.93	1	195.41
6	501.02	0	1	1	0	1	500	0	1.93	2	175.01
6	502.02	1	0	1	0	1	500	0	1.71	2	236.21
6	503.02	1	1	1	0	1	500	0	1.93	1	205.61
6	504.02	1	0	1	0	1	500	0	1.50	1	215.81
6	505.02	1	.	1	0	1	505	0	1.29	2	195.41
6	506.02	1	0	1	0	2	500	0	1.50	1	215.81
6	507.02	0	1	0	0	2	500	0	1.50	1	215.81
6	508.02	0	.	0	0	1	508	0	1.29	1	195.41
6	509.02	1	.	1	0	2	509	0	1.50	1	124.01
6	510.02	1	0	1	0	1	509	0	1.50	1	124.01
6	511.02	0	.	1	0	2	511	0	1.29	2	185.21

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	462.02	104.24	0.36	2.81	0.36	2.81	1	0	0	2.83
6	463.02	102.20	0.35	2.83	0.35	2.83	1	0	0	2.80
6	464.02	102.20	0.35	2.86	0.35	2.83	0		1	.
6	465.02	77.54	0.36	2.79	0.36	2.81	0		1	.
6	466.02	294.86	0.36	2.77	0.36	2.81	0		0	.
6	467.02	427.73	0.36	2.76	0.36	2.81	0		0	.
6	468.02	424.43	0.37	2.74	0.36	2.81	0		0	.
6	469.02	93.42	0.36	2.76	0.36	2.81	0		0	.
6	470.02	95.02	0.37	2.72	0.36	2.81	0		0	.
6	471.02	184.62	0.40	2.49	0.36	2.81	0		0	.
6	472.02	183.35	0.37	2.68	0.36	2.81	0		0	.
6	473.02	326.92	0.51	1.96	0.51	1.96	1	2	0	2.81
6	474.02	97.26	0.37	2.70	0.36	2.81	0		0	.
6	475.02	529.16	0.38	2.64	0.36	2.81	0		0	.
6	476.02	145.65	0.48	2.09	0.51	1.96	0		1	.
6	477.02	100.33	0.38	2.61	0.36	2.81	0		0	.
6	478.02	137.17	0.38	2.64	0.38	2.64	1	3	0	2.81
6	479.02	336.53	0.43	2.34	0.51	1.96	0		0	.
6	480.02	460.03	0.42	2.40	0.51	1.96	0		0	.
6	481.02	134.24	0.37	2.67	0.38	2.64	0		1	.
6	482.02	154.89	0.43	2.34	0.51	1.96	0		0	.
6	483.02	109.27	0.36	2.78	0.38	2.64	0		0	.
6	484.02	106.97	0.36	2.78	0.38	2.64	0		0	.
6	485.02	108.17	0.35	2.88	0.38	2.64	0		0	.
6	486.02	101.80	0.35	2.83	0.38	2.64	0		0	.
6	487.02	111.47	0.35	2.85	0.38	2.64	0		0	.
6	488.02	114.24	0.36	2.80	0.36	2.80	1	1	0	2.81
6	489.02	115.18	0.37	2.73	0.36	2.80	0		1	.
6	490.02	141.31	0.38	2.60	0.38	2.62	0		1	.
6	491.02	151.72	0.38	2.62	0.38	2.62	1	1	0	2.80
6	492.02	149.82	0.39	2.57	0.38	2.62	0		0	.
6	493.02	171.01	0.38	2.61	0.38	2.62	0		0	.
6	494.02	169.54	0.38	2.66	0.38	2.62	0		0	.
6	495.02	175.61	0.37	2.68	0.37	2.68	1	3	0	2.62
6	496.02	178.61	0.38	2.66	0.37	2.68	0		1	.
6	497.02	180.88	0.38	2.65	0.38	2.65	1	2	0	2.62
6	498.02	82.68	0.28	3.56	0.28	3.56	1	0	0	3.05
6	499.02	244.17	0.39	2.60	0.38	2.65	0		1	.
6	500.02	252.18	0.38	2.60	0.38	2.60	1	1	0	2.62
6	501.02	409.05	0.38	2.61	0.38	2.60	0		1	.
6	502.02	203.53	0.39	2.57	0.38	2.60	0		0	.
6	503.02	233.50	0.38	2.62	0.38	2.60	0		0	.
6	504.02	351.62	0.39	2.56	0.38	2.60	0		0	.
6	505.02	377.94	0.38	2.60	0.38	2.60	1	2	0	2.60
6	506.02	350.59	0.38	2.62	0.38	2.60	0		0	.
6	507.02	354.03	0.37	2.70	0.38	2.60	0		0	.
6	508.02	377.57	0.34	2.90	0.34	2.90	1	1	0	2.60
6	509.02	560.73	0.33	3.05	0.33	3.05	1	0	0	2.90
6	510.02	563.10	0.34	2.96	0.33	3.05	0		1	.
6	511.02	250.01	0.33	3.03	0.33	3.03	1	3	0	2.60

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	512.02	1	.	0	0	.	512	0	0.43	2	124.01
6	65.03	0	.	1	0	1	65	0	1.07	2	1.60
6	66.03	1	1	0	0	1	65	0	1.07	1	1.60
6	94.03	1	.	1	0	1	94	0	0.64	1	32.20
6	95.03	1	0	1	0	1	94	0	0.86	2	32.20
6	96.03	0	1	1	0	1	94	0	1.29	1	32.20
6	97.03	1	.	0	0	2	97	0	1.07	1	22.00
6	99.03	1	0	1	0	1	97	0	1.07	0	1.60
6	106.03	1	.	1	0	.	106	0	0.43	0	22.00
6	108.03	1	1	1	0	1	108	0	1.29	2	32.20
6	109.03	1	1	1	0	1	108	0	1.93	2	32.20
6	110.03	1	.	1	0	1	110	1	1.50	2	32.20
6	111.03	1	0	1	0	1	110	1	1.50	2	32.20
6	113.03	1	0	0	0	1	113	1	1.50	2	32.20
6	114.03	0	.	0	0	1	108	0	1.29	1	32.20
6	116.03	0	1	0	0	1	113	1	1.29	2	32.20
6	117.03	1	.	1	0	1	117	1	1.29	1	1.60
6	118.03	0	1	0	0	1	119	0	1.71	0	22.00
6	119.03	1	.	1	0	1	119	0	1.93	1	1.60
6	120.03	1	.	1	0	1	113	1	1.29	2	42.40
6	123.03	0	0	0	0	2	128	0	1.07	2	32.20
6	125.03	1	0	1	0	1	129	0	0.86	2	42.40
6	128.03	0	.	1	0	2	128	0	1.29	1	22.00
6	129.03	1	.	1	0	1	129	0	1.07	1	42.40
6	130.03	0	1	0	0	2	129	0	0.64	2	22.00
6	131.03	1	1	0	0	2	129	0	0.86	0	42.40
6	135.03	1	.	1	0	1	135	0	0.64	2	1.60
6	138.03	1	0	1	0	1	135	0	1.29	1	1.60
6	140.03	0	1	0	0	1	135	0	1.07	1	42.40
6	141.03	0	0	0	0	1	135	0	1.07	2	42.40
6	143.03	1	.	1	0	1	143	1	1.07	2	83.20
6	144.03	1	0	1	0	1	143	1	1.50	2	83.20
6	145.03	0	1	1	0	1	143	1	1.71	2	83.20
6	146.03	1	1	1	0	1	143	1	1.29	2	42.40
6	148.03	1	0	1	0	1	143	1	1.29	2	73.00
6	149.03	1	.	1	0	1	149	1	1.07	0	1.60
6	150.03	1	.	1	0	1	150	1	1.07	1	1.60
6	151.03	1	0	1	0	1	150	1	1.93	1	22.00
6	153.03	1	0	1	0	1	143	1	1.29	2	52.60
6	155.03	1	0	1	0	1	150	1	1.29	1	1.60
6	156.03	1	0	1	0	1	150	1	1.93	1	1.60
6	159.03	1	0	0	0	1	150	1	1.93	1	1.60
6	160.03	0	.	1	0	2	160	1	0.43	2	32.20
6	165.03	1	.	1	0	2	165	0	0.64	2	32.20
6	166.03	0	1	0	0	1	165	0	0.86	2	32.20
6	169.03	1	.	1	0	1	169	0	0.86	2	52.60
6	171.03	1	.	1	0	2	171	0	0.43	2	83.20
6	172.03	1	0	0	0	1	171	0	0.86	0	1.60
6	173.03	0	1	0	0	2	171	0	1.07	0	73.00
6	174.03	1	1	1	0	1	171	0	0.86	2	83.20

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	512.02	748.35	0.50	2.00	0.50	2.00	1	0	0	3.56
6	65.03	63.30	0.64	1.57	0.64	1.57	1	1	0	.
6	66.03	64.30	0.63	1.59	0.64	1.57	0		1	.
6	94.03	68.57	0.66	1.52	0.66	1.52	1	1	0	1.94
6	95.03	69.14	0.65	1.53	0.66	1.52	0		1	.
6	96.03	69.94	0.65	1.54	0.66	1.52	0		0	.
6	97.03	71.31	0.67	1.50	0.67	1.50	1	1	0	1.52
6	99.03	103.51	0.69	1.45	0.67	1.50	0		0	.
6	106.03	46.88	0.52	1.94	0.52	1.94	1	0	0	1.57
6	108.03	74.18	0.61	1.64	0.61	1.64	0		0	1.50
6	109.03	75.64	0.62	1.61	0.61	1.64	0		0	.
6	110.03	78.18	0.62	1.60	0.62	1.60	1	2	0	1.64
6	111.03	79.62	0.62	1.62	0.62	1.60	0		1	.
6	113.03	83.89	0.57	1.76	0.57	1.76	0		0	1.64
6	114.03	72.54	0.62	1.61	0.61	1.64	1	0	1	.
6	116.03	81.25	0.57	1.75	0.57	1.76	0		1	.
6	117.03	105.21	0.51	1.97	0.51	1.97	1	3	0	1.64
6	118.03	74.18	0.55	1.81	0.53	1.87	0		1	.
6	119.03	108.38	0.53	1.87	0.53	1.87	1	3	0	1.64
6	120.03	68.30	0.57	1.76	0.57	1.76	1	0	0	.
6	123.03	95.03	0.55	1.83	0.55	1.82	0		1	.
6	125.03	71.27	0.58	1.72	0.56	1.78	0		1	.
6	128.03	94.56	0.55	1.82	0.55	1.82	1	4	0	1.76
6	129.03	69.80	0.56	1.78	0.56	1.78	1	1	0	1.82
6	130.03	96.17	0.58	1.71	0.56	1.78	0		0	.
6	131.03	72.74	0.58	1.73	0.56	1.78	0		0	.
6	135.03	129.40	0.57	1.75	0.57	1.75	1	0	0	1.78
6	138.03	130.67	0.56	1.79	0.57	1.75	0		1	.
6	140.03	73.77	0.55	1.82	0.57	1.75	0		0	.
6	141.03	75.01	0.56	1.80	0.57	1.75	0		0	.
6	143.03	37.39	0.56	1.78	0.56	1.78	1	2	0	1.75
6	144.03	38.28	0.57	1.75	0.56	1.78	0		1	.
6	145.03	40.68	0.55	1.81	0.56	1.78	0		0	.
6	146.03	82.58	0.55	1.83	0.56	1.78	0		0	.
6	148.03	63.19	0.50	2.01	0.56	1.78	0		0	.
6	149.03	149.12	0.51	1.95	0.51	1.95	1	2	0	1.75
6	150.03	134.60	0.44	2.26	0.44	2.26	1	3	0	1.75
6	151.03	115.58	0.45	2.21	0.44	2.26	0		0	.
6	153.03	87.79	0.49	2.03	0.56	1.78	0		0	.
6	155.03	135.60	0.44	2.25	0.44	2.26	0		1	.
6	156.03	140.14	0.44	2.26	0.44	2.26	0		0	.
6	159.03	138.31	0.45	2.24	0.44	2.26	0		0	.
6	160.03	118.82	0.46	2.16	0.46	2.16	1	3	0	1.75
6	165.03	120.79	0.48	2.10	0.48	2.10	1	1	0	1.75
6	166.03	121.96	0.48	2.07	0.48	2.10	0		1	.
6	169.03	90.99	0.54	1.85	0.54	1.85	1	4	0	2.10
6	171.03	48.95	0.55	1.82	0.55	1.82	1	1	0	1.85
6	172.03	164.83	0.54	1.85	0.55	1.82	0		1	.
6	173.03	79.27	0.54	1.84	0.55	1.82	0		0	.
6	174.03	55.19	0.54	1.85	0.55	1.82	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	175.03	1	0	1	0	1	171	0	1.29	2	83.20
6	176.03	1	.	1	0	1	176	1	1.50	2	83.20
6	177.03	1	0	0	0	1	176	1	1.71	2	83.20
6	178.03	0	1	0	0	1	176	1	1.29	2	103.60
6	179.03	1	.	1	0	1	179	1	1.07	1	83.20
6	180.03	0	1	1	0	1	179	1	1.50	1	83.20
6	181.03	0	0	1	0	1	176	1	1.07	0	52.60
6	182.03	1	1	1	0	2	179	1	1.29	1	52.60
6	183.03	1	.	1	0	1	183	0	0.64	1	32.20
6	184.03	1	0	1	0	1	183	0	1.29	2	42.40
6	185.03	1	0	0	0	1	183	0	1.07	1	42.40
6	186.03	1	0	1	0	1	183	0	0.86	2	83.20
6	187.03	1	0	1	0	1	183	0	0.86	2	103.60
6	188.03	1	0	1	1	1	183	0	0.86	2	52.60
6	189.03	1	0	1	0	1	183	0	0.86	2	83.20
6	190.03	1	0	1	0	1	183	0	0.86	2	52.60
6	191.03	1	.	0	1	2	191	0	0.64	2	52.60
6	192.03	1	0	1	0	1	191	0	1.07	2	52.60
6	193.03	1	0	1	0	1	191	0	1.07	1	22.00
6	194.03	1	.	1	0	1	194	0	0.86	1	42.40
6	195.03	1	.	1	0	1	195	0	0.86	1	22.00
6	196.03	1	.	1	0	1	196	0	1.29	2	73.00
6	197.03	1	0	1	0	1	196	0	0.86	1	73.00
6	198.03	1	0	1	0	1	196	0	1.50	1	52.60
6	199.03	1	0	1	0	1	196	0	1.93	2	73.00
6	200.03	1	0	1	0	2	196	0	1.50	2	73.00
6	201.03	1	0	1	0	1	196	0	1.07	1	52.60
6	202.03	1	0	0	0	1	196	0	1.71	1	52.60
6	203.03	1	0	1	0	1	196	0	1.50	2	52.60
6	204.03	1	0	1	0	1	196	0	1.50	0	22.00
6	211.03	1	.	0	0	1	211	0	1.71	1	83.20
6	212.03	0	1	1	0	1	211	0	1.71	2	83.20
6	213.03	0	.	0	0	1	213	1	1.71	2	83.20
6	214.03	0	0	0	0	1	211	0	1.93	0	83.20
6	215.03	1	.	1	0	1	215	1	1.71	1	22.00
6	216.03	1	0	1	0	1	215	1	1.29	1	22.00
6	219.03	0	.	0	0	1	219	0	1.29	0	62.80
6	220.03	0	0	0	0	1	213	1	1.50	2	62.80
6	222.03	0	0	1	0	2	219	0	0.86	2	62.80
6	223.03	0	1	0	0	1	215	1	1.71	1	83.20
6	224.03	1	1	1	0	1	219	0	0.86	1	52.60
6	225.03	1	.	1	0	2	225	0	0.86	1	32.20
6	228.03	1	0	1	0	1	225	0	1.07	2	32.20
6	229.03	1	0	1	0	1	225	0	1.29	1	32.20
6	230.03	0	1	0	0	1	225	0	1.50	1	32.20
6	231.03	0	0	0	0	1	225	0	1.29	1	83.20
6	232.03	0	0	0	1	1	225	0	1.50	2	83.20
6	233.03	1	1	1	0	2	225	0	0.86	0	83.20
6	234.03	0	.	0	0	1	234	0	1.29	2	83.20
6	235.03	1	.	1	0	1	235	0	1.29	1	52.60

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	175.03	61.63	0.55	1.82	0.55	1.82	0		0	.
6	176.03	62.50	0.55	1.83	0.55	1.83	1	2	0	1.82
6	177.03	63.67	0.56	1.79	0.55	1.83	0		1	.
6	178.03	64.80	0.58	1.73	0.55	1.83	0		0	.
6	179.03	47.82	0.52	1.94	0.52	1.94	1	3	0	1.82
6	180.03	53.52	0.53	1.90	0.52	1.94	0		1	.
6	181.03	117.98	0.57	1.76	0.55	1.83	0		0	.
6	182.03	114.75	0.53	1.89	0.52	1.94	0		0	.
6	183.03	146.22	0.54	1.84	0.54	1.84	1	0	0	1.82
6	184.03	124.19	0.55	1.83	0.54	1.84	0		1	.
6	185.03	123.16	0.54	1.84	0.54	1.84	0		0	.
6	186.03	65.57	0.54	1.85	0.54	1.84	0		0	.
6	187.03	68.81	0.54	1.84	0.54	1.84	0		0	.
6	188.03	128.49	0.54	1.86	0.54	1.84	0		0	.
6	189.03	68.97	0.53	1.89	0.54	1.84	0		0	.
6	190.03	133.23	0.53	1.90	0.54	1.84	0		0	.
6	191.03	132.63	0.54	1.84	0.54	1.84	1	1	0	1.84
6	192.03	134.77	0.55	1.81	0.54	1.84	0		0	.
6	193.03	164.47	0.54	1.86	0.54	1.84	0		1	.
6	194.03	134.07	0.59	1.70	0.59	1.70	1	2	0	1.84
6	195.03	165.37	0.51	1.97	0.51	1.97	1	3	0	1.84
6	196.03	100.73	0.54	1.86	0.54	1.86	1	1	0	1.84
6	197.03	99.96	0.53	1.89	0.54	1.86	0		1	.
6	198.03	137.50	0.53	1.90	0.54	1.86	0		0	.
6	199.03	103.36	0.53	1.87	0.54	1.86	0		0	.
6	200.03	104.20	0.54	1.86	0.54	1.86	0		0	.
6	201.03	139.61	0.55	1.83	0.54	1.86	0		0	.
6	202.03	140.54	0.55	1.81	0.54	1.86	0		0	.
6	203.03	143.08	0.55	1.83	0.54	1.86	0		0	.
6	204.03	179.11	0.55	1.83	0.54	1.86	0		0	.
6	211.03	70.78	0.51	1.94	0.51	1.94	1	4	0	1.86
6	212.03	72.98	0.49	2.03	0.51	1.94	0		1	.
6	213.03	75.91	0.49	2.05	0.49	2.05	1	2	0	1.94
6	214.03	77.65	0.50	1.99	0.51	1.94	0		0	.
6	215.03	181.28	0.45	2.22	0.45	2.22	1	3	0	1.94
6	216.03	180.12	0.45	2.25	0.45	2.22	0		1	.
6	219.03	112.74	0.45	2.23	0.45	2.23	1	1	0	1.94
6	220.03	109.04	0.46	2.19	0.49	2.05	0		1	.
6	222.03	113.94	0.44	2.26	0.45	2.23	0		1	.
6	223.03	73.51	0.44	2.28	0.45	2.22	0		0	.
6	224.03	153.12	0.45	2.25	0.45	2.23	0		0	.
6	225.03	192.53	0.45	2.24	0.45	2.24	1	0	0	2.23
6	228.03	195.90	0.45	2.24	0.45	2.24	0		1	.
6	229.03	193.86	0.44	2.26	0.45	2.24	0		0	.
6	230.03	196.67	0.44	2.26	0.45	2.24	0		0	.
6	231.03	78.85	0.44	2.27	0.45	2.24	0		0	.
6	232.03	80.75	0.44	2.28	0.45	2.24	0		0	.
6	233.03	82.49	0.44	2.27	0.45	2.24	0		0	.
6	234.03	83.22	0.44	2.26	0.44	2.26	1	3	0	2.24
6	235.03	158.29	0.46	2.19	0.46	2.19	1	2	0	2.24

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	236.03	0	0	0	0	1	237	0	1.50	1	52.60
6	237.03	0	.	1	0	1	237	0	1.50	2	83.20
6	238.03	1	1	1	0	1	237	0	1.71	1	83.20
6	239.03	0	0	1	0	1	237	0	1.71	2	83.20
6	240.03	1	0	1	0	2	237	0	1.50	1	62.80
6	241.03	0	0	0	0	1	237	0	1.93	0	83.20
6	242.03	0	0	0	0	1	237	0	1.71	1	83.20
6	243.03	0	0	1	0	1	237	0	1.29	1	103.60
6	244.03	1	1	1	0	1	237	0	1.93	2	83.20
6	245.03	0	1	0	0	1	237	0	1.93	1	83.20
6	246.03	0	0	0	0	1	237	0	2.14	1	103.60
6	247.03	0	1	0	0	1	237	0	1.50	2	83.20
6	248.03	0	0	0	0	1	237	0	2.36	1	103.60
6	249.03	1	1	1	0	1	237	0	2.36	1	103.60
6	250.03	0	0	1	0	1	237	0	2.14	2	83.20
6	251.03	0	0	0	0	1	237	0	2.57	2	83.20
6	252.03	0	1	0	0	1	237	0	2.14	1	103.60
6	253.03	1	.	1	0	1	253	1	2.36	1	103.60
6	254.03	1	0	1	0	1	237	0	2.36	2	103.60
6	255.03	0	0	0	0	1	257	1	2.57	0	103.60
6	256.03	0	0	0	0	1	257	1	2.14	2	83.20
6	257.03	0	.	0	0	1	257	1	2.57	2	103.60
6	258.03	1	0	1	0	1	253	1	2.57	1	83.20
6	259.03	1	0	1	0	1	253	1	2.36	1	83.20
6	260.03	1	0	1	0	1	253	1	2.57	1	83.20
6	261.03	0	1	1	0	1	253	1	2.14	1	103.60
6	262.03	1	1	1	0	1	257	1	2.14	2	52.60
6	263.03	0	.	1	0	1	263	0	1.71	1	83.20
6	264.03	1	1	0	0	1	263	0	1.71	2	103.60
6	265.03	1	0	1	0	1	263	0	1.50	1	103.60
6	266.03	1	0	1	0	1	263	0	1.93	2	103.60
6	267.03	0	1	1	0	1	263	0	1.50	1	83.20
6	268.03	1	1	1	0	1	263	0	1.93	2	83.20
6	269.03	1	0	0	0	1	263	0	1.71	1	52.60
6	270.03	1	0	1	0	1	263	0	2.36	2	103.60
6	271.03	0	1	0	0	1	263	0	2.14	1	52.60
6	272.03	1	1	1	0	2	263	0	1.93	1	103.60
6	273.03	1	0	0	0	1	263	0	2.14	2	83.20
6	274.03	0	1	1	0	1	263	0	1.93	1	83.20
6	275.03	1	1	1	0	1	263	0	2.14	2	103.60
6	276.03	1	0	1	0	1	263	0	1.93	1	103.60
6	277.03	1	0	1	0	1	263	0	1.93	2	154.61
6	278.03	1	0	1	0	1	263	0	2.36	1	73.00
6	279.03	1	.	1	0	1	279	1	1.93	2	103.60
6	280.03	0	.	0	0	1	280	1	1.93	1	73.00
6	281.03	1	0	1	0	1	279	1	1.71	2	103.60
6	282.03	1	1	1	0	1	280	1	1.93	2	103.60
6	283.03	0	0	1	0	1	280	1	2.14	1	83.20
6	284.03	1	0	1	0	1	280	1	2.14	1	185.21
6	285.03	1	0	1	1	1	285	0	1.50	2	134.21

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	236.03	161.39	0.45	2.24	0.44	2.25	0		1	.
6	237.03	86.89	0.44	2.25	0.44	2.25	1	1	0	2.24
6	238.03	84.59	0.45	2.21	0.44	2.25	0		0	.
6	239.03	93.30	0.46	2.17	0.44	2.25	0		0	.
6	240.03	123.92	0.46	2.18	0.44	2.25	0		0	.
6	241.03	98.40	0.45	2.24	0.44	2.25	0		0	.
6	242.03	97.27	0.44	2.25	0.44	2.25	0		0	.
6	243.03	90.43	0.45	2.21	0.44	2.25	0		0	.
6	244.03	95.10	0.42	2.36	0.44	2.25	0		0	.
6	245.03	101.74	0.42	2.37	0.44	2.25	0		0	.
6	246.03	98.40	0.42	2.41	0.44	2.25	0		0	.
6	247.03	91.80	0.45	2.22	0.44	2.25	0		0	.
6	248.03	105.08	0.40	2.49	0.44	2.25	0		0	.
6	249.03	106.34	0.40	2.49	0.44	2.25	0		0	.
6	250.03	105.98	0.41	2.42	0.44	2.25	0		0	.
6	251.03	108.28	0.39	2.54	0.44	2.25	0		0	.
6	252.03	112.38	0.40	2.51	0.44	2.25	0		0	.
6	253.03	113.78	0.40	2.50	0.40	2.50	1	2	0	2.25
6	254.03	116.25	0.39	2.55	0.44	2.25	0		0	.
6	255.03	121.79	0.39	2.55	0.39	2.56	0		1	.
6	256.03	120.69	0.39	2.59	0.39	2.56	0		0	.
6	257.03	119.86	0.39	2.56	0.39	2.56	1	3	0	2.25
6	258.03	111.08	0.40	2.51	0.40	2.50	0		1	.
6	259.03	112.95	0.40	2.51	0.40	2.50	0		0	.
6	260.03	99.74	0.40	2.52	0.40	2.50	0		0	.
6	261.03	118.46	0.39	2.55	0.40	2.50	0		0	.
6	262.03	191.22	0.38	2.64	0.39	2.56	0		0	.
6	263.03	119.29	0.39	2.55	0.39	2.55	1	1	0	2.25
6	264.03	125.33	0.38	2.60	0.39	2.55	0		1	.
6	265.03	123.63	0.40	2.49	0.39	2.55	0		0	.
6	266.03	126.73	0.39	2.55	0.39	2.55	0		0	.
6	267.03	128.87	0.39	2.54	0.39	2.55	0		0	.
6	268.03	127.70	0.40	2.52	0.39	2.55	0		0	.
6	269.03	198.40	0.39	2.54	0.39	2.55	0		0	.
6	270.03	132.70	0.40	2.50	0.39	2.55	0		0	.
6	271.03	199.93	0.40	2.52	0.39	2.55	0		0	.
6	272.03	131.37	0.40	2.52	0.39	2.55	0		0	.
6	273.03	130.67	0.39	2.54	0.39	2.55	0		0	.
6	274.03	133.34	0.39	2.54	0.39	2.55	0		0	.
6	275.03	135.61	0.39	2.53	0.39	2.55	0		0	.
6	276.03	137.27	0.40	2.53	0.39	2.55	0		0	.
6	277.03	55.73	0.39	2.53	0.39	2.55	0		0	.
6	278.03	177.64	0.40	2.52	0.39	2.55	0		0	.
6	279.03	140.41	0.39	2.55	0.39	2.55	1	3	0	2.55
6	280.03	180.74	0.40	2.51	0.40	2.51	1	2	0	2.55
6	281.03	139.28	0.39	2.57	0.39	2.55	0		1	.
6	282.03	142.01	0.39	2.57	0.40	2.51	0		0	.
6	283.03	134.87	0.40	2.53	0.40	2.51	0		1	.
6	284.03	44.25	0.39	2.56	0.40	2.51	0		0	.
6	285.03	86.55	0.35	2.84	0.35	2.84	0		0	2.55

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	287.03	1	.	0	0	1	287	1	1.71	0	134.21
6	288.03	1	0	1	0	1	285	0	1.29	2	134.21
6	289.03	1	0	1	0	1	289	1	1.29	1	124.01
6	290.03	0	1	0	0	1	289	1	1.29	1	52.60
6	291.03	1	1	1	0	1	289	1	1.71	1	22.00
6	292.03	1	1	1	0	1	295	1	1.93	2	124.01
6	293.03	1	0	1	0	1	289	1	1.93	1	83.20
6	294.03	1	1	1	0	1	295	1	1.29	0	124.01
6	295.03	0	.	1	0	1	295	1	1.07	2	83.20
6	296.03	0	1	1	0	1	295	1	1.50	2	154.61
6	297.03	0	1	0	0	1	295	1	1.29	2	124.01
6	298.03	1	1	1	0	1	295	1	1.07	2	144.41
6	299.03	1	0	1	0	1	285	0	1.07	2	22.00
6	300.03	1	0	1	0	1	295	1	1.50	2	124.01
6	301.03	1	0	0	0	1	295	1	1.50	2	103.60
6	302.03	1	0	1	0	1	295	1	1.50	2	103.60
6	303.03	1	1	0	0	2	295	1	1.71	2	124.01
6	304.03	1	0	1	0	1	295	1	1.50	2	103.60
6	305.03	1	0	0	0	1	311	1	1.93	1	124.01
6	306.03	0	1	0	0	1	295	1	1.71	2	103.60
6	307.03	0	0	0	0	1	295	1	1.93	2	124.01
6	308.03	1	0	0	0	1	311	1	1.93	1	124.01
6	309.03	0	1	1	0	1	295	1	1.71	0	103.60
6	310.03	1	0	1	0	1	311	1	1.29	1	103.60
6	311.03	1	.	1	0	1	311	1	1.29	1	22.00
6	312.03	1	1	1	0	1	311	1	1.93	1	62.80
6	313.03	1	0	1	0	1	311	1	1.50	1	83.20
6	314.03	0	1	0	0	1	311	1	2.14	1	83.20
6	315.03	1	0	1	0	1	295	1	1.29	2	124.01
6	316.03	0	0	1	0	1	295	1	1.50	2	185.21
6	317.03	1	1	1	0	1	295	1	1.50	2	103.60
6	318.03	1	0	1	0	1	318	1	1.29	1	83.20
6	319.03	1	.	1	0	1	319	1	1.50	0	83.20
6	320.03	1	0	1	0	1	318	1	1.71	1	83.20
6	321.03	1	0	0	0	1	319	1	1.07	2	103.60
6	322.03	1	.	1	0	1	322	1	1.50	1	103.60
6	323.03	1	0	1	0	1	324	0	1.29	2	154.61
6	324.03	1	.	1	0	1	324	0	1.50	1	103.60
6	325.03	0	.	0	0	1	325	0	1.50	2	124.01
6	326.03	0	.	0	0	1	326	0	1.07	1	103.60
6	327.03	1	1	1	0	1	328	0	1.29	2	124.01
6	328.03	0	.	1	0	1	328	0	1.50	1	103.60
6	329.03	1	0	1	0	2	328	0	0.86	2	103.60
6	330.03	1	1	1	0	1	328	0	0.86	1	83.20
6	331.03	0	1	0	0	1	328	0	1.07	2	83.20
6	332.03	0	1	0	0	1	328	0	1.29	1	103.60
6	333.03	1	0	0	0	1	328	0	1.71	1	124.01
6	334.03	1	1	1	0	1	328	0	1.29	2	124.01
6	335.03	1	0	1	0	1	328	0	1.50	1	103.60
6	336.03	1	0	1	0	1	328	0	1.93	2	103.60

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	287.03	91.15	0.38	2.60	0.38	2.60	1	2	0	2.55
6	288.03	88.85	0.36	2.76	0.35	2.84	0		1	.
6	289.03	86.12	0.43	2.33	0.43	2.33	0		0	2.55
6	290.03	240.57	0.43	2.32	0.43	2.33	0		1	.
6	291.03	280.18	0.43	2.30	0.43	2.33	0		0	.
6	292.03	89.26	0.32	3.15	0.37	2.73	0		0	.
6	293.03	167.57	0.42	2.38	0.43	2.33	0		0	.
6	294.03	83.71	0.35	2.86	0.37	2.73	0		1	.
6	295.03	139.78	0.37	2.73	0.37	2.73	1	3	0	2.55
6	296.03	61.50	0.32	3.14	0.37	2.73	0		0	.
6	297.03	87.35	0.34	2.97	0.37	2.73	0		0	.
6	298.03	75.88	0.32	3.14	0.37	2.73	0		0	.
6	299.03	262.20	0.36	2.81	0.35	2.84	0		0	.
6	300.03	98.69	0.32	3.13	0.37	2.73	0		0	.
6	301.03	165.57	0.32	3.12	0.37	2.73	0		0	.
6	302.03	167.10	0.32	3.16	0.37	2.73	0		0	.
6	303.03	103.47	0.34	2.91	0.37	2.73	0		0	.
6	304.03	169.11	0.32	3.13	0.37	2.73	0		0	.
6	305.03	102.37	0.34	2.97	0.36	2.80	0		0	.
6	306.03	172.08	0.33	3.07	0.37	2.73	0		0	.
6	307.03	104.40	0.32	3.08	0.37	2.73	0		0	.
6	308.03	100.73	0.34	2.93	0.36	2.80	0		0	.
6	309.03	192.20	0.38	2.61	0.37	2.73	0		0	.
6	310.03	188.96	0.39	2.58	0.36	2.80	0		0	.
6	311.03	282.08	0.36	2.80	0.36	2.80	1	2	0	2.55
6	312.03	218.21	0.34	2.92	0.36	2.80	0		0	.
6	313.03	170.21	0.36	2.80	0.36	2.80	0		1	.
6	314.03	171.68	0.35	2.84	0.36	2.80	0		0	.
6	315.03	106.37	0.34	2.93	0.37	2.73	0		0	.
6	316.03	45.88	0.33	3.00	0.37	2.73	0		0	.
6	317.03	186.22	0.33	3.00	0.37	2.73	0		0	.
6	318.03	183.42	0.39	2.54	0.39	2.54	0		0	2.55
6	319.03	185.36	0.36	2.79	0.36	2.79	1	3	0	2.55
6	320.03	185.39	0.40	2.50	0.39	2.54	0		1	.
6	321.03	190.26	0.39	2.58	0.36	2.79	0		1	.
6	322.03	185.62	0.36	2.76	0.36	2.76	1	3	0	2.55
6	323.03	87.06	0.38	2.62	0.37	2.68	0		1	.
6	324.03	190.72	0.37	2.68	0.37	2.68	1	1	0	2.55
6	325.03	108.49	0.38	2.61	0.38	2.61	1	3	0	2.68
6	326.03	194.83	0.39	2.54	0.39	2.54	1	2	0	2.68
6	327.03	110.07	0.39	2.54	0.39	2.54	0		1	.
6	328.03	196.57	0.39	2.54	0.39	2.54	1	1	0	2.68
6	329.03	202.77	0.39	2.55	0.39	2.54	0		0	.
6	330.03	198.04	0.39	2.55	0.39	2.54	0		0	.
6	331.03	201.71	0.39	2.55	0.39	2.54	0		0	.
6	332.03	198.30	0.39	2.55	0.39	2.54	0		0	.
6	333.03	113.21	0.39	2.56	0.39	2.54	0		0	.
6	334.03	112.04	0.39	2.53	0.39	2.54	0		0	.
6	335.03	214.89	0.39	2.55	0.39	2.54	0		0	.
6	336.03	217.09	0.39	2.57	0.39	2.54	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	337.03	1	0	1	0	1	328	0	1.71	2	103.60
6	338.03	1	0	1	0	1	328	0	1.93	1	73.00
6	339.03	1	0	1	0	1	328	0	1.93	2	103.60
6	340.03	1	0	1	0	1	328	0	1.93	1	103.60
6	341.03	0	.	1	0	1	341	0	1.93	1	185.21
6	342.03	0	1	1	0	1	328	0	1.93	1	103.60
6	343.03	1	1	0	0	2	328	0	1.50	1	103.60
6	344.03	0	0	0	0	1	328	0	1.50	1	134.21
6	345.03	0	1	1	0	2	328	0	1.71	2	134.21
6	346.03	1	1	1	0	1	328	0	2.14	2	124.01
6	347.03	1	0	1	0	1	328	0	1.71	1	103.60
6	348.03	1	.	1	0	1	348	0	2.14	0	185.21
6	349.03	0	.	0	0	1	349	0	2.14	1	185.21
6	350.03	0	.	0	0	1	350	1	2.14	2	134.21
6	351.03	0	1	1	0	1	350	1	1.93	2	103.60
6	352.03	0	0	1	1	1	350	1	1.71	2	124.01
6	353.03	1	1	1	0	1	350	1	2.14	2	103.60
6	354.03	1	.	1	0	1	354	1	2.14	0	185.21
6	355.03	1	1	1	0	1	350	1	1.93	2	103.60
6	356.03	1	0	1	0	1	350	1	2.14	2	103.60
6	357.03	1	.	0	0	1	357	1	2.14	1	103.60
6	358.03	1	.	1	0	1	358	1	2.14	2	73.00
6	359.03	1	0	0	0	1	357	1	2.57	1	103.60
6	360.03	1	.	1	0	1	360	0	1.71	1	103.60
6	361.03	1	0	1	0	1	357	1	2.57	1	103.60
6	362.03	1	.	1	0	1	362	1	1.71	1	103.60
6	363.03	0	1	0	0	1	357	1	1.93	1	103.60
6	364.03	0	.	0	0	2	364	0	0.86	2	73.00
6	365.03	0	.	1	0	1	365	0	1.29	1	83.20
6	366.03	1	.	1	0	1	366	0	1.29	0	103.60
6	367.03	0	.	0	0	1	367	0	0.86	0	144.41
6	368.03	0	.	0	0	1	368	0	0.64	2	144.41
6	369.03	1	.	1	0	1	369	0	1.07	2	103.60
6	370.03	0	.	1	0	1	370	0	1.07	0	83.20
6	371.03	0	.	0	0	1	371	0	0.86	1	103.60
6	372.03	1	0	1	0	1	373	0	1.07	0	185.21
6	373.03	1	.	0	0	1	373	0	1.29	2	185.21
6	374.03	1	0	1	0	2	373	0	1.50	1	185.21
6	375.03	0	.	1	0	3	375	0	0.86	2	185.21
6	376.03	1	0	0	0	1	373	0	1.29	1	185.21
6	377.03	1	0	0	0	1	373	0	1.29	2	185.21
6	378.03	1	.	1	0	1	378	0	0.86	1	144.41
6	379.03	0	.	1	0	2	379	0	1.07	0	154.61
6	380.03	0	.	1	0	2	380	0	1.29	2	73.00
6	381.03	0	.	1	0	1	381	0	1.29	2	185.21
6	382.03	1	.	1	0	1	382	0	1.50	1	185.21
6	383.03	1	.	1	0	1	383	0	0.86	2	103.60
6	384.03	1	.	1	0	2	384	0	1.07	2	103.60
6	385.03	1	.	1	0	2	385	0	1.29	2	1.60
6	386.03	1	.	1	0	2	386	0	0.64	2	103.60

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	337.03	219.29	0.39	2.58	0.39	2.54	0		0	.
6	338.03	185.61	0.38	2.61	0.39	2.54	0		0	.
6	339.03	207.81	0.39	2.57	0.39	2.54	0		0	.
6	340.03	203.14	0.38	2.60	0.39	2.54	0		0	.
6	341.03	51.95	0.45	2.24	0.45	2.24	1	2	0	2.38
6	342.03	205.34	0.39	2.59	0.39	2.54	0		0	.
6	343.03	211.08	0.38	2.62	0.39	2.54	0		0	.
6	344.03	114.71	0.39	2.59	0.39	2.54	0		0	.
6	345.03	114.94	0.38	2.61	0.39	2.54	0		0	.
6	346.03	117.78	0.39	2.55	0.39	2.54	0		0	.
6	347.03	231.57	0.38	2.61	0.39	2.54	0		0	.
6	348.03	56.39	0.42	2.38	0.42	2.38	1	1	0	2.54
6	349.03	54.46	0.42	2.38	0.42	2.38	1	3	0	2.38
6	350.03	119.68	0.39	2.57	0.39	2.57	1	3	0	2.38
6	351.03	238.08	0.40	2.47	0.39	2.57	0		0	.
6	352.03	124.62	0.40	2.51	0.39	2.57	0		1	.
6	353.03	228.77	0.40	2.49	0.39	2.57	0		0	.
6	354.03	55.02	0.40	2.50	0.40	2.50	1	1	0	2.49
6	355.03	237.64	0.40	2.53	0.39	2.57	0		0	.
6	356.03	240.58	0.40	2.52	0.39	2.57	0		0	.
6	357.03	213.48	0.41	2.44	0.41	2.44	1	2	0	2.38
6	358.03	317.78	0.42	2.40	0.42	2.40	1	2	0	2.49
6	359.03	215.92	0.41	2.43	0.41	2.44	0		1	.
6	360.03	230.10	0.40	2.49	0.40	2.49	1	1	0	2.38
6	361.03	216.59	0.41	2.43	0.41	2.44	0		0	.
6	362.03	237.71	0.40	2.50	0.40	2.50	1	3	0	2.49
6	363.03	221.89	0.41	2.44	0.41	2.44	0		0	.
6	364.03	316.31	0.41	2.45	0.41	2.45	1	3	0	2.50
6	365.03	88.39	0.56	1.79	0.56	1.79	1	2	0	2.50
6	366.03	253.06	0.57	1.76	0.57	1.76	1	2	0	2.20
6	367.03	94.90	0.45	2.20	0.45	2.20	1	1	0	2.50
6	368.03	89.39	0.47	2.14	0.47	2.14	1	3	0	2.20
6	369.03	231.80	0.49	2.05	0.49	2.05	1	2	0	2.20
6	370.03	90.13	0.46	2.16	0.46	2.16	1	3	0	2.20
6	371.03	241.28	0.50	2.02	0.50	2.02	1	1	0	2.20
6	372.03	51.35	0.51	1.96	0.53	1.89	0		1	.
6	373.03	50.85	0.53	1.89	0.53	1.89	1	1	0	2.02
6	374.03	53.62	0.50	1.98	0.53	1.89	0		0	.
6	375.03	49.18	0.51	1.96	0.51	1.96	1	0	0	1.89
6	376.03	57.79	0.50	1.99	0.53	1.89	0		0	.
6	377.03	57.39	0.52	1.91	0.53	1.89	0		0	.
6	378.03	93.06	0.46	2.18	0.46	2.18	1	3	0	1.96
6	379.03	94.70	0.52	1.93	0.52	1.93	1	2	0	1.96
6	380.03	201.53	0.50	2.01	0.50	2.01	1	1	0	1.96
6	381.03	60.20	0.54	1.86	0.54	1.86	1	2	0	2.01
6	382.03	59.33	0.48	2.07	0.48	2.07	1	3	0	2.01
6	383.03	248.19	0.55	1.81	0.55	1.81	1	1	0	1.82
6	384.03	250.85	0.55	1.82	0.55	1.82	1	1	0	2.01
6	385.03	477.21	0.56	1.80	0.56	1.80	1	3	0	1.81
6	386.03	276.01	0.58	1.71	0.58	1.71	1	1	0	1.81

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	387.03	1	.	1	0	2	387	0	1.07	2	103.60
6	388.03	1	.	1	0	1	388	0	0.86	2	164.81
6	389.03	0	.	1	0	1	389	0	0.86	1	205.61
6	390.03	0	1	1	0	1	391	0	1.07	2	103.60
6	391.03	1	.	1	0	1	391	0	1.29	2	164.81
6	392.03	1	.	0	0	1	392	0	0.86	1	103.60
6	393.03	0	.	0	0	2	393	0	0.86	0	164.81
6	394.03	0	0	0	0	1	380	0	1.29	1	164.81
6	395.03	0	1	0	0	1	387	0	0.86	1	83.20
6	396.03	0	.	1	0	2	396	0	1.50	2	185.21
6	397.03	0	.	0	0	1	397	0	1.71	0	154.61
6	398.03	0	0	1	0	2	391	0	1.07	1	103.60
6	399.03	1	.	1	0	2	399	0	0.64	2	134.21
6	400.03	1	.	1	0	1	400	0	0.64	2	134.21
6	401.03	0	1	0	0	2	400	0	0.64	2	134.21
6	402.03	0	.	1	0	1	402	0	1.07	2	134.21
6	403.03	0	.	1	0	1	403	0	1.07	2	154.61
6	404.03	1	.	1	0	1	404	0	1.50	1	103.60
6	405.03	1	.	1	0	1	405	0	1.71	1	103.60
6	406.03	0	.	1	0	1	406	0	1.07	1	185.21
6	407.03	1	0	1	0	1	406	0	1.29	1	185.21
6	408.03	1	0	1	0	1	406	0	1.29	2	175.01
6	409.03	1	1	1	0	1	406	0	1.07	1	185.21
6	410.03	1	0	1	0	2	406	0	1.50	2	175.01
6	411.03	0	1	1	0	1	406	0	1.29	1	175.01
6	412.03	1	.	1	0	3	412	1	0.64	2	144.41
6	413.03	1	0	1	0	1	412	1	1.29	2	144.41
6	414.03	1	0	1	0	1	412	1	1.93	2	144.41
6	415.03	1	0	1	0	1	412	1	1.93	2	215.81
6	416.03	1	.	1	0	1	416	1	0.86	1	103.60
6	417.03	0	1	1	0	1	416	1	1.29	1	185.21
6	418.03	0	.	1	0	1	418	0	1.93	1	185.21
6	419.03	0	0	0	0	1	416	1	1.71	1	185.21
6	420.03	0	0	1	0	2	418	0	1.71	1	185.21
6	421.03	1	0	0	0	1	418	0	1.71	2	144.41
6	422.03	1	0	1	0	1	418	0	1.50	1	175.01
6	423.03	1	1	1	0	1	418	0	1.71	1	144.41
6	424.03	1	1	1	0	1	418	0	2.14	2	175.01
6	425.03	0	1	1	0	2	418	0	2.14	1	175.01
6	426.03	1	.	0	0	2	426	0	0.43	1	73.00
6	427.03	1	.	1	0	1	427	0	1.29	1	73.00
6	428.03	1	0	1	0	1	418	0	1.93	1	175.01
6	429.03	0	1	1	0	2	418	0	2.36	1	185.21
6	430.03	1	.	1	0	1	430	0	1.93	1	42.40
6	431.03	0	0	0	0	1	430	0	1.93	1	83.20
6	432.03	0	.	1	0	1	432	0	2.14	1	164.81
6	433.03	1	.	1	0	1	433	0	1.71	1	164.81
6	434.03	1	0	1	1	2	433	0	1.71	0	185.21
6	435.03	1	.	1	0	2	435	0	1.71	2	164.81
6	436.03	1	1	1	0	1	418	0	1.93	2	175.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	387.03	273.18	0.59	1.69	0.59	1.69	1	1	0	1.71
6	388.03	81.08	0.70	1.43	0.70	1.43	1	0	0	1.33
6	389.03	30.19	0.69	1.46	0.69	1.46	1	2	0	1.81
6	390.03	282.69	0.66	1.51	0.70	1.43	0		1	.
6	391.03	84.72	0.70	1.43	0.70	1.43	1	1	0	1.43
6	392.03	224.86	0.39	2.57	0.39	2.57	1	3	0	1.96
6	393.03	86.75	0.57	1.76	0.57	1.76	1	3	0	1.43
6	394.03	83.01	0.49	2.04	0.50	2.01	0		1	.
6	395.03	256.46	0.62	1.62	0.59	1.69	0		1	.
6	396.03	66.80	0.75	1.33	0.75	1.33	1	1	0	1.69
6	397.03	125.06	0.71	1.40	0.71	1.40	1	2	0	1.43
6	398.03	287.59	0.68	1.48	0.70	1.43	0		0	.
6	399.03	156.52	0.56	1.79	0.56	1.79	1	0	0	1.43
6	400.03	158.59	0.54	1.84	0.54	1.84	1	0	0	1.79
6	401.03	160.32	0.54	1.85	0.54	1.84	0		1	.
6	402.03	161.96	0.54	1.86	0.54	1.86	1	2	0	1.84
6	403.03	128.60	0.49	2.04	0.49	2.04	1	2	0	1.84
6	404.03	305.98	0.44	2.27	0.44	2.27	1	1	0	1.84
6	405.03	304.21	0.44	2.27	0.44	2.27	1	3	0	1.84
6	406.03	72.11	0.45	2.23	0.45	2.23	1	1	0	2.27
6	407.03	69.80	0.46	2.19	0.45	2.23	0		0	.
6	408.03	104.13	0.45	2.23	0.45	2.23	0		0	.
6	409.03	70.44	0.46	2.19	0.45	2.23	0		1	.
6	410.03	107.87	0.45	2.22	0.45	2.23	0		0	.
6	411.03	110.87	0.45	2.22	0.45	2.23	0		0	.
6	412.03	145.48	0.47	2.12	0.47	2.12	1	0	0	2.23
6	413.03	148.35	0.46	2.16	0.47	2.12	0		1	.
6	414.03	148.75	0.46	2.19	0.47	2.12	0		0	.
6	415.03	67.46	0.46	2.16	0.47	2.12	0		0	.
6	416.03	321.39	0.45	2.23	0.45	2.23	1	3	0	2.12
6	417.03	77.45	0.44	2.25	0.45	2.23	0		1	.
6	418.03	73.64	0.44	2.26	0.44	2.26	1	1	0	2.12
6	419.03	74.91	0.45	2.24	0.45	2.23	0		0	.
6	420.03	79.21	0.44	2.26	0.44	2.26	0		1	.
6	421.03	169.64	0.45	2.23	0.44	2.26	0		0	.
6	422.03	131.23	0.44	2.25	0.44	2.26	0		0	.
6	423.03	168.32	0.44	2.25	0.44	2.26	0		0	.
6	424.03	144.78	0.45	2.23	0.44	2.26	0		0	.
6	425.03	140.90	0.44	2.25	0.44	2.26	0		0	.
6	426.03	310.84	0.35	2.88	0.35	2.88	1	3	0	1.84
6	427.03	312.77	0.35	2.89	0.35	2.89	1	3	0	1.84
6	428.03	140.14	0.44	2.25	0.44	2.26	0		0	.
6	429.03	84.32	0.44	2.26	0.44	2.26	0		0	.
6	430.03	451.68	0.44	2.29	0.44	2.29	1	1	0	2.26
6	431.03	353.86	0.45	2.22	0.44	2.29	0		0	.
6	432.03	132.13	0.44	2.25	0.44	2.25	1	3	0	2.11
6	433.03	129.16	0.45	2.23	0.45	2.23	1	1	0	2.11
6	434.03	80.98	0.46	2.18	0.45	2.23	0		1	.
6	435.03	147.34	0.47	2.11	0.47	2.11	1	1	0	2.29
6	436.03	123.82	0.43	2.31	0.44	2.26	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	437.03	0	1	0	0	1	430	0	2.14	2	175.01
6	438.03	1	1	1	1	1	440	0	0.86	2	175.01
6	439.03	1	0	1	0	1	440	0	1.07	1	175.01
6	440.03	0	.	1	0	.	440	0	0.43	2	185.21
6	441.03	0	1	1	0	2	440	0	1.07	1	185.21
6	442.03	1	.	1	0	2	442	0	1.29	1	185.21
6	443.03	0	1	1	0	1	442	0	1.29	2	185.21
6	444.03	1	1	0	0	1	442	0	1.29	1	1.60
6	445.03	0	1	1	0	1	442	0	1.07	2	185.21
6	446.03	1	1	1	0	1	442	0	1.07	1	175.01
6	447.03	0	0	0	0	2	442	0	1.29	2	175.01
6	448.03	0	1	1	0	2	442	0	1.29	1	164.81
6	449.03	0	0	0	0	1	442	0	1.71	2	164.81
6	450.03	1	1	1	0	1	442	0	1.71	1	185.21
6	451.03	0	1	1	0	2	442	0	1.71	2	185.21
6	452.03	1	1	1	0	1	442	0	1.71	1	205.61
6	453.03	1	.	1	0	1	453	1	1.71	1	205.61
6	454.03	0	.	1	0	1	454	1	1.93	2	175.01
6	455.03	1	0	1	0	1	453	1	1.50	1	205.61
6	456.03	0	1	1	0	1	353	1	1.93	1	164.81
6	457.03	0	0	1	0	1	454	1	1.93	2	175.01
6	458.03	1	.	1	0	1	458	0	2.14	1	175.01
6	459.03	1	.	1	0	1	459	0	2.36	2	205.61
6	460.03	1	.	0	0	1	460	0	2.36	1	205.61
6	461.03	0	1	1	0	2	460	0	2.36	1	185.21
6	462.03	0	1	1	0	1	463	0	1.93	1	185.21
6	463.03	1	.	1	1	1	463	0	1.93	2	185.21
6	464.03	1	0	0	0	1	463	0	2.36	1	185.21
6	465.03	0	0	0	1	1	463	0	1.50	2	205.61
6	466.03	0	0	1	0	2	463	0	1.71	1	134.21
6	467.03	0	1	0	0	1	463	0	1.71	1	103.60
6	468.03	1	1	1	0	2	463	0	1.71	2	103.60
6	469.03	1	1	1	0	2	463	0	1.50	2	215.81
6	470.03	1	0	1	0	1	463	0	0.86	2	215.81
6	471.03	1	0	1	0	1	463	0	1.29	1	175.01
6	472.03	0	1	0	0	1	463	0	1.29	1	175.01
6	473.03	1	0	1	0	1	463	0	1.71	1	134.21
6	474.03	1	0	1	0	1	463	0	0.86	2	215.81
6	475.03	0	0	1	0	1	463	0	1.29	0	42.40
6	476.03	1	0	1	0	1	463	0	2.14	1	185.21
6	477.03	1	1	1	0	1	463	0	1.50	2	215.81
6	478.03	1	0	1	0	1	463	0	1.50	2	185.21
6	479.03	0	.	0	0	1	479	1	2.36	1	134.21
6	480.03	0	0	1	0	1	479	1	2.14	1	83.20
6	481.03	1	0	1	0	2	463	0	1.07	2	185.21
6	482.03	1	1	1	0	1	479	1	1.93	1	195.41
6	483.03	1	0	1	0	1	463	0	1.50	2	215.81
6	484.03	1	0	1	0	1	463	0	1.29	1	215.81
6	485.03	1	0	1	0	1	463	0	2.14	2	215.81
6	486.03	1	0	1	0	1	463	0	1.29	0	215.81

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	437.03	142.87	0.43	2.34	0.44	2.29	0		1	.
6	438.03	126.46	0.36	2.78	0.36	2.75	0		1	.
6	439.03	121.62	0.37	2.67	0.36	2.75	0		0	.
6	440.03	66.27	0.36	2.75	0.36	2.75	1	0	0	2.23
6	441.03	90.66	0.37	2.69	0.36	2.75	0		0	.
6	442.03	95.70	0.37	2.70	0.37	2.70	1	0	0	2.75
6	443.03	88.36	0.38	2.63	0.37	2.70	0		1	.
6	444.03	590.09	0.36	2.75	0.37	2.70	0		0	.
6	445.03	93.33	0.37	2.70	0.37	2.70	0		0	.
6	446.03	127.99	0.38	2.65	0.37	2.70	0		0	.
6	447.03	129.19	0.37	2.67	0.37	2.70	0		0	.
6	448.03	152.22	0.38	2.64	0.37	2.70	0		0	.
6	449.03	150.51	0.38	2.64	0.37	2.70	0		0	.
6	450.03	97.70	0.38	2.60	0.37	2.70	0		0	.
6	451.03	100.27	0.39	2.55	0.37	2.70	0		0	.
6	452.03	69.03	0.40	2.50	0.37	2.70	0		0	.
6	453.03	70.27	0.40	2.47	0.40	2.47	1	2	0	2.70
6	454.03	157.32	0.39	2.59	0.39	2.59	1	3	0	2.70
6	455.03	75.20	0.39	2.53	0.40	2.47	0		1	.
6	456.03	163.96	0.39	2.55	0.40	2.47	0		0	.
6	457.03	183.31	0.38	2.65	0.39	2.59	0		1	.
6	458.03	163.19	0.39	2.55	0.39	2.55	1	2	0	2.70
6	459.03	72.17	0.38	2.63	0.38	2.63	1	3	0	2.70
6	460.03	73.70	0.38	2.60	0.38	2.60	1	1	0	2.70
6	461.03	93.83	0.38	2.60	0.38	2.60	0		1	.
6	462.03	104.24	0.40	2.52	0.40	2.50	0		0	.
6	463.03	102.20	0.40	2.50	0.40	2.50	1	1	0	2.60
6	464.03	102.20	0.41	2.46	0.40	2.50	0		1	.
6	465.03	77.54	0.40	2.51	0.40	2.50	0		0	.
6	466.03	294.86	0.40	2.52	0.40	2.50	0		0	.
6	467.03	427.73	0.39	2.59	0.40	2.50	0		0	.
6	468.03	424.43	0.40	2.53	0.40	2.50	0		0	.
6	469.03	93.42	0.39	2.54	0.40	2.50	0		0	.
6	470.03	95.02	0.39	2.56	0.40	2.50	0		0	.
6	471.03	184.62	0.40	2.50	0.40	2.50	0		0	.
6	472.03	183.35	0.39	2.54	0.40	2.50	0		0	.
6	473.03	326.92	0.37	2.68	0.40	2.50	0		0	.
6	474.03	97.26	0.39	2.57	0.40	2.50	0		0	.
6	475.03	529.16	0.40	2.52	0.40	2.50	0		0	.
6	476.03	145.65	0.37	2.68	0.40	2.50	0		0	.
6	477.03	100.33	0.38	2.63	0.40	2.50	0		0	.
6	478.03	137.17	0.39	2.58	0.40	2.50	0		0	.
6	479.03	336.53	0.36	2.77	0.36	2.77	1	3	0	2.50
6	480.03	460.03	0.37	2.69	0.36	2.77	0		1	.
6	481.03	134.24	0.39	2.54	0.40	2.50	0		0	.
6	482.03	154.89	0.36	2.75	0.36	2.77	0		0	.
6	483.03	109.27	0.38	2.66	0.40	2.50	0		0	.
6	484.03	106.97	0.39	2.59	0.40	2.50	0		0	.
6	485.03	108.17	0.36	2.74	0.40	2.50	0		0	.
6	486.03	101.80	0.37	2.74	0.40	2.50	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	487.03	1	.	1	0	1	487	1	1.93	2	215.81
6	488.03	1	0	1	0	1	487	1	1.71	2	215.81
6	489.03	0	1	1	0	1	487	1	1.50	2	215.81
6	490.03	1	1	1	0	1	491	0	1.07	1	185.21
6	491.03	0	.	1	0	2	491	0	1.29	2	185.21
6	492.03	1	0	1	0	1	491	0	1.50	1	185.21
6	493.03	1	1	1	0	1	491	0	1.93	1	185.21
6	494.03	0	1	0	0	1	491	0	1.93	2	185.21
6	495.03	1	0	1	0	1	491	0	1.71	1	185.21
6	496.03	1	1	1	0	1	491	0	1.71	1	185.21
6	497.03	0	1	1	0	1	491	0	1.93	2	185.21
6	498.03	0	.	1	0	.	498	0	0.64	2	185.21
6	499.03	1	0	1	1	1	491	0	1.71	2	175.01
6	500.03	1	0	1	0	1	491	0	2.14	1	175.01
6	501.03	0	1	1	0	1	491	0	1.93	2	154.61
6	502.03	1	0	1	0	1	491	0	1.71	2	215.81
6	503.03	1	1	1	0	1	491	0	2.14	1	185.21
6	504.03	1	0	1	0	1	491	0	1.71	1	195.41
6	505.03	1	1	1	0	1	507	0	1.07	2	175.01
6	506.03	1	0	1	0	2	491	0	1.71	1	195.41
6	507.03	0	.	0	0	2	507	0	1.71	1	195.41
6	508.03	0	1	0	0	1	507	0	0.64	1	175.01
6	509.03	1	.	1	0	2	509	0	1.29	1	103.60
6	510.03	1	0	1	0	1	509	0	1.07	1	103.60
6	511.03	0	0	1	0	2	507	0	1.07	2	164.81
6	512.03	1	.	0	0	.	512	0	0.43	2	103.60
6	94.04	1	.	1	0	1	94	0	0.43	1	11.80
6	95.04	1	.	1	0	1	95	0	0.86	2	11.80
6	96.04	0	.	1	0	2	96	0	1.29	1	11.80
6	97.04	1	.	0	0	1	97	0	0.86	1	1.60
6	106.04	1	.	1	0	.	106	0	0.43	2	1.60
6	108.04	1	.	1	0	1	108	1	1.50	2	11.80
6	109.04	1	0	1	0	1	108	1	1.71	2	11.80
6	110.04	1	.	1	0	1	110	0	1.07	2	11.80
6	111.04	1	0	1	0	1	110	0	1.07	2	11.80
6	113.04	1	.	0	0	1	113	0	0.86	2	11.80
6	114.04	0	.	0	0	1	114	1	1.07	1	11.80
6	116.04	0	.	0	0	1	116	0	0.86	1	11.80
6	118.04	0	.	0	0	1	118	1	1.50	1	1.60
6	120.04	1	.	1	0	2	120	0	0.64	2	22.00
6	123.04	0	0	0	0	1	128	0	0.86	2	11.80
6	125.04	1	.	1	0	1	125	1	0.86	2	22.00
6	128.04	0	.	1	0	2	128	0	0.86	1	1.60
6	129.04	1	.	1	0	2	129	0	0.86	2	22.00
6	130.04	0	.	0	0	1	130	1	0.86	0	1.60
6	131.04	1	1	0	0	1	130	1	1.07	1	22.00
6	140.04	0	.	0	0	1	140	1	1.07	0	22.00
6	141.04	0	0	0	0	1	140	1	0.86	2	22.00
6	143.04	1	1	1	0	1	140	1	1.07	1	62.80
6	144.04	1	0	1	0	1	140	1	1.50	2	62.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	487.03	111.47	0.38	2.63	0.38	2.63	1	2	0	2.50
6	488.03	114.24	0.37	2.69	0.38	2.63	0		1	.
6	489.03	115.18	0.38	2.66	0.38	2.63	0		0	.
6	490.03	141.31	0.35	2.83	0.35	2.84	0		1	.
6	491.03	151.72	0.35	2.84	0.35	2.84	1	0	0	2.50
6	492.03	149.82	0.35	2.84	0.35	2.84	0		0	.
6	493.03	171.01	0.35	2.86	0.35	2.84	0		0	.
6	494.03	169.54	0.35	2.85	0.35	2.84	0		0	.
6	495.03	175.61	0.35	2.88	0.35	2.84	0		0	.
6	496.03	178.61	0.35	2.85	0.35	2.84	0		0	.
6	497.03	180.88	0.35	2.89	0.35	2.84	0		0	.
6	498.03	82.68	0.41	2.44	0.41	2.44	1	0	0	2.66
6	499.03	244.17	0.35	2.86	0.35	2.84	0		0	.
6	500.03	252.18	0.35	2.86	0.35	2.84	0		0	.
6	501.03	409.05	0.35	2.83	0.35	2.84	0		0	.
6	502.03	203.53	0.35	2.85	0.35	2.84	0		0	.
6	503.03	233.50	0.36	2.82	0.35	2.84	0		0	.
6	504.03	351.62	0.35	2.85	0.35	2.84	0		0	.
6	505.03	377.94	0.37	2.69	0.37	2.74	0		0	.
6	506.03	350.59	0.36	2.81	0.35	2.84	0		0	.
6	507.03	354.03	0.37	2.74	0.37	2.74	1	1	0	2.84
6	508.03	377.57	0.37	2.71	0.37	2.74	0		0	.
6	509.03	560.73	0.38	2.66	0.38	2.66	1	1	0	2.74
6	510.03	563.10	0.38	2.62	0.38	2.66	0		1	.
6	511.03	250.01	0.36	2.74	0.37	2.74	0		1	.
6	512.03	748.35	0.48	2.07	0.48	2.07	1	0	0	2.44
6	94.04	68.57	0.70	1.44	0.70	1.44	1	2	0	2.00
6	95.04	69.14	0.67	1.48	0.67	1.48	1	3	0	2.00
6	96.04	69.94	0.68	1.47	0.68	1.47	1	1	0	2.00
6	97.04	71.31	0.67	1.50	0.67	1.50	1	0	0	1.47
6	106.04	46.88	0.50	2.00	0.50	2.00	1	0	0	.
6	108.04	74.18	0.62	1.61	0.62	1.61	1	2	0	1.50
6	109.04	75.64	0.62	1.62	0.62	1.61	0		1	.
6	110.04	78.18	0.61	1.64	0.61	1.64	1	1	0	1.75
6	111.04	79.62	0.62	1.60	0.61	1.64	0		1	.
6	113.04	83.89	0.66	1.52	0.66	1.52	1	2	0	1.64
6	114.04	72.54	0.59	1.68	0.59	1.68	1	3	0	1.50
6	116.04	81.25	0.60	1.66	0.60	1.66	1	3	0	1.64
6	118.04	74.18	0.57	1.75	0.57	1.75	1	4	0	1.50
6	120.04	68.30	0.80	1.24	0.80	1.24	1	1	0	1.64
6	123.04	95.03	0.79	1.27	0.81	1.23	0		1	.
6	125.04	71.27	0.78	1.27	0.78	1.27	1	2	0	1.27
6	128.04	94.56	0.81	1.23	0.81	1.23	1	1	0	1.24
6	129.04	69.80	0.78	1.27	0.78	1.27	1	0	0	1.23
6	130.04	96.17	0.70	1.42	0.70	1.42	1	3	0	1.27
6	131.04	72.74	0.72	1.39	0.70	1.42	0		1	.
6	140.04	73.77	0.64	1.55	0.64	1.55	1	4	0	1.27
6	141.04	75.01	0.66	1.51	0.64	1.55	0		1	.
6	143.04	37.39	0.64	1.56	0.64	1.55	0		0	.
6	144.04	38.28	0.62	1.61	0.64	1.55	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	145.04	0	1	1	0	1	140	1	1.50	0	62.80
6	146.04	1	.	1	0	1	146	1	1.07	2	22.00
6	148.04	1	0	1	0	1	146	1	1.07	2	52.60
6	151.04	1	.	1	0	1	151	1	1.29	1	1.60
6	153.04	1	0	1	0	1	146	1	0.86	2	32.20
6	160.04	0	.	1	0	2	160	1	0.43	0	11.80
6	165.04	1	.	1	0	2	165	0	0.64	0	11.80
6	166.04	0	1	0	0	2	165	0	0.86	0	11.80
6	169.04	1	.	1	0	1	169	0	0.64	0	32.20
6	171.04	1	.	1	0	2	171	0	0.43	2	62.80
6	173.04	0	.	0	0	2	173	0	0.86	0	52.60
6	174.04	1	.	1	0	1	174	1	0.86	2	62.80
6	175.04	1	0	1	0	1	174	1	1.50	2	62.80
6	176.04	1	0	1	0	1	174	1	1.50	2	62.80
6	177.04	1	.	0	0	1	177	0	1.50	0	62.80
6	178.04	0	.	0	0	2	178	0	0.86	2	83.20
6	179.04	1	.	1	0	1	179	1	0.86	1	62.80
6	180.04	0	.	1	0	1	180	1	1.07	1	62.80
6	181.04	0	.	1	0	2	181	1	1.07	2	32.20
6	182.04	1	.	1	0	2	182	0	0.86	2	32.20
6	183.04	1	.	1	0	1	183	1	0.64	1	11.80
6	184.04	1	.	1	0	1	184	1	1.29	2	22.00
6	185.04	1	.	0	0	2	185	1	1.07	1	22.00
6	186.04	1	.	1	0	1	186	0	0.86	2	62.80
6	187.04	1	0	1	0	1	186	0	0.64	2	83.20
6	188.04	1	0	1	1	1	186	0	0.86	2	32.20
6	189.04	1	0	1	0	2	186	0	0.86	2	62.80
6	190.04	1	.	1	0	2	190	0	0.64	2	32.20
6	191.04	1	.	0	1	1	191	1	0.86	2	32.20
6	192.04	1	0	1	0	1	191	1	0.86	2	32.20
6	193.04	1	.	1	0	1	193	1	0.86	1	1.60
6	194.04	1	.	1	0	1	194	0	1.29	1	22.00
6	195.04	1	0	1	0	1	193	1	0.86	1	1.60
6	196.04	1	0	1	0	1	194	0	1.29	2	52.60
6	197.04	1	0	1	0	1	194	0	1.07	1	52.60
6	198.04	1	0	1	0	1	194	0	1.50	1	32.20
6	199.04	1	0	1	0	1	194	0	1.71	2	52.60
6	200.04	1	0	1	0	2	194	0	1.29	2	52.60
6	201.04	1	0	1	0	1	194	0	1.07	1	32.20
6	202.04	1	.	0	0	1	202	1	1.50	1	32.20
6	203.04	1	.	1	0	1	203	1	1.29	2	32.20
6	204.04	1	0	1	0	1	202	1	1.71	1	1.60
6	211.04	1	0	0	0	1	202	1	1.93	0	62.80
6	212.04	0	1	1	0	1	203	1	1.93	2	62.80
6	213.04	0	0	0	0	1	203	1	1.71	2	62.80
6	214.04	0	0	0	0	1	203	1	2.14	2	62.80
6	215.04	1	0	1	0	1	202	1	1.93	1	1.60
6	216.04	1	0	1	0	1	202	1	1.50	1	1.60
6	219.04	0	0	0	0	1	223	0	1.07	2	42.40
6	220.04	0	0	0	0	1	223	0	1.29	2	42.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	145.04	40.68	0.63	1.59	0.64	1.55	0		0	.
6	146.04	82.58	0.63	1.60	0.63	1.60	1	1	0	1.55
6	148.04	63.19	0.62	1.61	0.63	1.60	0		1	.
6	151.04	115.58	0.70	1.43	0.70	1.43	1	2	0	1.60
6	153.04	87.79	0.63	1.60	0.63	1.60	0		0	.
6	160.04	118.82	0.67	1.50	0.67	1.50	1	0	0	1.60
6	165.04	120.79	0.66	1.52	0.66	1.52	1	4	0	1.50
6	166.04	121.96	0.64	1.56	0.66	1.52	0		1	.
6	169.04	90.99	0.53	1.87	0.53	1.87	1	0	0	1.52
6	171.04	48.95	0.61	1.63	0.61	1.63	1	0	0	1.87
6	173.04	79.27	0.59	1.70	0.59	1.70	1	1	0	1.63
6	174.04	55.19	0.61	1.65	0.61	1.65	1	2	0	1.70
6	175.04	61.63	0.60	1.66	0.61	1.65	0		1	.
6	176.04	62.50	0.60	1.67	0.61	1.65	0		0	.
6	177.04	63.67	0.58	1.72	0.58	1.72	1	1	0	1.70
6	178.04	64.80	0.62	1.62	0.62	1.62	1	1	0	1.71
6	179.04	47.82	0.46	2.16	0.46	2.16	1	3	0	1.70
6	180.04	53.52	0.53	1.89	0.53	1.89	1	3	0	1.70
6	181.04	117.98	0.62	1.62	0.62	1.62	1	2	0	1.62
6	182.04	114.75	0.59	1.71	0.59	1.71	1	1	0	1.72
6	183.04	146.22	0.57	1.76	0.57	1.76	1	3	0	1.62
6	184.04	124.19	0.59	1.68	0.59	1.68	1	3	0	1.62
6	185.04	123.16	0.60	1.67	0.60	1.67	1	2	0	1.62
6	186.04	65.57	0.61	1.65	0.61	1.65	1	1	0	1.62
6	187.04	68.81	0.61	1.64	0.61	1.65	0		1	.
6	188.04	128.49	0.60	1.67	0.61	1.65	0		0	.
6	189.04	68.97	0.60	1.67	0.61	1.65	0		0	.
6	190.04	133.23	0.61	1.63	0.61	1.63	1	1	0	1.65
6	191.04	132.63	0.61	1.65	0.61	1.65	1	2	0	1.63
6	192.04	134.77	0.58	1.73	0.61	1.65	0		1	.
6	193.04	164.47	0.57	1.74	0.57	1.74	1	3	0	1.63
6	194.04	134.07	0.56	1.80	0.56	1.80	1	1	0	1.63
6	195.04	165.37	0.54	1.87	0.57	1.74	0		1	.
6	196.04	100.73	0.54	1.85	0.56	1.80	0		1	.
6	197.04	99.96	0.54	1.84	0.56	1.80	0		0	.
6	198.04	137.50	0.56	1.79	0.56	1.80	0		0	.
6	199.04	103.36	0.53	1.87	0.56	1.80	0		0	.
6	200.04	104.20	0.53	1.89	0.56	1.80	0		0	.
6	201.04	139.61	0.54	1.84	0.56	1.80	0		0	.
6	202.04	140.54	0.53	1.88	0.53	1.88	1	3	0	1.80
6	203.04	143.08	0.54	1.85	0.54	1.85	1	2	0	1.80
6	204.04	179.11	0.54	1.87	0.53	1.88	0		1	.
6	211.04	70.78	0.52	1.93	0.53	1.88	0		0	.
6	212.04	72.98	0.54	1.87	0.54	1.85	0		1	.
6	213.04	75.91	0.53	1.87	0.54	1.85	0		0	.
6	214.04	77.65	0.54	1.86	0.54	1.85	0		0	.
6	215.04	181.28	0.51	1.96	0.53	1.88	0		0	.
6	216.04	180.12	0.52	1.93	0.53	1.88	0		0	.
6	219.04	112.74	0.53	1.89	0.52	1.94	0		0	.
6	220.04	109.04	0.53	1.90	0.52	1.94	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	222.04	0	0	1	0	2	223	0	0.86	2	42.40
6	223.04	0	.	0	0	1	223	0	2.14	1	62.80
6	224.04	1	1	1	0	1	223	0	1.07	2	32.20
6	225.04	1	0	1	0	1	223	0	0.86	1	11.80
6	228.04	1	0	1	0	1	223	0	1.29	2	11.80
6	229.04	1	0	1	0	1	223	0	1.50	1	11.80
6	230.04	0	1	0	0	1	223	0	1.50	1	11.80
6	231.04	0	0	0	0	1	223	0	1.50	1	62.80
6	232.04	0	0	0	1	1	223	0	1.29	2	62.80
6	233.04	1	1	1	0	2	223	0	0.86	2	62.80
6	234.04	0	.	0	0	1	234	1	1.29	2	62.80
6	235.04	1	.	1	0	1	235	1	1.29	1	32.20
6	236.04	0	1	0	0	1	235	1	1.50	1	32.20
6	237.04	0	0	1	0	1	234	1	1.71	2	62.80
6	238.04	1	.	1	0	1	238	0	1.71	1	62.80
6	239.04	0	0	1	0	1	238	0	1.50	2	62.80
6	240.04	1	0	1	0	2	238	0	1.50	1	42.40
6	241.04	0	0	0	0	1	238	0	1.93	0	62.80
6	242.04	0	0	0	0	1	238	0	1.50	1	62.80
6	243.04	0	0	1	0	1	238	0	1.29	1	83.20
6	244.04	1	1	1	0	1	238	0	1.93	2	62.80
6	245.04	0	0	0	0	1	238	0	1.93	1	62.80
6	246.04	0	0	0	0	1	238	0	1.93	1	83.20
6	247.04	0	1	0	0	1	238	0	1.29	2	62.80
6	248.04	0	0	0	0	1	238	0	1.93	1	83.20
6	249.04	1	1	1	0	1	238	0	1.93	1	83.20
6	250.04	0	1	1	0	1	238	0	1.93	2	62.80
6	251.04	0	0	0	0	1	238	0	2.14	2	62.80
6	252.04	0	.	0	0	1	252	1	1.93	1	83.20
6	253.04	1	1	1	0	1	252	1	2.14	1	83.20
6	254.04	1	.	1	0	1	254	1	2.36	2	83.20
6	255.04	0	0	0	0	1	254	1	1.93	2	83.20
6	256.04	0	0	0	0	1	254	1	1.71	2	62.80
6	257.04	0	1	0	0	1	254	1	2.14	2	83.20
6	258.04	1	0	1	0	1	252	1	2.36	1	62.80
6	259.04	1	.	1	0	1	259	0	1.93	1	62.80
6	260.04	1	0	1	0	1	252	1	1.93	1	62.80
6	261.04	0	1	1	0	1	259	0	1.93	1	83.20
6	262.04	1	0	1	0	1	259	0	2.14	2	32.20
6	263.04	0	0	1	0	2	259	0	2.14	1	62.80
6	264.04	1	1	0	0	1	259	0	1.71	2	83.20
6	265.04	1	0	1	0	1	259	0	1.50	1	83.20
6	266.04	1	0	1	0	1	259	0	1.93	2	83.20
6	267.04	0	1	1	0	1	259	0	1.71	1	62.80
6	268.04	1	1	1	0	1	259	0	1.93	2	62.80
6	269.04	1	0	0	0	1	259	0	1.71	1	32.20
6	270.04	1	0	1	0	1	259	0	2.36	2	83.20
6	271.04	0	1	0	0	1	259	0	2.14	1	32.20
6	272.04	1	1	1	0	2	259	0	2.14	1	83.20
6	273.04	1	0	0	0	1	259	0	2.36	2	62.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	222.04	113.94	0.53	1.88	0.52	1.94	0		0	.
6	223.04	73.51	0.52	1.94	0.52	1.94	1	1	0	1.80
6	224.04	153.12	0.53	1.89	0.52	1.94	0		0	.
6	225.04	192.53	0.50	1.99	0.52	1.94	0		0	.
6	228.04	195.90	0.51	1.95	0.52	1.94	0		0	.
6	229.04	193.86	0.50	2.00	0.52	1.94	0		0	.
6	230.04	196.67	0.50	2.00	0.52	1.94	0		0	.
6	231.04	78.85	0.49	2.03	0.52	1.94	0		0	.
6	232.04	80.75	0.49	2.03	0.52	1.94	0		0	.
6	233.04	82.49	0.50	2.02	0.52	1.94	0		0	.
6	234.04	83.22	0.50	1.99	0.50	1.99	1	2	0	1.94
6	235.04	158.29	0.48	2.07	0.48	2.07	1	3	0	1.94
6	236.04	161.39	0.49	2.05	0.48	2.07	0		1	.
6	237.04	86.89	0.50	2.00	0.50	1.99	0		1	.
6	238.04	84.59	0.49	2.04	0.49	2.04	1	1	0	1.94
6	239.04	93.30	0.47	2.11	0.49	2.04	0		0	.
6	240.04	123.92	0.48	2.10	0.49	2.04	0		1	.
6	241.04	98.40	0.48	2.10	0.49	2.04	0		0	.
6	242.04	97.27	0.48	2.07	0.49	2.04	0		0	.
6	243.04	90.43	0.48	2.08	0.49	2.04	0		0	.
6	244.04	95.10	0.49	2.06	0.49	2.04	0		0	.
6	245.04	101.74	0.48	2.07	0.49	2.04	0		0	.
6	246.04	98.40	0.49	2.05	0.49	2.04	0		0	.
6	247.04	91.80	0.48	2.07	0.49	2.04	0		0	.
6	248.04	105.08	0.49	2.02	0.49	2.04	0		0	.
6	249.04	106.34	0.49	2.05	0.49	2.04	0		0	.
6	250.04	105.98	0.49	2.05	0.49	2.04	0		0	.
6	251.04	108.28	0.49	2.03	0.49	2.04	0		0	.
6	252.04	112.38	0.49	2.05	0.49	2.05	1	3	0	2.04
6	253.04	113.78	0.49	2.05	0.49	2.05	0		1	.
6	254.04	116.25	0.50	1.99	0.50	1.99	1	2	0	2.04
6	255.04	121.79	0.50	2.02	0.50	1.99	0		0	.
6	256.04	120.69	0.50	2.02	0.50	1.99	0		0	.
6	257.04	119.86	0.49	2.03	0.50	1.99	0		1	.
6	258.04	111.08	0.49	2.05	0.49	2.05	0		0	.
6	259.04	112.95	0.49	2.05	0.49	2.05	1	1	0	2.04
6	260.04	99.74	0.49	2.04	0.49	2.05	0		0	.
6	261.04	118.46	0.48	2.06	0.49	2.05	0		0	.
6	262.04	191.22	0.49	2.04	0.49	2.05	0		1	.
6	263.04	119.29	0.48	2.07	0.49	2.05	0		0	.
6	264.04	125.33	0.49	2.06	0.49	2.05	0		0	.
6	265.04	123.63	0.47	2.15	0.49	2.05	0		0	.
6	266.04	126.73	0.48	2.09	0.49	2.05	0		0	.
6	267.04	128.87	0.47	2.11	0.49	2.05	0		0	.
6	268.04	127.70	0.47	2.12	0.49	2.05	0		0	.
6	269.04	198.40	0.48	2.10	0.49	2.05	0		0	.
6	270.04	132.70	0.47	2.14	0.49	2.05	0		0	.
6	271.04	199.93	0.47	2.15	0.49	2.05	0		0	.
6	272.04	131.37	0.47	2.15	0.49	2.05	0		0	.
6	273.04	130.67	0.47	2.13	0.49	2.05	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	274.04	0	1	1	0	1	259	0	2.14	1	62.80
6	275.04	1	1	1	0	1	259	0	2.14	2	83.20
6	276.04	1	0	1	0	1	259	0	1.93	1	83.20
6	277.04	1	0	1	0	1	259	0	1.93	2	134.21
6	278.04	1	0	1	0	1	259	0	1.93	1	52.60
6	279.04	1	0	1	0	1	259	0	1.93	2	83.20
6	280.04	0	1	0	0	1	259	0	1.71	1	52.60
6	281.04	1	1	1	0	1	259	0	1.50	2	83.20
6	282.04	1	1	1	0	1	259	0	1.93	2	83.20
6	283.04	0	1	1	0	1	259	0	1.93	1	62.80
6	284.04	1	0	1	0	1	259	0	2.14	1	164.81
6	285.04	1	0	1	1	1	259	0	1.50	2	113.80
6	287.04	1	0	0	0	1	259	0	1.29	1	113.80
6	288.04	1	0	1	0	1	259	0	1.29	2	113.80
6	289.04	1	0	1	0	1	295	0	0.86	1	103.60
6	290.04	0	0	0	0	1	295	0	1.07	1	32.20
6	291.04	1	.	1	0	1	291	1	1.50	1	1.60
6	292.04	1	.	1	0	1	292	1	1.50	2	103.60
6	293.04	1	0	1	0	1	291	1	1.71	1	62.80
6	294.04	1	1	1	0	2	295	0	0.43	2	103.60
6	295.04	0	.	1	0	.	295	0	0.43	2	62.80
6	296.04	0	1	1	0	1	292	1	2.14	2	134.21
6	297.04	0	1	0	0	1	295	0	1.29	2	103.60
6	298.04	1	.	1	0	1	298	1	1.50	2	124.01
6	299.04	1	.	1	0	2	299	0	0.86	2	1.60
6	300.04	1	0	1	0	1	298	1	1.07	2	103.60
6	301.04	1	0	0	0	1	298	1	1.50	2	83.20
6	302.04	1	0	1	0	1	298	1	1.50	2	83.20
6	303.04	1	1	0	0	1	307	1	1.50	2	103.60
6	304.04	1	0	1	0	1	298	1	1.29	2	83.20
6	305.04	1	.	0	0	1	305	1	1.29	1	103.60
6	306.04	0	1	0	0	1	298	1	1.29	2	83.20
6	307.04	0	.	0	0	1	307	1	1.50	2	103.60
6	308.04	1	0	0	0	1	305	1	1.71	1	103.60
6	309.04	0	1	1	0	1	310	0	1.07	0	83.20
6	310.04	1	.	1	0	1	310	0	0.86	1	83.20
6	311.04	1	.	1	0	1	311	1	1.50	1	1.60
6	312.04	1	1	1	0	1	311	1	1.93	1	42.40
6	313.04	1	0	1	0	1	311	1	1.29	1	62.80
6	314.04	0	1	0	0	1	311	1	2.14	1	62.80
6	315.04	1	.	1	0	1	315	0	0.64	2	103.60
6	316.04	0	.	1	0	2	316	0	0.64	2	164.81
6	317.04	1	1	1	0	2	316	0	0.86	2	83.20
6	318.04	1	.	1	0	2	318	1	0.64	1	62.80
6	319.04	1	.	1	0	1	319	1	0.86	2	62.80
6	320.04	1	0	1	0	1	318	1	1.07	1	62.80
6	321.04	1	0	0	0	2	318	1	0.86	0	83.20
6	322.04	1	0	1	0	2	319	1	1.07	2	83.20
6	323.04	1	.	1	0	1	323	0	0.86	2	134.21
6	324.04	1	.	1	0	1	324	0	1.29	1	83.20

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	274.04	133.34	0.47	2.13	0.49	2.05	0		0	.
6	275.04	135.61	0.47	2.12	0.49	2.05	0		0	.
6	276.04	137.27	0.46	2.16	0.49	2.05	0		0	.
6	277.04	55.73	0.47	2.13	0.49	2.05	0		0	.
6	278.04	177.64	0.47	2.14	0.49	2.05	0		0	.
6	279.04	140.41	0.47	2.14	0.49	2.05	0		0	.
6	280.04	180.74	0.46	2.16	0.49	2.05	0		0	.
6	281.04	139.28	0.47	2.14	0.49	2.05	0		0	.
6	282.04	142.01	0.47	2.14	0.49	2.05	0		0	.
6	283.04	134.87	0.47	2.13	0.49	2.05	0		0	.
6	284.04	44.25	0.47	2.13	0.49	2.05	0		0	.
6	285.04	86.55	0.47	2.11	0.49	2.05	0		0	.
6	287.04	91.15	0.49	2.04	0.49	2.05	0		0	.
6	288.04	88.85	0.49	2.05	0.49	2.05	0		0	.
6	289.04	86.12	0.51	1.96	0.50	2.01	0		0	.
6	290.04	240.57	0.51	1.96	0.50	2.01	0		0	.
6	291.04	280.18	0.51	1.96	0.51	1.96	1	2	0	2.01
6	292.04	89.26	0.50	2.01	0.50	2.01	1	3	0	2.01
6	293.04	167.57	0.54	1.85	0.51	1.96	0		1	.
6	294.04	83.71	0.49	2.03	0.50	2.01	0		1	.
6	295.04	139.78	0.50	2.01	0.50	2.01	1	0	0	2.03
6	296.04	61.50	0.50	2.00	0.50	2.01	0		1	.
6	297.04	87.35	0.49	2.02	0.50	2.01	0		0	.
6	298.04	75.88	0.49	2.02	0.49	2.02	1	2	0	2.01
6	299.04	262.20	0.49	2.03	0.49	2.03	1	1	0	2.05
6	300.04	98.69	0.50	2.00	0.49	2.02	0		1	.
6	301.04	165.57	0.50	2.01	0.49	2.02	0		0	.
6	302.04	167.10	0.49	2.05	0.49	2.02	0		0	.
6	303.04	103.47	0.43	2.34	0.45	2.23	0		1	.
6	304.04	169.11	0.49	2.06	0.49	2.02	0		0	.
6	305.04	102.37	0.49	2.04	0.49	2.04	1	2	0	2.01
6	306.04	172.08	0.46	2.16	0.49	2.02	0		0	.
6	307.04	104.40	0.45	2.23	0.45	2.23	1	3	0	2.01
6	308.04	100.73	0.47	2.15	0.49	2.04	0		1	.
6	309.04	192.20	0.48	2.10	0.47	2.11	0		1	.
6	310.04	188.96	0.47	2.11	0.47	2.11	1	1	0	2.22
6	311.04	282.08	0.41	2.43	0.41	2.43	1	3	0	2.01
6	312.04	218.21	0.42	2.38	0.41	2.43	0		0	.
6	313.04	170.21	0.42	2.38	0.41	2.43	0		1	.
6	314.04	171.68	0.42	2.37	0.41	2.43	0		0	.
6	315.04	106.37	0.44	2.29	0.44	2.29	1	1	0	2.01
6	316.04	45.88	0.45	2.22	0.45	2.22	1	1	0	2.29
6	317.04	186.22	0.45	2.24	0.45	2.22	0		1	.
6	318.04	183.42	0.51	1.96	0.51	1.96	1	0	0	2.11
6	319.04	185.36	0.48	2.07	0.48	2.07	1	3	0	1.96
6	320.04	185.39	0.51	1.96	0.51	1.96	0		1	.
6	321.04	190.26	0.52	1.93	0.51	1.96	0		0	.
6	322.04	185.62	0.50	2.00	0.48	2.07	0		1	.
6	323.04	87.06	0.49	2.04	0.49	2.04	1	1	0	1.96
6	324.04	190.72	0.49	2.06	0.49	2.06	1	3	0	1.96

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	325.04	0	.	0	0	1	325	0	1.07	2	103.60
6	326.04	0	0	0	0	1	325	0	0.86	1	83.20
6	327.04	1	1	1	0	1	325	0	1.07	2	103.60
6	328.04	0	0	1	0	2	325	0	1.29	1	83.20
6	329.04	1	0	1	0	2	325	0	0.64	2	83.20
6	330.04	1	.	1	0	1	330	0	0.64	1	62.80
6	331.04	0	.	0	0	1	331	0	1.07	2	62.80
6	332.04	0	1	0	0	1	330	0	1.29	1	83.20
6	333.04	1	0	0	0	1	330	0	1.71	1	103.60
6	334.04	1	1	1	0	1	330	0	1.29	2	103.60
6	335.04	1	.	1	0	1	335	1	1.50	0	83.20
6	336.04	1	.	1	0	1	336	1	1.71	2	83.20
6	337.04	1	0	1	0	1	336	1	1.71	2	83.20
6	338.04	1	.	1	0	1	338	1	1.50	1	52.60
6	339.04	1	0	1	0	1	336	1	1.93	2	83.20
6	340.04	1	0	1	0	1	338	1	1.93	1	83.20
6	341.04	0	.	1	0	1	341	1	1.50	0	164.81
6	342.04	0	1	1	0	1	338	1	2.14	1	83.20
6	343.04	1	.	0	0	1	343	0	1.50	1	83.20
6	344.04	0	0	0	0	1	343	0	1.29	1	113.80
6	345.04	0	1	1	0	2	343	0	1.50	0	113.80
6	346.04	1	.	1	0	1	346	0	1.71	2	103.60
6	347.04	1	.	1	0	1	347	0	1.29	1	83.20
6	348.04	1	.	1	0	1	348	0	1.93	1	164.81
6	349.04	0	1	0	0	1	348	0	1.93	0	164.81
6	350.04	0	.	0	0	2	350	0	1.29	2	113.80
6	351.04	0	1	1	0	1	341	1	1.71	2	83.20
6	352.04	0	.	1	1	1	352	1	1.71	2	103.60
6	353.04	1	1	1	0	2	341	1	2.14	2	83.20
6	354.04	1	.	1	0	1	354	0	1.29	0	164.81
6	355.04	1	1	1	0	1	341	1	1.71	0	83.20
6	356.04	1	0	1	0	1	341	1	1.50	2	83.20
6	357.04	1	1	0	0	1	352	1	1.71	1	83.20
6	358.04	1	0	1	0	1	362	1	1.93	2	52.60
6	359.04	1	0	0	0	1	352	1	1.93	1	83.20
6	360.04	1	.	1	0	1	360	1	1.29	1	83.20
6	361.04	1	0	1	0	1	352	1	2.36	1	83.20
6	362.04	1	.	1	0	1	362	1	1.29	1	83.20
6	363.04	0	1	0	0	1	352	1	1.50	1	83.20
6	364.04	0	.	0	0	.	364	0	0.43	2	52.60
6	365.04	0	.	1	0	1	365	0	0.86	1	62.80
6	366.04	1	.	1	0	1	366	0	1.07	0	83.20
6	367.04	0	.	0	0	1	367	0	0.64	0	124.01
6	368.04	0	.	0	0	.	368	0	0.43	2	124.01
6	369.04	1	.	1	0	1	369	0	1.07	2	83.20
6	370.04	0	.	1	0	2	370	0	0.86	2	62.80
6	371.04	0	.	0	0	.	371	0	0.43	2	83.20
6	372.04	1	0	1	0	1	373	0	0.64	0	164.81
6	373.04	1	.	0	0	1	373	0	1.07	2	164.81
6	374.04	1	.	1	0	2	374	0	1.07	1	164.81

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	325.04	108.49	0.48	2.07	0.48	2.07	1	0	0	2.04
6	326.04	194.83	0.49	2.04	0.48	2.07	0		1	.
6	327.04	110.07	0.48	2.08	0.48	2.07	0		0	.
6	328.04	196.57	0.49	2.04	0.48	2.07	0		0	.
6	329.04	202.77	0.48	2.10	0.48	2.07	0		0	.
6	330.04	198.04	0.49	2.04	0.49	2.04	1	1	0	2.06
6	331.04	201.71	0.48	2.06	0.48	2.06	1	1	0	2.07
6	332.04	198.30	0.49	2.05	0.49	2.04	0		1	.
6	333.04	113.21	0.49	2.06	0.49	2.04	0		0	.
6	334.04	112.04	0.50	2.02	0.49	2.04	0		0	.
6	335.04	214.89	0.49	2.04	0.49	2.04	1	3	0	2.04
6	336.04	217.09	0.52	1.91	0.52	1.91	1	2	0	2.04
6	337.04	219.29	0.52	1.92	0.52	1.91	0		1	.
6	338.04	185.61	0.49	2.05	0.49	2.05	1	3	0	2.04
6	339.04	207.81	0.52	1.93	0.52	1.91	0		0	.
6	340.04	203.14	0.49	2.06	0.49	2.05	0		1	.
6	341.04	51.95	0.49	2.02	0.49	2.02	1	2	0	1.97
6	342.04	205.34	0.48	2.07	0.49	2.05	0		0	.
6	343.04	211.08	0.49	2.04	0.49	2.04	1	1	0	2.04
6	344.04	114.71	0.48	2.07	0.49	2.04	0		0	.
6	345.04	114.94	0.49	2.05	0.49	2.04	0		1	.
6	346.04	117.78	0.48	2.10	0.48	2.10	1	3	0	2.04
6	347.04	231.57	0.54	1.86	0.54	1.86	1	2	0	2.04
6	348.04	56.39	0.51	1.97	0.51	1.97	1	1	0	2.20
6	349.04	54.46	0.49	2.06	0.51	1.97	0		1	.
6	350.04	119.68	0.45	2.20	0.45	2.20	1	1	0	2.04
6	351.04	238.08	0.50	1.99	0.49	2.02	0		0	.
6	352.04	124.62	0.46	2.19	0.46	2.19	1	3	0	1.97
6	353.04	228.77	0.50	1.99	0.49	2.02	0		0	.
6	354.04	55.02	0.84	1.20	0.84	1.20	1	2	0	1.97
6	355.04	237.64	0.50	1.99	0.49	2.02	0		0	.
6	356.04	240.58	0.47	2.13	0.49	2.02	0		0	.
6	357.04	213.48	0.43	2.33	0.46	2.19	0		1	.
6	358.04	317.78	0.47	2.14	0.45	2.20	0		0	.
6	359.04	215.92	0.43	2.33	0.46	2.19	0		0	.
6	360.04	230.10	0.49	2.03	0.49	2.03	1	2	0	1.97
6	361.04	216.59	0.44	2.29	0.46	2.19	0		0	.
6	362.04	237.71	0.45	2.20	0.45	2.20	1	3	0	1.97
6	363.04	221.89	0.44	2.30	0.46	2.19	0		0	.
6	364.04	316.31	0.49	2.04	0.49	2.04	1	3	0	1.97
6	365.04	88.39	0.67	1.49	0.67	1.49	1	2	0	1.57
6	366.04	253.06	0.67	1.50	0.67	1.50	1	2	0	1.57
6	367.04	94.90	0.74	1.35	0.74	1.35	1	2	0	1.97
6	368.04	89.39	0.62	1.61	0.62	1.61	1	3	0	1.97
6	369.04	231.80	0.63	1.58	0.63	1.58	1	3	0	1.57
6	370.04	90.13	0.64	1.57	0.64	1.57	1	1	0	1.97
6	371.04	241.28	0.63	1.58	0.63	1.58	1	3	0	1.57
6	372.04	51.35	0.66	1.51	0.66	1.51	0		1	.
6	373.04	50.85	0.66	1.51	0.66	1.51	1	1	0	1.57
6	374.04	53.62	0.74	1.35	0.74	1.35	1	1	0	1.51

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	375.04	0	.	1	0	.	375	0	0.64	2	164.81
6	376.04	1	0	0	0	1	374	0	0.86	0	164.81
6	377.04	1	0	0	0	1	374	0	0.86	0	164.81
6	378.04	1	.	1	0	1	378	0	0.64	1	124.01
6	379.04	0	1	1	0	1	378	0	0.86	2	134.21
6	380.04	0	.	1	0	2	380	0	0.43	2	52.60
6	381.04	0	.	1	0	2	381	0	1.29	2	164.81
6	382.04	1	.	1	0	1	382	0	1.29	2	164.81
6	383.04	1	.	1	0	1	383	0	0.86	0	83.20
6	384.04	1	.	1	0	1	384	0	1.07	2	83.20
6	386.04	1	.	1	0	1	386	0	1.29	2	83.20
6	387.04	1	.	1	0	2	387	0	1.50	0	83.20
6	388.04	1	.	1	0	1	388	1	1.71	1	144.41
6	389.04	0	.	1	0	1	389	0	1.29	1	185.21
6	390.04	0	.	1	0	1	390	0	1.71	1	83.20
6	391.04	1	1	1	0	1	397	0	1.93	1	144.41
6	392.04	1	.	0	0	2	392	0	0.64	1	83.20
6	393.04	0	.	0	0	1	393	0	1.50	2	144.41
6	394.04	0	.	0	0	2	394	0	1.07	2	144.41
6	395.04	0	.	0	0	1	395	0	1.07	0	62.80
6	396.04	0	0	1	0	1	393	0	1.71	0	164.81
6	397.04	0	.	0	0	1	397	0	2.36	2	134.21
6	398.04	0	.	1	0	2	398	0	1.93	1	83.20
6	399.04	1	1	1	0	1	398	0	1.29	2	113.80
6	400.04	1	0	1	0	1	398	0	1.07	2	113.80
6	401.04	0	1	0	0	1	398	0	1.07	2	113.80
6	402.04	0	1	1	0	1	398	0	1.71	2	113.80
6	403.04	0	1	1	0	1	398	0	1.29	2	134.21
6	404.04	1	1	1	0	1	398	0	1.29	1	83.20
6	405.04	1	1	1	0	1	398	0	1.50	1	83.20
6	406.04	0	0	1	0	1	398	0	1.29	1	164.81
6	407.04	1	.	1	0	1	407	1	1.50	1	164.81
6	408.04	1	.	1	0	1	408	1	1.29	2	154.61
6	409.04	1	1	1	0	2	398	0	1.29	1	164.81
6	410.04	1	0	1	0	1	408	1	1.50	2	154.61
6	411.04	0	1	1	0	1	407	1	1.50	1	154.61
6	412.04	1	.	1	0	1	412	0	0.86	2	124.01
6	413.04	1	0	1	0	2	412	0	1.71	2	124.01
6	414.04	1	1	1	0	1	412	0	2.14	2	124.01
6	415.04	1	1	1	0	1	412	0	1.93	2	195.41
6	416.04	1	0	1	0	1	412	0	1.07	1	83.20
6	417.04	0	1	1	0	1	412	0	1.29	1	164.81
6	418.04	0	1	1	0	1	412	0	1.93	1	164.81
6	419.04	0	1	0	0	1	412	0	1.50	1	164.81
6	420.04	0	0	1	0	1	412	0	1.71	1	164.81
6	421.04	1	0	0	0	1	412	1	1.71	2	124.01
6	422.04	1	0	1	0	1	412	0	1.93	1	154.61
6	423.04	1	1	1	0	2	412	1	1.71	1	124.01
6	424.04	1	1	1	0	1	412	0	2.14	2	154.61
6	425.04	0	1	1	0	1	412	0	2.14	1	154.61

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	375.04	49.18	0.59	1.70	0.59	1.70	1	3	0	1.35
6	376.04	57.79	0.70	1.42	0.74	1.35	0		1	.
6	377.04	57.39	0.73	1.37	0.74	1.35	0		0	.
6	378.04	93.06	0.68	1.47	0.68	1.47	1	1	0	1.35
6	379.04	94.70	0.66	1.52	0.68	1.47	0		1	.
6	380.04	201.53	0.68	1.48	0.68	1.48	1	1	0	1.47
6	381.04	60.20	0.80	1.26	0.80	1.26	1	0	0	1.26
6	382.04	59.33	0.79	1.26	0.79	1.26	1	1	0	1.42
6	383.04	248.19	0.62	1.61	0.62	1.61	1	3	0	1.41
6	384.04	250.85	0.71	1.41	0.71	1.41	1	0	0	1.26
6	386.04	276.01	0.57	1.76	0.57	1.76	1	0	0	1.41
6	387.04	273.18	0.64	1.57	0.64	1.57	1	2	0	1.73
6	388.04	81.08	0.45	2.20	0.45	2.20	1	2	0	1.86
6	389.04	30.19	0.58	1.73	0.58	1.73	1	1	0	1.76
6	390.04	282.69	0.47	2.14	0.47	2.14	1	3	0	1.98
6	391.04	84.72	0.49	2.02	0.50	1.98	0		1	.
6	392.04	224.86	0.38	2.61	0.38	2.61	1	3	0	1.57
6	393.04	86.75	0.54	1.86	0.54	1.86	1	0	0	1.73
6	394.04	83.01	0.70	1.42	0.70	1.42	1	1	0	1.48
6	395.04	256.46	0.51	1.97	0.51	1.97	1	3	0	1.73
6	396.04	66.80	0.51	1.94	0.54	1.86	0		1	.
6	397.04	125.06	0.50	1.98	0.50	1.98	1	1	0	1.86
6	398.04	287.59	0.48	2.09	0.48	2.09	1	1	0	1.98
6	399.04	156.52	0.46	2.16	0.48	2.09	0		1	.
6	400.04	158.59	0.46	2.15	0.48	2.09	0		0	.
6	401.04	160.32	0.47	2.13	0.48	2.09	0		0	.
6	402.04	161.96	0.47	2.12	0.48	2.09	0		0	.
6	403.04	128.60	0.47	2.13	0.48	2.09	0		0	.
6	404.04	305.98	0.46	2.19	0.48	2.09	0		0	.
6	405.04	304.21	0.45	2.22	0.48	2.09	0		0	.
6	406.04	72.11	0.45	2.22	0.48	2.09	0		0	.
6	407.04	69.80	0.44	2.26	0.44	2.26	1	3	0	2.09
6	408.04	104.13	0.46	2.17	0.46	2.17	1	2	0	2.09
6	409.04	70.44	0.44	2.28	0.48	2.09	0		0	.
6	410.04	107.87	0.45	2.21	0.46	2.17	0		1	.
6	411.04	110.87	0.45	2.24	0.44	2.26	0		1	.
6	412.04	145.48	0.44	2.29	0.44	2.29	1	0	0	2.09
6	413.04	148.35	0.44	2.26	0.44	2.29	0		0	.
6	414.04	148.75	0.44	2.25	0.44	2.29	0		0	.
6	415.04	67.46	0.44	2.27	0.44	2.29	0		0	.
6	416.04	321.39	0.43	2.33	0.44	2.29	0		1	.
6	417.04	77.45	0.43	2.30	0.44	2.29	0		0	.
6	418.04	73.64	0.43	2.30	0.44	2.29	0		0	.
6	419.04	74.91	0.43	2.32	0.44	2.29	0		0	.
6	420.04	79.21	0.43	2.31	0.44	2.29	0		0	.
6	421.04	169.64	0.43	2.34	0.44	2.29	0		0	.
6	422.04	131.23	0.43	2.31	0.44	2.29	0		0	.
6	423.04	168.32	0.44	2.29	0.44	2.29	0		0	.
6	424.04	144.78	0.43	2.34	0.44	2.29	0		0	.
6	425.04	140.90	0.43	2.31	0.44	2.29	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	426.04	1	.	0	0	2	426	1	0.64	1	52.60
6	427.04	1	0	1	0	1	426	1	1.07	1	52.60
6	428.04	1	0	1	0	1	412	0	1.93	0	154.61
6	429.04	0	1	1	0	2	412	0	2.57	1	164.81
6	430.04	1	1	1	0	1	437	0	2.36	1	22.00
6	431.04	0	1	0	0	1	437	0	1.93	2	62.80
6	432.04	0	0	1	0	1	437	0	1.71	1	144.41
6	433.04	1	.	1	0	1	433	0	1.71	1	144.41
6	434.04	1	.	1	1	2	434	0	1.50	1	164.81
6	435.04	1	0	1	0	1	433	0	1.71	2	144.41
6	436.04	1	1	1	0	1	412	0	2.14	2	154.61
6	437.04	0	.	0	0	2	437	0	1.93	2	154.61
6	438.04	1	.	1	1	1	438	0	1.07	2	154.61
6	439.04	1	.	1	0	1	439	0	0.64	1	154.61
6	440.04	0	.	1	0	.	440	0	0.64	2	164.81
6	441.04	0	.	1	0	2	441	0	1.07	1	164.81
6	442.04	1	1	1	0	2	441	0	1.29	1	164.81
6	443.04	0	1	1	0	1	441	0	1.07	2	164.81
6	445.04	0	.	1	0	1	445	0	0.86	2	164.81
6	446.04	1	1	1	0	1	445	0	0.86	1	154.61
6	447.04	0	0	0	0	2	445	0	1.29	2	154.61
6	448.04	0	1	1	0	2	445	0	1.29	1	144.41
6	449.04	0	0	0	0	1	445	0	1.71	2	144.41
6	450.04	1	1	1	0	1	445	0	2.14	1	164.81
6	451.04	0	1	1	0	1	445	0	1.93	2	164.81
6	452.04	1	1	1	0	1	445	0	1.71	1	185.21
6	453.04	1	.	1	0	1	453	1	1.71	1	185.21
6	454.04	0	.	1	0	1	454	1	2.14	2	154.61
6	455.04	1	0	1	0	1	453	1	1.93	1	185.21
6	456.04	0	.	1	0	1	456	0	1.93	1	144.41
6	457.04	0	0	1	0	1	454	1	1.71	2	154.61
6	458.04	1	0	1	0	1	456	0	1.93	1	154.61
6	459.04	1	1	1	0	1	456	0	2.36	2	185.21
6	460.04	1	0	0	0	1	456	0	2.36	1	185.21
6	461.04	0	1	1	0	2	456	0	2.14	1	164.81
6	462.04	0	.	1	0	1	462	0	1.71	1	164.81
6	463.04	1	.	1	1	3	463	0	2.14	0	164.81
6	465.04	0	0	0	1	1	462	0	1.50	2	185.21
6	466.04	0	0	1	0	1	462	0	1.93	1	113.80
6	467.04	0	1	0	0	1	468	0	1.93	1	83.20
6	468.04	1	.	1	0	2	468	0	1.93	2	83.20
6	469.04	1	1	1	0	1	468	0	1.50	2	195.41
6	470.04	1	0	1	0	1	468	0	1.07	2	195.41
6	471.04	1	0	1	0	1	468	0	1.50	1	154.61
6	472.04	0	1	0	0	1	468	0	1.07	1	154.61
6	473.04	1	0	1	0	1	484	1	1.71	1	113.80
6	474.04	1	0	1	0	2	468	0	0.86	2	195.41
6	475.04	0	0	1	0	1	468	0	1.29	1	22.00
6	476.04	1	0	1	0	1	483	1	1.93	2	164.81
6	477.04	1	1	1	0	1	468	0	1.50	2	195.41

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	426.04	310.84	0.36	2.78	0.36	2.78	1	3	0	1.86
6	427.04	312.77	0.36	2.81	0.36	2.78	0		1	.
6	428.04	140.14	0.44	2.29	0.44	2.29	0		0	.
6	429.04	84.32	0.43	2.32	0.44	2.29	0		0	.
6	430.04	451.68	0.45	2.22	0.45	2.22	0		1	.
6	431.04	353.86	0.44	2.25	0.45	2.22	0		0	.
6	432.04	132.13	0.43	2.35	0.45	2.22	0		0	.
6	433.04	129.16	0.43	2.30	0.43	2.30	1	0	0	2.22
6	434.04	80.98	0.45	2.25	0.45	2.25	1	1	0	2.30
6	435.04	147.34	0.44	2.29	0.43	2.30	0		1	.
6	436.04	123.82	0.42	2.36	0.44	2.29	0		0	.
6	437.04	142.87	0.45	2.22	0.45	2.22	1	0	0	2.29
6	438.04	126.46	0.38	2.60	0.38	2.60	1	2	0	2.59
6	439.04	121.62	0.36	2.80	0.36	2.80	1	3	0	2.59
6	440.04	66.27	0.39	2.59	0.39	2.59	1	0	0	2.25
6	441.04	90.66	0.36	2.77	0.36	2.77	1	1	0	2.59
6	442.04	95.70	0.37	2.74	0.36	2.77	0		1	.
6	443.04	88.36	0.36	2.76	0.36	2.77	0		0	.
6	445.04	93.33	0.36	2.78	0.36	2.78	1	4	0	2.77
6	446.04	127.99	0.36	2.81	0.36	2.78	0		0	.
6	447.04	129.19	0.36	2.79	0.36	2.78	0		1	.
6	448.04	152.22	0.35	2.83	0.36	2.78	0		0	.
6	449.04	150.51	0.35	2.83	0.36	2.78	0		0	.
6	450.04	97.70	0.35	2.84	0.36	2.78	0		0	.
6	451.04	100.27	0.35	2.89	0.36	2.78	0		0	.
6	452.04	69.03	0.34	2.96	0.36	2.78	0		0	.
6	453.04	70.27	0.34	2.96	0.34	2.96	1	3	0	2.78
6	454.04	157.32	0.35	2.83	0.35	2.83	1	2	0	2.78
6	455.04	75.20	0.34	2.92	0.34	2.96	0		1	.
6	456.04	163.96	0.34	2.92	0.34	2.92	1	1	0	2.78
6	457.04	183.31	0.35	2.82	0.35	2.83	0		1	.
6	458.04	163.19	0.34	2.92	0.34	2.92	0		0	.
6	459.04	72.17	0.35	2.88	0.34	2.92	0		1	.
6	460.04	73.70	0.34	2.91	0.34	2.92	0		0	.
6	461.04	93.83	0.34	2.91	0.34	2.92	0		0	.
6	462.04	104.24	0.33	3.04	0.33	3.04	1	4	0	2.97
6	463.04	102.20	0.34	2.97	0.34	2.97	1	0	0	2.92
6	465.04	77.54	0.33	3.00	0.33	3.04	0		1	.
6	466.04	294.86	0.32	3.08	0.33	3.04	0		0	.
6	467.04	427.73	0.34	2.93	0.33	3.02	0		1	.
6	468.04	424.43	0.33	3.02	0.33	3.02	1	1	0	3.04
6	469.04	93.42	0.33	3.03	0.33	3.02	0		0	.
6	470.04	95.02	0.32	3.08	0.33	3.02	0		0	.
6	471.04	184.62	0.32	3.10	0.33	3.02	0		0	.
6	472.04	183.35	0.33	3.07	0.33	3.02	0		0	.
6	473.04	326.92	0.35	2.86	0.35	2.87	0		0	.
6	474.04	97.26	0.33	3.06	0.33	3.02	0		0	.
6	475.04	529.16	0.32	3.12	0.33	3.02	0		0	.
6	476.04	145.65	0.33	3.05	0.33	3.05	0		0	.
6	477.04	100.33	0.32	3.10	0.33	3.02	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	478.04	1	0	1	0	1	468	0	1.71	2	164.81
6	479.04	0	1	0	0	1	484	1	2.14	1	113.80
6	480.04	0	0	1	0	1	484	1	2.14	1	62.80
6	481.04	1	.	1	0	2	481	0	0.86	2	164.81
6	482.04	1	1	1	0	1	484	1	2.14	1	175.01
6	483.04	1	.	1	0	1	483	1	1.50	2	195.41
6	484.04	1	.	1	0	1	484	1	1.29	1	195.41
6	485.04	1	0	1	0	1	483	1	1.93	2	195.41
6	486.04	1	0	1	0	1	484	1	1.50	1	195.41
6	487.04	1	0	1	0	1	483	1	1.71	2	195.41
6	488.04	1	0	1	0	1	483	1	1.71	2	195.41
6	489.04	0	1	1	0	1	483	1	1.71	2	195.41
6	490.04	1	1	1	0	1	491	0	1.29	1	164.81
6	491.04	0	.	1	0	2	491	0	1.50	2	164.81
6	492.04	1	0	1	0	1	491	0	1.50	1	164.81
6	493.04	1	1	1	0	1	491	0	1.93	1	164.81
6	494.04	0	1	0	0	2	491	0	1.93	2	164.81
6	495.04	1	0	1	0	1	491	0	1.71	1	164.81
6	496.04	1	1	1	0	1	491	0	1.93	1	164.81
6	497.04	0	1	1	0	1	491	0	1.93	2	164.81
6	498.04	0	.	1	0	.	498	0	0.43	0	164.81
6	499.04	1	0	1	1	1	491	0	1.71	2	154.61
6	500.04	1	0	1	0	1	491	0	1.93	1	154.61
6	501.04	0	1	1	0	1	491	0	1.71	2	134.21
6	502.04	1	0	1	0	1	491	0	1.50	2	195.41
6	503.04	1	1	1	0	1	491	0	1.71	1	164.81
6	504.04	1	0	1	0	1	491	0	1.71	1	175.01
6	505.04	1	.	1	0	1	505	0	0.64	2	154.61
6	506.04	1	0	1	0	2	491	0	1.93	1	175.01
6	507.04	0	.	0	0	1	507	0	1.93	2	175.01
6	508.04	0	1	0	0	1	505	0	0.64	1	154.61
6	509.04	1	.	1	0	3	509	0	1.07	1	83.20
6	510.04	1	0	1	0	1	509	0	0.86	1	83.20
6	511.04	0	.	1	0	2	511	0	0.64	2	144.41
6	512.04	1	.	0	0	.	512	0	0.43	2	83.20
6	514.04	0	.	0	0	.	514	0	0.43	2	195.41
6	120.05	1	.	1	0	.	120	0	0.43	2	1.60
6	125.05	1	.	1	0	1	125	0	1.07	2	1.60
6	129.05	1	.	1	0	2	129	0	0.86	2	1.60
6	131.05	1	0	0	0	1	125	0	1.07	1	1.60
6	140.05	0	1	0	0	1	125	0	1.07	0	1.60
6	141.05	0	.	0	0	2	141	0	0.86	1	1.60
6	143.05	1	1	1	0	2	141	0	0.86	0	42.40
6	144.05	1	0	1	0	1	141	0	0.64	2	42.40
6	145.05	0	.	1	0	2	145	0	0.64	2	42.40
6	146.05	1	.	1	0	2	146	0	0.43	2	1.60
6	148.05	1	0	1	0	2	146	0	0.43	2	32.20
6	153.05	1	.	1	0	2	153	0	0.43	2	11.80
6	169.05	1	.	1	0	1	169	0	0.64	2	11.80
6	171.05	1	0	1	0	2	179	0	0.64	2	42.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	478.04	137.17	0.32	3.09	0.33	3.02	0		0	.
6	479.04	336.53	0.35	2.84	0.35	2.87	0		0	.
6	480.04	460.03	0.35	2.89	0.35	2.87	0		0	.
6	481.04	134.24	0.32	3.10	0.32	3.10	1	1	0	3.02
6	482.04	154.89	0.35	2.89	0.35	2.87	0		0	.
6	483.04	109.27	0.33	3.05	0.33	3.05	1	3	0	3.10
6	484.04	106.97	0.35	2.87	0.35	2.87	1	2	0	3.10
6	485.04	108.17	0.33	3.06	0.33	3.05	0		1	.
6	486.04	101.80	0.35	2.87	0.35	2.87	0		1	.
6	487.04	111.47	0.33	3.06	0.33	3.05	0		0	.
6	488.04	114.24	0.33	3.06	0.33	3.05	0		0	.
6	489.04	115.18	0.33	3.05	0.33	3.05	0		0	.
6	490.04	141.31	0.35	2.89	0.34	2.92	0		1	.
6	491.04	151.72	0.34	2.92	0.34	2.92	1	1	0	3.10
6	492.04	149.82	0.34	2.90	0.34	2.92	0		0	.
6	493.04	171.01	0.34	2.91	0.34	2.92	0		0	.
6	494.04	169.54	0.35	2.89	0.34	2.92	0		0	.
6	495.04	175.61	0.35	2.87	0.34	2.92	0		0	.
6	496.04	178.61	0.34	2.91	0.34	2.92	0		0	.
6	497.04	180.88	0.35	2.82	0.34	2.92	0		0	.
6	498.04	82.68	0.41	2.42	0.41	2.42	1	0	0	2.17
6	499.04	244.17	0.35	2.86	0.34	2.92	0		0	.
6	500.04	252.18	0.35	2.88	0.34	2.92	0		0	.
6	501.04	409.05	0.35	2.87	0.34	2.92	0		0	.
6	502.04	203.53	0.37	2.68	0.34	2.92	0		0	.
6	503.04	233.50	0.37	2.69	0.34	2.92	0		0	.
6	504.04	351.62	0.38	2.67	0.34	2.92	0		0	.
6	505.04	377.94	0.45	2.21	0.45	2.21	1	1	0	2.28
6	506.04	350.59	0.37	2.68	0.34	2.92	0		0	.
6	507.04	354.03	0.36	2.79	0.36	2.79	1	0	0	2.92
6	508.04	377.57	0.46	2.19	0.45	2.21	0		1	.
6	509.04	560.73	0.46	2.17	0.46	2.17	1	0	0	2.21
6	510.04	563.10	0.44	2.25	0.46	2.17	0		1	.
6	511.04	250.01	0.44	2.28	0.44	2.28	1	1	0	2.79
6	512.04	748.35	0.50	2.01	0.50	2.01	1	0	0	2.70
6	514.04	429.03	0.37	2.70	0.37	2.70	1	0	0	2.42
6	120.05	68.30	0.86	1.16	0.86	1.16	1	0	0	.
6	125.05	71.27	0.76	1.31	0.76	1.31	1	4	0	1.30
6	129.05	69.80	0.77	1.30	0.77	1.30	1	1	0	1.16
6	131.05	72.74	0.75	1.33	0.76	1.31	0		1	.
6	140.05	73.77	0.77	1.30	0.76	1.31	0		0	.
6	141.05	75.01	0.75	1.33	0.75	1.33	1	1	0	1.31
6	143.05	37.39	0.75	1.34	0.75	1.33	0		1	.
6	144.05	38.28	0.76	1.31	0.75	1.33	0		0	.
6	145.05	40.68	0.79	1.26	0.79	1.26	1	1	0	1.33
6	146.05	82.58	0.78	1.28	0.78	1.28	1	0	1	1.26
6	148.05	63.19	0.77	1.29	0.78	1.28	0		0	.
6	153.05	87.79	0.78	1.28	0.78	1.28	1	0	0	1.28
6	169.05	90.99	0.61	1.64	0.61	1.64	1	1	0	1.28
6	171.05	48.95	0.73	1.37	0.74	1.36	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	173.05	0	.	0	0	2	173	0	0.64	1	32.20
6	174.05	1	.	1	0	1	174	0	0.86	2	42.40
6	175.05	1	.	1	0	1	175	0	1.07	0	42.40
6	176.05	1	0	1	0	1	175	0	0.86	2	42.40
6	177.05	1	0	0	0	2	175	0	0.86	2	42.40
6	178.05	0	.	0	0	2	178	1	0.86	0	62.80
6	179.05	1	.	1	0	.	179	0	0.43	0	42.40
6	180.05	0	.	1	0	1	180	0	0.64	1	42.40
6	181.05	0	0	1	0	2	178	1	1.07	1	11.80
6	182.05	1	.	1	0	3	182	0	0.43	2	11.80
6	184.05	1	.	1	0	1	184	0	1.07	1	1.60
6	185.05	1	.	0	0	2	185	0	0.64	0	1.60
6	186.05	1	.	1	0	1	186	0	0.86	2	42.40
6	187.05	1	.	1	0	1	187	0	0.43	2	62.80
6	188.05	1	0	1	1	1	187	0	0.64	2	11.80
6	189.05	1	0	1	0	1	187	0	0.86	2	42.40
6	190.05	1	.	1	0	3	190	0	0.64	2	11.80
6	191.05	1	.	0	1	1	191	0	0.86	0	11.80
6	192.05	1	.	1	0	1	192	0	1.29	2	11.80
6	194.05	1	0	1	0	1	192	0	1.50	1	1.60
6	196.05	1	0	1	0	1	192	0	1.29	2	32.20
6	197.05	1	0	1	0	1	192	0	1.29	1	32.20
6	198.05	1	.	1	0	1	198	1	1.71	1	11.80
6	199.05	1	.	1	0	1	199	1	1.50	2	32.20
6	200.05	1	0	1	0	1	199	1	1.50	2	32.20
6	201.05	1	0	1	0	1	198	1	1.29	1	11.80
6	202.05	1	.	0	0	1	202	0	1.71	1	11.80
6	203.05	1	0	1	0	1	202	0	1.29	2	11.80
6	211.05	1	.	0	0	1	211	0	1.93	1	42.40
6	212.05	0	1	1	0	1	211	0	1.71	0	42.40
6	213.05	0	0	0	0	1	214	1	1.50	2	42.40
6	214.05	0	.	0	0	1	214	1	1.93	2	42.40
6	219.05	0	0	0	0	1	220	0	1.07	0	22.00
6	220.05	0	.	0	0	2	220	0	1.07	2	22.00
6	222.05	0	0	1	0	1	220	0	1.07	2	22.00
6	223.05	0	.	0	0	1	223	1	1.71	1	42.40
6	224.05	1	1	1	0	1	220	0	1.29	0	11.80
6	231.05	0	0	0	0	1	232	0	1.29	1	42.40
6	232.05	0	.	0	1	1	232	0	1.29	2	42.40
6	233.05	1	1	1	0	2	232	0	1.07	2	42.40
6	234.05	0	.	0	0	1	234	1	1.29	2	42.40
6	235.05	1	.	1	0	1	235	1	1.50	1	11.80
6	236.05	0	1	0	0	1	235	1	1.50	1	11.80
6	237.05	0	0	1	0	1	234	1	1.71	2	42.40
6	238.05	1	.	1	0	1	238	0	1.50	1	42.40
6	239.05	0	0	1	0	1	238	0	1.29	2	42.40
6	240.05	1	0	1	0	2	238	0	1.29	1	22.00
6	241.05	0	0	0	0	1	238	0	1.71	2	42.40
6	242.05	0	0	0	0	1	238	0	1.29	1	42.40
6	243.05	0	0	1	0	1	238	0	1.50	1	62.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	173.05	79.27	0.73	1.38	0.73	1.38	1	0	0	1.36
6	174.05	55.19	0.73	1.38	0.73	1.38	1	2	0	1.38
6	175.05	61.63	0.71	1.40	0.71	1.40	1	1	0	1.38
6	176.05	62.50	0.72	1.39	0.71	1.40	0		1	.
6	177.05	63.67	0.71	1.41	0.71	1.40	0		0	.
6	178.05	64.80	0.67	1.49	0.67	1.49	1	0	0	1.43
6	179.05	47.82	0.74	1.36	0.74	1.36	1	0	0	1.64
6	180.05	53.52	0.68	1.47	0.68	1.47	1	3	0	1.38
6	181.05	117.98	0.66	1.50	0.67	1.49	0		1	.
6	182.05	114.75	0.70	1.43	0.70	1.43	1	0	0	1.40
6	184.05	124.19	0.78	1.29	0.78	1.29	1	2	0	1.49
6	185.05	123.16	0.73	1.37	0.73	1.37	1	3	0	1.49
6	186.05	65.57	0.68	1.47	0.68	1.47	1	0	0	1.49
6	187.05	68.81	0.68	1.48	0.68	1.48	1	1	0	1.47
6	188.05	128.49	0.68	1.46	0.68	1.48	0		1	.
6	189.05	68.97	0.68	1.48	0.68	1.48	0		0	.
6	190.05	133.23	0.68	1.48	0.68	1.48	1	0	0	1.48
6	191.05	132.63	0.63	1.58	0.63	1.58	1	1	0	1.48
6	192.05	134.77	0.62	1.63	0.62	1.63	1	4	0	1.58
6	194.05	134.07	0.60	1.67	0.62	1.63	0		1	.
6	196.05	100.73	0.60	1.66	0.62	1.63	0		0	.
6	197.05	99.96	0.59	1.68	0.62	1.63	0		0	.
6	198.05	137.50	0.57	1.75	0.57	1.75	1	3	0	1.63
6	199.05	103.36	0.62	1.62	0.62	1.62	1	2	0	1.63
6	200.05	104.20	0.61	1.64	0.62	1.62	0		1	.
6	201.05	139.61	0.56	1.79	0.57	1.75	0		1	.
6	202.05	140.54	0.57	1.75	0.57	1.75	1	1	0	1.63
6	203.05	143.08	0.59	1.69	0.57	1.75	0		1	.
6	211.05	70.78	0.57	1.76	0.57	1.76	1	4	0	1.75
6	212.05	72.98	0.57	1.77	0.57	1.76	0		0	.
6	213.05	75.91	0.55	1.82	0.56	1.79	0		1	.
6	214.05	77.65	0.56	1.79	0.56	1.79	1	4	0	1.76
6	219.05	112.74	0.53	1.87	0.54	1.85	0		1	.
6	220.05	109.04	0.54	1.85	0.54	1.85	1	1	0	1.79
6	222.05	113.94	0.52	1.93	0.54	1.85	0		0	.
6	223.05	73.51	0.52	1.92	0.52	1.92	1	3	0	1.79
6	224.05	153.12	0.52	1.94	0.54	1.85	0		0	.
6	231.05	78.85	0.47	2.12	0.47	2.13	0		1	.
6	232.05	80.75	0.47	2.13	0.47	2.13	1	4	0	1.85
6	233.05	82.49	0.46	2.17	0.47	2.13	0		0	.
6	234.05	83.22	0.45	2.20	0.45	2.20	1	3	0	2.13
6	235.05	158.29	0.48	2.10	0.48	2.10	1	2	0	2.13
6	236.05	161.39	0.47	2.11	0.48	2.10	0		1	.
6	237.05	86.89	0.46	2.18	0.45	2.20	0		1	.
6	238.05	84.59	0.47	2.13	0.47	2.13	1	1	0	2.13
6	239.05	93.30	0.47	2.11	0.47	2.13	0		0	.
6	240.05	123.92	0.48	2.09	0.47	2.13	0		1	.
6	241.05	98.40	0.47	2.11	0.47	2.13	0		0	.
6	242.05	97.27	0.49	2.06	0.47	2.13	0		0	.
6	243.05	90.43	0.47	2.11	0.47	2.13	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	244.05	1	1	1	0	1	238	0	1.71	2	42.40
6	245.05	0	1	0	0	1	238	0	1.71	1	42.40
6	246.05	0	.	0	0	2	246	1	1.71	1	62.80
6	247.05	0	1	0	0	1	238	0	1.29	2	42.40
6	248.05	0	0	0	0	1	246	1	1.50	1	62.80
6	249.05	1	1	1	0	1	246	1	1.93	1	62.80
6	250.05	0	.	1	0	1	250	1	1.71	2	42.40
6	251.05	0	0	0	0	1	250	1	2.14	2	42.40
6	252.05	0	.	0	0	1	252	0	1.93	1	62.80
6	253.05	1	0	1	0	1	252	0	1.71	1	62.80
6	254.05	1	1	1	0	1	252	0	2.14	2	62.80
6	255.05	0	1	0	0	1	252	0	1.71	2	62.80
6	256.05	0	1	0	0	1	252	0	1.93	2	42.40
6	257.05	0	1	0	0	1	252	0	2.14	2	62.80
6	258.05	1	1	1	0	1	252	0	1.93	1	42.40
6	259.05	1	1	1	0	1	252	0	1.93	1	42.40
6	260.05	1	1	1	0	1	252	0	1.93	1	42.40
6	261.05	0	.	1	0	1	261	0	2.14	1	62.80
6	262.05	1	.	1	0	1	262	0	1.71	2	11.80
6	263.05	0	0	1	0	2	261	0	2.14	1	42.40
6	264.05	1	.	0	0	1	264	0	1.50	2	62.80
6	265.05	1	0	1	0	1	264	0	1.50	1	62.80
6	266.05	1	0	1	0	1	264	0	1.71	0	62.80
6	267.05	0	1	1	0	1	264	0	1.71	1	42.40
6	268.05	1	1	1	0	1	264	0	1.50	2	42.40
6	269.05	1	0	0	0	1	264	0	1.50	1	11.80
6	270.05	1	0	1	0	1	264	0	2.14	2	62.80
6	271.05	0	1	0	0	1	264	0	1.71	1	11.80
6	272.05	1	1	1	0	2	264	0	1.93	1	62.80
6	273.05	1	0	0	0	1	264	0	2.14	2	42.40
6	274.05	0	1	1	0	1	264	0	2.14	1	42.40
6	275.05	1	.	1	0	1	275	0	1.93	2	62.80
6	276.05	1	0	1	0	1	275	0	1.50	1	62.80
6	277.05	1	0	1	0	2	275	0	1.71	2	113.80
6	278.05	1	0	1	0	1	275	0	1.29	1	32.20
6	279.05	1	0	1	0	1	275	0	1.71	2	62.80
6	280.05	0	1	0	0	1	275	0	1.50	1	32.20
6	281.05	1	1	1	0	1	275	0	1.29	2	62.80
6	282.05	1	1	1	0	1	275	0	1.71	2	62.80
6	283.05	0	1	1	0	1	275	0	1.71	1	42.40
6	284.05	1	0	1	0	1	275	0	1.71	1	144.41
6	285.05	1	.	1	1	2	285	0	0.86	0	93.40
6	287.05	1	.	0	0	2	287	0	0.64	1	93.40
6	288.05	1	.	1	0	1	288	0	0.86	1	93.40
6	289.05	1	.	1	0	1	289	0	0.64	1	83.20
6	290.05	0	0	0	0	1	289	0	0.86	1	11.80
6	292.05	1	1	1	0	1	289	0	1.07	2	83.20
6	293.05	1	.	1	0	1	293	0	1.50	1	42.40
6	294.05	1	.	1	0	2	294	0	0.43	0	83.20
6	295.05	0	.	1	0	.	295	0	0.64	2	42.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	244.05	95.10	0.47	2.13	0.47	2.13	0		0	.
6	245.05	101.74	0.48	2.10	0.47	2.13	0		0	.
6	246.05	98.40	0.47	2.11	0.47	2.11	1	3	0	2.13
6	247.05	91.80	0.47	2.12	0.47	2.13	0		0	.
6	248.05	105.08	0.47	2.13	0.47	2.11	0		1	.
6	249.05	106.34	0.47	2.13	0.47	2.11	0		0	.
6	250.05	105.98	0.49	2.03	0.49	2.03	1	2	0	2.13
6	251.05	108.28	0.49	2.03	0.49	2.03	0		1	.
6	252.05	112.38	0.48	2.09	0.48	2.09	1	1	0	2.13
6	253.05	113.78	0.47	2.11	0.48	2.09	0		0	.
6	254.05	116.25	0.48	2.08	0.48	2.09	0		1	.
6	255.05	121.79	0.48	2.06	0.48	2.09	0		0	.
6	256.05	120.69	0.49	2.05	0.48	2.09	0		0	.
6	257.05	119.86	0.49	2.03	0.48	2.09	0		0	.
6	258.05	111.08	0.48	2.08	0.48	2.09	0		0	.
6	259.05	112.95	0.47	2.13	0.48	2.09	0		0	.
6	260.05	99.74	0.47	2.11	0.48	2.09	0		0	.
6	261.05	118.46	0.48	2.09	0.48	2.09	1	3	0	2.09
6	262.05	191.22	0.52	1.91	0.52	1.91	1	2	0	2.09
6	263.05	119.29	0.48	2.10	0.48	2.09	0		1	.
6	264.05	125.33	0.50	1.99	0.50	1.99	1	1	0	2.09
6	265.05	123.63	0.49	2.04	0.50	1.99	0		1	.
6	266.05	126.73	0.49	2.04	0.50	1.99	0		0	.
6	267.05	128.87	0.50	2.00	0.50	1.99	0		0	.
6	268.05	127.70	0.50	2.00	0.50	1.99	0		0	.
6	269.05	198.40	0.50	1.98	0.50	1.99	0		0	.
6	270.05	132.70	0.50	1.99	0.50	1.99	0		0	.
6	271.05	199.93	0.50	1.98	0.50	1.99	0		0	.
6	272.05	131.37	0.50	2.00	0.50	1.99	0		0	.
6	273.05	130.67	0.50	1.99	0.50	1.99	0		0	.
6	274.05	133.34	0.50	2.00	0.50	1.99	0		0	.
6	275.05	135.61	0.50	2.00	0.50	2.00	1	1	0	1.99
6	276.05	137.27	0.51	1.96	0.50	2.00	0		1	.
6	277.05	55.73	0.50	2.01	0.50	2.00	0		0	.
6	278.05	177.64	0.50	1.99	0.50	2.00	0		0	.
6	279.05	140.41	0.50	2.00	0.50	2.00	0		0	.
6	280.05	180.74	0.51	1.96	0.50	2.00	0		0	.
6	281.05	139.28	0.50	2.00	0.50	2.00	0		0	.
6	282.05	142.01	0.50	2.00	0.50	2.00	0		0	.
6	283.05	134.87	0.51	1.98	0.50	2.00	0		0	.
6	284.05	44.25	0.51	1.98	0.50	2.00	0		0	.
6	285.05	86.55	0.66	1.51	0.66	1.51	1	1	0	2.00
6	287.05	91.15	0.67	1.50	0.67	1.50	1	1	0	1.51
6	288.05	88.85	0.69	1.46	0.69	1.46	1	2	0	1.50
6	289.05	86.12	0.53	1.87	0.53	1.87	1	1	0	1.86
6	290.05	240.57	0.55	1.83	0.53	1.87	0		0	.
6	292.05	89.26	0.54	1.84	0.53	1.87	0		0	.
6	293.05	167.57	0.49	2.04	0.49	2.04	1	3	0	1.87
6	294.05	83.71	0.54	1.86	0.54	1.86	1	1	0	1.50
6	295.05	139.78	0.52	1.91	0.52	1.91	1	3	0	1.50

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	296.05	0	.	1	0	2	296	0	1.71	2	113.80
6	297.05	0	1	0	0	1	289	0	1.29	2	83.20
6	298.05	1	.	1	0	1	298	1	1.71	2	103.60
6	300.05	1	0	1	0	1	298	1	1.07	2	83.20
6	301.05	1	.	0	0	1	301	0	1.29	2	62.80
6	302.05	1	0	1	0	1	301	0	1.07	0	62.80
6	303.05	1	.	0	0	1	303	0	1.29	2	83.20
6	304.05	1	0	1	0	1	301	0	0.86	2	62.80
6	305.05	1	1	0	0	1	307	0	0.64	1	83.20
6	306.05	0	.	0	0	2	306	0	0.64	2	62.80
6	307.05	0	.	0	0	2	307	0	0.86	2	83.20
6	308.05	1	.	0	0	1	308	0	1.29	1	83.20
6	309.05	0	.	1	0	2	309	0	0.86	0	62.80
6	310.05	1	.	1	0	2	310	0	0.64	2	62.80
6	312.05	1	0	1	0	1	301	0	1.29	1	22.00
6	313.05	1	.	1	0	1	313	1	1.07	1	42.40
6	314.05	0	1	0	0	1	313	1	1.71	1	42.40
6	315.05	1	.	1	0	3	315	0	0.43	2	83.20
6	316.05	0	.	1	0	2	316	0	0.43	2	144.41
6	317.05	1	1	1	0	2	316	0	0.64	2	62.80
6	318.05	1	.	1	0	2	318	0	0.64	1	42.40
6	319.05	1	.	1	0	1	319	0	0.86	2	42.40
6	320.05	1	.	1	0	1	320	0	0.86	1	42.40
6	321.05	1	0	0	0	2	324	0	1.07	1	62.80
6	322.05	1	.	1	0	1	322	0	0.86	0	62.80
6	323.05	1	0	1	0	1	324	0	0.86	2	113.80
6	324.05	1	.	1	0	2	324	0	1.29	1	62.80
6	325.05	0	1	0	0	1	324	0	0.64	2	83.20
6	326.05	0	0	0	0	1	324	0	0.86	1	62.80
6	327.05	1	1	1	0	1	324	0	1.07	2	83.20
6	328.05	0	0	1	0	2	324	0	1.07	1	62.80
6	329.05	1	0	1	0	2	324	0	0.43	2	62.80
6	330.05	1	1	1	0	3	331	0	0.43	1	42.40
6	331.05	0	.	0	0	1	331	0	0.86	2	42.40
6	332.05	0	1	0	0	2	331	0	1.29	1	62.80
6	333.05	1	0	0	0	1	331	0	1.29	1	83.20
6	334.05	1	1	1	0	1	331	0	1.29	2	83.20
6	335.05	1	0	1	0	1	331	0	1.07	2	62.80
6	336.05	1	0	1	0	1	331	0	1.29	2	62.80
6	337.05	1	.	1	0	1	337	1	1.71	2	62.80
6	338.05	1	0	1	0	1	331	0	1.07	1	32.20
6	339.05	1	0	1	0	1	337	1	1.71	2	62.80
6	340.05	1	.	1	0	1	340	1	1.50	1	62.80
6	341.05	0	0	1	0	1	348	0	1.50	1	144.41
6	342.05	0	1	1	0	1	340	1	2.14	1	62.80
6	343.05	1	.	0	0	1	343	0	1.29	1	62.80
6	344.05	0	0	0	0	1	343	0	0.86	1	93.40
6	345.05	0	1	1	0	2	343	0	1.07	2	93.40
6	346.05	1	1	1	0	2	343	0	1.07	2	83.20
6	347.05	1	.	1	0	1	347	0	1.07	2	62.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	296.05	61.50	0.54	1.84	0.54	1.84	1	2	0	1.87
6	297.05	87.35	0.55	1.80	0.53	1.87	0		1	.
6	298.05	75.88	0.54	1.84	0.54	1.84	1	2	0	1.87
6	300.05	98.69	0.53	1.88	0.54	1.84	0		1	.
6	301.05	165.57	0.53	1.90	0.53	1.90	1	1	0	1.87
6	302.05	167.10	0.54	1.86	0.53	1.90	0		0	.
6	303.05	103.47	0.55	1.82	0.55	1.82	1	2	0	1.82
6	304.05	169.11	0.54	1.86	0.53	1.90	0		0	.
6	305.05	102.37	0.53	1.87	0.55	1.82	0		1	.
6	306.05	172.08	0.55	1.83	0.55	1.83	1	1	0	1.90
6	307.05	104.40	0.55	1.82	0.55	1.82	1	1	0	1.83
6	308.05	100.73	0.53	1.88	0.53	1.88	1	3	0	1.82
6	309.05	192.20	0.69	1.45	0.69	1.45	1	2	0	1.58
6	310.05	188.96	0.63	1.58	0.63	1.58	1	0	0	1.70
6	312.05	218.21	0.54	1.84	0.53	1.90	0		1	.
6	313.05	170.21	0.51	1.98	0.51	1.98	1	3	0	1.87
6	314.05	171.68	0.51	1.95	0.51	1.98	0		1	.
6	315.05	106.37	0.62	1.61	0.62	1.61	1	0	0	1.82
6	316.05	45.88	0.59	1.70	0.59	1.70	1	0	0	1.61
6	317.05	186.22	0.60	1.67	0.59	1.70	0		0	.
6	318.05	183.42	0.48	2.10	0.48	2.10	1	3	0	1.58
6	319.05	185.36	0.51	1.96	0.51	1.96	1	3	0	1.58
6	320.05	185.39	0.49	2.03	0.49	2.03	1	3	0	1.58
6	321.05	190.26	0.53	1.89	0.53	1.88	0		1	.
6	322.05	185.62	0.55	1.82	0.55	1.82	1	2	0	1.58
6	323.05	87.06	0.53	1.88	0.53	1.88	0		0	.
6	324.05	190.72	0.53	1.88	0.53	1.88	1	1	0	1.58
6	325.05	108.49	0.54	1.86	0.53	1.88	0		0	.
6	326.05	194.83	0.54	1.84	0.53	1.88	0		0	.
6	327.05	110.07	0.54	1.84	0.53	1.88	0		0	.
6	328.05	196.57	0.54	1.84	0.53	1.88	0		0	.
6	329.05	202.77	0.55	1.83	0.53	1.88	0		0	.
6	330.05	198.04	0.54	1.85	0.55	1.81	0		1	.
6	331.05	201.71	0.55	1.81	0.55	1.81	1	1	0	1.88
6	332.05	198.30	0.55	1.83	0.55	1.81	0		0	.
6	333.05	113.21	0.55	1.81	0.55	1.81	0		0	.
6	334.05	112.04	0.53	1.88	0.55	1.81	0		0	.
6	335.05	214.89	0.53	1.89	0.55	1.81	0		0	.
6	336.05	217.09	0.53	1.89	0.55	1.81	0		0	.
6	337.05	219.29	0.53	1.89	0.53	1.89	1	3	0	1.81
6	338.05	185.61	0.53	1.89	0.55	1.81	0		0	.
6	339.05	207.81	0.53	1.90	0.53	1.89	0		1	.
6	340.05	203.14	0.53	1.87	0.53	1.87	1	2	0	1.81
6	341.05	51.95	0.59	1.70	0.60	1.67	0		0	.
6	342.05	205.34	0.53	1.88	0.53	1.87	0		1	.
6	343.05	211.08	0.53	1.88	0.53	1.88	1	1	0	1.81
6	344.05	114.71	0.54	1.85	0.53	1.88	0		0	.
6	345.05	114.94	0.54	1.86	0.53	1.88	0		1	.
6	346.05	117.78	0.53	1.87	0.53	1.88	0		0	.
6	347.05	231.57	0.60	1.68	0.60	1.68	1	1	0	1.70

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	348.05	1	.	1	0	1	348	0	1.50	1	144.41
6	349.05	0	1	0	0	1	348	0	1.93	2	144.41
6	350.05	0	.	0	0	1	350	0	0.86	2	93.40
6	351.05	0	.	1	0	2	351	0	1.07	1	62.80
6	352.05	0	.	1	1	1	352	0	1.29	2	83.20
6	353.05	1	.	1	0	1	353	1	1.29	2	62.80
6	354.05	1	.	1	0	1	354	0	1.29	0	144.41
6	355.05	1	.	1	0	1	355	0	0.86	1	62.80
6	356.05	1	.	1	0	1	356	0	0.86	2	62.80
6	357.05	1	.	0	0	1	357	0	0.64	1	62.80
6	358.05	1	.	1	0	1	358	0	1.07	2	32.20
6	359.05	1	.	0	0	1	359	0	0.86	1	62.80
6	360.05	1	.	1	0	1	360	0	1.07	1	62.80
6	361.05	1	.	1	0	1	361	1	1.50	1	62.80
6	362.05	1	.	1	0	1	362	0	0.64	2	62.80
6	363.05	0	1	0	0	1	361	1	1.07	1	62.80
6	364.05	0	.	0	0	.	364	0	0.43	0	32.20
6	365.05	0	1	1	0	1	370	0	1.50	1	42.40
6	366.05	1	1	1	0	1	371	0	1.71	1	62.80
6	367.05	0	.	0	0	1	367	0	1.50	0	103.60
6	368.05	0	.	0	0	.	368	0	0.64	2	103.60
6	369.05	1	1	1	0	1	370	0	1.07	0	62.80
6	370.05	0	.	1	0	1	370	0	1.29	2	42.40
6	371.05	0	.	0	0	1	371	0	1.29	0	62.80
6	372.05	1	0	1	0	1	371	0	1.50	0	144.41
6	373.05	1	0	0	0	1	371	0	1.50	2	144.41
6	374.05	1	.	1	0	1	374	0	1.29	1	144.41
6	375.05	0	.	1	0	1	375	0	0.86	2	144.41
6	376.05	1	.	0	0	1	376	0	1.71	2	144.41
6	377.05	1	.	0	0	1	377	0	1.93	2	144.41
6	378.05	1	.	1	0	1	378	0	1.50	1	103.60
6	379.05	0	.	1	0	1	379	0	1.50	0	113.80
6	380.05	0	.	1	0	2	380	0	1.29	0	32.20
6	381.05	0	.	1	0	1	381	0	2.14	2	144.41
6	382.05	1	.	1	0	1	382	0	1.93	2	144.41
6	383.05	1	.	1	0	1	383	0	1.50	1	62.80
6	384.05	1	.	1	0	1	384	0	1.93	1	62.80
6	386.05	1	.	1	0	1	386	0	2.36	0	62.80
6	387.05	1	0	1	0	1	395	1	2.14	1	62.80
6	388.05	1	1	1	0	1	395	1	1.93	1	124.01
6	389.05	0	0	1	0	1	395	1	2.14	1	164.81
6	390.05	0	0	1	0	1	393	0	1.93	1	62.80
6	391.05	1	1	1	0	1	393	0	2.14	1	124.01
6	392.05	1	.	0	0	1	392	0	0.43	1	62.80
6	393.05	0	.	0	0	1	393	0	2.14	2	124.01
6	394.05	0	.	0	0	1	394	0	1.50	2	124.01
6	395.05	0	.	0	0	1	395	1	1.93	1	42.40
6	396.05	0	0	1	0	1	393	0	1.93	1	144.41
6	397.05	0	0	0	0	1	393	0	2.36	2	113.80
6	398.05	0	.	1	0	1	398	1	2.57	1	62.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	348.05	56.39	0.60	1.67	0.60	1.67	1	1	0	1.92
6	349.05	54.46	0.61	1.64	0.60	1.67	0		1	.
6	350.05	119.68	0.59	1.70	0.59	1.70	1	0	0	1.88
6	351.05	238.08	0.55	1.80	0.55	1.80	1	1	0	1.67
6	352.05	124.62	0.61	1.65	0.61	1.65	1	2	0	1.68
6	353.05	228.77	0.59	1.70	0.59	1.70	1	2	0	1.67
6	354.05	55.02	0.92	1.09	0.92	1.09	1	2	0	1.60
6	355.05	237.64	0.59	1.69	0.59	1.69	1	2	0	1.80
6	356.05	240.58	0.56	1.78	0.56	1.78	1	3	0	1.80
6	357.05	213.48	0.51	1.95	0.51	1.95	1	3	0	1.68
6	358.05	317.78	0.62	1.60	0.62	1.60	1	1	0	1.80
6	359.05	215.92	0.52	1.92	0.52	1.92	1	1	0	1.68
6	360.05	230.10	0.53	1.89	0.53	1.89	1	3	0	1.80
6	361.05	216.59	0.50	1.99	0.50	1.99	1	3	0	1.67
6	362.05	237.71	0.58	1.72	0.58	1.72	1	2	0	1.80
6	363.05	221.89	0.51	1.98	0.50	1.99	0		0	.
6	364.05	316.31	0.66	1.51	0.66	1.51	1	2	0	1.60
6	365.05	88.39	0.59	1.69	0.58	1.73	0		0	.
6	366.05	253.06	0.59	1.70	0.58	1.71	0		1	.
6	367.05	94.90	0.67	1.49	0.67	1.49	1	2	0	1.60
6	368.05	89.39	0.54	1.87	0.54	1.87	1	3	0	1.60
6	369.05	231.80	0.57	1.76	0.58	1.73	0		1	.
6	370.05	90.13	0.58	1.73	0.58	1.73	1	3	0	1.60
6	371.05	241.28	0.58	1.71	0.58	1.71	1	0	0	1.60
6	372.05	51.35	0.56	1.77	0.58	1.71	0		0	.
6	373.05	50.85	0.56	1.79	0.58	1.71	0		0	.
6	374.05	53.62	0.58	1.71	0.58	1.71	1	1	0	1.81
6	375.05	49.18	0.55	1.81	0.55	1.81	1	0	0	1.71
6	376.05	57.79	0.61	1.65	0.61	1.65	1	1	0	1.71
6	377.05	57.39	0.61	1.64	0.61	1.64	1	2	0	1.65
6	378.05	93.06	0.50	2.01	0.50	2.01	1	3	0	1.65
6	379.05	94.70	0.52	1.92	0.52	1.92	1	2	0	1.65
6	380.05	201.53	0.44	2.29	0.44	2.29	1	3	0	1.65
6	381.05	60.20	0.49	2.04	0.49	2.04	1	2	0	1.97
6	382.05	59.33	0.51	1.97	0.51	1.97	1	1	0	1.65
6	383.05	248.19	0.40	2.49	0.40	2.49	1	3	0	1.97
6	384.05	250.85	0.41	2.46	0.41	2.46	1	3	0	1.97
6	386.05	276.01	0.49	2.04	0.49	2.04	1	2	0	1.97
6	387.05	273.18	0.41	2.46	0.41	2.46	0		0	.
6	388.05	81.08	0.41	2.44	0.41	2.46	0		0	.
6	389.05	30.19	0.41	2.43	0.41	2.46	0		1	.
6	390.05	282.69	0.43	2.33	0.44	2.29	0		1	.
6	391.05	84.72	0.43	2.35	0.44	2.29	0		0	.
6	392.05	224.86	0.45	2.24	0.45	2.24	1	3	0	1.60
6	393.05	86.75	0.44	2.29	0.44	2.29	1	1	0	1.97
6	394.05	83.01	0.54	1.86	0.54	1.86	1	2	0	1.65
6	395.05	256.46	0.41	2.46	0.41	2.46	1	3	0	1.97
6	396.05	66.80	0.43	2.35	0.44	2.29	0		0	.
6	397.05	125.06	0.43	2.35	0.44	2.29	0		0	.
6	398.05	287.59	0.43	2.34	0.43	2.34	1	3	0	2.29

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	399.05	1	.	1	0	1	399	1	1.71	2	93.40
6	400.05	1	0	1	0	1	399	1	1.50	2	93.40
6	401.05	0	1	0	0	1	399	1	1.50	2	93.40
6	402.05	0	0	1	0	1	399	1	1.29	2	93.40
6	403.05	0	0	1	0	1	399	1	1.29	2	113.80
6	404.05	1	0	1	0	1	398	1	1.50	1	62.80
6	405.05	1	1	1	0	1	398	1	1.50	1	62.80
6	406.05	0	1	1	0	1	398	1	1.29	1	144.41
6	407.05	1	.	1	0	1	407	1	1.71	1	144.41
6	408.05	1	.	1	0	1	408	1	1.29	2	134.21
6	409.05	1	1	1	0	1	398	1	1.29	1	144.41
6	410.05	1	0	1	0	1	408	1	1.29	2	134.21
6	411.05	0	1	1	0	1	407	1	1.29	1	134.21
6	412.05	1	.	1	0	1	412	0	1.07	2	103.60
6	413.05	1	0	1	0	2	412	0	1.71	2	103.60
6	414.05	1	1	1	0	2	412	0	2.14	2	103.60
6	415.05	1	1	1	0	1	412	0	1.93	2	175.01
6	416.05	1	0	1	0	2	412	0	1.29	1	62.80
6	417.05	0	1	1	0	1	412	0	1.29	1	144.41
6	418.05	0	0	1	0	2	412	0	1.93	1	144.41
6	419.05	0	1	0	0	1	412	0	1.29	1	144.41
6	420.05	0	1	1	0	1	412	0	1.71	1	144.41
6	421.05	1	0	0	0	1	412	0	1.71	2	103.60
6	422.05	1	0	1	0	1	412	0	1.71	1	134.21
6	423.05	1	1	1	0	2	412	0	1.71	1	103.60
6	424.05	1	1	1	0	1	412	0	2.14	2	134.21
6	425.05	0	1	1	0	1	412	0	1.93	1	134.21
6	426.05	1	.	0	0	3	426	0	0.64	1	32.20
6	427.05	1	0	1	0	1	426	0	1.07	1	32.20
6	428.05	1	.	1	0	1	428	0	1.29	2	134.21
6	429.05	0	.	1	0	1	429	0	2.14	0	144.41
6	430.05	1	.	1	0	1	430	0	1.93	1	1.60
6	431.05	0	.	0	0	1	431	0	1.93	0	42.40
6	432.05	0	1	1	0	1	430	0	1.71	0	124.01
6	433.05	1	.	1	0	1	433	0	1.93	1	124.01
6	434.05	1	.	1	1	2	434	0	1.29	0	144.41
6	435.05	1	.	1	0	1	435	0	1.71	0	124.01
6	436.05	1	.	1	0	1	436	0	1.71	2	134.21
6	437.05	0	.	0	0	1	437	0	1.50	2	134.21
6	438.05	1	.	1	1	1	438	0	1.07	2	134.21
6	439.05	1	.	1	0	1	439	0	1.29	1	134.21
6	440.05	0	.	1	0	.	440	0	0.64	2	144.41
6	441.05	0	.	1	0	2	441	0	1.07	1	144.41
6	442.05	1	1	1	0	1	441	0	1.07	0	144.41
6	443.05	0	.	1	0	2	443	0	0.86	2	144.41
6	445.05	0	0	1	0	2	443	0	0.64	2	144.41
6	446.05	1	1	1	0	1	443	0	0.86	1	134.21
6	447.05	0	0	0	0	1	443	0	1.29	2	134.21
6	448.05	0	1	1	0	2	443	0	1.50	1	124.01
6	449.05	0	0	0	0	1	443	0	1.93	2	124.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	399.05	156.52	0.44	2.27	0.44	2.27	1	2	0	2.29
6	400.05	158.59	0.45	2.21	0.44	2.27	0		1	.
6	401.05	160.32	0.45	2.20	0.44	2.27	0		0	.
6	402.05	161.96	0.46	2.19	0.44	2.27	0		0	.
6	403.05	128.60	0.46	2.15	0.44	2.27	0		0	.
6	404.05	305.98	0.42	2.38	0.43	2.34	0		0	.
6	405.05	304.21	0.42	2.38	0.43	2.34	0		1	.
6	406.05	72.11	0.45	2.22	0.43	2.34	0		0	.
6	407.05	69.80	0.45	2.24	0.45	2.24	1	2	0	2.29
6	408.05	104.13	0.44	2.25	0.44	2.25	1	3	0	2.29
6	409.05	70.44	0.45	2.22	0.43	2.34	0		0	.
6	410.05	107.87	0.44	2.26	0.44	2.25	0		1	.
6	411.05	110.87	0.45	2.24	0.45	2.24	0		1	.
6	412.05	145.48	0.43	2.31	0.43	2.31	1	1	0	2.29
6	413.05	148.35	0.43	2.31	0.43	2.31	0		0	.
6	414.05	148.75	0.43	2.31	0.43	2.31	0		0	.
6	415.05	67.46	0.43	2.30	0.43	2.31	0		0	.
6	416.05	321.39	0.43	2.32	0.43	2.31	0		1	.
6	417.05	77.45	0.43	2.33	0.43	2.31	0		0	.
6	418.05	73.64	0.43	2.32	0.43	2.31	0		0	.
6	419.05	74.91	0.43	2.33	0.43	2.31	0		0	.
6	420.05	79.21	0.43	2.32	0.43	2.31	0		0	.
6	421.05	169.64	0.44	2.28	0.43	2.31	0		0	.
6	422.05	131.23	0.44	2.25	0.43	2.31	0		0	.
6	423.05	168.32	0.43	2.31	0.43	2.31	0		0	.
6	424.05	144.78	0.45	2.21	0.43	2.31	0		0	.
6	425.05	140.90	0.45	2.23	0.43	2.31	0		0	.
6	426.05	310.84	0.30	3.30	0.30	3.30	1	3	0	1.65
6	427.05	312.77	0.30	3.29	0.30	3.30	0		1	.
6	428.05	140.14	0.50	2.00	0.50	2.00	1	1	0	2.31
6	429.05	84.32	0.50	2.01	0.50	2.01	1	2	0	2.31
6	430.05	451.68	0.41	2.42	0.41	2.42	1	3	0	2.00
6	431.05	353.86	0.49	2.04	0.49	2.04	1	2	0	2.00
6	432.05	132.13	0.40	2.49	0.41	2.42	0		1	.
6	433.05	129.16	0.39	2.58	0.39	2.58	1	3	0	2.00
6	434.05	80.98	0.41	2.46	0.41	2.46	1	3	0	2.00
6	435.05	147.34	0.49	2.05	0.49	2.05	1	2	0	2.00
6	436.05	123.82	0.45	2.23	0.45	2.23	1	3	0	2.31
6	437.05	142.87	0.51	1.96	0.51	1.96	1	2	0	2.00
6	438.05	126.46	0.36	2.81	0.36	2.81	1	1	0	2.00
6	439.05	121.62	0.28	3.52	0.28	3.52	1	3	0	2.00
6	440.05	66.27	0.36	2.81	0.36	2.81	1	2	0	2.00
6	441.05	90.66	0.37	2.73	0.37	2.73	1	1	0	2.81
6	442.05	95.70	0.36	2.79	0.37	2.73	0		1	.
6	443.05	88.36	0.37	2.72	0.37	2.72	1	1	0	2.73
6	445.05	93.33	0.37	2.69	0.37	2.72	0		1	.
6	446.05	127.99	0.36	2.78	0.37	2.72	0		0	.
6	447.05	129.19	0.36	2.75	0.37	2.72	0		0	.
6	448.05	152.22	0.36	2.76	0.37	2.72	0		0	.
6	449.05	150.51	0.36	2.76	0.37	2.72	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	450.05	1	1	1	0	1	443	0	1.93	1	144.41
6	451.05	0	1	1	0	1	443	0	2.14	2	144.41
6	452.05	1	1	1	0	1	443	0	1.71	1	164.81
6	453.05	1	0	1	0	1	443	0	2.14	1	164.81
6	454.05	0	1	1	0	1	443	0	1.93	2	134.21
6	455.05	1	.	1	0	1	455	0	2.14	1	164.81
6	456.05	0	.	1	0	1	456	1	1.93	1	124.01
6	457.05	0	.	1	0	1	457	1	1.50	2	134.21
6	458.05	1	1	1	0	1	456	1	1.71	1	134.21
6	459.05	1	1	1	0	1	457	1	1.93	2	164.81
6	460.05	1	.	0	0	1	460	0	1.93	1	164.81
6	461.05	0	1	1	0	2	460	0	1.93	1	144.41
6	462.05	0	.	1	0	2	462	0	1.29	2	144.41
6	463.05	1	.	1	1	3	463	0	1.71	1	144.41
6	465.05	0	0	0	1	2	462	0	1.07	2	164.81
6	466.05	0	.	1	0	1	466	0	1.50	0	93.40
6	467.05	0	.	0	0	1	467	0	1.50	1	62.80
6	468.05	1	.	1	0	2	468	0	1.29	1	62.80
6	469.05	1	1	1	0	1	467	0	0.86	2	175.01
6	470.05	1	0	1	0	2	467	0	1.07	2	175.01
6	471.05	1	0	1	0	1	467	0	1.71	1	134.21
6	472.05	0	1	0	0	1	467	0	1.07	1	134.21
6	473.05	1	0	1	0	2	481	0	1.93	1	93.40
6	474.05	1	0	1	0	2	467	0	1.07	2	175.01
6	475.05	0	0	1	0	1	467	0	1.29	1	1.60
6	476.05	1	0	1	0	1	481	0	1.93	2	144.41
6	477.05	1	1	1	0	1	467	0	1.29	2	175.01
6	478.05	1	0	1	0	1	467	0	1.50	2	144.41
6	479.05	0	1	0	0	1	481	0	1.71	1	93.40
6	480.05	0	1	1	0	1	481	0	1.93	1	42.40
6	481.05	1	.	1	0	3	481	0	0.64	2	144.41
6	482.05	1	1	1	0	1	481	0	1.50	0	154.61
6	483.05	1	0	1	0	2	481	0	0.86	2	175.01
6	484.05	1	0	1	0	1	481	0	1.07	1	175.01
6	485.05	1	0	1	0	1	481	0	1.29	2	175.01
6	486.05	1	0	1	0	1	481	0	1.71	1	175.01
6	487.05	1	0	1	0	1	481	0	1.71	2	175.01
6	488.05	1	1	1	0	1	481	0	1.50	2	175.01
6	489.05	0	0	1	0	2	481	0	1.50	2	175.01
6	490.05	1	.	1	0	1	490	0	0.86	1	144.41
6	491.05	0	.	1	0	1	491	0	1.29	2	144.41
6	492.05	1	.	1	0	1	492	0	1.07	0	144.41
6	493.05	1	0	1	0	1	492	0	1.71	1	144.41
6	494.05	0	1	0	0	1	492	0	1.71	2	144.41
6	495.05	1	.	1	0	1	495	0	1.50	1	144.41
6	496.05	1	1	1	0	1	495	0	1.50	1	144.41
6	497.05	0	1	1	0	1	495	0	1.71	2	144.41
6	498.05	0	.	1	0	.	498	0	0.43	0	144.41
6	499.05	1	0	1	1	1	495	0	1.50	2	134.21
6	500.05	1	0	1	0	1	495	0	1.71	1	134.21

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	450.05	97.70	0.36	2.78	0.37	2.72	0		0	.
6	451.05	100.27	0.36	2.75	0.37	2.72	0		0	.
6	452.05	69.03	0.36	2.79	0.37	2.72	0		0	.
6	453.05	70.27	0.35	2.83	0.37	2.72	0		0	.
6	454.05	157.32	0.35	2.83	0.37	2.72	0		0	.
6	455.05	75.20	0.36	2.78	0.36	2.78	1	1	0	2.72
6	456.05	163.96	0.35	2.85	0.35	2.85	1	3	0	2.78
6	457.05	183.31	0.37	2.72	0.37	2.72	1	2	0	2.78
6	458.05	163.19	0.35	2.85	0.35	2.85	0		1	.
6	459.05	72.17	0.36	2.75	0.37	2.72	0		1	.
6	460.05	73.70	0.35	2.85	0.35	2.85	1	1	0	2.78
6	461.05	93.83	0.35	2.84	0.35	2.85	0		1	.
6	462.05	104.24	0.37	2.71	0.37	2.71	1	1	0	2.86
6	463.05	102.20	0.35	2.86	0.35	2.86	1	0	0	2.85
6	465.05	77.54	0.37	2.69	0.37	2.71	0		1	.
6	466.05	294.86	0.39	2.56	0.39	2.56	1	2	0	2.71
6	467.05	427.73	0.36	2.76	0.36	2.76	1	1	0	2.71
6	468.05	424.43	0.36	2.75	0.36	2.75	1	3	0	2.71
6	469.05	93.42	0.38	2.66	0.36	2.76	0		1	.
6	470.05	95.02	0.39	2.58	0.36	2.76	0		0	.
6	471.05	184.62	0.38	2.66	0.36	2.76	0		0	.
6	472.05	183.35	0.39	2.57	0.36	2.76	0		0	.
6	473.05	326.92	0.36	2.74	0.37	2.69	0		0	.
6	474.05	97.26	0.39	2.56	0.36	2.76	0		0	.
6	475.05	529.16	0.39	2.57	0.36	2.76	0		0	.
6	476.05	145.65	0.37	2.72	0.37	2.69	0		0	.
6	477.05	100.33	0.38	2.61	0.36	2.76	0		0	.
6	478.05	137.17	0.37	2.69	0.36	2.76	0		0	.
6	479.05	336.53	0.36	2.77	0.37	2.69	0		0	.
6	480.05	460.03	0.36	2.78	0.37	2.69	0		0	.
6	481.05	134.24	0.37	2.69	0.37	2.69	1	0	0	2.76
6	482.05	154.89	0.37	2.68	0.37	2.69	0		0	.
6	483.05	109.27	0.37	2.71	0.37	2.69	0		1	.
6	484.05	106.97	0.37	2.73	0.37	2.69	0		0	.
6	485.05	108.17	0.37	2.70	0.37	2.69	0		0	.
6	486.05	101.80	0.36	2.74	0.37	2.69	0		0	.
6	487.05	111.47	0.37	2.73	0.37	2.69	0		0	.
6	488.05	114.24	0.37	2.68	0.37	2.69	0		0	.
6	489.05	115.18	0.37	2.68	0.37	2.69	0		0	.
6	490.05	141.31	0.37	2.72	0.37	2.72	1	3	0	2.69
6	491.05	151.72	0.38	2.62	0.38	2.62	1	2	0	2.69
6	492.05	149.82	0.37	2.71	0.37	2.71	1	1	0	2.69
6	493.05	171.01	0.38	2.67	0.37	2.71	0		1	.
6	494.05	169.54	0.37	2.69	0.37	2.71	0		0	.
6	495.05	175.61	0.37	2.68	0.37	2.68	1	1	0	2.71
6	496.05	178.61	0.37	2.71	0.37	2.68	0		0	.
6	497.05	180.88	0.37	2.74	0.37	2.68	0		1	.
6	498.05	82.68	0.30	3.38	0.30	3.38	1	3	0	1.71
6	499.05	244.17	0.37	2.72	0.37	2.68	0		0	.
6	500.05	252.18	0.37	2.73	0.37	2.68	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	501.05	0	.	1	0	1	501	0	1.29	2	113.80
6	502.05	1	.	1	0	1	502	0	0.86	2	175.01
6	503.05	1	.	1	0	1	503	0	1.29	1	144.41
6	504.05	1	0	1	0	1	502	0	1.29	1	154.61
6	505.05	1	.	1	0	3	505	0	0.64	2	134.21
6	506.05	1	0	1	0	2	502	0	1.50	1	154.61
6	507.05	0	1	0	0	1	502	0	1.71	2	154.61
6	508.05	0	1	0	0	1	505	0	0.64	1	134.21
6	509.05	1	.	1	0	3	509	0	0.86	0	62.80
6	510.05	1	0	1	0	1	509	0	0.86	2	62.80
6	511.05	0	.	1	0	3	511	0	0.43	2	124.01
6	512.05	1	.	0	0	.	512	0	0.43	2	62.80
6	514.05	0	.	0	0	.	514	0	0.43	2	175.01
6	143.06	1	.	1	0	2	143	0	0.64	2	22.00
6	144.06	1	.	1	0	2	144	0	0.43	2	22.00
6	145.06	0	.	1	0	3	145	0	0.64	2	22.00
6	148.06	1	.	1	0	2	148	0	0.43	2	11.80
6	171.06	1	.	1	0	2	171	0	0.64	2	22.00
6	173.06	0	.	0	0	2	173	0	0.64	2	11.80
6	174.06	1	1	1	0	1	180	0	0.64	2	22.00
6	175.06	1	0	1	0	2	180	0	0.64	0	22.00
6	176.06	1	.	1	0	1	176	0	0.64	2	22.00
6	177.06	1	.	0	0	2	177	0	0.64	0	22.00
6	178.06	0	.	0	0	2	178	0	0.64	2	42.40
6	179.06	1	.	1	0	.	179	0	0.43	2	22.00
6	180.06	0	.	1	0	2	180	0	0.64	0	22.00
6	186.06	1	.	1	0	1	186	0	0.86	2	22.00
6	187.06	1	.	1	0	3	187	0	0.43	2	42.40
6	189.06	1	.	1	0	1	189	0	1.07	2	22.00
6	196.06	1	.	1	0	1	196	0	1.07	0	11.80
6	197.06	1	.	1	0	1	197	0	1.07	1	11.80
6	199.06	1	.	1	0	1	199	0	1.29	0	11.80
6	200.06	1	.	1	0	1	200	0	1.50	2	11.80
6	211.06	1	.	0	0	1	211	0	1.71	1	22.00
6	212.06	0	1	1	0	1	211	0	1.07	2	22.00
6	213.06	0	.	0	0	1	213	0	1.50	2	22.00
6	214.06	0	0	0	0	1	211	0	1.29	2	22.00
6	219.06	0	.	0	0	1	219	0	1.07	1	1.60
6	220.06	0	.	0	0	1	220	0	0.86	0	1.60
6	222.06	0	0	1	0	1	219	0	1.29	2	1.60
6	223.06	0	0	0	0	1	211	0	1.07	1	22.00
6	231.06	0	.	0	0	1	231	1	1.07	1	22.00
6	232.06	0	.	0	1	1	232	1	1.50	2	22.00
6	233.06	1	1	1	0	2	232	1	1.29	2	22.00
6	234.06	0	1	0	0	1	232	1	1.07	2	22.00
6	237.06	0	0	1	0	1	232	1	1.07	2	22.00
6	238.06	1	.	1	0	2	238	1	1.29	1	22.00
6	239.06	0	0	1	0	1	240	0	1.07	2	22.00
6	240.06	1	.	1	0	2	240	0	1.07	1	1.60
6	241.06	0	.	0	0	1	241	0	1.29	2	22.00

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	501.05	409.05	0.39	2.59	0.39	2.59	1	2	0	2.68
6	502.05	203.53	0.36	2.75	0.36	2.75	1	1	0	2.68
6	503.05	233.50	0.34	2.97	0.34	2.97	1	3	0	2.68
6	504.05	351.62	0.37	2.73	0.36	2.75	0		1	.
6	505.05	377.94	0.59	1.68	0.59	1.68	1	0	0	3.20
6	506.05	350.59	0.36	2.76	0.36	2.75	0		0	.
6	507.05	354.03	0.36	2.78	0.36	2.75	0		0	.
6	508.05	377.57	0.58	1.71	0.59	1.68	0		1	.
6	509.05	560.73	0.58	1.71	0.58	1.71	1	0	0	1.68
6	510.05	563.10	0.58	1.74	0.58	1.71	0		1	.
6	511.05	250.01	0.31	3.20	0.31	3.20	1	0	0	2.75
6	512.05	748.35	0.48	2.09	0.48	2.09	1	0	0	2.97
6	514.05	429.03	0.34	2.97	0.34	2.97	1	0	0	1.71
6	143.06	37.39	0.98	1.02	0.98	1.02	1	1	0	.
6	144.06	38.28	0.99	1.01	0.99	1.01	1	1	0	1.02
6	145.06	40.68	0.94	1.06	0.94	1.06	1	0	0	1.01
6	148.06	63.19	0.90	1.12	0.90	1.12	1	1	0	1.06
6	171.06	48.95	0.74	1.36	0.74	1.36	1	1	0	1.40
6	173.06	79.27	0.77	1.30	0.77	1.30	1	1	0	1.36
6	174.06	55.19	0.78	1.27	0.78	1.29	0		1	.
6	175.06	61.63	0.79	1.27	0.78	1.29	0		0	.
6	176.06	62.50	0.80	1.25	0.80	1.25	1	1	0	1.29
6	177.06	63.67	0.82	1.23	0.82	1.23	1	0	0	1.25
6	178.06	64.80	0.77	1.31	0.77	1.31	1	4	0	1.23
6	179.06	47.82	0.72	1.40	0.72	1.40	1	0	0	1.12
6	180.06	53.52	0.78	1.29	0.78	1.29	1	1	0	1.30
6	186.06	65.57	0.74	1.34	0.74	1.34	1	1	0	1.31
6	187.06	68.81	0.74	1.35	0.74	1.35	1	0	0	1.34
6	189.06	68.97	0.72	1.40	0.72	1.40	1	1	0	1.35
6	196.06	100.73	0.59	1.68	0.59	1.68	1	2	0	1.40
6	197.06	99.96	0.56	1.77	0.56	1.77	1	3	0	1.40
6	199.06	103.36	0.57	1.75	0.57	1.75	1	4	0	1.40
6	200.06	104.20	0.54	1.85	0.54	1.85	1	4	0	1.75
6	211.06	70.78	0.53	1.89	0.53	1.89	1	4	0	1.85
6	212.06	72.98	0.52	1.94	0.53	1.89	0		1	.
6	213.06	75.91	0.54	1.85	0.54	1.85	1	2	0	1.89
6	214.06	77.65	0.54	1.87	0.53	1.89	0		0	.
6	219.06	112.74	0.53	1.89	0.53	1.89	1	1	0	1.89
6	220.06	109.04	0.50	2.00	0.50	2.00	1	3	0	1.89
6	222.06	113.94	0.53	1.88	0.53	1.89	0		1	.
6	223.06	73.51	0.53	1.90	0.53	1.89	0		0	.
6	231.06	78.85	0.51	1.97	0.51	1.97	1	3	0	1.89
6	232.06	80.75	0.52	1.91	0.52	1.91	1	2	0	1.89
6	233.06	82.49	0.52	1.92	0.52	1.91	0		1	.
6	234.06	83.22	0.52	1.92	0.52	1.91	0		0	.
6	237.06	86.89	0.52	1.92	0.52	1.91	0		0	.
6	238.06	84.59	0.48	2.07	0.48	2.07	1	4	0	1.89
6	239.06	93.30	0.50	2.00	0.48	2.08	0		0	.
6	240.06	123.92	0.48	2.08	0.48	2.08	1	1	0	2.07
6	241.06	98.40	0.51	1.96	0.51	1.96	1	3	0	2.08

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	242.06	0	0	0	0	1	241	0	0.86	1	22.00
6	243.06	0	0	1	0	1	240	0	1.29	1	42.40
6	244.06	1	.	1	0	1	244	1	1.50	2	22.00
6	245.06	0	.	0	0	1	245	1	1.50	1	22.00
6	246.06	0	0	0	0	1	245	1	1.93	1	42.40
6	247.06	0	1	0	0	1	240	0	1.07	2	22.00
6	248.06	0	0	0	0	2	245	1	1.71	0	42.40
6	249.06	1	1	1	0	1	245	1	1.71	1	42.40
6	250.06	0	1	1	0	1	244	1	1.29	2	22.00
6	251.06	0	.	0	0	1	251	0	1.50	2	22.00
6	252.06	0	0	0	0	2	251	0	1.29	1	42.40
6	253.06	1	.	1	0	1	253	1	1.50	2	42.40
6	254.06	1	.	1	0	1	254	1	1.50	2	42.40
6	255.06	0	0	0	0	2	254	1	1.71	2	42.40
6	256.06	0	0	0	0	1	254	1	1.93	0	22.00
6	257.06	0	1	0	0	2	254	1	1.93	2	42.40
6	258.06	1	.	1	0	1	258	1	1.71	1	22.00
6	259.06	1	0	1	0	1	258	1	1.71	1	22.00
6	260.06	1	0	1	0	1	258	1	1.71	1	22.00
6	261.06	0	1	1	0	1	258	1	1.93	1	42.40
6	263.06	0	0	1	0	2	258	1	1.93	1	22.00
6	264.06	1	.	0	0	2	264	0	0.86	2	42.40
6	265.06	1	0	1	0	1	264	0	1.07	1	42.40
6	266.06	1	0	1	0	1	264	0	1.29	2	42.40
6	267.06	0	1	1	0	1	264	0	1.29	2	22.00
6	268.06	1	1	1	0	1	264	0	1.07	2	22.00
6	270.06	1	.	1	0	1	270	0	1.50	2	42.40
6	272.06	1	.	1	0	2	272	0	1.29	1	42.40
6	273.06	1	.	0	0	1	273	0	1.29	0	22.00
6	274.06	0	1	1	0	1	273	0	1.50	0	22.00
6	275.06	1	.	1	0	3	275	0	1.07	2	42.40
6	276.06	1	0	1	0	1	275	0	1.07	1	42.40
6	277.06	1	0	1	0	1	275	0	1.29	2	93.40
6	278.06	1	0	1	0	1	275	0	1.29	1	11.80
6	279.06	1	0	1	0	1	275	0	1.29	2	42.40
6	280.06	0	1	0	0	1	275	0	1.07	1	11.80
6	281.06	1	1	1	0	1	275	0	1.29	2	42.40
6	282.06	1	.	1	0	1	282	0	1.29	2	42.40
6	283.06	0	1	1	0	1	275	0	1.50	1	22.00
6	284.06	1	0	1	0	1	282	0	1.29	1	124.01
6	285.06	1	.	1	1	3	285	0	0.64	1	73.00
6	287.06	1	.	0	0	2	287	0	0.86	1	73.00
6	288.06	1	.	1	0	1	288	0	0.86	0	73.00
6	289.06	1	.	1	0	3	289	0	0.86	1	62.80
6	292.06	1	.	1	0	1	292	0	1.50	2	62.80
6	293.06	1	0	1	0	1	292	0	1.50	1	22.00
6	294.06	1	.	1	0	1	294	0	1.07	2	62.80
6	295.06	0	.	1	0	.	295	0	0.86	2	22.00
6	296.06	0	.	1	0	1	296	0	1.29	2	93.40
6	297.06	0	.	0	0	2	297	0	1.50	2	62.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	242.06	97.27	0.53	1.89	0.51	1.96	0		1	.
6	243.06	90.43	0.50	1.99	0.48	2.08	0		0	.
6	244.06	95.10	0.53	1.88	0.53	1.88	1	2	0	2.08
6	245.06	101.74	0.52	1.92	0.52	1.92	1	3	0	2.08
6	246.06	98.40	0.52	1.93	0.52	1.92	0		1	.
6	247.06	91.80	0.50	2.01	0.48	2.08	0		1	.
6	248.06	105.08	0.51	1.97	0.52	1.92	0		0	.
6	249.06	106.34	0.51	1.96	0.52	1.92	0		0	.
6	250.06	105.98	0.55	1.82	0.53	1.88	0		1	.
6	251.06	108.28	0.55	1.83	0.55	1.83	1	1	0	2.08
6	252.06	112.38	0.54	1.84	0.55	1.83	0		0	.
6	253.06	113.78	0.54	1.87	0.54	1.87	1	3	0	1.83
6	254.06	116.25	0.57	1.76	0.57	1.76	1	2	0	1.83
6	255.06	121.79	0.62	1.62	0.57	1.76	0		0	.
6	256.06	120.69	0.66	1.51	0.57	1.76	0		0	.
6	257.06	119.86	0.60	1.65	0.57	1.76	0		1	.
6	258.06	111.08	0.54	1.86	0.54	1.86	1	3	0	1.83
6	259.06	112.95	0.53	1.88	0.54	1.86	0		0	.
6	260.06	99.74	0.53	1.89	0.54	1.86	0		1	.
6	261.06	118.46	0.56	1.78	0.54	1.86	0		0	.
6	263.06	119.29	0.55	1.81	0.54	1.86	0		0	.
6	264.06	125.33	0.58	1.71	0.58	1.71	1	1	0	1.83
6	265.06	123.63	0.61	1.65	0.58	1.71	0		1	.
6	266.06	126.73	0.59	1.70	0.58	1.71	0		0	.
6	267.06	128.87	0.58	1.71	0.58	1.71	0		0	.
6	268.06	127.70	0.60	1.67	0.58	1.71	0		0	.
6	270.06	132.70	0.62	1.62	0.62	1.62	1	2	0	1.71
6	272.06	131.37	0.56	1.79	0.56	1.79	1	3	0	1.71
6	273.06	130.67	0.62	1.62	0.62	1.62	1	1	0	1.71
6	274.06	133.34	0.60	1.67	0.62	1.62	0		1	.
6	275.06	135.61	0.60	1.67	0.60	1.67	1	0	0	1.62
6	276.06	137.27	0.63	1.59	0.60	1.67	0		1	.
6	277.06	55.73	0.62	1.62	0.60	1.67	0		0	.
6	278.06	177.64	0.64	1.56	0.60	1.67	0		0	.
6	279.06	140.41	0.64	1.56	0.60	1.67	0		0	.
6	280.06	180.74	0.66	1.50	0.60	1.67	0		0	.
6	281.06	139.28	0.64	1.56	0.60	1.67	0		0	.
6	282.06	142.01	0.72	1.40	0.72	1.40	1	1	0	1.67
6	283.06	134.87	0.65	1.53	0.60	1.67	0		0	.
6	284.06	44.25	0.73	1.37	0.72	1.40	0		0	.
6	285.06	86.55	0.67	1.50	0.67	1.50	1	0	0	1.40
6	287.06	91.15	0.65	1.53	0.65	1.53	1	0	0	1.50
6	288.06	88.85	0.63	1.58	0.63	1.58	1	1	0	1.53
6	289.06	86.12	0.59	1.71	0.59	1.71	1	3	0	1.58
6	292.06	89.26	0.61	1.65	0.61	1.65	1	4	0	1.64
6	293.06	167.57	0.62	1.60	0.61	1.65	0		1	.
6	294.06	83.71	0.66	1.52	0.66	1.52	1	2	0	1.58
6	295.06	139.78	0.51	1.94	0.51	1.94	1	3	0	1.53
6	296.06	61.50	0.60	1.67	0.60	1.67	1	0	0	1.65
6	297.06	87.35	0.61	1.64	0.61	1.64	1	1	0	1.58

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	298.06	1	0	1	0	1	296	0	1.50	2	83.20
6	300.06	1	1	1	0	1	296	0	1.29	2	62.80
6	301.06	1	0	0	0	2	296	0	1.29	2	42.40
6	302.06	1	0	1	0	1	296	0	1.29	2	42.40
6	303.06	1	.	0	0	1	303	0	1.29	2	62.80
6	304.06	1	0	1	0	2	296	0	1.29	2	42.40
6	305.06	1	.	0	0	1	305	0	1.07	1	62.80
6	306.06	0	.	0	0	3	306	0	0.86	2	42.40
6	307.06	0	.	0	0	1	307	0	1.29	2	62.80
6	308.06	1	0	0	0	1	305	0	1.50	1	62.80
6	309.06	0	.	1	0	1	309	0	1.29	2	42.40
6	310.06	1	0	1	0	2	316	1	1.07	2	42.40
6	312.06	1	0	1	0	1	296	0	1.29	1	1.60
6	313.06	1	1	1	0	1	296	0	1.29	1	22.00
6	314.06	0	1	0	0	1	296	0	1.71	1	22.00
6	315.06	1	.	1	0	1	315	0	1.07	2	62.80
6	316.06	0	.	1	0	1	316	1	1.07	2	124.01
6	317.06	1	1	1	0	2	316	1	1.07	2	42.40
6	318.06	1	.	1	0	.	318	1	1.29	1	22.00
6	319.06	1	0	1	0	1	318	1	1.50	1	22.00
6	320.06	1	0	1	0	1	318	1	1.50	1	22.00
6	321.06	1	.	0	0	2	321	0	1.50	1	42.40
6	322.06	1	.	1	0	1	322	0	1.07	1	42.40
6	323.06	1	.	1	0	1	323	0	1.29	2	93.40
6	324.06	1	.	1	0	2	324	0	1.50	1	42.40
6	325.06	0	.	0	0	2	325	0	1.07	2	62.80
6	326.06	0	0	0	0	2	325	0	1.29	0	42.40
6	327.06	1	1	1	0	1	325	0	1.50	2	62.80
6	328.06	0	0	1	0	2	325	0	1.29	1	42.40
6	329.06	1	.	1	0	2	329	0	0.86	0	42.40
6	330.06	1	.	1	0	2	330	0	1.07	1	22.00
6	331.06	0	1	0	0	1	330	0	1.29	2	22.00
6	332.06	0	.	0	0	1	332	0	1.50	1	42.40
6	333.06	1	.	0	0	1	333	0	1.50	0	62.80
6	334.06	1	.	1	0	1	334	0	1.29	2	62.80
6	335.06	1	.	1	0	1	335	1	1.29	2	42.40
6	336.06	1	0	1	0	1	335	1	1.50	2	42.40
6	337.06	1	0	1	0	1	335	1	1.50	2	42.40
6	338.06	1	.	1	0	1	338	1	0.86	1	11.80
6	339.06	1	.	1	0	1	339	1	1.50	0	42.40
6	340.06	1	0	1	0	1	338	1	1.71	1	42.40
6	341.06	0	.	1	0	1	341	1	1.71	1	124.01
6	342.06	0	1	1	0	1	338	1	1.93	1	42.40
6	343.06	1	.	0	0	2	343	0	1.50	1	42.40
6	344.06	0	0	0	0	1	343	0	1.07	1	73.00
6	345.06	0	1	1	0	1	343	0	1.29	2	73.00
6	346.06	1	1	1	0	2	343	0	1.29	2	62.80
6	347.06	1	1	1	0	1	350	1	1.71	2	42.40
6	348.06	1	1	1	0	1	350	1	1.50	1	124.01
6	349.06	0	.	0	0	1	349	1	2.36	0	124.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	298.06	75.88	0.60	1.65	0.60	1.67	0		0	.
6	300.06	98.69	0.61	1.64	0.60	1.67	0		0	.
6	301.06	165.57	0.61	1.63	0.60	1.67	0		0	.
6	302.06	167.10	0.60	1.66	0.60	1.67	0		0	.
6	303.06	103.47	0.62	1.61	0.62	1.61	1	1	0	1.67
6	304.06	169.11	0.59	1.68	0.60	1.67	0		0	.
6	305.06	102.37	0.56	1.77	0.56	1.77	1	3	0	1.67
6	306.06	172.08	0.60	1.67	0.60	1.67	1	0	0	1.67
6	307.06	104.40	0.63	1.59	0.63	1.59	1	2	0	1.67
6	308.06	100.73	0.57	1.74	0.56	1.77	0		1	.
6	309.06	192.20	0.67	1.49	0.67	1.49	1	2	0	1.73
6	310.06	188.96	0.58	1.72	0.58	1.72	0		0	.
6	312.06	218.21	0.59	1.68	0.60	1.67	0		0	.
6	313.06	170.21	0.61	1.65	0.60	1.67	0		1	.
6	314.06	171.68	0.61	1.64	0.60	1.67	0		0	.
6	315.06	106.37	0.58	1.73	0.58	1.73	1	0	1	1.61
6	316.06	45.88	0.62	1.61	0.62	1.61	1	2	0	1.73
6	317.06	186.22	0.65	1.54	0.62	1.61	0		1	.
6	318.06	183.42	0.48	2.08	0.48	2.08	1	3	0	1.73
6	319.06	185.36	0.52	1.92	0.48	2.08	0		1	.
6	320.06	185.39	0.50	2.01	0.48	2.08	0		0	.
6	321.06	190.26	0.58	1.73	0.58	1.73	1	2	0	1.80
6	322.06	185.62	0.55	1.83	0.55	1.83	1	3	0	1.73
6	323.06	87.06	0.54	1.86	0.54	1.86	1	3	0	1.80
6	324.06	190.72	0.55	1.80	0.55	1.80	1	1	0	1.73
6	325.06	108.49	0.56	1.78	0.56	1.78	1	1	0	1.80
6	326.06	194.83	0.56	1.78	0.56	1.78	0		1	.
6	327.06	110.07	0.58	1.72	0.56	1.78	0		0	.
6	328.06	196.57	0.56	1.79	0.56	1.78	0		0	.
6	329.06	202.77	0.58	1.71	0.58	1.71	1	1	0	1.78
6	330.06	198.04	0.57	1.75	0.57	1.75	1	0	0	1.71
6	331.06	201.71	0.57	1.75	0.57	1.75	0		1	.
6	332.06	198.30	0.61	1.64	0.61	1.64	1	2	0	1.75
6	333.06	113.21	0.59	1.70	0.59	1.70	1	1	0	1.75
6	334.06	112.04	0.57	1.75	0.57	1.75	1	3	0	1.75
6	335.06	214.89	0.63	1.59	0.63	1.59	1	2	0	1.70
6	336.06	217.09	0.64	1.56	0.63	1.59	0		1	.
6	337.06	219.29	0.64	1.56	0.63	1.59	0		0	.
6	338.06	185.61	0.57	1.75	0.57	1.75	1	3	0	1.70
6	339.06	207.81	0.59	1.68	0.59	1.68	1	2	0	1.70
6	340.06	203.14	0.56	1.80	0.57	1.75	0		1	.
6	341.06	51.95	0.64	1.56	0.64	1.56	1	1	0	1.82
6	342.06	205.34	0.57	1.77	0.57	1.75	0		0	.
6	343.06	211.08	0.60	1.66	0.60	1.66	1	1	0	1.70
6	344.06	114.71	0.60	1.67	0.60	1.66	0		0	.
6	345.06	114.94	0.60	1.68	0.60	1.66	0		1	.
6	346.06	117.78	0.60	1.68	0.60	1.66	0		0	.
6	347.06	231.57	0.61	1.65	0.56	1.78	0		1	.
6	348.06	56.39	0.68	1.48	0.56	1.78	0		0	.
6	349.06	54.46	0.54	1.87	0.54	1.87	1	3	0	1.82

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	350.06	0	.	0	0	1	350	1	1.71	2	73.00
6	351.06	0	0	1	0	1	341	1	1.07	1	42.40
6	352.06	0	1	1	1	1	350	1	1.50	2	62.80
6	353.06	1	.	1	0	1	353	1	1.50	2	42.40
6	354.06	1	.	1	0	1	354	0	2.36	2	124.01
6	355.06	1	.	1	0	1	355	0	0.64	0	42.40
6	356.06	1	0	1	0	1	353	1	1.29	2	42.40
6	357.06	1	.	0	0	2	357	0	0.86	1	42.40
6	358.06	1	.	1	0	1	358	0	1.50	2	11.80
6	359.06	1	.	0	0	1	359	1	1.29	1	42.40
6	360.06	1	.	1	0	1	360	0	1.50	2	42.40
6	361.06	1	0	1	0	1	359	1	1.50	1	42.40
6	362.06	1	.	1	0	1	362	0	1.29	2	42.40
6	363.06	0	1	0	0	1	359	1	1.71	1	42.40
6	364.06	0	.	0	0	1	364	0	1.29	2	11.80
6	365.06	0	.	1	0	1	365	0	2.14	1	22.00
6	366.06	1	.	1	0	1	366	0	2.36	0	42.40
6	367.06	0	.	0	0	1	367	0	1.93	2	83.20
6	368.06	0	.	0	0	1	368	0	1.29	2	83.20
6	369.06	1	.	1	0	1	369	0	1.71	1	42.40
6	370.06	0	.	1	0	1	370	0	1.71	0	22.00
6	371.06	0	1	0	0	1	354	0	2.14	1	42.40
6	372.06	1	0	1	0	1	373	0	2.36	0	124.01
6	373.06	1	.	0	0	1	373	0	2.14	2	124.01
6	374.06	1	1	1	0	1	375	1	2.36	2	124.01
6	375.06	0	.	1	0	1	375	1	1.93	2	124.01
6	376.06	1	0	0	0	1	375	1	2.57	2	124.01
6	377.06	1	0	0	0	1	375	1	2.79	2	124.01
6	378.06	1	.	1	0	1	378	1	2.36	1	83.20
6	379.06	0	1	1	0	1	378	1	2.14	1	93.40
6	380.06	0	.	1	0	2	380	1	1.71	1	11.80
6	381.06	0	1	1	0	1	375	1	2.14	2	124.01
6	382.06	1	1	1	0	1	375	1	2.36	2	124.01
6	383.06	1	1	1	0	1	378	1	1.71	1	42.40
6	384.06	1	0	1	0	1	378	1	2.57	0	42.40
6	386.06	1	0	1	0	1	378	1	2.36	1	42.40
6	387.06	1	0	1	0	1	378	1	2.36	1	42.40
6	388.06	1	1	1	0	1	378	1	2.36	1	103.60
6	389.06	0	0	1	0	1	378	1	2.57	1	144.41
6	390.06	0	0	1	0	1	378	1	2.36	1	42.40
6	391.06	1	1	1	0	1	378	1	2.14	1	103.60
6	392.06	1	.	0	0	1	392	0	0.86	1	42.40
6	393.06	0	0	0	0	1	375	1	1.93	2	103.60
6	394.06	0	1	0	0	1	375	1	1.93	2	103.60
6	395.06	0	1	0	0	1	378	1	2.57	1	22.00
6	396.06	0	1	1	0	2	378	1	2.36	1	124.01
6	397.06	0	0	0	0	1	375	1	2.14	2	93.40
6	398.06	0	.	1	0	1	398	0	2.36	1	42.40
6	399.06	1	1	1	0	1	398	0	1.71	2	73.00
6	400.06	1	.	1	0	1	400	0	1.50	2	73.00

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	350.06	119.68	0.56	1.78	0.56	1.78	1	2	0	1.82
6	351.06	238.08	0.66	1.51	0.64	1.56	0		1	.
6	352.06	124.62	0.60	1.65	0.56	1.78	0		0	.
6	353.06	228.77	0.57	1.74	0.57	1.74	1	3	0	1.56
6	354.06	55.02	0.43	2.33	0.43	2.33	1	1	0	2.15
6	355.06	237.64	0.62	1.61	0.62	1.61	1	1	0	1.56
6	356.06	240.58	0.58	1.73	0.57	1.74	0		1	.
6	357.06	213.48	0.55	1.82	0.55	1.82	1	0	0	1.66
6	358.06	317.78	0.65	1.54	0.65	1.54	1	2	0	1.43
6	359.06	215.92	0.55	1.83	0.55	1.83	1	3	0	1.82
6	360.06	230.10	0.68	1.48	0.68	1.48	1	1	0	1.61
6	361.06	216.59	0.54	1.84	0.55	1.83	0		1	.
6	362.06	237.71	0.70	1.43	0.70	1.43	1	1	0	1.48
6	363.06	221.89	0.54	1.85	0.55	1.83	0		0	.
6	364.06	316.31	0.57	1.75	0.57	1.75	1	0	0	1.43
6	365.06	88.39	0.43	2.33	0.43	2.33	1	2	0	2.15
6	366.06	253.06	0.39	2.55	0.39	2.55	1	3	0	2.33
6	367.06	94.90	0.41	2.45	0.41	2.45	1	3	0	2.15
6	368.06	89.39	0.47	2.15	0.47	2.15	1	0	0	1.75
6	369.06	231.80	0.41	2.43	0.41	2.43	1	3	0	2.15
6	370.06	90.13	0.44	2.28	0.44	2.28	1	2	0	2.15
6	371.06	241.28	0.42	2.36	0.43	2.33	0		1	.
6	372.06	51.35	0.42	2.36	0.43	2.34	0		1	.
6	373.06	50.85	0.43	2.34	0.43	2.34	1	1	0	2.33
6	374.06	53.62	0.43	2.32	0.43	2.35	0		1	.
6	375.06	49.18	0.43	2.35	0.43	2.35	1	2	0	2.34
6	376.06	57.79	0.43	2.30	0.43	2.35	0		0	.
6	377.06	57.39	0.44	2.26	0.43	2.35	0		0	.
6	378.06	93.06	0.37	2.69	0.37	2.69	1	3	0	2.34
6	379.06	94.70	0.38	2.65	0.37	2.69	0		1	.
6	380.06	201.53	0.31	3.27	0.31	3.27	1	3	0	2.34
6	381.06	60.20	0.41	2.41	0.43	2.35	0		0	.
6	382.06	59.33	0.41	2.44	0.43	2.35	0		0	.
6	383.06	248.19	0.38	2.66	0.37	2.69	0		0	.
6	384.06	250.85	0.38	2.66	0.37	2.69	0		0	.
6	386.06	276.01	0.39	2.57	0.37	2.69	0		0	.
6	387.06	273.18	0.39	2.56	0.37	2.69	0		0	.
6	388.06	81.08	0.39	2.57	0.37	2.69	0		0	.
6	389.06	30.19	0.38	2.67	0.37	2.69	0		0	.
6	390.06	282.69	0.39	2.56	0.37	2.69	0		0	.
6	391.06	84.72	0.39	2.56	0.37	2.69	0		0	.
6	392.06	224.86	0.43	2.34	0.43	2.34	1	3	0	1.43
6	393.06	86.75	0.40	2.52	0.43	2.35	0		0	.
6	394.06	83.01	0.41	2.42	0.43	2.35	0		0	.
6	395.06	256.46	0.38	2.64	0.37	2.69	0		0	.
6	396.06	66.80	0.39	2.56	0.37	2.69	0		0	.
6	397.06	125.06	0.40	2.49	0.43	2.35	0		0	.
6	398.06	287.59	0.39	2.56	0.39	2.56	1	1	0	2.34
6	399.06	156.52	0.39	2.56	0.39	2.56	0		1	.
6	400.06	158.59	0.39	2.59	0.39	2.59	1	3	0	2.56

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	401.06	0	1	0	0	1	404	0	1.71	2	73.00
6	402.06	0	0	1	0	1	404	0	1.07	2	73.00
6	403.06	0	0	1	0	1	404	0	1.50	2	93.40
6	404.06	1	.	1	0	1	404	0	1.71	1	42.40
6	405.06	1	.	1	0	1	405	0	1.29	1	42.40
6	406.06	0	0	1	0	1	404	0	1.29	1	124.01
6	407.06	1	0	1	0	1	404	0	1.71	1	124.01
6	408.06	1	0	1	0	1	404	0	1.50	2	113.80
6	409.06	1	1	1	0	1	404	0	1.29	1	124.01
6	410.06	1	.	1	0	1	410	1	1.71	2	113.80
6	411.06	0	.	1	0	1	411	1	1.50	1	113.80
6	412.06	1	0	1	0	1	410	1	1.50	2	83.20
6	413.06	1	0	1	0	1	410	1	1.93	2	83.20
6	414.06	1	0	1	0	1	410	1	2.36	2	83.20
6	415.06	1	0	1	0	1	410	1	1.93	2	154.61
6	416.06	1	1	1	0	2	411	1	1.50	1	42.40
6	417.06	0	1	1	0	1	411	1	1.50	1	124.01
6	418.06	0	0	1	0	1	411	1	1.71	1	124.01
6	419.06	0	0	0	0	1	411	1	1.29	1	124.01
6	420.06	0	0	1	0	2	411	1	1.93	1	124.01
6	421.06	1	0	0	0	1	423	0	1.93	2	83.20
6	422.06	1	0	1	0	1	423	0	1.50	1	113.80
6	423.06	1	.	1	0	1	423	0	1.93	1	83.20
6	424.06	1	.	1	0	1	424	0	1.93	0	113.80
6	425.06	0	1	1	0	2	423	0	1.71	1	113.80
6	426.06	1	.	0	0	3	426	0	0.86	1	11.80
6	427.06	1	0	1	0	1	426	0	1.29	1	11.80
6	428.06	1	.	1	0	1	428	1	1.29	2	113.80
6	429.06	0	.	1	0	1	429	1	1.93	2	124.01
6	431.06	0	.	0	0	1	431	1	1.71	1	22.00
6	432.06	0	.	1	0	1	432	1	1.29	0	103.60
6	433.06	1	.	1	0	1	433	1	1.50	0	103.60
6	434.06	1	.	1	1	1	434	1	1.71	0	124.01
6	435.06	1	.	1	0	1	435	1	1.71	1	103.60
6	436.06	1	.	1	0	1	436	0	1.71	2	113.80
6	437.06	0	.	0	0	1	437	1	1.29	0	113.80
6	438.06	1	1	1	1	1	440	0	0.86	2	113.80
6	439.06	1	.	1	0	3	439	1	1.50	1	113.80
6	440.06	0	.	1	0	.	440	0	0.43	2	124.01
6	441.06	0	.	1	0	2	441	0	0.86	0	124.01
6	442.06	1	1	1	0	1	441	0	1.07	0	124.01
6	443.06	0	.	1	0	3	443	0	0.86	2	124.01
6	445.06	0	0	1	0	2	443	0	0.64	2	124.01
6	446.06	1	1	1	0	2	443	0	0.86	1	113.80
6	447.06	0	1	0	0	1	443	0	1.29	2	113.80
6	448.06	0	0	1	0	2	443	0	1.50	1	103.60
6	449.06	0	0	0	0	1	443	0	1.93	2	103.60
6	450.06	1	1	1	0	1	443	0	1.93	1	124.01
6	451.06	0	1	1	0	1	443	0	2.14	2	124.01
6	452.06	1	1	1	0	1	443	0	1.71	1	144.41

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	401.06	160.32	0.39	2.58	0.39	2.55	0		1	.
6	402.06	161.96	0.39	2.60	0.39	2.55	0		0	.
6	403.06	128.60	0.38	2.60	0.39	2.55	0		0	.
6	404.06	305.98	0.39	2.55	0.39	2.55	1	1	0	2.56
6	405.06	304.21	0.40	2.52	0.40	2.52	1	2	0	2.56
6	406.06	72.11	0.39	2.58	0.39	2.55	0		0	.
6	407.06	69.80	0.40	2.52	0.39	2.55	0		0	.
6	408.06	104.13	0.39	2.59	0.39	2.55	0		0	.
6	409.06	70.44	0.39	2.56	0.39	2.55	0		0	.
6	410.06	107.87	0.39	2.54	0.39	2.54	1	2	0	2.55
6	411.06	110.87	0.39	2.56	0.39	2.56	1	3	0	2.55
6	412.06	145.48	0.40	2.48	0.39	2.54	0		1	.
6	413.06	148.35	0.40	2.51	0.39	2.54	0		0	.
6	414.06	148.75	0.41	2.46	0.39	2.54	0		0	.
6	415.06	67.46	0.41	2.46	0.39	2.54	0		0	.
6	416.06	321.39	0.40	2.53	0.39	2.56	0		1	.
6	417.06	77.45	0.40	2.53	0.39	2.56	0		0	.
6	418.06	73.64	0.39	2.54	0.39	2.56	0		0	.
6	419.06	74.91	0.40	2.53	0.39	2.56	0		0	.
6	420.06	79.21	0.39	2.56	0.39	2.56	0		0	.
6	421.06	169.64	0.39	2.55	0.39	2.56	0		1	.
6	422.06	131.23	0.39	2.59	0.39	2.56	0		0	.
6	423.06	168.32	0.39	2.56	0.39	2.56	1	1	0	2.55
6	424.06	144.78	0.40	2.50	0.40	2.50	1	2	0	2.56
6	425.06	140.90	0.38	2.64	0.39	2.56	0		0	.
6	426.06	310.84	0.36	2.77	0.36	2.77	1	3	0	2.15
6	427.06	312.77	0.36	2.77	0.36	2.77	0		0	.
6	428.06	140.14	0.44	2.27	0.44	2.27	1	2	0	2.56
6	429.06	84.32	0.44	2.29	0.44	2.29	1	2	0	2.56
6	431.06	353.86	0.37	2.70	0.37	2.70	1	3	0	2.56
6	432.06	132.13	0.42	2.37	0.42	2.37	1	2	0	2.56
6	433.06	129.16	0.39	2.55	0.39	2.55	1	3	0	2.56
6	434.06	80.98	0.37	2.68	0.37	2.68	1	3	0	2.56
6	435.06	147.34	0.37	2.70	0.37	2.70	1	1	0	2.56
6	436.06	123.82	0.37	2.70	0.37	2.70	1	3	0	2.56
6	437.06	142.87	0.42	2.38	0.42	2.38	1	2	0	2.56
6	438.06	126.46	0.38	2.62	0.38	2.64	0		1	.
6	439.06	121.62	0.37	2.72	0.37	2.72	1	3	0	2.56
6	440.06	66.27	0.38	2.64	0.38	2.64	1	0	0	2.70
6	441.06	90.66	0.38	2.66	0.38	2.66	1	0	0	2.64
6	442.06	95.70	0.38	2.66	0.38	2.66	0		1	.
6	443.06	88.36	0.37	2.71	0.37	2.71	1	0	0	2.66
6	445.06	93.33	0.37	2.74	0.37	2.71	0		1	.
6	446.06	127.99	0.37	2.69	0.37	2.71	0		0	.
6	447.06	129.19	0.37	2.69	0.37	2.71	0		0	.
6	448.06	152.22	0.37	2.69	0.37	2.71	0		0	.
6	449.06	150.51	0.37	2.70	0.37	2.71	0		0	.
6	450.06	97.70	0.37	2.70	0.37	2.71	0		0	.
6	451.06	100.27	0.37	2.72	0.37	2.71	0		0	.
6	452.06	69.03	0.38	2.66	0.37	2.71	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	453.06	1	0	1	0	1	443	0	1.93	1	144.41
6	454.06	0	1	1	0	1	443	0	1.50	2	113.80
6	455.06	1	.	1	0	1	455	0	1.29	2	144.41
6	456.06	0	.	1	0	1	456	0	1.29	1	103.60
6	457.06	0	.	1	0	1	457	0	1.50	2	113.80
6	458.06	1	.	1	0	1	458	0	1.29	0	113.80
6	459.06	1	.	1	0	2	459	0	1.29	2	144.41
6	460.06	1	.	0	0	1	460	0	1.29	0	144.41
6	461.06	0	.	1	0	2	461	0	1.07	1	124.01
6	462.06	0	.	1	0	3	462	0	1.50	0	124.01
6	463.06	1	.	1	1	3	463	0	1.50	2	124.01
6	464.06	1	.	0	0	1	464	0	1.50	2	124.01
6	465.06	0	.	0	1	1	465	1	1.07	2	144.41
6	466.06	0	0	1	0	1	465	1	1.07	2	73.00
6	467.06	0	1	0	0	1	468	1	1.29	1	42.40
6	468.06	1	.	1	0	2	468	1	0.86	1	42.40
6	469.06	1	.	1	0	2	469	0	0.86	2	154.61
6	470.06	1	0	1	0	1	469	0	1.07	2	154.61
6	471.06	1	.	1	0	1	471	0	1.50	1	113.80
6	472.06	0	1	0	0	1	469	0	1.07	1	113.80
6	473.06	1	.	1	0	2	473	1	1.71	1	73.00
6	474.06	1	0	1	0	2	469	0	1.29	2	154.61
6	476.06	1	.	1	0	1	476	1	1.93	2	124.01
6	477.06	1	.	1	0	1	477	0	1.29	2	154.61
6	478.06	1	.	1	0	1	478	0	1.29	2	124.01
6	479.06	0	1	0	0	1	473	1	1.71	1	73.00
6	480.06	0	1	1	0	1	488	0	1.71	1	22.00
6	481.06	1	.	1	0	2	481	0	0.86	2	124.01
6	482.06	1	1	1	0	2	488	0	1.07	2	134.21
6	483.06	1	.	1	0	1	483	0	1.29	0	154.61
6	484.06	1	0	1	0	2	483	0	1.07	1	154.61
6	485.06	1	0	1	0	1	483	0	1.50	2	154.61
6	486.06	1	0	1	0	1	483	0	1.50	1	154.61
6	487.06	1	0	1	0	1	476	1	1.71	2	154.61
6	488.06	1	.	1	0	1	488	0	1.71	2	154.61
6	489.06	0	0	1	0	1	488	0	1.29	2	154.61
6	490.06	1	.	1	0	2	490	0	1.07	1	124.01
6	491.06	0	.	1	0	1	491	0	1.29	1	124.01
6	492.06	1	.	1	0	1	492	0	1.07	1	124.01
6	493.06	1	1	1	0	1	494	0	1.50	1	124.01
6	494.06	0	.	0	0	1	494	0	1.71	2	124.01
6	495.06	1	0	1	0	1	494	0	1.29	1	124.01
6	496.06	1	1	1	0	1	494	0	1.29	1	124.01
6	497.06	0	1	1	0	1	494	0	1.50	2	124.01
6	498.06	0	.	1	0	.	498	0	0.43	1	124.01
6	499.06	1	0	1	1	1	494	0	1.29	2	113.80
6	500.06	1	0	1	0	1	494	0	1.71	1	113.80
6	501.06	0	1	1	0	2	503	0	0.86	2	93.40
6	502.06	1	.	1	0	3	502	0	0.43	2	154.61
6	503.06	1	.	1	0	3	503	0	1.29	1	124.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	453.06	70.27	0.38	2.67	0.37	2.71	0		0	.
6	454.06	157.32	0.38	2.66	0.37	2.71	0		0	.
6	455.06	75.20	0.46	2.18	0.46	2.18	1	2	0	2.71
6	456.06	163.96	0.37	2.74	0.37	2.74	1	3	0	2.71
6	457.06	183.31	0.52	1.91	0.52	1.91	1	2	0	2.71
6	458.06	163.19	0.38	2.65	0.38	2.65	1	3	0	2.71
6	459.06	72.17	0.62	1.61	0.62	1.61	1	1	0	2.71
6	460.06	73.70	0.52	1.92	0.52	1.92	1	3	0	1.61
6	461.06	93.83	0.35	2.86	0.35	2.86	1	3	0	1.61
6	462.06	104.24	0.56	1.78	0.56	1.78	1	0	0	1.61
6	463.06	102.20	0.59	1.70	0.59	1.70	1	2	0	1.61
6	464.06	102.20	0.58	1.73	0.58	1.73	1	3	0	1.61
6	465.06	77.54	0.55	1.81	0.55	1.81	1	2	0	1.78
6	466.06	294.86	0.55	1.83	0.55	1.81	0		1	.
6	467.06	427.73	0.53	1.90	0.51	1.95	0		1	.
6	468.06	424.43	0.51	1.95	0.51	1.95	1	3	0	1.78
6	469.06	93.42	0.54	1.86	0.54	1.86	1	1	0	1.78
6	470.06	95.02	0.51	1.98	0.54	1.86	0		1	.
6	471.06	184.62	0.51	1.95	0.51	1.95	1	2	0	2.11
6	472.06	183.35	0.49	2.04	0.54	1.86	0		0	.
6	473.06	326.92	0.46	2.17	0.46	2.17	1	3	0	2.09
6	474.06	97.26	0.50	1.99	0.54	1.86	0		0	.
6	476.06	145.65	0.50	2.01	0.50	2.01	1	2	0	2.09
6	477.06	100.33	0.47	2.11	0.47	2.11	1	4	0	1.86
6	478.06	137.17	0.47	2.11	0.47	2.11	1	3	0	2.11
6	479.06	336.53	0.47	2.11	0.46	2.17	0		1	.
6	480.06	460.03	0.49	2.03	0.48	2.08	0		1	.
6	481.06	134.24	0.48	2.07	0.48	2.07	1	0	0	2.11
6	482.06	154.89	0.48	2.10	0.48	2.08	0		0	.
6	483.06	109.27	0.48	2.09	0.48	2.09	1	1	0	2.07
6	484.06	106.97	0.45	2.21	0.48	2.09	0		1	.
6	485.06	108.17	0.48	2.10	0.48	2.09	0		0	.
6	486.06	101.80	0.46	2.17	0.48	2.09	0		0	.
6	487.06	111.47	0.49	2.02	0.50	2.01	0		1	.
6	488.06	114.24	0.48	2.08	0.48	2.08	1	1	0	2.09
6	489.06	115.18	0.48	2.09	0.48	2.08	0		0	.
6	490.06	141.31	0.47	2.14	0.47	2.14	1	0	0	2.08
6	491.06	151.72	0.49	2.04	0.49	2.04	1	2	0	2.14
6	492.06	149.82	0.46	2.15	0.46	2.15	1	3	0	2.14
6	493.06	171.01	0.48	2.10	0.47	2.13	0		1	.
6	494.06	169.54	0.47	2.13	0.47	2.13	1	1	0	2.14
6	495.06	175.61	0.47	2.13	0.47	2.13	0		0	.
6	496.06	178.61	0.47	2.11	0.47	2.13	0		0	.
6	497.06	180.88	0.47	2.12	0.47	2.13	0		0	.
6	498.06	82.68	0.47	2.15	0.47	2.15	1	0	0	1.72
6	499.06	244.17	0.47	2.11	0.47	2.13	0		0	.
6	500.06	252.18	0.46	2.15	0.47	2.13	0		0	.
6	501.06	409.05	0.48	2.09	0.47	2.12	0		1	.
6	502.06	203.53	0.52	1.92	0.52	1.92	1	0	0	2.12
6	503.06	233.50	0.47	2.12	0.47	2.12	1	0	0	2.13

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	504.06	1	.	1	0	1	504	0	0.86	1	134.21
6	505.06	1	.	1	0	.	505	0	0.86	2	113.80
6	506.06	1	.	1	0	2	506	0	1.07	1	134.21
6	507.06	0	1	0	0	1	506	0	1.29	2	134.21
6	508.06	0	1	0	0	1	505	0	0.43	1	113.80
6	509.06	1	.	1	0	2	509	0	0.86	1	42.40
6	510.06	1	0	1	0	1	509	0	0.86	2	42.40
6	511.06	0	.	1	0	3	511	0	0.43	2	103.60
6	512.06	1	.	0	0	.	512	0	0.43	2	42.40
6	514.06	0	.	0	0	.	514	0	0.43	2	154.61
6	143.07	1	.	1	0	.	143	0	0.43	2	1.60
6	144.07	1	.	1	0	3	144	0	0.64	0	1.60
6	145.07	0	.	1	0	3	145	0	0.43	2	1.60
6	171.07	1	.	1	0	2	171	0	0.64	2	1.60
6	174.07	1	1	1	0	2	180	0	0.64	2	1.60
6	175.07	1	.	1	0	2	175	0	0.43	0	1.60
6	176.07	1	.	1	0	2	176	0	0.64	0	1.60
6	177.07	1	.	0	0	2	177	0	0.64	1	1.60
6	178.07	0	1	0	0	1	177	0	0.64	0	22.00
6	179.07	1	.	1	0	.	179	0	0.43	0	1.60
6	180.07	0	.	1	0	3	180	0	0.43	0	1.60
6	186.07	1	.	1	0	2	186	0	0.86	2	1.60
6	187.07	1	.	1	0	1	187	0	0.64	2	22.00
6	189.07	1	.	1	0	2	189	0	1.07	2	1.60
6	211.07	1	.	0	0	1	211	0	1.29	0	1.60
6	212.07	0	1	1	0	1	211	0	0.86	0	1.60
6	213.07	0	.	0	0	1	213	0	1.29	1	1.60
6	214.07	0	.	0	0	1	214	0	1.07	2	1.60
6	223.07	0	0	0	0	1	211	0	1.29	2	1.60
6	231.07	0	.	0	0	2	231	0	1.29	1	1.60
6	232.07	0	0	0	1	1	231	0	1.29	2	1.60
6	233.07	1	1	1	0	1	231	0	1.29	0	1.60
6	234.07	0	1	0	0	1	231	0	1.07	2	1.60
6	237.07	0	1	1	0	1	231	0	0.86	2	1.60
6	238.07	1	1	1	0	1	231	0	1.29	1	1.60
6	239.07	0	0	1	0	2	247	0	1.07	2	1.60
6	241.07	0	.	0	0	1	241	1	1.29	0	1.60
6	242.07	0	.	0	0	1	242	1	0.64	1	1.60
6	243.07	0	0	1	0	1	247	0	1.07	2	22.00
6	244.07	1	.	1	0	1	244	1	1.07	2	1.60
6	245.07	0	0	0	0	1	241	1	1.93	1	1.60
6	246.07	0	.	0	0	1	246	0	1.71	0	22.00
6	247.07	0	.	0	0	2	247	0	1.07	1	1.60
6	248.07	0	0	0	0	1	246	0	1.50	1	22.00
6	249.07	1	1	1	0	1	246	0	1.50	1	22.00
6	250.07	0	1	1	0	2	246	0	1.07	2	1.60
6	251.07	0	0	0	0	2	246	0	1.29	2	1.60
6	252.07	0	0	0	0	2	246	0	1.07	1	22.00
6	253.07	1	.	1	0	1	253	1	1.50	2	22.00
6	254.07	1	0	1	0	1	253	1	1.50	2	22.00

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	504.06	351.62	0.58	1.73	0.58	1.73	1	1	0	1.92
6	505.06	377.94	0.60	1.68	0.60	1.68	1	0	0	2.15
6	506.06	350.59	0.58	1.72	0.58	1.72	1	1	0	1.73
6	507.06	354.03	0.58	1.73	0.58	1.72	0		1	.
6	508.06	377.57	0.60	1.67	0.60	1.68	0		1	.
6	509.06	560.73	0.58	1.72	0.58	1.72	1	0	0	1.68
6	510.06	563.10	0.58	1.74	0.58	1.72	0		1	.
6	511.06	250.01	0.46	2.16	0.46	2.16	1	3	0	1.72
6	512.06	748.35	0.49	2.03	0.49	2.03	1	0	0	1.95
6	514.06	429.03	0.51	1.95	0.51	1.95	1	0	0	1.72
6	143.07	37.39	1.02	0.98	1.02	0.98	1	0	0	.
6	144.07	38.28	1.03	0.97	1.03	0.97	1	0	0	0.98
6	145.07	40.68	1.05	0.96	1.05	0.96	1	0	0	0.97
6	171.07	48.95	0.78	1.28	0.78	1.28	1	0	0	1.24
6	174.07	55.19	0.77	1.30	0.76	1.32	0		1	.
6	175.07	61.63	0.90	1.11	0.90	1.11	1	1	0	1.32
6	176.07	62.50	0.87	1.15	0.87	1.15	1	0	0	1.11
6	177.07	63.67	0.87	1.15	0.87	1.15	1	0	0	1.15
6	178.07	64.80	0.79	1.26	0.87	1.15	0		1	.
6	179.07	47.82	0.81	1.24	0.81	1.24	1	0	0	0.96
6	180.07	53.52	0.76	1.32	0.76	1.32	1	0	0	1.28
6	186.07	65.57	0.70	1.44	0.70	1.44	1	0	0	1.15
6	187.07	68.81	0.69	1.45	0.69	1.45	1	0	0	1.44
6	189.07	68.97	0.66	1.51	0.66	1.51	1	0	0	1.45
6	211.07	70.78	0.59	1.70	0.59	1.70	1	4	0	1.51
6	212.07	72.98	0.62	1.61	0.59	1.70	0		1	.
6	213.07	75.91	0.59	1.68	0.59	1.68	1	3	0	1.70
6	214.07	77.65	0.65	1.54	0.65	1.54	1	2	0	1.70
6	223.07	73.51	0.61	1.64	0.59	1.70	0		0	.
6	231.07	78.85	0.56	1.77	0.56	1.77	1	1	0	1.70
6	232.07	80.75	0.58	1.72	0.56	1.77	0		1	.
6	233.07	82.49	0.57	1.75	0.56	1.77	0		0	.
6	234.07	83.22	0.56	1.77	0.56	1.77	0		0	.
6	237.07	86.89	0.57	1.74	0.56	1.77	0		0	.
6	238.07	84.59	0.56	1.78	0.56	1.77	0		0	.
6	239.07	93.30	0.59	1.69	0.60	1.68	0		0	.
6	241.07	98.40	0.68	1.47	0.68	1.47	1	2	0	1.68
6	242.07	97.27	0.61	1.63	0.61	1.63	1	3	0	1.68
6	243.07	90.43	0.57	1.75	0.60	1.68	0		1	.
6	244.07	95.10	0.58	1.72	0.58	1.72	1	3	0	1.68
6	245.07	101.74	0.64	1.56	0.68	1.47	0		1	.
6	246.07	98.40	0.62	1.62	0.62	1.62	1	1	0	1.68
6	247.07	91.80	0.60	1.68	0.60	1.68	1	4	0	1.77
6	248.07	105.08	0.63	1.60	0.62	1.62	0		1	.
6	249.07	106.34	0.62	1.63	0.62	1.62	0		0	.
6	250.07	105.98	0.62	1.61	0.62	1.62	0		0	.
6	251.07	108.28	0.62	1.62	0.62	1.62	0		0	.
6	252.07	112.38	0.62	1.61	0.62	1.62	0		0	.
6	253.07	113.78	0.67	1.50	0.67	1.50	1	2	0	1.62
6	254.07	116.25	0.69	1.45	0.67	1.50	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	255.07	0	0	0	0	1	253	1	1.50	2	22.00
6	256.07	0	.	0	0	1	256	1	1.71	2	1.60
6	257.07	0	1	0	0	1	253	1	1.71	2	22.00
6	258.07	1	.	1	0	1	258	1	1.50	1	1.60
6	259.07	1	0	1	0	1	258	1	1.50	1	1.60
6	260.07	1	0	1	0	1	258	1	1.71	1	1.60
6	261.07	0	.	1	0	1	261	1	1.71	0	22.00
6	263.07	0	.	1	0	1	263	1	1.71	1	1.60
6	264.07	1	.	0	0	1	264	1	0.64	2	22.00
6	265.07	1	.	1	0	1	265	1	0.86	1	22.00
6	266.07	1	.	1	0	1	266	1	1.07	2	22.00
6	267.07	0	.	1	0	1	267	1	1.07	2	1.60
6	268.07	1	.	1	0	2	268	1	1.07	1	1.60
6	270.07	1	0	1	0	1	272	1	1.07	2	22.00
6	272.07	1	.	1	0	2	272	1	1.29	2	22.00
6	273.07	1	.	0	0	1	273	1	0.86	1	1.60
6	274.07	0	.	1	0	1	274	1	1.29	1	1.60
6	275.07	1	.	1	0	2	275	0	0.86	2	22.00
6	276.07	1	.	1	0	1	276	0	1.07	1	22.00
6	277.07	1	0	1	0	1	276	0	1.07	2	73.00
6	279.07	1	.	1	0	1	279	0	1.29	2	22.00
6	281.07	1	.	1	0	2	281	0	1.29	0	22.00
6	282.07	1	.	1	0	2	282	0	1.29	0	22.00
6	283.07	0	.	1	0	1	283	0	1.29	1	1.60
6	284.07	1	.	1	0	1	284	0	1.29	1	103.60
6	285.07	1	.	1	1	1	285	0	0.86	2	52.60
6	287.07	1	.	0	0	2	287	0	1.29	2	52.60
6	288.07	1	.	1	0	1	288	0	1.29	2	52.60
6	289.07	1	.	1	0	2	289	0	0.86	1	42.40
6	292.07	1	1	1	0	1	297	0	1.29	2	42.40
6	293.07	1	.	1	0	1	293	1	1.50	1	1.60
6	294.07	1	.	1	0	1	294	0	1.29	0	42.40
6	295.07	0	.	1	0	3	295	0	1.07	2	1.60
6	296.07	0	.	1	0	1	296	1	1.07	2	73.00
6	297.07	0	.	0	0	1	297	0	1.29	2	42.40
6	298.07	1	1	1	0	1	296	1	1.07	2	62.80
6	300.07	1	0	1	0	1	296	1	1.07	2	42.40
6	301.07	1	0	0	0	2	296	1	1.29	2	22.00
6	302.07	1	0	1	0	1	296	1	1.29	0	22.00
6	303.07	1	.	0	0	1	303	0	1.29	2	42.40
6	304.07	1	0	1	0	1	296	1	1.50	2	22.00
6	305.07	1	1	0	0	2	306	0	1.50	1	42.40
6	306.07	0	.	0	0	1	306	0	1.71	2	22.00
6	307.07	0	1	0	0	1	306	0	1.71	2	42.40
6	308.07	1	1	0	0	1	306	0	1.71	1	42.40
6	309.07	0	1	1	0	1	324	0	1.71	1	22.00
6	310.07	1	.	1	0	1	310	1	1.50	2	22.00
6	313.07	1	0	1	0	1	293	1	1.71	1	1.60
6	314.07	0	1	0	0	1	293	1	1.93	1	1.60
6	315.07	1	.	1	0	1	315	0	1.29	2	42.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	255.07	121.79	0.63	1.58	0.67	1.50	0		0	.
6	256.07	120.69	0.58	1.71	0.58	1.71	1	0	0	1.69
6	257.07	119.86	0.65	1.54	0.67	1.50	0		0	.
6	258.07	111.08	0.59	1.70	0.59	1.70	1	3	0	1.62
6	259.07	112.95	0.62	1.63	0.59	1.70	0		0	.
6	260.07	99.74	0.60	1.67	0.59	1.70	0		1	.
6	261.07	118.46	0.56	1.78	0.56	1.78	1	3	0	1.62
6	263.07	119.29	0.59	1.69	0.59	1.69	1	1	0	1.62
6	264.07	125.33	0.59	1.69	0.59	1.69	1	2	0	1.71
6	265.07	123.63	0.55	1.82	0.55	1.82	1	3	0	1.71
6	266.07	126.73	0.58	1.71	0.58	1.71	1	1	0	1.71
6	267.07	128.87	0.59	1.68	0.59	1.68	1	2	0	1.71
6	268.07	127.70	0.56	1.78	0.56	1.78	1	3	0	1.71
6	270.07	132.70	0.58	1.74	0.57	1.76	0		1	.
6	272.07	131.37	0.57	1.76	0.57	1.76	1	0	0	1.71
6	273.07	130.67	0.51	1.95	0.51	1.95	1	3	0	1.76
6	274.07	133.34	0.54	1.86	0.54	1.86	1	2	0	1.76
6	275.07	135.61	0.53	1.87	0.53	1.87	1	0	0	1.76
6	276.07	137.27	0.53	1.88	0.53	1.88	1	1	0	1.87
6	277.07	55.73	0.54	1.84	0.53	1.88	0		1	.
6	279.07	140.41	0.53	1.90	0.53	1.90	1	2	0	1.88
6	281.07	139.28	0.49	2.03	0.49	2.03	1	3	0	1.88
6	282.07	142.01	0.49	2.06	0.49	2.06	1	0	0	1.88
6	283.07	134.87	0.43	2.32	0.43	2.32	1	3	0	1.88
6	284.07	44.25	0.49	2.02	0.49	2.02	1	2	0	2.06
6	285.07	86.55	0.39	2.54	0.39	2.54	1	0	0	2.06
6	287.07	91.15	0.41	2.43	0.41	2.43	1	2	0	2.54
6	288.07	88.85	0.38	2.61	0.38	2.61	1	3	0	2.54
6	289.07	86.12	0.41	2.44	0.41	2.44	1	2	0	2.54
6	292.07	89.26	0.39	2.54	0.39	2.55	0		1	.
6	293.07	167.57	0.50	1.98	0.50	1.98	1	2	0	2.55
6	294.07	83.71	0.38	2.64	0.38	2.64	1	3	0	2.54
6	295.07	139.78	0.40	2.48	0.40	2.48	1	3	0	2.06
6	296.07	61.50	0.39	2.54	0.39	2.54	1	3	0	2.55
6	297.07	87.35	0.39	2.55	0.39	2.55	1	1	0	2.54
6	298.07	75.88	0.39	2.55	0.39	2.54	0		1	.
6	300.07	98.69	0.39	2.57	0.39	2.54	0		0	.
6	301.07	165.57	0.39	2.57	0.39	2.54	0		0	.
6	302.07	167.10	0.39	2.56	0.39	2.54	0		0	.
6	303.07	103.47	0.39	2.54	0.39	2.54	1	0	0	2.45
6	304.07	169.11	0.40	2.48	0.39	2.54	0		0	.
6	305.07	102.37	0.41	2.47	0.41	2.45	0		1	.
6	306.07	172.08	0.41	2.45	0.41	2.45	1	0	0	2.55
6	307.07	104.40	0.40	2.52	0.41	2.45	0		0	.
6	308.07	100.73	0.41	2.45	0.41	2.45	0		0	.
6	309.07	192.20	0.34	2.95	0.34	2.98	0		0	.
6	310.07	188.96	0.35	2.84	0.35	2.84	1	1	0	2.62
6	313.07	170.21	0.50	2.00	0.50	1.98	0		1	.
6	314.07	171.68	0.50	2.00	0.50	1.98	0		0	.
6	315.07	106.37	0.37	2.67	0.37	2.67	1	1	0	2.54

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	316.07	0	1	1	0	1	318	1	1.50	2	103.60
6	317.07	1	.	1	0	1	317	1	2.14	2	22.00
6	318.07	1	.	1	0	.	318	1	1.29	1	1.60
6	319.07	1	1	1	0	1	318	1	1.71	1	1.60
6	320.07	1	.	1	0	1	320	1	1.93	1	1.60
6	321.07	1	0	0	0	1	324	0	1.50	1	22.00
6	322.07	1	0	1	0	1	310	1	1.71	1	22.00
6	323.07	1	0	1	0	1	324	0	1.71	2	73.00
6	324.07	1	.	1	0	2	324	0	1.71	1	22.00
6	325.07	0	0	0	0	1	324	0	1.50	2	42.40
6	326.07	0	0	0	0	1	324	0	1.71	1	22.00
6	327.07	1	1	1	0	1	324	0	1.93	2	42.40
6	328.07	0	0	1	0	2	324	0	1.71	1	22.00
6	329.07	1	.	1	0	1	329	0	1.50	2	22.00
6	330.07	1	.	1	0	1	330	0	1.93	1	1.60
6	331.07	0	.	0	0	1	331	0	1.93	1	1.60
6	332.07	0	1	0	0	1	334	0	2.14	1	22.00
6	333.07	1	.	0	0	1	333	1	1.93	2	42.40
6	334.07	1	.	1	0	1	334	0	1.50	2	42.40
6	335.07	1	0	1	0	1	333	1	2.14	2	22.00
6	336.07	1	0	1	0	1	333	1	2.14	2	22.00
6	337.07	1	0	1	0	1	333	1	1.71	2	22.00
6	339.07	1	1	1	0	1	340	1	1.71	1	22.00
6	340.07	1	.	1	0	1	340	1	2.14	1	22.00
6	341.07	0	1	1	0	1	357	1	1.93	2	103.60
6	342.07	0	1	1	0	2	340	1	1.93	1	22.00
6	343.07	1	0	0	0	1	340	1	1.71	1	22.00
6	344.07	0	.	0	0	1	344	1	1.71	2	52.60
6	345.07	0	1	1	0	1	333	1	2.14	2	52.60
6	346.07	1	1	1	0	1	333	1	2.14	2	42.40
6	347.07	1	1	1	0	1	333	1	2.14	2	22.00
6	348.07	1	1	1	0	1	333	1	2.36	2	103.60
6	349.07	0	0	0	0	1	357	1	2.36	1	103.60
6	350.07	0	1	0	0	1	333	1	2.14	2	52.60
6	351.07	0	.	1	0	1	351	1	1.93	0	22.00
6	352.07	0	1	1	1	1	333	1	1.93	2	42.40
6	353.07	1	0	1	0	1	357	1	2.14	0	22.00
6	354.07	1	0	1	0	1	368	1	2.57	2	103.60
6	355.07	1	.	1	0	1	355	0	1.29	0	22.00
6	356.07	1	0	1	0	1	333	1	2.14	2	22.00
6	357.07	1	.	0	0	1	357	1	1.71	1	22.00
6	359.07	1	0	0	0	1	357	1	1.93	1	22.00
6	360.07	1	.	1	0	1	360	0	1.71	0	22.00
6	361.07	1	0	1	0	1	357	1	1.93	1	22.00
6	362.07	1	.	1	0	1	362	0	2.14	1	22.00
6	363.07	0	1	0	0	1	357	1	2.14	1	22.00
6	365.07	0	0	1	0	1	370	1	1.50	0	1.60
6	366.07	1	1	1	0	1	368	1	2.36	2	22.00
6	367.07	0	0	0	0	1	368	1	2.14	2	62.80
6	368.07	0	.	0	0	1	368	1	1.93	2	62.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	316.07	45.88	0.36	2.79	0.38	2.62	0		1	.
6	317.07	186.22	0.35	2.86	0.35	2.86	1	3	0	2.62
6	318.07	183.42	0.38	2.62	0.38	2.62	1	0	0	2.67
6	319.07	185.36	0.37	2.70	0.38	2.62	0		0	.
6	320.07	185.39	0.37	2.74	0.37	2.74	1	2	0	2.62
6	321.07	190.26	0.33	3.04	0.34	2.98	0		0	.
6	322.07	185.62	0.34	2.95	0.35	2.84	0		1	.
6	323.07	87.06	0.34	2.95	0.34	2.98	0		1	.
6	324.07	190.72	0.34	2.98	0.34	2.98	1	0	0	2.84
6	325.07	108.49	0.33	3.02	0.34	2.98	0		0	.
6	326.07	194.83	0.33	3.05	0.34	2.98	0		0	.
6	327.07	110.07	0.32	3.12	0.34	2.98	0		0	.
6	328.07	196.57	0.33	3.04	0.34	2.98	0		0	.
6	329.07	202.77	0.33	3.08	0.33	3.08	1	2	0	2.98
6	330.07	198.04	0.31	3.27	0.31	3.27	1	3	0	2.98
6	331.07	201.71	0.32	3.17	0.32	3.17	1	1	0	2.98
6	332.07	198.30	0.31	3.27	0.31	3.20	0		1	.
6	333.07	113.21	0.34	2.96	0.34	2.96	1	2	0	3.20
6	334.07	112.04	0.31	3.20	0.31	3.20	1	0	0	3.17
6	335.07	214.89	0.33	3.02	0.34	2.96	0		1	.
6	336.07	217.09	0.33	3.05	0.34	2.96	0		0	.
6	337.07	219.29	0.33	3.04	0.34	2.96	0		0	.
6	339.07	207.81	0.31	3.25	0.30	3.38	0		0	.
6	340.07	203.14	0.30	3.38	0.30	3.38	1	3	0	3.20
6	341.07	51.95	0.31	3.20	0.29	3.47	0		0	.
6	342.07	205.34	0.31	3.23	0.30	3.38	0		1	.
6	343.07	211.08	0.31	3.27	0.30	3.38	0		0	.
6	344.07	114.71	0.31	3.18	0.31	3.18	1	3	0	3.20
6	345.07	114.94	0.34	2.93	0.34	2.96	0		0	.
6	346.07	117.78	0.34	2.93	0.34	2.96	0		0	.
6	347.07	231.57	0.33	3.05	0.34	2.96	0		0	.
6	348.07	56.39	0.32	3.15	0.34	2.96	0		0	.
6	349.07	54.46	0.29	3.39	0.29	3.47	0		0	.
6	350.07	119.68	0.33	2.99	0.34	2.96	0		0	.
6	351.07	238.08	0.33	3.01	0.33	3.01	1	2	0	3.20
6	352.07	124.62	0.33	3.04	0.34	2.96	0		0	.
6	353.07	228.77	0.29	3.41	0.29	3.47	0		0	.
6	354.07	55.02	0.28	3.63	0.27	3.70	0		0	.
6	355.07	237.64	0.30	3.39	0.30	3.39	1	3	0	3.20
6	356.07	240.58	0.32	3.09	0.34	2.96	0		0	.
6	357.07	213.48	0.29	3.47	0.29	3.47	1	3	0	3.20
6	359.07	215.92	0.29	3.47	0.29	3.47	0		1	.
6	360.07	230.10	0.27	3.65	0.27	3.65	1	3	0	3.20
6	361.07	216.59	0.29	3.42	0.29	3.47	0		0	.
6	362.07	237.71	0.28	3.52	0.28	3.52	1	0	0	3.20
6	363.07	221.89	0.29	3.39	0.29	3.47	0		0	.
6	365.07	88.39	0.08	11.78	0.09	11.60	0		1	.
6	366.07	253.06	0.28	3.63	0.27	3.70	0		0	.
6	367.07	94.90	0.27	3.67	0.27	3.70	0		1	.
6	368.07	89.39	0.27	3.70	0.27	3.70	1	2	0	3.52

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	369.07	1	.	1	0	1	369	1	2.36	1	22.00
6	370.07	0	.	1	0	1	370	1	1.29	1	1.60
6	371.07	0	.	0	0	1	371	0	2.36	1	22.00
6	372.07	1	.	1	0	1	372	0	2.14	0	103.60
6	373.07	1	.	0	0	1	373	0	2.14	2	103.60
6	374.07	1	1	1	0	1	375	1	2.79	0	103.60
6	375.07	0	.	1	0	1	375	1	2.36	2	103.60
6	376.07	1	0	0	0	1	375	1	2.57	2	103.60
6	377.07	1	1	0	0	1	383	1	2.79	1	103.60
6	378.07	1	.	1	0	1	378	0	2.36	1	62.80
6	379.07	0	.	1	0	1	379	1	2.14	1	73.00
6	381.07	0	1	1	0	1	375	1	2.36	2	103.60
6	382.07	1	1	1	0	2	375	1	2.57	2	103.60
6	383.07	1	.	1	0	1	383	1	1.93	1	22.00
6	384.07	1	0	1	0	1	383	1	2.57	1	22.00
6	386.07	1	0	1	0	1	383	1	2.57	1	22.00
6	387.07	1	0	1	0	1	383	1	2.57	1	22.00
6	388.07	1	0	1	0	1	383	1	3.00	1	83.20
6	389.07	0	0	1	0	1	383	1	2.14	1	124.01
6	390.07	0	0	1	0	1	383	1	2.57	1	22.00
6	391.07	1	.	1	0	1	391	0	2.57	1	83.20
6	392.07	1	1	0	0	1	357	1	1.71	1	22.00
6	393.07	0	0	0	0	1	375	1	2.57	2	83.20
6	394.07	0	1	0	0	1	375	1	2.57	2	83.20
6	395.07	0	1	0	0	1	383	1	2.36	1	1.60
6	396.07	0	1	1	0	1	383	1	2.79	1	103.60
6	397.07	0	1	0	0	1	391	0	2.57	2	73.00
6	398.07	0	0	1	0	1	391	0	3.00	1	22.00
6	399.07	1	1	1	0	1	391	0	1.71	2	52.60
6	400.07	1	0	1	0	1	391	0	1.50	2	52.60
6	401.07	0	.	0	0	1	401	1	1.71	2	52.60
6	402.07	0	0	1	0	1	401	1	1.29	2	52.60
6	403.07	0	0	1	0	1	401	1	1.50	2	73.00
6	404.07	1	.	1	0	1	404	1	1.71	1	22.00
6	405.07	1	0	1	0	1	391	0	1.29	1	22.00
6	406.07	0	1	1	0	1	404	1	1.50	1	103.60
6	407.07	1	0	1	0	1	409	0	1.71	1	103.60
6	408.07	1	0	1	0	1	409	0	1.50	2	93.40
6	409.07	1	.	1	0	1	409	0	1.50	1	103.60
6	410.07	1	1	1	0	1	409	0	1.71	2	93.40
6	411.07	0	1	1	0	2	409	0	1.71	1	93.40
6	412.07	1	0	1	0	1	416	0	1.71	2	62.80
6	413.07	1	.	1	0	1	413	1	1.50	2	62.80
6	414.07	1	0	1	0	1	413	1	1.93	2	62.80
6	415.07	1	0	1	0	1	413	1	1.71	2	134.21
6	416.07	1	.	1	0	2	416	0	1.50	1	22.00
6	417.07	0	.	1	0	1	417	1	1.50	1	103.60
6	418.07	0	0	1	0	1	417	1	1.71	1	103.60
6	419.07	0	0	0	0	1	417	1	1.50	1	103.60
6	420.07	0	.	1	0	2	420	1	1.93	1	103.60

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	369.07	231.80	0.23	4.41	0.23	4.41	1	3	0	3.52
6	370.07	90.13	0.09	11.60	0.09	11.60	1	3	0	.
6	371.07	241.28	0.24	4.11	0.24	4.11	1	3	0	3.52
6	372.07	51.35	0.30	3.39	0.30	3.39	1	3	0	4.07
6	373.07	50.85	0.31	3.27	0.31	3.27	1	2	0	4.07
6	374.07	53.62	0.30	3.34	0.27	3.71	0		1	.
6	375.07	49.18	0.27	3.71	0.27	3.71	1	2	0	4.07
6	376.07	57.79	0.30	3.34	0.27	3.71	0		0	.
6	377.07	57.39	0.29	3.42	0.25	4.07	0		0	.
6	378.07	93.06	0.25	4.07	0.25	4.07	1	1	0	3.52
6	379.07	94.70	0.24	4.13	0.24	4.13	1	3	0	4.07
6	381.07	60.20	0.36	2.78	0.27	3.71	0		0	.
6	382.07	59.33	0.36	2.78	0.27	3.71	0		0	.
6	383.07	248.19	0.25	4.07	0.25	4.07	1	3	0	4.07
6	384.07	250.85	0.24	4.10	0.25	4.07	0		1	.
6	386.07	276.01	0.35	2.82	0.25	4.07	0		0	.
6	387.07	273.18	0.33	3.01	0.25	4.07	0		0	.
6	388.07	81.08	0.29	3.40	0.25	4.07	0		0	.
6	389.07	30.19	0.28	3.52	0.25	4.07	0		0	.
6	390.07	282.69	0.35	2.84	0.25	4.07	0		0	.
6	391.07	84.72	0.35	2.82	0.35	2.82	1	1	0	4.07
6	392.07	224.86	0.28	3.54	0.29	3.47	0		0	.
6	393.07	86.75	0.36	2.77	0.27	3.71	0		0	.
6	394.07	83.01	0.30	3.29	0.27	3.71	0		0	.
6	395.07	256.46	0.25	3.93	0.25	4.07	0		0	.
6	396.07	66.80	0.36	2.79	0.25	4.07	0		0	.
6	397.07	125.06	0.36	2.77	0.35	2.82	0		1	.
6	398.07	287.59	0.36	2.78	0.35	2.82	0		0	.
6	399.07	156.52	0.36	2.78	0.35	2.82	0		0	.
6	400.07	158.59	0.36	2.80	0.35	2.82	0		0	.
6	401.07	160.32	0.35	2.83	0.35	2.83	1	3	0	2.82
6	402.07	161.96	0.36	2.80	0.35	2.83	0		1	.
6	403.07	128.60	0.35	2.85	0.35	2.83	0		0	.
6	404.07	305.98	0.37	2.72	0.37	2.72	1	2	0	2.82
6	405.07	304.21	0.36	2.76	0.35	2.82	0		0	.
6	406.07	72.11	0.36	2.80	0.37	2.72	0		1	.
6	407.07	69.80	0.36	2.80	0.36	2.81	0		0	.
6	408.07	104.13	0.37	2.73	0.36	2.81	0		1	.
6	409.07	70.44	0.36	2.81	0.36	2.81	1	1	0	2.82
6	410.07	107.87	0.37	2.68	0.36	2.81	0		0	.
6	411.07	110.87	0.37	2.72	0.36	2.81	0		0	.
6	412.07	145.48	0.37	2.67	0.37	2.68	0		1	.
6	413.07	148.35	0.38	2.65	0.38	2.65	1	3	0	2.68
6	414.07	148.75	0.37	2.71	0.38	2.65	0		1	.
6	415.07	67.46	0.39	2.58	0.38	2.65	0		0	.
6	416.07	321.39	0.37	2.68	0.37	2.68	1	1	0	2.81
6	417.07	77.45	0.40	2.53	0.40	2.53	1	2	0	2.68
6	418.07	73.64	0.40	2.48	0.40	2.53	0		0	.
6	419.07	74.91	0.40	2.49	0.40	2.53	0		1	.
6	420.07	79.21	0.42	2.40	0.42	2.40	1	2	0	2.68

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	421.07	1	0	0	0	1	423	0	1.71	2	62.80
6	422.07	1	.	1	0	1	422	0	1.50	1	93.40
6	423.07	1	.	1	0	1	423	0	1.71	1	62.80
6	424.07	1	.	1	0	1	424	1	1.93	0	93.40
6	425.07	0	1	1	0	1	422	0	1.50	1	93.40
6	428.07	1	.	1	0	1	428	1	1.71	2	93.40
6	429.07	0	1	1	0	1	434	1	1.93	0	103.60
6	431.07	0	.	0	0	1	431	1	1.50	1	1.60
6	432.07	0	.	1	0	1	432	1	1.29	1	83.20
6	433.07	1	.	1	0	1	433	1	1.50	0	83.20
6	434.07	1	.	1	1	1	434	1	1.93	0	103.60
6	435.07	1	1	1	0	1	431	1	1.50	1	83.20
6	436.07	1	.	1	0	1	436	0	1.71	2	93.40
6	437.07	0	.	0	0	1	437	1	1.71	1	93.40
6	438.07	1	1	1	1	1	440	1	1.07	2	93.40
6	439.07	1	.	1	0	2	439	1	0.86	1	93.40
6	440.07	0	.	1	0	1	440	1	0.86	2	103.60
6	441.07	0	.	1	0	2	441	1	1.29	0	103.60
6	442.07	1	1	1	0	1	441	1	1.07	1	103.60
6	443.07	0	.	1	0	2	443	0	0.86	2	103.60
6	445.07	0	.	1	0	2	445	0	0.64	2	103.60
6	446.07	1	1	1	0	1	445	0	1.07	1	93.40
6	447.07	0	1	0	0	1	445	0	1.29	2	93.40
6	448.07	0	0	1	0	1	445	0	1.50	1	83.20
6	449.07	0	0	0	0	1	445	0	1.71	2	83.20
6	450.07	1	.	1	0	1	450	0	1.50	1	103.60
6	451.07	0	.	1	0	1	451	0	1.93	0	103.60
6	452.07	1	.	1	0	1	452	0	1.71	1	124.01
6	453.07	1	0	1	0	1	452	0	1.50	0	124.01
6	454.07	0	.	1	0	1	454	0	1.29	1	93.40
6	455.07	1	0	1	0	1	458	0	0.86	1	124.01
6	456.07	0	.	1	0	2	456	0	0.86	0	83.20
6	457.07	0	.	1	0	2	457	0	1.50	0	93.40
6	458.07	1	.	1	0	2	458	0	1.07	0	93.40
6	459.07	1	.	1	0	1	459	0	1.29	0	124.01
6	460.07	1	.	0	0	1	460	0	1.29	1	124.01
6	461.07	0	.	1	0	.	461	0	0.43	1	103.60
6	462.07	0	.	1	0	1	462	0	1.50	1	103.60
6	463.07	1	.	1	1	3	463	0	1.29	1	103.60
6	464.07	1	0	0	0	1	463	0	1.50	2	103.60
6	465.07	0	1	0	1	1	462	0	1.29	2	124.01
6	466.07	0	0	1	0	1	462	0	1.07	2	52.60
6	467.07	0	0	0	0	1	462	0	1.50	1	22.00
6	468.07	1	1	1	0	2	462	0	1.07	1	22.00
6	469.07	1	.	1	0	2	469	0	1.29	2	134.21
6	470.07	1	0	1	0	1	469	0	1.29	2	134.21
6	471.07	1	.	1	0	1	471	0	1.50	1	93.40
6	472.07	0	1	0	0	1	469	0	1.07	1	93.40
6	473.07	1	0	1	0	1	481	0	1.71	1	52.60
6	474.07	1	0	1	0	2	469	0	1.07	2	134.21

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	421.07	169.64	0.41	2.44	0.41	2.45	0		1	.
6	422.07	131.23	0.45	2.24	0.45	2.24	1	1	0	2.45
6	423.07	168.32	0.41	2.45	0.41	2.45	1	1	0	2.68
6	424.07	144.78	0.44	2.28	0.44	2.28	1	1	0	2.24
6	425.07	140.90	0.44	2.25	0.45	2.24	0		1	.
6	428.07	140.14	0.41	2.42	0.41	2.42	1	3	0	2.28
6	429.07	84.32	0.49	2.06	0.46	2.16	0		1	.
6	431.07	353.86	0.41	2.46	0.41	2.46	1	3	0	2.28
6	432.07	132.13	0.37	2.70	0.37	2.70	1	3	0	2.28
6	433.07	129.16	0.43	2.35	0.43	2.35	1	2	0	2.28
6	434.07	80.98	0.46	2.16	0.46	2.16	1	2	0	2.28
6	435.07	147.34	0.44	2.28	0.41	2.46	0		1	.
6	436.07	123.82	0.40	2.52	0.40	2.52	1	3	0	2.24
6	437.07	142.87	0.43	2.34	0.43	2.34	1	2	0	2.28
6	438.07	126.46	0.34	2.95	0.34	2.92	0		1	.
6	439.07	121.62	0.40	2.51	0.40	2.51	1	3	0	2.28
6	440.07	66.27	0.34	2.92	0.34	2.92	1	3	0	2.28
6	441.07	90.66	0.38	2.66	0.38	2.66	1	1	0	2.28
6	442.07	95.70	0.39	2.54	0.38	2.66	0		1	.
6	443.07	88.36	0.37	2.69	0.37	2.69	1	3	0	2.66
6	445.07	93.33	0.37	2.69	0.37	2.69	1	1	0	2.66
6	446.07	127.99	0.37	2.72	0.37	2.69	0		1	.
6	447.07	129.19	0.37	2.71	0.37	2.69	0		0	.
6	448.07	152.22	0.37	2.68	0.37	2.69	0		0	.
6	449.07	150.51	0.37	2.72	0.37	2.69	0		0	.
6	450.07	97.70	0.45	2.21	0.45	2.21	1	1	0	2.69
6	451.07	100.27	0.48	2.06	0.48	2.06	1	1	0	2.21
6	452.07	69.03	0.51	1.97	0.51	1.97	1	1	0	2.06
6	453.07	70.27	0.51	1.96	0.51	1.97	0		1	.
6	454.07	157.32	0.46	2.18	0.46	2.18	1	3	0	1.97
6	455.07	75.20	0.44	2.29	0.47	2.12	0		1	.
6	456.07	163.96	0.50	2.00	0.50	2.00	1	2	0	1.97
6	457.07	183.31	0.40	2.47	0.40	2.47	1	0	0	2.12
6	458.07	163.19	0.47	2.12	0.47	2.12	1	0	0	1.97
6	459.07	72.17	0.32	3.09	0.32	3.09	1	3	0	2.47
6	460.07	73.70	0.37	2.72	0.37	2.72	1	3	0	2.47
6	461.07	93.83	0.35	2.83	0.35	2.83	1	3	0	1.97
6	462.07	104.24	0.37	2.70	0.37	2.70	1	0	0	2.70
6	463.07	102.20	0.37	2.70	0.37	2.70	1	0	0	2.47
6	464.07	102.20	0.38	2.60	0.37	2.70	0		1	.
6	465.07	77.54	0.37	2.69	0.37	2.70	0		0	.
6	466.07	294.86	0.37	2.68	0.37	2.70	0		0	.
6	467.07	427.73	0.38	2.67	0.37	2.70	0		0	.
6	468.07	424.43	0.37	2.70	0.37	2.70	0		1	.
6	469.07	93.42	0.38	2.65	0.38	2.65	1	1	0	2.70
6	470.07	95.02	0.38	2.60	0.38	2.65	0		1	.
6	471.07	184.62	0.31	3.27	0.31	3.27	1	3	0	2.65
6	472.07	183.35	0.38	2.63	0.38	2.65	0		0	.
6	473.07	326.92	0.38	2.66	0.38	2.61	0		0	.
6	474.07	97.26	0.38	2.61	0.38	2.65	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	476.07	1	0	1	0	2	481	0	1.93	0	103.60
6	477.07	1	1	1	0	1	469	0	1.29	2	134.21
6	478.07	1	0	1	0	2	469	0	1.29	2	103.60
6	479.07	0	1	0	0	2	481	0	1.93	1	52.60
6	480.07	0	1	1	0	1	481	0	1.50	1	1.60
6	481.07	1	.	1	0	2	481	0	0.86	2	103.60
6	482.07	1	1	1	0	1	481	0	1.50	2	113.80
6	483.07	1	0	1	0	1	481	0	1.71	2	134.21
6	484.07	1	0	1	0	1	481	0	0.86	1	134.21
6	485.07	1	0	1	0	1	481	0	2.14	2	134.21
6	486.07	1	0	1	0	1	481	0	1.29	1	134.21
6	487.07	1	1	1	0	1	481	0	1.29	2	134.21
6	488.07	1	0	1	0	1	481	0	1.93	2	134.21
6	489.07	0	0	1	0	1	481	0	1.50	2	134.21
6	490.07	1	0	1	0	1	481	0	1.50	1	103.60
6	491.07	0	1	1	0	1	481	0	1.50	1	103.60
6	492.07	1	0	1	0	1	481	0	1.50	1	103.60
6	493.07	1	1	1	0	1	481	0	1.71	1	103.60
6	494.07	0	0	0	0	1	481	0	1.93	2	103.60
6	495.07	1	0	1	0	1	481	0	1.71	1	103.60
6	496.07	1	1	1	0	1	481	0	1.50	1	103.60
6	497.07	0	1	1	0	1	481	0	1.71	2	103.60
6	498.07	0	.	1	0	.	498	0	0.43	1	103.60
6	499.07	1	0	1	1	1	481	0	1.71	2	93.40
6	500.07	1	0	1	0	1	481	0	1.93	1	93.40
6	501.07	0	.	1	0	2	501	0	1.29	2	73.00
6	502.07	1	.	1	0	.	502	0	0.43	1	134.21
6	503.07	1	.	1	0	2	503	0	1.50	0	103.60
6	504.07	1	.	1	0	1	504	0	0.64	1	113.80
6	505.07	1	.	1	0	.	505	0	0.86	2	93.40
6	506.07	1	.	1	0	1	506	0	0.86	0	113.80
6	507.07	0	1	0	0	1	506	0	1.07	2	113.80
6	508.07	0	1	0	0	1	505	0	0.43	1	93.40
6	509.07	1	1	1	0	2	505	0	1.07	1	22.00
6	510.07	1	0	1	0	1	505	0	0.86	2	22.00
6	511.07	0	.	1	0	3	511	0	0.64	2	83.20
6	512.07	1	.	0	0	.	512	0	0.43	2	22.00
6	514.07	0	.	0	0	.	514	0	0.43	2	134.21
6	516.07	1	.	1	0	1	516	0	1.29	2	93.40
6	517.07	1	.	0	1	1	517	0	1.29	1	83.20
6	518.07	.	0	0	0	1	258	1	1.50	1	1.60
6	277.08	1	.	1	0	1	277	0	1.07	2	32.20
6	284.08	1	.	1	0	1	284	0	0.86	1	62.80
6	285.08	1	.	1	1	1	285	0	1.07	2	11.80
6	287.08	1	.	0	0	1	287	0	1.29	2	11.80
6	288.08	1	.	1	0	1	288	0	1.50	2	11.80
6	289.08	1	.	1	0	1	289	0	0.86	1	1.60
6	292.08	1	.	1	0	1	292	0	1.07	0	1.60
6	294.08	1	.	1	0	2	294	0	0.64	1	1.60
6	296.08	0	.	1	0	1	296	0	0.64	2	32.20

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	476.07	145.65	0.38	2.65	0.38	2.61	0		0	.
6	477.07	100.33	0.38	2.61	0.38	2.65	0		0	.
6	478.07	137.17	0.38	2.62	0.38	2.65	0		0	.
6	479.07	336.53	0.38	2.61	0.38	2.61	0		0	.
6	480.07	460.03	0.39	2.57	0.38	2.61	0		0	.
6	481.07	134.24	0.38	2.61	0.38	2.61	1	1	0	2.65
6	482.07	154.89	0.41	2.42	0.38	2.61	0		0	.
6	483.07	109.27	0.39	2.59	0.38	2.61	0		0	.
6	484.07	106.97	0.38	2.61	0.38	2.61	0		1	.
6	485.07	108.17	0.39	2.57	0.38	2.61	0		0	.
6	486.07	101.80	0.38	2.65	0.38	2.61	0		0	.
6	487.07	111.47	0.39	2.56	0.38	2.61	0		0	.
6	488.07	114.24	0.40	2.52	0.38	2.61	0		0	.
6	489.07	115.18	0.40	2.49	0.38	2.61	0		0	.
6	490.07	141.31	0.41	2.46	0.38	2.61	0		0	.
6	491.07	151.72	0.41	2.45	0.38	2.61	0		0	.
6	492.07	149.82	0.41	2.46	0.38	2.61	0		0	.
6	493.07	171.01	0.42	2.41	0.38	2.61	0		0	.
6	494.07	169.54	0.41	2.47	0.38	2.61	0		0	.
6	495.07	175.61	0.41	2.46	0.38	2.61	0		0	.
6	496.07	178.61	0.41	2.43	0.38	2.61	0		0	.
6	497.07	180.88	0.41	2.45	0.38	2.61	0		0	.
6	498.07	82.68	0.49	2.05	0.38	2.61	1	3	0	1.58
6	499.07	244.17	0.41	2.42	0.38	2.61	0		0	.
6	500.07	252.18	0.41	2.42	0.38	2.61	0		0	.
6	501.07	409.05	0.42	2.40	0.42	2.40	1	1	0	2.47
6	502.07	203.53	0.45	2.23	0.45	2.23	1	0	0	2.40
6	503.07	233.50	0.40	2.47	0.40	2.47	1	0	0	2.61
6	504.07	351.62	0.54	1.85	0.54	1.85	1	1	0	2.31
6	505.07	377.94	0.56	1.78	0.56	1.78	1	0	0	1.58
6	506.07	350.59	0.63	1.58	0.63	1.58	1	0	0	1.85
6	507.07	354.03	0.65	1.54	0.63	1.58	0		1	.
6	508.07	377.57	0.56	1.80	0.56	1.78	0		1	.
6	509.07	560.73	0.56	1.79	0.56	1.78	0		0	.
6	510.07	563.10	0.59	1.71	0.56	1.78	0		0	.
6	511.07	250.01	0.43	2.31	0.43	2.31	1	0	0	2.23
6	512.07	748.35	0.48	2.06	0.48	2.06	1	0	0	1.78
6	514.07	429.03	0.25	3.98	0.25	3.98	1	0	0	1.78
6	516.07	138.87	0.26	3.87	0.26	3.87	1	3	0	2.47
6	517.07	167.13	0.34	2.96	0.34	2.96	1	3	0	2.70
6	518.07	115.79	0.63	1.58	0.59	1.70	0		0	.
6	277.08	55.73	0.74	1.34	0.74	1.34	1	1	0	.
6	284.08	44.25	0.77	1.30	0.77	1.30	1	2	0	1.44
6	285.08	86.55	0.69	1.44	0.69	1.44	1	1	0	1.34
6	287.08	91.15	0.70	1.43	0.70	1.43	1	2	0	1.44
6	288.08	88.85	0.70	1.43	0.70	1.43	1	3	0	1.44
6	289.08	86.12	0.61	1.65	0.61	1.65	1	1	0	1.44
6	292.08	89.26	0.61	1.63	0.61	1.63	1	1	0	1.65
6	294.08	83.71	0.61	1.64	0.61	1.64	1	3	0	1.44
6	296.08	61.50	0.63	1.59	0.63	1.59	1	1	0	1.63

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	297.08	0	1	0	0	1	289	0	1.07	0	1.60
6	298.08	1	.	1	0	1	298	0	0.64	2	22.00
6	300.08	1	.	1	0	2	300	0	0.43	0	1.60
6	303.08	1	.	0	0	1	303	0	1.29	0	1.60
6	305.08	1	.	0	0	2	305	0	1.29	1	1.60
6	307.08	0	1	0	0	1	305	0	1.50	2	1.60
6	308.08	1	.	0	0	1	308	0	1.29	1	1.60
6	315.08	1	0	1	0	2	303	0	1.07	2	1.60
6	316.08	0	.	1	0	1	316	0	1.07	2	62.80
6	323.08	1	.	1	0	1	323	0	1.50	2	32.20
6	325.08	0	.	0	0	1	325	0	1.29	0	1.60
6	327.08	1	.	1	0	1	327	0	1.71	2	1.60
6	333.08	1	.	0	0	1	333	1	1.71	0	1.60
6	334.08	1	.	1	0	1	334	1	1.50	2	1.60
6	341.08	0	.	1	0	1	341	0	1.71	1	62.80
6	344.08	0	.	0	0	1	344	1	1.71	2	11.80
6	345.08	0	.	1	0	1	345	1	2.14	2	11.80
6	346.08	1	1	1	0	1	349	0	2.14	0	1.60
6	348.08	1	.	1	0	1	348	0	2.36	0	62.80
6	349.08	0	.	0	0	1	349	0	2.14	1	62.80
6	350.08	0	.	0	0	1	350	0	2.14	2	11.80
6	352.08	0	.	1	1	1	352	0	1.93	0	1.60
6	354.08	1	.	1	0	1	354	0	2.14	1	62.80
6	367.08	0	.	0	0	1	367	0	1.93	2	22.00
6	368.08	0	.	0	0	1	368	0	1.50	2	22.00
6	372.08	1	1	1	0	1	375	0	1.71	0	62.80
6	373.08	1	0	0	0	1	375	0	1.93	2	62.80
6	374.08	1	.	1	0	1	374	0	1.93	2	62.80
6	375.08	0	.	1	0	1	375	0	1.50	2	62.80
6	376.08	1	.	0	0	1	376	0	1.71	2	62.80
6	377.08	1	0	0	0	1	376	0	2.14	1	62.80
6	378.08	1	1	1	0	1	368	0	1.71	1	22.00
6	379.08	0	1	1	0	1	368	0	1.71	0	32.20
6	381.08	0	.	1	0	1	381	0	1.93	2	62.80
6	382.08	1	.	1	0	1	382	0	1.71	0	62.80
6	388.08	1	.	1	0	1	388	0	1.93	1	42.40
6	389.08	0	.	1	0	1	389	0	1.50	1	83.20
6	391.08	1	1	1	0	1	393	0	1.93	1	42.40
6	393.08	0	.	0	0	1	393	0	2.14	2	42.40
6	394.08	0	.	0	0	1	394	0	1.71	2	42.40
6	396.08	0	.	1	0	1	396	0	2.14	1	62.80
6	397.08	0	1	0	0	1	393	0	1.93	2	32.20
6	399.08	1	.	1	0	1	399	1	1.07	2	11.80
6	400.08	1	0	1	0	1	399	1	1.07	2	11.80
6	401.08	0	.	0	0	1	399	1	1.07	2	11.80
6	402.08	0	.	1	0	1	402	0	1.07	2	11.80
6	403.08	0	0	1	0	1	402	0	1.29	2	32.20
6	406.08	0	0	1	0	1	402	0	1.29	1	62.80
6	407.08	1	.	1	0	1	407	0	1.50	1	62.80
6	408.08	1	0	1	0	1	402	0	1.50	2	52.60

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	297.08	87.35	0.61	1.63	0.61	1.65	0		1	.
6	298.08	75.88	0.68	1.48	0.68	1.48	1	2	0	1.59
6	300.08	98.69	0.64	1.57	0.64	1.57	1	3	0	1.59
6	303.08	103.47	0.54	1.85	0.54	1.85	1	1	0	1.82
6	305.08	102.37	0.55	1.82	0.55	1.82	1	4	0	1.59
6	307.08	104.40	0.56	1.78	0.55	1.82	0		1	.
6	308.08	100.73	0.52	1.91	0.52	1.91	1	3	0	1.82
6	315.08	106.37	0.54	1.86	0.54	1.85	0		1	.
6	316.08	45.88	0.54	1.87	0.54	1.87	1	1	0	1.85
6	323.08	87.06	0.50	2.00	0.50	2.00	1	4	0	1.87
6	325.08	108.49	0.47	2.13	0.47	2.13	1	4	0	2.00
6	327.08	110.07	0.47	2.15	0.47	2.15	1	4	0	2.13
6	333.08	113.21	0.44	2.27	0.44	2.27	1	4	0	2.25
6	334.08	112.04	0.44	2.25	0.44	2.25	1	4	0	2.15
6	341.08	51.95	0.40	2.50	0.40	2.50	1	2	0	2.71
6	344.08	114.71	0.39	2.57	0.39	2.57	1	4	0	2.27
6	345.08	114.94	0.39	2.54	0.39	2.54	1	4	0	2.57
6	346.08	117.78	0.39	2.55	0.39	2.56	0		1	.
6	348.08	56.39	0.37	2.68	0.37	2.68	1	3	0	2.71
6	349.08	54.46	0.39	2.56	0.39	2.56	1	4	0	2.54
6	350.08	119.68	0.38	2.61	0.38	2.61	1	4	0	2.56
6	352.08	124.62	0.37	2.71	0.37	2.71	1	4	0	2.61
6	354.08	55.02	0.34	2.94	0.34	2.94	1	2	0	2.93
6	367.08	94.90	0.34	2.93	0.34	2.93	1	1	0	2.96
6	368.08	89.39	0.34	2.96	0.34	2.96	1	4	0	2.71
6	372.08	51.35	0.31	3.18	0.32	3.12	0		1	.
6	373.08	50.85	0.31	3.22	0.32	3.12	0		0	.
6	374.08	53.62	0.30	3.33	0.30	3.33	1	3	0	3.12
6	375.08	49.18	0.32	3.12	0.32	3.12	1	4	0	2.93
6	376.08	57.79	0.30	3.33	0.30	3.33	1	1	0	3.12
6	377.08	57.39	0.30	3.32	0.30	3.33	0		1	.
6	378.08	93.06	0.34	2.97	0.34	2.96	0		1	.
6	379.08	94.70	0.34	2.98	0.34	2.96	0		0	.
6	381.08	60.20	0.28	3.62	0.28	3.62	1	4	0	3.33
6	382.08	59.33	0.28	3.56	0.28	3.56	1	2	0	3.33
6	388.08	81.08	0.31	3.25	0.31	3.25	1	2	0	3.33
6	389.08	30.19	0.31	3.24	0.31	3.24	1	2	0	3.12
6	391.08	84.72	0.28	3.62	0.28	3.61	0		1	.
6	393.08	86.75	0.28	3.61	0.28	3.61	1	4	0	3.61
6	394.08	83.01	0.30	3.34	0.30	3.34	1	3	0	3.33
6	396.08	66.80	0.28	3.61	0.28	3.61	1	1	0	3.62
6	397.08	125.06	0.27	3.64	0.28	3.61	0		0	.
6	399.08	156.52	0.28	3.63	0.28	3.63	1	4	0	3.61
6	400.08	158.59	0.27	3.64	0.28	3.63	0		1	.
6	401.08	160.32	0.27	3.65	0.28	3.63	1	0	0	.
6	402.08	161.96	0.27	3.65	0.27	3.65	1	4	0	3.63
6	403.08	128.60	0.28	3.59	0.27	3.65	0		1	.
6	406.08	72.11	0.28	3.60	0.27	3.65	0		0	.
6	407.08	69.80	0.29	3.46	0.29	3.46	1	2	0	3.65
6	408.08	104.13	0.28	3.62	0.27	3.65	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	409.08	1	1	1	0	1	402	0	1.50	1	62.80
6	410.08	1	.	1	0	1	410	0	1.50	2	52.60
6	411.08	0	.	1	0	2	411	0	1.50	0	52.60
6	412.08	1	.	1	0	2	412	0	1.07	2	22.00
6	413.08	1	.	1	0	2	413	0	0.64	2	22.00
6	414.08	1	.	1	0	2	414	0	1.07	2	22.00
6	415.08	1	.	1	0	1	415	0	1.29	2	93.40
6	417.08	0	.	1	0	1	417	0	1.29	1	62.80
6	418.08	0	.	1	0	1	418	0	1.29	1	62.80
6	419.08	0	0	0	0	2	417	0	1.71	1	62.80
6	420.08	0	.	1	0	3	420	0	1.29	1	62.80
6	421.08	1	0	0	0	1	423	0	1.50	2	22.00
6	422.08	1	.	1	0	1	422	0	1.50	0	52.60
6	423.08	1	.	1	0	1	423	0	1.29	1	22.00
6	424.08	1	.	1	0	1	424	0	1.71	0	52.60
6	425.08	0	.	1	0	1	425	0	1.29	0	52.60
6	428.08	1	.	1	0	1	428	1	1.50	2	52.60
6	429.08	0	1	1	0	1	434	0	1.50	0	62.80
6	432.08	0	.	1	0	1	432	0	1.71	1	42.40
6	433.08	1	.	1	0	1	433	0	1.71	1	42.40
6	434.08	1	.	1	1	1	434	1	1.71	1	62.80
6	435.08	1	0	1	0	1	434	1	1.29	1	42.40
6	436.08	1	.	1	0	1	436	0	1.29	2	52.60
6	437.08	0	1	0	0	1	428	1	1.71	2	52.60
6	438.08	1	1	1	1	1	440	1	1.29	2	52.60
6	439.08	1	.	1	0	2	439	0	0.64	1	52.60
6	440.08	0	.	1	0	1	440	1	1.07	2	62.80
6	441.08	0	.	1	0	1	441	0	1.29	1	62.80
6	442.08	1	.	1	0	1	442	0	1.07	0	62.80
6	443.08	0	0	1	0	1	441	0	1.07	2	62.80
6	445.08	0	.	1	0	1	445	0	0.86	2	62.80
6	446.08	1	.	1	0	1	446	0	1.29	1	52.60
6	447.08	0	.	0	0	1	447	0	1.50	0	52.60
6	448.08	0	0	1	0	1	449	0	1.71	1	42.40
6	449.08	0	.	0	0	1	449	0	1.29	0	42.40
6	450.08	1	.	1	0	1	450	0	1.29	1	62.80
6	451.08	0	.	1	0	1	451	0	1.71	0	62.80
6	452.08	1	1	1	0	1	451	0	1.50	1	83.20
6	453.08	1	0	1	0	1	451	0	1.93	0	83.20
6	454.08	0	0	1	0	1	451	0	1.50	1	52.60
6	455.08	1	0	1	0	1	451	0	1.50	0	83.20
6	456.08	0	1	1	0	1	451	0	1.50	1	42.40
6	457.08	0	1	1	0	2	451	0	1.29	2	52.60
6	458.08	1	1	1	0	1	451	0	1.50	1	52.60
6	459.08	1	0	1	0	1	451	0	1.50	2	83.20
6	460.08	1	0	0	0	1	451	0	1.50	0	83.20
6	461.08	0	.	1	0	1	461	0	0.86	1	62.80
6	462.08	0	1	1	0	1	463	0	1.50	1	62.80
6	463.08	1	.	1	1	3	463	0	0.86	1	62.80
6	464.08	1	0	0	0	1	463	0	1.07	0	62.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	409.08	70.44	0.28	3.58	0.27	3.65	0		0	.
6	410.08	107.87	0.27	3.69	0.27	3.69	1	3	0	3.65
6	411.08	110.87	0.28	3.60	0.28	3.60	1	3	0	3.65
6	412.08	145.48	0.28	3.60	0.28	3.60	1	1	0	3.65
6	413.08	148.35	0.29	3.42	0.29	3.42	1	1	0	3.60
6	414.08	148.75	0.30	3.33	0.30	3.33	1	1	0	3.42
6	415.08	67.46	0.35	2.89	0.35	2.89	1	1	0	3.16
6	417.08	77.45	0.32	3.16	0.32	3.16	1	1	0	3.33
6	418.08	73.64	0.29	3.40	0.29	3.40	1	3	0	3.16
6	419.08	74.91	0.32	3.17	0.32	3.16	0		1	.
6	420.08	79.21	0.34	2.90	0.34	2.90	1	2	0	2.89
6	421.08	169.64	0.30	3.29	0.30	3.28	0		1	.
6	422.08	131.23	0.35	2.85	0.35	2.85	1	0	0	2.82
6	423.08	168.32	0.30	3.28	0.30	3.28	1	3	0	2.89
6	424.08	144.78	0.37	2.72	0.37	2.72	1	2	0	2.85
6	425.08	140.90	0.36	2.80	0.36	2.80	1	2	0	2.85
6	428.08	140.14	0.32	3.11	0.32	3.11	1	3	0	2.85
6	429.08	84.32	0.33	3.04	0.33	3.05	0		0	.
6	432.08	132.13	0.35	2.89	0.35	2.89	1	3	0	2.85
6	433.08	129.16	0.34	2.95	0.34	2.95	1	3	0	2.85
6	434.08	80.98	0.33	3.05	0.33	3.05	1	2	0	2.85
6	435.08	147.34	0.34	2.90	0.33	3.05	0		1	.
6	436.08	123.82	0.35	2.82	0.35	2.82	1	0	0	2.89
6	437.08	142.87	0.32	3.09	0.32	3.11	0		1	.
6	438.08	126.46	0.31	3.25	0.31	3.24	0		1	.
6	439.08	121.62	0.31	3.25	0.31	3.25	1	3	0	2.85
6	440.08	66.27	0.31	3.24	0.31	3.24	1	3	0	2.85
6	441.08	90.66	0.37	2.72	0.37	2.72	1	1	0	2.85
6	442.08	95.70	0.38	2.63	0.38	2.63	1	2	0	2.72
6	443.08	88.36	0.36	2.77	0.37	2.72	0		1	.
6	445.08	93.33	0.36	2.77	0.36	2.77	1	3	0	2.72
6	446.08	127.99	0.27	3.77	0.27	3.77	1	3	0	2.72
6	447.08	129.19	0.27	3.67	0.27	3.67	1	1	0	2.72
6	448.08	152.22	0.36	2.77	0.36	2.79	0		1	.
6	449.08	150.51	0.36	2.79	0.36	2.79	1	1	0	3.67
6	450.08	97.70	0.33	3.02	0.33	3.02	1	2	0	2.79
6	451.08	100.27	0.32	3.11	0.32	3.11	1	1	0	2.79
6	452.08	69.03	0.32	3.12	0.32	3.11	0		0	.
6	453.08	70.27	0.32	3.12	0.32	3.11	0		0	.
6	454.08	157.32	0.32	3.08	0.32	3.11	0		1	.
6	455.08	75.20	0.32	3.17	0.32	3.11	0		0	.
6	456.08	163.96	0.31	3.19	0.32	3.11	0		0	.
6	457.08	183.31	0.32	3.13	0.32	3.11	0		0	.
6	458.08	163.19	0.31	3.18	0.32	3.11	0		0	.
6	459.08	72.17	0.31	3.21	0.32	3.11	0		0	.
6	460.08	73.70	0.32	3.15	0.32	3.11	0		0	.
6	461.08	93.83	0.31	3.27	0.31	3.27	1	3	0	2.79
6	462.08	104.24	0.32	3.11	0.32	3.12	0		0	.
6	463.08	102.20	0.32	3.12	0.32	3.12	1	0	0	3.11
6	464.08	102.20	0.32	3.15	0.32	3.12	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	465.08	0	.	0	1	1	465	0	1.71	2	83.20
6	466.08	0	.	1	0	1	466	0	1.50	0	11.80
6	469.08	1	0	1	0	1	466	0	1.29	2	93.40
6	470.08	1	.	1	0	1	470	0	1.29	2	93.40
6	471.08	1	1	1	0	1	466	0	1.71	1	52.60
6	472.08	0	.	0	0	1	472	0	1.50	1	52.60
6	473.08	1	0	1	0	1	486	1	1.93	1	11.80
6	474.08	1	0	1	0	2	470	0	0.64	2	93.40
6	476.08	1	.	1	0	1	476	0	2.14	1	62.80
6	477.08	1	.	1	0	1	477	0	1.07	2	93.40
6	478.08	1	0	1	0	1	477	0	1.07	2	62.80
6	479.08	0	1	0	0	1	476	0	1.93	1	11.80
6	481.08	1	.	1	0	2	481	0	0.86	2	62.80
6	482.08	1	1	1	0	1	489	0	1.50	2	73.00
6	483.08	1	.	1	0	1	483	1	1.93	2	93.40
6	484.08	1	0	1	0	1	481	0	0.86	1	93.40
6	485.08	1	0	1	0	1	483	1	2.36	2	93.40
6	486.08	1	.	1	0	1	486	1	1.29	1	93.40
6	487.08	1	1	1	0	2	476	0	1.50	2	93.40
6	488.08	1	0	1	0	1	476	0	1.71	2	93.40
6	489.08	0	.	1	0	2	489	0	1.50	1	93.40
6	490.08	1	0	1	0	1	489	0	1.50	1	62.80
6	491.08	0	1	1	0	1	489	0	1.71	1	62.80
6	492.08	1	0	1	0	1	489	0	1.71	1	62.80
6	493.08	1	.	1	0	1	493	0	2.14	1	62.80
6	494.08	0	.	0	0	1	494	0	1.93	2	62.80
6	495.08	1	.	1	0	1	495	0	1.93	1	62.80
6	496.08	1	1	1	0	1	495	0	1.71	1	62.80
6	497.08	0	1	1	0	1	495	0	2.14	2	62.80
6	498.08	0	.	1	0	1	498	0	0.64	0	62.80
6	499.08	1	0	1	1	1	495	0	1.93	2	52.60
6	500.08	1	0	1	0	1	495	0	2.14	1	52.60
6	501.08	0	.	1	0	.	501	0	1.07	0	32.20
6	502.08	1	.	1	0	3	502	0	0.64	0	93.40
6	503.08	1	0	1	0	2	495	0	1.71	0	62.80
6	504.08	1	.	1	0	.	504	0	0.43	1	73.00
6	505.08	1	.	1	0	.	505	0	0.86	2	52.60
6	506.08	1	.	1	0	1	506	0	0.64	1	73.00
6	507.08	0	1	0	0	1	506	0	0.86	2	73.00
6	508.08	0	1	0	0	1	505	0	0.43	1	52.60
6	511.08	0	.	1	0	2	511	0	1.07	2	42.40
6	514.08	0	.	0	0	.	514	0	0.43	2	93.40
6	516.08	1	.	1	0	1	516	0	0.86	0	52.60
6	517.08	1	1	0	1	1	451	0	1.07	1	42.40
6	277.09	1	.	1	0	.	277	0	0.64	1	11.80
6	284.09	1	.	1	0	.	284	0	0.43	1	42.40
6	296.09	0	.	1	0	1	296	0	0.64	2	11.80
6	298.09	1	.	1	0	1	298	0	0.64	2	1.60
6	316.09	0	.	1	0	2	316	1	0.64	2	42.40
6	323.09	1	1	1	0	1	316	1	0.86	2	11.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	465.08	77.54	0.32	3.13	0.32	3.13	1	4	0	3.12
6	466.08	294.86	0.31	3.20	0.31	3.20	1	4	0	3.13
6	469.08	93.42	0.31	3.19	0.31	3.20	0		0	.
6	470.08	95.02	0.32	3.17	0.32	3.17	1	2	0	3.20
6	471.08	184.62	0.31	3.18	0.31	3.20	0		1	.
6	472.08	183.35	0.31	3.28	0.31	3.28	1	3	0	3.20
6	473.08	326.92	0.34	2.92	0.34	2.94	0		1	.
6	474.08	97.26	0.32	3.15	0.32	3.17	0		1	.
6	476.08	145.65	0.34	2.92	0.34	2.92	1	1	0	2.96
6	477.08	100.33	0.32	3.14	0.32	3.14	1	1	0	3.20
6	478.08	137.17	0.33	3.04	0.32	3.14	0		1	.
6	479.08	336.53	0.34	2.94	0.34	2.92	0		1	.
6	481.08	134.24	0.34	2.96	0.34	2.96	1	0	0	3.14
6	482.08	154.89	0.33	3.02	0.33	3.00	0		1	.
6	483.08	109.27	0.35	2.89	0.35	2.89	1	2	0	2.96
6	484.08	106.97	0.34	2.95	0.34	2.96	0		1	.
6	485.08	108.17	0.35	2.90	0.35	2.89	0		1	.
6	486.08	101.80	0.34	2.94	0.34	2.94	1	3	0	2.96
6	487.08	111.47	0.34	2.98	0.34	2.92	0		0	.
6	488.08	114.24	0.33	2.99	0.34	2.92	0		0	.
6	489.08	115.18	0.33	3.00	0.33	3.00	1	4	0	2.92
6	490.08	141.31	0.33	3.06	0.33	3.00	0		0	.
6	491.08	151.72	0.33	3.05	0.33	3.00	0		0	.
6	492.08	149.82	0.33	3.05	0.33	3.00	0		0	.
6	493.08	171.01	0.33	3.04	0.33	3.04	1	3	0	3.00
6	494.08	169.54	0.34	2.97	0.34	2.97	1	2	0	3.00
6	495.08	175.61	0.33	3.01	0.33	3.01	1	1	0	3.00
6	496.08	178.61	0.33	3.02	0.33	3.01	0		0	.
6	497.08	180.88	0.33	3.00	0.33	3.01	0		1	.
6	498.08	82.68	0.15	6.73	0.33	3.01	1	3	0	.
6	499.08	244.17	0.34	2.96	0.33	3.01	0		0	.
6	500.08	252.18	0.35	2.89	0.33	3.01	0		0	.
6	501.08	409.05	0.63	1.59	0.63	1.59	1	0	0	3.01
6	502.08	203.53	0.32	3.09	0.32	3.09	1	3	0	1.59
6	503.08	233.50	0.34	2.91	0.33	3.01	0		0	.
6	504.08	351.62	0.61	1.63	0.61	1.63	1	2	0	1.59
6	505.08	377.94	0.49	2.04	0.49	2.04	1	0	0	1.64
6	506.08	350.59	0.61	1.64	0.61	1.64	1	1	0	1.63
6	507.08	354.03	0.60	1.66	0.61	1.64	0		1	.
6	508.08	377.57	0.49	2.04	0.49	2.04	0		1	.
6	511.08	250.01	0.31	3.27	0.31	3.27	1	3	0	1.59
6	514.08	429.03	0.53	1.87	0.53	1.87	1	0	1	2.04
6	516.08	138.87	0.29	3.47	0.29	3.47	1	3	0	2.79
6	517.08	167.13	0.32	3.10	0.32	3.11	0		0	.
6	277.09	55.73	0.73	1.38	0.73	1.38	1	0	0	.
6	284.09	44.25	0.89	1.12	0.89	1.12	1	2	0	1.38
6	296.09	61.50	0.60	1.66	0.60	1.66	1	3	0	1.38
6	298.09	75.88	0.80	1.25	0.80	1.25	1	1	0	1.38
6	316.09	45.88	0.83	1.21	0.83	1.21	1	1	0	1.25
6	323.09	87.06	0.78	1.29	0.83	1.21	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	341.09	0	.	1	0	1	341	0	1.50	1	42.40
6	348.09	1	.	1	0	1	348	0	1.29	1	42.40
6	349.09	0	.	0	0	1	349	0	1.50	1	42.40
6	354.09	1	1	1	0	1	341	0	1.71	1	42.40
6	367.09	0	.	0	0	2	367	0	1.50	2	1.60
6	368.09	0	.	0	0	2	368	0	0.64	0	1.60
6	372.09	1	1	1	0	1	367	0	1.29	0	42.40
6	373.09	1	0	0	0	1	367	0	1.50	2	42.40
6	374.09	1	0	1	0	1	341	0	1.29	2	42.40
6	375.09	0	0	1	0	2	367	0	0.64	2	42.40
6	376.09	1	1	0	0	1	341	0	1.07	2	42.40
6	377.09	1	0	0	0	1	341	0	1.29	0	42.40
6	378.09	1	1	1	0	1	368	0	1.29	1	1.60
6	379.09	0	1	1	0	1	368	0	1.29	2	11.80
6	381.09	0	1	1	0	1	394	0	1.29	2	42.40
6	382.09	1	1	1	0	1	394	0	1.07	1	42.40
6	388.09	1	1	1	0	1	394	0	0.64	1	22.00
6	389.09	0	1	1	0	1	341	0	1.29	1	62.80
6	391.09	1	1	1	0	2	393	0	0.86	1	22.00
6	393.09	0	.	0	0	1	393	0	0.64	2	22.00
6	394.09	0	.	0	0	3	394	0	0.64	2	22.00
6	396.09	0	.	1	0	2	396	0	1.07	1	42.40
6	397.09	0	1	0	0	1	393	0	0.86	2	11.80
6	403.09	0	0	1	0	1	406	0	1.07	2	11.80
6	406.09	0	.	1	0	1	406	0	0.86	0	42.40
6	407.09	1	.	1	0	1	407	0	1.07	0	42.40
6	408.09	1	.	1	0	1	408	0	1.07	2	32.20
6	409.09	1	.	1	0	1	409	0	0.86	1	42.40
6	410.09	1	0	1	0	1	408	0	0.86	2	32.20
6	411.09	0	1	1	0	2	408	0	1.07	2	32.20
6	412.09	1	.	1	0	3	412	0	0.43	2	1.60
6	413.09	1	.	1	0	2	413	0	0.43	2	1.60
6	414.09	1	.	1	0	1	414	0	0.86	2	1.60
6	415.09	1	0	1	0	1	439	0	1.29	1	73.00
6	417.09	0	.	1	0	3	417	0	0.86	2	42.40
6	418.09	0	.	1	0	1	418	0	0.64	1	42.40
6	419.09	0	.	0	0	2	419	0	1.29	1	42.40
6	420.09	0	.	1	0	1	420	0	1.07	1	42.40
6	421.09	1	0	0	0	1	423	0	1.50	0	1.60
6	422.09	1	0	1	0	1	440	1	1.50	2	32.20
6	423.09	1	.	1	0	2	423	0	0.86	1	1.60
6	424.09	1	.	1	0	1	424	0	1.07	1	32.20
6	425.09	0	1	1	0	1	432	0	1.50	2	32.20
6	428.09	1	1	1	0	1	432	0	1.29	2	32.20
6	429.09	0	.	1	0	1	429	0	1.29	1	42.40
6	432.09	0	.	1	0	1	432	0	1.50	0	22.00
6	433.09	1	1	1	0	1	432	0	1.71	1	22.00
6	434.09	1	0	1	1	1	432	0	1.50	1	42.40
6	435.09	1	1	1	0	2	429	0	1.07	1	22.00
6	436.09	1	0	1	0	1	440	1	1.50	2	32.20

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	341.09	51.95	0.61	1.65	0.61	1.65	1	1	0	1.68
6	348.09	56.39	0.73	1.37	0.73	1.37	1	2	0	1.68
6	349.09	54.46	0.65	1.55	0.65	1.55	1	1	0	1.21
6	354.09	55.02	0.63	1.58	0.61	1.65	0		1	.
6	367.09	94.90	0.60	1.68	0.60	1.68	1	3	0	1.68
6	368.09	89.39	0.59	1.68	0.59	1.68	1	1	0	1.55
6	372.09	51.35	0.59	1.68	0.60	1.68	0		0	.
6	373.09	50.85	0.60	1.68	0.60	1.68	0		0	.
6	374.09	53.62	0.61	1.65	0.61	1.65	0		0	.
6	375.09	49.18	0.59	1.68	0.60	1.68	0		1	.
6	376.09	57.79	0.60	1.66	0.61	1.65	0		0	.
6	377.09	57.39	0.60	1.66	0.61	1.65	0		0	.
6	378.09	93.06	0.60	1.66	0.59	1.68	0		1	.
6	379.09	94.70	0.60	1.67	0.59	1.68	0		0	.
6	381.09	60.20	0.65	1.54	0.67	1.50	0		0	.
6	382.09	59.33	0.64	1.56	0.67	1.50	0		0	.
6	388.09	81.08	0.65	1.53	0.67	1.50	0		1	.
6	389.09	30.19	0.60	1.66	0.61	1.65	0		0	.
6	391.09	84.72	0.72	1.39	0.71	1.40	0		1	.
6	393.09	86.75	0.71	1.40	0.71	1.40	1	1	0	1.48
6	394.09	83.01	0.67	1.50	0.67	1.50	1	0	0	1.65
6	396.09	66.80	0.68	1.48	0.68	1.48	1	1	0	1.50
6	397.09	125.06	0.73	1.38	0.71	1.40	0		0	.
6	403.09	128.60	0.52	1.92	0.51	1.97	0		1	.
6	406.09	72.11	0.51	1.97	0.51	1.97	1	1	0	1.40
6	407.09	69.80	0.54	1.85	0.54	1.85	1	1	0	1.84
6	408.09	104.13	0.54	1.84	0.54	1.84	1	1	0	1.90
6	409.09	70.44	0.53	1.90	0.53	1.90	1	1	0	1.97
6	410.09	107.87	0.56	1.80	0.54	1.84	0		1	.
6	411.09	110.87	0.54	1.87	0.54	1.84	0		0	.
6	412.09	145.48	0.59	1.68	0.59	1.68	1	0	0	1.85
6	413.09	148.35	0.48	2.07	0.48	2.07	1	0	0	1.68
6	414.09	148.75	0.44	2.26	0.44	2.26	1	0	0	2.07
6	415.09	67.46	0.45	2.21	0.44	2.27	0		1	.
6	417.09	77.45	0.48	2.09	0.48	2.09	1	3	0	2.26
6	418.09	73.64	0.59	1.70	0.59	1.70	1	2	0	2.26
6	419.09	74.91	0.51	1.95	0.51	1.95	1	1	0	2.26
6	420.09	79.21	0.44	2.25	0.44	2.25	1	0	0	2.27
6	421.09	169.64	0.53	1.87	0.52	1.92	0		1	.
6	422.09	131.23	0.39	2.58	0.37	2.68	0		0	.
6	423.09	168.32	0.52	1.92	0.52	1.92	1	1	0	1.95
6	424.09	144.78	0.43	2.32	0.43	2.32	1	1	0	2.43
6	425.09	140.90	0.41	2.41	0.41	2.43	0		0	.
6	428.09	140.14	0.42	2.38	0.41	2.43	0		0	.
6	429.09	84.32	0.48	2.08	0.48	2.08	1	1	0	2.32
6	432.09	132.13	0.41	2.43	0.41	2.43	1	1	0	2.25
6	433.09	129.16	0.41	2.47	0.41	2.43	0		1	.
6	434.09	80.98	0.42	2.38	0.41	2.43	0		0	.
6	435.09	147.34	0.49	2.02	0.48	2.08	0		1	.
6	436.09	123.82	0.40	2.53	0.37	2.68	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	437.09	0	1	0	0	1	432	0	1.29	2	32.20
6	438.09	1	1	1	1	1	440	1	1.50	2	32.20
6	439.09	1	.	1	0	1	439	0	1.07	1	32.20
6	440.09	0	.	1	0	1	440	1	0.86	2	42.40
6	441.09	0	.	1	0	1	441	1	1.07	1	42.40
6	442.09	1	.	1	0	1	442	0	1.50	2	42.40
6	443.09	0	.	1	0	1	443	1	1.07	2	42.40
6	445.09	0	0	1	0	1	443	1	1.07	2	42.40
6	446.09	1	.	1	0	1	446	1	1.50	1	32.20
6	447.09	0	1	0	0	1	446	1	1.50	1	32.20
6	448.09	0	0	1	0	1	442	0	1.93	1	22.00
6	449.09	0	1	0	0	1	442	0	1.50	1	22.00
6	450.09	1	1	1	0	1	442	0	1.93	1	42.40
6	451.09	0	1	1	0	1	442	0	1.93	2	42.40
6	452.09	1	1	1	0	1	442	0	1.93	2	62.80
6	453.09	1	1	1	0	1	442	0	2.14	2	62.80
6	454.09	0	0	1	0	1	442	0	2.14	1	32.20
6	455.09	1	0	1	0	1	442	0	1.29	0	62.80
6	456.09	0	1	1	0	1	442	0	1.71	1	22.00
6	457.09	0	.	1	0	1	457	0	1.07	2	32.20
6	458.09	1	0	1	0	1	442	0	2.14	1	32.20
6	459.09	1	0	1	0	1	442	0	1.71	2	62.80
6	460.09	1	0	0	0	2	442	0	1.07	2	62.80
6	461.09	0	0	1	0	1	441	1	1.07	1	42.40
6	462.09	0	1	1	0	1	463	0	1.50	1	42.40
6	463.09	1	.	1	1	3	463	0	1.29	1	42.40
6	464.09	1	0	0	0	1	463	0	1.50	2	42.40
6	465.09	0	0	0	1	1	463	0	2.14	2	62.80
6	469.09	1	.	1	0	1	469	0	1.29	2	73.00
6	470.09	1	.	1	0	1	470	0	1.50	2	73.00
6	471.09	1	.	1	0	1	471	0	1.71	1	32.20
6	472.09	0	.	0	0	1	472	0	1.71	1	32.20
6	474.09	1	0	1	0	2	470	0	0.64	2	73.00
6	476.09	1	0	1	0	1	485	0	1.71	1	42.40
6	477.09	1	0	1	0	1	470	0	0.86	2	73.00
6	478.09	1	0	1	0	1	470	0	0.86	2	42.40
6	481.09	1	0	1	0	2	470	0	0.86	2	42.40
6	482.09	1	.	1	0	1	482	1	1.29	2	52.60
6	483.09	1	0	1	0	1	470	0	1.93	2	73.00
6	484.09	1	0	1	0	1	470	0	0.86	1	73.00
6	485.09	1	.	1	0	1	485	0	1.93	2	73.00
6	486.09	1	0	1	0	1	470	0	1.29	1	73.00
6	487.09	1	0	1	0	1	485	0	1.71	2	73.00
6	488.09	1	.	1	0	1	488	0	1.29	2	73.00
6	489.09	0	.	1	0	2	489	0	1.29	2	73.00
6	490.09	1	.	1	0	1	490	1	1.50	1	42.40
6	491.09	0	1	1	0	1	490	1	1.93	1	42.40
6	492.09	1	0	1	0	1	490	1	1.71	1	42.40
6	493.09	1	1	1	0	1	490	1	2.14	1	42.40
6	494.09	0	1	0	0	1	482	1	2.14	2	42.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	437.09	142.87	0.41	2.42	0.41	2.43	0		0	.
6	438.09	126.46	0.39	2.55	0.37	2.68	0		1	.
6	439.09	121.62	0.44	2.27	0.44	2.27	1	0	0	1.92
6	440.09	66.27	0.37	2.68	0.37	2.68	1	3	0	2.25
6	441.09	90.66	0.40	2.50	0.40	2.50	1	2	0	2.08
6	442.09	95.70	0.38	2.60	0.38	2.60	1	1	0	2.08
6	443.09	88.36	0.38	2.60	0.38	2.60	1	3	0	2.08
6	445.09	93.33	0.38	2.64	0.38	2.60	0		1	.
6	446.09	127.99	0.46	2.17	0.46	2.17	1	2	0	2.25
6	447.09	129.19	0.43	2.30	0.46	2.17	0		1	.
6	448.09	152.22	0.39	2.57	0.38	2.60	0		0	.
6	449.09	150.51	0.39	2.57	0.38	2.60	0		1	.
6	450.09	97.70	0.39	2.55	0.38	2.60	0		0	.
6	451.09	100.27	0.40	2.53	0.38	2.60	0		0	.
6	452.09	69.03	0.40	2.49	0.38	2.60	0		0	.
6	453.09	70.27	0.40	2.49	0.38	2.60	0		0	.
6	454.09	157.32	0.39	2.58	0.38	2.60	0		0	.
6	455.09	75.20	0.40	2.52	0.38	2.60	0		0	.
6	456.09	163.96	0.39	2.53	0.38	2.60	0		0	.
6	457.09	183.31	0.40	2.53	0.40	2.53	1	2	0	2.60
6	458.09	163.19	0.40	2.49	0.38	2.60	0		0	.
6	459.09	72.17	0.39	2.54	0.38	2.60	0		0	.
6	460.09	73.70	0.40	2.52	0.38	2.60	0		0	.
6	461.09	93.83	0.41	2.42	0.40	2.50	0		1	.
6	462.09	104.24	0.37	2.69	0.37	2.67	0		0	.
6	463.09	102.20	0.37	2.67	0.37	2.67	1	0	0	2.60
6	464.09	102.20	0.37	2.72	0.37	2.67	0		1	.
6	465.09	77.54	0.36	2.75	0.37	2.67	0		0	.
6	469.09	93.42	0.38	2.64	0.38	2.64	1	2	0	2.70
6	470.09	95.02	0.38	2.64	0.38	2.64	1	1	0	2.70
6	471.09	184.62	0.37	2.70	0.37	2.70	1	1	0	2.67
6	472.09	183.35	0.36	2.77	0.36	2.77	1	3	0	2.70
6	474.09	97.26	0.37	2.68	0.38	2.64	0		1	.
6	476.09	145.65	0.30	3.29	0.31	3.22	0		1	.
6	477.09	100.33	0.37	2.73	0.38	2.64	0		0	.
6	478.09	137.17	0.34	2.93	0.38	2.64	0		0	.
6	481.09	134.24	0.31	3.18	0.38	2.64	0		0	.
6	482.09	154.89	0.32	3.08	0.32	3.08	1	3	0	3.14
6	483.09	109.27	0.31	3.22	0.38	2.64	0		0	.
6	484.09	106.97	0.31	3.18	0.38	2.64	0		0	.
6	485.09	108.17	0.31	3.22	0.31	3.22	1	4	0	2.64
6	486.09	101.80	0.31	3.19	0.38	2.64	0		0	.
6	487.09	111.47	0.31	3.23	0.31	3.22	0		0	.
6	488.09	114.24	0.31	3.21	0.31	3.21	1	4	0	3.22
6	489.09	115.18	0.32	3.14	0.32	3.14	1	1	0	3.21
6	490.09	141.31	0.33	3.04	0.33	3.04	1	2	0	3.14
6	491.09	151.72	0.33	3.02	0.33	3.04	0		0	.
6	492.09	149.82	0.33	3.04	0.33	3.04	0		1	.
6	493.09	171.01	0.32	3.10	0.33	3.04	0		0	.
6	494.09	169.54	0.31	3.19	0.32	3.08	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	495.09	1	0	1	0	1	490	1	2.14	1	42.40
6	496.09	1	0	1	0	1	496	0	2.14	1	42.40
6	497.09	0	0	1	0	1	482	1	1.93	2	42.40
6	498.09	0	.	1	0	1	498	0	0.86	2	42.40
6	499.09	1	0	1	1	1	496	0	1.71	2	32.20
6	500.09	1	0	1	0	1	496	0	2.14	1	32.20
6	501.09	0	.	1	0	.	501	0	0.43	0	11.80
6	502.09	1	.	1	0	3	502	0	0.64	0	73.00
6	503.09	1	.	1	0	1	503	0	1.50	0	42.40
6	504.09	1	.	1	0	.	504	0	0.43	1	52.60
6	505.09	1	.	1	0	.	505	0	0.86	2	32.20
6	506.09	1	.	1	0	.	506	0	0.43	1	52.60
6	507.09	0	1	0	0	1	506	0	0.86	2	52.60
6	508.09	0	1	0	0	1	505	0	0.43	1	32.20
6	511.09	0	.	1	0	1	511	0	1.07	2	22.00
6	514.09	0	.	0	0	.	514	0	0.43	0	73.00
6	516.09	1	.	1	0	.	516	0	0.43	1	32.20
6	517.09	1	.	0	1	1	517	0	1.07	1	22.00
6	284.1	1	.	1	0	.	284	0	0.43	2	22.00
6	316.1	0	.	1	0	.	316	0	0.43	2	22.00
6	341.1	0	.	1	0	1	341	0	1.29	1	22.00
6	348.1	1	0	1	0	1	373	0	1.29	1	22.00
6	349.1	0	.	0	0	1	349	0	0.86	0	22.00
6	354.1	1	.	1	0	1	354	0	1.29	0	22.00
6	372.1	1	1	1	0	1	375	0	1.29	0	22.00
6	373.1	1	.	0	0	1	373	0	1.29	2	22.00
6	374.1	1	.	1	0	2	374	0	1.07	2	22.00
6	375.1	0	.	1	0	2	375	0	0.43	2	22.00
6	376.1	1	1	0	0	1	389	0	1.71	2	22.00
6	377.1	1	.	0	0	1	377	0	1.50	0	22.00
6	381.1	0	.	1	0	1	381	0	1.50	2	22.00
6	382.1	1	.	1	0	1	382	0	1.50	1	22.00
6	388.1	1	.	1	0	1	388	0	0.64	1	1.60
6	389.1	0	.	1	0	2	389	0	1.29	1	42.40
6	391.1	1	.	1	0	1	391	0	1.29	1	1.60
6	393.1	0	.	0	0	1	393	0	1.07	0	1.60
6	394.1	0	.	0	0	2	394	0	1.07	0	1.60
6	396.1	0	.	1	0	2	396	0	1.07	0	22.00
6	406.1	0	.	1	0	2	406	0	0.64	0	22.00
6	407.1	1	.	1	0	3	407	0	0.64	0	22.00
6	408.1	1	.	1	0	3	408	0	0.43	2	11.80
6	409.1	1	.	1	0	.	409	0	0.43	1	22.00
6	410.1	1	.	1	0	2	410	0	0.43	2	11.80
6	411.1	0	.	1	0	2	411	0	0.64	2	11.80
6	415.1	1	.	1	0	1	415	0	2.14	2	52.60
6	417.1	0	.	1	0	2	417	0	0.43	2	22.00
6	418.1	0	.	1	0	1	418	0	0.86	0	22.00
6	419.1	0	0	0	0	1	418	0	1.29	0	22.00
6	420.1	0	1	1	0	1	438	0	1.50	0	22.00
6	422.1	1	.	1	0	1	422	1	1.71	2	11.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	495.09	175.61	0.32	3.10	0.33	3.04	0		0	.
6	496.09	178.61	0.32	3.12	0.32	3.12	0		0	3.14
6	497.09	180.88	0.32	3.16	0.32	3.08	0		0	.
6	498.09	82.68	0.43	2.31	0.43	2.31	1	3	0	2.08
6	499.09	244.17	0.31	3.27	0.32	3.12	0		0	.
6	500.09	252.18	0.30	3.28	0.32	3.12	0		0	.
6	501.09	409.05	1.19	0.84	1.19	0.84	1	0	0	2.91
6	502.09	203.53	0.34	2.91	0.34	2.91	1	0	0	3.12
6	503.09	233.50	0.32	3.14	0.32	3.14	1	2	0	3.12
6	504.09	351.62	0.65	1.55	0.65	1.55	1	0	0	0.84
6	505.09	377.94	0.54	1.87	0.54	1.87	1	0	0	1.64
6	506.09	350.59	0.61	1.64	0.61	1.64	1	0	0	1.55
6	507.09	354.03	0.62	1.60	0.61	1.64	0		1	.
6	508.09	377.57	0.54	1.87	0.54	1.87	0		1	.
6	511.09	250.01	0.29	3.39	0.29	3.39	1	3	0	3.12
6	514.09	429.03	0.49	2.06	0.49	2.06	1	0	0	1.87
6	516.09	138.87	0.35	2.84	0.35	2.84	1	3	0	2.08
6	517.09	167.13	0.37	2.73	0.37	2.73	1	3	0	2.60
6	284.1	44.25	1.57	0.64	1.57	0.64	1	0	0	.
6	316.1	45.88	0.99	1.01	0.99	1.01	1	0	0	0.64
6	341.1	51.95	0.82	1.22	0.82	1.22	1	1	0	1.26
6	348.1	56.39	0.81	1.24	0.79	1.26	0		1	.
6	349.1	54.46	1.30	0.77	1.30	0.77	1	0	0	1.01
6	354.1	55.02	0.76	1.31	0.76	1.31	1	3	0	1.22
6	372.1	51.35	0.79	1.26	0.78	1.28	0		1	.
6	373.1	50.85	0.79	1.26	0.79	1.26	1	1	0	1.28
6	374.1	53.62	0.82	1.21	0.82	1.21	1	2	0	1.22
6	375.1	49.18	0.78	1.28	0.78	1.28	1	1	0	0.77
6	376.1	57.79	0.82	1.22	0.81	1.24	0		1	.
6	377.1	57.39	0.84	1.19	0.84	1.19	1	1	0	1.24
6	381.1	60.20	0.68	1.47	0.68	1.47	1	2	0	1.19
6	382.1	59.33	0.66	1.51	0.66	1.51	1	3	0	1.19
6	388.1	81.08	0.63	1.59	0.63	1.59	1	3	0	1.19
6	389.1	30.19	0.81	1.24	0.81	1.24	1	1	0	1.22
6	391.1	84.72	0.56	1.79	0.56	1.79	1	3	0	1.43
6	393.1	86.75	0.62	1.62	0.62	1.62	1	3	0	1.43
6	394.1	83.01	0.70	1.44	0.70	1.44	1	2	0	1.19
6	396.1	66.80	0.70	1.42	0.70	1.42	1	2	0	1.43
6	406.1	72.11	0.60	1.67	0.60	1.67	1	1	0	1.43
6	407.1	69.80	0.80	1.24	0.80	1.24	1	0	0	1.34
6	408.1	104.13	0.68	1.46	0.68	1.46	1	0	0	1.45
6	409.1	70.44	0.69	1.45	0.69	1.45	1	0	0	1.67
6	410.1	107.87	0.69	1.44	0.69	1.44	1	1	0	1.46
6	411.1	110.87	0.74	1.34	0.74	1.34	1	1	0	1.44
6	415.1	67.46	0.47	2.15	0.47	2.15	1	2	0	2.39
6	417.1	77.45	0.52	1.92	0.52	1.92	1	0	0	1.24
6	418.1	73.64	0.51	1.95	0.51	1.95	1	1	0	1.92
6	419.1	74.91	0.51	1.95	0.51	1.95	0		1	.
6	420.1	79.21	0.42	2.36	0.43	2.32	0		1	.
6	422.1	131.23	0.45	2.22	0.45	2.22	1	2	0	2.39

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	424.1	1	.	1	0	1	424	1	1.50	0	11.80
6	425.1	0	.	1	0	1	425	1	1.50	0	11.80
6	428.1	1	.	1	0	1	428	1	1.07	2	11.80
6	429.1	0	.	1	0	1	429	1	1.50	0	22.00
6	432.1	0	1	1	0	1	422	1	1.93	2	1.60
6	433.1	1	1	1	0	1	446	1	1.71	1	1.60
6	434.1	1	0	1	1	1	446	1	1.71	1	22.00
6	435.1	1	.	1	0	1	435	0	1.29	1	1.60
6	436.1	1	.	1	0	1	436	0	1.71	1	11.80
6	437.1	0	.	0	0	1	437	1	1.29	0	11.80
6	438.1	1	.	1	1	1	438	0	1.50	0	11.80
6	439.1	1	.	1	0	1	439	0	1.29	1	11.80
6	440.1	0	.	1	0	1	440	0	0.64	2	22.00
6	441.1	0	0	1	0	1	435	0	1.50	1	22.00
6	442.1	1	.	1	0	1	442	0	2.14	2	22.00
6	443.1	0	1	1	0	1	435	0	1.50	2	22.00
6	445.1	0	.	1	0	1	445	0	1.71	2	22.00
6	446.1	1	.	1	0	1	446	1	1.93	1	11.80
6	447.1	0	1	0	0	1	446	1	1.71	1	11.80
6	448.1	0	.	1	0	1	448	0	1.93	0	1.60
6	449.1	0	.	0	0	1	449	0	1.93	1	1.60
6	450.1	1	1	1	0	2	448	0	2.36	1	22.00
6	451.1	0	1	1	0	1	448	0	2.14	2	22.00
6	452.1	1	1	1	0	1	448	0	2.14	2	42.40
6	453.1	1	1	1	0	1	448	0	2.57	2	42.40
6	454.1	0	0	1	0	1	448	0	2.14	1	11.80
6	455.1	1	.	1	0	1	455	0	1.93	0	42.40
6	456.1	0	1	1	0	1	448	0	1.93	1	1.60
6	457.1	0	.	1	0	1	457	0	1.50	2	11.80
6	458.1	1	0	1	0	1	448	0	2.36	1	11.80
6	459.1	1	0	1	0	1	448	0	2.79	2	42.40
6	460.1	1	0	0	0	1	455	0	1.71	2	42.40
6	461.1	0	0	1	0	1	445	0	1.50	1	22.00
6	462.1	0	.	1	0	1	462	0	2.14	1	22.00
6	463.1	1	.	1	1	1	463	0	1.93	1	22.00
6	464.1	1	.	0	0	1	464	0	2.14	2	22.00
6	465.1	0	.	0	1	1	465	0	1.71	2	42.40
6	469.1	1	.	1	0	1	469	0	1.29	2	52.60
6	470.1	1	0	1	0	1	469	0	1.50	2	52.60
6	471.1	1	.	1	0	1	471	0	1.71	0	11.80
6	472.1	0	.	0	0	1	472	0	1.93	1	11.80
6	474.1	1	0	1	0	2	469	0	0.86	2	52.60
6	476.1	1	.	1	0	1	476	0	1.50	1	22.00
6	477.1	1	0	1	0	1	469	0	0.86	2	52.60
6	478.1	1	0	1	0	1	469	0	0.86	2	22.00
6	481.1	1	0	1	0	2	469	0	1.29	2	22.00
6	482.1	1	.	1	0	2	482	1	1.29	2	32.20
6	483.1	1	0	1	0	1	469	0	1.93	2	52.60
6	484.1	1	0	1	0	1	469	0	1.07	2	52.60
6	485.1	1	.	1	0	1	485	0	2.14	2	52.60

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	424.1	144.78	0.45	2.24	0.45	2.24	1	2	0	2.20
6	425.1	140.90	0.48	2.08	0.48	2.08	1	2	0	2.39
6	428.1	140.14	0.44	2.28	0.44	2.28	1	2	0	2.39
6	429.1	84.32	0.38	2.62	0.38	2.62	1	1	0	2.63
6	432.1	132.13	0.43	2.30	0.45	2.22	0		1	.
6	433.1	129.16	0.41	2.43	0.41	2.46	0		0	.
6	434.1	80.98	0.40	2.53	0.41	2.46	0		0	.
6	435.1	147.34	0.37	2.67	0.37	2.67	1	1	0	2.62
6	436.1	123.82	0.39	2.54	0.39	2.54	1	3	0	2.39
6	437.1	142.87	0.45	2.20	0.45	2.20	1	1	0	2.39
6	438.1	126.46	0.43	2.32	0.43	2.32	1	3	0	2.39
6	439.1	121.62	0.42	2.39	0.42	2.39	1	1	0	1.95
6	440.1	66.27	0.39	2.55	0.39	2.55	1	3	0	1.95
6	441.1	90.66	0.37	2.73	0.37	2.67	0		0	.
6	442.1	95.70	0.37	2.71	0.37	2.71	1	2	0	2.74
6	443.1	88.36	0.36	2.75	0.37	2.67	0		1	.
6	445.1	93.33	0.37	2.74	0.37	2.74	1	1	0	2.67
6	446.1	127.99	0.41	2.46	0.41	2.46	1	3	0	2.39
6	447.1	129.19	0.41	2.43	0.41	2.46	0		1	.
6	448.1	152.22	0.35	2.83	0.35	2.83	1	1	0	2.74
6	449.1	150.51	0.33	3.06	0.33	3.06	1	3	0	2.74
6	450.1	97.70	0.35	2.84	0.35	2.83	0		1	.
6	451.1	100.27	0.36	2.81	0.35	2.83	0		0	.
6	452.1	69.03	0.35	2.86	0.35	2.83	0		0	.
6	453.1	70.27	0.36	2.77	0.35	2.83	0		0	.
6	454.1	157.32	0.35	2.86	0.35	2.83	0		0	.
6	455.1	75.20	0.39	2.56	0.39	2.56	1	1	0	2.83
6	456.1	163.96	0.34	2.90	0.35	2.83	0		0	.
6	457.1	183.31	0.38	2.65	0.38	2.65	1	2	0	2.56
6	458.1	163.19	0.35	2.83	0.35	2.83	0		0	.
6	459.1	72.17	0.37	2.71	0.35	2.83	0		0	.
6	460.1	73.70	0.39	2.59	0.39	2.56	0		1	.
6	461.1	93.83	0.36	2.76	0.37	2.74	0		1	.
6	462.1	104.24	0.34	2.93	0.34	2.93	1	1	0	2.56
6	463.1	102.20	0.35	2.89	0.35	2.89	1	3	0	2.56
6	464.1	102.20	0.35	2.82	0.35	2.82	1	3	0	2.56
6	465.1	77.54	0.36	2.76	0.36	2.76	1	1	0	2.93
6	469.1	93.42	0.34	2.94	0.34	2.94	1	1	0	2.76
6	470.1	95.02	0.34	2.93	0.34	2.94	0		1	.
6	471.1	184.62	0.34	2.91	0.34	2.91	1	2	0	2.76
6	472.1	183.35	0.32	3.14	0.32	3.14	1	3	0	2.76
6	474.1	97.26	0.34	2.92	0.34	2.94	0		0	.
6	476.1	145.65	0.41	2.41	0.41	2.41	1	2	0	2.94
6	477.1	100.33	0.34	2.91	0.34	2.94	0		0	.
6	478.1	137.17	0.40	2.52	0.34	2.94	0		0	.
6	481.1	134.24	0.40	2.51	0.34	2.94	0		0	.
6	482.1	154.89	0.37	2.69	0.37	2.69	1	2	0	2.65
6	483.1	109.27	0.40	2.51	0.34	2.94	0		0	.
6	484.1	106.97	0.40	2.52	0.34	2.94	0		0	.
6	485.1	108.17	0.39	2.54	0.39	2.54	1	3	0	2.94

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	486.1	1	0	1	0	1	469	0	1.29	1	52.60
6	487.1	1	0	1	0	1	485	0	1.29	2	52.60
6	488.1	1	.	1	0	1	488	0	1.50	2	52.60
6	489.1	0	.	1	0	1	489	0	1.29	2	52.60
6	490.1	1	.	1	0	1	490	1	1.71	1	22.00
6	491.1	0	1	1	0	1	490	1	1.93	1	22.00
6	492.1	1	0	1	0	1	490	1	1.71	1	22.00
6	493.1	1	1	1	0	1	490	1	1.50	0	22.00
6	494.1	0	1	0	0	1	482	1	1.71	2	22.00
6	495.1	1	.	1	0	1	495	1	1.50	1	22.00
6	496.1	1	0	1	0	1	495	1	1.71	1	22.00
6	497.1	0	0	1	0	2	482	1	1.29	2	22.00
6	498.1	0	.	1	0	1	498	1	1.29	2	22.00
6	499.1	1	.	1	1	1	499	0	1.07	2	11.80
6	500.1	1	.	1	0	1	500	0	1.50	1	11.80
6	502.1	1	.	1	0	.	502	0	0.43	2	52.60
6	503.1	1	.	1	0	1	503	0	0.86	0	22.00
6	504.1	1	.	1	0	.	504	0	0.86	1	32.20
6	505.1	1	.	1	0	.	505	0	0.86	2	11.80
6	506.1	1	.	1	0	.	506	0	1.07	1	32.20
6	507.1	0	1	0	0	1	506	0	1.29	2	32.20
6	508.1	0	1	0	0	1	505	0	0.43	1	11.80
6	511.1	0	.	1	0	1	511	0	0.64	2	1.60
6	514.1	0	.	0	0	.	514	0	0.43	2	52.60
6	516.1	1	.	1	0	3	516	1	0.64	1	11.80
6	517.1	1	.	0	1	1	517	0	1.93	1	1.60
6	519.1	1	.	1	0	1	519	0	1.29	2	22.00
6	284.11	1	.	1	0	.	284	0	0.43	2	1.60
6	316.11	0	.	1	0	.	316	0	0.43	2	1.60
6	341.11	0	.	1	0	1	341	0	1.07	1	1.60
6	348.11	1	.	1	0	1	348	0	1.71	1	1.60
6	349.11	0	.	0	0	1	349	0	1.29	1	1.60
6	354.11	1	.	1	0	1	354	0	1.29	0	1.60
6	372.11	1	.	1	0	1	372	0	1.29	1	1.60
6	373.11	1	.	0	0	1	373	0	1.07	2	1.60
6	374.11	1	.	1	0	2	374	0	1.07	2	1.60
6	375.11	0	.	1	0	2	375	0	0.43	2	1.60
6	376.11	1	.	0	0	1	376	0	1.71	2	1.60
6	377.11	1	.	0	0	1	377	1	1.71	1	1.60
6	381.11	0	1	1	0	1	377	1	1.29	0	1.60
6	382.11	1	0	1	0	1	377	1	1.50	0	1.60
6	389.11	0	.	1	0	1	389	0	1.07	0	22.00
6	396.11	0	.	1	0	2	396	0	1.07	1	1.60
6	406.11	0	.	1	0	1	406	0	0.86	1	1.60
6	407.11	1	.	1	0	2	407	0	0.86	2	1.60
6	409.11	1	.	1	0	1	409	0	0.86	1	1.60
6	415.11	1	.	1	0	1	415	0	1.50	2	32.20
6	417.11	0	.	1	0	2	417	0	0.64	2	1.60
6	418.11	0	.	1	0	1	418	0	1.29	2	1.60
6	419.11	0	0	0	0	1	418	0	1.71	2	1.60

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	486.1	101.80	0.39	2.55	0.34	2.94	0		0	.
6	487.1	111.47	0.39	2.57	0.39	2.54	0		1	.
6	488.1	114.24	0.38	2.60	0.38	2.60	1	1	0	2.94
6	489.1	115.18	0.38	2.65	0.38	2.65	1	0	0	2.60
6	490.1	141.31	0.34	2.98	0.34	2.98	1	3	0	2.65
6	491.1	151.72	0.33	3.01	0.34	2.98	0		0	.
6	492.1	149.82	0.34	2.97	0.34	2.98	0		1	.
6	493.1	171.01	0.35	2.86	0.34	2.98	0		0	.
6	494.1	169.54	0.37	2.71	0.37	2.69	0		1	.
6	495.1	175.61	0.36	2.77	0.36	2.77	1	3	0	2.65
6	496.1	178.61	0.36	2.78	0.36	2.77	0		1	.
6	497.1	180.88	0.39	2.56	0.37	2.69	0		0	.
6	498.1	82.68	0.38	2.63	0.38	2.63	1	1	0	2.20
6	499.1	244.17	0.40	2.50	0.40	2.50	1	1	0	2.65
6	500.1	252.18	0.43	2.33	0.43	2.33	1	1	0	2.50
6	502.1	203.53	0.48	2.07	0.48	2.07	1	2	0	2.19
6	503.1	233.50	0.46	2.19	0.46	2.19	1	1	0	2.34
6	504.1	351.62	0.63	1.58	0.63	1.58	1	0	0	2.19
6	505.1	377.94	0.49	2.05	0.49	2.05	1	0	0	1.72
6	506.1	350.59	0.58	1.72	0.58	1.72	1	0	0	1.58
6	507.1	354.03	0.57	1.74	0.58	1.72	0		1	.
6	508.1	377.57	0.50	2.01	0.49	2.05	0		1	.
6	511.1	250.01	0.43	2.34	0.43	2.34	1	1	0	2.33
6	514.1	429.03	0.48	2.07	0.48	2.07	1	2	0	2.05
6	516.1	138.87	0.36	2.78	0.36	2.78	1	3	0	2.20
6	517.1	167.13	0.35	2.84	0.35	2.84	1	3	0	2.56
6	519.1	62.23	0.70	1.43	0.70	1.43	1	1	0	1.19
6	284.11	44.25	1.39	0.72	1.39	0.72	1	0	0	.
6	316.11	45.88	1.16	0.86	1.16	0.86	1	0	0	0.72
6	341.11	51.95	0.78	1.28	0.78	1.28	1	3	0	1.20
6	348.11	56.39	0.98	1.02	0.98	1.02	1	2	0	1.20
6	349.11	54.46	0.95	1.05	0.95	1.05	1	2	0	1.20
6	354.11	55.02	0.90	1.11	0.90	1.11	1	3	0	1.20
6	372.11	51.35	0.83	1.20	0.83	1.20	1	1	0	1.21
6	373.11	50.85	0.82	1.22	0.82	1.22	1	3	0	1.20
6	374.11	53.62	0.78	1.28	0.78	1.28	1	3	0	1.20
6	375.11	49.18	0.83	1.21	0.83	1.21	1	1	0	0.86
6	376.11	57.79	0.84	1.20	0.84	1.20	1	1	0	1.26
6	377.11	57.39	0.80	1.25	0.80	1.25	1	4	0	1.20
6	381.11	60.20	0.79	1.26	0.80	1.25	0		0	.
6	382.11	59.33	0.78	1.29	0.80	1.25	0		1	.
6	389.11	30.19	0.79	1.26	0.79	1.26	1	1	0	1.20
6	396.11	66.80	0.90	1.12	0.90	1.12	1	1	0	1.27
6	406.11	72.11	1.03	0.97	1.03	0.97	1	2	0	1.12
6	407.11	69.80	0.49	2.03	0.49	2.03	1	2	0	1.12
6	409.11	70.44	0.67	1.49	0.67	1.49	1	3	0	1.12
6	415.11	67.46	0.47	2.12	0.47	2.12	1	2	0	2.35
6	417.11	77.45	0.48	2.10	0.48	2.10	1	2	0	1.12
6	418.11	73.64	0.41	2.42	0.41	2.42	1	3	0	1.12
6	419.11	74.91	0.42	2.40	0.41	2.42	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	420.11	0	.	1	0	1	420	0	1.29	0	1.60
6	429.11	0	.	1	0	1	429	0	1.29	0	1.60
6	434.11	1	.	1	1	1	434	0	1.71	0	1.60
6	440.11	0	.	1	0	1	440	0	0.43	2	1.60
6	441.11	0	0	1	0	1	443	0	1.29	1	1.60
6	442.11	1	.	1	0	2	442	0	1.93	1	1.60
6	443.11	0	.	1	0	1	443	0	1.50	2	1.60
6	445.11	0	.	1	0	1	445	0	1.50	2	1.60
6	450.11	1	.	1	0	2	450	0	1.93	1	1.60
6	451.11	0	.	1	0	1	451	0	1.50	0	1.60
6	452.11	1	.	1	0	1	452	0	1.50	2	22.00
6	453.11	1	0	1	0	1	452	0	2.57	2	22.00
6	455.11	1	.	1	0	1	455	0	2.14	2	22.00
6	459.11	1	.	1	0	1	459	0	2.57	2	22.00
6	460.11	1	.	0	0	1	460	0	1.93	2	22.00
6	461.11	0	0	1	0	1	445	0	1.50	1	1.60
6	462.11	0	.	1	0	1	462	0	2.57	1	1.60
6	463.11	1	.	1	1	1	463	0	2.14	1	1.60
6	464.11	1	0	0	0	1	463	0	2.36	0	1.60
6	465.11	0	.	0	1	1	465	0	1.29	2	22.00
6	469.11	1	.	1	0	1	469	0	0.86	2	32.20
6	470.11	1	0	1	0	1	469	0	1.07	2	32.20
6	474.11	1	0	1	0	2	469	0	0.64	2	32.20
6	476.11	1	.	1	0	1	476	0	1.71	1	1.60
6	477.11	1	.	1	0	1	477	0	0.64	2	32.20
6	478.11	1	.	1	0	1	478	0	0.86	2	1.60
6	481.11	1	.	1	0	2	481	0	1.07	2	1.60
6	482.11	1	1	1	0	1	488	0	1.50	2	11.80
6	483.11	1	0	1	0	1	484	0	2.14	2	32.20
6	484.11	1	.	1	0	1	484	0	1.07	0	32.20
6	485.11	1	.	1	0	1	485	0	2.36	2	32.20
6	486.11	1	0	1	0	1	484	0	1.29	1	32.20
6	487.11	1	0	1	0	1	485	0	1.71	2	32.20
6	488.11	1	.	1	0	1	488	0	1.93	2	32.20
6	489.11	0	1	1	0	1	488	0	1.71	2	32.20
6	490.11	1	0	1	0	1	488	0	1.29	1	1.60
6	491.11	0	0	1	0	1	488	0	1.71	1	1.60
6	492.11	1	0	1	0	1	488	0	1.71	1	1.60
6	493.11	1	.	1	0	1	493	0	0.86	0	1.60
6	494.11	0	.	0	0	2	494	0	0.64	2	1.60
6	495.11	1	.	1	0	2	495	0	0.43	2	1.60
6	496.11	1	.	1	0	1	496	0	0.64	2	1.60
6	497.11	0	1	1	0	2	496	0	0.86	2	1.60
6	498.11	0	.	1	0	2	498	0	1.29	2	1.60
6	502.11	1	.	1	0	.	502	0	0.43	2	32.20
6	503.11	1	.	1	0	.	503	0	0.43	0	1.60
6	504.11	1	.	1	0	.	504	0	1.07	1	11.80
6	506.11	1	.	1	0	3	506	0	1.07	1	11.80
6	507.11	0	1	0	0	1	506	0	1.29	2	11.80
6	514.11	0	.	0	0	.	514	0	0.43	2	32.20

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	420.11	79.21	0.43	2.35	0.43	2.35	1	4	0	1.12
6	429.11	84.32	0.33	3.02	0.33	3.02	1	4	0	3.02
6	434.11	80.98	0.36	2.75	0.36	2.75	1	4	0	2.35
6	440.11	66.27	0.41	2.45	0.41	2.45	1	3	0	1.12
6	441.11	90.66	0.34	2.95	0.34	2.98	0		1	.
6	442.11	95.70	0.34	2.94	0.34	2.94	1	0	0	2.92
6	443.11	88.36	0.34	2.98	0.34	2.98	1	1	0	3.02
6	445.11	93.33	0.34	2.92	0.34	2.92	1	1	0	2.98
6	450.11	97.70	0.33	3.00	0.33	3.00	1	4	0	2.94
6	451.11	100.27	0.34	2.98	0.34	2.98	1	1	0	3.00
6	452.11	69.03	0.32	3.11	0.32	3.11	1	4	0	2.98
6	453.11	70.27	0.32	3.14	0.32	3.11	0		1	.
6	455.11	75.20	0.32	3.17	0.32	3.17	1	2	0	3.11
6	459.11	72.17	0.31	3.18	0.31	3.18	1	2	0	3.11
6	460.11	73.70	0.30	3.31	0.30	3.31	1	3	0	3.11
6	461.11	93.83	0.35	2.90	0.34	2.92	0		1	.
6	462.11	104.24	0.28	3.57	0.28	3.57	1	4	0	3.11
6	463.11	102.20	0.28	3.62	0.28	3.62	1	3	0	3.11
6	464.11	102.20	0.27	3.66	0.28	3.62	0		1	.
6	465.11	77.54	0.28	3.52	0.28	3.52	1	4	0	3.57
6	469.11	93.42	0.30	3.36	0.30	3.36	1	1	0	3.52
6	470.11	95.02	0.29	3.41	0.30	3.36	0		1	.
6	474.11	97.26	0.29	3.42	0.30	3.36	0		0	.
6	476.11	145.65	0.27	3.65	0.27	3.65	1	3	0	3.48
6	477.11	100.33	0.30	3.38	0.30	3.38	1	1	0	3.36
6	478.11	137.17	0.29	3.41	0.29	3.41	1	2	0	3.38
6	481.11	134.24	0.27	3.64	0.27	3.64	1	3	0	3.38
6	482.11	154.89	0.28	3.54	0.28	3.56	0		0	.
6	483.11	109.27	0.29	3.46	0.29	3.47	0		0	.
6	484.11	106.97	0.29	3.47	0.29	3.47	1	1	0	3.38
6	485.11	108.17	0.29	3.48	0.29	3.48	1	1	0	3.47
6	486.11	101.80	0.29	3.44	0.29	3.47	0		1	.
6	487.11	111.47	0.28	3.52	0.29	3.48	0		1	.
6	488.11	114.24	0.28	3.56	0.28	3.56	1	1	0	3.48
6	489.11	115.18	0.28	3.57	0.28	3.56	0		0	.
6	490.11	141.31	0.28	3.54	0.28	3.56	0		1	.
6	491.11	151.72	0.28	3.53	0.28	3.56	0		0	.
6	492.11	149.82	0.28	3.54	0.28	3.56	0		0	.
6	493.11	171.01	0.33	2.99	0.33	2.99	1	2	0	3.56
6	494.11	169.54	0.32	3.16	0.32	3.16	1	3	0	3.56
6	495.11	175.61	0.33	2.99	0.33	2.99	1	1	0	3.56
6	496.11	178.61	0.34	2.90	0.34	2.90	1	1	0	2.99
6	497.11	180.88	0.35	2.89	0.34	2.90	0		1	.
6	498.11	82.68	0.33	3.02	0.33	3.02	1	1	0	2.75
6	502.11	203.53	0.59	1.69	0.59	1.69	1	0	0	1.25
6	503.11	233.50	0.80	1.25	0.80	1.25	1	0	0	2.90
6	504.11	351.62	0.62	1.62	0.62	1.62	1	0	0	1.69
6	506.11	350.59	0.60	1.66	0.60	1.66	1	0	0	1.62
6	507.11	354.03	0.61	1.63	0.60	1.66	0		1	.
6	514.11	429.03	0.53	1.89	0.53	1.89	1	0	0	1.66

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
6	515.11	1	.	0	0	.	515	0	0.43	2	1.60
6	519.11	1	.	1	0	1	519	0	1.07	0	1.60
6	389.12	0	.	1	0	1	389	0	0.64	2	1.60
6	415.12	1	.	1	0	1	415	0	0.43	2	11.80
6	452.12	1	.	1	0	1	452	0	0.86	2	1.60
6	453.12	1	0	1	0	1	452	0	1.50	1	1.60
6	455.12	1	0	1	0	1	460	0	1.29	0	1.60
6	459.12	1	.	1	0	1	459	0	1.50	0	1.60
6	460.12	1	.	0	0	1	460	0	1.29	0	1.60
6	465.12	0	1	0	1	2	460	0	1.07	0	1.60
6	469.12	1	.	1	0	.	469	0	0.43	2	11.80
6	470.12	1	0	1	0	1	469	0	0.86	2	11.80
6	474.12	1	.	1	0	2	474	0	0.43	2	11.80
6	477.12	1	.	1	0	3	477	0	0.43	2	11.80
6	483.12	1	.	1	0	1	483	0	1.50	2	11.80
6	484.12	1	.	1	0	3	484	0	0.64	2	11.80
6	485.12	1	.	1	0	1	485	0	1.50	1	11.80
6	486.12	1	.	1	0	1	486	0	1.07	0	11.80
6	487.12	1	.	1	0	2	487	0	1.29	0	11.80
6	488.12	1	.	1	0	1	488	0	1.07	1	11.80
6	489.12	0	.	1	0	1	489	0	1.50	2	11.80
6	502.12	1	.	1	0	.	502	0	0.43	0	11.80
6	514.12	0	.	0	0	.	514	0	0.43	0	11.80
7	1.01	1	.	0	0	1	1	0	0.64	0	1.60
7	2.01	1	.	0	0	3	2	0	0.43	1	1.60
7	3.01	0	.	0	0	.	3	0	0.43	0	32.20
7	4.01	0	.	0	0	2	4	0	0.86	2	42.40
7	5.01	1	0	1	0	1	7	0	0.86	2	1.60
7	6.01	1	.	1	0	2	6	0	1.07	0	1.60
7	7.01	1	.	1	0	.	7	0	0.43	1	1.60
7	8.01	1	.	1	0	.	8	0	0.64	0	1.60
7	9.01	1	0	0	1	1	8	0	1.29	2	1.60
7	10.01	1	0	0	0	2	8	0	0.86	1	1.60
7	11.01	1	0	1	0	1	8	0	1.07	1	1.60
7	12.01	0	.	0	0	1	12	0	1.71	2	1.60
7	16.01	0	.	0	0	1	16	0	1.07	2	1.60
7	17.01	1	.	1	0	1	17	0	1.29	1	1.60
7	18.01	0	.	0	0	2	18	0	1.07	1	42.40
7	19.01	1	1	1	0	1	18	0	1.07	1	42.40
7	20.01	1	0	1	0	1	18	0	1.50	1	22.00
7	23.01	0	.	0	0	1	23	0	1.07	2	22.00
7	24.01	1	1	1	0	1	23	0	0.86	1	22.00
7	25.01	1	0	0	0	1	23	0	1.29	2	73.00
7	27.01	1	.	1	0	1	27	0	1.29	1	1.60
7	28.01	1	.	1	0	1	28	0	1.07	2	22.00
7	30.01	0	.	1	0	1	30	0	1.71	1	32.20
7	31.01	0	.	0	0	1	31	0	1.29	1	22.00
7	32.01	1	1	1	0	1	30	0	1.50	2	42.40
7	33.01	0	.	0	0	1	33	0	1.29	1	22.00
7	34.01	0	1	0	0	1	30	0	1.50	1	22.00

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
6	515.11	1170.84	0.63	1.58	0.63	1.58	1	0	0	1.89
6	519.11	62.23	0.79	1.27	0.79	1.27	1	1	0	1.25
6	389.12	30.19	0.80	1.26	0.80	1.26	1	1	0	.
6	415.12	67.46	1.00	1.00	1.00	1.00	1	1	0	1.26
6	452.12	69.03	0.62	1.61	0.62	1.61	1	1	0	1.00
6	453.12	70.27	0.59	1.69	0.62	1.61	0		1	.
6	455.12	75.20	0.54	1.85	0.53	1.87	0		1	.
6	459.12	72.17	0.58	1.73	0.58	1.73	1	4	0	1.61
6	460.12	73.70	0.53	1.87	0.53	1.87	1	4	0	1.73
6	465.12	77.54	0.53	1.90	0.53	1.87	0		0	.
6	469.12	93.42	0.68	1.47	0.68	1.47	1	0	0	1.87
6	470.12	95.02	0.69	1.45	0.68	1.47	0		1	.
6	474.12	97.26	0.68	1.46	0.68	1.46	1	1	0	1.47
6	477.12	100.33	0.66	1.51	0.66	1.51	1	0	0	1.46
6	483.12	109.27	0.55	1.83	0.55	1.83	1	2	0	1.51
6	484.12	106.97	0.55	1.81	0.55	1.81	1	2	0	1.51
6	485.12	108.17	0.52	1.92	0.52	1.92	1	3	0	1.51
6	486.12	101.80	0.46	2.17	0.46	2.17	1	3	0	1.51
6	487.12	111.47	0.53	1.87	0.53	1.87	1	1	0	1.51
6	488.12	114.24	0.57	1.75	0.57	1.75	1	2	0	1.87
6	489.12	115.18	0.53	1.90	0.53	1.90	1	3	0	1.87
6	502.12	203.53	0.57	1.75	0.57	1.75	1	0	0	1.87
6	514.12	429.03	0.56	1.80	0.56	1.80	1	0	0	1.75
7	1.01	38.24	0.79	1.27	0.79	1.27	1	2	0	.
7	2.01	37.17	0.60	1.66	0.60	1.66	1	3	0	.
7	3.01	42.48	1.10	0.91	1.10	0.91	1	0	0	.
7	4.01	54.59	0.93	1.07	0.93	1.07	1	2	0	1.52
7	5.01	81.42	0.71	1.40	0.66	1.52	0		1	.
7	6.01	82.55	0.65	1.53	0.65	1.53	1	3	0	1.52
7	7.01	79.92	0.66	1.52	0.66	1.52	1	0	0	0.91
7	8.01	88.06	0.59	1.70	0.59	1.70	1	0	0	1.52
7	9.01	92.46	0.61	1.65	0.59	1.70	0		0	.
7	10.01	90.06	0.59	1.70	0.59	1.70	0		1	.
7	11.01	91.73	0.58	1.72	0.59	1.70	0		0	.
7	12.01	95.13	0.62	1.62	0.62	1.62	1	4	0	1.70
7	16.01	97.43	0.55	1.81	0.55	1.81	1	2	0	1.62
7	17.01	94.76	0.48	2.09	0.48	2.09	1	3	0	1.62
7	18.01	46.81	0.51	1.95	0.51	1.95	1	1	0	1.62
7	19.01	48.02	0.52	1.93	0.51	1.95	0		1	.
7	20.01	81.64	0.53	1.90	0.51	1.95	0		0	.
7	23.01	87.38	0.64	1.57	0.64	1.57	1	0	0	1.95
7	24.01	86.12	0.59	1.70	0.64	1.57	0		1	.
7	25.01	46.68	0.63	1.59	0.64	1.57	0		0	.
7	27.01	116.79	0.58	1.73	0.58	1.73	1	4	0	1.57
7	28.01	91.22	0.61	1.63	0.61	1.63	1	1	0	1.73
7	30.01	96.26	0.64	1.57	0.64	1.57	1	1	0	1.63
7	31.01	96.09	0.59	1.69	0.59	1.69	1	3	0	1.63
7	32.01	68.47	0.66	1.52	0.64	1.57	0		1	.
7	33.01	96.89	0.67	1.50	0.67	1.50	1	2	0	1.63
7	34.01	99.40	0.68	1.47	0.64	1.57	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	35.01	1	1	0	0	1	30	0	1.29	2	42.40
7	36.01	0	0	1	0	1	30	0	1.71	2	62.80
7	37.01	0	1	0	0	1	30	0	1.50	1	62.80
7	38.01	1	.	1	0	2	38	0	1.29	2	42.40
7	39.01	0	1	1	0	2	38	0	0.86	0	32.20
7	40.01	1	.	0	0	1	40	1	0.64	2	32.20
7	41.01	1	.	1	0	.	41	1	0.43	1	22.00
7	42.01	1	.	1	0	1	42	1	1.50	2	22.00
7	43.01	1	0	1	0	1	42	1	1.71	2	42.40
7	44.01	1	0	1	0	1	41	1	1.07	1	1.60
7	45.01	1	0	0	0	1	41	1	1.50	1	22.00
7	46.01	1	0	1	0	1	42	1	1.71	2	22.00
7	47.01	1	0	1	0	1	49	0	1.50	2	62.80
7	48.01	0	1	0	1	1	49	0	1.29	1	62.80
7	49.01	1	.	1	0	1	49	0	1.93	1	1.60
7	50.01	1	0	1	0	1	49	0	1.29	1	1.60
7	51.01	0	1	0	0	1	49	0	1.71	1	1.60
7	52.01	1	1	1	0	1	49	0	1.07	2	32.20
7	53.01	1	1	1	0	2	49	0	1.29	1	32.20
7	54.01	1	0	1	0	1	49	0	1.29	2	22.00
7	55.01	1	1	1	0	1	49	0	1.29	2	22.00
7	56.01	0	1	1	0	1	49	0	1.07	1	22.00
7	57.01	0	1	0	0	1	49	0	1.29	2	32.20
7	58.01	1	0	1	0	1	49	0	1.71	1	62.80
7	59.01	0	0	0	0	1	49	0	1.50	2	42.40
7	60.01	0	0	0	0	1	49	0	1.29	1	42.40
7	61.01	0	0	0	0	1	49	0	1.29	2	73.00
7	62.01	1	1	1	0	1	49	0	1.71	1	32.20
7	63.01	1	0	1	0	1	49	0	1.29	1	73.00
7	64.01	0	1	0	1	1	49	0	1.50	2	52.60
7	65.01	1	1	1	0	1	49	0	1.29	1	73.00
7	66.01	1	0	1	0	2	49	0	1.29	1	11.80
7	67.01	1	0	1	0	1	49	0	0.86	1	73.00
7	68.01	1	0	1	0	1	49	0	1.07	2	73.00
7	69.01	0	1	0	0	1	49	0	1.29	1	73.00
7	70.01	1	1	1	0	1	49	0	1.29	2	73.00
7	71.01	1	0	1	0	1	72	0	1.29	2	73.00
7	72.01	1	.	1	0	2	72	0	1.29	1	73.00
7	73.01	1	0	1	0	2	72	0	1.29	1	52.60
7	74.01	1	0	1	0	1	72	0	1.29	2	52.60
7	75.01	1	0	1	0	1	72	0	1.29	1	11.80
7	76.01	1	0	1	0	1	72	0	1.50	1	11.80
7	77.01	1	0	0	0	1	72	0	1.50	2	73.00
7	78.01	1	0	1	0	1	72	0	1.29	2	73.00
7	79.01	0	1	0	0	1	72	0	1.71	1	32.20
7	80.01	1	1	1	0	1	72	0	1.50	2	52.60
7	81.01	0	1	1	1	1	72	0	1.29	2	32.20
7	82.01	1	1	1	0	1	72	0	1.71	1	11.80
7	83.01	1	0	1	0	1	72	0	1.50	1	11.80
7	84.01	1	.	1	0	3	84	0	1.07	1	32.20

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	35.01	74.71	0.66	1.52	0.64	1.57	0		0	.
7	36.01	65.30	0.65	1.54	0.64	1.57	0		0	.
7	37.01	64.19	0.66	1.52	0.64	1.57	0		0	.
7	38.01	83.88	0.65	1.53	0.65	1.53	1	1	0	1.57
7	39.01	108.80	0.65	1.53	0.65	1.53	0		1	.
7	40.01	112.24	0.94	1.06	0.94	1.06	1	2	0	1.53
7	41.01	101.80	0.68	1.48	0.68	1.48	1	3	0	1.53
7	42.01	109.30	0.77	1.30	0.77	1.30	1	2	0	1.53
7	43.01	86.19	0.75	1.34	0.77	1.30	0		1	.
7	44.01	140.34	0.62	1.62	0.68	1.48	0		1	.
7	45.01	107.20	0.61	1.63	0.68	1.48	0		0	.
7	46.01	110.57	0.73	1.38	0.77	1.30	0		0	.
7	47.01	67.60	0.62	1.61	0.62	1.62	0		1	.
7	48.01	145.48	0.62	1.62	0.62	1.62	0		0	.
7	49.01	149.12	0.62	1.62	0.62	1.62	1	1	0	1.53
7	50.01	150.72	0.61	1.64	0.62	1.62	0		0	.
7	51.01	119.39	0.66	1.51	0.62	1.62	0		0	.
7	52.01	116.75	0.56	1.77	0.62	1.62	0		0	.
7	53.01	122.12	0.63	1.58	0.62	1.62	0		0	.
7	54.01	123.25	0.59	1.70	0.62	1.62	0		0	.
7	55.01	120.82	0.59	1.70	0.62	1.62	0		0	.
7	56.01	125.69	0.56	1.79	0.62	1.62	0		0	.
7	57.01	69.10	0.57	1.76	0.62	1.62	0		0	.
7	58.01	93.96	0.59	1.70	0.62	1.62	0		0	.
7	59.01	92.09	0.58	1.71	0.62	1.62	0		0	.
7	60.01	70.23	0.58	1.72	0.62	1.62	0		0	.
7	61.01	130.93	0.58	1.71	0.62	1.62	0		0	.
7	62.01	71.73	0.56	1.79	0.62	1.62	0		0	.
7	63.01	100.03	0.56	1.79	0.62	1.62	0		0	.
7	64.01	47.31	0.58	1.71	0.62	1.62	0		0	.
7	65.01	172.41	0.57	1.74	0.62	1.62	0		0	.
7	66.01	74.90	0.57	1.74	0.62	1.62	0		0	.
7	67.01	78.78	0.57	1.76	0.62	1.62	0		0	.
7	68.01	76.57	0.57	1.74	0.62	1.62	0		0	.
7	69.01	79.94	0.55	1.81	0.62	1.62	0		0	.
7	70.01	81.64	0.57	1.77	0.62	1.62	0		0	.
7	71.01	87.15	0.56	1.79	0.55	1.83	0		1	.
7	72.01	115.22	0.55	1.83	0.55	1.83	1	0	0	1.62
7	73.01	114.18	0.56	1.80	0.55	1.83	0		0	.
7	74.01	184.49	0.57	1.76	0.55	1.83	0		0	.
7	75.01	185.12	0.57	1.74	0.55	1.83	0		0	.
7	76.01	91.49	0.57	1.76	0.55	1.83	0		0	.
7	77.01	91.09	0.56	1.77	0.55	1.83	0		0	.
7	78.01	150.91	0.58	1.73	0.55	1.83	0		0	.
7	79.01	121.22	0.58	1.71	0.55	1.83	0		0	.
7	80.01	159.49	0.59	1.71	0.55	1.83	0		0	.
7	81.01	192.20	0.60	1.67	0.55	1.83	0		0	.
7	82.01	190.83	0.54	1.85	0.55	1.83	0		0	.
7	83.01	153.42	0.57	1.76	0.55	1.83	0		0	.
7	84.01	198.30	0.53	1.87	0.53	1.87	1	0	0	1.83

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	85.01	0	1	0	0	1	84	0	1.07	0	11.80
7	86.01	1	0	1	0	2	84	0	0.86	1	32.20
7	87.01	1	1	1	0	1	84	0	1.29	1	32.20
7	88.01	0	.	0	0	1	88	1	1.07	1	32.20
7	89.01	1	1	1	0	1	88	1	1.29	1	32.20
7	90.01	1	.	1	0	1	90	1	1.50	2	73.00
7	91.01	1	0	1	0	1	88	1	1.93	1	73.00
7	92.01	1	0	0	0	1	90	1	1.93	2	73.00
7	93.01	1	0	0	0	1	90	1	1.71	2	124.01
7	94.01	1	0	1	0	1	90	1	1.93	2	93.40
7	95.01	0	1	0	0	1	88	1	1.71	1	124.01
7	96.01	1	0	0	0	1	90	1	1.71	2	73.00
7	97.01	0	1	0	0	1	90	1	1.71	2	73.00
7	98.01	1	0	1	0	1	90	1	1.93	2	73.00
7	99.01	1	1	1	0	1	88	1	1.71	1	32.20
7	100.01	1	0	1	0	1	88	1	1.71	1	32.20
7	101.01	1	0	1	0	1	88	1	1.93	1	32.20
7	102.01	1	1	1	0	1	90	1	1.93	2	32.20
7	103.01	1	0	1	0	1	88	1	1.71	1	11.80
7	104.01	1	0	1	0	1	90	1	1.93	2	52.60
7	105.01	1	0	1	0	1	88	1	2.14	1	32.20
7	106.01	0	1	1	0	1	90	1	1.93	2	52.60
7	107.01	1	.	1	0	1	107	1	1.93	2	93.40
7	108.01	1	0	0	0	1	88	1	2.36	1	11.80
7	109.01	0	.	0	0	1	109	1	1.93	2	62.80
7	110.01	1	1	1	0	1	109	1	2.36	2	42.40
7	111.01	1	0	1	0	2	88	1	2.14	1	52.60
7	112.01	1	1	1	0	1	115	0	2.57	2	42.40
7	113.01	1	.	0	0	1	113	1	2.36	1	1.60
7	114.01	1	0	1	0	1	113	1	2.14	1	11.80
7	115.01	0	.	0	0	1	115	0	2.57	1	1.60
7	116.01	0	.	1	0	1	116	1	1.93	2	73.00
7	117.01	1	0	1	0	1	115	0	2.14	1	73.00
7	118.01	0	0	0	0	1	116	1	2.36	2	42.40
7	119.01	0	0	0	0	1	116	1	2.36	2	73.00
7	120.01	1	.	1	0	1	120	1	1.93	1	1.60
7	121.01	0	1	1	0	1	116	1	1.71	2	32.20
7	122.01	0	1	1	0	1	120	1	2.36	1	1.60
7	123.01	1	1	1	0	1	116	1	2.36	2	42.40
7	124.01	0	0	0	0	1	120	1	2.57	1	52.60
7	125.01	1	1	1	0	1	120	1	2.14	1	1.60
7	126.01	0	1	0	0	1	120	1	2.14	1	32.20
7	127.01	1	0	0	0	1	120	1	1.71	1	73.00
7	128.01	1	0	1	0	1	120	1	2.14	1	32.20
7	129.01	1	0	1	0	1	120	1	1.93	1	52.60
7	130.01	1	1	1	0	1	120	1	1.93	1	83.20
7	131.01	1	0	0	0	1	116	1	2.14	2	22.00
7	132.01	1	0	0	0	1	116	1	2.57	2	22.00
7	133.01	0	1	0	0	1	120	1	1.93	1	83.20
7	134.01	0	0	0	0	1	116	1	2.57	2	73.00

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	85.01	156.19	0.57	1.77	0.53	1.87	0		0	.
7	86.01	156.25	0.53	1.87	0.53	1.87	0		1	.
7	87.01	159.69	0.56	1.78	0.53	1.87	0		0	.
7	88.01	161.32	0.51	1.97	0.51	1.97	1	3	0	1.87
7	89.01	95.73	0.52	1.94	0.51	1.97	0		1	.
7	90.01	93.59	0.56	1.80	0.56	1.80	1	2	0	1.87
7	91.01	97.19	0.52	1.93	0.51	1.97	0		0	.
7	92.01	54.42	0.56	1.79	0.56	1.80	0		1	.
7	93.01	84.08	0.57	1.75	0.56	1.80	0		0	.
7	94.01	40.00	0.57	1.76	0.56	1.80	0		0	.
7	95.01	100.43	0.50	2.02	0.51	1.97	0		0	.
7	96.01	104.13	0.57	1.77	0.56	1.80	0		0	.
7	97.01	99.36	0.58	1.72	0.56	1.80	0		0	.
7	98.01	167.50	0.57	1.75	0.56	1.80	0		0	.
7	99.01	169.60	0.53	1.87	0.51	1.97	0		0	.
7	100.01	170.07	0.54	1.84	0.51	1.97	0		0	.
7	101.01	172.97	0.52	1.94	0.51	1.97	0		0	.
7	102.01	213.92	0.56	1.78	0.56	1.80	0		0	.
7	103.01	134.70	0.52	1.92	0.51	1.97	0		0	.
7	104.01	171.71	0.56	1.78	0.56	1.80	0		0	.
7	105.01	138.54	0.53	1.88	0.51	1.97	0		0	.
7	106.01	97.36	0.57	1.74	0.56	1.80	0		0	.
7	107.01	216.75	0.57	1.76	0.57	1.76	1	1	0	1.87
7	108.01	115.38	0.54	1.87	0.51	1.97	0		0	.
7	109.01	137.30	0.56	1.78	0.56	1.78	1	3	0	1.76
7	110.01	126.19	0.57	1.76	0.56	1.78	0		1	.
7	111.01	139.91	0.52	1.91	0.51	1.97	0		0	.
7	112.01	224.46	0.57	1.75	0.60	1.67	0		0	.
7	113.01	221.26	0.62	1.62	0.62	1.62	1	2	0	1.76
7	114.01	226.96	0.60	1.67	0.62	1.62	0		1	.
7	115.01	102.40	0.60	1.67	0.60	1.67	1	1	0	1.76
7	116.01	101.60	0.63	1.59	0.63	1.59	1	2	0	1.67
7	117.01	142.01	0.55	1.80	0.60	1.67	0		0	.
7	118.01	109.07	0.64	1.57	0.63	1.59	0		0	.
7	119.01	230.57	0.63	1.60	0.63	1.59	0		1	.
7	120.01	196.53	0.51	1.95	0.51	1.95	1	3	0	1.67
7	121.01	232.34	0.60	1.67	0.63	1.59	0		0	.
7	122.01	147.98	0.52	1.91	0.51	1.95	0		1	.
7	123.01	131.63	0.59	1.71	0.63	1.59	0		0	.
7	124.01	233.27	0.51	1.94	0.51	1.95	0		0	.
7	125.01	191.25	0.50	2.00	0.51	1.95	0		0	.
7	126.01	104.20	0.48	2.09	0.51	1.95	0		0	.
7	127.01	189.08	0.49	2.04	0.51	1.95	0		0	.
7	128.01	146.98	0.49	2.05	0.51	1.95	0		0	.
7	129.01	73.37	0.48	2.08	0.51	1.95	0		0	.
7	130.01	196.49	0.46	2.15	0.51	1.95	0		0	.
7	131.01	199.43	0.55	1.83	0.63	1.59	0		0	.
7	132.01	74.24	0.55	1.82	0.63	1.59	0		0	.
7	133.01	116.21	0.47	2.15	0.51	1.95	0		0	.
7	134.01	247.95	0.56	1.79	0.63	1.59	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	135.01	0	0	0	0	1	120	1	2.36	1	1.60
7	136.01	1	1	1	0	1	120	1	2.36	1	1.60
7	137.01	1	0	1	0	1	120	1	2.79	1	1.60
7	138.01	0	0	1	0	1	120	1	1.93	1	11.80
7	139.01	1	1	0	0	1	120	1	2.36	1	22.00
7	140.01	1	1	1	0	1	116	1	2.14	2	73.00
7	141.01	1	0	1	0	1	120	1	2.36	1	73.00
7	142.01	0	1	1	0	1	116	1	2.57	2	42.40
7	143.01	0	0	0	0	1	116	1	2.57	2	42.40
7	144.01	0	0	1	0	1	116	1	2.57	2	42.40
7	145.01	1	0	1	0	1	120	1	2.57	1	42.40
7	146.01	1	.	1	0	1	146	0	2.14	1	22.00
7	147.01	1	.	1	0	1	147	0	1.71	1	1.60
7	148.01	1	0	1	0	1	147	0	1.71	2	32.20
7	149.01	1	0	0	0	2	147	0	1.50	1	52.60
7	150.01	1	0	1	0	1	147	0	1.93	1	32.20
7	151.01	1	0	1	0	2	147	0	2.14	1	62.80
7	152.01	1	0	1	0	1	147	0	1.93	1	73.00
7	153.01	0	1	0	0	2	147	0	1.50	1	73.00
7	154.01	1	1	1	0	1	147	0	1.50	0	73.00
7	155.01	0	.	1	0	2	155	0	1.29	1	32.20
7	156.01	1	1	1	0	1	155	0	1.29	0	32.20
7	157.01	0	0	0	0	1	155	0	1.71	2	73.00
7	158.01	0	1	0	0	1	155	0	1.50	1	73.00
7	159.01	0	0	0	0	1	155	0	1.93	1	73.00
7	160.01	1	1	0	0	1	155	0	2.36	2	83.20
7	161.01	1	0	1	0	1	155	0	2.14	1	73.00
7	162.01	1	0	1	0	1	155	0	2.36	1	113.80
7	163.01	1	0	1	0	1	155	0	2.36	2	113.80
7	164.01	1	0	1	0	1	155	0	2.14	2	73.00
7	165.01	1	0	1	0	1	155	0	2.14	1	73.00
7	166.01	1	0	1	0	1	155	0	2.36	1	32.20
7	167.01	1	0	1	0	1	155	0	2.14	2	73.00
7	168.01	1	0	1	0	1	155	0	1.93	1	32.20
7	169.01	1	.	1	0	1	169	1	2.57	2	113.80
7	171.01	1	0	1	0	1	169	1	2.57	2	113.80
7	172.01	1	.	1	0	1	172	1	2.36	1	1.60
7	173.01	0	1	1	1	1	169	1	2.79	2	113.80
7	174.01	0	1	0	0	1	172	1	2.14	1	1.60
7	175.01	1	1	1	0	1	169	1	2.79	2	73.00
7	176.01	1	0	1	0	1	169	1	2.36	2	73.00
7	177.01	1	1	1	0	1	172	1	2.57	1	42.40
7	178.01	1	0	1	0	1	172	1	2.36	1	42.40
7	179.01	1	0	1	0	1	172	1	2.36	1	42.40
7	180.01	1	0	1	0	1	172	1	2.36	1	73.00
7	181.01	0	1	0	0	1	169	1	2.36	2	73.00
7	182.01	0	0	0	0	1	169	1	2.36	2	83.20
7	183.01	1	0	1	0	1	172	1	2.36	1	73.00
7	184.01	1	0	1	0	1	172	1	2.57	1	73.00
7	185.01	0	1	0	0	1	172	1	2.57	1	42.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	135.01	249.22	0.47	2.14	0.51	1.95	0		0	.
7	136.01	250.29	0.47	2.11	0.51	1.95	0		0	.
7	137.01	247.35	0.48	2.09	0.51	1.95	0		0	.
7	138.01	201.56	0.47	2.13	0.51	1.95	0		0	.
7	139.01	113.54	0.46	2.17	0.51	1.95	0		0	.
7	140.01	111.24	0.61	1.64	0.63	1.59	0		0	.
7	141.01	150.02	0.46	2.19	0.51	1.95	0		0	.
7	142.01	151.82	0.59	1.69	0.63	1.59	0		0	.
7	143.01	153.09	0.57	1.75	0.63	1.59	0		0	.
7	144.01	155.39	0.50	1.99	0.63	1.59	0		0	.
7	145.01	207.27	0.46	2.15	0.51	1.95	0		0	.
7	146.01	261.60	0.47	2.13	0.47	2.13	1	1	0	1.67
7	147.01	211.21	0.45	2.23	0.45	2.23	1	0	0	2.13
7	148.01	154.02	0.50	2.01	0.45	2.23	0		1	.
7	149.01	209.67	0.45	2.20	0.45	2.23	0		0	.
7	150.01	117.18	0.46	2.19	0.45	2.23	0		0	.
7	151.01	118.21	0.45	2.22	0.45	2.23	0		0	.
7	152.01	120.52	0.46	2.17	0.45	2.23	0		0	.
7	153.01	121.82	0.45	2.20	0.45	2.23	0		0	.
7	154.01	220.05	0.45	2.22	0.45	2.23	0		0	.
7	155.01	222.15	0.46	2.18	0.46	2.18	1	1	0	2.23
7	156.01	126.76	0.45	2.20	0.46	2.18	0		1	.
7	157.01	123.29	0.46	2.19	0.46	2.18	0		0	.
7	158.01	124.22	0.46	2.18	0.46	2.18	0		0	.
7	159.01	98.40	0.45	2.23	0.46	2.18	0		0	.
7	160.01	127.39	0.45	2.22	0.46	2.18	0		0	.
7	161.01	79.11	0.45	2.21	0.46	2.18	0		0	.
7	162.01	76.41	0.45	2.22	0.46	2.18	0		0	.
7	163.01	131.69	0.45	2.21	0.46	2.18	0		0	.
7	164.01	129.39	0.45	2.22	0.46	2.18	0		0	.
7	165.01	229.29	0.45	2.24	0.46	2.18	0		0	.
7	166.01	135.80	0.44	2.26	0.46	2.18	0		0	.
7	167.01	231.56	0.47	2.13	0.46	2.18	0		0	.
7	168.01	82.78	0.44	2.27	0.46	2.18	0		0	.
7	169.01	314.04	0.47	2.13	0.47	2.13	1	2	0	2.18
7	171.01	289.33	0.47	2.13	0.47	2.13	0		1	.
7	172.01	85.62	0.40	2.49	0.40	2.49	1	3	0	2.18
7	173.01	291.56	0.54	1.86	0.47	2.13	0		0	.
7	174.01	145.01	0.41	2.46	0.40	2.49	0		1	.
7	175.01	144.04	0.53	1.90	0.47	2.13	0		0	.
7	176.01	174.58	0.51	1.94	0.47	2.13	0		0	.
7	177.01	177.54	0.41	2.46	0.40	2.49	0		0	.
7	178.01	180.15	0.40	2.47	0.40	2.49	0		0	.
7	179.01	133.63	0.41	2.43	0.40	2.49	0		0	.
7	180.01	150.65	0.41	2.42	0.40	2.49	0		0	.
7	181.01	114.85	0.51	1.95	0.47	2.13	0		0	.
7	182.01	136.17	0.51	1.94	0.47	2.13	0		0	.
7	183.01	137.03	0.41	2.43	0.40	2.49	0		0	.
7	184.01	185.72	0.41	2.44	0.40	2.49	0		0	.
7	185.01	142.84	0.40	2.47	0.40	2.49	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	186.01	0	0	1	0	1	172	1	2.14	1	62.80
7	187.01	0	0	0	0	1	169	1	2.14	2	62.80
7	188.01	1	1	1	0	1	169	1	2.14	2	83.20
7	189.01	1	1	1	0	1	172	1	2.14	1	11.80
7	190.01	1	0	1	0	1	172	1	1.93	1	11.80
7	191.01	0	1	0	0	1	191	1	1.93	2	22.00
7	192.01	0	1	0	0	1	172	1	1.93	1	22.00
7	193.01	1	1	1	0	1	194	1	1.50	2	93.40
7	194.01	0	.	1	1	2	194	1	1.50	2	93.40
7	195.01	1	0	1	0	1	199	0	2.14	2	73.00
7	196.01	1	0	1	0	1	199	0	1.93	1	73.00
7	197.01	1	1	1	0	1	172	1	1.29	1	73.00
7	198.01	0	1	1	0	1	199	0	1.71	2	32.20
7	199.01	1	.	0	0	2	199	0	1.50	1	73.00
7	200.01	0	0	0	0	1	199	0	1.71	1	124.01
7	201.01	0	0	1	0	1	199	0	1.50	1	124.01
7	202.01	1	1	0	0	1	199	0	1.29	1	83.20
7	203.01	1	0	0	0	1	199	0	1.29	1	83.20
7	204.01	1	0	1	0	1	199	0	1.50	0	93.40
7	205.01	1	0	1	0	2	199	0	1.50	1	73.00
7	206.01	1	1	1	0	1	207	0	1.71	1	11.80
7	207.01	0	.	0	0	1	207	0	1.50	2	32.20
7	208.01	1	1	1	0	1	209	0	1.93	0	93.40
7	209.01	0	.	1	0	2	209	0	1.93	1	93.40
7	210.01	0	1	1	0	1	209	0	1.93	1	32.20
7	211.01	0	0	0	0	1	209	0	1.71	2	73.00
7	212.01	1	0	1	0	1	213	0	1.50	2	113.80
7	213.01	1	.	1	0	1	213	0	1.29	1	113.80
7	214.01	0	.	0	0	2	214	0	1.29	0	32.20
7	215.01	0	0	0	0	1	214	0	1.29	2	32.20
7	216.01	0	1	1	0	1	214	0	1.71	2	73.00
7	217.01	1	1	1	0	1	214	0	1.71	1	73.00
7	218.01	0	0	1	0	1	214	0	2.14	2	42.40
7	219.01	0	0	0	0	1	214	0	1.93	1	42.40
7	220.01	0	0	1	0	1	214	0	2.14	1	113.80
7	221.01	0	0	0	0	1	214	0	2.14	2	144.41
7	222.01	1	1	1	0	1	214	0	1.93	2	93.40
7	223.01	1	0	1	0	1	214	0	1.93	1	32.20
7	224.01	1	0	1	0	2	214	0	2.14	1	73.00
7	225.01	0	.	1	0	2	225	0	2.14	2	103.60
7	226.01	1	1	1	0	1	225	0	1.93	1	113.80
7	227.01	1	0	1	0	1	225	0	2.14	2	93.40
7	228.01	1	0	0	0	1	225	0	2.36	1	73.00
7	229.01	1	0	1	0	1	225	0	2.79	2	93.40
7	230.01	1	0	0	0	1	225	0	2.36	1	73.00
7	231.01	1	.	1	0	1	231	0	2.14	2	73.00
7	232.01	0	.	0	0	1	232	0	2.36	1	73.00
7	233.01	1	.	1	0	1	233	0	2.57	1	73.00
7	234.01	1	0	1	0	1	235	0	1.50	2	62.80
7	235.01	1	.	1	0	1	235	0	1.07	2	62.80

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	186.01	151.85	0.40	2.48	0.40	2.49	0		0	.
7	187.01	125.66	0.49	2.05	0.47	2.13	0		0	.
7	188.01	304.97	0.48	2.09	0.47	2.13	0		0	.
7	189.01	307.44	0.39	2.53	0.40	2.49	0		0	.
7	190.01	257.39	0.40	2.52	0.40	2.49	0		0	.
7	191.01	256.72	0.44	2.28	0.44	2.28	0		0	2.18
7	192.01	129.83	0.40	2.50	0.40	2.49	0		0	.
7	193.01	129.19	0.42	2.37	0.43	2.33	0		1	.
7	194.01	162.19	0.43	2.33	0.43	2.33	1	2	0	2.18
7	195.01	147.74	0.41	2.43	0.41	2.46	0		1	.
7	196.01	146.61	0.41	2.41	0.41	2.46	0		0	.
7	197.01	274.17	0.41	2.47	0.40	2.49	0		0	.
7	198.01	149.15	0.43	2.35	0.41	2.46	0		0	.
7	199.01	58.09	0.41	2.46	0.41	2.46	1	1	0	2.18
7	200.01	57.02	0.42	2.38	0.41	2.46	0		0	.
7	201.01	121.89	0.42	2.36	0.41	2.46	0		0	.
7	202.01	123.09	0.43	2.34	0.41	2.46	0		0	.
7	203.01	132.13	0.44	2.29	0.41	2.46	0		0	.
7	204.01	169.07	0.44	2.28	0.41	2.46	0		0	.
7	205.01	337.27	0.44	2.27	0.41	2.46	0		0	.
7	206.01	282.48	0.42	2.37	0.41	2.44	0		1	.
7	207.01	135.23	0.41	2.44	0.41	2.44	1	0	0	2.46
7	208.01	133.33	0.42	2.36	0.42	2.40	0		1	.
7	209.01	286.48	0.42	2.40	0.42	2.40	1	0	0	2.44
7	210.01	173.24	0.42	2.36	0.42	2.40	0		0	.
7	211.01	97.43	0.40	2.49	0.42	2.40	0		0	.
7	212.01	95.69	0.41	2.45	0.40	2.47	0		1	.
7	213.01	295.72	0.40	2.47	0.40	2.47	1	0	0	2.40
7	214.01	293.63	0.42	2.40	0.42	2.40	1	0	0	2.47
7	215.01	178.51	0.42	2.40	0.42	2.40	0		1	.
7	216.01	176.77	0.43	2.33	0.42	2.40	0		0	.
7	217.01	235.14	0.43	2.31	0.42	2.40	0		0	.
7	218.01	232.13	0.43	2.35	0.42	2.40	0		0	.
7	219.01	102.17	0.44	2.28	0.42	2.40	0		0	.
7	220.01	66.84	0.43	2.35	0.42	2.40	0		0	.
7	221.01	141.71	0.42	2.38	0.42	2.40	0		0	.
7	222.01	302.90	0.43	2.35	0.42	2.40	0		0	.
7	223.01	178.88	0.43	2.32	0.42	2.40	0		0	.
7	224.01	107.97	0.44	2.29	0.42	2.40	0		0	.
7	225.01	104.14	0.45	2.22	0.45	2.22	1	1	0	2.40
7	226.01	149.85	0.44	2.25	0.45	2.22	0		1	.
7	227.01	182.35	0.45	2.25	0.45	2.22	0		0	.
7	228.01	143.51	0.45	2.25	0.45	2.22	0		0	.
7	229.01	183.98	0.46	2.19	0.45	2.22	0		0	.
7	230.01	194.36	0.45	2.20	0.45	2.22	0		0	.
7	231.01	187.82	0.45	2.23	0.45	2.23	1	3	0	2.22
7	232.01	189.49	0.46	2.15	0.46	2.15	1	2	0	2.22
7	233.01	196.86	0.46	2.15	0.46	2.15	1	1	0	2.22
7	234.01	195.19	0.49	2.06	0.49	2.05	0		1	.
7	235.01	193.19	0.49	2.05	0.49	2.05	1	2	0	2.15

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	236.01	1	.	1	1	2	236	0	1.50	1	62.80
7	237.01	1	.	1	0	2	237	0	1.71	1	11.80
7	238.01	1	0	1	0	1	236	0	1.93	1	11.80
7	239.01	1	0	1	0	2	236	0	1.93	1	11.80
7	240.01	1	1	1	0	1	236	0	1.71	1	52.60
7	241.01	0	1	0	0	1	236	0	1.71	2	93.40
7	242.01	1	0	1	0	1	236	0	1.93	2	144.41
7	243.01	0	1	0	0	2	236	0	1.50	2	144.41
7	244.01	0	.	1	0	1	244	1	2.14	2	144.41
7	245.01	1	1	1	0	1	244	1	1.93	2	93.40
7	246.01	1	1	1	0	1	236	0	1.93	1	93.40
7	247.01	1	.	1	0	1	247	1	1.71	1	93.40
7	248.01	0	1	0	0	1	244	1	2.14	2	83.20
7	249.01	1	0	1	0	1	247	1	1.71	1	93.40
7	250.01	0	0	1	0	1	244	1	2.14	2	93.40
7	251.01	0	1	0	0	1	247	1	2.14	1	73.00
7	252.01	0	0	1	0	1	247	1	1.93	1	185.21
7	253.01	1	.	1	0	2	253	0	1.71	1	73.00
7	254.01	1	1	1	0	1	247	1	2.14	1	83.20
7	255.01	0	0	0	0	1	247	1	2.14	1	185.21
7	256.01	1	0	1	0	1	253	0	1.50	2	93.40
7	257.01	1	0	1	0	1	253	0	1.71	1	73.00
7	258.01	1	1	1	0	1	253	0	1.71	1	93.40
7	259.01	0	1	1	0	1	253	0	2.14	2	73.00
7	260.01	0	1	1	0	1	253	0	2.14	2	93.40
7	261.01	1	1	1	0	1	253	0	1.93	2	93.40
7	262.01	1	0	1	0	2	253	0	2.14	1	83.20
7	263.01	0	0	0	1	1	253	0	2.57	1	73.00
7	264.01	0	1	0	0	1	253	0	2.14	2	93.40
7	265.01	1	1	1	0	1	253	0	2.14	1	93.40
7	266.01	1	0	1	0	2	253	0	1.71	2	93.40
7	267.01	1	0	1	0	1	253	0	1.50	1	93.40
7	268.01	1	0	1	0	1	253	0	1.71	2	93.40
7	269.01	1	0	1	0	1	253	0	1.93	1	42.40
7	270.01	0	0	0	0	1	273	1	1.93	2	134.21
7	271.01	0	1	1	0	1	253	0	1.71	1	11.80
7	272.01	0	0	1	0	1	253	0	1.71	2	73.00
7	273.01	0	.	1	0	1	273	1	1.71	2	154.61
7	274.01	1	0	1	0	1	275	1	1.71	1	42.40
7	275.01	1	.	1	0	1	275	1	1.29	1	42.40
7	276.01	1	1	1	0	1	273	1	1.71	2	124.01
7	277.01	1	0	0	0	1	273	1	2.14	2	124.01
7	278.01	0	0	1	0	1	275	1	2.14	1	154.61
7	279.01	0	0	0	0	1	275	1	1.93	1	73.00
7	280.01	0	0	1	0	1	275	1	2.14	1	144.41
7	281.01	0	1	0	0	1	275	1	2.14	1	73.00
7	282.01	0	1	0	0	1	273	1	1.71	2	124.01
7	283.01	0	0	1	0	1	273	1	2.36	2	93.40
7	284.01	0	0	1	0	1	273	1	2.57	2	93.40
7	285.01	0	0	0	0	1	275	1	1.93	1	154.61

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	236.01	374.88	0.43	2.35	0.43	2.35	1	1	0	2.15
7	237.01	379.28	0.41	2.47	0.41	2.47	1	3	0	2.15
7	238.01	381.02	0.43	2.34	0.43	2.35	0		1	.
7	239.01	252.92	0.43	2.34	0.43	2.35	0		0	.
7	240.01	156.75	0.44	2.29	0.43	2.35	0		0	.
7	241.01	70.87	0.43	2.31	0.43	2.35	0		0	.
7	242.01	71.81	0.44	2.26	0.43	2.35	0		0	.
7	243.01	76.04	0.45	2.21	0.43	2.35	0		0	.
7	244.01	166.00	0.45	2.22	0.45	2.22	1	2	0	2.35
7	245.01	145.48	0.45	2.25	0.45	2.22	0		1	.
7	246.01	155.32	0.46	2.20	0.43	2.35	0		0	.
7	247.01	168.47	0.41	2.44	0.41	2.44	1	3	0	2.35
7	248.01	158.29	0.45	2.23	0.45	2.22	0		0	.
7	249.01	164.66	0.42	2.40	0.41	2.44	0		1	.
7	250.01	201.80	0.47	2.13	0.45	2.22	0		0	.
7	251.01	39.07	0.42	2.41	0.41	2.44	0		0	.
7	252.01	209.27	0.42	2.40	0.41	2.44	0		0	.
7	253.01	160.72	0.41	2.41	0.41	2.41	1	0	0	2.35
7	254.01	39.91	0.42	2.38	0.41	2.44	0		0	.
7	255.01	165.36	0.42	2.38	0.41	2.44	0		0	.
7	256.01	213.31	0.44	2.29	0.41	2.41	0		1	.
7	257.01	166.43	0.42	2.40	0.41	2.41	0		0	.
7	258.01	218.98	0.43	2.32	0.41	2.41	0		0	.
7	259.01	172.54	0.44	2.25	0.41	2.41	0		0	.
7	260.01	176.27	0.43	2.33	0.41	2.41	0		0	.
7	261.01	170.13	0.44	2.25	0.41	2.41	0		0	.
7	262.01	221.78	0.43	2.34	0.41	2.41	0		0	.
7	263.01	175.21	0.44	2.29	0.41	2.41	0		0	.
7	264.01	169.07	0.44	2.28	0.41	2.41	0		0	.
7	265.01	173.54	0.43	2.33	0.41	2.41	0		0	.
7	266.01	171.44	0.44	2.28	0.41	2.41	0		0	.
7	267.01	174.67	0.43	2.34	0.41	2.41	0		0	.
7	268.01	304.30	0.43	2.31	0.41	2.41	0		0	.
7	269.01	119.28	0.43	2.33	0.41	2.41	0		0	.
7	270.01	423.06	0.46	2.17	0.47	2.15	0		1	.
7	271.01	231.13	0.44	2.30	0.41	2.41	0		0	.
7	272.01	79.75	0.44	2.30	0.41	2.41	0		0	.
7	273.01	309.54	0.47	2.15	0.47	2.15	1	1	0	2.41
7	274.01	307.51	0.41	2.42	0.42	2.37	0		1	.
7	275.01	117.45	0.42	2.37	0.42	2.37	1	3	0	2.15
7	276.01	118.85	0.46	2.17	0.47	2.15	0		0	.
7	277.01	83.52	0.46	2.18	0.47	2.15	0		0	.
7	278.01	236.83	0.43	2.30	0.42	2.37	0		0	.
7	279.01	92.16	0.43	2.33	0.42	2.37	0		0	.
7	280.01	229.26	0.44	2.30	0.42	2.37	0		0	.
7	281.01	120.55	0.43	2.35	0.42	2.37	0		0	.
7	282.01	195.63	0.47	2.13	0.47	2.15	0		0	.
7	283.01	196.86	0.48	2.09	0.47	2.15	0		0	.
7	284.01	88.66	0.48	2.09	0.47	2.15	0		0	.
7	285.01	244.24	0.44	2.29	0.42	2.37	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	286.01	1	0	1	0	1	275	1	2.36	1	73.00
7	287.01	1	1	1	0	1	275	1	1.71	1	154.61
7	288.01	1	0	1	0	1	289	1	1.93	2	134.21
7	289.01	1	.	1	0	1	289	1	1.93	2	73.00
7	290.01	1	.	1	0	1	290	1	2.36	1	93.40
7	291.01	1	0	1	0	1	289	1	1.93	2	42.40
7	292.01	1	0	1	0	1	289	1	1.93	2	73.00
7	293.01	1	0	1	0	1	290	1	2.14	1	93.40
7	294.01	1	0	1	0	1	290	1	2.14	1	93.40
7	295.01	1	0	1	0	2	290	1	2.14	1	93.40
7	296.01	0	.	1	0	1	296	1	1.71	2	113.80
7	297.01	1	1	0	0	1	311	1	1.71	1	83.20
7	298.01	0	.	0	1	1	298	0	1.50	2	154.61
7	299.01	0	1	1	0	1	311	1	2.14	1	134.21
7	300.01	1	.	0	0	1	300	0	2.14	1	124.01
7	301.01	0	.	1	0	1	301	0	0.86	2	154.61
7	302.01	0	.	1	0	1	302	0	1.07	2	154.61
7	303.01	1	.	1	0	1	303	0	2.57	1	93.40
7	304.01	1	.	1	0	1	304	0	1.07	2	93.40
7	305.01	1	.	1	0	1	305	0	1.29	0	93.40
7	306.01	1	.	1	0	1	306	0	1.93	2	144.41
7	307.01	1	0	1	0	1	305	0	1.71	2	144.41
7	308.01	1	.	1	0	1	308	1	1.71	2	154.61
7	309.01	1	.	1	0	1	309	1	1.71	2	154.61
7	310.01	1	0	1	0	1	309	1	2.14	2	144.41
7	311.01	0	.	1	0	2	311	1	1.93	1	32.20
7	312.01	1	.	1	0	1	312	1	1.93	0	83.20
7	313.01	1	.	1	0	1	313	1	1.93	1	93.40
7	314.01	1	0	1	0	1	309	1	2.14	2	93.40
7	315.01	1	0	1	0	1	309	1	2.14	2	154.61
7	316.01	1	0	1	0	1	309	1	2.14	2	93.40
7	317.01	1	0	1	0	1	313	1	2.36	1	93.40
7	318.01	1	0	1	0	1	309	1	2.36	2	154.61
7	319.01	1	0	1	0	1	309	1	2.57	2	154.61
7	320.01	1	0	1	0	1	313	1	2.14	1	134.21
7	321.01	1	0	0	1	1	309	1	2.14	2	144.41
7	322.01	1	1	1	0	1	313	1	2.36	1	93.40
7	323.01	1	0	1	0	1	313	1	1.93	1	154.61
7	324.01	1	.	1	0	1	324	0	2.36	2	144.41
7	325.01	0	1	0	0	1	324	0	2.36	1	144.41
7	326.01	1	1	1	0	1	324	0	2.36	1	154.61
7	327.01	0	1	0	0	1	324	0	2.36	2	73.00
7	328.01	0	0	0	0	1	324	0	1.93	1	144.41
7	329.01	0	1	0	0	1	324	0	2.36	2	154.61
7	330.01	0	1	0	1	1	324	0	2.36	2	154.61
7	331.01	1	0	1	0	1	324	0	2.36	2	154.61
7	332.01	0	0	0	1	1	324	0	1.93	2	154.61
7	333.01	1	0	1	0	1	313	1	1.71	1	52.60
7	334.01	0	1	1	0	1	313	1	1.93	1	93.40
7	335.01	1	0	1	0	1	324	0	1.71	2	144.41

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	286.01	90.19	0.45	2.25	0.42	2.37	0		0	.
7	287.01	122.25	0.44	2.26	0.42	2.37	0		0	.
7	288.01	264.36	0.45	2.23	0.44	2.27	0		1	.
7	289.01	189.79	0.44	2.27	0.44	2.27	1	0	0	2.15
7	290.01	352.55	0.42	2.35	0.42	2.35	1	3	0	2.27
7	291.01	271.07	0.62	1.62	0.44	2.27	0		0	.
7	292.01	195.56	0.48	2.08	0.44	2.27	0		0	.
7	293.01	192.86	0.44	2.28	0.42	2.35	0		0	.
7	294.01	202.27	0.43	2.32	0.42	2.35	0		1	.
7	295.01	154.99	0.44	2.27	0.42	2.35	0		0	.
7	296.01	208.61	0.46	2.18	0.46	2.18	1	2	0	2.27
7	297.01	93.93	0.43	2.31	0.44	2.27	0		1	.
7	298.01	123.79	0.61	1.63	0.61	1.63	1	1	0	2.27
7	299.01	124.69	0.45	2.22	0.44	2.27	0		0	.
7	300.01	92.16	0.44	2.27	0.44	2.27	1	0	0	2.27
7	301.01	94.56	0.57	1.76	0.57	1.76	1	0	0	1.63
7	302.01	188.42	0.42	2.36	0.42	2.36	1	3	0	1.76
7	303.01	216.55	0.23	4.28	0.23	4.28	1	3	0	.
7	304.01	215.21	0.50	1.98	0.50	1.98	1	2	0	1.76
7	305.01	100.64	0.46	2.19	0.46	2.19	1	1	0	1.76
7	306.01	97.13	0.46	2.17	0.46	2.17	1	1	0	2.19
7	307.01	102.00	0.46	2.20	0.46	2.19	0		1	.
7	308.01	102.94	0.48	2.09	0.48	2.09	1	2	0	2.17
7	309.01	103.57	0.39	2.54	0.39	2.54	1	2	0	2.17
7	310.01	402.73	0.39	2.54	0.39	2.54	0		1	.
7	311.01	218.38	0.44	2.27	0.44	2.27	1	3	0	2.27
7	312.01	212.31	0.35	2.83	0.35	2.83	1	2	0	2.17
7	313.01	237.23	0.31	3.23	0.31	3.23	1	3	0	2.17
7	314.01	108.44	0.41	2.45	0.39	2.54	0		0	.
7	315.01	242.74	0.41	2.46	0.39	2.54	0		0	.
7	316.01	215.41	0.40	2.51	0.39	2.54	0		0	.
7	317.01	110.61	0.32	3.08	0.31	3.23	0		1	.
7	318.01	111.91	0.40	2.53	0.39	2.54	0		0	.
7	319.01	130.26	0.42	2.41	0.39	2.54	0		0	.
7	320.01	116.75	0.34	2.96	0.31	3.23	0		0	.
7	321.01	231.20	0.39	2.56	0.39	2.54	0		0	.
7	322.01	96.73	0.36	2.77	0.31	3.23	0		0	.
7	323.01	111.45	0.34	2.93	0.31	3.23	0		0	.
7	324.01	113.08	0.38	2.64	0.38	2.64	1	1	0	2.17
7	325.01	115.88	0.35	2.83	0.38	2.64	0		1	.
7	326.01	306.54	0.34	2.91	0.38	2.64	0		0	.
7	327.01	105.17	0.36	2.81	0.38	2.64	0		0	.
7	328.01	124.43	0.35	2.86	0.38	2.64	0		0	.
7	329.01	125.89	0.37	2.72	0.38	2.64	0		0	.
7	330.01	129.10	0.35	2.84	0.38	2.64	0		0	.
7	331.01	131.00	0.37	2.72	0.38	2.64	0		0	.
7	332.01	360.16	0.38	2.66	0.38	2.64	0		0	.
7	333.01	225.02	0.33	3.01	0.31	3.23	0		0	.
7	334.01	132.83	0.35	2.86	0.31	3.23	0		0	.
7	335.01	131.99	0.40	2.53	0.38	2.64	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	336.01	0	0	1	0	1	313	1	2.14	1	134.21
7	337.01	0	1	0	0	1	313	1	2.36	1	134.21
7	338.01	1	1	0	0	1	313	1	2.36	1	144.41
7	339.01	1	1	1	0	1	324	0	2.57	1	154.61
7	340.01	1	1	1	0	1	324	0	2.36	1	154.61
7	341.01	1	0	1	0	1	324	0	1.93	2	154.61
7	342.01	1	1	1	0	1	324	0	2.36	2	144.41
7	343.01	1	.	1	0	2	343	1	0.64	1	124.01
7	344.01	0	1	1	0	1	343	1	1.07	1	124.01
7	345.01	1	0	1	1	1	324	0	2.36	2	154.61
7	346.01	1	1	1	0	1	324	0	2.79	1	93.40
7	347.01	0	1	0	0	1	324	0	2.14	2	154.61
7	348.01	0	1	0	0	1	324	0	2.57	1	73.00
7	349.01	1	0	1	0	1	324	0	1.93	2	154.61
7	350.01	1	1	1	0	1	324	0	1.71	1	93.40
7	351.01	0	.	1	0	1	351	1	2.36	2	144.41
7	352.01	1	0	1	0	1	324	0	1.71	1	154.61
7	353.01	0	0	1	0	1	351	1	2.36	2	185.21
7	354.01	0	1	0	0	1	324	0	2.14	1	93.40
7	355.01	0	0	1	0	1	351	1	2.36	2	175.01
7	356.01	0	0	1	0	1	351	1	2.36	2	124.01
7	357.01	1	0	1	0	1	324	0	2.14	1	73.00
7	358.01	0	0	0	0	1	351	1	2.79	2	185.21
7	359.01	1	0	0	0	1	324	0	2.57	1	73.00
7	360.01	1	1	1	0	1	324	0	2.14	1	73.00
7	361.01	1	1	1	1	1	351	1	2.57	2	144.41
7	362.01	0	1	0	0	1	324	0	2.14	1	93.40
7	363.01	0	1	1	0	1	351	1	2.14	2	144.41
7	364.01	1	1	1	0	1	351	1	2.14	2	73.00
7	365.01	1	.	1	0	1	365	1	2.14	1	83.20
7	366.01	1	0	1	0	1	376	0	2.36	1	144.41
7	367.01	1	0	1	0	1	365	1	2.14	1	83.20
7	368.01	1	0	1	0	1	365	1	2.57	1	83.20
7	369.01	1	0	1	0	1	365	1	2.14	1	93.40
7	370.01	0	1	0	0	1	365	1	2.79	1	144.41
7	371.01	1	0	1	0	1	365	1	2.57	1	93.40
7	372.01	1	0	1	0	1	378	0	2.14	2	154.61
7	373.01	0	0	0	0	1	365	1	2.79	1	154.61
7	374.01	1	1	1	0	1	365	1	2.14	1	93.40
7	375.01	0	1	0	0	1	365	1	2.57	1	154.61
7	376.01	1	.	1	0	1	376	0	2.36	1	93.40
7	377.01	1	0	1	0	1	376	0	1.93	1	93.40
7	378.01	1	.	1	0	2	378	0	2.14	1	144.41
7	379.01	1	0	1	0	1	378	0	1.93	1	144.41
7	380.01	0	1	0	0	1	378	0	1.93	1	93.40
7	381.01	0	0	0	0	1	378	0	2.14	2	93.40
7	382.01	1	1	1	0	1	378	0	2.14	1	93.40
7	383.01	1	0	0	0	1	378	0	1.93	2	195.41
7	384.01	0	1	1	0	1	378	0	1.71	2	185.21
7	385.01	0	.	1	0	1	385	1	1.93	2	144.41

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	336.01	133.36	0.36	2.79	0.31	3.23	0		0	.
7	337.01	98.23	0.35	2.88	0.31	3.23	0		0	.
7	338.01	110.18	0.34	2.97	0.31	3.23	0		0	.
7	339.01	104.31	0.35	2.90	0.38	2.64	0		0	.
7	340.01	122.46	0.35	2.82	0.38	2.64	0		0	.
7	341.01	129.33	0.39	2.59	0.38	2.64	0		0	.
7	342.01	81.31	0.39	2.58	0.38	2.64	0		0	.
7	343.01	76.81	0.25	3.95	0.25	3.95	1	3	0	2.17
7	344.01	132.13	0.26	3.85	0.25	3.95	0		1	.
7	345.01	243.87	0.40	2.53	0.38	2.64	0		0	.
7	346.01	135.04	0.36	2.75	0.38	2.64	0		0	.
7	347.01	315.48	0.42	2.40	0.38	2.64	0		0	.
7	348.01	133.24	0.38	2.64	0.38	2.64	0		0	.
7	349.01	248.51	0.41	2.43	0.38	2.64	0		0	.
7	350.01	125.03	0.38	2.66	0.38	2.64	0		0	.
7	351.01	106.61	0.43	2.32	0.43	2.32	1	2	0	2.64
7	352.01	62.80	0.39	2.59	0.38	2.64	0		0	.
7	353.01	251.82	0.42	2.37	0.43	2.32	0		1	.
7	354.01	101.67	0.40	2.53	0.38	2.64	0		0	.
7	355.01	184.61	0.47	2.12	0.43	2.32	0		0	.
7	356.01	328.86	0.50	2.02	0.43	2.32	0		0	.
7	357.01	61.26	0.39	2.54	0.38	2.64	0		0	.
7	358.01	331.03	0.50	2.00	0.43	2.32	0		0	.
7	359.01	334.16	0.40	2.50	0.38	2.64	0		0	.
7	360.01	121.46	0.40	2.50	0.38	2.64	0		0	.
7	361.01	255.19	0.52	1.92	0.43	2.32	0		0	.
7	362.01	130.93	0.41	2.45	0.38	2.64	0		0	.
7	363.01	379.24	0.53	1.90	0.43	2.32	0		0	.
7	364.01	262.16	0.50	2.00	0.43	2.32	0		0	.
7	365.01	127.06	0.41	2.46	0.41	2.46	1	3	0	2.64
7	366.01	263.79	0.44	2.25	0.44	2.27	0		1	.
7	367.01	267.60	0.39	2.55	0.41	2.46	0		1	.
7	368.01	266.60	0.40	2.51	0.41	2.46	0		0	.
7	369.01	115.05	0.40	2.49	0.41	2.46	0		0	.
7	370.01	277.11	0.41	2.44	0.41	2.46	0		0	.
7	371.01	139.07	0.43	2.32	0.41	2.46	0		0	.
7	372.01	114.52	0.43	2.33	0.44	2.27	0		1	.
7	373.01	273.54	0.41	2.46	0.41	2.46	0		0	.
7	374.01	118.09	0.42	2.36	0.41	2.46	0		0	.
7	375.01	281.95	0.44	2.27	0.41	2.46	0		0	.
7	376.01	294.02	0.44	2.27	0.44	2.27	1	1	0	2.64
7	377.01	135.30	0.45	2.24	0.44	2.27	0		0	.
7	378.01	137.67	0.44	2.27	0.44	2.27	1	0	0	2.27
7	379.01	283.65	0.44	2.27	0.44	2.27	0		0	.
7	380.01	318.42	0.44	2.30	0.44	2.27	0		0	.
7	381.01	300.66	0.44	2.27	0.44	2.27	0		0	.
7	382.01	98.03	0.45	2.21	0.44	2.27	0		0	.
7	383.01	77.98	0.44	2.28	0.44	2.27	0		0	.
7	384.01	148.08	0.44	2.27	0.44	2.27	0		0	.
7	385.01	322.72	0.45	2.24	0.45	2.24	1	1	0	2.27

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	386.01	1	1	0	0	1	378	0	1.71	1	93.40
7	387.01	1	.	1	0	1	387	1	1.93	1	93.40
7	388.01	1	1	0	0	1	385	1	2.14	2	113.80
7	389.01	1	0	1	0	1	387	1	1.71	1	93.40
7	390.01	1	1	1	1	1	391	0	1.50	2	134.21
7	391.01	0	.	1	0	1	391	0	1.93	1	144.41
7	392.01	1	0	1	0	1	391	0	1.50	2	164.81
7	393.01	1	0	1	0	1	391	0	1.50	1	144.41
7	394.01	0	1	1	0	1	391	0	1.71	1	113.80
7	395.01	1	0	1	0	1	391	0	1.71	1	113.80
7	396.01	1	0	1	1	1	391	0	2.14	2	144.41
7	397.01	1	1	1	1	1	391	0	1.93	2	144.41
7	398.01	0	1	0	0	1	391	0	1.93	2	124.01
7	399.01	1	0	1	0	1	391	0	1.93	1	93.40
7	400.01	1	0	0	0	1	391	0	2.14	2	124.01
7	401.01	1	1	1	0	1	391	0	2.36	1	113.80
7	402.01	1	0	1	0	1	391	0	1.93	1	113.80
7	403.01	0	1	1	0	1	391	0	1.93	1	154.61
7	404.01	0	0	1	0	1	391	0	1.71	2	113.80
7	405.01	1	.	0	0	1	405	0	1.07	1	113.80
7	406.01	0	1	1	0	1	405	0	1.07	1	185.21
7	407.01	1	0	1	0	1	408	0	1.29	2	93.40
7	408.01	1	.	1	0	3	408	0	1.29	1	93.40
7	409.01	1	0	1	0	1	408	0	1.50	1	154.61
7	410.01	0	1	0	0	2	408	0	1.71	1	154.61
7	411.01	0	0	1	0	1	408	0	1.71	1	154.61
7	412.01	1	1	1	0	1	408	0	1.50	1	154.61
7	413.01	0	1	0	0	1	408	0	1.50	1	154.61
7	414.01	1	1	1	0	2	408	0	1.50	1	83.20
7	415.01	0	1	0	0	1	408	0	1.29	1	154.61
7	416.01	0	0	0	0	1	408	0	1.50	1	154.61
7	417.01	0	0	0	0	1	408	0	1.71	2	154.61
7	418.01	0	0	1	1	1	408	0	1.71	2	164.81
7	419.01	1	1	1	0	1	408	0	1.71	1	154.61
7	420.01	1	0	1	0	1	408	0	1.71	2	164.81
7	421.01	1	0	1	0	1	408	0	1.71	1	164.81
7	422.01	1	0	1	0	1	408	0	2.14	2	185.21
7	423.01	1	0	1	0	1	408	0	1.71	1	164.81
7	424.01	1	0	0	0	1	408	0	1.93	1	185.21
7	425.01	1	0	1	0	1	408	0	2.14	2	195.41
7	426.01	1	0	1	0	1	408	0	1.93	1	195.41
7	427.01	1	0	1	1	1	408	0	1.93	2	205.61
7	428.01	0	1	1	0	1	408	0	2.36	1	195.41
7	429.01	1	.	1	0	1	429	0	2.36	1	195.41
7	430.01	1	.	1	0	1	430	0	2.14	2	205.61
7	431.01	1	.	1	0	1	431	0	1.93	2	205.61
7	432.01	1	0	1	0	1	431	0	2.36	1	83.20
7	433.01	0	1	0	0	1	431	0	1.71	2	205.61
7	434.01	0	0	0	0	1	431	0	1.71	1	93.40
7	435.01	0	0	1	0	1	431	0	2.14	2	175.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	386.01	323.42	0.42	2.37	0.44	2.27	0		0	.
7	387.01	249.68	0.43	2.35	0.43	2.35	1	3	0	2.24
7	388.01	326.06	0.46	2.19	0.45	2.24	0		1	.
7	389.01	195.73	0.43	2.33	0.43	2.35	0		1	.
7	390.01	141.28	0.45	2.22	0.44	2.29	0		1	.
7	391.01	116.98	0.44	2.29	0.44	2.29	1	1	0	2.24
7	392.01	145.65	0.45	2.25	0.44	2.29	0		0	.
7	393.01	248.98	0.43	2.30	0.44	2.29	0		0	.
7	394.01	251.22	0.43	2.32	0.44	2.29	0		0	.
7	395.01	154.39	0.44	2.30	0.44	2.29	0		0	.
7	396.01	151.39	0.45	2.21	0.44	2.29	0		0	.
7	397.01	205.27	0.46	2.19	0.44	2.29	0		0	.
7	398.01	337.00	0.46	2.18	0.44	2.29	0		0	.
7	399.01	203.33	0.45	2.24	0.44	2.29	0		0	.
7	400.01	252.32	0.46	2.15	0.44	2.29	0		0	.
7	401.01	255.65	0.45	2.22	0.44	2.29	0		0	.
7	402.01	113.01	0.45	2.22	0.44	2.29	0		0	.
7	403.01	264.10	0.45	2.22	0.44	2.29	0		0	.
7	404.01	261.16	0.44	2.27	0.44	2.29	0		0	.
7	405.01	37.70	0.44	2.25	0.44	2.25	1	0	0	2.29
7	406.01	353.82	0.44	2.29	0.44	2.25	0		1	.
7	407.01	351.25	0.45	2.24	0.44	2.29	0		1	.
7	408.01	150.29	0.44	2.29	0.44	2.29	1	0	0	2.25
7	409.01	152.42	0.44	2.26	0.44	2.29	0		0	.
7	410.01	154.76	0.47	2.14	0.44	2.29	0		0	.
7	411.01	156.76	0.46	2.16	0.44	2.29	0		0	.
7	412.01	160.46	0.46	2.18	0.44	2.29	0		0	.
7	413.01	379.38	0.46	2.16	0.44	2.29	0		0	.
7	414.01	162.26	0.47	2.13	0.44	2.29	0		0	.
7	415.01	163.93	0.47	2.14	0.44	2.29	0		0	.
7	416.01	165.13	0.47	2.13	0.44	2.29	0		0	.
7	417.01	117.92	0.48	2.10	0.44	2.29	0		0	.
7	418.01	167.60	0.47	2.14	0.44	2.29	0		0	.
7	419.01	122.12	0.46	2.15	0.44	2.29	0		0	.
7	420.01	123.06	0.46	2.17	0.44	2.29	0		0	.
7	421.01	99.27	0.47	2.14	0.44	2.29	0		0	.
7	422.01	124.16	0.46	2.18	0.44	2.29	0		0	.
7	423.01	100.87	0.47	2.13	0.44	2.29	0		0	.
7	424.01	102.97	0.48	2.10	0.44	2.29	0		0	.
7	425.01	101.27	0.49	2.04	0.44	2.29	0		0	.
7	426.01	86.28	0.48	2.09	0.44	2.29	0		0	.
7	427.01	106.01	0.48	2.08	0.44	2.29	0		0	.
7	428.01	107.98	0.50	2.00	0.44	2.29	0		0	.
7	429.01	87.85	0.52	1.94	0.52	1.94	1	2	0	2.29
7	430.01	88.82	0.48	2.08	0.48	2.08	1	3	0	2.29
7	431.01	409.47	0.49	2.03	0.49	2.03	1	1	0	2.29
7	432.01	89.32	0.50	2.01	0.49	2.03	0		1	.
7	433.01	407.20	0.49	2.04	0.49	2.03	0		0	.
7	434.01	152.82	0.48	2.09	0.49	2.03	0		0	.
7	435.01	181.68	0.50	1.98	0.49	2.03	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	436.01	0	0	1	0	1	431	0	1.93	1	154.61
7	437.01	0	0	0	0	1	431	0	1.71	1	154.61
7	438.01	1	0	0	0	1	431	0	2.14	2	205.61
7	439.01	1	1	1	0	1	431	0	1.71	1	154.61
7	440.01	0	1	0	0	1	431	0	1.93	1	185.21
7	441.01	0	0	1	0	1	431	0	1.93	2	144.41
7	442.01	1	1	1	0	1	431	0	1.71	1	175.01
7	443.01	1	0	1	0	1	431	0	1.50	2	226.01
7	444.01	1	.	1	0	1	444	1	2.14	2	226.01
7	445.01	1	0	1	0	1	431	0	1.93	2	154.61
7	446.01	1	0	1	0	1	444	1	2.57	2	205.61
7	447.01	1	0	1	0	1	431	0	1.50	1	93.40
7	448.01	0	1	0	1	1	444	1	2.14	2	205.61
7	449.01	1	.	0	0	1	449	1	1.93	1	93.40
7	450.01	0	1	0	0	1	449	1	2.14	1	93.40
7	451.01	0	0	0	0	1	444	1	2.36	2	205.61
7	452.01	0	0	1	0	1	449	1	2.14	1	205.61
7	453.01	1	1	1	0	1	449	1	2.14	1	134.21
7	454.01	1	1	1	0	1	444	1	2.14	2	215.81
7	455.01	1	0	1	0	1	449	1	2.14	1	144.41
7	456.01	1	0	1	0	1	460	0	2.36	2	195.41
7	457.01	0	1	1	0	1	449	1	2.14	1	226.01
7	458.01	0	1	1	0	1	460	0	2.36	2	154.61
7	459.01	1	.	1	0	1	459	1	2.14	2	154.61
7	460.01	1	.	0	0	1	460	0	2.36	1	144.41
7	461.01	1	0	1	0	1	460	0	2.36	1	144.41
7	462.01	1	0	1	0	1	459	1	1.71	2	144.41
7	463.01	0	0	0	0	1	460	0	1.93	1	144.41
7	464.01	0	0	1	0	1	465	1	2.57	1	205.61
7	465.01	0	.	0	0	1	465	1	2.57	1	226.01
7	466.01	1	.	1	0	1	466	1	2.14	1	144.41
7	467.01	1	0	0	0	1	466	1	1.50	0	144.41
7	468.01	0	1	1	0	1	466	1	1.93	1	154.61
7	469.01	1	.	1	0	2	469	0	1.93	1	42.40
7	470.01	1	0	1	0	1	469	0	2.36	2	226.01
7	471.01	1	0	1	0	1	469	0	2.14	1	42.40
7	472.01	0	1	0	0	1	469	0	2.14	2	144.41
7	473.01	0	0	1	0	1	469	0	1.71	1	144.41
7	474.01	1	0	1	0	1	469	0	2.57	1	93.40
7	475.01	1	1	1	0	1	469	0	2.14	2	195.41
7	476.01	1	0	0	0	1	469	0	2.14	1	134.21
7	477.01	1	0	1	0	1	469	0	2.14	2	195.41
7	478.01	1	1	1	0	1	469	0	1.71	2	195.41
7	479.01	0	1	0	0	1	469	0	1.71	1	195.41
7	480.01	1	1	0	0	1	481	0	1.29	1	124.01
7	481.01	0	.	0	0	2	481	0	1.50	2	124.01
7	482.01	0	0	1	0	1	481	0	2.14	2	195.41
7	483.01	0	1	1	0	1	481	0	1.93	1	164.81
7	484.01	0	0	0	0	1	481	0	1.71	1	205.61
7	485.01	1	1	1	0	1	481	0	1.93	2	226.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	436.01	183.92	0.47	2.15	0.49	2.03	0		0	.
7	437.01	94.13	0.48	2.08	0.49	2.03	0		0	.
7	438.01	185.79	0.49	2.05	0.49	2.03	0		0	.
7	439.01	66.70	0.47	2.11	0.49	2.03	0		0	.
7	440.01	199.17	0.48	2.07	0.49	2.03	0		0	.
7	441.01	152.39	0.49	2.02	0.49	2.03	0		0	.
7	442.01	66.33	0.48	2.09	0.49	2.03	0		0	.
7	443.01	62.99	0.49	2.06	0.49	2.03	0		0	.
7	444.01	202.70	0.49	2.06	0.49	2.06	1	2	0	2.03
7	445.01	105.17	0.48	2.09	0.49	2.03	0		0	.
7	446.01	422.35	0.48	2.08	0.49	2.06	0		1	.
7	447.01	110.47	0.45	2.20	0.49	2.03	0		0	.
7	448.01	423.79	0.48	2.07	0.49	2.06	0		0	.
7	449.01	426.79	0.46	2.18	0.46	2.18	1	3	0	2.03
7	450.01	111.61	0.44	2.25	0.46	2.18	0		1	.
7	451.01	98.26	0.47	2.11	0.49	2.06	0		0	.
7	452.01	245.41	0.44	2.25	0.46	2.18	0		0	.
7	453.01	112.94	0.45	2.25	0.46	2.18	0		0	.
7	454.01	197.53	0.49	2.06	0.49	2.06	0		0	.
7	455.01	144.24	0.45	2.22	0.46	2.18	0		0	.
7	456.01	64.56	0.49	2.05	0.45	2.20	0		1	.
7	457.01	214.35	0.45	2.20	0.46	2.18	0		0	.
7	458.01	211.48	0.49	2.06	0.45	2.20	0		0	.
7	459.01	202.40	0.49	2.06	0.49	2.06	1	2	0	2.20
7	460.01	204.74	0.45	2.20	0.45	2.20	1	1	0	2.03
7	461.01	220.79	0.45	2.20	0.45	2.20	0		0	.
7	462.01	206.41	0.59	1.69	0.49	2.06	0		1	.
7	463.01	99.93	0.46	2.18	0.45	2.20	0		0	.
7	464.01	73.67	0.47	2.14	0.46	2.17	0		1	.
7	465.01	214.15	0.46	2.17	0.46	2.17	1	3	0	2.20
7	466.01	224.13	0.45	2.21	0.45	2.21	1	3	0	2.20
7	467.01	215.25	0.45	2.24	0.45	2.21	0		1	.
7	468.01	590.76	0.45	2.20	0.45	2.21	0		0	.
7	469.01	91.46	0.50	2.01	0.50	2.01	1	1	0	2.20
7	470.01	592.06	0.50	2.00	0.50	2.01	0		1	.
7	471.01	139.34	0.49	2.04	0.50	2.01	0		0	.
7	472.01	225.56	0.49	2.04	0.50	2.01	0		0	.
7	473.01	476.01	0.48	2.08	0.50	2.01	0		0	.
7	474.01	153.92	0.48	2.07	0.50	2.01	0		0	.
7	475.01	289.05	0.50	2.01	0.50	2.01	0		0	.
7	476.01	152.45	0.49	2.06	0.50	2.01	0		0	.
7	477.01	154.49	0.49	2.03	0.50	2.01	0		0	.
7	478.01	149.82	0.52	1.94	0.50	2.01	0		0	.
7	479.01	300.56	0.49	2.06	0.50	2.01	0		0	.
7	480.01	302.43	0.50	1.98	0.50	1.99	0		1	.
7	481.01	160.79	0.50	1.99	0.50	1.99	1	0	0	2.01
7	482.01	184.35	0.52	1.91	0.50	1.99	0		0	.
7	483.01	127.22	0.50	1.99	0.50	1.99	0		0	.
7	484.01	115.35	0.50	2.00	0.50	1.99	0		0	.
7	485.01	156.16	0.52	1.93	0.50	1.99	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	486.01	1	0	0	1	1	481	0	1.93	1	185.21
7	487.01	0	1	0	1	1	481	0	1.93	2	195.41
7	488.01	1	1	1	0	1	481	0	2.36	1	205.61
7	489.01	0	1	0	0	1	481	0	1.71	2	226.01
7	490.01	1	1	1	0	1	481	0	1.93	1	205.61
7	491.01	0	1	1	0	1	481	0	1.71	2	226.01
7	492.01	0	0	1	0	1	481	0	1.93	1	205.61
7	493.01	0	0	1	0	1	481	0	1.71	2	226.01
7	494.01	1	.	0	0	1	494	0	1.71	2	226.01
7	495.01	1	.	1	0	1	495	0	1.71	1	154.61
7	496.01	1	0	0	0	1	501	0	1.07	1	124.01
7	497.01	1	.	1	0	1	497	0	1.93	1	205.61
7	498.01	0	1	0	1	1	497	0	1.71	1	215.81
7	499.01	1	0	1	0	1	501	0	1.29	2	226.01
7	500.01	1	1	1	0	1	501	0	1.71	1	226.01
7	501.01	1	.	1	0	3	501	0	0.86	1	185.21
7	502.01	0	1	0	0	1	501	0	1.93	2	185.21
7	503.01	1	.	1	0	1	503	1	1.71	1	205.61
7	504.01	0	.	0	0	1	504	1	1.93	2	205.61
7	505.01	0	1	0	0	1	503	1	1.93	1	226.01
7	506.01	0	0	1	0	1	504	1	1.93	2	226.01
7	507.01	1	.	1	0	1	507	0	1.93	1	215.81
7	508.01	0	1	1	0	1	507	0	1.93	2	215.81
7	509.01	1	1	1	0	1	507	0	1.93	1	226.01
7	510.01	0	1	1	0	1	507	0	2.57	2	215.81
7	511.01	1	1	0	0	1	507	0	1.93	1	226.01
7	512.01	1	0	1	0	1	507	0	2.36	2	256.61
7	513.01	1	0	1	0	1	507	0	2.14	1	226.01
7	514.01	1	.	1	0	1	514	0	2.57	2	215.81
7	515.01	1	.	1	0	1	515	0	2.14	1	215.81
7	516.01	0	.	0	1	1	516	0	2.36	1	124.01
7	517.01	1	1	1	1	1	516	0	2.14	2	215.81
7	518.01	1	0	1	0	1	516	0	2.14	1	256.61
7	519.01	0	1	1	1	1	516	0	2.14	2	215.81
7	520.01	1	1	1	0	1	516	0	1.50	1	215.81
7	521.01	1	0	1	0	1	516	0	1.50	1	154.61
7	522.01	1	0	1	0	1	516	0	1.71	2	154.61
7	523.01	1	.	1	0	1	523	1	1.50	2	154.61
7	524.01	0	1	1	0	1	523	1	1.71	2	256.61
7	525.01	0	0	1	0	1	523	1	1.93	2	256.61
7	526.01	0	0	1	0	1	523	1	2.36	2	124.01
7	527.01	1	.	1	0	1	527	1	1.50	1	93.40
7	528.01	0	1	1	0	1	527	1	1.93	1	93.40
7	529.01	0	0	1	0	1	527	1	1.93	1	52.60
7	530.01	1	1	1	0	1	523	1	2.36	2	185.21
7	531.01	0	0	0	0	1	527	1	2.14	1	185.21
7	532.01	1	0	1	0	1	523	1	1.71	2	185.21
7	533.01	0	0	1	0	1	527	1	1.93	1	226.01
7	534.01	0	0	0	0	1	527	1	2.36	1	226.01
7	535.01	1	.	1	0	1	535	0	1.71	1	215.81

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	486.01	162.66	0.50	2.00	0.50	1.99	0		0	.
7	487.01	129.86	0.50	1.99	0.50	1.99	0		0	.
7	488.01	110.27	0.49	2.02	0.50	1.99	0		0	.
7	489.01	131.80	0.50	2.01	0.50	1.99	0		0	.
7	490.01	118.58	0.49	2.05	0.50	1.99	0		0	.
7	491.01	132.73	0.49	2.02	0.50	1.99	0		0	.
7	492.01	112.94	0.48	2.06	0.50	1.99	0		0	.
7	493.01	111.21	0.49	2.03	0.50	1.99	0		0	.
7	494.01	240.51	0.51	1.96	0.51	1.96	1	2	0	1.99
7	495.01	360.96	0.47	2.15	0.47	2.15	1	3	0	1.99
7	496.01	134.83	0.47	2.11	0.48	2.09	0		0	.
7	497.01	133.66	0.46	2.15	0.46	2.15	1	1	0	1.99
7	498.01	122.62	0.47	2.14	0.46	2.15	0		1	.
7	499.01	116.98	0.49	2.05	0.48	2.09	0		1	.
7	500.01	162.56	0.45	2.20	0.48	2.09	0		0	.
7	501.01	172.41	0.48	2.09	0.48	2.09	1	0	0	2.15
7	502.01	140.84	0.50	2.01	0.48	2.09	0		0	.
7	503.01	144.61	0.46	2.15	0.46	2.15	1	3	0	2.09
7	504.01	123.22	0.50	2.01	0.50	2.01	1	2	0	2.09
7	505.01	124.52	0.46	2.17	0.46	2.15	0		1	.
7	506.01	153.78	0.49	2.05	0.50	2.01	0		1	.
7	507.01	152.85	0.47	2.12	0.47	2.12	1	1	0	2.09
7	508.01	135.43	0.47	2.11	0.47	2.12	0		1	.
7	509.01	155.35	0.47	2.15	0.47	2.12	0		0	.
7	510.01	136.57	0.48	2.08	0.47	2.12	0		0	.
7	511.01	111.84	0.47	2.11	0.47	2.12	0		0	.
7	512.01	138.27	0.47	2.12	0.47	2.12	0		0	.
7	513.01	171.10	0.48	2.09	0.47	2.12	0		0	.
7	514.01	174.17	0.49	2.03	0.49	2.03	1	2	0	2.12
7	515.01	397.76	0.47	2.13	0.47	2.13	1	3	0	2.12
7	516.01	167.53	0.48	2.09	0.48	2.09	1	1	0	2.12
7	517.01	110.71	0.49	2.02	0.48	2.09	0		1	.
7	518.01	175.24	0.48	2.07	0.48	2.09	0		0	.
7	519.01	169.67	0.47	2.11	0.48	2.09	0		0	.
7	520.01	315.58	0.52	1.94	0.48	2.09	0		0	.
7	521.01	313.42	0.51	1.95	0.48	2.09	0		0	.
7	522.01	312.51	0.46	2.16	0.48	2.09	0		0	.
7	523.01	115.48	0.51	1.95	0.51	1.95	1	2	0	2.09
7	524.01	114.05	0.50	2.01	0.51	1.95	0		1	.
7	525.01	401.53	0.51	1.95	0.51	1.95	0		0	.
7	526.01	538.54	0.53	1.90	0.51	1.95	0		0	.
7	527.01	540.04	0.47	2.11	0.47	2.11	1	3	0	2.09
7	528.01	653.82	0.46	2.18	0.47	2.11	0		1	.
7	529.01	199.63	0.45	2.23	0.47	2.11	0		0	.
7	530.01	188.96	0.50	2.00	0.51	1.95	0		0	.
7	531.01	215.75	0.44	2.25	0.47	2.11	0		0	.
7	532.01	95.29	0.53	1.90	0.51	1.95	0		0	.
7	533.01	96.63	0.44	2.26	0.47	2.11	0		0	.
7	534.01	163.23	0.45	2.24	0.47	2.11	0		0	.
7	535.01	234.60	0.46	2.19	0.46	2.19	1	1	0	2.09

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	536.01	1	1	1	0	1	527	1	1.93	1	175.01
7	537.01	0	1	1	0	1	535	0	1.71	1	215.81
7	538.01	0	0	0	0	1	535	0	1.71	1	215.81
7	539.01	1	1	1	0	1	535	0	1.50	1	215.81
7	540.01	1	0	1	0	1	541	0	1.29	1	164.81
7	541.01	1	.	1	0	3	541	0	1.29	1	164.81
7	542.01	1	0	1	0	1	541	0	1.29	1	256.61
7	543.01	1	0	1	0	1	541	0	1.50	1	205.61
7	544.01	1	0	1	0	1	541	0	1.29	1	256.61
7	545.01	1	0	1	0	1	541	0	1.50	2	256.61
7	546.01	0	1	0	0	1	541	0	2.14	2	256.61
7	547.01	0	0	0	0	1	541	0	1.71	1	175.01
7	548.01	0	0	1	0	1	541	0	2.36	1	175.01
7	549.01	1	1	1	0	1	541	0	1.71	2	154.61
7	550.01	1	0	1	0	1	541	0	1.71	2	154.61
7	551.01	1	0	1	0	1	541	0	1.93	1	154.61
7	552.01	1	1	1	0	1	541	0	1.71	2	195.41
7	553.01	0	1	1	0	1	541	0	1.93	1	185.21
7	554.01	1	0	1	0	1	541	0	2.14	1	134.21
7	555.01	1	0	1	0	1	541	0	1.71	2	205.61
7	556.01	1	1	1	0	1	541	0	2.14	2	215.81
7	557.01	0	1	1	0	1	541	0	1.71	1	175.01
7	558.01	0	0	0	0	1	541	0	1.71	1	175.01
7	559.01	1	0	0	0	1	541	0	2.14	1	256.61
7	560.01	0	1	1	0	1	541	0	2.14	1	175.01
7	561.01	1	1	1	0	1	541	0	1.71	2	215.81
7	562.01	0	1	0	0	1	541	0	1.29	1	154.61
7	563.01	0	0	0	0	2	541	0	1.07	1	205.61
7	564.01	1	0	1	0	1	565	0	0.86	1	215.81
7	565.01	1	.	1	0	.	565	0	0.43	1	205.61
7	566.01	1	0	0	0	1	565	0	1.29	1	256.61
7	567.01	1	0	1	0	1	565	0	1.29	1	256.61
7	568.01	0	1	1	0	1	565	0	1.29	1	164.81
7	569.01	0	0	1	0	1	565	0	1.50	1	195.41
7	570.01	0	0	0	0	2	565	0	1.29	1	164.81
7	571.01	1	1	1	0	1	565	0	1.71	2	256.61
7	572.01	0	1	1	0	1	565	0	1.50	1	215.81
7	573.01	1	1	0	0	1	565	0	1.50	2	256.61
7	574.01	0	.	1	0	2	574	0	1.93	1	256.61
7	575.01	0	0	1	0	1	574	0	1.93	2	256.61
7	576.01	1	0	1	0	1	574	0	1.71	0	256.61
7	577.01	1	1	1	0	1	574	0	1.71	1	256.61
7	578.01	1	0	0	0	1	574	0	1.93	2	256.61
7	579.01	1	0	1	0	1	574	0	2.14	1	256.61
7	580.01	1	0	1	0	2	574	0	1.93	1	256.61
7	581.01	0	1	0	0	1	574	0	2.14	1	154.61
7	582.01	0	0	0	0	1	574	0	2.36	1	195.41
7	583.01	0	0	0	0	1	574	0	2.14	2	236.21
7	584.01	0	0	1	0	1	574	0	1.93	2	236.21
7	585.01	1	1	1	0	1	574	0	2.14	1	256.61

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	536.01	164.46	0.47	2.13	0.47	2.11	0		0	.
7	537.01	165.80	0.46	2.17	0.46	2.19	0		1	.
7	538.01	172.77	0.46	2.17	0.46	2.19	0		0	.
7	539.01	254.05	0.46	2.19	0.46	2.19	0		0	.
7	540.01	252.09	0.46	2.18	0.46	2.18	0		1	.
7	541.01	118.18	0.46	2.18	0.46	2.18	1	0	0	2.19
7	542.01	188.89	0.46	2.19	0.46	2.18	0		0	.
7	543.01	125.02	0.46	2.18	0.46	2.18	0		0	.
7	544.01	126.33	0.46	2.18	0.46	2.18	0		0	.
7	545.01	126.83	0.46	2.18	0.46	2.18	0		0	.
7	546.01	222.49	0.45	2.21	0.46	2.18	0		0	.
7	547.01	225.19	0.47	2.14	0.46	2.18	0		0	.
7	548.01	348.65	0.47	2.14	0.46	2.18	0		0	.
7	549.01	336.30	0.46	2.18	0.46	2.18	0		0	.
7	550.01	355.59	0.46	2.17	0.46	2.18	0		0	.
7	551.01	228.50	0.47	2.13	0.46	2.18	0		0	.
7	552.01	230.63	0.46	2.17	0.46	2.18	0		0	.
7	553.01	452.62	0.47	2.11	0.46	2.18	0		0	.
7	554.01	192.52	0.46	2.15	0.46	2.18	0		0	.
7	555.01	217.11	0.48	2.10	0.46	2.18	0		0	.
7	556.01	274.31	0.48	2.09	0.46	2.18	0		0	.
7	557.01	276.34	0.46	2.18	0.46	2.18	0		0	.
7	558.01	130.30	0.45	2.21	0.46	2.18	0		0	.
7	559.01	268.20	0.46	2.16	0.46	2.18	0		0	.
7	560.01	220.45	0.47	2.13	0.46	2.18	0		0	.
7	561.01	364.13	0.47	2.13	0.46	2.18	0		0	.
7	562.01	210.54	0.48	2.08	0.46	2.18	0		0	.
7	563.01	207.64	0.48	2.07	0.46	2.18	0		0	.
7	564.01	191.22	0.45	2.22	0.45	2.23	0		1	.
7	565.01	133.73	0.45	2.23	0.45	2.23	1	0	0	2.18
7	566.01	132.73	0.45	2.24	0.45	2.23	0		0	.
7	567.01	292.79	0.44	2.27	0.45	2.23	0		0	.
7	568.01	256.19	0.45	2.24	0.45	2.23	0		0	.
7	569.01	297.36	0.44	2.25	0.45	2.23	0		0	.
7	570.01	168.33	0.45	2.21	0.45	2.23	0		0	.
7	571.01	222.72	0.44	2.27	0.45	2.23	0		0	.
7	572.01	178.74	0.46	2.18	0.45	2.23	0		0	.
7	573.01	170.87	0.45	2.23	0.45	2.23	0		0	.
7	574.01	180.71	0.46	2.16	0.46	2.16	1	1	0	2.23
7	575.01	174.14	0.46	2.18	0.46	2.16	0		1	.
7	576.01	172.77	0.50	2.00	0.46	2.16	0		0	.
7	577.01	178.18	0.47	2.12	0.46	2.16	0		0	.
7	578.01	176.28	0.48	2.08	0.46	2.16	0		0	.
7	579.01	176.11	0.49	2.05	0.46	2.16	0		0	.
7	580.01	431.83	0.48	2.07	0.46	2.16	0		0	.
7	581.01	278.18	0.48	2.06	0.46	2.16	0		0	.
7	582.01	223.92	0.48	2.07	0.46	2.16	0		0	.
7	583.01	225.96	0.49	2.03	0.46	2.16	0		0	.
7	584.01	188.42	0.49	2.04	0.46	2.16	0		0	.
7	585.01	187.85	0.49	2.04	0.46	2.16	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	586.01	1	0	1	0	1	574	0	1.93	2	256.61
7	587.01	1	0	1	0	1	574	0	1.93	2	215.81
7	588.01	0	1	0	0	1	574	0	1.93	2	256.61
7	589.01	1	0	1	0	1	574	0	2.14	1	154.61
7	590.01	0	0	1	0	1	574	0	2.36	1	205.61
7	591.01	0	0	1	0	2	574	0	1.93	1	195.41
7	592.01	0	0	1	1	2	574	0	1.07	2	256.61
7	593.01	1	1	1	0	1	574	0	1.07	1	256.61
7	594.01	0	1	0	0	1	574	0	1.50	2	256.61
7	595.01	1	1	1	0	1	574	0	1.29	1	256.61
7	596.01	0	1	0	0	1	574	0	1.29	2	226.01
7	597.01	1	1	1	0	1	574	0	1.29	1	256.61
7	598.01	0	1	0	0	1	574	0	1.29	1	256.61
7	599.01	1	0	1	0	1	574	0	1.29	2	256.61
7	600.01	1	1	1	0	1	601	0	1.71	2	256.61
7	601.01	1	.	1	0	2	601	0	1.50	1	256.61
7	602.01	0	1	0	0	1	601	0	1.50	1	83.20
7	603.01	0	1	1	0	1	601	0	1.29	1	256.61
7	604.01	1	1	1	0	2	601	0	1.50	1	256.61
7	605.01	0	1	1	0	1	601	0	1.71	2	256.61
7	606.01	1	1	1	0	1	601	0	1.71	1	195.41
7	607.01	0	1	1	0	1	601	0	2.14	2	185.21
7	608.01	1	1	1	0	1	601	0	1.71	2	226.01
7	609.01	0	0	1	0	1	601	0	1.93	1	256.61
7	610.01	1	0	1	0	1	601	0	2.14	1	256.61
7	611.01	1	0	0	0	1	601	0	1.29	2	256.61
7	612.01	0	1	1	0	1	601	0	1.93	1	256.61
7	613.01	0	0	1	0	1	601	0	2.36	2	226.01
7	614.01	1	1	1	0	1	601	0	1.71	1	256.61
7	615.01	1	0	1	0	1	601	0	1.71	2	256.61
7	616.01	1	0	1	0	1	601	0	1.93	1	256.61
7	617.01	0	1	1	0	1	601	0	2.14	2	226.01
7	618.01	1	0	1	0	1	601	0	2.14	2	226.01
7	619.01	1	1	1	0	1	601	0	1.71	1	154.61
7	620.01	1	0	0	0	1	601	0	1.71	1	154.61
7	621.01	1	0	1	0	1	601	0	1.93	1	215.81
7	622.01	1	0	1	0	1	601	0	1.50	1	215.81
7	623.01	1	0	1	0	2	601	0	1.29	1	154.61
7	624.01	1	0	1	1	1	601	0	1.07	2	154.61
7	625.01	1	0	1	0	1	601	0	1.29	1	175.01
7	626.01	1	0	1	0	1	601	0	1.29	2	226.01
7	627.01	1	0	1	0	1	601	0	1.07	1	226.01
7	628.01	1	.	1	0	2	628	0	1.50	1	154.61
7	629.01	1	.	1	0	2	629	0	0.86	1	154.61
7	630.01	1	0	0	0	2	629	0	1.29	1	195.41
7	631.01	0	.	0	0	1	631	0	1.71	2	256.61
7	632.01	1	1	1	0	1	631	0	1.29	0	256.61
7	633.01	0	1	0	0	1	631	0	1.93	1	52.60
7	634.01	0	0	1	0	1	631	0	1.71	2	226.01
7	635.01	1	1	1	0	1	631	0	1.93	1	226.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	586.01	272.87	0.49	2.04	0.46	2.16	0		0	.
7	587.01	193.66	0.49	2.03	0.46	2.16	0		0	.
7	588.01	437.41	0.50	1.99	0.46	2.16	0		0	.
7	589.01	223.49	0.49	2.04	0.46	2.16	0		0	.
7	590.01	288.36	0.50	2.01	0.46	2.16	0		0	.
7	591.01	201.83	0.50	1.99	0.46	2.16	0		0	.
7	592.01	184.18	0.50	2.01	0.46	2.16	0		0	.
7	593.01	213.98	0.49	2.05	0.46	2.16	0		0	.
7	594.01	186.62	0.50	2.00	0.46	2.16	0		0	.
7	595.01	250.38	0.49	2.02	0.46	2.16	0		0	.
7	596.01	191.79	0.49	2.04	0.46	2.16	0		0	.
7	597.01	195.03	0.50	2.02	0.46	2.16	0		0	.
7	598.01	199.03	0.51	1.95	0.46	2.16	0		0	.
7	599.01	232.23	0.49	2.03	0.46	2.16	0		0	.
7	600.01	197.83	0.50	1.99	0.49	2.02	0		0	.
7	601.01	670.90	0.49	2.02	0.49	2.02	1	0	0	2.16
7	602.01	201.70	0.50	2.00	0.49	2.02	0		1	.
7	603.01	240.27	0.51	1.97	0.49	2.02	0		0	.
7	604.01	217.32	0.50	1.98	0.49	2.02	0		0	.
7	605.01	341.14	0.49	2.03	0.49	2.02	0		0	.
7	606.01	311.71	0.50	2.00	0.49	2.02	0		0	.
7	607.01	262.63	0.49	2.02	0.49	2.02	0		0	.
7	608.01	241.01	0.50	2.02	0.49	2.02	0		0	.
7	609.01	210.14	0.50	1.98	0.49	2.02	0		0	.
7	610.01	207.07	0.52	1.93	0.49	2.02	0		0	.
7	611.01	256.86	0.50	2.00	0.49	2.02	0		0	.
7	612.01	273.34	0.50	1.99	0.49	2.02	0		0	.
7	613.01	242.54	0.49	2.03	0.49	2.02	0		0	.
7	614.01	213.01	0.51	1.97	0.49	2.02	0		0	.
7	615.01	215.21	0.51	1.96	0.49	2.02	0		0	.
7	616.01	308.94	0.50	2.01	0.49	2.02	0		0	.
7	617.01	306.67	0.51	1.97	0.49	2.02	0		0	.
7	618.01	505.24	0.50	1.99	0.49	2.02	0		0	.
7	619.01	530.50	0.48	2.09	0.49	2.02	0		0	.
7	620.01	302.10	0.47	2.12	0.49	2.02	0		0	.
7	621.01	302.00	0.48	2.09	0.49	2.02	0		0	.
7	622.01	496.47	0.49	2.05	0.49	2.02	0		0	.
7	623.01	498.27	0.50	2.01	0.49	2.02	0		0	.
7	624.01	501.80	0.49	2.06	0.49	2.02	0		0	.
7	625.01	313.38	0.48	2.06	0.49	2.02	0		0	.
7	626.01	311.14	0.46	2.15	0.49	2.02	0		0	.
7	627.01	509.04	0.47	2.11	0.49	2.02	0		0	.
7	628.01	529.46	0.48	2.10	0.48	2.10	1	0	0	2.02
7	629.01	353.25	0.47	2.11	0.47	2.11	1	0	0	2.10
7	630.01	273.81	0.47	2.11	0.47	2.11	0		1	.
7	631.01	272.34	0.47	2.14	0.47	2.14	1	1	0	2.11
7	632.01	818.55	0.47	2.13	0.47	2.14	0		1	.
7	633.01	271.07	0.47	2.13	0.47	2.14	0		0	.
7	634.01	323.92	0.45	2.24	0.47	2.14	0		0	.
7	635.01	306.07	0.47	2.13	0.47	2.14	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	636.01	0	.	0	0	2	636	0	1.71	1	256.61
7	637.01	0	0	0	0	1	636	0	1.50	2	256.61
7	638.01	0	0	0	0	1	636	0	1.29	1	185.21
7	639.01	0	0	0	0	1	636	0	1.71	1	256.61
7	640.01	0	0	0	0	1	636	0	1.29	0	205.61
7	641.01	1	0	1	0	2	642	0	1.29	1	215.81
7	642.01	1	.	1	0	2	642	0	1.29	1	205.61
7	643.01	1	0	1	0	1	642	0	1.29	1	215.81
7	644.01	0	.	1	0	2	644	0	0.86	1	62.80
7	645.01	0	.	0	0	2	645	0	1.07	1	185.21
7	646.01	0	.	1	0	1	646	0	1.07	2	185.21
7	647.01	0	1	0	0	1	642	0	1.29	2	246.41
7	648.01	0	.	1	0	3	648	0	0.43	2	236.21
7	649.01	0	.	0	0	1	649	0	0.64	2	236.21
7	650.01	0	.	0	0	2	650	0	0.64	1	185.21
7	651.01	0	.	0	0	.	651	0	0.43	0	215.81
7	652.01	1	.	1	0	.	652	0	0.43	1	73.00
7	653.01	1	0	1	0	1	652	0	0.86	1	73.00
7	654.01	0	1	0	0	1	652	0	1.07	1	73.00
7	655.01	0	.	1	0	3	655	0	0.86	1	124.01
7	656.01	0	.	1	0	.	656	0	0.43	2	185.21
7	657.01	0	.	1	0	.	657	0	0.43	1	236.21
7	658.01	1	.	1	0	.	658	0	0.43	2	154.61
7	659.01	0	.	1	0	.	659	0	0.43	0	246.41
7	661.01	0	.	0	0	.	661	0	0.43	1	236.21
7	662.01	0	0	0	0	1	661	0	0.86	2	236.21
7	663.01	1	.	1	0	.	663	0	0.43	1	246.41
7	664.01	1	.	1	0	.	664	0	0.43	1	256.61
7	665.01	1	0	1	0	1	41	1	1.50	1	1.60
7	3.02	0	.	0	0	.	3	0	0.36	0	12.78
7	4.02	0	.	0	0	1	4	0	0.54	2	22.98
7	18.02	0	.	0	0	3	18	0	0.54	1	22.98
7	19.02	1	.	1	0	2	19	0	0.90	1	22.98
7	20.02	1	.	1	0	1	20	0	0.72	1	2.58
7	23.02	0	.	0	0	1	23	0	0.72	0	2.58
7	24.02	1	.	1	0	.	24	0	0.36	1	2.58
7	25.02	1	1	0	0	1	23	0	0.90	2	53.58
7	28.02	1	.	1	0	3	28	0	0.72	0	2.58
7	30.02	0	.	1	0	1	30	0	1.08	1	12.78
7	31.02	0	.	0	0	2	31	0	0.72	1	2.58
7	32.02	1	.	1	0	1	32	0	1.08	2	22.98
7	33.02	0	0	0	0	1	31	0	0.90	1	2.58
7	34.02	0	.	0	0	1	34	0	1.44	1	2.58
7	35.02	1	1	0	0	1	34	0	1.26	2	22.98
7	36.02	0	0	1	0	1	34	0	1.62	1	43.38
7	37.02	0	1	0	0	1	34	0	1.44	1	43.38
7	38.02	1	.	1	0	3	38	0	1.26	2	22.98
7	39.02	0	.	1	0	1	39	0	0.90	2	12.78
7	40.02	1	.	0	0	1	40	1	1.26	2	12.78
7	41.02	1	.	1	0	3	41	0	1.08	1	2.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	636.01	307.37	0.48	2.09	0.48	2.09	1	0	0	2.14
7	637.01	415.95	0.53	1.90	0.48	2.09	0		1	.
7	638.01	460.16	0.49	2.03	0.48	2.09	0		0	.
7	639.01	430.26	0.50	1.99	0.48	2.09	0		0	.
7	640.01	343.64	0.48	2.07	0.48	2.09	0		0	.
7	641.01	422.65	0.50	2.00	0.49	2.03	0		1	.
7	642.01	594.89	0.49	2.03	0.49	2.03	1	0	0	2.09
7	643.01	883.41	0.50	2.00	0.49	2.03	0		0	.
7	644.01	592.63	0.68	1.47	0.68	1.47	1	1	0	1.88
7	645.01	595.33	0.53	1.88	0.53	1.88	1	1	0	2.03
7	646.01	651.72	0.49	2.05	0.49	2.05	1	3	0	1.47
7	647.01	697.19	0.51	1.95	0.49	2.03	0		0	.
7	648.01	694.93	0.85	1.17	0.85	1.17	1	0	0	1.13
7	649.01	102.77	0.82	1.22	0.82	1.22	1	1	0	1.47
7	650.01	531.93	0.88	1.13	0.88	1.13	1	1	0	1.22
7	651.01	933.76	0.89	1.12	0.89	1.12	1	0	0	1.17
7	652.01	935.10	0.62	1.62	0.62	1.62	1	0	0	1.12
7	653.01	936.30	0.61	1.63	0.62	1.62	0		1	.
7	654.01	822.75	0.63	1.59	0.62	1.62	0		0	.
7	655.01	721.59	0.65	1.53	0.65	1.53	1	0	0	1.62
7	656.01	770.43	1.55	0.64	1.55	0.64	1	0	0	1.62
7	657.01	1072.34	0.62	1.62	0.62	1.62	1	0	0	1.53
7	658.01	979.98	0.86	1.17	0.86	1.17	1	0	0	0.64
7	659.01	1252.95	0.88	1.13	0.88	1.13	1	0	0	1.17
7	661.01	1010.74	0.65	1.53	0.65	1.53	1	4	0	1.13
7	662.01	1222.05	0.59	1.70	0.65	1.53	0		0	.
7	663.01	1049.52	0.89	1.13	0.89	1.13	1	0	0	1.53
7	664.01	142.65	0.89	1.12	0.89	1.12	1	2	0	1.13
7	665.01	66.36	0.59	1.70	0.68	1.48	0		0	.
7	3.02	42.48	1.10	0.91	1.10	0.91	1	0	0	.
7	4.02	54.59	1.53	0.65	1.53	0.65	1	0	0	0.91
7	18.02	46.81	0.71	1.42	0.71	1.42	1	0	0	0.65
7	19.02	48.02	0.74	1.35	0.74	1.35	1	1	0	1.42
7	20.02	81.64	0.84	1.19	0.84	1.19	1	1	0	1.35
7	23.02	87.38	0.85	1.17	0.85	1.17	1	1	0	1.31
7	24.02	86.12	0.76	1.31	0.76	1.31	1	0	0	1.19
7	25.02	46.68	0.84	1.19	0.85	1.17	0		1	.
7	28.02	91.22	0.76	1.31	0.76	1.31	1	0	0	1.17
7	30.02	96.26	0.81	1.24	0.81	1.24	1	2	0	1.22
7	31.02	96.09	0.82	1.22	0.82	1.22	1	1	0	1.31
7	32.02	68.47	0.76	1.32	0.76	1.32	1	3	0	1.22
7	33.02	96.89	0.81	1.24	0.82	1.22	0		1	.
7	34.02	99.40	0.77	1.30	0.77	1.30	1	1	0	1.22
7	35.02	74.71	0.78	1.28	0.77	1.30	0		1	.
7	36.02	65.30	0.79	1.27	0.77	1.30	0		0	.
7	37.02	64.19	0.78	1.29	0.77	1.30	0		0	.
7	38.02	83.88	0.80	1.25	0.80	1.25	1	0	0	1.30
7	39.02	108.80	0.90	1.12	0.90	1.12	1	2	0	1.25
7	40.02	112.24	0.77	1.30	0.77	1.30	1	2	0	1.25
7	41.02	101.80	0.64	1.57	0.64	1.57	1	3	0	1.25

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	42.02	1	0	1	0	1	45	1	1.44	1	2.58
7	43.02	1	.	1	0	1	43	1	1.26	2	22.98
7	45.02	1	.	0	0	1	45	1	1.26	1	2.58
7	46.02	1	.	1	0	1	46	1	1.80	1	2.58
7	47.02	1	0	1	0	1	43	1	1.26	2	43.38
7	48.02	0	.	0	1	1	48	1	1.62	0	43.38
7	52.02	1	.	1	0	1	52	1	1.26	2	12.78
7	53.02	1	.	1	0	2	53	1	1.26	1	12.78
7	54.02	1	.	1	0	1	54	1	1.80	0	2.58
7	55.02	1	.	1	0	1	55	0	1.80	0	2.58
7	56.02	0	.	1	0	1	56	1	1.26	1	2.58
7	57.02	0	1	0	0	1	55	0	1.98	2	12.78
7	58.02	1	0	1	0	1	55	0	1.80	1	43.38
7	59.02	0	0	0	0	1	55	0	1.62	2	22.98
7	60.02	0	0	0	0	1	55	0	1.62	1	22.98
7	61.02	0	0	0	0	2	55	0	1.44	2	53.58
7	62.02	1	1	1	0	1	55	0	1.80	1	12.78
7	63.02	1	0	1	0	1	55	0	1.44	1	53.58
7	64.02	0	1	0	1	1	55	0	1.62	2	33.18
7	65.02	1	1	1	0	1	55	0	1.44	1	53.58
7	67.02	1	.	1	0	1	67	1	1.26	1	53.58
7	68.02	1	.	1	0	1	68	1	1.44	2	53.58
7	69.02	0	1	0	0	1	67	1	1.26	1	53.58
7	70.02	1	0	1	0	1	68	1	1.26	0	53.58
7	71.02	1	1	1	0	1	67	1	1.08	1	53.58
7	72.02	1	0	1	0	2	68	1	1.44	2	53.58
7	73.02	1	0	1	0	2	67	1	1.08	1	33.18
7	74.02	1	.	1	0	1	74	1	1.26	2	33.18
7	77.02	1	.	0	0	1	77	1	1.26	2	53.58
7	78.02	1	0	1	0	1	77	1	1.26	2	53.58
7	79.02	0	.	0	0	1	79	1	1.26	1	12.78
7	80.02	1	0	1	0	1	77	1	1.80	2	33.18
7	81.02	0	1	1	1	1	77	1	1.62	2	12.78
7	84.02	1	.	1	0	1	84	1	1.08	1	12.78
7	86.02	1	0	1	0	1	84	1	1.26	1	12.78
7	87.02	1	.	1	0	1	87	1	1.62	1	12.78
7	88.02	0	1	0	0	1	87	1	1.80	1	12.78
7	89.02	1	.	1	0	1	89	1	1.62	1	12.78
7	90.02	1	.	1	0	1	90	1	1.80	2	53.58
7	91.02	1	0	1	0	1	89	1	1.62	1	53.58
7	92.02	1	0	0	0	1	90	1	1.98	2	53.58
7	93.02	1	0	0	0	1	90	1	1.98	2	104.58
7	94.02	1	0	1	0	1	90	1	1.98	2	73.98
7	95.02	0	1	0	0	1	89	1	1.98	1	104.58
7	96.02	1	0	0	0	1	90	1	2.16	2	53.58
7	97.02	0	1	0	0	1	90	1	2.34	2	53.58
7	98.02	1	0	1	0	1	90	1	2.52	2	53.58
7	99.02	1	1	1	0	1	89	1	2.16	1	12.78
7	100.02	1	0	1	0	1	89	1	2.16	1	12.78
7	101.02	1	0	1	0	1	89	1	2.52	1	12.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	42.02	109.30	0.63	1.60	0.60	1.67	0		1	.
7	43.02	86.19	0.72	1.39	0.72	1.39	1	2	0	1.67
7	45.02	107.20	0.60	1.67	0.60	1.67	1	4	0	1.25
7	46.02	110.57	0.61	1.65	0.61	1.65	1	3	0	1.67
7	47.02	67.60	0.70	1.42	0.72	1.39	0		1	.
7	48.02	145.48	0.65	1.54	0.65	1.54	1	2	0	1.72
7	52.02	116.75	0.61	1.64	0.61	1.64	1	3	0	1.72
7	53.02	122.12	0.58	1.72	0.58	1.72	1	4	0	1.67
7	54.02	123.25	0.60	1.67	0.60	1.67	1	2	0	1.72
7	55.02	120.82	0.60	1.68	0.60	1.68	1	1	0	1.72
7	56.02	125.69	0.55	1.81	0.55	1.81	1	3	0	1.72
7	57.02	69.10	0.60	1.68	0.60	1.68	0		0	.
7	58.02	93.96	0.59	1.70	0.60	1.68	0		1	.
7	59.02	92.09	0.59	1.71	0.60	1.68	0		0	.
7	60.02	70.23	0.59	1.70	0.60	1.68	0		0	.
7	61.02	130.93	0.59	1.69	0.60	1.68	0		0	.
7	62.02	71.73	0.59	1.68	0.60	1.68	0		0	.
7	63.02	100.03	0.59	1.69	0.60	1.68	0		0	.
7	64.02	47.31	0.58	1.72	0.60	1.68	0		0	.
7	65.02	172.41	0.60	1.68	0.60	1.68	0		0	.
7	67.02	78.78	0.57	1.76	0.57	1.76	1	3	0	1.68
7	68.02	76.57	0.59	1.71	0.59	1.71	1	2	0	1.68
7	69.02	79.94	0.56	1.78	0.57	1.76	0		1	.
7	70.02	81.64	0.59	1.69	0.59	1.71	0		1	.
7	71.02	87.15	0.59	1.69	0.57	1.76	0		0	.
7	72.02	115.22	0.60	1.66	0.59	1.71	0		0	.
7	73.02	114.18	0.60	1.67	0.57	1.76	0		0	.
7	74.02	184.49	0.61	1.63	0.61	1.63	1	1	0	1.68
7	77.02	91.09	0.62	1.60	0.62	1.60	1	2	0	1.63
7	78.02	150.91	0.62	1.61	0.62	1.60	0		1	.
7	79.02	121.22	0.53	1.89	0.53	1.89	1	3	0	1.63
7	80.02	159.49	0.61	1.64	0.62	1.60	0		0	.
7	81.02	192.20	0.61	1.65	0.62	1.60	0		0	.
7	84.02	198.30	0.51	1.98	0.51	1.98	1	3	0	1.63
7	86.02	156.25	0.51	1.95	0.51	1.98	0		1	.
7	87.02	159.69	0.49	2.04	0.49	2.04	1	4	0	1.63
7	88.02	161.32	0.49	2.02	0.49	2.04	0		1	.
7	89.02	95.73	0.50	2.00	0.50	2.00	1	3	0	2.04
7	90.02	93.59	0.54	1.85	0.54	1.85	1	2	0	2.04
7	91.02	97.19	0.51	1.96	0.50	2.00	0		1	.
7	92.02	54.42	0.53	1.87	0.54	1.85	0		1	.
7	93.02	84.08	0.53	1.90	0.54	1.85	0		0	.
7	94.02	40.00	0.53	1.88	0.54	1.85	0		0	.
7	95.02	100.43	0.51	1.95	0.50	2.00	0		0	.
7	96.02	104.13	0.53	1.88	0.54	1.85	0		0	.
7	97.02	99.36	0.55	1.83	0.54	1.85	0		0	.
7	98.02	167.50	0.53	1.90	0.54	1.85	0		0	.
7	99.02	169.60	0.50	1.99	0.50	2.00	0		0	.
7	100.02	170.07	0.50	2.00	0.50	2.00	0		0	.
7	101.02	172.97	0.49	2.03	0.50	2.00	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	102.02	1	.	1	0	1	102	1	2.34	2	12.78
7	104.02	1	.	1	0	1	104	1	2.34	2	33.18
7	105.02	1	.	1	0	1	105	1	2.70	1	12.78
7	106.02	0	1	1	0	1	104	1	2.34	2	33.18
7	107.02	1	1	1	0	1	104	1	2.34	2	73.98
7	109.02	0	1	0	0	1	104	1	2.34	2	43.38
7	110.02	1	.	1	0	1	110	1	2.52	0	22.98
7	111.02	1	.	1	0	1	111	1	2.52	1	33.18
7	112.02	1	0	1	0	1	110	1	2.88	0	22.98
7	116.02	0	.	1	0	1	116	1	2.52	1	53.58
7	117.02	1	.	1	0	1	117	1	2.52	1	53.58
7	118.02	0	0	0	0	1	119	1	2.34	2	22.98
7	119.02	0	.	0	0	1	119	1	2.70	2	53.58
7	121.02	0	1	1	0	1	119	1	2.34	2	12.78
7	123.02	1	0	1	0	1	119	1	2.34	2	22.98
7	124.02	0	.	0	0	1	124	1	2.70	1	33.18
7	126.02	0	.	0	0	1	126	1	2.16	1	12.78
7	127.02	1	.	0	0	1	127	1	2.52	1	53.58
7	128.02	1	0	1	0	1	127	1	2.16	1	12.78
7	129.02	1	.	1	0	1	129	1	2.16	1	33.18
7	130.02	1	1	1	0	1	126	1	1.98	1	63.78
7	131.02	1	.	0	0	1	131	1	2.16	0	2.58
7	132.02	1	0	0	0	1	131	1	2.34	0	2.58
7	133.02	0	1	0	0	1	126	1	1.98	1	63.78
7	134.02	0	0	0	0	1	142	1	2.52	2	53.58
7	139.02	1	.	0	0	1	139	1	2.52	1	2.58
7	140.02	1	1	1	0	1	119	1	2.34	2	53.58
7	141.02	1	0	1	0	1	139	1	2.52	1	53.58
7	142.02	0	.	1	0	1	142	1	2.70	2	22.98
7	143.02	0	0	0	0	1	142	1	2.16	1	22.98
7	144.02	0	1	1	0	1	139	1	2.52	1	22.98
7	145.02	1	0	1	0	1	139	1	2.52	1	22.98
7	146.02	1	1	1	0	1	139	1	2.16	1	2.58
7	148.02	1	0	1	0	1	149	0	2.16	2	12.78
7	149.02	1	.	0	0	1	149	0	1.98	1	33.18
7	150.02	1	0	1	0	1	149	0	2.34	1	12.78
7	151.02	1	0	1	0	1	149	0	2.34	1	43.38
7	152.02	1	0	1	0	2	149	0	2.16	1	53.58
7	153.02	0	.	0	0	2	153	0	1.80	1	53.58
7	154.02	1	1	1	0	1	153	0	1.80	1	53.58
7	155.02	0	.	1	0	2	155	0	1.44	1	12.78
7	156.02	1	1	1	0	1	155	0	1.44	0	12.78
7	157.02	0	0	0	0	1	155	0	1.62	2	53.58
7	158.02	0	1	0	0	1	155	0	1.62	1	53.58
7	159.02	0	0	0	0	1	155	0	2.16	1	53.58
7	160.02	1	1	0	0	1	155	0	2.52	2	63.78
7	161.02	1	0	1	0	1	155	0	2.16	1	53.58
7	162.02	1	.	1	0	1	162	1	2.52	0	94.38
7	163.02	1	0	1	0	1	155	0	2.88	2	94.38
7	164.02	1	.	1	0	1	164	1	2.52	2	53.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	102.02	213.92	0.50	2.01	0.50	2.01	1	4	0	2.04
7	104.02	171.71	0.51	1.95	0.51	1.95	1	2	0	2.01
7	105.02	138.54	0.47	2.13	0.47	2.13	1	3	0	2.01
7	106.02	97.36	0.50	1.98	0.51	1.95	0		1	.
7	107.02	216.75	0.51	1.96	0.51	1.95	0		0	.
7	109.02	137.30	0.51	1.95	0.51	1.95	0		0	.
7	110.02	126.19	0.50	2.01	0.50	2.01	1	4	0	2.01
7	111.02	139.91	0.46	2.15	0.46	2.15	1	3	0	2.01
7	112.02	224.46	0.48	2.08	0.50	2.01	0		1	.
7	116.02	101.60	0.40	2.53	0.40	2.53	1	3	0	2.01
7	117.02	142.01	0.40	2.51	0.40	2.51	1	3	0	2.01
7	118.02	109.07	0.44	2.27	0.44	2.27	0		1	.
7	119.02	230.57	0.44	2.27	0.44	2.27	1	2	0	2.01
7	121.02	232.34	0.47	2.14	0.44	2.27	0		0	.
7	123.02	131.63	0.47	2.14	0.44	2.27	0		0	.
7	124.02	233.27	0.39	2.56	0.39	2.56	1	3	0	2.01
7	126.02	104.20	0.41	2.45	0.41	2.45	1	3	0	2.42
7	127.02	189.08	0.41	2.44	0.41	2.44	1	3	0	2.01
7	128.02	146.98	0.42	2.38	0.41	2.44	0		1	.
7	129.02	73.37	0.41	2.42	0.41	2.42	1	1	0	2.01
7	130.02	196.49	0.41	2.45	0.41	2.45	0		1	.
7	131.02	199.43	0.42	2.36	0.42	2.36	1	1	0	2.42
7	132.02	74.24	0.42	2.39	0.42	2.36	0		1	.
7	133.02	116.21	0.41	2.43	0.41	2.45	0		0	.
7	134.02	247.95	0.45	2.23	0.43	2.33	0		0	.
7	139.02	113.54	0.39	2.57	0.39	2.57	1	3	0	2.36
7	140.02	111.24	0.49	2.05	0.44	2.27	0		0	.
7	141.02	150.02	0.39	2.58	0.39	2.57	0		1	.
7	142.02	151.82	0.43	2.33	0.43	2.33	1	2	0	2.36
7	143.02	153.09	0.44	2.29	0.43	2.33	0		1	.
7	144.02	155.39	0.40	2.53	0.39	2.57	0		0	.
7	145.02	207.27	0.39	2.56	0.39	2.57	0		0	.
7	146.02	261.60	0.40	2.49	0.39	2.57	0		0	.
7	148.02	154.02	0.40	2.50	0.39	2.56	0		1	.
7	149.02	209.67	0.39	2.56	0.39	2.56	1	4	0	2.36
7	150.02	117.18	0.39	2.54	0.39	2.56	0		0	.
7	151.02	118.21	0.40	2.53	0.39	2.56	0		0	.
7	152.02	120.52	0.39	2.53	0.39	2.56	0		0	.
7	153.02	121.82	0.40	2.49	0.40	2.49	1	1	0	2.56
7	154.02	220.05	0.40	2.48	0.40	2.49	0		1	.
7	155.02	222.15	0.41	2.46	0.41	2.46	1	0	0	2.49
7	156.02	126.76	0.41	2.46	0.41	2.46	0		1	.
7	157.02	123.29	0.41	2.46	0.41	2.46	0		0	.
7	158.02	124.22	0.41	2.44	0.41	2.46	0		0	.
7	159.02	98.40	0.41	2.41	0.41	2.46	0		0	.
7	160.02	127.39	0.41	2.43	0.41	2.46	0		0	.
7	161.02	79.11	0.41	2.43	0.41	2.46	0		0	.
7	162.02	76.41	0.43	2.32	0.43	2.32	1	2	0	2.46
7	163.02	131.69	0.42	2.40	0.41	2.46	0		0	.
7	164.02	129.39	0.43	2.31	0.43	2.31	1	2	0	2.46

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	165.02	1	.	1	0	1	165	1	2.34	1	53.58
7	166.02	1	0	1	0	1	165	1	2.70	1	12.78
7	167.02	1	0	1	0	1	164	1	2.34	2	53.58
7	168.02	1	0	1	0	1	165	1	2.34	1	12.78
7	169.02	1	0	1	0	1	164	1	2.88	2	94.38
7	171.02	1	0	1	0	1	164	1	2.52	2	94.38
7	173.02	0	1	1	1	1	164	1	2.88	2	94.38
7	175.02	1	1	1	0	1	164	1	2.88	2	53.58
7	176.02	1	0	1	0	1	164	1	2.52	2	53.58
7	177.02	1	.	1	0	1	177	1	2.70	1	22.98
7	178.02	1	0	1	0	1	177	1	2.88	1	22.98
7	179.02	1	0	1	0	1	177	1	2.70	1	22.98
7	180.02	1	0	1	0	1	177	1	2.70	1	53.58
7	181.02	0	1	0	0	1	164	1	2.52	2	53.58
7	182.02	0	0	0	0	1	164	1	2.52	2	63.78
7	183.02	1	0	1	0	1	177	1	2.70	1	53.58
7	184.02	1	0	1	0	1	177	1	2.70	1	53.58
7	185.02	0	1	0	0	1	177	1	2.88	1	22.98
7	186.02	0	0	1	0	1	177	1	2.88	1	43.38
7	187.02	0	0	0	0	1	164	1	2.16	2	43.38
7	188.02	1	1	1	0	1	164	1	2.16	2	63.78
7	191.02	0	0	0	0	1	192	1	2.34	1	2.58
7	192.02	0	.	0	0	1	192	1	1.98	1	2.58
7	193.02	1	1	1	0	1	164	1	1.98	2	73.98
7	194.02	0	1	1	1	1	164	1	2.16	2	73.98
7	195.02	1	0	1	0	1	164	1	2.34	2	53.58
7	196.02	1	0	1	0	1	192	1	1.98	1	53.58
7	197.02	1	1	1	0	1	192	1	2.16	1	53.58
7	198.02	0	1	1	0	1	164	1	1.98	0	12.78
7	199.02	1	0	0	0	1	192	1	1.62	1	53.58
7	200.02	0	1	0	0	1	192	1	1.98	1	104.58
7	201.02	0	0	1	0	1	192	1	1.98	0	104.58
7	202.02	1	1	0	0	1	192	1	1.98	1	63.78
7	203.02	1	0	0	0	1	192	1	1.98	1	63.78
7	204.02	1	.	1	0	1	204	0	2.16	0	73.98
7	205.02	1	0	1	0	2	204	0	1.98	1	53.58
7	207.02	0	1	0	0	1	204	0	1.44	2	12.78
7	208.02	1	1	1	0	1	209	0	1.80	0	73.98
7	209.02	0	.	1	0	2	209	0	1.62	1	73.98
7	210.02	0	1	1	0	1	209	0	1.80	1	12.78
7	211.02	0	0	0	0	1	209	0	1.80	2	53.58
7	212.02	1	0	1	0	1	209	0	1.98	2	94.38
7	213.02	1	1	1	0	1	209	0	1.62	1	94.38
7	214.02	0	.	0	0	1	214	1	1.62	1	12.78
7	215.02	0	.	0	0	1	215	1	1.80	0	12.78
7	216.02	0	.	1	0	1	216	1	1.98	0	53.58
7	217.02	1	.	1	0	1	217	1	2.16	1	53.58
7	218.02	0	0	1	0	1	216	1	2.52	2	22.98
7	219.02	0	1	0	0	1	217	1	2.34	1	22.98
7	220.02	0	.	1	0	1	220	1	2.16	1	94.38

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	165.02	229.29	0.40	2.48	0.40	2.48	1	3	0	2.46
7	166.02	135.80	0.41	2.46	0.40	2.48	0		1	.
7	167.02	231.56	0.43	2.34	0.43	2.31	0		1	.
7	168.02	82.78	0.41	2.46	0.40	2.48	0		0	.
7	169.02	314.04	0.44	2.26	0.43	2.31	0		0	.
7	171.02	289.33	0.45	2.23	0.43	2.31	0		0	.
7	173.02	291.56	0.43	2.33	0.43	2.31	0		0	.
7	175.02	144.04	0.43	2.31	0.43	2.31	0		0	.
7	176.02	174.58	0.43	2.33	0.43	2.31	0		0	.
7	177.02	177.54	0.38	2.64	0.38	2.64	1	3	0	2.46
7	178.02	180.15	0.38	2.64	0.38	2.64	0		1	.
7	179.02	133.63	0.38	2.66	0.38	2.64	0		0	.
7	180.02	150.65	0.38	2.64	0.38	2.64	0		0	.
7	181.02	114.85	0.45	2.23	0.43	2.31	0		0	.
7	182.02	136.17	0.47	2.14	0.43	2.31	0		0	.
7	183.02	137.03	0.38	2.62	0.38	2.64	0		0	.
7	184.02	185.72	0.38	2.61	0.38	2.64	0		0	.
7	185.02	142.84	0.39	2.59	0.38	2.64	0		0	.
7	186.02	151.85	0.39	2.59	0.38	2.64	0		0	.
7	187.02	125.66	0.46	2.15	0.43	2.31	0		0	.
7	188.02	304.97	0.46	2.15	0.43	2.31	0		0	.
7	191.02	256.72	0.37	2.72	0.36	2.76	0		1	.
7	192.02	129.83	0.36	2.76	0.36	2.76	1	3	0	2.46
7	193.02	129.19	0.45	2.20	0.43	2.31	0		0	.
7	194.02	162.19	0.45	2.22	0.43	2.31	0		0	.
7	195.02	147.74	0.45	2.21	0.43	2.31	0		0	.
7	196.02	146.61	0.36	2.81	0.36	2.76	0		0	.
7	197.02	274.17	0.36	2.78	0.36	2.76	0		0	.
7	198.02	149.15	0.44	2.30	0.43	2.31	0		0	.
7	199.02	58.09	0.36	2.79	0.36	2.76	0		0	.
7	200.02	57.02	0.35	2.85	0.36	2.76	0		0	.
7	201.02	121.89	0.35	2.85	0.36	2.76	0		0	.
7	202.02	123.09	0.35	2.84	0.36	2.76	0		0	.
7	203.02	132.13	0.35	2.86	0.36	2.76	0		0	.
7	204.02	169.07	0.37	2.74	0.37	2.74	1	1	0	2.46
7	205.02	337.27	0.38	2.67	0.37	2.74	0		1	.
7	207.02	135.23	0.39	2.56	0.37	2.74	0		0	.
7	208.02	133.33	0.38	2.67	0.38	2.67	0		1	.
7	209.02	286.48	0.38	2.67	0.38	2.67	1	4	0	2.74
7	210.02	173.24	0.38	2.66	0.38	2.67	0		0	.
7	211.02	97.43	0.39	2.59	0.38	2.67	0		0	.
7	212.02	95.69	0.38	2.62	0.38	2.67	0		0	.
7	213.02	295.72	0.38	2.63	0.38	2.67	0		0	.
7	214.02	293.63	0.39	2.60	0.39	2.60	1	2	0	2.67
7	215.02	178.51	0.37	2.67	0.37	2.67	1	3	0	2.67
7	216.02	176.77	0.37	2.67	0.37	2.67	1	2	0	2.67
7	217.02	235.14	0.37	2.69	0.37	2.69	1	3	0	2.67
7	218.02	232.13	0.37	2.68	0.37	2.67	0		1	.
7	219.02	102.17	0.37	2.73	0.37	2.69	0		1	.
7	220.02	66.84	0.37	2.70	0.37	2.70	1	3	0	2.67

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	221.02	0	0	0	0	1	216	1	2.70	2	124.98
7	222.02	1	1	1	0	1	216	1	2.34	2	73.98
7	223.02	1	.	1	0	1	223	1	2.34	1	12.78
7	224.02	1	0	1	0	1	223	1	2.52	1	53.58
7	225.02	0	.	1	0	1	225	1	2.52	2	84.18
7	226.02	1	.	1	0	1	226	1	2.16	1	94.38
7	227.02	1	1	1	0	1	225	1	2.16	2	73.98
7	228.02	1	0	0	0	1	226	1	2.52	1	53.58
7	229.02	1	0	1	0	1	225	1	2.70	2	73.98
7	230.02	1	0	0	0	1	226	1	2.52	1	53.58
7	231.02	1	0	1	0	1	225	1	2.70	2	53.58
7	232.02	0	1	0	0	1	226	1	2.52	1	53.58
7	233.02	1	1	1	0	1	226	1	2.70	1	53.58
7	234.02	1	0	1	0	1	225	1	2.34	2	43.38
7	235.02	1	0	1	0	1	225	1	2.16	2	43.38
7	236.02	1	.	1	1	1	236	1	2.16	1	43.38
7	240.02	1	.	1	0	1	240	1	2.34	1	33.18
7	241.02	0	1	0	0	1	225	1	2.34	2	73.98
7	242.02	1	1	1	0	1	225	1	2.34	2	124.98
7	243.02	0	1	0	0	2	225	1	1.98	2	124.98
7	244.02	0	0	1	0	1	225	1	2.34	2	124.98
7	245.02	1	1	1	0	1	225	1	2.34	2	73.98
7	246.02	1	0	1	0	1	240	1	2.16	1	73.98
7	247.02	1	0	1	0	1	240	1	2.34	1	73.98
7	248.02	0	1	0	0	1	225	1	2.88	2	63.78
7	249.02	1	0	1	0	1	240	1	2.34	1	73.98
7	250.02	0	0	1	0	1	225	1	2.52	2	73.98
7	251.02	0	1	0	0	1	240	1	2.34	1	53.58
7	252.02	0	1	1	0	1	240	1	2.16	1	165.78
7	253.02	1	.	1	0	1	253	0	2.34	1	53.58
7	254.02	1	1	1	0	1	240	1	2.34	1	63.78
7	255.02	0	0	0	0	1	240	1	2.70	1	165.78
7	256.02	1	0	1	0	1	253	0	1.98	2	73.98
7	257.02	1	0	1	0	1	253	0	2.16	1	53.58
7	258.02	1	.	1	0	1	258	0	2.16	1	73.98
7	259.02	0	.	1	0	1	259	0	2.34	2	53.58
7	260.02	0	1	1	0	1	262	0	2.34	2	73.98
7	261.02	1	1	1	0	1	262	0	2.52	2	73.98
7	262.02	1	.	1	0	1	262	0	2.16	1	63.78
7	263.02	0	0	0	1	1	262	0	2.34	1	53.58
7	264.02	0	1	0	0	1	262	0	2.34	2	73.98
7	265.02	1	0	1	0	1	262	0	2.34	1	73.98
7	266.02	1	.	1	0	1	266	0	2.16	2	73.98
7	267.02	1	.	1	0	1	267	0	2.16	1	73.98
7	268.02	1	0	1	0	1	269	0	1.98	2	73.98
7	269.02	1	.	1	0	1	269	0	2.34	1	22.98
7	270.02	0	0	0	0	1	272	1	2.34	2	114.78
7	272.02	0	.	1	0	1	272	1	2.16	2	53.58
7	273.02	0	0	1	0	1	272	1	1.98	2	135.18
7	274.02	1	0	1	0	1	275	1	1.98	1	22.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	221.02	141.71	0.39	2.58	0.37	2.67	0		0	.
7	222.02	302.90	0.39	2.59	0.37	2.67	0		0	.
7	223.02	178.88	0.36	2.75	0.36	2.75	1	3	0	2.67
7	224.02	107.97	0.37	2.73	0.36	2.75	0		1	.
7	225.02	104.14	0.38	2.66	0.38	2.66	1	2	0	2.67
7	226.02	149.85	0.37	2.73	0.37	2.73	1	3	0	2.67
7	227.02	182.35	0.38	2.60	0.38	2.66	0		1	.
7	228.02	143.51	0.37	2.70	0.37	2.73	0		1	.
7	229.02	183.98	0.38	2.64	0.38	2.66	0		0	.
7	230.02	194.36	0.37	2.71	0.37	2.73	0		0	.
7	231.02	187.82	0.39	2.57	0.38	2.66	0		0	.
7	232.02	189.49	0.38	2.64	0.37	2.73	0		0	.
7	233.02	196.86	0.38	2.64	0.37	2.73	0		0	.
7	234.02	195.19	0.37	2.73	0.38	2.66	0		0	.
7	235.02	193.19	0.37	2.73	0.38	2.66	0		0	.
7	236.02	374.88	0.36	2.76	0.36	2.76	1	3	0	2.67
7	240.02	156.75	0.34	2.92	0.34	2.92	1	3	0	2.67
7	241.02	70.87	0.35	2.85	0.38	2.66	0		0	.
7	242.02	71.81	0.35	2.82	0.38	2.66	0		0	.
7	243.02	76.04	0.36	2.77	0.38	2.66	0		0	.
7	244.02	166.00	0.37	2.73	0.38	2.66	0		0	.
7	245.02	145.48	0.37	2.73	0.38	2.66	0		0	.
7	246.02	155.32	0.33	3.04	0.34	2.92	0		1	.
7	247.02	168.47	0.34	2.90	0.34	2.92	0		0	.
7	248.02	158.29	0.37	2.72	0.38	2.66	0		0	.
7	249.02	164.66	0.34	2.93	0.34	2.92	0		0	.
7	250.02	201.80	0.36	2.76	0.38	2.66	0		0	.
7	251.02	39.07	0.35	2.87	0.34	2.92	0		0	.
7	252.02	209.27	0.34	2.91	0.34	2.92	0		0	.
7	253.02	160.72	0.35	2.85	0.35	2.85	1	1	0	2.67
7	254.02	39.91	0.34	2.91	0.34	2.92	0		0	.
7	255.02	165.36	0.34	2.93	0.34	2.92	0		0	.
7	256.02	213.31	0.36	2.78	0.35	2.85	0		1	.
7	257.02	166.43	0.36	2.80	0.35	2.85	0		0	.
7	258.02	218.98	0.36	2.80	0.36	2.80	1	3	0	2.85
7	259.02	172.54	0.36	2.75	0.36	2.75	1	2	0	2.85
7	260.02	176.27	0.37	2.71	0.36	2.75	0		1	.
7	261.02	170.13	0.37	2.70	0.36	2.75	0		0	.
7	262.02	221.78	0.36	2.75	0.36	2.75	1	1	0	2.85
7	263.02	175.21	0.37	2.73	0.36	2.75	0		0	.
7	264.02	169.07	0.37	2.68	0.36	2.75	0		0	.
7	265.02	173.54	0.37	2.72	0.36	2.75	0		0	.
7	266.02	171.44	0.37	2.68	0.37	2.68	1	2	0	2.75
7	267.02	174.67	0.36	2.76	0.36	2.76	1	3	0	2.75
7	268.02	304.30	0.37	2.69	0.36	2.76	0		1	.
7	269.02	119.28	0.36	2.76	0.36	2.76	1	1	0	2.75
7	270.02	423.06	0.40	2.51	0.37	2.68	0		0	.
7	272.02	79.75	0.37	2.68	0.37	2.68	1	2	0	2.76
7	273.02	309.54	0.40	2.50	0.37	2.68	0		1	.
7	274.02	307.51	0.36	2.81	0.35	2.85	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	275.02	1	.	1	0	1	275	1	1.80	1	22.98
7	276.02	1	1	1	0	1	272	1	1.80	2	104.58
7	277.02	1	0	0	0	1	277	1	1.98	2	104.58
7	278.02	0	0	1	0	1	275	1	1.98	1	135.18
7	279.02	0	0	0	0	1	275	1	2.16	1	53.58
7	280.02	0	0	1	0	1	275	1	2.52	1	124.98
7	281.02	0	1	0	0	1	275	1	2.16	1	53.58
7	282.02	0	1	0	0	1	277	1	1.80	2	104.58
7	283.02	0	0	1	0	1	277	1	2.34	2	73.98
7	284.02	0	0	1	0	1	277	1	2.34	2	73.98
7	285.02	0	.	0	0	1	285	1	1.80	1	135.18
7	286.02	1	0	1	0	1	287	1	1.62	1	53.58
7	287.02	1	.	1	0	1	287	1	1.80	1	135.18
7	288.02	1	0	1	0	1	277	1	2.34	2	114.78
7	289.02	1	1	1	0	1	277	1	2.16	2	53.58
7	290.02	1	0	1	0	1	287	1	2.34	1	73.98
7	291.02	1	.	1	0	1	291	1	2.16	0	22.98
7	292.02	1	.	1	0	1	292	1	1.80	0	53.58
7	293.02	1	0	1	0	1	287	1	2.16	1	73.98
7	294.02	1	0	1	0	1	287	1	2.16	1	73.98
7	295.02	1	0	1	0	1	287	1	2.16	1	73.98
7	296.02	0	1	1	0	1	287	1	1.98	1	94.38
7	297.02	1	1	0	0	1	287	1	1.98	1	63.78
7	298.02	0	.	0	1	1	298	1	2.16	2	135.18
7	299.02	0	0	1	0	1	287	1	2.16	1	114.78
7	300.02	1	1	0	0	1	287	1	2.16	1	104.58
7	301.02	0	0	1	0	1	298	1	1.62	2	135.18
7	302.02	0	.	1	0	1	302	1	1.44	1	135.18
7	303.02	1	0	1	0	1	287	1	1.98	1	73.98
7	304.02	1	.	1	0	1	304	1	1.62	2	73.98
7	305.02	1	.	1	0	1	305	1	1.62	1	73.98
7	306.02	1	0	1	0	1	304	1	2.16	2	124.98
7	307.02	1	0	1	0	1	304	1	2.16	2	124.98
7	308.02	1	0	1	0	1	304	1	2.16	2	135.18
7	309.02	1	0	1	0	1	304	1	1.80	2	135.18
7	310.02	1	0	1	0	1	304	1	2.34	2	124.98
7	311.02	0	1	1	0	2	287	1	2.16	1	12.78
7	312.02	1	0	1	0	1	305	1	1.98	1	63.78
7	313.02	1	0	1	0	1	305	1	1.80	1	73.98
7	314.02	1	0	1	0	1	304	1	2.34	2	73.98
7	315.02	1	0	1	0	1	304	1	2.16	2	135.18
7	316.02	1	0	1	0	1	304	1	2.16	2	73.98
7	317.02	1	0	1	0	1	305	1	2.34	1	73.98
7	318.02	1	0	1	0	1	304	1	2.16	2	135.18
7	319.02	1	0	1	0	1	304	1	2.16	2	135.18
7	320.02	1	0	1	0	1	305	1	2.34	1	114.78
7	321.02	1	.	0	1	1	321	0	1.80	2	124.98
7	322.02	1	1	1	0	1	305	1	2.52	1	73.98
7	323.02	1	0	1	0	1	305	1	2.52	1	135.18
7	324.02	1	1	1	0	1	321	0	1.80	2	124.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	275.02	117.45	0.35	2.85	0.35	2.85	1	3	0	2.76
7	276.02	118.85	0.40	2.50	0.37	2.68	0		0	.
7	277.02	83.52	0.40	2.50	0.40	2.50	0		0	2.76
7	278.02	236.83	0.36	2.77	0.35	2.85	0		0	.
7	279.02	92.16	0.36	2.76	0.35	2.85	0		0	.
7	280.02	229.26	0.36	2.78	0.35	2.85	0		0	.
7	281.02	120.55	0.36	2.80	0.35	2.85	0		0	.
7	282.02	195.63	0.42	2.37	0.40	2.50	0		1	.
7	283.02	196.86	0.42	2.36	0.40	2.50	0		0	.
7	284.02	88.66	0.43	2.34	0.40	2.50	0		0	.
7	285.02	244.24	0.38	2.64	0.38	2.64	1	1	0	2.76
7	286.02	90.19	0.37	2.72	0.38	2.65	0		1	.
7	287.02	122.25	0.38	2.65	0.38	2.65	1	3	0	2.64
7	288.02	264.36	0.45	2.24	0.40	2.50	0		0	.
7	289.02	189.79	0.44	2.25	0.40	2.50	0		0	.
7	290.02	352.55	0.39	2.58	0.38	2.65	0		0	.
7	291.02	271.07	0.50	1.99	0.50	1.99	1	2	0	2.64
7	292.02	195.56	0.54	1.85	0.54	1.85	1	2	0	2.64
7	293.02	192.86	0.40	2.50	0.38	2.65	0		0	.
7	294.02	202.27	0.39	2.55	0.38	2.65	0		0	.
7	295.02	154.99	0.40	2.50	0.38	2.65	0		0	.
7	296.02	208.61	0.41	2.44	0.38	2.65	0		0	.
7	297.02	93.93	0.40	2.49	0.38	2.65	0		0	.
7	298.02	123.79	0.37	2.68	0.37	2.68	1	2	0	2.64
7	299.02	124.69	0.41	2.43	0.38	2.65	0		0	.
7	300.02	92.16	0.43	2.33	0.38	2.65	0		0	.
7	301.02	94.56	0.37	2.69	0.37	2.68	0		1	.
7	302.02	188.42	0.38	2.60	0.38	2.60	1	1	0	2.64
7	303.02	216.55	0.39	2.59	0.38	2.65	0		0	.
7	304.02	215.21	0.39	2.58	0.39	2.58	1	2	0	2.60
7	305.02	100.64	0.37	2.67	0.37	2.67	1	3	0	2.60
7	306.02	97.13	0.39	2.56	0.39	2.58	0		0	.
7	307.02	102.00	0.39	2.59	0.39	2.58	0		1	.
7	308.02	102.94	0.39	2.57	0.39	2.58	0		0	.
7	309.02	103.57	0.39	2.54	0.39	2.58	0		0	.
7	310.02	402.73	0.40	2.49	0.39	2.58	0		0	.
7	311.02	218.38	0.40	2.51	0.38	2.65	0		1	.
7	312.02	212.31	0.39	2.58	0.37	2.67	0		0	.
7	313.02	237.23	0.38	2.65	0.37	2.67	0		1	.
7	314.02	108.44	0.40	2.51	0.39	2.58	0		0	.
7	315.02	242.74	0.39	2.54	0.39	2.58	0		0	.
7	316.02	215.41	0.39	2.53	0.39	2.58	0		0	.
7	317.02	110.61	0.38	2.63	0.37	2.67	0		0	.
7	318.02	111.91	0.39	2.55	0.39	2.58	0		0	.
7	319.02	130.26	0.38	2.63	0.39	2.58	0		0	.
7	320.02	116.75	0.38	2.66	0.37	2.67	0		0	.
7	321.02	231.20	0.39	2.54	0.39	2.54	1	1	0	2.60
7	322.02	96.73	0.37	2.73	0.37	2.67	0		0	.
7	323.02	111.45	0.38	2.66	0.37	2.67	0		0	.
7	324.02	113.08	0.40	2.53	0.39	2.54	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	325.02	0	1	0	0	1	321	0	1.62	1	124.98
7	326.02	1	1	1	0	1	321	0	2.16	0	135.18
7	327.02	0	.	0	0	1	327	0	1.80	2	53.58
7	328.02	0	.	0	0	1	328	0	1.44	1	124.98
7	329.02	0	.	0	0	1	329	1	2.34	2	135.18
7	330.02	0	0	0	1	1	329	1	2.16	2	135.18
7	331.02	1	0	1	0	1	346	0	2.52	2	135.18
7	332.02	0	0	0	1	1	346	0	2.52	2	135.18
7	333.02	1	0	1	0	1	305	1	1.80	1	33.18
7	334.02	0	1	1	0	1	305	1	2.16	1	73.98
7	335.02	1	0	1	0	1	346	0	2.16	2	124.98
7	336.02	0	0	1	0	1	305	1	1.98	1	114.78
7	337.02	0	1	0	0	1	305	1	2.34	1	114.78
7	338.02	1	1	0	0	1	305	1	2.34	1	124.98
7	339.02	1	0	1	0	1	340	1	2.34	1	135.18
7	340.02	1	.	1	0	1	340	1	2.16	1	135.18
7	341.02	1	0	1	0	1	346	0	1.98	2	135.18
7	342.02	1	.	1	0	1	342	1	2.52	2	124.98
7	343.02	1	.	1	0	2	343	1	1.26	2	104.58
7	344.02	0	1	1	0	1	343	1	1.44	2	104.58
7	345.02	1	0	1	1	1	342	1	1.98	2	135.18
7	346.02	1	.	1	0	1	346	0	2.34	1	73.98
7	347.02	0	1	0	0	1	342	1	1.98	2	135.18
7	348.02	0	1	0	0	1	346	0	2.52	1	53.58
7	349.02	1	1	1	0	1	342	1	2.34	2	135.18
7	350.02	1	1	1	0	1	346	0	2.16	1	73.98
7	351.02	0	1	1	0	1	365	0	2.70	2	124.98
7	352.02	1	0	1	0	1	346	0	2.16	1	135.18
7	353.02	0	.	1	0	1	353	0	2.70	2	165.78
7	354.02	0	.	0	0	1	354	1	2.16	1	73.98
7	355.02	0	1	1	0	1	369	0	2.70	2	155.58
7	356.02	0	0	1	0	1	369	0	2.52	2	104.58
7	357.02	1	1	1	0	1	354	1	2.52	1	53.58
7	358.02	0	0	0	0	1	369	0	3.06	2	165.78
7	359.02	1	0	0	0	1	354	1	2.52	1	53.58
7	360.02	1	0	1	0	1	354	1	2.34	1	53.58
7	361.02	1	.	1	1	1	361	1	2.88	2	124.98
7	362.02	0	1	0	0	1	354	1	2.16	1	73.98
7	363.02	0	1	1	0	1	361	1	2.34	2	124.98
7	364.02	1	1	1	0	1	361	1	2.52	2	53.58
7	365.02	1	.	1	0	1	365	0	2.34	1	63.78
7	366.02	1	0	1	0	1	371	1	2.34	1	124.98
7	367.02	1	1	1	0	1	365	0	2.34	1	63.78
7	368.02	1	.	1	0	1	368	0	2.70	1	63.78
7	369.02	1	.	1	0	1	369	0	2.52	1	73.98
7	370.02	0	0	0	0	1	369	0	2.88	1	124.98
7	371.02	1	.	1	0	1	371	1	2.88	1	73.98
7	372.02	1	.	1	0	1	372	0	2.16	2	135.18
7	373.02	0	0	0	0	1	369	0	2.88	1	135.18
7	374.02	1	1	1	0	1	369	0	2.52	1	73.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	325.02	115.88	0.39	2.54	0.39	2.54	0		0	.
7	326.02	306.54	0.40	2.48	0.39	2.54	0		0	.
7	327.02	105.17	0.42	2.40	0.42	2.40	1	2	0	2.54
7	328.02	124.43	0.40	2.48	0.40	2.48	1	3	0	2.54
7	329.02	125.89	0.40	2.50	0.40	2.50	1	3	0	2.54
7	330.02	129.10	0.41	2.47	0.40	2.50	0		1	.
7	331.02	131.00	0.40	2.53	0.41	2.47	0		1	.
7	332.02	360.16	0.40	2.51	0.41	2.47	0		0	.
7	333.02	225.02	0.38	2.65	0.37	2.67	0		0	.
7	334.02	132.83	0.37	2.67	0.37	2.67	0		0	.
7	335.02	131.99	0.39	2.56	0.41	2.47	0		0	.
7	336.02	133.36	0.37	2.71	0.37	2.67	0		0	.
7	337.02	98.23	0.36	2.75	0.37	2.67	0		0	.
7	338.02	110.18	0.37	2.71	0.37	2.67	0		0	.
7	339.02	104.31	0.41	2.42	0.41	2.43	0		1	.
7	340.02	122.46	0.41	2.43	0.41	2.43	1	2	0	2.54
7	341.02	129.33	0.39	2.58	0.41	2.47	0		0	.
7	342.02	81.31	0.39	2.55	0.39	2.55	1	2	0	2.47
7	343.02	76.81	0.34	2.93	0.34	2.93	1	3	0	2.64
7	344.02	132.13	0.34	2.94	0.34	2.93	0		1	.
7	345.02	243.87	0.41	2.45	0.39	2.55	0		1	.
7	346.02	135.04	0.41	2.47	0.41	2.47	1	1	0	2.54
7	347.02	315.48	0.40	2.49	0.39	2.55	0		0	.
7	348.02	133.24	0.40	2.50	0.41	2.47	0		0	.
7	349.02	248.51	0.40	2.48	0.39	2.55	0		0	.
7	350.02	125.03	0.40	2.52	0.41	2.47	0		0	.
7	351.02	106.61	0.40	2.53	0.38	2.62	0		1	.
7	352.02	62.80	0.39	2.57	0.41	2.47	0		0	.
7	353.02	251.82	0.40	2.51	0.40	2.51	1	2	0	2.62
7	354.02	101.67	0.39	2.58	0.39	2.58	1	3	0	2.47
7	355.02	184.61	0.38	2.66	0.38	2.65	0		1	.
7	356.02	328.86	0.38	2.66	0.38	2.65	0		0	.
7	357.02	61.26	0.39	2.59	0.39	2.58	0		1	.
7	358.02	331.03	0.38	2.63	0.38	2.65	0		0	.
7	359.02	334.16	0.38	2.60	0.39	2.58	0		0	.
7	360.02	121.46	0.38	2.61	0.39	2.58	0		0	.
7	361.02	255.19	0.38	2.61	0.38	2.61	1	2	0	2.65
7	362.02	130.93	0.38	2.62	0.39	2.58	0		0	.
7	363.02	379.24	0.38	2.61	0.38	2.61	0		1	.
7	364.02	262.16	0.40	2.53	0.38	2.61	0		0	.
7	365.02	127.06	0.38	2.62	0.38	2.62	1	1	0	2.47
7	366.02	263.79	0.37	2.71	0.37	2.73	0		0	.
7	367.02	267.60	0.38	2.61	0.38	2.62	0		0	.
7	368.02	266.60	0.38	2.63	0.38	2.63	1	3	0	2.62
7	369.02	115.05	0.38	2.65	0.38	2.65	1	1	0	2.62
7	370.02	277.11	0.37	2.67	0.38	2.65	0		0	.
7	371.02	139.07	0.37	2.73	0.37	2.73	1	3	0	2.65
7	372.02	114.52	0.38	2.61	0.38	2.61	1	2	0	2.65
7	373.02	273.54	0.37	2.67	0.38	2.65	0		0	.
7	374.02	118.09	0.37	2.71	0.38	2.65	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	375.02	0	1	0	0	1	371	1	2.88	1	135.18
7	376.02	1	1	1	0	1	371	1	2.70	1	73.98
7	377.02	1	0	1	0	1	371	1	2.34	1	73.98
7	378.02	1	0	1	0	2	371	1	2.34	1	124.98
7	379.02	1	.	1	0	1	379	0	1.98	1	124.98
7	380.02	0	.	0	0	1	380	0	2.16	1	73.98
7	381.02	0	0	0	0	1	380	0	2.16	2	73.98
7	382.02	1	1	1	0	1	380	0	2.16	1	73.98
7	383.02	1	0	0	0	1	380	0	2.34	2	175.99
7	384.02	0	.	1	0	1	384	1	2.34	2	165.78
7	385.02	0	0	1	0	1	384	1	2.16	2	124.98
7	386.02	1	.	0	0	1	386	1	1.98	1	73.98
7	387.02	1	0	1	0	1	386	1	2.16	1	73.98
7	388.02	1	1	0	0	1	384	1	2.34	2	94.38
7	389.02	1	0	1	0	1	386	1	1.98	1	73.98
7	390.02	1	0	1	1	1	384	1	1.98	2	114.78
7	391.02	0	1	1	0	1	386	1	2.16	1	124.98
7	392.02	1	0	1	0	1	384	1	2.16	2	145.38
7	393.02	1	1	1	0	1	386	1	2.16	1	124.98
7	394.02	0	1	1	0	1	386	1	1.80	1	94.38
7	395.02	1	1	1	0	1	386	1	2.34	1	94.38
7	396.02	1	0	1	1	1	384	1	2.34	2	124.98
7	397.02	1	0	1	1	1	384	1	2.34	2	124.98
7	398.02	0	1	0	0	1	384	1	2.16	2	104.58
7	399.02	1	0	1	0	1	386	1	2.16	1	73.98
7	400.02	1	1	0	0	1	384	1	2.16	2	104.58
7	401.02	1	0	1	0	1	386	1	2.34	1	94.38
7	402.02	1	0	1	0	1	386	1	1.98	1	94.38
7	403.02	0	1	1	0	1	386	1	1.98	1	135.18
7	404.02	0	1	1	0	1	384	1	1.98	2	94.38
7	405.02	1	1	0	0	1	386	1	1.98	1	94.38
7	406.02	0	1	1	0	1	386	1	1.62	1	165.78
7	407.02	1	.	1	0	1	407	0	1.80	2	73.98
7	408.02	1	.	1	0	1	408	0	1.62	1	73.98
7	409.02	1	.	1	0	1	409	0	1.98	1	135.18
7	410.02	0	1	0	0	2	409	0	1.98	1	135.18
7	411.02	0	0	1	0	1	409	0	1.98	1	135.18
7	412.02	1	1	1	0	1	409	0	1.80	1	135.18
7	413.02	0	1	0	0	1	409	0	1.62	1	135.18
7	414.02	1	1	1	0	2	409	0	1.62	1	63.78
7	415.02	0	1	0	0	1	409	0	1.62	1	135.18
7	416.02	0	0	0	0	1	409	0	1.80	1	135.18
7	417.02	0	0	0	0	1	409	0	1.98	0	135.18
7	418.02	0	0	1	1	1	409	0	1.80	2	145.38
7	419.02	1	1	1	0	1	409	0	1.80	1	135.18
7	420.02	1	0	1	0	1	409	0	1.98	2	145.38
7	421.02	1	0	1	0	1	409	0	1.98	1	145.38
7	422.02	1	0	1	0	1	409	0	2.34	2	165.78
7	423.02	1	0	1	0	1	409	0	1.98	1	145.38
7	424.02	1	0	0	0	2	409	0	2.34	1	165.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	375.02	281.95	0.36	2.76	0.37	2.73	0		1	.
7	376.02	294.02	0.36	2.76	0.37	2.73	0		0	.
7	377.02	135.30	0.37	2.70	0.37	2.73	0		0	.
7	378.02	137.67	0.37	2.69	0.37	2.73	0		0	.
7	379.02	283.65	0.37	2.68	0.37	2.68	1	3	0	2.65
7	380.02	318.42	0.38	2.65	0.38	2.65	1	1	0	2.65
7	381.02	300.66	0.38	2.64	0.38	2.65	0		1	.
7	382.02	98.03	0.38	2.67	0.38	2.65	0		0	.
7	383.02	77.98	0.38	2.63	0.38	2.65	0		0	.
7	384.02	148.08	0.38	2.60	0.38	2.60	1	2	0	2.65
7	385.02	322.72	0.40	2.53	0.38	2.60	0		1	.
7	386.02	323.42	0.37	2.69	0.37	2.69	1	3	0	2.65
7	387.02	249.68	0.37	2.70	0.37	2.69	0		1	.
7	388.02	326.06	0.39	2.53	0.38	2.60	0		0	.
7	389.02	195.73	0.37	2.68	0.37	2.69	0		0	.
7	390.02	141.28	0.40	2.52	0.38	2.60	0		0	.
7	391.02	116.98	0.38	2.64	0.37	2.69	0		0	.
7	392.02	145.65	0.39	2.54	0.38	2.60	0		0	.
7	393.02	248.98	0.38	2.64	0.37	2.69	0		0	.
7	394.02	251.22	0.38	2.63	0.37	2.69	0		0	.
7	395.02	154.39	0.38	2.65	0.37	2.69	0		0	.
7	396.02	151.39	0.39	2.55	0.38	2.60	0		0	.
7	397.02	205.27	0.39	2.58	0.38	2.60	0		0	.
7	398.02	337.00	0.40	2.52	0.38	2.60	0		0	.
7	399.02	203.33	0.38	2.64	0.37	2.69	0		0	.
7	400.02	252.32	0.40	2.49	0.38	2.60	0		0	.
7	401.02	255.65	0.38	2.65	0.37	2.69	0		0	.
7	402.02	113.01	0.38	2.61	0.37	2.69	0		0	.
7	403.02	264.10	0.38	2.62	0.37	2.69	0		0	.
7	404.02	261.16	0.41	2.44	0.38	2.60	0		0	.
7	405.02	37.70	0.39	2.59	0.37	2.69	0		0	.
7	406.02	353.82	0.39	2.58	0.37	2.69	0		0	.
7	407.02	351.25	0.37	2.68	0.37	2.68	1	3	0	2.65
7	408.02	150.29	0.38	2.61	0.38	2.61	1	2	0	2.65
7	409.02	152.42	0.39	2.59	0.39	2.59	1	1	0	2.65
7	410.02	154.76	0.39	2.59	0.39	2.59	0		1	.
7	411.02	156.76	0.39	2.55	0.39	2.59	0		0	.
7	412.02	160.46	0.39	2.58	0.39	2.59	0		0	.
7	413.02	379.38	0.39	2.56	0.39	2.59	0		0	.
7	414.02	162.26	0.40	2.53	0.39	2.59	0		0	.
7	415.02	163.93	0.40	2.51	0.39	2.59	0		0	.
7	416.02	165.13	0.40	2.50	0.39	2.59	0		0	.
7	417.02	117.92	0.41	2.44	0.39	2.59	0		0	.
7	418.02	167.60	0.41	2.43	0.39	2.59	0		0	.
7	419.02	122.12	0.41	2.46	0.39	2.59	0		0	.
7	420.02	123.06	0.42	2.41	0.39	2.59	0		0	.
7	421.02	99.27	0.41	2.41	0.39	2.59	0		0	.
7	422.02	124.16	0.42	2.40	0.39	2.59	0		0	.
7	423.02	100.87	0.42	2.40	0.39	2.59	0		0	.
7	424.02	102.97	0.41	2.43	0.39	2.59	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	425.02	1	0	1	0	1	409	0	2.52	2	175.99
7	426.02	1	0	1	0	1	409	0	2.52	1	175.99
7	427.02	1	.	1	1	1	427	1	2.34	2	186.19
7	428.02	0	.	1	0	1	428	1	2.52	1	175.99
7	429.02	1	1	1	0	1	428	1	2.34	1	175.99
7	430.02	1	0	1	0	1	427	1	2.34	2	186.19
7	431.02	1	0	1	0	1	427	1	2.34	2	186.19
7	432.02	1	0	1	0	1	428	1	2.34	1	63.78
7	433.02	0	1	0	0	1	427	1	2.34	2	186.19
7	434.02	0	1	0	0	1	428	1	2.16	1	73.98
7	435.02	0	0	1	0	1	427	1	2.34	2	155.58
7	436.02	0	0	1	0	1	428	1	2.16	1	135.18
7	437.02	0	0	0	0	1	428	1	1.98	1	135.18
7	438.02	1	1	0	0	1	427	1	1.98	2	186.19
7	439.02	1	1	1	0	1	428	1	2.16	1	135.18
7	440.02	0	.	0	0	1	440	1	1.80	0	165.78
7	441.02	0	1	1	0	1	427	1	2.16	2	124.98
7	442.02	1	.	1	0	1	442	1	1.98	1	155.58
7	443.02	1	1	1	0	1	427	1	2.34	2	206.59
7	444.02	1	0	1	0	1	427	1	2.52	2	206.59
7	445.02	1	0	1	0	1	427	1	2.52	2	135.18
7	446.02	1	0	1	0	1	427	1	2.52	2	186.19
7	447.02	1	0	1	0	1	442	1	1.98	1	73.98
7	448.02	0	1	0	1	1	427	1	2.52	2	186.19
7	449.02	1	0	0	0	1	442	1	2.34	1	73.98
7	450.02	0	1	0	0	1	442	1	2.16	1	73.98
7	451.02	0	0	0	0	1	427	1	2.52	2	186.19
7	452.02	0	0	1	0	1	442	1	2.34	1	186.19
7	453.02	1	1	1	0	1	442	1	2.34	1	114.78
7	454.02	1	1	1	0	1	427	1	2.16	2	196.39
7	455.02	1	0	1	0	1	442	1	2.34	1	124.98
7	456.02	1	0	1	0	1	427	1	2.34	2	175.99
7	457.02	0	1	1	0	1	442	1	2.34	1	206.59
7	458.02	0	1	1	0	1	427	1	2.34	2	135.18
7	459.02	1	1	1	0	1	427	1	2.16	0	135.18
7	460.02	1	1	0	0	1	442	1	2.52	1	124.98
7	461.02	1	0	1	0	1	442	1	2.34	1	124.98
7	462.02	1	.	1	0	1	462	0	2.16	0	124.98
7	463.02	0	1	0	0	1	442	1	2.34	1	124.98
7	464.02	0	0	1	0	1	442	1	2.52	1	186.19
7	465.02	0	0	0	0	1	442	1	2.70	1	206.59
7	466.02	1	1	1	0	1	442	1	2.34	1	124.98
7	467.02	1	.	0	0	1	467	0	1.80	0	124.98
7	468.02	0	.	1	0	1	468	0	2.16	1	135.18
7	469.02	1	.	1	0	1	469	0	2.34	1	22.98
7	470.02	1	.	1	0	1	470	0	2.52	2	206.59
7	471.02	1	.	1	0	1	471	0	2.52	1	22.98
7	472.02	0	1	0	0	1	471	0	2.16	2	124.98
7	473.02	0	0	1	0	1	471	0	2.16	1	124.98
7	474.02	1	.	1	0	1	474	1	2.34	1	73.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	425.02	101.27	0.41	2.43	0.39	2.59	0		0	.
7	426.02	86.28	0.41	2.44	0.39	2.59	0		0	.
7	427.02	106.01	0.42	2.38	0.42	2.38	1	2	0	2.59
7	428.02	107.98	0.41	2.46	0.41	2.46	1	3	0	2.59
7	429.02	87.85	0.40	2.49	0.41	2.46	0		1	.
7	430.02	88.82	0.42	2.37	0.42	2.38	0		1	.
7	431.02	409.47	0.42	2.37	0.42	2.38	0		0	.
7	432.02	89.32	0.40	2.48	0.41	2.46	0		0	.
7	433.02	407.20	0.43	2.34	0.42	2.38	0		0	.
7	434.02	152.82	0.40	2.47	0.41	2.46	0		0	.
7	435.02	181.68	0.45	2.23	0.42	2.38	0		0	.
7	436.02	183.92	0.41	2.46	0.41	2.46	0		0	.
7	437.02	94.13	0.41	2.47	0.41	2.46	0		0	.
7	438.02	185.79	0.45	2.24	0.42	2.38	0		0	.
7	439.02	66.70	0.41	2.46	0.41	2.46	0		0	.
7	440.02	199.17	0.42	2.37	0.42	2.37	1	3	0	2.59
7	441.02	152.39	0.45	2.24	0.42	2.38	0		0	.
7	442.02	66.33	0.40	2.53	0.40	2.53	1	3	0	2.59
7	443.02	62.99	0.44	2.26	0.42	2.38	0		0	.
7	444.02	202.70	0.45	2.20	0.42	2.38	0		0	.
7	445.02	105.17	0.45	2.22	0.42	2.38	0		0	.
7	446.02	422.35	0.46	2.16	0.42	2.38	0		0	.
7	447.02	110.47	0.39	2.56	0.40	2.53	0		1	.
7	448.02	423.79	0.46	2.18	0.42	2.38	0		0	.
7	449.02	426.79	0.39	2.58	0.40	2.53	0		0	.
7	450.02	111.61	0.39	2.56	0.40	2.53	0		0	.
7	451.02	98.26	0.46	2.17	0.42	2.38	0		0	.
7	452.02	245.41	0.39	2.57	0.40	2.53	0		0	.
7	453.02	112.94	0.39	2.55	0.40	2.53	0		0	.
7	454.02	197.53	0.46	2.17	0.42	2.38	0		0	.
7	455.02	144.24	0.39	2.57	0.40	2.53	0		0	.
7	456.02	64.56	0.46	2.18	0.42	2.38	0		0	.
7	457.02	214.35	0.39	2.57	0.40	2.53	0		0	.
7	458.02	211.48	0.46	2.16	0.42	2.38	0		0	.
7	459.02	202.40	0.45	2.21	0.42	2.38	0		0	.
7	460.02	204.74	0.39	2.55	0.40	2.53	0		0	.
7	461.02	220.79	0.40	2.53	0.40	2.53	0		0	.
7	462.02	206.41	0.43	2.32	0.43	2.32	1	2	0	2.38
7	463.02	99.93	0.40	2.53	0.40	2.53	0		0	.
7	464.02	73.67	0.39	2.55	0.40	2.53	0		0	.
7	465.02	214.15	0.40	2.53	0.40	2.53	0		0	.
7	466.02	224.13	0.40	2.51	0.40	2.53	0		0	.
7	467.02	215.25	0.42	2.38	0.42	2.38	1	1	0	2.59
7	468.02	590.76	0.42	2.41	0.42	2.41	1	3	0	2.38
7	469.02	91.46	0.41	2.44	0.41	2.44	1	2	0	2.38
7	470.02	592.06	0.40	2.52	0.40	2.52	1	3	0	2.38
7	471.02	139.34	0.41	2.45	0.41	2.45	1	1	0	2.38
7	472.02	225.56	0.40	2.51	0.41	2.45	0		1	.
7	473.02	476.01	0.41	2.42	0.41	2.45	0		0	.
7	474.02	153.92	0.41	2.42	0.41	2.42	1	2	0	2.45

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	475.02	1	.	1	0	1	475	1	2.34	2	175.99
7	476.02	1	0	0	0	1	474	1	2.34	1	114.78
7	477.02	1	0	1	0	1	475	1	2.34	2	175.99
7	478.02	1	0	1	0	1	475	1	1.98	2	175.99
7	479.02	0	1	0	0	1	474	1	2.16	1	175.99
7	480.02	1	1	0	0	1	481	0	1.98	1	104.58
7	481.02	0	.	0	0	1	481	0	1.98	2	104.58
7	482.02	0	0	1	0	1	481	0	2.34	2	175.99
7	483.02	0	1	1	0	1	481	0	1.98	1	145.38
7	484.02	0	0	0	0	1	481	0	2.16	1	186.19
7	485.02	1	1	1	0	1	481	0	2.34	2	206.59
7	486.02	1	0	0	1	1	481	0	2.16	1	165.78
7	487.02	0	.	0	1	1	487	1	2.34	2	175.99
7	488.02	1	.	1	0	1	488	1	2.34	1	186.19
7	489.02	0	0	0	0	1	487	1	2.16	2	206.59
7	490.02	1	0	1	0	1	488	1	2.16	1	186.19
7	491.02	0	0	1	0	1	487	1	1.80	2	206.59
7	492.02	0	1	1	0	1	488	1	2.52	1	186.19
7	493.02	0	0	1	0	1	487	1	1.98	2	206.59
7	494.02	1	0	0	0	1	487	1	1.98	2	206.59
7	495.02	1	1	1	0	1	488	1	1.80	1	135.18
7	496.02	1	0	0	0	1	501	0	1.80	1	104.58
7	497.02	1	0	1	0	1	488	1	2.16	1	186.19
7	498.02	0	1	0	1	1	487	1	2.16	1	196.39
7	499.02	1	0	1	0	1	501	0	1.98	2	206.59
7	500.02	1	1	1	0	1	501	0	2.16	1	206.59
7	501.02	1	.	1	0	2	501	0	1.80	1	165.78
7	502.02	0	1	0	0	1	501	0	2.52	2	165.78
7	503.02	1	0	1	0	1	501	0	2.34	1	186.19
7	504.02	0	1	0	0	1	501	0	2.34	2	186.19
7	505.02	0	0	0	0	1	501	0	2.16	1	206.59
7	506.02	0	0	1	0	1	501	0	1.98	2	206.59
7	507.02	1	1	1	0	1	501	0	2.34	1	196.39
7	508.02	0	1	1	0	1	501	0	2.16	2	196.39
7	509.02	1	1	1	0	1	501	0	2.34	1	206.59
7	510.02	0	1	1	0	1	501	0	2.70	2	196.39
7	511.02	1	1	0	0	1	501	0	2.34	1	206.59
7	512.02	1	0	1	0	1	501	0	2.34	2	237.19
7	513.02	1	0	1	0	1	501	0	2.70	1	206.59
7	514.02	1	.	1	0	1	514	1	2.16	2	196.39
7	515.02	1	.	1	0	1	515	1	1.62	1	196.39
7	516.02	0	1	0	1	1	515	1	1.98	1	104.58
7	517.02	1	0	1	1	1	514	1	1.62	2	196.39
7	518.02	1	1	1	0	1	515	1	1.98	0	237.19
7	519.02	0	.	1	1	1	519	1	1.98	2	196.39
7	520.02	1	1	1	0	1	519	1	1.62	2	196.39
7	521.02	1	0	1	0	1	519	1	1.44	2	135.18
7	522.02	1	0	1	0	1	519	1	1.98	2	135.18
7	523.02	1	0	1	0	1	519	1	2.16	2	135.18
7	524.02	0	1	1	0	1	519	1	2.16	2	237.19

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	475.02	289.05	0.40	2.50	0.40	2.50	1	3	0	2.45
7	476.02	152.45	0.41	2.42	0.41	2.42	0		1	.
7	477.02	154.49	0.40	2.50	0.40	2.50	0		1	.
7	478.02	149.82	0.39	2.57	0.40	2.50	0		0	.
7	479.02	300.56	0.41	2.43	0.41	2.42	0		0	.
7	480.02	302.43	0.40	2.49	0.41	2.45	0		1	.
7	481.02	160.79	0.41	2.45	0.41	2.45	1	1	0	2.45
7	482.02	184.35	0.41	2.46	0.41	2.45	0		0	.
7	483.02	127.22	0.41	2.47	0.41	2.45	0		0	.
7	484.02	115.35	0.40	2.47	0.41	2.45	0		0	.
7	485.02	156.16	0.41	2.46	0.41	2.45	0		0	.
7	486.02	162.66	0.40	2.49	0.41	2.45	0		0	.
7	487.02	129.86	0.41	2.45	0.41	2.45	1	2	0	2.45
7	488.02	110.27	0.40	2.50	0.40	2.50	1	3	0	2.45
7	489.02	131.80	0.42	2.40	0.41	2.45	0		1	.
7	490.02	118.58	0.40	2.47	0.40	2.50	0		1	.
7	491.02	132.73	0.42	2.39	0.41	2.45	0		0	.
7	492.02	112.94	0.41	2.46	0.40	2.50	0		0	.
7	493.02	111.21	0.45	2.23	0.41	2.45	0		0	.
7	494.02	240.51	0.45	2.22	0.41	2.45	0		0	.
7	495.02	360.96	0.41	2.42	0.40	2.50	0		0	.
7	496.02	134.83	0.42	2.40	0.42	2.39	0		0	.
7	497.02	133.66	0.42	2.40	0.40	2.50	0		0	.
7	498.02	122.62	0.42	2.36	0.41	2.45	0		0	.
7	499.02	116.98	0.42	2.38	0.42	2.39	0		1	.
7	500.02	162.56	0.42	2.37	0.42	2.39	0		0	.
7	501.02	172.41	0.42	2.39	0.42	2.39	1	0	0	2.45
7	502.02	140.84	0.42	2.39	0.42	2.39	0		0	.
7	503.02	144.61	0.42	2.39	0.42	2.39	0		0	.
7	504.02	123.22	0.42	2.40	0.42	2.39	0		0	.
7	505.02	124.52	0.42	2.37	0.42	2.39	0		0	.
7	506.02	153.78	0.42	2.37	0.42	2.39	0		0	.
7	507.02	152.85	0.42	2.37	0.42	2.39	0		0	.
7	508.02	135.43	0.43	2.33	0.42	2.39	0		0	.
7	509.02	155.35	0.42	2.38	0.42	2.39	0		0	.
7	510.02	136.57	0.43	2.33	0.42	2.39	0		0	.
7	511.02	111.84	0.42	2.36	0.42	2.39	0		0	.
7	512.02	138.27	0.43	2.30	0.42	2.39	0		0	.
7	513.02	171.10	0.42	2.37	0.42	2.39	0		0	.
7	514.02	174.17	0.43	2.35	0.43	2.35	1	3	0	2.39
7	515.02	397.76	0.47	2.14	0.47	2.14	1	2	0	2.39
7	516.02	167.53	0.46	2.18	0.47	2.14	0		1	.
7	517.02	110.71	0.43	2.32	0.43	2.35	0		1	.
7	518.02	175.24	0.47	2.13	0.47	2.14	0		0	.
7	519.02	169.67	0.48	2.10	0.48	2.10	1	2	0	2.39
7	520.02	315.58	0.48	2.08	0.48	2.10	0		1	.
7	521.02	313.42	0.49	2.04	0.48	2.10	0		0	.
7	522.02	312.51	0.50	1.99	0.48	2.10	0		0	.
7	523.02	115.48	0.49	2.02	0.48	2.10	0		0	.
7	524.02	114.05	0.48	2.07	0.48	2.10	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	525.02	0	0	1	0	1	519	1	2.16	2	237.19
7	526.02	0	.	1	0	1	526	1	2.16	0	104.58
7	527.02	1	.	1	0	1	527	1	1.26	1	73.98
7	528.02	0	1	1	0	1	527	1	1.80	1	73.98
7	529.02	0	0	1	0	1	527	1	1.62	1	33.18
7	530.02	1	1	1	0	1	534	1	2.52	1	165.78
7	531.02	0	1	0	0	1	527	1	1.98	1	165.78
7	532.02	1	1	1	0	1	526	1	1.44	0	165.78
7	533.02	0	0	1	0	1	527	1	1.80	1	206.59
7	534.02	0	0	0	0	1	534	1	2.16	1	206.59
7	535.02	1	.	1	0	1	535	1	1.80	1	196.39
7	536.02	1	0	1	0	1	534	1	2.34	1	155.58
7	537.02	0	1	1	0	1	535	1	1.98	1	196.39
7	538.02	0	0	0	0	1	535	1	1.98	1	196.39
7	539.02	1	1	1	0	1	535	1	1.62	1	196.39
7	540.02	1	0	1	0	1	541	0	1.44	1	145.38
7	541.02	1	.	1	0	3	541	0	1.44	1	145.38
7	542.02	1	0	1	0	1	541	0	1.44	1	237.19
7	543.02	1	0	1	0	1	541	0	1.44	1	186.19
7	544.02	1	.	1	0	1	544	1	1.44	1	237.19
7	545.02	1	.	1	0	1	545	1	1.44	2	237.19
7	546.02	0	1	0	0	1	545	1	1.98	2	237.19
7	547.02	0	1	0	0	1	544	1	1.80	1	155.58
7	548.02	0	.	1	0	1	548	0	2.16	1	155.58
7	549.02	1	1	1	0	1	548	0	1.98	2	135.18
7	550.02	1	0	1	0	1	548	0	2.16	2	135.18
7	551.02	1	0	1	0	1	548	0	1.98	1	135.18
7	552.02	1	1	1	0	1	548	0	1.80	2	175.99
7	553.02	0	1	1	0	1	548	0	2.16	1	165.78
7	554.02	1	0	1	0	1	548	0	2.16	1	114.78
7	555.02	1	0	1	0	1	548	0	2.16	2	186.19
7	556.02	1	0	1	0	1	548	0	1.98	2	196.39
7	557.02	0	1	1	0	1	548	0	1.98	1	155.58
7	558.02	0	0	0	0	1	548	0	2.16	1	155.58
7	559.02	1	1	0	0	1	548	0	2.34	1	237.19
7	560.02	0	1	1	0	1	548	0	2.34	1	155.58
7	561.02	1	1	1	0	1	548	0	1.98	2	196.39
7	562.02	0	1	0	0	1	548	0	1.62	1	135.18
7	563.02	0	0	0	0	2	548	0	1.44	1	186.19
7	564.02	1	0	1	0	1	565	0	0.90	1	196.39
7	565.02	1	.	1	0	.	565	0	0.54	1	186.19
7	566.02	1	0	0	0	1	565	0	1.08	1	237.19
7	567.02	1	0	1	0	1	565	0	1.26	1	237.19
7	568.02	0	1	1	0	1	565	0	1.26	1	145.38
7	569.02	0	0	1	0	1	565	0	1.44	0	175.99
7	570.02	0	0	0	0	2	565	0	1.44	1	145.38
7	571.02	1	1	1	0	1	565	0	1.62	2	237.19
7	572.02	0	1	1	0	1	565	0	1.26	1	196.39
7	573.02	1	.	0	0	1	573	1	1.62	2	237.19
7	574.02	0	.	1	0	2	574	1	1.80	1	237.19

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	525.02	401.53	0.48	2.07	0.48	2.10	0		0	.
7	526.02	538.54	0.50	1.98	0.50	1.98	1	2	0	2.39
7	527.02	540.04	0.38	2.65	0.38	2.65	1	3	0	2.39
7	528.02	653.82	0.38	2.64	0.38	2.65	0		0	.
7	529.02	199.63	0.39	2.54	0.38	2.65	0		0	.
7	530.02	188.96	0.39	2.55	0.39	2.59	0		1	.
7	531.02	215.75	0.39	2.57	0.38	2.65	0		0	.
7	532.02	95.29	0.49	2.03	0.50	1.98	0		1	.
7	533.02	96.63	0.39	2.58	0.38	2.65	0		0	.
7	534.02	163.23	0.39	2.59	0.39	2.59	0		0	2.39
7	535.02	234.60	0.39	2.54	0.39	2.54	1	3	0	2.39
7	536.02	164.46	0.39	2.55	0.39	2.59	0		0	.
7	537.02	165.80	0.39	2.54	0.39	2.54	0		1	.
7	538.02	172.77	0.41	2.44	0.39	2.54	0		0	.
7	539.02	254.05	0.41	2.46	0.39	2.54	0		0	.
7	540.02	252.09	0.43	2.34	0.43	2.34	0		1	.
7	541.02	118.18	0.43	2.34	0.43	2.34	1	0	0	2.39
7	542.02	188.89	0.43	2.33	0.43	2.34	0		0	.
7	543.02	125.02	0.43	2.33	0.43	2.34	0		0	.
7	544.02	126.33	0.43	2.31	0.43	2.31	1	3	0	2.34
7	545.02	126.83	0.44	2.27	0.44	2.27	1	2	0	2.34
7	546.02	222.49	0.44	2.29	0.44	2.27	0		1	.
7	547.02	225.19	0.43	2.34	0.43	2.31	0		1	.
7	548.02	348.65	0.43	2.33	0.43	2.33	1	1	0	2.34
7	549.02	336.30	0.44	2.26	0.43	2.33	0		1	.
7	550.02	355.59	0.44	2.25	0.43	2.33	0		0	.
7	551.02	228.50	0.44	2.28	0.43	2.33	0		0	.
7	552.02	230.63	0.44	2.27	0.43	2.33	0		0	.
7	553.02	452.62	0.44	2.29	0.43	2.33	0		0	.
7	554.02	192.52	0.44	2.26	0.43	2.33	0		0	.
7	555.02	217.11	0.44	2.26	0.43	2.33	0		0	.
7	556.02	274.31	0.46	2.20	0.43	2.33	0		0	.
7	557.02	276.34	0.44	2.25	0.43	2.33	0		0	.
7	558.02	130.30	0.45	2.23	0.43	2.33	0		0	.
7	559.02	268.20	0.44	2.27	0.43	2.33	0		0	.
7	560.02	220.45	0.45	2.24	0.43	2.33	0		0	.
7	561.02	364.13	0.45	2.23	0.43	2.33	0		0	.
7	562.02	210.54	0.44	2.28	0.43	2.33	0		0	.
7	563.02	207.64	0.44	2.29	0.43	2.33	0		0	.
7	564.02	191.22	0.42	2.37	0.42	2.36	0		1	.
7	565.02	133.73	0.42	2.36	0.42	2.36	1	0	0	2.33
7	566.02	132.73	0.42	2.37	0.42	2.36	0		0	.
7	567.02	292.79	0.42	2.38	0.42	2.36	0		0	.
7	568.02	256.19	0.42	2.37	0.42	2.36	0		0	.
7	569.02	297.36	0.42	2.37	0.42	2.36	0		0	.
7	570.02	168.33	0.42	2.39	0.42	2.36	0		0	.
7	571.02	222.72	0.43	2.33	0.42	2.36	0		0	.
7	572.02	178.74	0.42	2.37	0.42	2.36	0		0	.
7	573.02	170.87	0.44	2.30	0.44	2.30	1	2	0	2.36
7	574.02	180.71	0.41	2.46	0.41	2.46	1	3	0	2.36

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	575.02	0	.	1	0	1	575	1	1.80	2	237.19
7	576.02	1	0	1	0	1	574	1	1.80	1	237.19
7	577.02	1	1	1	0	1	574	1	1.80	1	237.19
7	578.02	1	1	0	0	1	575	1	2.16	2	237.19
7	579.02	1	0	1	0	1	574	1	2.16	1	237.19
7	580.02	1	.	1	0	2	580	0	2.16	1	237.19
7	581.02	0	1	0	0	1	580	0	2.16	1	135.18
7	582.02	0	0	0	0	1	580	0	2.34	1	175.99
7	583.02	0	0	0	0	1	580	0	2.16	2	216.79
7	584.02	0	0	1	0	1	580	0	2.16	2	216.79
7	585.02	1	1	1	0	1	580	0	2.16	1	237.19
7	586.02	1	0	1	0	1	580	0	2.34	2	237.19
7	587.02	1	.	1	0	1	587	1	1.80	2	196.39
7	588.02	0	.	0	0	1	588	1	1.62	2	237.19
7	589.02	1	.	1	0	1	589	1	2.16	1	135.18
7	590.02	0	1	1	0	1	589	1	1.98	1	186.19
7	591.02	0	.	1	0	2	591	1	1.62	1	175.99
7	592.02	0	.	1	1	2	592	0	1.26	2	237.19
7	593.02	1	1	1	0	1	592	0	1.26	1	237.19
7	594.02	0	0	0	0	1	592	0	1.62	2	237.19
7	595.02	1	0	1	0	1	592	0	1.44	1	237.19
7	596.02	0	1	0	0	1	592	0	1.62	2	206.59
7	597.02	1	1	1	0	1	592	0	1.44	1	237.19
7	598.02	0	.	0	0	1	598	0	1.80	1	237.19
7	599.02	1	.	1	0	1	599	0	1.44	2	237.19
7	600.02	1	1	1	0	1	601	0	1.80	2	237.19
7	601.02	1	.	1	0	1	601	0	1.44	1	237.19
7	602.02	0	1	0	0	1	601	0	1.80	1	63.78
7	603.02	0	1	1	0	1	601	0	1.62	1	237.19
7	604.02	1	1	1	0	2	601	0	1.80	1	237.19
7	605.02	0	1	1	0	1	601	0	1.80	2	237.19
7	606.02	1	1	1	0	1	601	0	1.98	1	175.99
7	607.02	0	1	1	0	1	601	0	2.16	2	165.78
7	608.02	1	1	1	0	1	601	0	2.16	2	206.59
7	609.02	0	0	1	0	1	601	0	2.16	1	237.19
7	610.02	1	0	1	0	1	601	0	2.52	1	237.19
7	611.02	1	0	0	0	1	601	0	1.80	2	237.19
7	612.02	0	1	1	0	1	601	0	2.16	1	237.19
7	613.02	0	0	1	0	1	601	0	2.34	2	206.59
7	614.02	1	1	1	0	1	601	0	1.80	1	237.19
7	615.02	1	0	1	0	1	601	0	2.16	2	237.19
7	616.02	1	0	1	0	1	601	0	2.16	1	237.19
7	617.02	0	1	1	0	1	618	1	2.70	2	206.59
7	618.02	1	.	1	0	1	618	1	2.52	2	206.59
7	619.02	1	0	1	0	1	620	1	2.34	1	135.18
7	620.02	1	.	0	0	1	620	1	2.34	1	135.18
7	621.02	1	0	1	0	1	620	1	2.34	1	196.39
7	622.02	1	.	1	0	1	622	0	1.98	1	196.39
7	623.02	1	0	1	0	1	622	0	1.80	1	135.18
7	624.02	1	0	1	1	1	622	0	1.62	2	135.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	575.02	174.14	0.43	2.32	0.43	2.32	1	1	0	2.36
7	576.02	172.77	0.41	2.46	0.41	2.46	0		0	.
7	577.02	178.18	0.40	2.48	0.41	2.46	0		1	.
7	578.02	176.28	0.41	2.45	0.43	2.32	0		1	.
7	579.02	176.11	0.41	2.46	0.41	2.46	0		0	.
7	580.02	431.83	0.41	2.46	0.41	2.46	1	1	0	2.32
7	581.02	278.18	0.41	2.42	0.41	2.46	0		0	.
7	582.02	223.92	0.42	2.40	0.41	2.46	0		0	.
7	583.02	225.96	0.42	2.39	0.41	2.46	0		0	.
7	584.02	188.42	0.42	2.38	0.41	2.46	0		0	.
7	585.02	187.85	0.42	2.41	0.41	2.46	0		0	.
7	586.02	272.87	0.41	2.43	0.41	2.46	0		1	.
7	587.02	193.66	0.45	2.24	0.45	2.24	1	2	0	2.46
7	588.02	437.41	0.45	2.20	0.45	2.20	1	2	0	2.46
7	589.02	223.49	0.42	2.39	0.42	2.39	1	3	0	2.46
7	590.02	288.36	0.42	2.37	0.42	2.39	0		1	.
7	591.02	201.83	0.43	2.32	0.43	2.32	1	3	0	2.46
7	592.02	184.18	0.45	2.23	0.45	2.23	1	1	0	2.46
7	593.02	213.98	0.44	2.26	0.45	2.23	0		1	.
7	594.02	186.62	0.45	2.24	0.45	2.23	0		0	.
7	595.02	250.38	0.44	2.28	0.45	2.23	0		0	.
7	596.02	191.79	0.45	2.22	0.45	2.23	0		0	.
7	597.02	195.03	0.43	2.30	0.45	2.23	0		0	.
7	598.02	199.03	0.43	2.32	0.43	2.32	1	3	0	2.23
7	599.02	232.23	0.46	2.19	0.46	2.19	1	2	0	2.23
7	600.02	197.83	0.44	2.28	0.43	2.32	0		0	.
7	601.02	670.90	0.43	2.32	0.43	2.32	1	1	0	2.23
7	602.02	201.70	0.43	2.32	0.43	2.32	0		1	.
7	603.02	240.27	0.43	2.31	0.43	2.32	0		0	.
7	604.02	217.32	0.43	2.33	0.43	2.32	0		0	.
7	605.02	341.14	0.43	2.30	0.43	2.32	0		0	.
7	606.02	311.71	0.43	2.33	0.43	2.32	0		0	.
7	607.02	262.63	0.44	2.28	0.43	2.32	0		0	.
7	608.02	241.01	0.44	2.30	0.43	2.32	0		0	.
7	609.02	210.14	0.43	2.33	0.43	2.32	0		0	.
7	610.02	207.07	0.42	2.35	0.43	2.32	0		0	.
7	611.02	256.86	0.43	2.31	0.43	2.32	0		0	.
7	612.02	273.34	0.43	2.34	0.43	2.32	0		0	.
7	613.02	242.54	0.44	2.27	0.43	2.32	0		0	.
7	614.02	213.01	0.42	2.36	0.43	2.32	0		0	.
7	615.02	215.21	0.44	2.28	0.43	2.32	0		0	.
7	616.02	308.94	0.43	2.31	0.43	2.32	0		0	.
7	617.02	306.67	0.44	2.25	0.44	2.27	0		1	.
7	618.02	505.24	0.44	2.27	0.44	2.27	1	2	0	2.32
7	619.02	530.50	0.43	2.34	0.43	2.32	0		1	.
7	620.02	302.10	0.43	2.32	0.43	2.32	1	3	0	2.32
7	621.02	302.00	0.43	2.35	0.43	2.32	0		0	.
7	622.02	496.47	0.43	2.33	0.43	2.33	1	1	0	2.32
7	623.02	498.27	0.43	2.33	0.43	2.33	0		1	.
7	624.02	501.80	0.44	2.29	0.43	2.33	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	625.02	1	0	1	0	1	622	0	1.80	1	155.58
7	626.02	1	0	1	0	1	622	0	1.62	2	206.59
7	627.02	1	0	1	0	1	622	0	1.62	1	206.59
7	628.02	1	0	1	0	2	622	0	1.80	1	135.18
7	629.02	1	0	1	0	2	622	0	1.44	1	135.18
7	630.02	1	0	0	0	2	622	0	1.62	1	175.99
7	631.02	0	1	0	0	1	622	0	1.80	2	237.19
7	632.02	1	1	1	0	1	622	0	1.44	0	237.19
7	633.02	0	1	0	0	1	622	0	1.98	1	33.18
7	634.02	0	0	1	0	1	622	0	1.80	2	206.59
7	635.02	1	1	1	0	1	622	0	1.98	1	206.59
7	636.02	0	.	0	0	2	636	0	1.98	1	237.19
7	637.02	0	.	0	0	2	637	0	1.80	2	237.19
7	638.02	0	0	0	0	1	637	0	1.62	1	165.78
7	639.02	0	0	0	0	1	637	0	1.80	1	237.19
7	640.02	0	.	0	0	1	640	0	1.44	1	186.19
7	641.02	1	0	1	0	2	642	0	1.44	1	196.39
7	642.02	1	.	1	0	2	642	0	1.44	1	186.19
7	643.02	1	0	1	0	1	642	0	1.26	1	196.39
7	644.02	0	.	1	0	.	644	0	0.36	1	43.38
7	645.02	0	.	0	0	1	645	0	0.54	1	165.78
7	646.02	0	0	1	0	1	645	0	0.72	2	165.78
7	647.02	0	.	0	0	1	647	0	1.08	1	226.99
7	648.02	0	.	1	0	3	648	0	0.54	2	216.79
7	649.02	0	.	0	0	.	649	0	0.36	2	216.79
7	650.02	0	.	0	0	3	650	0	0.54	1	165.78
7	651.02	0	.	0	0	.	651	0	0.36	1	196.39
7	652.02	1	.	1	0	.	652	0	0.36	1	53.58
7	653.02	1	0	1	0	1	652	0	0.72	1	53.58
7	654.02	0	1	0	0	1	652	0	0.90	1	53.58
7	655.02	0	.	1	0	.	655	0	0.90	1	104.58
7	656.02	0	.	1	0	.	656	0	0.36	2	165.78
7	657.02	0	.	1	0	.	657	0	0.36	0	216.79
7	658.02	1	.	1	0	.	658	0	0.36	2	135.18
7	659.02	0	.	1	0	.	659	0	0.54	0	226.99
7	661.02	0	.	0	0	.	661	0	0.36	1	216.79
7	662.02	0	0	0	0	1	661	0	0.72	2	216.79
7	663.02	1	.	1	0	.	663	0	0.36	1	226.99
7	664.02	1	.	1	0	.	664	0	0.36	1	237.19
7	4.03	0	.	0	0	1	4	0	0.47	2	2.58
7	18.03	0	.	0	0	.	18	0	0.31	1	2.58
7	19.03	1	.	1	0	2	19	0	0.78	1	2.58
7	25.03	1	.	0	0	1	25	0	0.62	2	33.18
7	32.03	1	.	1	0	1	32	0	0.78	0	2.58
7	35.03	1	.	0	0	1	35	0	0.93	1	2.58
7	36.03	0	.	1	0	1	36	0	1.24	0	22.98
7	37.03	0	.	0	0	1	37	0	0.93	0	22.98
7	38.03	1	.	1	0	2	38	0	0.93	0	2.58
7	43.03	1	.	1	0	3	43	0	0.93	2	2.58
7	47.03	1	.	1	0	1	47	0	0.78	2	22.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	625.02	313.38	0.43	2.35	0.43	2.33	0		0	.
7	626.02	311.14	0.43	2.32	0.43	2.33	0		0	.
7	627.02	509.04	0.43	2.33	0.43	2.33	0		0	.
7	628.02	529.46	0.42	2.35	0.43	2.33	0		0	.
7	629.02	353.25	0.43	2.30	0.43	2.33	0		0	.
7	630.02	273.81	0.43	2.33	0.43	2.33	0		0	.
7	631.02	272.34	0.43	2.32	0.43	2.33	0		0	.
7	632.02	818.55	0.43	2.33	0.43	2.33	0		0	.
7	633.02	271.07	0.43	2.34	0.43	2.33	0		0	.
7	634.02	323.92	0.44	2.25	0.43	2.33	0		0	.
7	635.02	306.07	0.43	2.32	0.43	2.33	0		0	.
7	636.02	307.37	0.43	2.33	0.43	2.33	1	1	0	2.33
7	637.02	415.95	0.43	2.34	0.43	2.34	1	1	0	2.33
7	638.02	460.16	0.43	2.32	0.43	2.34	0		1	.
7	639.02	430.26	0.43	2.33	0.43	2.34	0		0	.
7	640.02	343.64	0.45	2.23	0.45	2.23	1	1	0	2.34
7	641.02	422.65	0.45	2.24	0.44	2.27	0		1	.
7	642.02	594.89	0.44	2.27	0.44	2.27	1	1	0	2.23
7	643.02	883.41	0.45	2.20	0.44	2.27	0		0	.
7	644.02	592.63	0.88	1.13	0.88	1.13	1	0	0	1.97
7	645.02	595.33	0.51	1.97	0.51	1.97	1	0	0	2.14
7	646.02	651.72	0.49	2.04	0.51	1.97	0		1	.
7	647.02	697.19	0.47	2.14	0.47	2.14	1	1	0	2.27
7	648.02	694.93	0.91	1.10	0.91	1.10	1	0	0	1.11
7	649.02	102.77	0.93	1.08	0.93	1.08	1	0	0	1.13
7	650.02	531.93	0.90	1.11	0.90	1.11	1	0	0	1.08
7	651.02	933.76	0.80	1.26	0.80	1.26	1	0	0	1.10
7	652.02	935.10	0.68	1.48	0.68	1.48	1	0	0	1.26
7	653.02	936.30	0.68	1.48	0.68	1.48	0		1	.
7	654.02	822.75	0.67	1.50	0.68	1.48	0		0	.
7	655.02	721.59	0.66	1.51	0.66	1.51	1	0	0	1.48
7	656.02	770.43	1.28	0.78	1.28	0.78	1	0	0	1.82
7	657.02	1072.34	0.55	1.82	0.55	1.82	1	0	0	1.51
7	658.02	979.98	0.92	1.09	0.92	1.09	1	0	0	0.78
7	659.02	1252.95	0.91	1.10	0.91	1.10	1	0	0	1.09
7	661.02	1010.74	0.69	1.45	0.69	1.45	1	0	0	1.10
7	662.02	1222.05	0.69	1.45	0.69	1.45	0		1	.
7	663.02	1049.52	0.82	1.23	0.82	1.23	1	0	0	1.45
7	664.02	142.65	0.90	1.11	0.90	1.11	1	0	0	1.23
7	4.03	54.59	1.04	0.96	1.04	0.96	1	2	0	.
7	18.03	46.81	0.77	1.30	0.77	1.30	1	3	0	.
7	19.03	48.02	0.74	1.35	0.74	1.35	1	0	0	.
7	25.03	46.68	0.92	1.09	0.92	1.09	1	1	0	1.35
7	32.03	68.47	0.74	1.36	0.74	1.36	1	1	0	1.09
7	35.03	74.71	0.78	1.28	0.78	1.28	1	1	0	1.36
7	36.03	65.30	1.03	0.97	1.03	0.97	1	1	0	1.01
7	37.03	64.19	0.99	1.01	0.99	1.01	1	1	0	1.28
7	38.03	83.88	0.99	1.01	0.99	1.01	1	0	0	0.97
7	43.03	86.19	0.70	1.42	0.70	1.42	1	0	0	1.01
7	47.03	67.60	0.68	1.47	0.68	1.47	1	1	0	1.42

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	48.03	0	.	0	1	1	48	0	1.24	1	22.98
7	58.03	1	.	1	0	1	58	0	1.55	0	22.98
7	59.03	0	0	0	0	1	60	0	1.40	2	2.58
7	60.03	0	.	0	0	1	60	0	1.40	1	2.58
7	61.03	0	0	0	0	2	60	0	1.40	0	33.18
7	63.03	1	.	1	0	1	63	0	1.09	1	33.18
7	64.03	0	.	0	1	1	64	0	1.24	2	12.78
7	65.03	1	.	1	0	1	65	0	1.24	2	33.18
7	67.03	1	.	1	0	2	67	0	1.09	1	33.18
7	68.03	1	1	1	0	1	67	0	1.24	2	33.18
7	69.03	0	1	0	0	1	67	0	0.93	1	33.18
7	70.03	1	0	1	0	1	67	0	1.09	2	33.18
7	71.03	1	0	1	0	1	67	0	1.09	1	33.18
7	72.03	1	.	1	0	1	72	0	1.24	2	33.18
7	73.03	1	0	1	0	1	72	0	0.93	0	12.78
7	74.03	1	.	1	0	2	74	0	1.09	1	12.78
7	77.03	1	.	0	0	1	77	1	1.24	2	33.18
7	78.03	1	.	1	0	1	78	1	1.24	0	33.18
7	80.03	1	0	1	0	2	78	1	1.40	0	12.78
7	90.03	1	.	1	0	1	90	1	1.55	2	33.18
7	91.03	1	.	1	0	1	91	1	1.09	1	33.18
7	92.03	1	0	0	0	1	90	1	1.71	2	33.18
7	93.03	1	.	0	0	1	94	1	1.87	2	84.18
7	94.03	1	.	1	0	1	94	1	1.87	2	53.58
7	95.03	0	.	0	0	1	95	1	2.02	1	84.18
7	96.03	1	.	0	0	1	94	1	2.18	2	33.18
7	97.03	0	.	0	0	1	97	1	2.33	2	33.18
7	98.03	1	.	1	0	1	98	1	2.33	0	33.18
7	104.03	1	.	1	0	1	104	1	2.33	0	12.78
7	106.03	0	.	1	0	1	106	1	2.33	2	12.78
7	107.03	1	0	1	0	1	106	1	2.33	2	53.58
7	109.03	0	1	0	0	1	106	1	2.33	2	22.98
7	110.03	1	1	1	0	1	111	1	2.33	1	2.58
7	111.03	1	.	1	0	1	111	1	1.71	1	12.78
7	112.03	1	0	1	0	1	111	1	2.49	1	2.58
7	116.03	0	1	1	0	1	111	1	2.02	1	33.18
7	117.03	1	0	1	0	1	111	1	1.87	1	33.18
7	118.03	0	.	0	0	1	118	1	2.18	0	2.58
7	119.03	0	.	0	0	1	119	1	2.18	2	33.18
7	123.03	1	.	1	0	1	123	1	2.02	1	2.58
7	124.03	0	0	0	0	1	111	1	2.18	1	12.78
7	127.03	1	.	0	0	1	127	1	2.49	1	33.18
7	129.03	1	.	1	0	1	129	1	2.02	2	12.78
7	130.03	1	.	1	0	1	130	1	2.33	1	43.38
7	133.03	0	1	0	0	1	130	1	2.02	1	43.38
7	134.03	0	.	0	0	1	134	0	2.18	0	33.18
7	140.03	1	.	1	0	1	140	1	2.18	2	33.18
7	141.03	1	.	1	0	1	141	1	2.18	1	33.18
7	142.03	0	.	1	0	1	142	0	2.33	0	2.58
7	143.03	0	.	0	0	1	143	0	1.87	0	2.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	48.03	145.48	0.62	1.61	0.62	1.61	1	4	0	1.47
7	58.03	93.96	0.58	1.74	0.58	1.74	1	4	0	1.61
7	59.03	92.09	0.57	1.76	0.56	1.78	0		1	.
7	60.03	70.23	0.56	1.78	0.56	1.78	1	4	0	1.74
7	61.03	130.93	0.56	1.78	0.56	1.78	0		0	.
7	63.03	100.03	0.60	1.67	0.60	1.67	1	2	0	1.78
7	64.03	47.31	0.57	1.75	0.57	1.75	1	3	0	1.78
7	65.03	172.41	0.57	1.74	0.57	1.74	1	1	0	1.78
7	67.03	78.78	0.60	1.66	0.60	1.66	1	1	0	1.74
7	68.03	76.57	0.61	1.64	0.60	1.66	0		0	.
7	69.03	79.94	0.60	1.66	0.60	1.66	0		1	.
7	70.03	81.64	0.61	1.65	0.60	1.66	0		0	.
7	71.03	87.15	0.59	1.71	0.60	1.66	0		0	.
7	72.03	115.22	0.68	1.48	0.68	1.48	1	2	0	1.66
7	73.03	114.18	0.64	1.57	0.68	1.48	0		1	.
7	74.03	184.49	0.58	1.73	0.58	1.73	1	3	0	1.66
7	77.03	91.09	0.59	1.69	0.59	1.69	1	2	0	1.66
7	78.03	150.91	0.55	1.82	0.55	1.82	1	3	0	1.66
7	80.03	159.49	0.56	1.79	0.55	1.82	0		1	.
7	90.03	93.59	0.53	1.88	0.53	1.88	1	2	0	1.66
7	91.03	97.19	0.49	2.02	0.49	2.02	1	3	0	1.66
7	92.03	54.42	0.53	1.87	0.53	1.88	0		1	.
7	93.03	84.08	0.56	1.79	0.56	1.80	1	0	1	.
7	94.03	40.00	0.56	1.80	0.56	1.80	1	1	0	1.82
7	95.03	100.43	0.55	1.82	0.55	1.82	1	1	0	1.66
7	96.03	104.13	0.56	1.80	0.56	1.80	1	0	0	.
7	97.03	99.36	0.50	1.98	0.50	1.98	1	2	0	1.91
7	98.03	167.50	0.52	1.91	0.52	1.91	1	1	0	1.80
7	104.03	171.71	0.48	2.09	0.48	2.09	1	2	0	1.91
7	106.03	97.36	0.48	2.08	0.48	2.08	1	2	0	1.91
7	107.03	216.75	0.48	2.10	0.48	2.08	0		1	.
7	109.03	137.30	0.49	2.03	0.48	2.08	0		0	.
7	110.03	126.19	0.43	2.32	0.40	2.48	0		0	.
7	111.03	139.91	0.40	2.48	0.40	2.48	1	3	0	1.91
7	112.03	224.46	0.43	2.32	0.40	2.48	0		0	.
7	116.03	101.60	0.40	2.53	0.40	2.48	0		0	.
7	117.03	142.01	0.40	2.50	0.40	2.48	0		1	.
7	118.03	109.07	0.42	2.39	0.42	2.39	1	1	0	1.91
7	119.03	230.57	0.48	2.07	0.48	2.07	1	2	0	1.91
7	123.03	131.63	0.38	2.61	0.38	2.61	1	4	0	2.39
7	124.03	233.27	0.40	2.53	0.40	2.48	0		0	.
7	127.03	189.08	0.42	2.36	0.42	2.36	1	3	0	1.91
7	129.03	73.37	0.46	2.20	0.46	2.20	1	2	0	2.39
7	130.03	196.49	0.40	2.52	0.40	2.52	1	3	0	2.39
7	133.03	116.21	0.40	2.53	0.40	2.52	0		0	.
7	134.03	247.95	0.42	2.36	0.42	2.36	1	2	0	2.64
7	140.03	111.24	0.44	2.25	0.44	2.25	1	2	0	2.39
7	141.03	150.02	0.38	2.64	0.38	2.64	1	1	0	2.61
7	142.03	151.82	0.41	2.42	0.41	2.42	1	2	0	2.64
7	143.03	153.09	0.37	2.69	0.37	2.69	1	3	0	2.64

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	144.03	0	.	1	0	1	144	0	2.33	1	2.58
7	145.03	1	.	1	0	1	145	0	2.33	1	2.58
7	149.03	1	.	0	0	1	149	0	2.02	1	12.78
7	151.03	1	.	1	0	1	151	0	2.33	1	22.98
7	152.03	1	.	1	0	1	152	0	2.02	1	33.18
7	153.03	0	.	0	0	2	153	0	1.71	1	33.18
7	154.03	1	1	1	0	2	153	0	1.87	1	33.18
7	157.03	0	.	0	0	1	157	0	2.02	2	33.18
7	158.03	0	0	0	0	1	157	0	1.71	1	33.18
7	159.03	0	0	0	0	1	157	0	2.02	1	33.18
7	160.03	1	1	0	0	1	157	0	2.49	2	43.38
7	161.03	1	0	1	0	1	157	0	2.18	1	33.18
7	162.03	1	.	1	0	1	162	0	2.64	2	73.98
7	163.03	1	0	1	0	1	157	0	2.80	2	73.98
7	164.03	1	.	1	0	1	164	0	2.80	2	33.18
7	165.03	1	0	1	0	1	157	0	2.33	1	33.18
7	167.03	1	.	1	0	1	167	1	2.64	2	33.18
7	169.03	1	0	1	0	1	167	1	2.64	2	73.98
7	171.03	1	0	1	0	1	167	1	2.64	2	73.98
7	173.03	0	1	1	1	1	167	1	2.80	2	73.98
7	175.03	1	1	1	0	1	167	1	2.95	2	33.18
7	176.03	1	1	1	0	1	178	1	2.80	1	33.18
7	177.03	1	.	1	0	1	177	0	2.80	1	2.58
7	178.03	1	.	1	0	1	178	1	2.95	1	2.58
7	179.03	1	0	1	0	1	178	1	2.64	1	2.58
7	180.03	1	0	1	0	1	178	1	2.64	1	33.18
7	181.03	0	1	0	0	1	167	1	2.49	2	33.18
7	182.03	0	0	0	0	1	167	1	2.49	2	43.38
7	183.03	1	0	1	0	1	178	1	2.80	1	33.18
7	184.03	1	0	1	0	1	178	1	2.80	1	33.18
7	185.03	0	1	0	0	1	178	1	2.64	1	2.58
7	186.03	0	0	1	0	1	178	1	2.64	1	22.98
7	187.03	0	1	0	0	1	197	1	2.18	1	22.98
7	188.03	1	.	1	0	1	188	0	2.33	2	43.38
7	193.03	1	1	1	0	1	188	0	2.33	2	53.58
7	194.03	0	0	1	1	1	188	0	2.49	2	53.58
7	195.03	1	0	1	0	1	188	0	2.33	2	33.18
7	196.03	1	.	1	0	1	196	1	2.18	1	33.18
7	197.03	1	.	1	0	1	197	1	2.80	1	33.18
7	199.03	1	0	0	0	1	197	1	2.02	1	33.18
7	200.03	0	1	0	0	1	188	0	2.33	1	84.18
7	201.03	0	0	1	0	1	188	0	2.33	1	84.18
7	202.03	1	0	0	0	1	188	0	2.33	1	43.38
7	203.03	1	0	0	0	1	188	0	2.64	1	43.38
7	204.03	1	.	1	0	2	204	0	2.49	1	53.58
7	205.03	1	0	1	0	2	204	0	2.18	1	33.18
7	208.03	1	1	1	0	1	209	0	1.71	0	53.58
7	209.03	0	.	1	0	2	209	0	1.71	1	53.58
7	211.03	0	.	0	0	1	211	0	1.87	0	33.18
7	212.03	1	0	1	0	1	211	0	2.18	2	73.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	144.03	155.39	0.38	2.63	0.38	2.63	1	3	0	2.64
7	145.03	207.27	0.40	2.52	0.40	2.52	1	3	0	2.64
7	149.03	209.67	0.38	2.62	0.38	2.62	1	3	0	2.64
7	151.03	118.21	0.37	2.71	0.37	2.71	1	4	0	2.64
7	152.03	120.52	0.38	2.62	0.38	2.62	1	1	0	2.71
7	153.03	121.82	0.38	2.64	0.38	2.64	1	0	1	2.62
7	154.03	220.05	0.38	2.66	0.38	2.64	0		0	.
7	157.03	123.29	0.34	2.93	0.34	2.93	1	4	0	2.64
7	158.03	124.22	0.34	2.91	0.34	2.93	0		1	.
7	159.03	98.40	0.34	2.94	0.34	2.93	0		0	.
7	160.03	127.39	0.34	2.90	0.34	2.93	0		0	.
7	161.03	79.11	0.34	2.95	0.34	2.93	0		0	.
7	162.03	76.41	0.34	2.93	0.34	2.93	1	1	0	2.93
7	163.03	131.69	0.34	2.95	0.34	2.93	0		0	.
7	164.03	129.39	0.34	2.93	0.34	2.93	1	4	0	2.93
7	165.03	229.29	0.33	2.99	0.34	2.93	0		0	.
7	167.03	231.56	0.37	2.72	0.37	2.72	1	2	0	3.16
7	169.03	314.04	0.37	2.72	0.37	2.72	0		1	.
7	171.03	289.33	0.37	2.71	0.37	2.72	0		0	.
7	173.03	291.56	0.37	2.72	0.37	2.72	0		0	.
7	175.03	144.04	0.37	2.74	0.37	2.72	0		0	.
7	176.03	174.58	0.35	2.83	0.32	3.15	0		0	.
7	177.03	177.54	0.32	3.16	0.32	3.16	1	4	0	2.93
7	178.03	180.15	0.32	3.15	0.32	3.15	1	3	0	3.16
7	179.03	133.63	0.32	3.09	0.32	3.15	0		1	.
7	180.03	150.65	0.33	3.01	0.32	3.15	0		0	.
7	181.03	114.85	0.36	2.80	0.37	2.72	0		0	.
7	182.03	136.17	0.35	2.88	0.37	2.72	0		0	.
7	183.03	137.03	0.34	2.91	0.32	3.15	0		0	.
7	184.03	185.72	0.34	2.91	0.32	3.15	0		0	.
7	185.03	142.84	0.34	2.91	0.32	3.15	0		0	.
7	186.03	151.85	0.34	2.92	0.32	3.15	0		0	.
7	187.03	125.66	0.35	2.86	0.33	3.03	0		0	.
7	188.03	304.97	0.35	2.88	0.35	2.88	1	1	0	3.16
7	193.03	129.19	0.35	2.88	0.35	2.88	0		0	.
7	194.03	162.19	0.34	2.91	0.35	2.88	0		0	.
7	195.03	147.74	0.36	2.81	0.35	2.88	0		0	.
7	196.03	146.61	0.32	3.13	0.32	3.13	1	3	0	3.16
7	197.03	274.17	0.33	3.03	0.33	3.03	1	3	0	3.16
7	199.03	58.09	0.34	2.91	0.33	3.03	0		1	.
7	200.03	57.02	0.35	2.89	0.35	2.88	0		1	.
7	201.03	121.89	0.35	2.89	0.35	2.88	0		0	.
7	202.03	123.09	0.35	2.89	0.35	2.88	0		0	.
7	203.03	132.13	0.35	2.87	0.35	2.88	0		0	.
7	204.03	169.07	0.35	2.90	0.35	2.90	1	4	0	2.88
7	205.03	337.27	0.34	2.95	0.35	2.90	0		1	.
7	208.03	133.33	0.33	3.06	0.33	3.06	0		1	.
7	209.03	286.48	0.33	3.06	0.33	3.06	1	4	0	2.90
7	211.03	97.43	0.32	3.14	0.32	3.14	1	4	0	3.06
7	212.03	95.69	0.32	3.12	0.32	3.14	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	213.03	1	1	1	0	1	211	0	1.87	1	73.98
7	216.03	0	1	1	0	1	217	0	2.18	2	33.18
7	217.03	1	.	1	0	1	217	0	2.02	1	33.18
7	218.03	0	0	1	0	1	217	0	2.80	2	2.58
7	219.03	0	0	0	0	1	217	0	2.49	1	2.58
7	220.03	0	.	1	0	1	220	1	2.64	2	73.98
7	221.03	0	0	0	0	1	220	1	2.95	2	104.58
7	222.03	1	1	1	0	1	220	1	2.80	2	53.58
7	224.03	1	.	1	0	1	224	1	2.64	1	33.18
7	225.03	0	1	1	0	1	220	1	2.80	2	63.78
7	226.03	1	0	1	0	1	224	1	2.33	1	73.98
7	227.03	1	1	1	0	1	220	1	2.49	2	53.58
7	228.03	1	0	0	0	1	224	1	2.95	1	33.18
7	229.03	1	0	1	0	1	224	1	2.64	1	53.58
7	230.03	1	0	0	0	1	224	1	2.95	1	33.18
7	231.03	1	0	1	0	1	220	1	2.95	2	33.18
7	232.03	0	1	0	0	1	224	1	2.64	1	33.18
7	233.03	1	1	1	0	1	224	1	2.80	1	33.18
7	234.03	1	.	1	0	1	234	0	2.95	2	22.98
7	235.03	1	.	1	0	1	235	1	2.95	0	22.98
7	236.03	1	0	1	1	1	224	1	2.64	1	22.98
7	240.03	1	0	1	0	1	234	0	3.11	1	12.78
7	241.03	0	1	0	0	1	234	0	2.95	2	53.58
7	242.03	1	0	1	0	1	234	0	2.80	2	104.58
7	243.03	0	1	0	0	1	234	0	2.49	2	104.58
7	244.03	0	.	1	0	1	244	1	2.64	2	104.58
7	245.03	1	1	1	0	1	244	1	2.64	2	53.58
7	246.03	1	1	1	0	1	234	0	2.80	1	53.58
7	247.03	1	0	1	0	1	234	0	2.64	1	53.58
7	248.03	0	.	0	0	1	244	1	3.11	2	43.38
7	249.03	1	1	1	0	1	234	0	2.64	1	53.58
7	250.03	0	0	1	0	1	244	1	2.95	2	53.58
7	251.03	0	.	0	0	1	251	1	2.80	1	33.18
7	252.03	0	1	1	0	1	251	1	2.49	1	145.38
7	253.03	1	1	1	0	1	251	1	2.80	1	33.18
7	254.03	1	1	1	0	1	251	1	2.80	1	43.38
7	255.03	0	0	0	0	1	251	1	2.80	1	145.38
7	256.03	1	1	1	0	1	244	1	2.49	2	53.58
7	257.03	1	0	1	0	1	251	1	2.80	1	33.18
7	258.03	1	.	1	0	1	258	0	2.49	1	53.58
7	259.03	0	1	1	0	1	258	0	2.64	2	33.18
7	260.03	0	1	1	0	1	258	0	2.49	2	53.58
7	261.03	1	1	1	0	1	258	0	2.64	2	53.58
7	262.03	1	1	1	0	1	258	0	2.33	1	43.38
7	263.03	0	0	0	1	1	258	0	2.33	1	33.18
7	264.03	0	1	0	0	1	258	0	2.33	2	53.58
7	265.03	1	0	1	0	1	258	0	2.33	1	53.58
7	266.03	1	0	1	0	1	258	0	2.49	2	53.58
7	267.03	1	1	1	0	1	258	0	2.33	1	53.58
7	268.03	1	0	1	0	1	258	0	2.18	2	53.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	213.03	295.72	0.32	3.13	0.32	3.14	0		1	.
7	216.03	176.77	0.30	3.29	0.30	3.33	0		1	.
7	217.03	235.14	0.30	3.33	0.30	3.33	1	4	0	3.14
7	218.03	232.13	0.30	3.29	0.30	3.33	0		0	.
7	219.03	102.17	0.30	3.29	0.30	3.33	0		0	.
7	220.03	66.84	0.31	3.25	0.31	3.25	1	2	0	3.33
7	221.03	141.71	0.31	3.21	0.31	3.25	0		1	.
7	222.03	302.90	0.32	3.14	0.31	3.25	0		0	.
7	224.03	107.97	0.29	3.48	0.29	3.48	1	3	0	3.33
7	225.03	104.14	0.31	3.20	0.31	3.25	0		0	.
7	226.03	149.85	0.29	3.50	0.29	3.48	0		1	.
7	227.03	182.35	0.31	3.21	0.31	3.25	0		0	.
7	228.03	143.51	0.29	3.51	0.29	3.48	0		0	.
7	229.03	183.98	0.29	3.46	0.29	3.48	0		0	.
7	230.03	194.36	0.29	3.51	0.29	3.48	0		0	.
7	231.03	187.82	0.32	3.17	0.31	3.25	0		0	.
7	232.03	189.49	0.29	3.46	0.29	3.48	0		0	.
7	233.03	196.86	0.29	3.45	0.29	3.48	0		0	.
7	234.03	195.19	0.31	3.24	0.31	3.24	1	1	0	3.33
7	235.03	193.19	0.31	3.27	0.31	3.27	1	2	0	3.33
7	236.03	374.88	0.29	3.48	0.29	3.48	0		0	.
7	240.03	156.75	0.30	3.32	0.31	3.24	0		1	.
7	241.03	70.87	0.31	3.27	0.31	3.24	0		0	.
7	242.03	71.81	0.30	3.30	0.31	3.24	0		0	.
7	243.03	76.04	0.32	3.15	0.31	3.24	0		0	.
7	244.03	166.00	0.33	3.06	0.33	3.06	1	2	0	3.24
7	245.03	145.48	0.34	2.96	0.33	3.06	0		1	.
7	246.03	155.32	0.30	3.32	0.31	3.24	0		0	.
7	247.03	168.47	0.30	3.31	0.31	3.24	0		0	.
7	248.03	158.29	0.34	2.91	0.33	3.06	1	0	0	.
7	249.03	164.66	0.31	3.19	0.31	3.24	0		0	.
7	250.03	201.80	0.34	2.91	0.33	3.06	0		0	.
7	251.03	39.07	0.32	3.10	0.32	3.10	1	3	0	3.24
7	252.03	209.27	0.32	3.09	0.32	3.10	0		0	.
7	253.03	160.72	0.32	3.09	0.32	3.10	0		0	.
7	254.03	39.91	0.32	3.11	0.32	3.10	0		1	.
7	255.03	165.36	0.33	3.07	0.32	3.10	0		0	.
7	256.03	213.31	0.34	2.94	0.33	3.06	0		0	.
7	257.03	166.43	0.32	3.08	0.32	3.10	0		0	.
7	258.03	218.98	0.33	3.07	0.33	3.07	1	1	0	3.24
7	259.03	172.54	0.34	2.96	0.33	3.07	0		1	.
7	260.03	176.27	0.34	2.95	0.33	3.07	0		0	.
7	261.03	170.13	0.33	2.99	0.33	3.07	0		0	.
7	262.03	221.78	0.33	3.05	0.33	3.07	0		0	.
7	263.03	175.21	0.33	2.99	0.33	3.07	0		0	.
7	264.03	169.07	0.33	2.99	0.33	3.07	0		0	.
7	265.03	173.54	0.33	2.99	0.33	3.07	0		0	.
7	266.03	171.44	0.34	2.98	0.33	3.07	0		0	.
7	267.03	174.67	0.33	3.02	0.33	3.07	0		0	.
7	268.03	304.30	0.34	2.90	0.33	3.07	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	269.03	1	0	1	0	1	258	0	2.49	1	2.58
7	270.03	0	0	0	0	1	258	0	2.49	2	94.38
7	272.03	0	1	1	0	1	258	0	2.64	2	33.18
7	273.03	0	0	1	0	1	258	0	2.49	2	114.78
7	274.03	1	1	1	0	1	258	0	2.33	1	2.58
7	275.03	1	0	1	0	1	258	0	2.33	1	2.58
7	276.03	1	.	1	0	1	276	1	2.18	2	84.18
7	277.03	1	.	0	0	1	277	1	2.02	2	84.18
7	278.03	0	0	1	0	1	258	0	2.02	1	114.78
7	279.03	0	0	0	0	1	258	0	2.49	1	33.18
7	280.03	0	.	1	0	1	280	1	2.64	1	104.58
7	281.03	0	1	0	0	1	258	0	2.33	1	33.18
7	282.03	0	1	0	0	1	286	0	2.18	2	84.18
7	283.03	0	.	1	0	1	283	1	2.02	2	53.58
7	284.03	0	0	1	0	1	283	1	2.02	2	53.58
7	285.03	0	.	0	0	1	285	1	2.18	1	114.78
7	286.03	1	.	1	0	1	286	0	1.87	1	33.18
7	287.03	1	1	1	0	1	285	1	2.33	1	114.78
7	288.03	1	0	1	0	1	283	1	2.49	2	94.38
7	289.03	1	1	1	0	1	283	1	2.18	2	33.18
7	290.03	1	.	1	0	1	290	1	2.18	1	53.58
7	291.03	1	0	1	0	1	292	1	2.33	1	2.58
7	292.03	1	.	1	0	1	292	1	1.87	1	33.18
7	293.03	1	0	1	0	1	290	1	2.18	1	53.58
7	294.03	1	0	1	0	1	290	1	2.49	1	53.58
7	295.03	1	0	1	0	1	290	1	2.49	1	53.58
7	296.03	0	1	1	0	1	297	0	2.02	1	73.98
7	297.03	1	.	0	0	1	297	0	2.18	1	43.38
7	298.03	0	0	0	1	1	344	1	2.33	2	114.78
7	299.03	0	1	1	0	1	297	0	2.02	1	94.38
7	300.03	1	0	0	0	1	292	1	2.02	1	84.18
7	301.03	0	.	1	0	2	301	0	2.02	2	114.78
7	302.03	0	0	1	0	1	301	0	1.55	2	114.78
7	303.03	1	1	1	0	1	286	0	2.02	1	53.58
7	304.03	1	0	1	0	1	301	0	1.87	2	53.58
7	305.03	1	1	1	0	1	301	0	1.71	1	53.58
7	306.03	1	0	1	0	1	307	1	2.18	2	104.58
7	307.03	1	.	1	0	1	307	1	2.33	2	104.58
7	308.03	1	0	1	0	1	307	1	2.49	2	114.78
7	309.03	1	0	1	0	1	307	1	2.33	2	114.78
7	310.03	1	0	1	0	1	307	1	2.64	2	104.58
7	312.03	1	0	1	0	1	313	1	2.02	1	43.38
7	313.03	1	.	1	0	1	313	1	1.87	1	53.58
7	314.03	1	0	1	0	1	307	1	2.64	2	53.58
7	315.03	1	0	1	0	1	307	1	2.49	2	114.78
7	316.03	1	0	1	0	1	307	1	2.49	2	53.58
7	317.03	1	0	1	0	1	313	1	2.33	1	53.58
7	318.03	1	0	1	0	1	307	1	2.33	2	114.78
7	319.03	1	0	1	0	1	307	1	2.49	2	114.78
7	320.03	1	0	1	0	1	313	1	2.33	1	94.38

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	269.03	119.28	0.34	2.98	0.33	3.07	0		0	.
7	270.03	423.06	0.32	3.15	0.33	3.07	0		0	.
7	272.03	79.75	0.34	2.93	0.33	3.07	0		0	.
7	273.03	309.54	0.32	3.13	0.33	3.07	0		0	.
7	274.03	307.51	0.33	3.05	0.33	3.07	0		0	.
7	275.03	117.45	0.33	3.02	0.33	3.07	0		0	.
7	276.03	118.85	0.33	3.06	0.33	3.06	1	2	0	3.07
7	277.03	83.52	0.33	3.05	0.33	3.05	1	2	0	3.07
7	278.03	236.83	0.32	3.11	0.33	3.07	0		0	.
7	279.03	92.16	0.32	3.10	0.33	3.07	0		0	.
7	280.03	229.26	0.32	3.12	0.32	3.12	1	3	0	3.07
7	281.03	120.55	0.33	3.04	0.33	3.07	0		0	.
7	282.03	195.63	0.31	3.26	0.31	3.18	0		1	.
7	283.03	196.86	0.31	3.23	0.31	3.23	1	2	0	3.18
7	284.03	88.66	0.31	3.20	0.31	3.23	0		1	.
7	285.03	244.24	0.31	3.26	0.31	3.26	1	3	0	3.07
7	286.03	90.19	0.31	3.18	0.31	3.18	1	1	0	3.07
7	287.03	122.25	0.31	3.25	0.31	3.26	0		0	.
7	288.03	264.36	0.31	3.28	0.31	3.23	0		0	.
7	289.03	189.79	0.30	3.28	0.31	3.23	0		0	.
7	290.03	352.55	0.30	3.32	0.30	3.32	1	3	0	3.18
7	291.03	271.07	0.30	3.34	0.29	3.41	0		0	.
7	292.03	195.56	0.29	3.41	0.29	3.41	1	3	0	3.47
7	293.03	192.86	0.30	3.36	0.30	3.32	0		0	.
7	294.03	202.27	0.30	3.35	0.30	3.32	0		1	.
7	295.03	154.99	0.30	3.36	0.30	3.32	0		0	.
7	296.03	208.61	0.29	3.45	0.29	3.47	0		1	.
7	297.03	93.93	0.29	3.47	0.29	3.47	1	4	0	3.18
7	298.03	123.79	0.31	3.20	0.31	3.27	0		1	.
7	299.03	124.69	0.29	3.44	0.29	3.47	0		0	.
7	300.03	92.16	0.30	3.39	0.29	3.41	0		1	.
7	301.03	94.56	0.31	3.21	0.31	3.21	1	1	0	3.47
7	302.03	188.42	0.31	3.23	0.31	3.21	0		1	.
7	303.03	216.55	0.30	3.32	0.31	3.18	0		0	.
7	304.03	215.21	0.31	3.19	0.31	3.21	0		0	.
7	305.03	100.64	0.31	3.24	0.31	3.21	0		0	.
7	306.03	97.13	0.32	3.14	0.32	3.16	0		1	.
7	307.03	102.00	0.32	3.16	0.32	3.16	1	2	0	3.21
7	308.03	102.94	0.32	3.15	0.32	3.16	0		0	.
7	309.03	103.57	0.32	3.13	0.32	3.16	0		0	.
7	310.03	402.73	0.33	3.06	0.32	3.16	0		0	.
7	312.03	212.31	0.31	3.25	0.31	3.19	0		1	.
7	313.03	237.23	0.31	3.19	0.31	3.19	1	3	0	3.21
7	314.03	108.44	0.35	2.85	0.32	3.16	0		0	.
7	315.03	242.74	0.35	2.83	0.32	3.16	0		0	.
7	316.03	215.41	0.36	2.79	0.32	3.16	0		0	.
7	317.03	110.61	0.31	3.24	0.31	3.19	0		0	.
7	318.03	111.91	0.36	2.75	0.32	3.16	0		0	.
7	319.03	130.26	0.36	2.75	0.32	3.16	0		0	.
7	320.03	116.75	0.31	3.23	0.31	3.19	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	321.03	1	0	0	1	1	307	1	2.02	2	104.58
7	322.03	1	1	1	0	1	313	1	2.49	1	53.58
7	323.03	1	0	1	0	1	313	1	2.80	1	114.78
7	324.03	1	0	1	0	1	307	1	2.02	2	104.58
7	325.03	0	1	0	0	1	307	1	1.87	2	104.58
7	326.03	1	1	1	0	1	307	1	2.18	2	114.78
7	327.03	0	0	0	0	1	313	1	2.18	1	33.18
7	328.03	0	1	0	0	1	313	1	1.87	1	104.58
7	329.03	0	1	0	0	1	307	1	2.49	2	114.78
7	330.03	0	0	0	1	1	307	1	2.33	2	114.78
7	331.03	1	1	1	0	1	307	1	2.49	2	114.78
7	332.03	0	1	0	1	1	307	1	2.80	2	114.78
7	333.03	1	0	1	0	1	313	1	2.18	1	12.78
7	334.03	0	1	1	0	1	313	1	2.49	1	53.58
7	335.03	1	1	1	0	1	307	1	2.80	2	104.58
7	336.03	0	0	1	0	1	313	1	2.49	1	94.38
7	337.03	0	1	0	0	1	313	1	2.49	1	94.38
7	338.03	1	1	0	0	1	313	1	2.49	1	104.58
7	339.03	1	0	1	0	1	313	1	2.49	1	114.78
7	340.03	1	1	1	0	1	313	1	2.49	1	114.78
7	341.03	1	0	1	0	1	307	1	2.64	2	114.78
7	342.03	1	0	1	0	1	307	1	2.80	2	104.58
7	343.03	1	1	1	0	1	297	0	1.87	2	84.18
7	344.03	0	.	1	0	1	344	1	1.87	2	84.18
7	345.03	1	0	1	1	1	307	1	2.33	2	114.78
7	346.03	1	0	1	0	1	313	1	2.64	1	53.58
7	347.03	0	1	0	0	1	307	1	2.33	2	114.78
7	348.03	0	1	0	0	1	313	1	2.64	1	33.18
7	349.03	1	1	1	0	1	307	1	2.80	2	114.78
7	350.03	1	1	1	0	2	313	1	2.49	1	53.58
7	351.03	0	1	1	0	1	307	1	2.80	2	104.58
7	352.03	1	0	1	0	1	313	1	2.49	1	114.78
7	353.03	0	0	1	0	1	307	1	2.80	2	145.38
7	354.03	0	1	0	0	1	313	1	2.33	1	53.58
7	355.03	0	0	1	0	1	307	1	2.80	2	135.18
7	356.03	0	0	1	0	1	307	1	2.64	2	84.18
7	357.03	1	1	1	0	1	313	1	2.49	1	33.18
7	358.03	0	0	0	0	1	307	1	2.95	2	145.38
7	359.03	1	0	0	0	1	313	1	2.49	1	33.18
7	360.03	1	0	1	0	1	313	1	2.18	1	33.18
7	361.03	1	.	1	1	1	361	1	2.95	0	104.58
7	362.03	0	1	0	0	1	313	1	2.33	1	53.58
7	363.03	0	1	1	0	2	361	1	2.80	0	104.58
7	364.03	1	1	1	0	1	361	1	2.80	0	33.18
7	365.03	1	1	1	0	1	313	1	2.49	1	43.38
7	366.03	1	0	1	0	1	313	1	2.33	1	104.58
7	367.03	1	0	1	0	1	313	1	2.49	1	43.38
7	368.03	1	0	1	0	1	313	1	2.80	1	43.38
7	369.03	1	0	1	0	1	313	1	2.80	1	53.58
7	370.03	0	1	0	0	1	313	1	2.95	1	104.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	321.03	231.20	0.37	2.69	0.32	3.16	0		0	.
7	322.03	96.73	0.32	3.15	0.31	3.19	0		0	.
7	323.03	111.45	0.31	3.21	0.31	3.19	0		0	.
7	324.03	113.08	0.38	2.64	0.32	3.16	0		0	.
7	325.03	115.88	0.40	2.48	0.32	3.16	0		0	.
7	326.03	306.54	0.40	2.49	0.32	3.16	0		0	.
7	327.03	105.17	0.30	3.29	0.31	3.19	0		0	.
7	328.03	124.43	0.29	3.39	0.31	3.19	0		0	.
7	329.03	125.89	0.39	2.55	0.32	3.16	0		0	.
7	330.03	129.10	0.40	2.49	0.32	3.16	0		0	.
7	331.03	131.00	0.40	2.47	0.32	3.16	0		0	.
7	332.03	360.16	0.41	2.43	0.32	3.16	0		0	.
7	333.03	225.02	0.31	3.27	0.31	3.19	0		0	.
7	334.03	132.83	0.31	3.24	0.31	3.19	0		0	.
7	335.03	131.99	0.42	2.37	0.32	3.16	0		0	.
7	336.03	133.36	0.31	3.24	0.31	3.19	0		0	.
7	337.03	98.23	0.32	3.09	0.31	3.19	0		0	.
7	338.03	110.18	0.34	2.91	0.31	3.19	0		0	.
7	339.03	104.31	0.31	3.25	0.31	3.19	0		0	.
7	340.03	122.46	0.31	3.25	0.31	3.19	0		0	.
7	341.03	129.33	0.43	2.34	0.32	3.16	0		0	.
7	342.03	81.31	0.43	2.31	0.32	3.16	0		0	.
7	343.03	76.81	0.30	3.36	0.29	3.47	0		0	.
7	344.03	132.13	0.31	3.27	0.31	3.27	1	2	0	3.47
7	345.03	243.87	0.42	2.39	0.32	3.16	0		0	.
7	346.03	135.04	0.31	3.25	0.31	3.19	0		0	.
7	347.03	315.48	0.41	2.41	0.32	3.16	0		0	.
7	348.03	133.24	0.31	3.27	0.31	3.19	0		0	.
7	349.03	248.51	0.42	2.39	0.32	3.16	0		0	.
7	350.03	125.03	0.31	3.24	0.31	3.19	0		0	.
7	351.03	106.61	0.42	2.35	0.32	3.16	0		0	.
7	352.03	62.80	0.31	3.23	0.31	3.19	0		0	.
7	353.03	251.82	0.43	2.35	0.32	3.16	0		0	.
7	354.03	101.67	0.31	3.19	0.31	3.19	0		0	.
7	355.03	184.61	0.43	2.34	0.32	3.16	0		0	.
7	356.03	328.86	0.42	2.36	0.32	3.16	0		0	.
7	357.03	61.26	0.32	3.16	0.31	3.19	0		0	.
7	358.03	331.03	0.43	2.33	0.32	3.16	0		0	.
7	359.03	334.16	0.32	3.15	0.31	3.19	0		0	.
7	360.03	121.46	0.32	3.13	0.31	3.19	0		0	.
7	361.03	255.19	0.38	2.61	0.38	2.61	1	2	0	3.21
7	362.03	130.93	0.33	3.07	0.31	3.19	0		0	.
7	363.03	379.24	0.41	2.45	0.38	2.61	0		1	.
7	364.03	262.16	0.40	2.48	0.38	2.61	0		0	.
7	365.03	127.06	0.33	3.06	0.31	3.19	0		0	.
7	366.03	263.79	0.36	2.79	0.31	3.19	0		0	.
7	367.03	267.60	0.33	3.02	0.31	3.19	0		0	.
7	368.03	266.60	0.33	3.01	0.31	3.19	0		0	.
7	369.03	115.05	0.33	3.00	0.31	3.19	0		0	.
7	370.03	277.11	0.34	2.98	0.31	3.19	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	371.03	1	0	1	0	1	313	1	2.64	1	53.58
7	372.03	1	.	1	0	1	372	1	2.18	2	114.78
7	373.03	0	0	0	0	1	313	1	3.11	1	114.78
7	374.03	1	1	1	0	1	313	1	2.95	1	53.58
7	375.03	0	1	0	0	1	313	1	2.95	1	114.78
7	376.03	1	1	1	0	1	313	1	2.80	1	53.58
7	377.03	1	0	1	0	2	313	1	2.80	1	53.58
7	378.03	1	.	1	0	1	378	1	2.18	1	104.58
7	379.03	1	.	1	0	2	379	1	2.18	1	104.58
7	380.03	0	.	0	0	1	380	1	2.49	1	53.58
7	381.03	0	.	0	0	1	381	1	2.18	0	53.58
7	382.03	1	.	1	0	1	382	1	1.87	1	53.58
7	383.03	1	.	0	0	1	383	0	2.64	2	155.58
7	384.03	0	1	1	0	1	383	0	2.49	2	145.38
7	385.03	0	1	1	0	1	383	0	2.49	2	104.58
7	386.03	1	0	0	0	1	383	0	2.18	1	53.58
7	387.03	1	1	1	0	1	383	0	2.33	1	53.58
7	388.03	1	1	0	0	1	383	0	2.49	2	73.98
7	389.03	1	0	1	0	1	383	0	2.49	1	53.58
7	390.03	1	0	1	1	1	383	0	2.18	2	94.38
7	391.03	0	0	1	0	1	383	0	2.49	1	104.58
7	392.03	1	1	1	0	1	383	0	2.49	2	124.98
7	393.03	1	0	1	0	1	383	0	2.49	1	104.58
7	394.03	0	1	1	0	1	383	0	2.18	1	73.98
7	395.03	1	0	1	0	1	383	0	2.33	1	73.98
7	396.03	1	0	1	1	1	397	1	2.33	2	104.58
7	397.03	1	.	1	1	1	397	1	2.33	2	104.58
7	398.03	0	1	0	0	1	397	1	1.87	2	84.18
7	399.03	1	.	1	0	2	399	1	2.33	1	53.58
7	400.03	1	1	0	0	1	403	0	2.02	2	84.18
7	401.03	1	0	1	0	1	399	1	2.33	1	73.98
7	402.03	1	0	1	0	1	399	1	2.02	1	73.98
7	403.03	0	.	1	0	1	403	0	2.02	1	114.78
7	404.03	0	1	1	0	2	403	0	2.18	0	73.98
7	405.03	1	0	0	0	1	403	0	2.18	1	73.98
7	406.03	0	0	1	0	2	403	0	1.87	1	145.38
7	407.03	1	1	1	0	1	403	0	1.87	2	53.58
7	408.03	1	0	1	0	1	403	0	1.71	1	53.58
7	409.03	1	0	1	0	1	403	0	2.02	1	114.78
7	410.03	0	1	0	0	2	403	0	1.87	1	114.78
7	411.03	0	0	1	0	2	403	0	1.87	1	114.78
7	412.03	1	1	1	0	1	403	0	1.87	1	114.78
7	413.03	0	1	0	0	1	403	0	1.55	1	114.78
7	414.03	1	1	1	0	2	403	0	1.55	1	43.38
7	415.03	0	1	0	0	1	403	0	1.71	1	114.78
7	416.03	0	0	0	0	1	403	0	1.71	1	114.78
7	417.03	0	0	0	0	1	403	0	1.87	2	114.78
7	418.03	0	0	1	1	2	403	0	1.71	2	124.98
7	419.03	1	1	1	0	1	403	0	1.87	1	114.78
7	420.03	1	.	1	0	1	420	1	1.87	2	124.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	371.03	139.07	0.34	2.97	0.31	3.19	0		0	.
7	372.03	114.52	0.43	2.35	0.43	2.35	1	2	0	3.21
7	373.03	273.54	0.34	2.97	0.31	3.19	0		0	.
7	374.03	118.09	0.34	2.96	0.31	3.19	0		0	.
7	375.03	281.95	0.34	2.95	0.31	3.19	0		0	.
7	376.03	294.02	0.34	2.94	0.31	3.19	0		0	.
7	377.03	135.30	0.36	2.80	0.31	3.19	0		0	.
7	378.03	137.67	0.42	2.40	0.42	2.40	1	2	0	3.21
7	379.03	283.65	0.38	2.62	0.38	2.62	1	3	0	3.21
7	380.03	318.42	0.29	3.43	0.29	3.43	1	3	1	3.21
7	381.03	300.66	0.42	2.41	0.42	2.41	1	2	0	3.21
7	382.03	98.03	0.39	2.58	0.39	2.58	1	3	0	3.21
7	383.03	77.98	0.40	2.50	0.40	2.50	1	1	0	3.21
7	384.03	148.08	0.40	2.52	0.40	2.50	0		0	.
7	385.03	322.72	0.38	2.60	0.40	2.50	0		0	.
7	386.03	323.42	0.40	2.53	0.40	2.50	0		1	.
7	387.03	249.68	0.40	2.52	0.40	2.50	0		0	.
7	388.03	326.06	0.38	2.62	0.40	2.50	0		0	.
7	389.03	195.73	0.39	2.56	0.40	2.50	0		0	.
7	390.03	141.28	0.39	2.58	0.40	2.50	0		0	.
7	391.03	116.98	0.39	2.59	0.40	2.50	0		0	.
7	392.03	145.65	0.39	2.58	0.40	2.50	0		0	.
7	393.03	248.98	0.39	2.59	0.40	2.50	0		0	.
7	394.03	251.22	0.38	2.65	0.40	2.50	0		0	.
7	395.03	154.39	0.38	2.64	0.40	2.50	0		0	.
7	396.03	151.39	0.39	2.59	0.39	2.57	0		1	.
7	397.03	205.27	0.39	2.57	0.39	2.57	1	2	0	2.50
7	398.03	337.00	0.39	2.56	0.39	2.57	0		0	.
7	399.03	203.33	0.37	2.68	0.37	2.68	1	3	0	2.50
7	400.03	252.32	0.38	2.62	0.38	2.65	0		1	.
7	401.03	255.65	0.37	2.67	0.37	2.68	0		1	.
7	402.03	113.01	0.38	2.65	0.37	2.68	0		0	.
7	403.03	264.10	0.38	2.65	0.38	2.65	1	1	0	2.50
7	404.03	261.16	0.38	2.60	0.38	2.65	0		0	.
7	405.03	37.70	0.37	2.68	0.38	2.65	0		0	.
7	406.03	353.82	0.38	2.60	0.38	2.65	0		0	.
7	407.03	351.25	0.39	2.57	0.38	2.65	0		0	.
7	408.03	150.29	0.38	2.60	0.38	2.65	0		0	.
7	409.03	152.42	0.38	2.64	0.38	2.65	0		0	.
7	410.03	154.76	0.38	2.67	0.38	2.65	0		0	.
7	411.03	156.76	0.37	2.68	0.38	2.65	0		0	.
7	412.03	160.46	0.38	2.65	0.38	2.65	0		0	.
7	413.03	379.38	0.37	2.67	0.38	2.65	0		0	.
7	414.03	162.26	0.37	2.71	0.38	2.65	0		0	.
7	415.03	163.93	0.36	2.74	0.38	2.65	0		0	.
7	416.03	165.13	0.36	2.77	0.38	2.65	0		0	.
7	417.03	117.92	0.36	2.81	0.38	2.65	0		0	.
7	418.03	167.60	0.36	2.79	0.38	2.65	0		0	.
7	419.03	122.12	0.36	2.79	0.38	2.65	0		0	.
7	420.03	123.06	0.37	2.69	0.37	2.69	1	2	0	2.65

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	421.03	1	.	1	0	1	421	1	1.71	1	124.98
7	422.03	1	0	1	0	1	420	1	2.18	2	145.38
7	423.03	1	0	1	0	1	421	1	1.87	1	124.98
7	424.03	1	.	0	0	1	424	0	2.18	1	145.38
7	425.03	1	0	1	0	1	424	0	2.49	2	155.58
7	426.03	1	0	1	0	1	424	0	2.33	1	155.58
7	427.03	1	1	1	1	1	424	0	2.49	2	165.78
7	428.03	0	1	1	0	1	424	0	2.64	1	155.58
7	429.03	1	0	1	0	1	424	0	2.49	1	155.58
7	430.03	1	0	1	0	1	424	0	2.18	2	165.78
7	431.03	1	0	1	0	1	424	0	2.33	2	165.78
7	432.03	1	0	1	0	1	424	0	2.33	1	43.38
7	433.03	0	.	0	0	1	433	0	2.49	2	165.78
7	434.03	0	1	0	0	1	424	0	2.49	1	53.58
7	435.03	0	.	1	0	1	435	0	2.64	2	135.18
7	436.03	0	.	1	0	1	436	0	2.33	1	114.78
7	437.03	0	.	0	0	1	437	0	2.18	1	114.78
7	438.03	1	1	0	0	1	442	0	2.18	2	165.78
7	439.03	1	.	1	0	2	439	0	2.64	1	114.78
7	440.03	0	1	0	0	1	442	0	2.18	2	145.38
7	441.03	0	1	1	0	1	442	0	2.33	2	104.58
7	442.03	1	.	1	0	1	442	0	2.33	1	135.18
7	443.03	1	1	1	0	1	442	0	2.64	2	186.19
7	444.03	1	0	1	0	1	442	0	2.49	2	186.19
7	445.03	1	1	1	0	1	442	0	2.64	2	114.78
7	446.03	1	1	1	0	1	442	0	2.49	2	165.78
7	447.03	1	0	1	0	1	442	0	2.49	1	53.58
7	448.03	0	1	0	1	1	442	0	2.33	2	165.78
7	449.03	1	0	0	0	1	442	0	2.49	1	53.58
7	450.03	0	0	0	0	1	442	0	2.18	1	53.58
7	451.03	0	1	0	0	1	442	0	2.33	2	165.78
7	452.03	0	1	1	0	1	442	0	2.49	1	165.78
7	453.03	1	0	1	0	1	442	0	2.64	1	94.38
7	454.03	1	1	1	0	1	442	0	2.18	2	175.99
7	455.03	1	0	1	0	1	442	0	2.49	1	104.58
7	456.03	1	1	1	0	1	442	0	2.18	2	155.58
7	457.03	0	1	1	0	1	442	0	2.33	1	186.19
7	458.03	0	1	1	0	1	442	0	2.18	2	114.78
7	459.03	1	1	1	0	1	442	0	2.02	1	114.78
7	460.03	1	0	0	0	1	442	0	2.49	1	104.58
7	461.03	1	1	1	0	1	442	0	2.33	1	104.58
7	462.03	1	1	1	0	1	442	0	2.02	1	104.58
7	463.03	0	0	0	0	1	442	0	2.18	1	104.58
7	464.03	0	1	1	0	1	442	0	2.49	1	165.78
7	465.03	0	0	0	0	1	442	0	2.64	1	186.19
7	466.03	1	0	1	0	1	442	0	2.02	1	104.58
7	467.03	1	0	0	0	1	442	0	2.02	0	104.58
7	468.03	0	1	1	0	1	442	0	2.02	1	114.78
7	469.03	1	0	1	0	1	442	0	2.18	1	2.58
7	470.03	1	0	1	0	1	442	0	2.33	2	186.19

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	421.03	99.27	0.36	2.80	0.36	2.80	1	3	0	2.65
7	422.03	124.16	0.37	2.72	0.37	2.69	0		1	.
7	423.03	100.87	0.36	2.80	0.36	2.80	0		1	.
7	424.03	102.97	0.36	2.80	0.36	2.80	1	1	0	2.65
7	425.03	101.27	0.36	2.80	0.36	2.80	0		1	.
7	426.03	86.28	0.36	2.79	0.36	2.80	0		0	.
7	427.03	106.01	0.36	2.76	0.36	2.80	0		0	.
7	428.03	107.98	0.36	2.77	0.36	2.80	0		0	.
7	429.03	87.85	0.36	2.76	0.36	2.80	0		0	.
7	430.03	88.82	0.36	2.77	0.36	2.80	0		0	.
7	431.03	409.47	0.37	2.74	0.36	2.80	0		0	.
7	432.03	89.32	0.36	2.76	0.36	2.80	0		0	.
7	433.03	407.20	0.37	2.70	0.37	2.70	1	2	0	2.80
7	434.03	152.82	0.36	2.76	0.36	2.80	0		0	.
7	435.03	181.68	0.35	2.82	0.35	2.82	1	3	0	2.76
7	436.03	183.92	0.36	2.76	0.36	2.76	1	3	0	2.80
7	437.03	94.13	0.36	2.76	0.36	2.76	1	1	0	2.80
7	438.03	185.79	0.36	2.77	0.36	2.80	0		0	.
7	439.03	66.70	0.36	2.77	0.36	2.77	1	2	0	2.76
7	440.03	199.17	0.36	2.79	0.36	2.80	0		1	.
7	441.03	152.39	0.36	2.77	0.36	2.80	0		0	.
7	442.03	66.33	0.36	2.80	0.36	2.80	1	1	0	2.76
7	443.03	62.99	0.37	2.73	0.36	2.80	0		0	.
7	444.03	202.70	0.36	2.75	0.36	2.80	0		0	.
7	445.03	105.17	0.37	2.74	0.36	2.80	0		0	.
7	446.03	422.35	0.36	2.76	0.36	2.80	0		0	.
7	447.03	110.47	0.36	2.78	0.36	2.80	0		0	.
7	448.03	423.79	0.36	2.74	0.36	2.80	0		0	.
7	449.03	426.79	0.36	2.79	0.36	2.80	0		0	.
7	450.03	111.61	0.36	2.75	0.36	2.80	0		0	.
7	451.03	98.26	0.36	2.76	0.36	2.80	0		0	.
7	452.03	245.41	0.36	2.74	0.36	2.80	0		0	.
7	453.03	112.94	0.36	2.75	0.36	2.80	0		0	.
7	454.03	197.53	0.36	2.74	0.36	2.80	0		0	.
7	455.03	144.24	0.36	2.74	0.36	2.80	0		0	.
7	456.03	64.56	0.36	2.76	0.36	2.80	0		0	.
7	457.03	214.35	0.36	2.76	0.36	2.80	0		0	.
7	458.03	211.48	0.36	2.75	0.36	2.80	0		0	.
7	459.03	202.40	0.37	2.70	0.36	2.80	0		0	.
7	460.03	204.74	0.36	2.75	0.36	2.80	0		0	.
7	461.03	220.79	0.36	2.75	0.36	2.80	0		0	.
7	462.03	206.41	0.37	2.72	0.36	2.80	0		0	.
7	463.03	99.93	0.37	2.73	0.36	2.80	0		0	.
7	464.03	73.67	0.37	2.73	0.36	2.80	0		0	.
7	465.03	214.15	0.37	2.73	0.36	2.80	0		0	.
7	466.03	224.13	0.37	2.71	0.36	2.80	0		0	.
7	467.03	215.25	0.37	2.68	0.36	2.80	0		0	.
7	468.03	590.76	0.37	2.72	0.36	2.80	0		0	.
7	469.03	91.46	0.37	2.68	0.36	2.80	0		0	.
7	470.03	592.06	0.37	2.70	0.36	2.80	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	471.03	1	1	1	0	1	442	0	2.64	1	2.58
7	472.03	0	1	0	0	1	442	0	2.33	2	104.58
7	473.03	0	1	1	0	2	442	0	2.49	1	104.58
7	474.03	1	0	1	0	1	442	0	2.18	1	53.58
7	475.03	1	1	1	0	1	442	0	2.49	2	155.58
7	476.03	1	.	0	0	1	476	0	2.49	1	94.38
7	477.03	1	.	1	0	1	477	0	2.33	2	155.58
7	478.03	1	.	1	0	1	478	0	2.18	0	155.58
7	479.03	0	.	0	0	1	479	0	2.49	1	155.58
7	480.03	1	.	0	0	1	480	0	2.49	1	84.18
7	481.03	0	.	0	0	1	481	0	2.33	2	84.18
7	482.03	0	0	1	0	1	483	0	2.49	2	155.58
7	483.03	0	.	1	0	1	483	0	2.18	1	124.98
7	484.03	0	0	0	0	1	483	0	2.33	1	165.78
7	485.03	1	1	1	0	1	483	0	2.49	2	186.19
7	486.03	1	0	0	1	1	483	0	2.33	1	145.38
7	487.03	0	1	0	1	1	483	0	2.64	2	155.58
7	488.03	1	1	1	0	1	483	0	2.49	1	165.78
7	489.03	0	1	0	0	1	483	0	2.49	2	186.19
7	490.03	1	0	1	0	1	483	0	2.33	1	165.78
7	491.03	0	0	1	0	2	483	0	2.18	2	186.19
7	492.03	0	0	1	0	1	483	0	2.64	1	165.78
7	493.03	0	1	1	0	1	483	0	2.18	2	186.19
7	494.03	1	1	0	0	1	483	0	2.49	2	186.19
7	495.03	1	1	1	0	1	483	0	2.02	1	114.78
7	496.03	1	.	0	0	1	496	1	2.33	1	84.18
7	497.03	1	0	1	0	1	483	0	2.33	1	165.78
7	498.03	0	0	0	1	1	483	0	2.49	1	175.99
7	499.03	1	.	1	0	1	499	1	2.33	2	186.19
7	500.03	1	0	1	0	1	496	1	2.49	1	186.19
7	501.03	1	0	1	0	2	483	0	2.49	1	145.38
7	502.03	0	1	0	0	1	499	1	2.49	2	145.38
7	503.03	1	.	1	0	2	503	0	2.49	1	165.78
7	504.03	0	1	0	0	1	503	0	2.33	2	165.78
7	505.03	0	0	0	0	1	503	0	2.33	1	186.19
7	506.03	0	0	1	0	1	503	0	2.49	2	186.19
7	507.03	1	1	1	0	1	503	0	2.49	1	175.99
7	508.03	0	1	1	0	1	503	0	2.49	2	175.99
7	509.03	1	1	1	0	1	503	0	2.64	1	186.19
7	510.03	0	1	1	0	1	503	0	2.80	2	175.99
7	511.03	1	1	0	0	1	503	0	2.64	1	186.19
7	512.03	1	0	1	0	1	503	0	2.18	2	216.79
7	513.03	1	0	1	0	1	503	0	2.80	1	186.19
7	514.03	1	0	1	0	2	503	0	1.87	2	175.99
7	515.03	1	0	1	0	1	517	1	1.71	2	175.99
7	516.03	0	1	0	1	1	517	1	2.02	2	84.18
7	517.03	1	.	1	1	1	517	1	1.71	2	175.99
7	518.03	1	.	1	0	1	518	1	1.87	1	216.79
7	519.03	0	.	1	1	1	519	1	2.18	2	175.99
7	520.03	1	1	1	0	1	519	1	2.02	2	175.99

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	471.03	139.34	0.38	2.66	0.36	2.80	0		0	.
7	472.03	225.56	0.37	2.71	0.36	2.80	0		0	.
7	473.03	476.01	0.38	2.65	0.36	2.80	0		0	.
7	474.03	153.92	0.38	2.66	0.36	2.80	0		0	.
7	475.03	289.05	0.37	2.68	0.36	2.80	0		0	.
7	476.03	152.45	0.37	2.68	0.37	2.68	1	3	0	2.80
7	477.03	154.49	0.40	2.50	0.40	2.50	1	2	0	2.80
7	478.03	149.82	0.40	2.52	0.40	2.52	1	2	0	2.80
7	479.03	300.56	0.37	2.68	0.37	2.68	1	3	0	2.80
7	480.03	302.43	0.38	2.61	0.38	2.61	1	2	0	2.80
7	481.03	160.79	0.38	2.64	0.38	2.64	1	3	0	2.80
7	482.03	184.35	0.38	2.60	0.38	2.60	0		1	.
7	483.03	127.22	0.38	2.60	0.38	2.60	1	1	0	2.80
7	484.03	115.35	0.38	2.60	0.38	2.60	0		0	.
7	485.03	156.16	0.38	2.61	0.38	2.60	0		0	.
7	486.03	162.66	0.39	2.58	0.38	2.60	0		0	.
7	487.03	129.86	0.38	2.61	0.38	2.60	0		0	.
7	488.03	110.27	0.39	2.57	0.38	2.60	0		0	.
7	489.03	131.80	0.39	2.59	0.38	2.60	0		0	.
7	490.03	118.58	0.39	2.58	0.38	2.60	0		0	.
7	491.03	132.73	0.40	2.52	0.38	2.60	0		0	.
7	492.03	112.94	0.38	2.60	0.38	2.60	0		0	.
7	493.03	111.21	0.38	2.62	0.38	2.60	0		0	.
7	494.03	240.51	0.39	2.58	0.38	2.60	0		0	.
7	495.03	360.96	0.38	2.62	0.38	2.60	0		0	.
7	496.03	134.83	0.38	2.61	0.38	2.61	1	3	0	2.60
7	497.03	133.66	0.38	2.64	0.38	2.60	0		0	.
7	498.03	122.62	0.38	2.66	0.38	2.60	0		0	.
7	499.03	116.98	0.39	2.54	0.39	2.54	1	2	0	2.60
7	500.03	162.56	0.39	2.60	0.38	2.61	0		1	.
7	501.03	172.41	0.38	2.65	0.38	2.60	0		0	.
7	502.03	140.84	0.40	2.51	0.39	2.54	0		1	.
7	503.03	144.61	0.40	2.52	0.40	2.52	1	1	0	2.60
7	504.03	123.22	0.40	2.52	0.40	2.52	0		1	.
7	505.03	124.52	0.39	2.54	0.40	2.52	0		0	.
7	506.03	153.78	0.40	2.53	0.40	2.52	0		0	.
7	507.03	152.85	0.39	2.54	0.40	2.52	0		0	.
7	508.03	135.43	0.40	2.51	0.40	2.52	0		0	.
7	509.03	155.35	0.40	2.51	0.40	2.52	0		0	.
7	510.03	136.57	0.40	2.50	0.40	2.52	0		0	.
7	511.03	111.84	0.40	2.51	0.40	2.52	0		0	.
7	512.03	138.27	0.41	2.46	0.40	2.52	0		0	.
7	513.03	171.10	0.40	2.51	0.40	2.52	0		0	.
7	514.03	174.17	0.41	2.44	0.40	2.52	0		0	.
7	515.03	397.76	0.43	2.30	0.42	2.40	0		1	.
7	516.03	167.53	0.44	2.25	0.42	2.40	0		0	.
7	517.03	110.71	0.42	2.40	0.42	2.40	1	2	0	2.52
7	518.03	175.24	0.38	2.61	0.38	2.61	1	2	0	2.52
7	519.03	169.67	0.43	2.34	0.43	2.34	1	2	0	2.52
7	520.03	315.58	0.43	2.34	0.43	2.34	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	521.03	1	0	1	0	1	519	1	1.87	2	114.78
7	522.03	1	0	1	0	1	519	1	2.33	2	114.78
7	523.03	1	0	1	0	1	519	1	2.49	2	114.78
7	524.03	0	1	1	0	1	519	1	2.49	2	216.79
7	525.03	0	0	1	0	1	519	1	2.33	2	216.79
7	526.03	0	.	1	0	1	526	0	2.49	1	84.18
7	527.03	1	.	1	0	1	527	1	1.40	1	53.58
7	528.03	0	1	1	0	1	527	1	1.87	1	53.58
7	529.03	0	0	1	0	1	527	1	1.87	1	12.78
7	530.03	1	1	1	0	1	527	1	2.49	1	145.38
7	531.03	0	0	0	0	1	527	1	2.02	1	145.38
7	532.03	1	.	1	0	3	532	0	2.02	1	145.38
7	533.03	0	0	1	0	1	527	1	1.87	1	186.19
7	534.03	0	0	0	0	1	527	1	2.18	1	186.19
7	535.03	1	0	1	0	1	527	1	2.33	1	175.99
7	536.03	1	0	1	0	1	527	1	2.49	1	135.18
7	537.03	0	1	1	0	1	527	1	2.33	1	175.99
7	538.03	0	0	0	0	1	526	0	2.49	1	175.99
7	539.03	1	1	1	0	2	526	0	2.33	1	175.99
7	540.03	1	0	1	0	2	541	0	1.55	1	124.98
7	541.03	1	.	1	0	3	541	0	1.55	1	124.98
7	542.03	1	0	1	0	1	541	0	1.55	1	216.79
7	543.03	1	0	1	0	2	541	0	1.55	1	165.78
7	544.03	1	0	1	0	1	541	0	1.55	1	216.79
7	545.03	1	0	1	0	1	541	0	1.71	2	216.79
7	546.03	0	0	0	0	1	541	0	2.02	2	216.79
7	547.03	0	1	0	0	2	541	0	1.87	1	135.18
7	548.03	0	0	1	0	2	541	0	2.18	1	135.18
7	549.03	1	1	1	0	1	541	0	2.02	2	114.78
7	550.03	1	0	1	0	1	541	0	2.33	2	114.78
7	551.03	1	0	1	0	1	541	0	2.18	1	114.78
7	552.03	1	1	1	0	1	541	0	1.87	2	155.58
7	553.03	0	1	1	0	2	541	0	2.02	1	145.38
7	554.03	1	0	1	0	1	541	0	2.18	1	94.38
7	555.03	1	0	1	0	1	541	0	2.18	2	165.78
7	556.03	1	.	1	0	1	556	0	2.02	2	175.99
7	557.03	0	1	1	0	1	541	0	2.18	1	135.18
7	558.03	0	.	0	0	1	558	0	2.18	1	135.18
7	559.03	1	.	0	0	1	559	0	2.18	1	216.79
7	560.03	0	1	1	0	1	556	0	2.02	1	135.18
7	561.03	1	1	1	0	1	556	0	2.02	2	175.99
7	562.03	0	1	0	0	1	556	0	1.87	1	114.78
7	563.03	0	0	0	0	2	556	0	1.55	1	165.78
7	564.03	1	0	1	0	1	565	0	0.93	1	175.99
7	565.03	1	.	1	0	.	565	0	0.78	1	165.78
7	566.03	1	0	0	0	2	565	0	0.93	1	216.79
7	567.03	1	0	1	0	1	565	0	1.24	1	216.79
7	568.03	0	1	1	0	2	565	0	1.40	1	124.98
7	569.03	0	0	1	0	1	565	0	1.71	0	155.58
7	570.03	0	0	0	0	1	565	0	1.55	1	124.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	521.03	313.42	0.43	2.34	0.43	2.34	0		0	.
7	522.03	312.51	0.43	2.31	0.43	2.34	0		0	.
7	523.03	115.48	0.43	2.32	0.43	2.34	0		0	.
7	524.03	114.05	0.42	2.36	0.43	2.34	0		0	.
7	525.03	401.53	0.42	2.36	0.43	2.34	0		0	.
7	526.03	538.54	0.40	2.49	0.40	2.49	1	1	0	2.52
7	527.03	540.04	0.36	2.74	0.36	2.74	1	3	0	2.52
7	528.03	653.82	0.37	2.71	0.36	2.74	0		1	.
7	529.03	199.63	0.39	2.54	0.36	2.74	0		0	.
7	530.03	188.96	0.40	2.49	0.36	2.74	0		0	.
7	531.03	215.75	0.40	2.50	0.36	2.74	0		0	.
7	532.03	95.29	0.40	2.49	0.36	2.74	1	0	0	2.49
7	533.03	96.63	0.40	2.49	0.36	2.74	0		0	.
7	534.03	163.23	0.40	2.48	0.36	2.74	0		0	.
7	535.03	234.60	0.40	2.48	0.36	2.74	0		0	.
7	536.03	164.46	0.40	2.48	0.36	2.74	0		0	.
7	537.03	165.80	0.40	2.49	0.36	2.74	0		0	.
7	538.03	172.77	0.40	2.51	0.40	2.49	0		1	.
7	539.03	254.05	0.40	2.50	0.40	2.49	0		0	.
7	540.03	252.09	0.40	2.49	0.40	2.49	0		1	.
7	541.03	118.18	0.40	2.49	0.40	2.49	1	0	0	2.49
7	542.03	188.89	0.40	2.50	0.40	2.49	0		0	.
7	543.03	125.02	0.40	2.51	0.40	2.49	0		0	.
7	544.03	126.33	0.40	2.52	0.40	2.49	0		0	.
7	545.03	126.83	0.40	2.52	0.40	2.49	0		0	.
7	546.03	222.49	0.40	2.51	0.40	2.49	0		0	.
7	547.03	225.19	0.40	2.52	0.40	2.49	0		0	.
7	548.03	348.65	0.41	2.45	0.40	2.49	0		0	.
7	549.03	336.30	0.40	2.51	0.40	2.49	0		0	.
7	550.03	355.59	0.40	2.52	0.40	2.49	0		0	.
7	551.03	228.50	0.40	2.51	0.40	2.49	0		0	.
7	552.03	230.63	0.40	2.52	0.40	2.49	0		0	.
7	553.03	452.62	0.40	2.49	0.40	2.49	0		0	.
7	554.03	192.52	0.40	2.47	0.40	2.49	0		0	.
7	555.03	217.11	0.39	2.55	0.40	2.49	0		0	.
7	556.03	274.31	0.39	2.54	0.39	2.54	1	1	0	2.49
7	557.03	276.34	0.40	2.48	0.40	2.49	0		0	.
7	558.03	130.30	0.40	2.48	0.40	2.48	1	2	0	2.49
7	559.03	268.20	0.38	2.62	0.38	2.62	1	3	0	2.49
7	560.03	220.45	0.39	2.56	0.39	2.54	0		1	.
7	561.03	364.13	0.39	2.55	0.39	2.54	0		0	.
7	562.03	210.54	0.39	2.55	0.39	2.54	0		0	.
7	563.03	207.64	0.39	2.54	0.39	2.54	0		0	.
7	564.03	191.22	0.40	2.50	0.40	2.50	0		1	.
7	565.03	133.73	0.40	2.50	0.40	2.50	1	0	0	2.54
7	566.03	132.73	0.40	2.50	0.40	2.50	0		0	.
7	567.03	292.79	0.39	2.53	0.40	2.50	0		0	.
7	568.03	256.19	0.40	2.52	0.40	2.50	0		0	.
7	569.03	297.36	0.39	2.58	0.40	2.50	0		0	.
7	570.03	168.33	0.39	2.53	0.40	2.50	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	571.03	1	.	1	0	1	571	1	1.71	2	216.79
7	572.03	0	.	1	0	1	572	1	1.55	1	175.99
7	573.03	1	0	0	0	1	571	1	2.02	2	216.79
7	574.03	0	0	1	0	2	572	1	1.71	1	216.79
7	575.03	0	1	1	0	1	571	1	2.18	2	216.79
7	576.03	1	0	1	0	1	572	1	1.87	1	216.79
7	577.03	1	1	1	0	1	572	1	1.87	1	216.79
7	578.03	1	1	0	0	1	571	1	2.49	2	216.79
7	579.03	1	0	1	0	1	572	1	2.02	1	216.79
7	580.03	1	0	1	0	1	572	1	2.18	1	216.79
7	581.03	0	1	0	0	1	572	1	2.49	1	114.78
7	582.03	0	0	0	0	1	572	1	2.33	1	155.58
7	583.03	0	0	0	0	1	571	1	2.18	2	196.39
7	584.03	0	1	1	0	1	571	1	2.18	2	196.39
7	585.03	1	1	1	0	1	572	1	2.18	1	216.79
7	586.03	1	0	1	0	1	571	1	2.49	2	216.79
7	587.03	1	1	1	0	1	590	0	2.02	2	175.99
7	588.03	0	0	0	0	1	591	0	1.55	2	216.79
7	589.03	1	0	1	0	1	571	1	2.33	1	114.78
7	590.03	0	.	1	0	1	590	0	2.02	1	165.78
7	591.03	0	.	1	0	2	591	0	2.02	1	155.58
7	592.03	0	1	1	1	2	593	0	1.24	2	216.79
7	593.03	1	.	1	0	1	593	0	1.40	1	216.79
7	594.03	0	1	0	0	1	593	0	1.71	2	216.79
7	595.03	1	1	1	0	1	593	0	1.55	1	216.79
7	596.03	0	0	0	0	2	593	0	1.87	2	186.19
7	597.03	1	1	1	0	1	593	0	1.55	1	216.79
7	598.03	0	1	0	0	1	593	0	2.02	1	216.79
7	599.03	1	1	1	0	1	593	0	1.55	2	216.79
7	600.03	1	1	1	0	1	593	0	2.02	2	216.79
7	601.03	1	0	1	0	1	593	0	1.55	1	216.79
7	602.03	0	1	0	0	1	593	0	1.87	1	43.38
7	603.03	0	1	1	0	1	593	0	2.18	1	216.79
7	604.03	1	1	1	0	1	593	0	2.02	1	216.79
7	605.03	0	1	1	0	1	593	0	2.02	2	216.79
7	606.03	1	1	1	0	1	593	0	2.18	1	155.58
7	607.03	0	1	1	0	1	593	0	2.33	2	145.38
7	608.03	1	.	1	0	2	608	1	2.49	2	186.19
7	609.03	0	.	1	0	1	609	1	2.33	1	216.79
7	610.03	1	1	1	0	1	609	1	2.49	1	216.79
7	611.03	1	0	0	0	1	608	1	2.18	2	216.79
7	612.03	0	.	1	0	1	612	1	2.33	1	216.79
7	613.03	0	.	1	0	1	613	1	2.18	2	186.19
7	614.03	1	.	1	0	1	614	1	2.02	1	216.79
7	615.03	1	1	1	0	1	613	1	2.49	2	216.79
7	616.03	1	0	1	0	1	614	1	2.18	1	216.79
7	617.03	0	1	1	0	1	620	0	2.49	2	186.19
7	618.03	1	0	1	0	1	620	0	2.64	2	186.19
7	619.03	1	0	1	0	1	620	0	2.49	1	114.78
7	620.03	1	.	0	0	1	620	0	2.49	1	114.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	571.03	222.72	0.42	2.37	0.42	2.37	1	2	0	2.50
7	572.03	178.74	0.38	2.61	0.38	2.61	1	3	0	2.50
7	573.03	170.87	0.41	2.42	0.42	2.37	0		1	.
7	574.03	180.71	0.39	2.58	0.38	2.61	0		1	.
7	575.03	174.14	0.42	2.40	0.42	2.37	0		0	.
7	576.03	172.77	0.39	2.56	0.38	2.61	0		0	.
7	577.03	178.18	0.39	2.56	0.38	2.61	0		0	.
7	578.03	176.28	0.41	2.44	0.42	2.37	0		0	.
7	579.03	176.11	0.40	2.51	0.38	2.61	0		0	.
7	580.03	431.83	0.40	2.49	0.38	2.61	0		0	.
7	581.03	278.18	0.40	2.52	0.38	2.61	0		0	.
7	582.03	223.92	0.40	2.53	0.38	2.61	0		0	.
7	583.03	225.96	0.43	2.34	0.42	2.37	0		0	.
7	584.03	188.42	0.43	2.34	0.42	2.37	0		0	.
7	585.03	187.85	0.39	2.54	0.38	2.61	0		0	.
7	586.03	272.87	0.43	2.34	0.42	2.37	0		0	.
7	587.03	193.66	0.40	2.50	0.39	2.54	0		1	.
7	588.03	437.41	0.40	2.48	0.39	2.57	0		1	.
7	589.03	223.49	0.39	2.53	0.42	2.37	0		0	.
7	590.03	288.36	0.39	2.54	0.39	2.54	1	1	0	2.50
7	591.03	201.83	0.39	2.57	0.39	2.57	1	0	0	2.54
7	592.03	184.18	0.41	2.47	0.40	2.50	0		1	.
7	593.03	213.98	0.40	2.50	0.40	2.50	1	0	0	2.57
7	594.03	186.62	0.41	2.46	0.40	2.50	0		0	.
7	595.03	250.38	0.40	2.48	0.40	2.50	0		0	.
7	596.03	191.79	0.41	2.44	0.40	2.50	0		0	.
7	597.03	195.03	0.41	2.45	0.40	2.50	0		0	.
7	598.03	199.03	0.42	2.41	0.40	2.50	0		0	.
7	599.03	232.23	0.40	2.51	0.40	2.50	0		0	.
7	600.03	197.83	0.41	2.44	0.40	2.50	0		0	.
7	601.03	670.90	0.41	2.43	0.40	2.50	0		0	.
7	602.03	201.70	0.41	2.43	0.40	2.50	0		0	.
7	603.03	240.27	0.41	2.44	0.40	2.50	0		0	.
7	604.03	217.32	0.42	2.41	0.40	2.50	0		0	.
7	605.03	341.14	0.41	2.44	0.40	2.50	0		0	.
7	606.03	311.71	0.41	2.41	0.40	2.50	0		0	.
7	607.03	262.63	0.40	2.48	0.40	2.50	0		0	.
7	608.03	241.01	0.40	2.50	0.40	2.50	1	3	0	2.50
7	609.03	210.14	0.43	2.34	0.43	2.34	1	2	0	2.50
7	610.03	207.07	0.42	2.36	0.43	2.34	0		1	.
7	611.03	256.86	0.41	2.43	0.40	2.50	0		1	.
7	612.03	273.34	0.42	2.36	0.42	2.36	1	1	0	2.50
7	613.03	242.54	0.42	2.37	0.42	2.37	1	1	0	2.36
7	614.03	213.01	0.42	2.38	0.42	2.38	1	3	0	2.37
7	615.03	215.21	0.42	2.38	0.42	2.37	0		1	.
7	616.03	308.94	0.41	2.42	0.42	2.38	0		1	.
7	617.03	306.67	0.41	2.41	0.41	2.42	0		0	.
7	618.03	505.24	0.42	2.40	0.41	2.42	0		1	.
7	619.03	530.50	0.41	2.43	0.41	2.42	0		0	.
7	620.03	302.10	0.41	2.42	0.41	2.42	1	1	0	2.37

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	621.03	1	0	1	0	1	620	0	2.49	1	175.99
7	622.03	1	1	1	0	2	620	0	2.49	1	175.99
7	623.03	1	0	1	0	1	620	0	2.33	1	114.78
7	624.03	1	0	1	1	2	620	0	1.87	2	114.78
7	625.03	1	0	1	0	2	620	0	2.02	1	135.18
7	626.03	1	0	1	0	1	620	0	1.71	2	186.19
7	627.03	1	0	1	0	1	620	0	1.87	1	186.19
7	628.03	1	0	1	0	2	620	0	1.87	1	114.78
7	629.03	1	0	1	0	2	620	0	1.71	1	114.78
7	630.03	1	0	0	0	2	620	0	1.24	1	155.58
7	631.03	0	1	0	0	1	620	0	1.55	2	216.79
7	632.03	1	1	1	0	1	620	0	1.24	1	216.79
7	633.03	0	1	0	0	1	620	0	1.71	1	12.78
7	634.03	0	0	1	0	1	620	0	2.18	2	186.19
7	635.03	1	1	1	0	1	620	0	1.87	1	186.19
7	636.03	0	.	0	0	2	636	0	2.18	1	216.79
7	637.03	0	.	0	0	1	637	0	2.02	2	216.79
7	638.03	0	.	0	0	2	638	0	1.87	1	145.38
7	639.03	0	.	0	0	2	639	0	1.71	1	216.79
7	640.03	0	.	0	0	2	640	0	1.40	1	165.78
7	641.03	1	0	1	0	1	642	0	1.40	1	175.99
7	642.03	1	.	1	0	3	642	0	1.40	1	165.78
7	643.03	1	.	1	0	2	643	0	0.78	1	175.99
7	644.03	0	.	1	0	.	644	0	0.31	1	22.98
7	645.03	0	.	0	0	1	645	0	0.31	1	145.38
7	646.03	0	.	1	0	.	646	0	0.62	2	145.38
7	647.03	0	.	0	0	3	647	0	0.93	2	206.59
7	648.03	0	.	1	0	2	648	0	0.78	2	196.39
7	649.03	0	.	0	0	.	649	0	0.31	2	196.39
7	650.03	0	.	0	0	2	650	0	0.62	1	145.38
7	651.03	0	.	0	0	.	651	0	0.31	1	175.99
7	652.03	1	.	1	0	.	652	0	0.31	1	33.18
7	653.03	1	0	1	0	2	652	0	0.62	1	33.18
7	654.03	0	1	0	0	2	652	0	0.93	1	33.18
7	655.03	0	.	1	0	.	655	0	0.78	1	84.18
7	656.03	0	.	1	0	.	656	0	0.31	2	145.38
7	657.03	0	.	1	0	.	657	0	0.31	1	196.39
7	658.03	1	.	1	0	.	658	0	0.31	0	114.78
7	659.03	0	.	1	0	.	659	0	0.62	0	206.59
7	661.03	0	.	0	0	.	661	0	0.31	1	196.39
7	662.03	0	0	0	0	1	661	0	0.62	2	196.39
7	663.03	1	.	1	0	.	663	0	0.31	1	206.59
7	664.03	1	.	1	0	.	664	0	0.31	1	216.79
7	25.04	1	.	0	0	.	25	0	0.47	2	12.78
7	36.04	0	.	1	0	3	36	0	0.93	1	2.58
7	37.04	0	.	0	0	.	37	0	0.47	1	2.58
7	47.04	1	.	1	0	2	47	0	0.93	0	2.58
7	48.04	0	1	0	1	2	47	0	1.09	1	2.58
7	58.04	1	1	1	0	2	47	0	1.24	0	2.58
7	61.04	0	.	0	0	2	61	0	1.24	1	12.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	621.03	302.00	0.41	2.43	0.41	2.42	0		0	.
7	622.03	496.47	0.41	2.44	0.41	2.42	0		0	.
7	623.03	498.27	0.41	2.45	0.41	2.42	0		0	.
7	624.03	501.80	0.40	2.48	0.41	2.42	0		0	.
7	625.03	313.38	0.40	2.48	0.41	2.42	0		0	.
7	626.03	311.14	0.40	2.50	0.41	2.42	0		0	.
7	627.03	509.04	0.40	2.50	0.41	2.42	0		0	.
7	628.03	529.46	0.40	2.49	0.41	2.42	0		0	.
7	629.03	353.25	0.40	2.52	0.41	2.42	0		0	.
7	630.03	273.81	0.40	2.51	0.41	2.42	0		0	.
7	631.03	272.34	0.40	2.53	0.41	2.42	0		0	.
7	632.03	818.55	0.40	2.52	0.41	2.42	0		0	.
7	633.03	271.07	0.40	2.52	0.41	2.42	0		0	.
7	634.03	323.92	0.40	2.49	0.41	2.42	0		0	.
7	635.03	306.07	0.40	2.50	0.41	2.42	0		0	.
7	636.03	307.37	0.40	2.51	0.40	2.51	1	0	0	2.42
7	637.03	415.95	0.39	2.56	0.39	2.56	1	0	0	2.51
7	638.03	460.16	0.39	2.54	0.39	2.54	1	1	0	2.56
7	639.03	430.26	0.41	2.43	0.41	2.43	1	1	0	2.54
7	640.03	343.64	0.41	2.47	0.41	2.47	1	0	0	2.43
7	641.03	422.65	0.43	2.34	0.43	2.32	0		1	.
7	642.03	594.89	0.43	2.32	0.43	2.32	1	0	0	2.47
7	643.03	883.41	0.47	2.13	0.47	2.13	1	1	0	2.32
7	644.03	592.63	0.92	1.09	0.92	1.09	1	0	0	2.13
7	645.03	595.33	0.52	1.93	0.52	1.93	1	3	0	2.13
7	646.03	651.72	0.52	1.92	0.52	1.92	1	3	0	2.13
7	647.03	697.19	0.70	1.43	0.70	1.43	1	2	0	2.13
7	648.03	694.93	0.86	1.17	0.86	1.17	1	0	0	1.12
7	649.03	102.77	0.92	1.09	0.92	1.09	1	0	0	1.09
7	650.03	531.93	0.89	1.12	0.89	1.12	1	0	0	1.09
7	651.03	933.76	0.84	1.18	0.84	1.18	1	0	0	1.17
7	652.03	935.10	0.64	1.57	0.64	1.57	1	0	0	1.18
7	653.03	936.30	0.63	1.58	0.64	1.57	0		1	.
7	654.03	822.75	0.63	1.58	0.64	1.57	0		0	.
7	655.03	721.59	0.65	1.55	0.65	1.55	1	0	0	1.57
7	656.03	770.43	1.28	0.78	1.28	0.78	1	0	0	1.79
7	657.03	1072.34	0.56	1.79	0.56	1.79	1	0	0	1.55
7	658.03	979.98	0.89	1.13	0.89	1.13	1	0	0	0.78
7	659.03	1252.95	0.85	1.18	0.85	1.18	1	0	0	1.13
7	661.03	1010.74	0.68	1.46	0.68	1.46	1	0	0	1.18
7	662.03	1222.05	0.68	1.48	0.68	1.46	0		1	.
7	663.03	1049.52	0.86	1.16	0.86	1.16	1	0	0	1.46
7	664.03	142.65	0.89	1.13	0.89	1.13	1	0	0	1.16
7	25.04	46.68	0.92	1.09	0.92	1.09	1	0	0	.
7	36.04	65.30	1.12	0.89	1.12	0.89	1	0	0	0.89
7	37.04	64.19	1.12	0.89	1.12	0.89	1	0	0	1.09
7	47.04	67.60	0.88	1.14	0.88	1.14	1	0	0	0.89
7	48.04	145.48	0.87	1.15	0.88	1.14	0		1	.
7	58.04	93.96	0.87	1.15	0.88	1.14	0		0	.
7	61.04	130.93	0.80	1.26	0.80	1.26	1	1	0	1.14

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	63.04	1	.	1	0	2	63	0	0.93	1	12.78
7	65.04	1	.	1	0	1	65	0	0.78	2	12.78
7	67.04	1	.	1	0	.	67	0	0.78	0	12.78
7	68.04	1	1	1	0	2	69	0	1.09	2	12.78
7	69.04	0	.	0	0	2	69	0	0.78	1	12.78
7	70.04	1	0	1	0	1	69	0	0.93	0	12.78
7	71.04	1	0	1	0	1	69	0	0.93	0	12.78
7	72.04	1	.	1	0	1	72	0	0.62	0	12.78
7	77.04	1	0	0	0	1	78	0	0.93	0	12.78
7	78.04	1	.	1	0	1	78	0	0.78	0	12.78
7	90.04	1	.	1	0	2	90	0	1.09	2	12.78
7	91.04	1	.	1	0	.	91	0	0.78	1	12.78
7	92.04	1	.	0	0	1	92	1	1.24	0	12.78
7	93.04	1	0	0	0	1	95	1	1.87	2	63.78
7	94.04	1	1	1	0	1	95	1	2.18	2	33.18
7	95.04	0	.	0	0	1	95	1	1.71	2	63.78
7	96.04	1	0	0	0	1	98	1	1.55	0	12.78
7	97.04	0	.	0	0	1	97	0	2.02	1	12.78
7	98.04	1	.	1	0	1	98	1	1.40	1	12.78
7	107.04	1	.	1	0	1	107	0	1.71	2	33.18
7	109.04	0	.	0	0	1	109	0	1.55	0	2.58
7	116.04	0	1	1	0	1	117	1	1.40	1	12.78
7	117.04	1	.	1	0	1	117	1	1.09	1	12.78
7	119.04	0	0	0	0	1	130	0	1.87	1	12.78
7	127.04	1	.	0	0	1	127	0	2.18	1	12.78
7	130.04	1	.	1	0	1	130	0	2.33	1	22.98
7	133.04	0	1	0	0	1	130	0	2.18	1	22.98
7	134.04	0	1	0	0	2	151	0	1.87	1	12.78
7	140.04	1	.	1	0	1	140	0	1.71	1	12.78
7	141.04	1	.	1	0	3	141	0	1.55	1	12.78
7	151.04	1	.	1	0	1	151	0	2.02	1	2.58
7	152.04	1	1	1	0	1	151	0	1.87	1	12.78
7	153.04	0	1	0	0	2	151	0	1.55	1	12.78
7	154.04	1	1	1	0	2	151	0	1.71	1	12.78
7	157.04	0	.	0	0	1	157	1	1.87	2	12.78
7	158.04	0	.	0	0	1	158	1	1.71	1	12.78
7	159.04	0	0	0	0	1	158	1	1.71	1	12.78
7	160.04	1	1	0	0	1	157	1	2.18	2	22.98
7	161.04	1	1	1	0	1	158	1	2.02	1	12.78
7	162.04	1	0	1	0	1	157	1	2.33	2	53.58
7	163.04	1	0	1	0	1	157	1	2.18	2	53.58
7	164.04	1	.	1	0	1	164	1	2.49	1	12.78
7	165.04	1	0	1	0	1	158	1	2.02	1	12.78
7	167.04	1	0	1	0	1	180	0	2.18	2	12.78
7	169.04	1	.	1	0	1	169	0	2.02	2	53.58
7	171.04	1	.	1	0	1	171	0	2.02	2	53.58
7	173.04	0	0	1	1	1	186	0	2.02	2	53.58
7	175.04	1	0	1	0	1	186	0	2.33	2	12.78
7	176.04	1	1	1	0	1	186	0	2.33	1	12.78
7	180.04	1	.	1	0	1	180	0	2.33	1	12.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	63.04	100.03	0.70	1.43	0.70	1.43	1	1	0	1.26
7	65.04	172.41	0.77	1.29	0.77	1.29	1	1	0	1.43
7	67.04	78.78	0.68	1.47	0.68	1.47	1	0	0	1.29
7	68.04	76.57	0.70	1.42	0.68	1.47	0		1	.
7	69.04	79.94	0.68	1.47	0.68	1.47	1	1	0	1.47
7	70.04	81.64	0.68	1.47	0.68	1.47	0		0	.
7	71.04	87.15	0.68	1.47	0.68	1.47	0		0	.
7	72.04	115.22	0.68	1.46	0.68	1.46	1	1	0	1.47
7	77.04	91.09	0.73	1.37	0.71	1.41	0		1	.
7	78.04	150.91	0.71	1.41	0.71	1.41	1	1	0	1.46
7	90.04	93.59	0.65	1.53	0.65	1.53	1	0	0	1.52
7	91.04	97.19	0.66	1.52	0.66	1.52	1	0	0	1.41
7	92.04	54.42	0.64	1.56	0.64	1.56	1	3	0	1.53
7	93.04	84.08	0.71	1.41	0.71	1.41	0		0	.
7	94.04	40.00	0.72	1.40	0.71	1.41	0		1	.
7	95.04	100.43	0.71	1.41	0.71	1.41	1	3	0	1.53
7	96.04	104.13	0.60	1.68	0.57	1.75	0		0	.
7	97.04	99.36	0.64	1.55	0.64	1.55	1	4	0	1.53
7	98.04	167.50	0.57	1.75	0.57	1.75	1	3	0	1.53
7	107.04	216.75	0.77	1.30	0.77	1.30	1	2	0	1.55
7	109.04	137.30	0.73	1.37	0.73	1.37	1	2	0	1.55
7	116.04	101.60	0.76	1.31	0.79	1.26	0		1	.
7	117.04	142.01	0.79	1.26	0.79	1.26	1	2	0	1.53
7	119.04	230.57	0.56	1.79	0.55	1.83	0		0	.
7	127.04	189.08	0.57	1.76	0.57	1.76	1	3	0	1.55
7	130.04	196.49	0.55	1.83	0.55	1.83	1	3	0	1.55
7	133.04	116.21	0.55	1.82	0.55	1.83	0		1	.
7	134.04	247.95	0.46	2.15	0.47	2.13	0		1	.
7	140.04	111.24	0.54	1.86	0.54	1.86	1	1	0	1.87
7	141.04	150.02	0.54	1.87	0.54	1.87	1	0	0	1.55
7	151.04	118.21	0.47	2.13	0.47	2.13	1	4	0	1.86
7	152.04	120.52	0.46	2.16	0.47	2.13	0		0	.
7	153.04	121.82	0.46	2.17	0.47	2.13	0		0	.
7	154.04	220.05	0.46	2.19	0.47	2.13	0		0	.
7	157.04	123.29	0.48	2.07	0.48	2.07	1	2	0	2.13
7	158.04	124.22	0.46	2.19	0.46	2.19	1	3	0	2.13
7	159.04	98.40	0.46	2.19	0.46	2.19	0		1	.
7	160.04	127.39	0.47	2.14	0.48	2.07	0		1	.
7	161.04	79.11	0.46	2.18	0.46	2.19	0		0	.
7	162.04	76.41	0.46	2.18	0.48	2.07	0		0	.
7	163.04	131.69	0.46	2.16	0.48	2.07	0		0	.
7	164.04	129.39	0.44	2.29	0.44	2.29	1	3	0	2.13
7	165.04	229.29	0.46	2.19	0.46	2.19	0		0	.
7	167.04	231.56	0.40	2.52	0.40	2.52	0		1	.
7	169.04	314.04	0.40	2.53	0.40	2.53	1	2	0	2.52
7	171.04	289.33	0.39	2.59	0.39	2.59	1	1	0	2.52
7	173.04	291.56	0.38	2.62	0.39	2.59	0		1	.
7	175.04	144.04	0.38	2.63	0.39	2.59	0		0	.
7	176.04	174.58	0.38	2.61	0.39	2.59	0		0	.
7	180.04	150.65	0.40	2.52	0.40	2.52	1	4	0	2.13

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	181.04	0	.	0	0	1	181	1	1.87	2	12.78
7	182.04	0	0	0	0	1	181	1	2.18	2	22.98
7	183.04	1	0	1	0	1	180	0	2.18	1	12.78
7	184.04	1	.	1	0	1	184	0	2.33	1	12.78
7	186.04	0	.	1	0	1	186	0	1.87	1	2.58
7	187.04	0	1	0	0	1	199	1	1.87	1	2.58
7	188.04	1	1	1	0	1	181	1	2.18	2	22.98
7	193.04	1	.	1	0	1	193	1	1.87	0	33.18
7	194.04	0	1	1	1	1	181	1	1.71	2	33.18
7	195.04	1	0	1	0	2	202	1	1.71	1	12.78
7	196.04	1	0	1	0	1	186	0	2.18	1	12.78
7	197.04	1	0	1	0	2	186	0	2.18	1	12.78
7	199.04	1	.	0	0	1	199	1	1.87	1	12.78
7	200.04	0	0	0	0	1	199	1	2.02	1	63.78
7	201.04	0	0	1	0	1	199	1	2.02	1	63.78
7	202.04	1	.	0	0	1	202	1	1.87	1	22.98
7	203.04	1	0	0	0	1	202	1	2.02	1	22.98
7	204.04	1	.	1	0	2	204	0	1.87	1	33.18
7	205.04	1	0	1	0	2	204	0	1.71	1	12.78
7	208.04	1	1	1	0	1	204	0	1.55	0	33.18
7	209.04	0	1	1	0	2	204	0	1.55	1	33.18
7	211.04	0	1	0	0	1	204	0	1.55	1	12.78
7	212.04	1	0	1	0	1	204	0	1.87	2	53.58
7	213.04	1	1	1	0	1	204	0	1.71	1	53.58
7	216.04	0	1	1	0	1	204	0	1.87	2	12.78
7	217.04	1	0	1	0	1	204	0	1.87	1	12.78
7	220.04	0	.	1	0	1	220	1	2.49	2	53.58
7	221.04	0	0	0	0	1	220	1	2.49	2	84.18
7	222.04	1	0	1	0	1	230	0	2.64	2	33.18
7	224.04	1	.	1	0	1	224	1	2.18	1	12.78
7	225.04	0	.	1	0	1	225	1	2.49	2	43.38
7	226.04	1	0	1	0	1	224	1	2.18	1	53.58
7	227.04	1	1	1	0	1	225	1	2.02	2	33.18
7	228.04	1	0	0	0	1	224	1	2.33	1	12.78
7	229.04	1	0	1	0	1	230	0	2.33	1	33.18
7	230.04	1	.	0	0	1	230	0	2.49	1	12.78
7	231.04	1	0	1	0	1	236	0	2.33	2	12.78
7	232.04	0	.	0	0	1	232	1	2.49	1	12.78
7	233.04	1	1	1	0	1	232	1	2.49	1	12.78
7	234.04	1	0	1	0	1	236	0	2.49	1	2.58
7	235.04	1	0	1	0	1	236	0	2.33	1	2.58
7	236.04	1	.	1	1	1	236	0	2.18	1	2.58
7	241.04	0	.	0	0	1	241	1	2.49	2	33.18
7	242.04	1	1	1	0	1	241	1	2.64	2	84.18
7	243.04	0	1	0	0	1	241	1	2.64	2	84.18
7	244.04	0	0	1	0	1	251	0	2.80	2	84.18
7	245.04	1	1	1	0	1	251	0	2.64	2	33.18
7	246.04	1	.	1	0	1	246	1	2.33	1	33.18
7	247.04	1	0	1	0	1	246	1	2.49	1	33.18
7	248.04	0	.	0	0	1	248	0	2.80	2	22.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	181.04	114.85	0.39	2.54	0.39	2.54	1	2	0	2.59
7	182.04	136.17	0.39	2.54	0.39	2.54	0		1	.
7	183.04	137.03	0.38	2.61	0.40	2.52	0		0	.
7	184.04	185.72	0.38	2.64	0.38	2.64	1	3	0	2.52
7	186.04	151.85	0.39	2.59	0.39	2.59	1	4	0	2.59
7	187.04	125.66	0.37	2.67	0.37	2.67	0		1	.
7	188.04	304.97	0.40	2.52	0.39	2.54	0		0	.
7	193.04	129.19	0.41	2.45	0.41	2.45	1	2	0	2.59
7	194.04	162.19	0.43	2.34	0.39	2.54	0		0	.
7	195.04	147.74	0.36	2.77	0.36	2.76	0		0	.
7	196.04	146.61	0.38	2.63	0.39	2.59	0		0	.
7	197.04	274.17	0.39	2.59	0.39	2.59	0		0	.
7	199.04	58.09	0.37	2.67	0.37	2.67	1	3	0	2.59
7	200.04	57.02	0.37	2.74	0.37	2.67	0		0	.
7	201.04	121.89	0.36	2.76	0.37	2.67	0		0	.
7	202.04	123.09	0.36	2.76	0.36	2.76	1	3	0	2.59
7	203.04	132.13	0.36	2.75	0.36	2.76	0		1	.
7	204.04	169.07	0.38	2.66	0.38	2.66	1	1	0	2.59
7	205.04	337.27	0.38	2.66	0.38	2.66	0		1	.
7	208.04	133.33	0.37	2.69	0.38	2.66	0		0	.
7	209.04	286.48	0.37	2.69	0.38	2.66	0		0	.
7	211.04	97.43	0.37	2.71	0.38	2.66	0		0	.
7	212.04	95.69	0.36	2.76	0.38	2.66	0		0	.
7	213.04	295.72	0.37	2.74	0.38	2.66	0		0	.
7	216.04	176.77	0.36	2.79	0.38	2.66	0		0	.
7	217.04	235.14	0.36	2.75	0.38	2.66	0		0	.
7	220.04	66.84	0.35	2.82	0.35	2.82	1	2	0	2.66
7	221.04	141.71	0.35	2.86	0.35	2.82	0		1	.
7	222.04	302.90	0.34	2.94	0.34	2.95	0		1	.
7	224.04	107.97	0.34	2.92	0.34	2.92	1	3	0	2.66
7	225.04	104.14	0.34	2.92	0.34	2.92	1	2	0	2.95
7	226.04	149.85	0.34	2.92	0.34	2.92	0		1	.
7	227.04	182.35	0.34	2.93	0.34	2.92	0		1	.
7	228.04	143.51	0.34	2.95	0.34	2.92	0		0	.
7	229.04	183.98	0.33	2.99	0.34	2.95	0		0	.
7	230.04	194.36	0.34	2.95	0.34	2.95	1	1	0	2.66
7	231.04	187.82	0.33	3.00	0.34	2.98	0		0	.
7	232.04	189.49	0.33	3.01	0.33	3.01	1	3	0	2.95
7	233.04	196.86	0.33	3.03	0.33	3.01	0		1	.
7	234.04	195.19	0.33	3.05	0.34	2.98	0		0	.
7	235.04	193.19	0.33	3.00	0.34	2.98	0		1	.
7	236.04	374.88	0.34	2.98	0.34	2.98	1	1	0	2.95
7	241.04	70.87	0.33	3.03	0.33	3.03	1	2	0	2.98
7	242.04	71.81	0.33	3.04	0.33	3.03	0		1	.
7	243.04	76.04	0.31	3.22	0.33	3.03	0		0	.
7	244.04	166.00	0.30	3.37	0.29	3.43	0		1	.
7	245.04	145.48	0.29	3.47	0.29	3.43	0		0	.
7	246.04	155.32	0.32	3.11	0.32	3.11	1	3	0	2.98
7	247.04	168.47	0.31	3.21	0.32	3.11	0		1	.
7	248.04	158.29	0.29	3.39	0.29	3.39	1	2	0	3.43

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	249.04	1	0	1	0	1	246	1	2.49	1	33.18
7	250.04	0	.	1	0	1	250	0	2.80	0	33.18
7	251.04	0	.	0	0	1	251	0	2.64	1	12.78
7	252.04	0	1	1	0	1	251	0	2.49	1	124.98
7	253.04	1	.	1	0	1	253	0	2.80	1	12.78
7	254.04	1	1	1	0	1	251	0	2.64	1	22.98
7	255.04	0	1	0	0	1	251	0	2.64	1	124.98
7	256.04	1	0	1	0	1	250	0	2.33	2	33.18
7	257.04	1	1	1	0	1	250	0	2.64	1	12.78
7	258.04	1	0	1	0	1	250	0	2.18	1	33.18
7	259.04	0	1	1	0	1	250	0	2.64	2	12.78
7	260.04	0	1	1	0	1	250	0	2.18	2	33.18
7	261.04	1	1	1	0	1	250	0	2.33	2	33.18
7	262.04	1	1	1	0	1	250	0	2.33	1	22.98
7	263.04	0	0	0	1	1	250	0	2.33	1	12.78
7	264.04	0	1	0	0	1	250	0	2.33	2	33.18
7	265.04	1	0	1	0	1	250	0	2.02	1	33.18
7	266.04	1	0	1	0	1	250	0	2.18	2	33.18
7	267.04	1	1	1	0	1	250	0	2.02	1	33.18
7	268.04	1	.	1	0	1	268	0	1.87	0	33.18
7	270.04	0	0	0	0	1	273	0	2.33	2	73.98
7	272.04	0	.	1	0	1	272	0	2.33	1	12.78
7	273.04	0	.	1	0	1	273	0	2.33	2	94.38
7	276.04	1	1	1	0	1	273	0	2.33	2	63.78
7	277.04	1	1	0	0	1	273	0	2.49	2	63.78
7	278.04	0	0	1	0	1	273	0	2.02	1	94.38
7	279.04	0	0	0	0	1	273	0	2.49	1	12.78
7	280.04	0	0	1	0	1	273	0	2.18	1	84.18
7	281.04	0	.	0	0	1	281	0	2.18	1	12.78
7	282.04	0	1	0	0	1	273	0	2.49	2	63.78
7	283.04	0	1	1	0	1	273	0	1.87	2	33.18
7	284.04	0	1	1	0	1	273	0	2.18	2	33.18
7	285.04	0	1	0	0	1	273	0	2.64	1	94.38
7	286.04	1	0	1	0	1	273	0	2.64	1	12.78
7	287.04	1	0	1	0	1	273	0	2.64	1	94.38
7	288.04	1	0	1	0	1	295	1	2.33	1	73.98
7	289.04	1	.	1	0	1	289	1	2.18	0	12.78
7	290.04	1	0	1	0	1	273	0	2.49	1	33.18
7	292.04	1	1	1	0	1	295	1	2.02	1	12.78
7	293.04	1	1	1	0	1	273	0	2.33	1	33.18
7	294.04	1	1	1	0	1	273	0	2.49	1	33.18
7	295.04	1	.	1	0	1	295	1	2.33	1	33.18
7	296.04	0	1	1	0	1	295	1	2.18	1	53.58
7	297.04	1	0	0	0	1	295	1	2.18	1	22.98
7	298.04	0	0	0	1	1	343	1	2.33	2	94.38
7	299.04	0	.	1	0	1	295	1	2.02	1	73.98
7	300.04	1	0	0	0	1	295	1	2.18	1	63.78
7	301.04	0	0	1	0	1	343	1	2.33	2	94.38
7	302.04	0	.	1	0	1	302	0	1.87	2	94.38
7	303.04	1	1	1	0	1	273	0	2.49	1	33.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	249.04	164.66	0.30	3.31	0.32	3.11	0		0	.
7	250.04	201.80	0.29	3.48	0.29	3.48	1	1	0	3.43
7	251.04	39.07	0.29	3.43	0.29	3.43	1	1	0	2.98
7	252.04	209.27	0.29	3.44	0.29	3.43	0		0	.
7	253.04	160.72	0.29	3.45	0.29	3.45	1	3	0	3.43
7	254.04	39.91	0.29	3.41	0.29	3.43	0		0	.
7	255.04	165.36	0.29	3.44	0.29	3.43	0		0	.
7	256.04	213.31	0.28	3.51	0.29	3.48	0		0	.
7	257.04	166.43	0.29	3.43	0.29	3.48	0		1	.
7	258.04	218.98	0.29	3.47	0.29	3.48	0		0	.
7	259.04	172.54	0.28	3.53	0.29	3.48	0		0	.
7	260.04	176.27	0.28	3.60	0.29	3.48	0		0	.
7	261.04	170.13	0.28	3.61	0.29	3.48	0		0	.
7	262.04	221.78	0.28	3.53	0.29	3.48	0		0	.
7	263.04	175.21	0.28	3.58	0.29	3.48	0		0	.
7	264.04	169.07	0.28	3.60	0.29	3.48	0		0	.
7	265.04	173.54	0.28	3.58	0.29	3.48	0		0	.
7	266.04	171.44	0.28	3.57	0.29	3.48	0		0	.
7	267.04	174.67	0.28	3.58	0.29	3.48	0		0	.
7	268.04	304.30	0.28	3.52	0.28	3.52	1	2	0	3.48
7	270.04	423.06	0.27	3.72	0.27	3.75	0		0	.
7	272.04	79.75	0.27	3.77	0.27	3.77	1	3	0	3.48
7	273.04	309.54	0.27	3.75	0.27	3.75	1	1	0	3.48
7	276.04	118.85	0.26	3.83	0.27	3.75	0		0	.
7	277.04	83.52	0.26	3.84	0.27	3.75	0		0	.
7	278.04	236.83	0.26	3.78	0.27	3.75	0		1	.
7	279.04	92.16	0.26	3.78	0.27	3.75	0		0	.
7	280.04	229.26	0.27	3.77	0.27	3.75	0		0	.
7	281.04	120.55	0.25	4.05	0.25	4.05	1	3	0	3.48
7	282.04	195.63	0.26	3.85	0.27	3.75	0		0	.
7	283.04	196.86	0.27	3.76	0.27	3.75	0		0	.
7	284.04	88.66	0.27	3.76	0.27	3.75	0		0	.
7	285.04	244.24	0.27	3.77	0.27	3.75	0		0	.
7	286.04	90.19	0.27	3.76	0.27	3.75	0		0	.
7	287.04	122.25	0.27	3.76	0.27	3.75	0		0	.
7	288.04	264.36	0.28	3.56	0.28	3.61	0		1	.
7	289.04	189.79	0.32	3.14	0.32	3.14	1	2	0	3.75
7	290.04	352.55	0.27	3.73	0.27	3.75	0		0	.
7	292.04	195.56	0.29	3.43	0.28	3.61	0		0	.
7	293.04	192.86	0.28	3.61	0.27	3.75	0		0	.
7	294.04	202.27	0.27	3.70	0.27	3.75	0		0	.
7	295.04	154.99	0.28	3.61	0.28	3.61	1	3	0	3.75
7	296.04	208.61	0.28	3.53	0.28	3.61	0		0	.
7	297.04	93.93	0.29	3.51	0.28	3.61	0		0	.
7	298.04	123.79	0.24	4.14	0.25	3.99	0		0	.
7	299.04	124.69	0.29	3.41	0.28	3.61	1	0	0	.
7	300.04	92.16	0.29	3.45	0.28	3.61	0		0	.
7	301.04	94.56	0.25	4.06	0.25	3.99	0		0	.
7	302.04	188.42	0.26	3.84	0.26	3.84	1	1	0	3.75
7	303.04	216.55	0.27	3.76	0.27	3.75	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	304.04	1	0	1	0	1	302	0	2.49	2	33.18
7	305.04	1	1	1	0	1	302	0	2.02	1	33.18
7	306.04	1	0	1	0	1	302	0	2.49	2	84.18
7	307.04	1	0	1	0	1	302	0	2.95	2	84.18
7	308.04	1	.	1	0	1	308	1	2.95	2	94.38
7	309.04	1	0	1	0	1	308	1	2.80	2	94.38
7	310.04	1	0	1	0	1	308	1	2.80	2	84.18
7	312.04	1	0	1	0	1	302	0	2.49	1	22.98
7	313.04	1	0	1	0	1	302	0	2.33	1	33.18
7	314.04	1	0	1	0	1	308	1	2.64	2	33.18
7	315.04	1	0	1	0	1	308	1	2.80	2	94.38
7	316.04	1	0	1	0	1	308	1	2.80	2	33.18
7	317.04	1	0	1	0	1	302	0	2.64	1	33.18
7	318.04	1	0	1	0	1	308	1	2.49	2	94.38
7	319.04	1	0	1	0	1	308	1	3.11	2	94.38
7	320.04	1	.	1	0	1	320	1	2.64	1	73.98
7	321.04	1	0	0	1	1	308	1	2.64	2	84.18
7	322.04	1	1	1	0	1	320	1	2.80	1	33.18
7	323.04	1	0	1	0	1	320	1	2.95	1	94.38
7	324.04	1	.	1	0	1	324	1	2.80	2	84.18
7	325.04	0	1	0	0	1	324	1	2.64	2	84.18
7	326.04	1	1	1	0	1	324	1	2.49	2	94.38
7	327.04	0	0	0	0	1	320	1	2.64	1	12.78
7	328.04	0	1	0	0	1	320	1	2.49	1	84.18
7	329.04	0	1	0	0	1	324	1	2.80	2	94.38
7	330.04	0	0	0	1	1	324	1	2.95	2	94.38
7	331.04	1	1	1	0	1	324	1	2.95	2	94.38
7	332.04	0	1	0	1	1	324	1	3.11	2	94.38
7	334.04	0	1	1	0	1	320	1	2.49	1	33.18
7	335.04	1	1	1	0	1	324	1	2.95	2	84.18
7	336.04	0	0	1	0	1	320	1	2.80	1	73.98
7	337.04	0	1	0	0	1	320	1	2.95	1	73.98
7	338.04	1	1	0	0	1	320	1	2.49	1	84.18
7	339.04	1	.	1	0	1	339	1	2.95	1	94.38
7	340.04	1	1	1	0	1	320	1	3.11	1	94.38
7	341.04	1	0	1	0	1	324	1	3.26	2	94.38
7	342.04	1	0	1	0	1	324	1	2.95	2	84.18
7	343.04	1	.	1	0	1	343	1	2.18	2	63.78
7	344.04	0	.	1	0	1	343	1	2.02	2	63.78
7	345.04	1	0	1	1	1	324	1	2.80	2	94.38
7	346.04	1	.	1	0	1	346	1	2.95	1	33.18
7	347.04	0	1	0	0	1	324	1	2.64	2	94.38
7	348.04	0	1	0	0	1	346	1	2.80	1	12.78
7	349.04	1	0	1	0	1	324	1	2.80	2	94.38
7	350.04	1	1	1	0	1	346	1	2.64	1	33.18
7	351.04	0	1	1	0	1	324	1	2.80	2	84.18
7	352.04	1	0	1	0	1	346	1	2.80	1	94.38
7	353.04	0	0	1	0	1	324	1	2.64	2	124.98
7	354.04	0	1	0	0	1	346	1	2.49	1	33.18
7	355.04	0	0	1	0	1	324	1	2.95	2	114.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	304.04	215.21	0.26	3.78	0.26	3.84	0		0	.
7	305.04	100.64	0.27	3.74	0.26	3.84	0		1	.
7	306.04	97.13	0.26	3.79	0.26	3.84	0		0	.
7	307.04	102.00	0.27	3.76	0.26	3.84	0		0	.
7	308.04	102.94	0.26	3.78	0.26	3.78	1	2	0	3.84
7	309.04	103.57	0.26	3.85	0.26	3.78	0		1	.
7	310.04	402.73	0.28	3.59	0.26	3.78	0		0	.
7	312.04	212.31	0.27	3.75	0.26	3.84	0		0	.
7	313.04	237.23	0.26	3.81	0.26	3.84	0		0	.
7	314.04	108.44	0.26	3.82	0.26	3.78	0		0	.
7	315.04	242.74	0.26	3.79	0.26	3.78	0		0	.
7	316.04	215.41	0.27	3.75	0.26	3.78	0		0	.
7	317.04	110.61	0.27	3.75	0.26	3.84	0		0	.
7	318.04	111.91	0.27	3.76	0.26	3.78	0		0	.
7	319.04	130.26	0.27	3.68	0.26	3.78	0		0	.
7	320.04	116.75	0.25	3.92	0.25	3.92	1	3	0	3.84
7	321.04	231.20	0.28	3.56	0.26	3.78	0		0	.
7	322.04	96.73	0.25	4.00	0.25	3.92	0		0	.
7	323.04	111.45	0.25	3.94	0.25	3.92	0		1	.
7	324.04	113.08	0.28	3.63	0.28	3.63	1	2	0	3.83
7	325.04	115.88	0.28	3.61	0.28	3.63	0		1	.
7	326.04	306.54	0.29	3.47	0.28	3.63	0		0	.
7	327.04	105.17	0.25	4.03	0.25	3.92	0		0	.
7	328.04	124.43	0.24	4.08	0.25	3.92	0		0	.
7	329.04	125.89	0.29	3.48	0.28	3.63	0		0	.
7	330.04	129.10	0.29	3.50	0.28	3.63	0		0	.
7	331.04	131.00	0.29	3.49	0.28	3.63	0		0	.
7	332.04	360.16	0.28	3.53	0.28	3.63	0		0	.
7	334.04	132.83	0.25	3.93	0.25	3.92	0		0	.
7	335.04	131.99	0.28	3.59	0.28	3.63	0		0	.
7	336.04	133.36	0.25	3.94	0.25	3.92	0		0	.
7	337.04	98.23	0.25	4.02	0.25	3.92	0		0	.
7	338.04	110.18	0.24	4.15	0.25	3.92	0		0	.
7	339.04	104.31	0.26	3.83	0.26	3.83	1	1	0	3.84
7	340.04	122.46	0.25	4.05	0.25	3.92	0		0	.
7	341.04	129.33	0.28	3.59	0.28	3.63	0		0	.
7	342.04	81.31	0.28	3.63	0.28	3.63	0		0	.
7	343.04	76.81	0.25	3.99	0.25	3.99	1	3	0	3.75
7	344.04	132.13	0.24	4.10	0.25	3.99	1	0	1	.
7	345.04	243.87	0.28	3.63	0.28	3.63	0		0	.
7	346.04	135.04	0.24	4.10	0.24	4.10	1	3	0	3.83
7	347.04	315.48	0.28	3.62	0.28	3.63	0		0	.
7	348.04	133.24	0.25	4.07	0.24	4.10	0		1	.
7	349.04	248.51	0.28	3.55	0.28	3.63	0		0	.
7	350.04	125.03	0.25	4.02	0.24	4.10	0		0	.
7	351.04	106.61	0.29	3.50	0.28	3.63	0		0	.
7	352.04	62.80	0.25	4.00	0.24	4.10	0		0	.
7	353.04	251.82	0.29	3.50	0.28	3.63	0		0	.
7	354.04	101.67	0.25	4.02	0.24	4.10	0		0	.
7	355.04	184.61	0.29	3.46	0.28	3.63	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	356.04	0	0	1	0	1	324	1	2.95	2	63.78
7	357.04	1	1	1	0	1	346	1	2.80	1	12.78
7	358.04	0	0	0	0	1	324	1	2.95	2	124.98
7	359.04	1	0	0	0	1	346	1	2.80	1	12.78
7	360.04	1	0	1	0	1	346	1	2.33	1	12.78
7	361.04	1	1	1	1	1	346	1	2.95	1	84.18
7	362.04	0	1	0	0	1	346	1	2.80	1	33.18
7	363.04	0	1	1	0	1	346	1	3.11	1	84.18
7	364.04	1	1	1	0	1	346	1	2.95	1	12.78
7	365.04	1	1	1	0	1	346	1	3.11	1	22.98
7	366.04	1	0	1	0	1	346	1	2.49	1	84.18
7	367.04	1	0	1	0	1	346	1	2.95	1	22.98
7	368.04	1	0	1	0	1	346	1	2.95	1	22.98
7	369.04	1	0	1	0	1	346	1	3.26	1	33.18
7	370.04	0	1	0	0	1	346	1	3.26	1	84.18
7	371.04	1	0	1	0	1	346	1	2.80	1	33.18
7	372.04	1	.	1	0	1	372	1	2.33	2	94.38
7	373.04	0	0	0	0	1	346	1	3.26	1	94.38
7	374.04	1	1	1	0	1	346	1	3.11	1	33.18
7	375.04	0	1	0	0	1	346	1	3.11	1	94.38
7	376.04	1	1	1	0	1	346	1	2.95	1	33.18
7	377.04	1	0	1	0	1	346	1	2.95	1	33.18
7	378.04	1	0	1	0	1	379	0	2.64	1	84.18
7	379.04	1	.	1	0	1	379	0	2.64	1	84.18
7	380.04	0	1	0	0	1	346	1	2.80	1	33.18
7	381.04	0	.	0	0	1	381	1	2.33	1	33.18
7	382.04	1	.	1	0	2	382	0	2.18	1	33.18
7	383.04	1	0	0	0	1	372	1	2.80	2	135.18
7	384.04	0	1	1	0	1	372	1	2.80	2	124.98
7	385.04	0	0	1	0	1	372	1	2.64	2	84.18
7	386.04	1	1	0	0	1	381	1	2.49	1	33.18
7	387.04	1	0	1	0	1	381	1	2.80	1	33.18
7	388.04	1	1	0	0	1	372	1	2.33	2	53.58
7	389.04	1	0	1	0	1	381	1	2.95	1	33.18
7	390.04	1	0	1	1	1	372	1	2.49	2	73.98
7	391.04	0	1	1	0	1	381	1	2.80	1	84.18
7	392.04	1	0	1	0	1	372	1	2.80	2	104.58
7	393.04	1	1	1	0	1	381	1	2.80	1	84.18
7	394.04	0	1	1	0	1	381	1	2.64	1	53.58
7	395.04	1	1	1	0	1	381	1	2.33	1	53.58
7	396.04	1	0	1	1	1	372	1	2.49	2	84.18
7	397.04	1	0	1	1	1	372	1	2.33	2	84.18
7	398.04	0	1	0	0	1	372	1	2.18	2	63.78
7	399.04	1	0	1	0	2	381	1	2.64	1	33.18
7	400.04	1	1	0	0	1	372	1	2.33	2	63.78
7	401.04	1	0	1	0	1	381	1	2.64	1	53.58
7	402.04	1	0	1	0	1	381	1	2.49	1	53.58
7	403.04	0	1	1	0	1	381	1	2.33	1	94.38
7	404.04	0	1	1	0	1	381	1	2.49	1	53.58
7	405.04	1	1	0	0	1	381	1	2.18	1	53.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	356.04	328.86	0.30	3.38	0.28	3.63	0		0	.
7	357.04	61.26	0.25	4.03	0.24	4.10	0		0	.
7	358.04	331.03	0.31	3.18	0.28	3.63	0		0	.
7	359.04	334.16	0.25	3.96	0.24	4.10	0		0	.
7	360.04	121.46	0.26	3.90	0.24	4.10	0		0	.
7	361.04	255.19	0.26	3.87	0.24	4.10	0		0	.
7	362.04	130.93	0.26	3.90	0.24	4.10	0		0	.
7	363.04	379.24	0.26	3.86	0.24	4.10	0		0	.
7	364.04	262.16	0.26	3.90	0.24	4.10	0		0	.
7	365.04	127.06	0.26	3.88	0.24	4.10	0		0	.
7	366.04	263.79	0.26	3.87	0.24	4.10	0		0	.
7	367.04	267.60	0.26	3.86	0.24	4.10	0		0	.
7	368.04	266.60	0.26	3.88	0.24	4.10	0		0	.
7	369.04	115.05	0.26	3.89	0.24	4.10	0		0	.
7	370.04	277.11	0.26	3.90	0.24	4.10	0		0	.
7	371.04	139.07	0.26	3.91	0.24	4.10	0		0	.
7	372.04	114.52	0.28	3.56	0.28	3.56	1	2	0	3.82
7	373.04	273.54	0.26	3.89	0.24	4.10	0		0	.
7	374.04	118.09	0.26	3.92	0.24	4.10	0		0	.
7	375.04	281.95	0.25	3.93	0.24	4.10	0		0	.
7	376.04	294.02	0.25	3.92	0.24	4.10	0		0	.
7	377.04	135.30	0.26	3.86	0.24	4.10	0		0	.
7	378.04	137.67	0.26	3.84	0.26	3.89	0		1	.
7	379.04	283.65	0.26	3.89	0.26	3.89	1	1	0	3.83
7	380.04	318.42	0.26	3.89	0.24	4.10	0		0	.
7	381.04	300.66	0.27	3.67	0.27	3.67	1	3	0	3.82
7	382.04	98.03	0.26	3.82	0.26	3.82	1	0	0	3.89
7	383.04	77.98	0.28	3.57	0.28	3.56	0		1	.
7	384.04	148.08	0.29	3.46	0.28	3.56	0		0	.
7	385.04	322.72	0.32	3.14	0.28	3.56	0		0	.
7	386.04	323.42	0.27	3.65	0.27	3.67	0		1	.
7	387.04	249.68	0.27	3.65	0.27	3.67	0		0	.
7	388.04	326.06	0.33	3.06	0.28	3.56	0		0	.
7	389.04	195.73	0.29	3.43	0.27	3.67	0		0	.
7	390.04	141.28	0.33	3.03	0.28	3.56	0		0	.
7	391.04	116.98	0.29	3.40	0.27	3.67	0		0	.
7	392.04	145.65	0.33	3.01	0.28	3.56	0		0	.
7	393.04	248.98	0.30	3.31	0.27	3.67	0		0	.
7	394.04	251.22	0.31	3.28	0.27	3.67	0		0	.
7	395.04	154.39	0.30	3.28	0.27	3.67	0		0	.
7	396.04	151.39	0.34	2.97	0.28	3.56	0		0	.
7	397.04	205.27	0.33	3.00	0.28	3.56	0		0	.
7	398.04	337.00	0.34	2.94	0.28	3.56	0		0	.
7	399.04	203.33	0.31	3.23	0.27	3.67	0		0	.
7	400.04	252.32	0.35	2.89	0.28	3.56	0		0	.
7	401.04	255.65	0.31	3.19	0.27	3.67	0		0	.
7	402.04	113.01	0.31	3.18	0.27	3.67	0		0	.
7	403.04	264.10	0.32	3.17	0.27	3.67	0		0	.
7	404.04	261.16	0.31	3.19	0.27	3.67	0		0	.
7	405.04	37.70	0.31	3.22	0.27	3.67	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	406.04	0	.	1	0	1	406	0	2.33	1	124.98
7	407.04	1	0	1	0	1	406	0	2.02	2	33.18
7	408.04	1	1	1	0	2	406	0	2.02	1	33.18
7	409.04	1	0	1	0	1	406	0	2.18	1	94.38
7	410.04	0	1	0	0	2	406	0	1.71	1	94.38
7	411.04	0	0	1	0	1	406	0	1.71	1	94.38
7	412.04	1	1	1	0	1	406	0	1.87	1	94.38
7	413.04	0	1	0	0	2	406	0	1.71	1	94.38
7	414.04	1	1	1	0	2	406	0	1.55	1	22.98
7	415.04	0	1	0	0	1	406	0	1.55	1	94.38
7	416.04	0	0	0	0	1	406	0	1.71	1	94.38
7	417.04	0	0	0	0	1	406	0	1.71	2	94.38
7	418.04	0	0	1	1	2	406	0	1.55	2	104.58
7	419.04	1	1	1	0	1	406	0	1.87	1	94.38
7	420.04	1	.	1	0	1	420	1	1.87	2	104.58
7	421.04	1	.	1	0	1	421	1	1.71	1	104.58
7	422.04	1	0	1	0	1	420	1	2.02	2	124.98
7	423.04	1	0	1	0	1	421	1	1.87	1	104.58
7	424.04	1	.	0	0	1	424	0	2.02	1	124.98
7	425.04	1	0	1	0	1	424	0	2.33	2	135.18
7	426.04	1	0	1	0	1	424	0	2.18	1	135.18
7	427.04	1	1	1	1	1	424	0	2.64	2	145.38
7	428.04	0	1	1	0	1	424	0	2.49	1	135.18
7	429.04	1	0	1	0	1	424	0	2.64	1	135.18
7	430.04	1	0	1	0	1	424	0	2.33	2	145.38
7	431.04	1	0	1	0	1	424	0	2.33	2	145.38
7	432.04	1	0	1	0	1	424	0	2.64	1	22.98
7	433.04	0	0	0	0	1	424	0	2.64	2	145.38
7	434.04	0	1	0	0	1	424	0	2.33	1	33.18
7	435.04	0	0	1	0	1	424	0	3.11	2	114.78
7	436.04	0	0	1	0	1	424	0	2.33	1	94.38
7	437.04	0	0	0	0	1	424	0	2.33	1	94.38
7	438.04	1	.	0	0	1	438	0	2.49	2	145.38
7	439.04	1	1	1	0	1	424	0	2.95	1	94.38
7	440.04	0	.	0	0	1	440	0	2.64	2	124.98
7	441.04	0	1	1	0	1	438	0	2.64	2	84.18
7	442.04	1	.	1	0	1	442	0	2.49	1	114.78
7	443.04	1	.	1	0	1	443	1	2.33	2	165.78
7	444.04	1	0	1	0	1	443	1	2.18	2	165.78
7	445.04	1	0	1	0	2	443	1	2.33	2	94.38
7	446.04	1	0	1	0	1	443	1	2.33	2	145.38
7	447.04	1	0	1	0	1	438	0	2.80	1	33.18
7	448.04	0	1	0	1	1	443	1	2.18	2	145.38
7	449.04	1	0	0	0	1	438	0	2.49	1	33.18
7	450.04	0	.	0	0	1	450	1	2.33	1	33.18
7	451.04	0	1	0	0	1	461	0	1.87	2	145.38
7	452.04	0	0	1	0	1	450	1	2.49	1	145.38
7	453.04	1	1	1	0	1	450	1	2.49	1	73.98
7	454.04	1	1	1	0	1	461	0	2.18	2	155.58
7	455.04	1	0	1	0	1	450	1	2.33	1	84.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	406.04	353.82	0.31	3.18	0.31	3.18	1	1	0	3.82
7	407.04	351.25	0.32	3.08	0.31	3.18	0		0	.
7	408.04	150.29	0.32	3.15	0.31	3.18	0		1	.
7	409.04	152.42	0.33	3.05	0.31	3.18	0		0	.
7	410.04	154.76	0.33	3.02	0.31	3.18	0		0	.
7	411.04	156.76	0.33	3.01	0.31	3.18	0		0	.
7	412.04	160.46	0.34	2.98	0.31	3.18	0		0	.
7	413.04	379.38	0.34	2.97	0.31	3.18	0		0	.
7	414.04	162.26	0.34	2.94	0.31	3.18	0		0	.
7	415.04	163.93	0.34	2.91	0.31	3.18	0		0	.
7	416.04	165.13	0.35	2.85	0.31	3.18	0		0	.
7	417.04	117.92	0.36	2.81	0.31	3.18	0		0	.
7	418.04	167.60	0.36	2.80	0.31	3.18	0		0	.
7	419.04	122.12	0.35	2.82	0.31	3.18	0		0	.
7	420.04	123.06	0.35	2.88	0.35	2.88	1	3	0	3.18
7	421.04	99.27	0.36	2.78	0.36	2.78	1	2	0	3.18
7	422.04	124.16	0.35	2.85	0.35	2.88	0		1	.
7	423.04	100.87	0.36	2.78	0.36	2.78	0		1	.
7	424.04	102.97	0.36	2.79	0.36	2.79	1	1	0	3.18
7	425.04	101.27	0.36	2.77	0.36	2.79	0		0	.
7	426.04	86.28	0.36	2.81	0.36	2.79	0		1	.
7	427.04	106.01	0.38	2.63	0.36	2.79	0		0	.
7	428.04	107.98	0.36	2.80	0.36	2.79	0		0	.
7	429.04	87.85	0.39	2.54	0.36	2.79	0		0	.
7	430.04	88.82	0.39	2.57	0.36	2.79	0		0	.
7	431.04	409.47	0.39	2.58	0.36	2.79	0		0	.
7	432.04	89.32	0.39	2.55	0.36	2.79	0		0	.
7	433.04	407.20	0.39	2.54	0.36	2.79	0		0	.
7	434.04	152.82	0.40	2.52	0.36	2.79	0		0	.
7	435.04	181.68	0.40	2.52	0.36	2.79	0		0	.
7	436.04	183.92	0.40	2.52	0.36	2.79	0		0	.
7	437.04	94.13	0.40	2.50	0.36	2.79	0		0	.
7	438.04	185.79	0.38	2.61	0.38	2.61	1	1	0	2.79
7	439.04	66.70	0.40	2.50	0.36	2.79	0		0	.
7	440.04	199.17	0.38	2.60	0.38	2.60	1	3	0	2.79
7	441.04	152.39	0.39	2.56	0.38	2.61	0		0	.
7	442.04	66.33	0.40	2.53	0.40	2.53	1	2	0	2.79
7	443.04	62.99	0.38	2.62	0.38	2.62	1	3	0	2.61
7	444.04	202.70	0.38	2.63	0.38	2.62	0		0	.
7	445.04	105.17	0.38	2.61	0.38	2.62	0		1	.
7	446.04	422.35	0.38	2.62	0.38	2.62	0		0	.
7	447.04	110.47	0.39	2.57	0.38	2.61	0		1	.
7	448.04	423.79	0.39	2.58	0.38	2.62	0		0	.
7	449.04	426.79	0.39	2.57	0.38	2.61	0		0	.
7	450.04	111.61	0.41	2.46	0.41	2.46	1	2	0	2.61
7	451.04	98.26	0.40	2.52	0.40	2.50	0		1	.
7	452.04	245.41	0.40	2.49	0.41	2.46	0		1	.
7	453.04	112.94	0.40	2.49	0.41	2.46	0		0	.
7	454.04	197.53	0.40	2.52	0.40	2.50	0		0	.
7	455.04	144.24	0.40	2.48	0.41	2.46	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	456.04	1	1	1	0	1	461	0	2.18	2	135.18
7	457.04	0	1	1	0	1	450	1	2.33	1	165.78
7	458.04	0	.	1	0	1	458	1	1.87	0	94.38
7	459.04	1	.	1	0	1	459	1	1.87	1	94.38
7	460.04	1	1	0	0	1	450	1	2.18	1	84.18
7	461.04	1	.	1	0	1	461	0	2.18	1	84.18
7	462.04	1	.	1	0	1	462	0	1.71	1	84.18
7	463.04	0	0	0	0	1	461	0	1.87	1	84.18
7	464.04	0	1	1	0	1	461	0	2.18	1	145.38
7	465.04	0	1	0	0	1	461	0	2.18	1	165.78
7	466.04	1	.	1	0	2	466	0	1.87	1	84.18
7	467.04	1	.	0	0	1	467	1	1.87	0	84.18
7	468.04	0	.	1	0	1	468	1	1.55	1	94.38
7	470.04	1	0	1	0	1	462	0	2.02	2	165.78
7	472.04	0	.	0	0	1	472	1	2.33	2	84.18
7	473.04	0	.	1	0	1	473	1	2.33	1	84.18
7	474.04	1	1	1	0	1	473	0	2.18	1	33.18
7	475.04	1	1	1	0	1	472	1	2.33	2	135.18
7	476.04	1	.	0	0	1	476	0	2.18	1	73.98
7	477.04	1	1	1	0	1	479	0	1.87	2	135.18
7	478.04	1	0	1	0	1	479	0	2.18	1	135.18
7	479.04	0	.	0	0	1	479	0	2.33	1	135.18
7	480.04	1	1	0	0	1	479	0	2.18	1	63.78
7	481.04	0	1	0	0	2	479	0	2.02	2	63.78
7	482.04	0	0	1	0	1	479	0	2.49	2	135.18
7	483.04	0	1	1	0	2	479	0	2.18	1	104.58
7	484.04	0	0	0	0	1	479	0	2.18	1	145.38
7	485.04	1	1	1	0	1	479	0	2.49	2	165.78
7	486.04	1	0	0	1	1	479	0	2.18	1	124.98
7	487.04	0	.	0	1	1	487	1	2.49	2	135.18
7	488.04	1	.	1	0	1	488	1	2.33	1	145.38
7	489.04	0	0	0	0	1	487	1	2.33	2	165.78
7	490.04	1	0	1	0	1	488	1	2.18	1	145.38
7	491.04	0	0	1	0	1	487	1	2.33	2	165.78
7	492.04	0	1	1	0	1	488	1	2.49	1	145.38
7	493.04	0	1	1	0	1	497	0	2.33	2	165.78
7	494.04	1	1	0	0	1	497	0	2.49	2	165.78
7	495.04	1	1	1	0	1	488	1	2.33	1	94.38
7	496.04	1	.	0	0	1	496	0	2.33	1	63.78
7	497.04	1	.	1	0	1	497	0	2.33	1	145.38
7	498.04	0	0	0	1	1	497	0	2.49	1	155.58
7	499.04	1	.	1	0	1	499	0	2.33	2	165.78
7	500.04	1	0	1	0	1	499	0	2.49	1	165.78
7	501.04	1	0	1	0	1	497	0	2.33	1	124.98
7	502.04	0	.	0	0	1	502	0	2.18	2	124.98
7	503.04	1	1	1	0	2	502	0	2.18	1	145.38
7	504.04	0	1	0	0	1	502	0	2.18	2	145.38
7	505.04	0	0	0	0	1	502	0	2.33	1	165.78
7	506.04	0	0	1	0	1	502	0	2.33	2	165.78
7	507.04	1	1	1	0	1	502	0	2.02	1	155.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	456.04	64.56	0.40	2.52	0.40	2.50	0		0	.
7	457.04	214.35	0.40	2.47	0.41	2.46	0		0	.
7	458.04	211.48	0.44	2.25	0.44	2.25	1	2	0	2.51
7	459.04	202.40	0.41	2.44	0.41	2.44	1	3	0	2.51
7	460.04	204.74	0.40	2.47	0.41	2.46	0		0	.
7	461.04	220.79	0.40	2.50	0.40	2.50	1	1	0	2.61
7	462.04	206.41	0.43	2.34	0.43	2.34	1	1	0	2.51
7	463.04	99.93	0.40	2.50	0.40	2.50	0		0	.
7	464.04	73.67	0.40	2.49	0.40	2.50	0		0	.
7	465.04	214.15	0.40	2.49	0.40	2.50	0		0	.
7	466.04	224.13	0.40	2.51	0.40	2.51	1	1	0	2.50
7	467.04	215.25	0.42	2.36	0.42	2.36	1	3	0	2.51
7	468.04	590.76	0.43	2.33	0.43	2.33	1	2	0	2.51
7	470.04	592.06	0.43	2.34	0.43	2.34	0		1	.
7	472.04	225.56	0.42	2.37	0.42	2.37	1	2	0	2.34
7	473.04	476.01	0.39	2.58	0.39	2.58	1	3	0	2.34
7	474.04	153.92	0.39	2.56	0.39	2.58	0		1	.
7	475.04	289.05	0.42	2.38	0.42	2.37	0		1	.
7	476.04	152.45	0.40	2.53	0.40	2.53	1	1	0	2.34
7	477.04	154.49	0.40	2.49	0.40	2.52	0		1	.
7	478.04	149.82	0.40	2.53	0.40	2.52	0		0	.
7	479.04	300.56	0.40	2.52	0.40	2.52	1	1	0	2.53
7	480.04	302.43	0.40	2.51	0.40	2.52	0		0	.
7	481.04	160.79	0.40	2.49	0.40	2.52	0		0	.
7	482.04	184.35	0.40	2.53	0.40	2.52	0		0	.
7	483.04	127.22	0.40	2.52	0.40	2.52	0		0	.
7	484.04	115.35	0.40	2.52	0.40	2.52	0		0	.
7	485.04	156.16	0.40	2.51	0.40	2.52	0		0	.
7	486.04	162.66	0.40	2.53	0.40	2.52	0		0	.
7	487.04	129.86	0.41	2.46	0.41	2.46	1	2	0	2.52
7	488.04	110.27	0.39	2.54	0.39	2.54	1	3	0	2.52
7	489.04	131.80	0.40	2.48	0.41	2.46	0		1	.
7	490.04	118.58	0.39	2.55	0.39	2.54	0		1	.
7	491.04	132.73	0.40	2.53	0.41	2.46	0		0	.
7	492.04	112.94	0.39	2.55	0.39	2.54	0		0	.
7	493.04	111.21	0.39	2.54	0.40	2.52	0		1	.
7	494.04	240.51	0.38	2.61	0.40	2.52	0		0	.
7	495.04	360.96	0.39	2.55	0.39	2.54	0		0	.
7	496.04	134.83	0.40	2.52	0.40	2.52	1	2	0	2.52
7	497.04	133.66	0.40	2.52	0.40	2.52	1	1	0	2.52
7	498.04	122.62	0.39	2.54	0.40	2.52	0		0	.
7	499.04	116.98	0.37	2.67	0.37	2.67	1	3	0	2.52
7	500.04	162.56	0.37	2.74	0.37	2.67	0		1	.
7	501.04	172.41	0.39	2.54	0.40	2.52	0		0	.
7	502.04	140.84	0.37	2.71	0.37	2.71	1	1	0	2.52
7	503.04	144.61	0.37	2.70	0.37	2.71	0		1	.
7	504.04	123.22	0.37	2.70	0.37	2.71	0		0	.
7	505.04	124.52	0.37	2.68	0.37	2.71	0		0	.
7	506.04	153.78	0.37	2.71	0.37	2.71	0		0	.
7	507.04	152.85	0.37	2.68	0.37	2.71	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	508.04	0	1	1	0	1	502	0	2.18	2	155.58
7	509.04	1	1	1	0	1	502	0	2.18	1	165.78
7	510.04	0	1	1	0	1	502	0	2.33	2	155.58
7	511.04	1	1	0	0	1	502	0	2.18	1	165.78
7	512.04	1	.	1	0	1	512	0	1.87	2	196.39
7	513.04	1	.	1	0	1	513	0	2.18	0	165.78
7	514.04	1	.	1	0	1	514	1	1.87	2	155.58
7	515.04	1	0	1	0	1	514	1	2.18	2	155.58
7	516.04	0	1	0	1	1	514	1	2.18	2	63.78
7	517.04	1	0	1	1	1	514	1	2.02	2	155.58
7	518.04	1	1	1	0	1	527	1	1.87	1	196.39
7	519.04	0	0	1	1	1	514	1	2.33	2	155.58
7	520.04	1	1	1	0	1	514	1	2.02	2	155.58
7	521.04	1	0	1	0	1	514	1	2.18	2	94.38
7	522.04	1	0	1	0	1	514	1	2.33	2	94.38
7	523.04	1	0	1	0	1	514	1	2.33	2	94.38
7	524.04	0	1	1	0	1	514	1	2.02	2	196.39
7	525.04	0	0	1	0	1	514	1	2.02	2	196.39
7	526.04	0	0	1	0	1	531	1	2.49	1	63.78
7	527.04	1	.	1	0	1	527	1	1.55	1	33.18
7	528.04	0	1	1	0	1	527	1	2.02	1	33.18
7	530.04	1	1	1	0	1	531	1	2.33	1	124.98
7	531.04	0	.	0	0	1	531	1	2.02	1	124.98
7	532.04	1	.	1	0	2	532	0	2.49	1	124.98
7	533.04	0	0	1	0	1	531	1	1.87	1	165.78
7	534.04	0	0	0	0	1	531	1	2.18	1	165.78
7	535.04	1	0	1	0	1	531	1	2.33	1	155.58
7	536.04	1	0	1	0	1	531	1	2.18	1	114.78
7	537.04	0	1	1	0	1	531	1	2.18	1	155.58
7	538.04	0	0	0	0	1	531	1	2.49	1	155.58
7	539.04	1	1	1	0	1	531	1	2.64	1	155.58
7	540.04	1	.	1	0	1	540	0	1.40	1	104.58
7	541.04	1	.	1	0	1	541	0	1.71	1	104.58
7	542.04	1	.	1	0	1	542	0	1.71	1	196.39
7	543.04	1	0	1	0	1	542	0	1.87	1	145.38
7	544.04	1	0	1	0	1	542	0	1.87	1	196.39
7	545.04	1	0	1	0	1	542	0	2.02	2	196.39
7	546.04	0	0	0	0	1	542	0	2.02	2	196.39
7	547.04	0	1	0	0	1	542	0	2.02	1	114.78
7	548.04	0	0	1	0	1	542	0	2.18	1	114.78
7	549.04	1	1	1	0	1	542	0	2.02	2	94.38
7	550.04	1	.	1	0	1	550	1	2.33	2	94.38
7	551.04	1	.	1	0	1	551	1	2.18	1	94.38
7	552.04	1	0	1	0	1	550	1	1.87	2	135.18
7	553.04	0	1	1	0	1	551	1	2.02	1	124.98
7	554.04	1	1	1	0	1	551	1	2.02	1	73.98
7	555.04	1	0	1	0	1	550	1	2.02	2	145.38
7	556.04	1	.	1	0	1	556	1	2.18	2	155.58
7	557.04	0	1	1	0	1	551	1	2.18	1	114.78
7	558.04	0	0	0	0	1	551	1	2.18	1	114.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	508.04	135.43	0.37	2.73	0.37	2.71	0		0	.
7	509.04	155.35	0.38	2.62	0.37	2.71	0		0	.
7	510.04	136.57	0.37	2.73	0.37	2.71	0		0	.
7	511.04	111.84	0.38	2.64	0.37	2.71	0		0	.
7	512.04	138.27	0.37	2.73	0.37	2.73	1	3	0	2.71
7	513.04	171.10	0.39	2.56	0.39	2.56	1	2	0	2.71
7	514.04	174.17	0.39	2.59	0.39	2.59	1	2	0	2.71
7	515.04	397.76	0.38	2.63	0.39	2.59	0		0	.
7	516.04	167.53	0.38	2.63	0.39	2.59	0		0	.
7	517.04	110.71	0.38	2.62	0.39	2.59	0		1	.
7	518.04	175.24	0.36	2.76	0.37	2.73	0		0	.
7	519.04	169.67	0.38	2.61	0.39	2.59	0		0	.
7	520.04	315.58	0.39	2.59	0.39	2.59	0		0	.
7	521.04	313.42	0.38	2.60	0.39	2.59	0		0	.
7	522.04	312.51	0.38	2.62	0.39	2.59	0		0	.
7	523.04	115.48	0.38	2.61	0.39	2.59	0		0	.
7	524.04	114.05	0.43	2.33	0.39	2.59	0		0	.
7	525.04	401.53	0.43	2.34	0.39	2.59	0		0	.
7	526.04	538.54	0.33	3.02	0.33	3.05	0		0	.
7	527.04	540.04	0.37	2.73	0.37	2.73	1	3	0	2.71
7	528.04	653.82	0.36	2.76	0.37	2.73	0		1	.
7	530.04	188.96	0.33	3.02	0.33	3.05	0		0	.
7	531.04	215.75	0.33	3.05	0.33	3.05	1	3	0	2.71
7	532.04	95.29	0.34	2.92	0.34	2.92	1	0	0	2.71
7	533.04	96.63	0.33	3.01	0.33	3.05	0		1	.
7	534.04	163.23	0.33	3.00	0.33	3.05	0		0	.
7	535.04	234.60	0.33	3.02	0.33	3.05	0		0	.
7	536.04	164.46	0.33	3.02	0.33	3.05	0		0	.
7	537.04	165.80	0.33	3.02	0.33	3.05	0		0	.
7	538.04	172.77	0.33	3.02	0.33	3.05	0		0	.
7	539.04	254.05	0.33	2.99	0.33	3.05	0		0	.
7	540.04	252.09	0.34	2.94	0.34	2.94	1	1	0	2.94
7	541.04	118.18	0.34	2.94	0.34	2.94	1	0	0	2.92
7	542.04	188.89	0.34	2.92	0.34	2.92	1	1	0	2.94
7	543.04	125.02	0.34	2.92	0.34	2.92	0		1	.
7	544.04	126.33	0.35	2.90	0.34	2.92	0		0	.
7	545.04	126.83	0.34	2.92	0.34	2.92	0		0	.
7	546.04	222.49	0.35	2.88	0.34	2.92	0		0	.
7	547.04	225.19	0.35	2.90	0.34	2.92	0		0	.
7	548.04	348.65	0.34	2.96	0.34	2.92	0		0	.
7	549.04	336.30	0.35	2.85	0.34	2.92	0		0	.
7	550.04	355.59	0.35	2.87	0.35	2.87	1	1	0	2.92
7	551.04	228.50	0.34	2.92	0.34	2.92	1	3	0	2.87
7	552.04	230.63	0.38	2.63	0.35	2.87	0		1	.
7	553.04	452.62	0.34	2.91	0.34	2.92	0		1	.
7	554.04	192.52	0.35	2.88	0.34	2.92	0		0	.
7	555.04	217.11	0.38	2.66	0.35	2.87	0		0	.
7	556.04	274.31	0.40	2.50	0.40	2.50	1	2	0	2.87
7	557.04	276.34	0.35	2.84	0.34	2.92	0		0	.
7	558.04	130.30	0.35	2.83	0.34	2.92	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	559.04	1	0	0	0	1	550	1	2.02	2	196.39
7	560.04	0	.	1	0	1	560	1	1.87	1	114.78
7	561.04	1	0	1	0	1	556	1	2.18	0	155.58
7	562.04	0	0	0	0	1	560	1	2.02	1	94.38
7	563.04	0	.	0	0	2	563	0	1.55	1	145.38
7	564.04	1	0	1	0	1	565	0	0.93	1	155.58
7	565.04	1	.	1	0	.	565	0	0.93	1	145.38
7	566.04	1	0	0	0	2	565	0	1.09	1	196.39
7	567.04	1	0	1	0	1	565	0	1.24	1	196.39
7	568.04	0	1	1	0	2	565	0	1.55	1	104.58
7	569.04	0	0	1	0	1	565	0	1.71	2	135.18
7	570.04	0	0	0	0	1	565	0	1.55	1	104.58
7	571.04	1	1	1	0	1	574	0	1.87	2	196.39
7	572.04	0	.	1	0	2	572	0	1.87	1	155.58
7	573.04	1	0	0	0	1	574	0	2.02	2	196.39
7	574.04	0	.	1	0	2	574	0	1.71	1	196.39
7	575.04	0	1	1	0	1	574	0	2.33	2	196.39
7	576.04	1	0	1	0	1	574	0	1.87	1	196.39
7	577.04	1	0	1	0	1	574	0	1.87	1	196.39
7	578.04	1	0	0	0	1	574	0	2.33	2	196.39
7	579.04	1	1	1	0	1	574	0	1.87	1	196.39
7	580.04	1	0	1	0	1	574	0	2.18	1	196.39
7	581.04	0	1	0	0	2	574	0	2.33	1	94.38
7	582.04	0	0	0	0	1	574	0	2.18	1	135.18
7	583.04	0	1	0	0	1	574	0	2.18	0	175.99
7	584.04	0	1	1	0	1	574	0	2.18	2	175.99
7	585.04	1	0	1	0	1	574	0	2.49	1	196.39
7	586.04	1	1	1	0	1	574	0	2.33	2	196.39
7	587.04	1	.	1	0	1	587	1	2.18	2	155.58
7	588.04	0	.	0	0	1	588	1	1.87	2	196.39
7	589.04	1	1	1	0	1	574	0	2.49	1	94.38
7	590.04	0	.	1	0	1	590	1	2.33	1	145.38
7	591.04	0	.	1	0	1	591	1	2.49	1	135.18
7	592.04	0	.	1	1	2	592	1	1.71	2	196.39
7	593.04	1	.	1	0	1	593	1	1.55	1	196.39
7	594.04	0	1	0	0	1	595	0	1.55	2	196.39
7	595.04	1	.	1	0	2	595	0	1.71	1	196.39
7	596.04	0	0	0	0	2	595	0	1.71	2	165.78
7	597.04	1	1	1	0	1	595	0	1.71	1	196.39
7	598.04	0	1	0	0	1	595	0	1.87	1	196.39
7	599.04	1	0	1	0	1	595	0	1.55	2	196.39
7	600.04	1	.	1	0	1	600	1	2.02	2	196.39
7	601.04	1	1	1	0	2	595	0	1.71	1	196.39
7	602.04	0	1	0	0	1	595	0	1.87	1	22.98
7	603.04	0	.	1	0	1	603	1	2.18	1	196.39
7	604.04	1	1	1	0	1	603	1	1.87	1	196.39
7	605.04	0	1	1	0	1	600	1	2.02	2	196.39
7	606.04	1	.	1	0	1	606	0	2.18	1	135.18
7	607.04	0	1	1	0	1	606	0	2.49	2	124.98
7	608.04	1	.	1	0	1	608	1	2.49	2	165.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	559.04	268.20	0.38	2.67	0.35	2.87	0		0	.
7	560.04	220.45	0.35	2.84	0.35	2.84	1	3	0	2.87
7	561.04	364.13	0.37	2.68	0.40	2.50	0		1	.
7	562.04	210.54	0.35	2.88	0.35	2.84	0		1	.
7	563.04	207.64	0.38	2.64	0.38	2.64	1	1	0	2.87
7	564.04	191.22	0.38	2.65	0.38	2.66	0		1	.
7	565.04	133.73	0.38	2.66	0.38	2.66	1	0	0	2.64
7	566.04	132.73	0.38	2.64	0.38	2.66	0		0	.
7	567.04	292.79	0.38	2.61	0.38	2.66	0		0	.
7	568.04	256.19	0.38	2.62	0.38	2.66	0		0	.
7	569.04	297.36	0.38	2.61	0.38	2.66	0		0	.
7	570.04	168.33	0.38	2.62	0.38	2.66	0		0	.
7	571.04	222.72	0.39	2.59	0.39	2.60	0		1	.
7	572.04	178.74	0.38	2.63	0.38	2.63	1	0	0	2.66
7	573.04	170.87	0.38	2.61	0.39	2.60	0		0	.
7	574.04	180.71	0.39	2.60	0.39	2.60	1	1	0	2.63
7	575.04	174.14	0.39	2.57	0.39	2.60	0		0	.
7	576.04	172.77	0.38	2.62	0.39	2.60	0		0	.
7	577.04	178.18	0.38	2.63	0.39	2.60	0		0	.
7	578.04	176.28	0.39	2.55	0.39	2.60	0		0	.
7	579.04	176.11	0.39	2.58	0.39	2.60	0		0	.
7	580.04	431.83	0.39	2.59	0.39	2.60	0		0	.
7	581.04	278.18	0.39	2.59	0.39	2.60	0		0	.
7	582.04	223.92	0.39	2.58	0.39	2.60	0		0	.
7	583.04	225.96	0.40	2.53	0.39	2.60	0		0	.
7	584.04	188.42	0.38	2.62	0.39	2.60	0		0	.
7	585.04	187.85	0.39	2.57	0.39	2.60	0		0	.
7	586.04	272.87	0.38	2.60	0.39	2.60	0		0	.
7	587.04	193.66	0.40	2.50	0.40	2.50	1	3	0	2.60
7	588.04	437.41	0.36	2.79	0.36	2.79	1	3	0	2.60
7	589.04	223.49	0.39	2.55	0.39	2.60	0		0	.
7	590.04	288.36	0.42	2.38	0.42	2.38	1	2	0	2.60
7	591.04	201.83	0.38	2.61	0.38	2.61	1	3	0	2.60
7	592.04	184.18	0.38	2.66	0.38	2.66	1	3	0	2.60
7	593.04	213.98	0.38	2.63	0.38	2.63	1	2	0	2.60
7	594.04	186.62	0.38	2.64	0.38	2.65	0		1	.
7	595.04	250.38	0.38	2.65	0.38	2.65	1	1	0	2.60
7	596.04	191.79	0.38	2.66	0.38	2.65	0		0	.
7	597.04	195.03	0.38	2.62	0.38	2.65	0		0	.
7	598.04	199.03	0.38	2.66	0.38	2.65	0		0	.
7	599.04	232.23	0.37	2.71	0.38	2.65	0		0	.
7	600.04	197.83	0.38	2.60	0.38	2.60	1	2	0	2.65
7	601.04	670.90	0.38	2.62	0.38	2.65	0		0	.
7	602.04	201.70	0.38	2.63	0.38	2.65	0		0	.
7	603.04	240.27	0.38	2.61	0.38	2.61	1	3	0	2.65
7	604.04	217.32	0.38	2.64	0.38	2.61	0		1	.
7	605.04	341.14	0.38	2.62	0.38	2.60	0		1	.
7	606.04	311.71	0.38	2.63	0.38	2.63	1	1	0	2.65
7	607.04	262.63	0.38	2.60	0.38	2.63	0		1	.
7	608.04	241.01	0.39	2.58	0.39	2.58	1	2	0	2.63

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	609.04	0	.	1	0	1	609	1	2.33	1	196.39
7	610.04	1	1	1	0	1	609	1	2.64	1	196.39
7	611.04	1	0	0	0	1	608	1	2.33	2	196.39
7	612.04	0	.	1	0	1	612	0	2.49	1	196.39
7	613.04	0	1	1	0	1	612	0	2.33	2	165.78
7	614.04	1	1	1	0	1	612	0	2.18	1	196.39
7	615.04	1	0	1	0	1	612	0	2.64	2	196.39
7	616.04	1	1	1	0	1	612	0	2.18	1	196.39
7	617.04	0	1	1	0	1	621	0	2.49	2	165.78
7	618.04	1	.	1	0	1	618	0	2.49	2	165.78
7	619.04	1	.	1	0	1	619	0	2.49	1	94.38
7	620.04	1	0	0	0	1	612	0	2.33	1	94.38
7	621.04	1	.	1	0	1	621	0	2.49	1	155.58
7	622.04	1	1	1	0	1	621	0	2.64	1	155.58
7	623.04	1	0	1	0	1	621	0	2.49	1	94.38
7	624.04	1	0	1	1	1	621	0	2.02	2	94.38
7	625.04	1	0	1	0	2	621	0	1.71	1	114.78
7	626.04	1	0	1	0	1	621	0	1.40	2	165.78
7	627.04	1	.	1	0	1	627	0	1.55	0	165.78
7	628.04	1	.	1	0	2	628	0	1.71	1	94.38
7	629.04	1	0	1	0	2	628	0	1.40	1	94.38
7	630.04	1	.	0	0	2	630	0	0.93	1	135.18
7	631.04	0	1	0	0	1	630	0	1.40	2	196.39
7	632.04	1	1	1	0	1	630	0	1.09	1	196.39
7	634.04	0	.	1	0	2	634	0	1.87	2	165.78
7	635.04	1	1	1	0	1	634	0	1.55	1	165.78
7	636.04	0	.	0	0	2	636	0	1.87	1	196.39
7	637.04	0	0	0	0	1	636	0	1.55	2	196.39
7	638.04	0	.	0	0	2	638	0	1.71	1	124.98
7	639.04	0	.	0	0	2	639	0	1.40	1	196.39
7	640.04	0	0	0	0	2	639	0	1.24	1	145.38
7	641.04	1	.	1	0	1	641	0	0.78	1	155.58
7	642.04	1	.	1	0	2	642	0	1.24	1	145.38
7	643.04	1	.	1	0	.	643	0	0.31	1	155.58
7	644.04	0	.	1	0	.	644	0	0.31	1	2.58
7	645.04	0	.	0	0	1	645	0	0.47	1	124.98
7	646.04	0	.	1	0	.	646	0	0.47	2	124.98
7	647.04	0	.	0	0	.	647	0	0.62	2	186.19
7	648.04	0	.	1	0	2	648	0	0.78	2	175.99
7	649.04	0	.	0	0	.	649	0	0.31	2	175.99
7	650.04	0	.	0	0	2	650	0	0.62	1	124.98
7	651.04	0	.	0	0	.	651	0	0.31	1	155.58
7	652.04	1	.	1	0	.	652	0	0.31	1	12.78
7	653.04	1	0	1	0	2	652	0	0.62	1	12.78
7	654.04	0	1	0	0	2	652	0	0.93	1	12.78
7	655.04	0	.	1	0	.	655	0	0.62	1	63.78
7	656.04	0	.	1	0	.	656	0	0.31	2	124.98
7	657.04	0	.	1	0	.	657	0	0.31	1	175.99
7	658.04	1	.	1	0	.	658	0	0.31	2	94.38
7	659.04	0	.	1	0	.	659	0	0.62	0	186.19

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	609.04	210.14	0.37	2.72	0.37	2.72	1	3	0	2.63
7	610.04	207.07	0.37	2.70	0.37	2.72	0		1	.
7	611.04	256.86	0.38	2.66	0.39	2.58	0		1	.
7	612.04	273.34	0.37	2.70	0.37	2.70	1	1	0	2.63
7	613.04	242.54	0.38	2.62	0.37	2.70	0		0	.
7	614.04	213.01	0.37	2.70	0.37	2.70	0		1	.
7	615.04	215.21	0.38	2.62	0.37	2.70	0		0	.
7	616.04	308.94	0.37	2.68	0.37	2.70	0		0	.
7	617.04	306.67	0.38	2.62	0.37	2.68	0		1	.
7	618.04	505.24	0.38	2.64	0.38	2.64	1	2	0	2.70
7	619.04	530.50	0.37	2.67	0.37	2.67	1	3	0	2.70
7	620.04	302.10	0.37	2.68	0.37	2.70	0		0	.
7	621.04	302.00	0.37	2.68	0.37	2.68	1	1	0	2.70
7	622.04	496.47	0.37	2.67	0.37	2.68	0		0	.
7	623.04	498.27	0.37	2.68	0.37	2.68	0		0	.
7	624.04	501.80	0.37	2.67	0.37	2.68	0		0	.
7	625.04	313.38	0.38	2.65	0.37	2.68	0		0	.
7	626.04	311.14	0.38	2.64	0.37	2.68	0		0	.
7	627.04	509.04	0.42	2.38	0.42	2.38	1	2	0	2.68
7	628.04	529.46	0.37	2.71	0.37	2.71	1	3	0	2.68
7	629.04	353.25	0.37	2.69	0.37	2.71	0		1	.
7	630.04	273.81	0.39	2.56	0.39	2.56	1	1	0	2.68
7	631.04	272.34	0.40	2.51	0.39	2.56	0		1	.
7	632.04	818.55	0.40	2.53	0.39	2.56	0		0	.
7	634.04	323.92	0.38	2.62	0.38	2.62	1	4	0	2.56
7	635.04	306.07	0.38	2.63	0.38	2.62	0		1	.
7	636.04	307.37	0.38	2.64	0.38	2.64	1	1	0	2.62
7	637.04	415.95	0.39	2.58	0.38	2.64	0		1	.
7	638.04	460.16	0.38	2.61	0.38	2.61	1	0	0	2.64
7	639.04	430.26	0.38	2.60	0.38	2.60	1	2	0	2.61
7	640.04	343.64	0.39	2.56	0.38	2.60	0		1	.
7	641.04	422.65	0.41	2.46	0.41	2.46	1	1	0	2.61
7	642.04	594.89	0.33	3.05	0.33	3.05	1	3	0	2.61
7	643.04	883.41	0.69	1.45	0.69	1.45	1	0	0	2.46
7	644.04	592.63	0.92	1.09	0.92	1.09	1	0	0	1.19
7	645.04	595.33	0.55	1.81	0.55	1.81	1	2	0	1.45
7	646.04	651.72	0.55	1.82	0.55	1.82	1	3	0	1.45
7	647.04	697.19	0.84	1.19	0.84	1.19	1	0	0	1.45
7	648.04	694.93	0.91	1.09	0.91	1.09	1	1	0	1.13
7	649.04	102.77	0.84	1.20	0.84	1.20	1	0	0	1.09
7	650.04	531.93	0.89	1.13	0.89	1.13	1	1	0	1.20
7	651.04	933.76	0.92	1.08	0.92	1.08	1	0	0	1.09
7	652.04	935.10	0.69	1.44	0.69	1.44	1	0	0	1.08
7	653.04	936.30	0.69	1.45	0.69	1.44	0		1	.
7	654.04	822.75	0.68	1.47	0.69	1.44	0		0	.
7	655.04	721.59	0.69	1.44	0.69	1.44	1	0	0	1.44
7	656.04	770.43	1.33	0.75	1.33	0.75	1	0	0	1.50
7	657.04	1072.34	0.67	1.50	0.67	1.50	1	0	0	1.44
7	658.04	979.98	0.89	1.13	0.89	1.13	1	0	0	0.75
7	659.04	1252.95	0.91	1.10	0.91	1.10	1	0	0	1.13

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	661.04	0	.	0	0	.	661	0	0.31	1	175.99
7	662.04	0	0	0	0	1	661	0	0.62	2	175.99
7	663.04	1	.	1	0	.	663	0	0.31	1	186.19
7	664.04	1	.	1	0	.	664	0	0.31	1	196.39
7	666.04	1	.	1	0	1	666	1	2.02	1	63.78
7	667.04	1	0	1	0	1	666	1	2.33	0	63.78
7	93.05	1	.	0	0	1	93	0	1.24	2	43.38
7	94.05	1	.	1	0	1	94	0	1.55	2	12.78
7	95.05	0	.	0	0	1	95	0	0.93	2	43.38
7	107.05	1	.	1	0	1	107	0	0.78	0	12.78
7	130.05	1	.	1	0	3	130	0	1.24	0	2.58
7	133.05	0	1	0	0	2	130	0	1.40	1	2.58
7	160.05	1	.	0	0	1	160	0	1.24	2	2.58
7	162.05	1	.	1	0	1	162	0	1.24	0	33.18
7	163.05	1	.	1	0	1	163	0	1.24	0	33.18
7	169.05	1	.	1	0	1	169	0	0.93	2	33.18
7	171.05	1	0	1	0	1	169	0	0.93	2	33.18
7	173.05	0	.	1	1	2	173	0	1.09	0	33.18
7	182.05	0	.	0	0	1	182	0	1.24	1	2.58
7	188.05	1	.	1	0	2	188	0	1.40	0	2.58
7	193.05	1	1	1	0	1	194	0	0.93	1	12.78
7	194.05	0	.	1	1	1	194	0	0.78	2	12.78
7	200.05	0	.	0	0	2	200	0	1.24	1	43.38
7	201.05	0	0	1	0	2	200	0	1.40	1	43.38
7	202.05	1	.	0	0	1	202	0	1.24	1	2.58
7	203.05	1	0	0	0	2	202	0	1.09	1	2.58
7	204.05	1	0	1	0	2	194	0	1.09	1	12.78
7	208.05	1	1	1	0	1	209	0	1.24	2	12.78
7	209.05	0	.	1	0	2	209	0	1.09	1	12.78
7	212.05	1	0	1	0	1	213	0	1.40	2	33.18
7	213.05	1	.	1	0	2	213	0	1.40	1	33.18
7	220.05	0	1	1	0	1	226	0	1.55	2	33.18
7	221.05	0	.	0	0	1	221	0	1.71	2	63.78
7	222.05	1	.	1	0	1	222	0	1.87	0	12.78
7	225.05	0	.	1	0	1	225	1	1.87	2	22.98
7	226.05	1	.	1	0	2	226	0	1.55	1	33.18
7	227.05	1	1	1	0	1	225	1	1.24	2	12.78
7	229.05	1	0	1	0	1	222	0	1.71	1	12.78
7	241.05	0	.	0	0	1	241	0	1.24	2	12.78
7	242.05	1	0	1	0	1	247	0	1.71	2	63.78
7	243.05	0	1	0	0	1	247	0	2.02	2	63.78
7	244.05	0	.	1	0	1	244	1	2.33	2	63.78
7	245.05	1	.	1	0	1	245	1	2.33	2	12.78
7	246.05	1	.	1	0	2	246	1	1.71	1	12.78
7	247.05	1	.	1	0	1	247	0	1.24	1	12.78
7	248.05	0	.	0	0	1	248	1	2.33	0	2.58
7	249.05	1	0	1	0	2	247	0	1.55	1	12.78
7	250.05	0	.	1	0	1	250	1	2.02	1	12.78
7	252.05	0	1	1	0	1	254	1	2.18	1	104.58
7	254.05	1	.	1	0	1	254	1	2.02	1	2.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	661.04	1010.74	0.70	1.44	0.70	1.44	1	0	0	1.10
7	662.04	1222.05	0.69	1.45	0.70	1.44	0		1	.
7	663.04	1049.52	0.86	1.16	0.86	1.16	1	0	0	1.44
7	664.04	142.65	0.91	1.10	0.91	1.10	1	0	0	1.16
7	666.04	183.65	0.26	3.81	0.26	3.81	1	1	0	.
7	667.04	181.41	0.27	3.75	0.26	3.81	0		1	.
7	93.05	84.08	1.14	0.87	1.14	0.87	1	1	0	1.04
7	94.05	40.00	0.96	1.04	0.96	1.04	1	1	0	1.08
7	95.05	100.43	0.92	1.08	0.92	1.08	1	1	0	.
7	107.05	216.75	1.11	0.90	1.11	0.90	1	1	0	0.87
7	130.05	196.49	0.58	1.74	0.58	1.74	1	3	0	0.87
7	133.05	116.21	0.58	1.73	0.58	1.74	0		1	.
7	160.05	127.39	0.65	1.54	0.65	1.54	1	1	0	0.90
7	162.05	76.41	0.64	1.55	0.64	1.55	1	1	0	1.52
7	163.05	131.69	0.66	1.52	0.66	1.52	1	1	0	1.54
7	169.05	314.04	0.64	1.56	0.64	1.56	1	1	0	1.55
7	171.05	289.33	0.63	1.58	0.64	1.56	0		1	.
7	173.05	291.56	0.64	1.57	0.64	1.57	1	1	0	1.56
7	182.05	136.17	0.51	1.95	0.51	1.95	1	1	0	1.57
7	188.05	304.97	0.60	1.68	0.60	1.68	1	2	0	1.85
7	193.05	129.19	0.57	1.74	0.58	1.73	0		1	.
7	194.05	162.19	0.58	1.73	0.58	1.73	1	1	0	1.85
7	200.05	57.02	0.54	1.85	0.54	1.85	1	1	0	1.95
7	201.05	121.89	0.54	1.86	0.54	1.85	0		1	.
7	202.05	123.09	0.54	1.86	0.54	1.86	1	3	0	1.85
7	203.05	132.13	0.53	1.89	0.54	1.86	0		1	.
7	204.05	169.07	0.58	1.74	0.58	1.73	0		0	.
7	208.05	133.33	0.54	1.85	0.53	1.87	0		1	.
7	209.05	286.48	0.53	1.87	0.53	1.87	1	4	0	1.73
7	212.05	95.69	0.53	1.90	0.53	1.90	0		1	.
7	213.05	295.72	0.53	1.90	0.53	1.90	1	1	0	1.87
7	220.05	66.84	0.49	2.04	0.49	2.04	0		1	.
7	221.05	141.71	0.49	2.03	0.49	2.03	1	4	0	2.04
7	222.05	302.90	0.48	2.08	0.48	2.08	1	4	0	2.03
7	225.05	104.14	0.49	2.04	0.49	2.04	1	2	0	2.08
7	226.05	149.85	0.49	2.04	0.49	2.04	1	1	0	1.90
7	227.05	182.35	0.49	2.06	0.49	2.04	0		1	.
7	229.05	183.98	0.50	2.01	0.48	2.08	0		1	.
7	241.05	70.87	0.47	2.11	0.47	2.11	1	1	0	2.08
7	242.05	71.81	0.47	2.11	0.46	2.18	0		1	.
7	243.05	76.04	0.47	2.14	0.46	2.18	0		0	.
7	244.05	166.00	0.50	1.99	0.50	1.99	1	2	0	2.18
7	245.05	145.48	0.47	2.13	0.47	2.13	1	2	0	2.18
7	246.05	155.32	0.40	2.51	0.40	2.51	1	3	0	2.08
7	247.05	168.47	0.46	2.18	0.46	2.18	1	1	0	2.11
7	248.05	158.29	0.44	2.27	0.44	2.27	1	2	0	2.31
7	249.05	164.66	0.46	2.19	0.46	2.18	0		0	.
7	250.05	201.80	0.42	2.39	0.42	2.39	1	3	0	2.31
7	252.05	209.27	0.44	2.27	0.44	2.26	0		1	.
7	254.05	39.91	0.44	2.26	0.44	2.26	1	3	0	2.18

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	255.05	0	.	0	0	1	255	1	1.87	1	104.58
7	256.05	1	.	1	0	1	256	1	1.87	2	12.78
7	258.05	1	.	1	0	1	258	0	2.02	1	12.78
7	260.05	0	1	1	0	1	262	0	2.02	2	12.78
7	261.05	1	.	1	0	1	261	1	2.18	2	12.78
7	262.05	1	.	1	0	1	262	0	2.33	1	2.58
7	264.05	0	.	0	0	1	264	1	2.18	0	12.78
7	265.05	1	.	1	0	1	265	1	2.18	1	12.78
7	266.05	1	.	1	0	1	266	1	2.02	0	12.78
7	267.05	1	.	1	0	1	267	1	2.18	0	12.78
7	268.05	1	.	1	0	2	268	0	1.87	1	12.78
7	270.05	0	0	0	0	1	268	0	2.49	2	53.58
7	273.05	0	1	1	0	1	268	0	2.18	2	73.98
7	276.05	1	.	1	0	1	276	1	2.33	2	43.38
7	277.05	1	0	0	0	1	276	1	2.33	2	43.38
7	278.05	0	0	1	0	1	268	0	2.18	1	73.98
7	280.05	0	.	1	0	1	280	0	2.02	1	63.78
7	282.05	0	1	0	0	1	276	1	2.18	2	43.38
7	283.05	0	0	1	0	1	276	1	1.87	2	12.78
7	284.05	0	0	1	0	1	276	1	2.02	2	12.78
7	285.05	0	.	0	0	1	285	1	2.49	1	73.98
7	287.05	1	1	1	0	1	285	1	2.49	1	73.98
7	288.05	1	0	1	0	1	343	0	1.71	0	53.58
7	290.05	1	0	1	0	1	303	1	2.18	1	12.78
7	293.05	1	0	1	0	1	303	1	2.02	1	12.78
7	294.05	1	0	1	0	1	303	1	1.87	1	12.78
7	295.05	1	0	1	0	1	343	0	1.71	1	12.78
7	296.05	0	.	1	0	1	296	0	2.02	1	33.18
7	297.05	1	.	0	0	1	297	0	2.02	1	2.58
7	298.05	0	.	0	1	1	298	0	2.18	2	73.98
7	299.05	0	.	1	0	1	299	0	2.18	1	53.58
7	300.05	1	.	0	0	1	300	0	2.33	1	43.38
7	301.05	0	0	1	0	1	299	0	2.49	2	73.98
7	302.05	0	.	1	0	1	302	0	2.33	2	73.98
7	303.05	1	.	1	0	2	303	1	2.33	1	12.78
7	304.05	1	0	1	0	1	302	0	2.64	2	12.78
7	305.05	1	1	1	0	1	302	0	2.18	1	12.78
7	306.05	1	0	1	0	1	307	1	2.49	2	63.78
7	307.05	1	.	1	0	1	307	1	2.95	2	63.78
7	308.05	1	0	1	0	1	307	1	2.80	2	73.98
7	309.05	1	0	1	0	1	307	1	2.49	2	73.98
7	310.05	1	.	1	0	1	310	0	2.64	2	63.78
7	312.05	1	.	1	0	1	312	1	2.80	1	2.58
7	313.05	1	.	1	0	1	313	0	2.33	1	12.78
7	314.05	1	.	1	0	1	314	1	2.33	2	12.78
7	315.05	1	0	1	0	1	314	1	2.33	2	73.98
7	316.05	1	0	1	0	1	314	1	2.49	2	12.78
7	317.05	1	0	1	0	1	312	1	2.64	1	12.78
7	318.05	1	0	1	0	1	314	1	2.33	2	73.98
7	319.05	1	0	1	0	1	314	1	2.80	2	73.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	255.05	165.36	0.43	2.31	0.43	2.31	1	1	0	2.18
7	256.05	213.31	0.40	2.48	0.40	2.48	1	4	0	2.31
7	258.05	218.98	0.41	2.45	0.41	2.45	1	2	0	2.48
7	260.05	176.27	0.40	2.49	0.40	2.49	0		1	.
7	261.05	170.13	0.41	2.43	0.41	2.43	1	2	0	2.49
7	262.05	221.78	0.40	2.49	0.40	2.49	1	4	0	2.48
7	264.05	169.07	0.41	2.45	0.41	2.45	1	2	0	2.49
7	265.05	173.54	0.37	2.68	0.37	2.68	1	3	0	2.49
7	266.05	171.44	0.37	2.72	0.37	2.72	1	3	0	2.49
7	267.05	174.67	0.37	2.71	0.37	2.71	1	3	0	2.49
7	268.05	304.30	0.36	2.79	0.36	2.79	1	4	0	2.49
7	270.05	423.06	0.35	2.85	0.36	2.79	0		0	.
7	273.05	309.54	0.35	2.83	0.36	2.79	0		1	.
7	276.05	118.85	0.36	2.76	0.36	2.76	1	2	0	2.91
7	277.05	83.52	0.36	2.79	0.36	2.76	0		1	.
7	278.05	236.83	0.36	2.80	0.36	2.79	0		0	.
7	280.05	229.26	0.34	2.91	0.34	2.91	1	4	0	2.79
7	282.05	195.63	0.37	2.71	0.36	2.76	0		0	.
7	283.05	196.86	0.36	2.81	0.36	2.76	0		0	.
7	284.05	88.66	0.35	2.85	0.36	2.76	0		0	.
7	285.05	244.24	0.34	2.95	0.34	2.95	1	3	0	2.91
7	287.05	122.25	0.34	2.95	0.34	2.95	0		1	.
7	288.05	264.36	0.34	2.93	0.34	2.91	0		0	.
7	290.05	352.55	0.33	3.03	0.34	2.98	0		1	.
7	293.05	192.86	0.33	3.07	0.34	2.98	0		0	.
7	294.05	202.27	0.33	3.02	0.34	2.98	0		0	.
7	295.05	154.99	0.34	2.92	0.34	2.91	0		1	.
7	296.05	208.61	0.35	2.88	0.35	2.88	1	1	0	2.91
7	297.05	93.93	0.35	2.85	0.35	2.85	1	2	0	2.91
7	298.05	123.79	0.34	2.94	0.34	2.94	1	3	0	2.91
7	299.05	124.69	0.33	2.99	0.33	2.99	1	4	0	2.88
7	300.05	92.16	0.32	3.11	0.32	3.11	1	4	0	2.99
7	301.05	94.56	0.34	2.95	0.33	2.99	0		1	.
7	302.05	188.42	0.33	3.06	0.33	3.06	1	2	0	3.11
7	303.05	216.55	0.34	2.98	0.34	2.98	1	3	0	2.91
7	304.05	215.21	0.31	3.19	0.33	3.06	0		0	.
7	305.05	100.64	0.32	3.17	0.33	3.06	0		1	.
7	306.05	97.13	0.31	3.18	0.31	3.21	0		1	.
7	307.05	102.00	0.31	3.21	0.31	3.21	1	2	0	3.11
7	308.05	102.94	0.31	3.18	0.31	3.21	0		0	.
7	309.05	103.57	0.31	3.18	0.31	3.21	0		0	.
7	310.05	402.73	0.28	3.54	0.28	3.54	1	3	0	3.42
7	312.05	212.31	0.30	3.32	0.30	3.32	1	3	0	3.11
7	313.05	237.23	0.29	3.42	0.29	3.42	1	3	0	3.11
7	314.05	108.44	0.30	3.33	0.30	3.33	1	2	0	3.41
7	315.05	242.74	0.30	3.36	0.30	3.33	0		1	.
7	316.05	215.41	0.29	3.48	0.30	3.33	0		0	.
7	317.05	110.61	0.30	3.33	0.30	3.32	0		1	.
7	318.05	111.91	0.28	3.53	0.30	3.33	0		0	.
7	319.05	130.26	0.28	3.61	0.30	3.33	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	320.05	1	0	1	0	1	312	1	2.64	1	53.58
7	321.05	1	0	0	1	1	314	1	2.80	2	63.78
7	322.05	1	.	1	0	1	322	0	2.80	1	12.78
7	323.05	1	0	1	0	1	312	1	2.95	1	73.98
7	324.05	1	0	1	0	1	314	1	2.33	2	63.78
7	325.05	0	1	0	0	2	314	1	2.33	2	63.78
7	326.05	1	1	1	0	1	314	1	2.64	2	73.98
7	328.05	0	1	0	0	1	338	1	2.49	1	63.78
7	329.05	0	1	0	0	1	314	1	2.80	2	73.98
7	330.05	0	0	0	1	1	314	1	2.95	2	73.98
7	331.05	1	1	1	0	1	314	1	3.11	2	73.98
7	332.05	0	1	0	1	1	314	1	3.11	2	73.98
7	334.05	0	1	1	0	1	312	1	2.49	1	12.78
7	335.05	1	1	1	0	1	314	1	2.64	2	63.78
7	336.05	0	.	1	0	1	336	0	2.64	1	53.58
7	337.05	0	.	0	0	1	337	0	2.95	1	53.58
7	338.05	1	.	0	0	1	338	1	2.64	1	63.78
7	339.05	1	0	1	0	1	314	1	2.95	2	73.98
7	340.05	1	.	1	0	1	340	1	2.49	1	73.98
7	341.05	1	0	1	0	1	314	1	3.11	2	73.98
7	342.05	1	0	1	0	1	314	1	2.64	2	63.78
7	343.05	1	.	1	0	1	343	0	1.87	2	43.38
7	344.05	0	1	1	0	1	343	0	1.87	2	43.38
7	345.05	1	0	1	1	1	314	1	2.33	2	73.98
7	346.05	1	0	1	0	1	340	1	2.49	1	12.78
7	347.05	0	1	0	0	1	314	1	2.33	2	73.98
7	349.05	1	1	1	0	1	314	1	2.33	2	73.98
7	350.05	1	.	1	0	1	350	1	2.49	1	12.78
7	351.05	0	.	1	0	2	351	1	2.49	0	63.78
7	352.05	1	0	1	0	1	350	1	2.80	1	73.98
7	353.05	0	.	1	0	1	353	1	2.18	2	104.58
7	354.05	0	1	0	0	1	350	1	2.49	1	12.78
7	355.05	0	0	1	0	1	353	1	2.64	2	94.38
7	356.05	0	0	1	0	1	353	1	2.80	2	43.38
7	358.05	0	0	0	0	1	353	1	2.64	2	104.58
7	361.05	1	1	1	1	1	362	1	2.64	1	63.78
7	362.05	0	.	0	0	1	362	1	2.80	1	12.78
7	363.05	0	1	1	0	1	366	1	2.64	1	63.78
7	365.05	1	1	1	0	1	362	1	2.64	1	2.58
7	366.05	1	.	1	0	1	366	1	2.18	1	63.78
7	367.05	1	0	1	0	1	362	1	2.49	1	2.58
7	368.05	1	0	1	0	1	362	1	2.95	1	2.58
7	369.05	1	0	1	0	1	362	1	2.95	1	12.78
7	370.05	0	1	0	0	1	362	1	3.11	1	63.78
7	371.05	1	0	1	0	1	362	1	2.95	1	12.78
7	372.05	1	1	1	0	1	381	0	2.33	2	73.98
7	373.05	0	0	0	0	1	362	1	2.80	1	73.98
7	374.05	1	1	1	0	1	362	1	2.80	1	12.78
7	375.05	0	1	0	0	1	362	1	2.80	1	73.98
7	376.05	1	1	1	0	1	362	1	2.95	1	12.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	320.05	116.75	0.30	3.31	0.30	3.32	0		0	.
7	321.05	231.20	0.28	3.60	0.30	3.33	0		0	.
7	322.05	96.73	0.29	3.41	0.29	3.41	1	2	0	3.42
7	323.05	111.45	0.30	3.35	0.30	3.32	0		0	.
7	324.05	113.08	0.28	3.63	0.30	3.33	0		0	.
7	325.05	115.88	0.27	3.70	0.30	3.33	0		0	.
7	326.05	306.54	0.26	3.84	0.30	3.33	0		0	.
7	328.05	124.43	0.28	3.58	0.29	3.50	0		1	.
7	329.05	125.89	0.27	3.70	0.30	3.33	0		0	.
7	330.05	129.10	0.27	3.70	0.30	3.33	0		0	.
7	331.05	131.00	0.27	3.73	0.30	3.33	0		0	.
7	332.05	360.16	0.27	3.73	0.30	3.33	0		0	.
7	334.05	132.83	0.30	3.39	0.30	3.32	0		0	.
7	335.05	131.99	0.27	3.73	0.30	3.33	0		0	.
7	336.05	133.36	0.29	3.42	0.29	3.42	1	1	0	3.11
7	337.05	98.23	0.29	3.41	0.29	3.41	1	1	0	3.42
7	338.05	110.18	0.29	3.50	0.29	3.50	1	3	0	3.41
7	339.05	104.31	0.27	3.71	0.30	3.33	0		0	.
7	340.05	122.46	0.28	3.62	0.28	3.62	1	3	0	3.41
7	341.05	129.33	0.27	3.72	0.30	3.33	0		0	.
7	342.05	81.31	0.28	3.59	0.30	3.33	0		0	.
7	343.05	76.81	0.34	2.91	0.34	2.91	1	1	0	2.91
7	344.05	132.13	0.35	2.89	0.34	2.91	0		0	.
7	345.05	243.87	0.32	3.09	0.30	3.33	0		0	.
7	346.05	135.04	0.27	3.64	0.28	3.62	0		1	.
7	347.05	315.48	0.32	3.10	0.30	3.33	0		0	.
7	349.05	248.51	0.32	3.13	0.30	3.33	0		0	.
7	350.05	125.03	0.26	3.78	0.26	3.78	1	3	0	3.41
7	351.05	106.61	0.25	4.05	0.25	4.05	1	1	0	3.41
7	352.05	62.80	0.26	3.82	0.26	3.78	0		1	.
7	353.05	251.82	0.30	3.30	0.30	3.30	1	2	0	4.05
7	354.05	101.67	0.26	3.84	0.26	3.78	0		0	.
7	355.05	184.61	0.30	3.33	0.30	3.30	0		1	.
7	356.05	328.86	0.29	3.43	0.30	3.30	0		0	.
7	358.05	331.03	0.27	3.69	0.30	3.30	0		0	.
7	361.05	255.19	0.24	4.16	0.23	4.41	0		0	.
7	362.05	130.93	0.23	4.41	0.23	4.41	1	3	0	3.41
7	363.05	379.24	0.28	3.61	0.25	4.05	0		0	.
7	365.05	127.06	0.23	4.41	0.23	4.41	0		1	.
7	366.05	263.79	0.25	4.05	0.25	4.05	1	3	0	4.05
7	367.05	267.60	0.22	4.47	0.23	4.41	0		0	.
7	368.05	266.60	0.24	4.19	0.23	4.41	0		0	.
7	369.05	115.05	0.24	4.19	0.23	4.41	0		0	.
7	370.05	277.11	0.24	4.17	0.23	4.41	0		0	.
7	371.05	139.07	0.24	4.12	0.23	4.41	0		0	.
7	372.05	114.52	0.27	3.77	0.27	3.77	0		1	.
7	373.05	273.54	0.24	4.15	0.23	4.41	0		0	.
7	374.05	118.09	0.24	4.14	0.23	4.41	0		0	.
7	375.05	281.95	0.24	4.11	0.23	4.41	0		0	.
7	376.05	294.02	0.24	4.13	0.23	4.41	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	377.05	1	0	1	0	1	366	1	2.33	1	12.78
7	378.05	1	0	1	0	1	379	1	2.80	1	63.78
7	379.05	1	.	1	0	1	379	1	2.49	1	63.78
7	380.05	0	1	0	0	1	362	1	2.64	1	12.78
7	381.05	0	.	0	0	2	381	0	2.33	1	12.78
7	382.05	1	0	1	0	1	379	1	2.33	1	12.78
7	383.05	1	0	0	0	1	381	0	2.33	2	114.78
7	384.05	0	1	1	0	1	381	0	2.64	2	104.58
7	385.05	0	.	1	0	1	385	0	2.49	2	63.78
7	386.05	1	0	0	0	1	381	0	2.33	1	12.78
7	387.05	1	0	1	0	1	381	0	2.64	1	12.78
7	388.05	1	0	0	0	1	393	0	2.18	2	33.18
7	389.05	1	1	1	0	1	381	0	2.64	1	12.78
7	390.05	1	0	1	1	1	393	0	2.49	2	53.58
7	391.05	0	.	1	0	1	391	0	2.49	1	63.78
7	392.05	1	0	1	0	1	393	0	2.80	2	84.18
7	393.05	1	.	1	0	1	393	0	2.64	1	63.78
7	394.05	0	1	1	0	1	393	0	2.49	1	33.18
7	395.05	1	1	1	0	1	393	0	2.49	1	33.18
7	396.05	1	.	1	1	1	396	1	2.49	2	63.78
7	397.05	1	.	1	1	1	397	0	2.49	2	63.78
7	398.05	0	.	0	0	1	396	1	2.64	2	43.38
7	399.05	1	0	1	0	1	393	0	2.80	1	12.78
7	400.05	1	1	0	0	1	396	1	2.95	2	43.38
7	401.05	1	0	1	0	1	393	0	2.80	1	33.18
7	402.05	1	.	1	0	1	402	0	2.64	1	33.18
7	403.05	0	.	1	0	1	403	0	2.64	1	73.98
7	404.05	0	1	1	0	1	405	1	2.64	1	33.18
7	405.05	1	.	0	0	1	405	1	2.49	1	33.18
7	406.05	0	0	1	0	1	405	1	2.80	1	104.58
7	407.05	1	0	1	0	1	408	0	2.64	1	12.78
7	408.05	1	.	1	0	1	408	0	2.64	1	12.78
7	409.05	1	0	1	0	1	408	0	2.64	1	73.98
7	410.05	0	1	0	0	1	408	0	2.02	1	73.98
7	411.05	0	0	1	0	1	408	0	1.71	1	73.98
7	412.05	1	1	1	0	1	408	0	2.02	1	73.98
7	413.05	0	1	0	0	2	408	0	1.87	1	73.98
7	414.05	1	1	1	0	2	408	0	1.87	1	2.58
7	415.05	0	1	0	0	2	408	0	1.71	1	73.98
7	416.05	0	0	0	0	1	408	0	1.87	1	73.98
7	417.05	0	0	0	0	1	408	0	1.87	2	73.98
7	418.05	0	0	1	1	2	408	0	1.55	2	84.18
7	419.05	1	1	1	0	1	408	0	1.87	1	73.98
7	420.05	1	0	1	0	1	408	0	2.02	2	84.18
7	421.05	1	0	1	0	1	408	0	1.87	1	84.18
7	422.05	1	0	1	0	1	408	0	2.18	2	104.58
7	423.05	1	0	1	0	1	408	0	2.02	1	84.18
7	424.05	1	0	0	0	1	408	0	2.02	1	104.58
7	425.05	1	0	1	0	1	408	0	2.33	2	114.78
7	426.05	1	0	1	0	1	408	0	2.18	1	114.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	377.05	135.30	0.25	4.02	0.25	4.05	0		1	.
7	378.05	137.67	0.27	3.77	0.27	3.72	0		1	.
7	379.05	283.65	0.27	3.72	0.27	3.72	1	3	0	4.05
7	380.05	318.42	0.24	4.14	0.23	4.41	0		0	.
7	381.05	300.66	0.27	3.77	0.27	3.77	1	1	0	3.85
7	382.05	98.03	0.26	3.82	0.27	3.72	0		0	.
7	383.05	77.98	0.26	3.79	0.27	3.77	0		0	.
7	384.05	148.08	0.26	3.86	0.27	3.77	0		0	.
7	385.05	322.72	0.24	4.16	0.24	4.16	1	3	0	3.77
7	386.05	323.42	0.27	3.76	0.27	3.77	0		0	.
7	387.05	249.68	0.27	3.76	0.27	3.77	0		0	.
7	388.05	326.06	0.24	4.22	0.25	4.08	0		1	.
7	389.05	195.73	0.25	3.97	0.27	3.77	0		0	.
7	390.05	141.28	0.24	4.19	0.25	4.08	0		0	.
7	391.05	116.98	0.25	3.99	0.25	3.99	1	2	0	3.77
7	392.05	145.65	0.24	4.09	0.25	4.08	0		0	.
7	393.05	248.98	0.25	4.08	0.25	4.08	1	1	0	3.77
7	394.05	251.22	0.25	4.08	0.25	4.08	0		0	.
7	395.05	154.39	0.24	4.08	0.25	4.08	0		0	.
7	396.05	151.39	0.26	3.82	0.26	3.82	1	2	0	4.08
7	397.05	205.27	0.26	3.80	0.26	3.80	1	2	0	4.08
7	398.05	337.00	0.26	3.86	0.26	3.82	1	0	1	.
7	399.05	203.33	0.25	4.07	0.25	4.08	0		0	.
7	400.05	252.32	0.26	3.84	0.26	3.82	0		0	.
7	401.05	255.65	0.25	4.08	0.25	4.08	0		0	.
7	402.05	113.01	0.25	3.95	0.25	3.95	1	3	0	4.08
7	403.05	264.10	0.11	8.95	0.11	8.95	1	3	0	.
7	404.05	261.16	0.25	3.97	0.25	3.94	0		1	.
7	405.05	37.70	0.25	3.94	0.25	3.94	1	3	0	4.08
7	406.05	353.82	0.25	3.97	0.25	3.94	0		0	.
7	407.05	351.25	0.25	3.93	0.25	3.96	0		1	.
7	408.05	150.29	0.25	3.96	0.25	3.96	1	1	0	4.08
7	409.05	152.42	0.26	3.90	0.25	3.96	0		0	.
7	410.05	154.76	0.25	3.93	0.25	3.96	0		0	.
7	411.05	156.76	0.25	3.94	0.25	3.96	0		0	.
7	412.05	160.46	0.26	3.92	0.25	3.96	0		0	.
7	413.05	379.38	0.26	3.88	0.25	3.96	0		0	.
7	414.05	162.26	0.26	3.90	0.25	3.96	0		0	.
7	415.05	163.93	0.26	3.90	0.25	3.96	0		0	.
7	416.05	165.13	0.25	3.95	0.25	3.96	0		0	.
7	417.05	117.92	0.25	3.96	0.25	3.96	0		0	.
7	418.05	167.60	0.25	3.94	0.25	3.96	0		0	.
7	419.05	122.12	0.25	3.94	0.25	3.96	0		0	.
7	420.05	123.06	0.26	3.92	0.25	3.96	0		0	.
7	421.05	99.27	0.25	3.94	0.25	3.96	0		0	.
7	422.05	124.16	0.26	3.82	0.25	3.96	0		0	.
7	423.05	100.87	0.25	3.92	0.25	3.96	0		0	.
7	424.05	102.97	0.26	3.85	0.25	3.96	0		0	.
7	425.05	101.27	0.26	3.77	0.25	3.96	0		0	.
7	426.05	86.28	0.27	3.77	0.25	3.96	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	427.05	1	.	1	1	1	427	1	2.64	2	124.98
7	428.05	0	.	1	0	1	428	1	2.18	1	114.78
7	429.05	1	1	1	0	1	428	1	2.49	1	114.78
7	430.05	1	0	1	0	1	427	1	2.18	2	124.98
7	431.05	1	0	1	0	1	427	1	2.18	2	124.98
7	432.05	1	0	1	0	1	428	1	2.49	1	2.58
7	433.05	0	1	0	0	1	427	1	2.95	2	124.98
7	434.05	0	1	0	0	1	428	1	2.18	1	12.78
7	435.05	0	0	1	0	1	437	0	3.11	2	94.38
7	436.05	0	0	1	0	1	428	1	2.33	1	73.98
7	437.05	0	.	0	0	1	437	0	2.64	1	73.98
7	438.05	1	0	0	0	1	437	0	2.64	2	124.98
7	439.05	1	1	1	0	1	437	0	2.80	1	73.98
7	440.05	0	1	0	0	1	437	0	2.49	2	104.58
7	441.05	0	1	1	0	1	437	0	2.64	2	63.78
7	442.05	1	1	1	0	1	437	0	2.49	1	94.38
7	443.05	1	.	1	0	1	443	1	2.02	2	145.38
7	444.05	1	0	1	0	1	443	1	2.18	2	145.38
7	445.05	1	0	1	0	1	443	1	2.18	2	73.98
7	446.05	1	0	1	0	1	443	1	2.33	2	124.98
7	447.05	1	0	1	0	1	437	0	2.49	1	12.78
7	448.05	0	1	0	1	1	443	1	2.18	2	124.98
7	449.05	1	0	0	0	1	437	0	2.64	1	12.78
7	450.05	0	.	0	0	1	450	1	2.80	1	12.78
7	451.05	0	0	0	0	1	443	1	2.02	2	124.98
7	452.05	0	0	1	0	1	450	1	2.95	1	124.98
7	453.05	1	1	1	0	1	450	1	2.64	1	53.58
7	454.05	1	1	1	0	1	443	1	2.18	2	135.18
7	455.05	1	0	1	0	1	450	1	2.49	1	63.78
7	456.05	1	0	1	0	1	443	1	2.18	2	114.78
7	457.05	0	1	1	0	1	450	1	2.18	1	145.38
7	458.05	0	1	1	0	1	459	0	1.87	1	73.98
7	459.05	1	.	1	0	2	459	0	1.87	1	73.98
7	460.05	1	1	0	0	1	450	1	2.18	1	63.78
7	461.05	1	0	1	0	1	450	1	2.18	1	63.78
7	462.05	1	.	1	0	1	462	0	1.71	1	63.78
7	463.05	0	1	0	0	1	450	1	2.02	1	63.78
7	464.05	0	0	1	0	1	450	1	2.18	1	124.98
7	465.05	0	0	0	0	1	450	1	2.02	1	145.38
7	466.05	1	.	1	0	1	466	1	2.02	1	63.78
7	467.05	1	.	0	0	1	467	0	1.87	0	63.78
7	468.05	0	.	1	0	1	468	0	1.71	1	73.98
7	470.05	1	.	1	0	1	470	0	1.87	2	145.38
7	472.05	0	.	0	0	1	472	0	2.18	2	63.78
7	473.05	0	.	1	0	1	473	0	2.18	0	63.78
7	474.05	1	1	1	0	1	472	0	2.33	1	12.78
7	475.05	1	0	1	0	1	472	0	2.18	2	114.78
7	476.05	1	0	0	0	1	472	0	2.18	1	53.58
7	477.05	1	.	1	0	1	477	0	2.18	2	114.78
7	478.05	1	.	1	0	1	478	0	2.33	1	114.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	427.05	106.01	0.25	3.94	0.25	3.94	1	3	0	3.96
7	428.05	107.98	0.27	3.70	0.27	3.70	1	2	0	3.96
7	429.05	87.85	0.25	3.93	0.27	3.70	0		1	.
7	430.05	88.82	0.25	3.99	0.25	3.94	0		1	.
7	431.05	409.47	0.25	3.99	0.25	3.94	0		0	.
7	432.05	89.32	0.25	3.93	0.27	3.70	0		0	.
7	433.05	407.20	0.25	4.07	0.25	3.94	0		0	.
7	434.05	152.82	0.25	3.96	0.27	3.70	0		0	.
7	435.05	181.68	0.27	3.77	0.26	3.78	0		1	.
7	436.05	183.92	0.26	3.89	0.27	3.70	0		0	.
7	437.05	94.13	0.26	3.78	0.26	3.78	1	1	0	3.96
7	438.05	185.79	0.27	3.75	0.26	3.78	0		0	.
7	439.05	66.70	0.27	3.76	0.26	3.78	0		0	.
7	440.05	199.17	0.27	3.76	0.26	3.78	0		0	.
7	441.05	152.39	0.27	3.72	0.26	3.78	0		0	.
7	442.05	66.33	0.27	3.72	0.26	3.78	0		0	.
7	443.05	62.99	0.31	3.26	0.31	3.26	1	2	0	3.78
7	444.05	202.70	0.33	3.04	0.31	3.26	0		0	.
7	445.05	105.17	0.32	3.12	0.31	3.26	0		1	.
7	446.05	422.35	0.33	3.03	0.31	3.26	0		0	.
7	447.05	110.47	0.27	3.75	0.26	3.78	0		0	.
7	448.05	423.79	0.33	3.05	0.31	3.26	0		0	.
7	449.05	426.79	0.27	3.73	0.26	3.78	0		0	.
7	450.05	111.61	0.26	3.78	0.26	3.78	1	3	0	3.78
7	451.05	98.26	0.33	3.06	0.31	3.26	0		0	.
7	452.05	245.41	0.28	3.61	0.26	3.78	0		1	.
7	453.05	112.94	0.28	3.59	0.26	3.78	0		0	.
7	454.05	197.53	0.33	3.04	0.31	3.26	0		0	.
7	455.05	144.24	0.29	3.46	0.26	3.78	0		0	.
7	456.05	64.56	0.33	3.03	0.31	3.26	0		0	.
7	457.05	214.35	0.30	3.34	0.26	3.78	0		0	.
7	458.05	211.48	0.32	3.17	0.31	3.24	0		1	.
7	459.05	202.40	0.31	3.24	0.31	3.24	1	0	0	3.29
7	460.05	204.74	0.30	3.32	0.26	3.78	0		0	.
7	461.05	220.79	0.30	3.29	0.26	3.78	0		0	.
7	462.05	206.41	0.33	3.07	0.33	3.07	1	2	0	3.24
7	463.05	99.93	0.30	3.31	0.26	3.78	0		0	.
7	464.05	73.67	0.31	3.23	0.26	3.78	0		0	.
7	465.05	214.15	0.30	3.29	0.26	3.78	0		0	.
7	466.05	224.13	0.30	3.29	0.30	3.29	1	0	0	3.78
7	467.05	215.25	0.32	3.09	0.32	3.09	1	2	0	3.24
7	468.05	590.76	0.32	3.15	0.32	3.15	1	3	0	3.24
7	470.05	592.06	0.30	3.35	0.30	3.35	1	3	0	3.24
7	472.05	225.56	0.32	3.17	0.32	3.17	1	1	0	3.20
7	473.05	476.01	0.31	3.20	0.31	3.20	1	1	0	3.24
7	474.05	153.92	0.31	3.18	0.32	3.17	0		1	.
7	475.05	289.05	0.32	3.15	0.32	3.17	0		0	.
7	476.05	152.45	0.31	3.22	0.32	3.17	0		0	.
7	477.05	154.49	0.31	3.18	0.31	3.18	1	2	0	3.26
7	478.05	149.82	0.31	3.26	0.31	3.26	1	3	0	3.26

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	479.05	0	.	0	0	1	479	0	2.33	1	114.78
7	480.05	1	.	0	0	1	480	0	2.02	1	43.38
7	481.05	0	1	0	0	2	480	0	1.87	2	43.38
7	482.05	0	0	1	0	1	480	0	2.33	2	114.78
7	483.05	0	0	1	0	1	480	0	2.18	1	84.18
7	484.05	0	0	0	0	1	480	0	2.02	1	124.98
7	485.05	1	1	1	0	1	480	0	2.33	2	145.38
7	486.05	1	0	0	1	1	480	0	2.18	1	104.58
7	487.05	0	1	0	1	1	480	0	2.64	2	114.78
7	488.05	1	0	1	0	1	480	0	2.33	1	124.98
7	489.05	0	1	0	0	1	480	0	2.33	2	145.38
7	490.05	1	1	1	0	1	480	0	2.33	1	124.98
7	491.05	0	1	1	0	1	480	0	2.49	2	145.38
7	492.05	0	0	1	0	1	480	0	2.64	1	124.98
7	493.05	0	.	1	0	1	493	1	2.33	2	145.38
7	494.05	1	.	0	0	1	494	1	2.18	2	145.38
7	495.05	1	1	1	0	1	480	0	2.49	1	73.98
7	496.05	1	.	0	0	1	496	0	2.18	1	43.38
7	497.05	1	1	1	0	1	480	0	2.33	1	124.98
7	498.05	0	.	0	1	1	498	1	2.33	1	135.18
7	499.05	1	.	1	0	1	499	1	2.33	2	145.38
7	500.05	1	.	1	0	1	500	1	2.33	1	145.38
7	501.05	1	.	1	0	1	501	1	2.18	1	104.58
7	502.05	0	1	0	0	1	496	0	2.18	2	104.58
7	503.05	1	1	1	0	1	496	0	2.02	1	124.98
7	504.05	0	0	0	0	1	496	0	2.02	2	124.98
7	505.05	0	1	0	0	2	496	0	2.18	1	145.38
7	506.05	0	0	1	0	1	496	0	1.71	2	145.38
7	507.05	1	.	1	0	1	507	0	1.55	1	135.18
7	508.05	0	.	1	0	1	508	0	1.87	2	135.18
7	509.05	1	1	1	0	1	510	0	1.55	2	145.38
7	510.05	0	.	1	0	1	510	0	1.55	2	135.18
7	511.05	1	.	0	0	1	511	1	1.87	2	145.38
7	512.05	1	0	1	0	1	511	1	1.87	2	175.99
7	513.05	1	0	1	0	1	511	1	2.02	2	145.38
7	514.05	1	0	1	0	1	511	1	2.18	2	135.18
7	515.05	1	0	1	0	1	511	1	2.18	2	135.18
7	516.05	0	.	0	1	1	516	1	2.18	0	43.38
7	517.05	1	0	1	1	1	511	1	2.18	2	135.18
7	518.05	1	1	1	0	1	527	1	2.02	1	175.99
7	519.05	0	.	1	1	1	519	1	2.33	2	135.18
7	520.05	1	1	1	0	1	519	1	2.33	2	135.18
7	521.05	1	0	1	0	2	519	1	2.49	2	73.98
7	522.05	1	.	1	0	1	522	1	2.49	2	73.98
7	523.05	1	0	1	0	1	522	1	2.33	0	73.98
7	524.05	0	.	1	0	1	524	0	1.55	2	175.99
7	525.05	0	.	1	0	1	525	0	1.71	0	175.99
7	526.05	0	0	1	0	1	534	1	2.49	1	43.38
7	527.05	1	.	1	0	1	527	1	1.24	1	12.78
7	528.05	0	1	1	0	1	527	1	1.87	1	12.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	479.05	300.56	0.31	3.26	0.31	3.26	1	0	0	3.17
7	480.05	302.43	0.31	3.20	0.31	3.20	1	1	0	3.26
7	481.05	160.79	0.32	3.17	0.31	3.20	0		1	.
7	482.05	184.35	0.32	3.17	0.31	3.20	0		0	.
7	483.05	127.22	0.31	3.18	0.31	3.20	0		0	.
7	484.05	115.35	0.32	3.16	0.31	3.20	0		0	.
7	485.05	156.16	0.32	3.13	0.31	3.20	0		0	.
7	486.05	162.66	0.32	3.14	0.31	3.20	0		0	.
7	487.05	129.86	0.32	3.12	0.31	3.20	0		0	.
7	488.05	110.27	0.32	3.11	0.31	3.20	0		0	.
7	489.05	131.80	0.32	3.09	0.31	3.20	0		0	.
7	490.05	118.58	0.32	3.09	0.31	3.20	0		0	.
7	491.05	132.73	0.33	2.99	0.31	3.20	0		0	.
7	492.05	112.94	0.33	3.04	0.31	3.20	0		0	.
7	493.05	111.21	0.40	2.50	0.40	2.50	1	2	0	3.20
7	494.05	240.51	0.39	2.57	0.39	2.57	1	1	0	3.20
7	495.05	360.96	0.33	3.05	0.31	3.20	0		0	.
7	496.05	134.83	0.40	2.52	0.40	2.52	1	1	0	2.55
7	497.05	133.66	0.33	3.05	0.31	3.20	0		0	.
7	498.05	122.62	0.34	2.96	0.34	2.96	1	3	0	3.20
7	499.05	116.98	0.40	2.47	0.40	2.47	1	2	0	2.55
7	500.05	162.56	0.39	2.53	0.39	2.53	1	3	0	2.55
7	501.05	172.41	0.39	2.55	0.39	2.55	1	1	0	2.57
7	502.05	140.84	0.40	2.48	0.40	2.52	0		1	.
7	503.05	144.61	0.40	2.48	0.40	2.52	0		0	.
7	504.05	123.22	0.40	2.50	0.40	2.52	0		0	.
7	505.05	124.52	0.40	2.49	0.40	2.52	0		0	.
7	506.05	153.78	0.40	2.48	0.40	2.52	0		0	.
7	507.05	152.85	0.42	2.38	0.42	2.38	1	2	0	2.52
7	508.05	135.43	0.41	2.44	0.41	2.44	1	3	0	2.52
7	509.05	155.35	0.42	2.37	0.41	2.46	0		1	.
7	510.05	136.57	0.41	2.46	0.41	2.46	1	1	0	2.52
7	511.05	111.84	0.43	2.31	0.43	2.31	1	2	0	2.46
7	512.05	138.27	0.44	2.26	0.43	2.31	0		1	.
7	513.05	171.10	0.44	2.27	0.43	2.31	0		0	.
7	514.05	174.17	0.44	2.27	0.43	2.31	0		0	.
7	515.05	397.76	0.47	2.15	0.43	2.31	0		0	.
7	516.05	167.53	0.45	2.21	0.45	2.21	1	2	0	2.46
7	517.05	110.71	0.45	2.25	0.43	2.31	0		0	.
7	518.05	175.24	0.39	2.54	0.39	2.57	0		0	.
7	519.05	169.67	0.44	2.27	0.44	2.27	1	2	0	2.46
7	520.05	315.58	0.44	2.26	0.44	2.27	0		1	.
7	521.05	313.42	0.46	2.19	0.44	2.27	0		0	.
7	522.05	312.51	0.46	2.17	0.46	2.17	1	2	0	2.46
7	523.05	115.48	0.43	2.30	0.46	2.17	0		1	.
7	524.05	114.05	0.46	2.19	0.46	2.19	1	2	0	2.39
7	525.05	401.53	0.44	2.27	0.44	2.27	1	1	0	2.39
7	526.05	538.54	0.41	2.42	0.39	2.59	0		0	.
7	527.05	540.04	0.39	2.57	0.39	2.57	1	3	0	2.46
7	528.05	653.82	0.39	2.55	0.39	2.57	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	530.05	1	1	1	0	1	534	1	2.33	1	104.58
7	531.05	0	1	0	0	1	527	1	2.02	1	104.58
7	532.05	1	.	1	0	2	532	0	2.18	1	104.58
7	533.05	0	0	1	0	1	527	1	2.18	1	145.38
7	534.05	0	.	0	0	1	534	1	2.33	1	145.38
7	535.05	1	0	1	0	1	534	1	2.18	1	135.18
7	536.05	1	0	1	0	1	534	1	2.02	1	94.38
7	537.05	0	1	1	0	1	534	1	2.33	1	135.18
7	538.05	0	.	0	0	1	538	1	2.49	1	135.18
7	539.05	1	1	1	0	1	538	1	2.80	1	135.18
7	540.05	1	.	1	0	1	540	0	1.40	1	84.18
7	541.05	1	0	1	0	1	532	0	1.87	1	84.18
7	542.05	1	1	1	0	1	525	0	1.87	1	175.99
7	543.05	1	0	1	0	1	525	0	2.02	1	124.98
7	544.05	1	0	1	0	1	525	0	2.18	1	175.99
7	545.05	1	0	1	0	1	525	0	2.18	2	175.99
7	546.05	0	0	0	0	1	525	0	2.02	2	175.99
7	547.05	0	1	0	0	1	525	0	2.18	1	94.38
7	548.05	0	0	1	0	1	525	0	2.02	1	94.38
7	549.05	1	1	1	0	1	525	0	2.02	2	73.98
7	550.05	1	0	1	0	1	525	0	2.18	2	73.98
7	551.05	1	0	1	0	1	525	0	1.87	1	73.98
7	552.05	1	.	1	0	1	552	0	1.71	2	114.78
7	553.05	0	.	1	0	1	553	0	1.87	1	104.58
7	554.05	1	.	1	0	1	554	0	1.71	1	53.58
7	555.05	1	.	1	0	1	555	1	1.87	2	124.98
7	556.05	1	.	1	0	1	556	1	1.87	1	135.18
7	557.05	0	.	1	0	1	557	0	1.71	1	94.38
7	558.05	0	.	0	0	1	558	1	1.87	1	94.38
7	559.05	1	.	0	0	1	559	1	2.02	0	175.99
7	560.05	0	.	1	0	1	560	1	1.55	1	94.38
7	561.05	1	.	1	0	1	561	1	2.33	1	135.18
7	562.05	0	0	0	0	2	560	1	1.87	1	73.98
7	563.05	0	.	0	0	2	563	0	1.71	1	124.98
7	564.05	1	0	1	0	1	565	0	0.93	1	135.18
7	565.05	1	.	1	0	.	565	0	0.93	1	124.98
7	566.05	1	0	0	0	1	565	0	1.24	1	175.99
7	567.05	1	0	1	0	1	565	0	1.24	1	175.99
7	568.05	0	.	1	0	2	568	0	1.55	1	84.18
7	569.05	0	0	1	0	1	568	0	1.55	2	114.78
7	570.05	0	0	0	0	2	568	0	1.55	1	84.18
7	571.05	1	1	1	0	1	574	0	1.71	2	175.99
7	572.05	0	0	1	0	2	568	0	1.71	1	135.18
7	573.05	1	.	0	0	1	573	1	1.87	2	175.99
7	574.05	0	.	1	0	3	574	0	1.71	1	175.99
7	575.05	0	1	1	0	2	373	1	2.18	2	175.99
7	576.05	1	.	1	0	1	576	1	1.71	1	175.99
7	577.05	1	0	1	0	1	574	0	1.87	1	175.99
7	578.05	1	.	0	0	1	578	1	2.02	0	175.99
7	579.05	1	.	1	0	2	579	1	1.87	1	175.99

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	530.05	188.96	0.39	2.56	0.39	2.59	0		1	.
7	531.05	215.75	0.39	2.56	0.39	2.57	0		0	.
7	532.05	95.29	0.42	2.39	0.42	2.39	1	1	0	2.46
7	533.05	96.63	0.39	2.59	0.39	2.57	0		0	.
7	534.05	163.23	0.39	2.59	0.39	2.59	1	3	0	2.46
7	535.05	234.60	0.41	2.46	0.39	2.59	0		0	.
7	536.05	164.46	0.40	2.51	0.39	2.59	0		0	.
7	537.05	165.80	0.41	2.43	0.39	2.59	0		0	.
7	538.05	172.77	0.42	2.41	0.42	2.41	1	3	0	2.46
7	539.05	254.05	0.41	2.43	0.42	2.41	0		1	.
7	540.05	252.09	0.43	2.31	0.43	2.31	1	3	0	2.39
7	541.05	118.18	0.43	2.32	0.42	2.39	0		1	.
7	542.05	188.89	0.44	2.25	0.44	2.27	0		1	.
7	543.05	125.02	0.45	2.25	0.44	2.27	0		0	.
7	544.05	126.33	0.44	2.27	0.44	2.27	0		0	.
7	545.05	126.83	0.44	2.26	0.44	2.27	0		0	.
7	546.05	222.49	0.44	2.29	0.44	2.27	0		0	.
7	547.05	225.19	0.44	2.27	0.44	2.27	0		0	.
7	548.05	348.65	0.44	2.28	0.44	2.27	0		0	.
7	549.05	336.30	0.43	2.34	0.44	2.27	0		0	.
7	550.05	355.59	0.43	2.31	0.44	2.27	0		0	.
7	551.05	228.50	0.44	2.27	0.44	2.27	0		0	.
7	552.05	230.63	0.40	2.48	0.40	2.48	1	3	0	2.23
7	553.05	452.62	0.45	2.23	0.45	2.23	1	1	0	2.27
7	554.05	192.52	0.44	2.28	0.44	2.28	1	2	0	2.23
7	555.05	217.11	0.46	2.19	0.46	2.19	1	2	0	2.33
7	556.05	274.31	0.41	2.44	0.41	2.44	1	3	0	2.33
7	557.05	276.34	0.43	2.33	0.43	2.33	1	1	0	2.23
7	558.05	130.30	0.43	2.34	0.43	2.34	1	3	0	2.33
7	559.05	268.20	0.50	2.01	0.50	2.01	1	2	0	2.33
7	560.05	220.45	0.43	2.35	0.43	2.35	1	3	0	2.33
7	561.05	364.13	0.43	2.33	0.43	2.33	1	2	0	2.33
7	562.05	210.54	0.43	2.34	0.43	2.35	0		0	.
7	563.05	207.64	0.42	2.37	0.42	2.37	1	1	0	2.33
7	564.05	191.22	0.42	2.37	0.42	2.37	0		1	.
7	565.05	133.73	0.42	2.37	0.42	2.37	1	0	0	2.37
7	566.05	132.73	0.42	2.40	0.42	2.37	0		0	.
7	567.05	292.79	0.42	2.40	0.42	2.37	0		0	.
7	568.05	256.19	0.42	2.37	0.42	2.37	1	1	0	2.37
7	569.05	297.36	0.42	2.37	0.42	2.37	0		0	.
7	570.05	168.33	0.42	2.38	0.42	2.37	0		1	.
7	571.05	222.72	0.41	2.43	0.41	2.42	0		1	.
7	572.05	178.74	0.42	2.38	0.42	2.37	0		0	.
7	573.05	170.87	0.46	2.19	0.46	2.19	1	2	0	2.42
7	574.05	180.71	0.41	2.42	0.41	2.42	1	0	0	2.37
7	575.05	174.14	0.45	2.22	0.46	2.19	0		1	.
7	576.05	172.77	0.42	2.39	0.42	2.39	1	3	0	2.42
7	577.05	178.18	0.42	2.40	0.41	2.42	0		0	.
7	578.05	176.28	0.41	2.47	0.41	2.47	1	1	0	2.54
7	579.05	176.11	0.40	2.48	0.40	2.48	1	3	0	2.42

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	580.05	1	.	1	0	1	580	1	1.87	1	175.99
7	581.05	0	.	0	0	1	581	1	1.87	1	73.98
7	582.05	0	.	0	0	1	582	1	2.02	1	114.78
7	583.05	0	1	0	0	1	584	0	2.18	1	155.58
7	584.05	0	.	1	0	1	584	0	2.02	2	155.58
7	585.05	1	1	1	0	1	582	1	2.33	1	175.99
7	586.05	1	.	1	0	1	586	1	2.02	2	175.99
7	587.05	1	1	1	0	1	584	0	2.18	2	135.18
7	588.05	0	0	0	0	1	584	0	2.02	2	175.99
7	589.05	1	1	1	0	1	584	0	2.18	1	73.98
7	590.05	0	1	1	0	1	584	0	2.18	1	124.98
7	591.05	0	0	1	0	1	584	0	2.33	1	114.78
7	592.05	0	1	1	1	1	584	0	2.02	2	175.99
7	593.05	1	1	1	0	1	584	0	1.87	1	175.99
7	594.05	0	1	0	0	1	584	0	1.55	2	175.99
7	595.05	1	1	1	0	2	584	0	1.71	1	175.99
7	596.05	0	.	0	0	1	596	1	1.87	2	145.38
7	597.05	1	.	1	0	1	597	1	1.71	1	175.99
7	598.05	0	.	0	0	1	598	1	1.87	1	175.99
7	599.05	1	.	1	0	1	599	1	1.87	0	175.99
7	600.05	1	1	1	0	1	601	0	1.87	2	175.99
7	601.05	1	.	1	0	2	601	0	1.71	1	175.99
7	602.05	0	1	0	0	1	601	0	1.87	1	2.58
7	603.05	0	0	1	0	1	601	0	1.87	1	175.99
7	604.05	1	.	1	0	1	604	1	1.71	1	175.99
7	605.05	0	.	1	0	1	605	1	1.87	2	175.99
7	606.05	1	0	1	0	1	604	1	2.02	1	114.78
7	607.05	0	.	1	0	1	607	1	2.18	2	104.58
7	608.05	1	1	1	0	1	607	1	2.02	2	145.38
7	609.05	0	1	1	0	1	604	1	2.02	1	175.99
7	610.05	1	1	1	0	1	604	1	2.49	1	175.99
7	611.05	1	.	0	0	1	611	0	2.18	2	175.99
7	612.05	0	1	1	0	1	611	0	2.33	1	175.99
7	613.05	0	.	1	0	1	613	1	2.18	2	145.38
7	614.05	1	.	1	0	1	614	1	2.02	1	175.99
7	615.05	1	1	1	0	1	613	1	2.18	2	175.99
7	616.05	1	0	1	0	1	614	1	1.87	1	175.99
7	617.05	0	1	1	0	1	620	0	2.02	2	145.38
7	618.05	1	0	1	0	1	620	0	1.71	2	145.38
7	619.05	1	0	1	0	1	620	0	2.02	0	73.98
7	620.05	1	.	0	0	1	620	0	1.71	0	73.98
7	621.05	1	0	1	0	2	620	0	2.02	1	135.18
7	622.05	1	.	1	0	1	622	0	2.02	1	135.18
7	623.05	1	0	1	0	2	622	0	2.18	1	73.98
7	624.05	1	.	1	1	1	624	0	1.87	0	73.98
7	625.05	1	0	1	0	2	624	0	1.55	1	94.38
7	626.05	1	.	1	0	1	626	0	1.55	2	145.38
7	627.05	1	.	1	0	1	627	0	1.40	2	145.38
7	628.05	1	.	1	0	2	628	0	1.55	1	73.98
7	629.05	1	.	1	0	2	629	0	1.40	1	73.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	580.05	431.83	0.39	2.54	0.39	2.54	1	1	0	2.42
7	581.05	278.18	0.40	2.48	0.40	2.48	1	1	1	2.47
7	582.05	223.92	0.40	2.49	0.40	2.49	1	3	0	2.48
7	583.05	225.96	0.41	2.45	0.42	2.39	0		0	.
7	584.05	188.42	0.42	2.39	0.42	2.39	1	1	0	2.48
7	585.05	187.85	0.40	2.50	0.40	2.49	0		1	.
7	586.05	272.87	0.42	2.38	0.42	2.38	1	2	0	2.48
7	587.05	193.66	0.41	2.43	0.42	2.39	0		0	.
7	588.05	437.41	0.40	2.47	0.42	2.39	0		0	.
7	589.05	223.49	0.41	2.45	0.42	2.39	0		1	.
7	590.05	288.36	0.40	2.48	0.42	2.39	0		0	.
7	591.05	201.83	0.40	2.48	0.42	2.39	0		0	.
7	592.05	184.18	0.42	2.40	0.42	2.39	0		0	.
7	593.05	213.98	0.41	2.45	0.42	2.39	0		0	.
7	594.05	186.62	0.41	2.44	0.42	2.39	0		0	.
7	595.05	250.38	0.41	2.46	0.42	2.39	0		0	.
7	596.05	191.79	0.41	2.45	0.41	2.45	1	2	0	2.39
7	597.05	195.03	0.39	2.56	0.39	2.56	1	3	0	2.39
7	598.05	199.03	0.39	2.56	0.39	2.56	1	3	0	2.39
7	599.05	232.23	0.41	2.42	0.41	2.42	1	2	0	2.39
7	600.05	197.83	0.40	2.50	0.40	2.49	0		0	.
7	601.05	670.90	0.40	2.49	0.40	2.49	1	1	0	2.39
7	602.05	201.70	0.40	2.50	0.40	2.49	0		1	.
7	603.05	240.27	0.40	2.50	0.40	2.49	0		0	.
7	604.05	217.32	0.44	2.27	0.44	2.27	1	2	0	2.49
7	605.05	341.14	0.40	2.51	0.40	2.51	1	3	0	2.49
7	606.05	311.71	0.44	2.28	0.44	2.27	0		1	.
7	607.05	262.63	0.39	2.53	0.39	2.53	1	3	0	2.49
7	608.05	241.01	0.40	2.52	0.39	2.53	0		0	.
7	609.05	210.14	0.44	2.27	0.44	2.27	0		0	.
7	610.05	207.07	0.43	2.33	0.44	2.27	0		0	.
7	611.05	256.86	0.42	2.36	0.42	2.36	1	1	0	2.49
7	612.05	273.34	0.43	2.33	0.42	2.36	0		1	.
7	613.05	242.54	0.41	2.45	0.41	2.45	1	3	0	2.36
7	614.05	213.01	0.45	2.22	0.45	2.22	1	2	0	2.36
7	615.05	215.21	0.41	2.45	0.41	2.45	0		1	.
7	616.05	308.94	0.44	2.28	0.45	2.22	0		1	.
7	617.05	306.67	0.45	2.25	0.43	2.32	0		0	.
7	618.05	505.24	0.45	2.22	0.43	2.32	0		0	.
7	619.05	530.50	0.43	2.31	0.43	2.32	0		1	.
7	620.05	302.10	0.43	2.32	0.43	2.32	1	1	0	2.36
7	621.05	302.00	0.45	2.20	0.43	2.32	0		0	.
7	622.05	496.47	0.47	2.12	0.47	2.12	1	1	0	2.32
7	623.05	498.27	0.47	2.15	0.47	2.12	0		1	.
7	624.05	501.80	0.49	2.04	0.49	2.04	1	1	0	2.12
7	625.05	313.38	0.49	2.04	0.49	2.04	0		1	.
7	626.05	311.14	0.55	1.81	0.55	1.81	1	2	0	2.04
7	627.05	509.04	0.50	2.01	0.50	2.01	1	1	0	2.08
7	628.05	529.46	0.48	2.10	0.48	2.10	1	3	0	2.04
7	629.05	353.25	0.48	2.08	0.48	2.08	1	1	0	2.04

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	630.05	1	.	0	0	.	630	0	1.40	1	114.78
7	631.05	0	.	0	0	1	631	0	1.55	2	175.99
7	632.05	1	1	1	0	1	631	0	1.24	1	175.99
7	634.05	0	1	1	0	2	631	0	2.02	2	145.38
7	635.05	1	0	1	0	1	631	0	1.71	1	145.38
7	636.05	0	.	0	0	3	636	0	1.87	1	175.99
7	637.05	0	0	0	0	2	636	0	1.71	0	175.99
7	638.05	0	0	0	0	1	636	0	1.87	1	104.58
7	639.05	0	.	0	0	2	639	0	1.55	1	175.99
7	640.05	0	.	0	0	2	640	0	1.55	2	124.98
7	641.05	1	.	1	0	1	641	0	1.09	0	135.18
7	642.05	1	.	1	0	2	642	0	1.55	1	124.98
7	643.05	1	.	1	0	.	643	0	0.47	1	135.18
7	645.05	0	.	0	0	1	645	0	0.62	1	104.58
7	646.05	0	.	1	0	.	646	0	0.62	2	104.58
7	647.05	0	.	0	0	.	647	0	0.31	2	165.78
7	648.05	0	.	1	0	1	648	0	0.62	2	155.58
7	649.05	0	.	0	0	.	649	0	0.31	2	155.58
7	650.05	0	.	0	0	.	650	0	0.62	1	104.58
7	651.05	0	.	0	0	.	651	0	0.31	1	135.18
7	655.05	0	.	1	0	.	655	0	0.47	1	43.38
7	656.05	0	.	1	0	.	656	0	0.31	2	104.58
7	657.05	0	.	1	0	.	657	0	0.31	1	155.58
7	658.05	1	.	1	0	.	658	0	0.31	2	73.98
7	659.05	0	.	1	0	.	659	0	0.62	0	165.78
7	661.05	0	.	0	0	.	661	0	0.31	1	155.58
7	662.05	0	0	0	0	1	661	0	0.62	2	155.58
7	663.05	1	.	1	0	.	663	0	0.31	1	165.78
7	664.05	1	.	1	0	.	664	0	0.31	1	175.99
7	666.05	1	.	1	0	1	666	0	2.18	1	43.38
7	667.05	1	0	1	0	1	666	0	2.64	2	43.38
7	93.06	1	.	0	0	.	93	0	0.31	2	22.98
7	95.06	0	.	0	0	.	95	0	0.31	0	22.98
7	162.06	1	.	1	0	3	162	0	0.62	1	12.78
7	163.06	1	.	1	0	3	163	0	0.47	1	12.78
7	169.06	1	.	1	0	.	169	0	0.47	2	12.78
7	171.06	1	0	1	0	1	169	0	0.62	2	12.78
7	173.06	0	.	1	1	2	173	0	0.93	0	12.78
7	200.06	0	.	0	0	3	200	0	0.78	1	22.98
7	201.06	0	0	1	0	2	200	0	0.93	1	22.98
7	212.06	1	0	1	0	1	213	0	0.93	0	12.78
7	213.06	1	.	1	0	3	213	0	0.78	1	12.78
7	220.06	0	.	1	0	1	220	0	0.93	0	12.78
7	221.06	0	.	0	0	2	221	0	1.24	0	43.38
7	225.06	0	.	1	0	1	225	0	1.40	2	2.58
7	226.06	1	.	1	0	1	226	0	0.93	0	12.78
7	242.06	1	.	1	0	1	242	0	0.93	0	43.38
7	243.06	0	.	0	0	2	243	0	0.93	1	43.38
7	244.06	0	.	1	0	1	244	0	1.55	0	43.38
7	252.06	0	.	1	0	1	252	0	1.55	1	84.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	630.05	273.81	0.50	2.01	0.50	2.01	1	0	0	2.01
7	631.05	272.34	0.52	1.91	0.52	1.91	1	1	0	2.01
7	632.05	818.55	0.53	1.90	0.52	1.91	0		1	.
7	634.05	323.92	0.55	1.80	0.52	1.91	0		0	.
7	635.05	306.07	0.53	1.89	0.52	1.91	0		0	.
7	636.05	307.37	0.56	1.79	0.56	1.79	1	0	0	1.91
7	637.05	415.95	0.55	1.81	0.56	1.79	0		1	.
7	638.05	460.16	0.55	1.83	0.56	1.79	0		0	.
7	639.05	430.26	0.59	1.70	0.59	1.70	1	1	0	1.75
7	640.05	343.64	0.57	1.75	0.57	1.75	1	1	0	1.70
7	641.05	422.65	0.63	1.59	0.63	1.59	1	0	0	1.75
7	642.05	594.89	0.57	1.75	0.57	1.75	1	1	0	1.79
7	643.05	883.41	0.66	1.52	0.66	1.52	1	0	0	1.59
7	645.05	595.33	0.57	1.76	0.57	1.76	1	3	0	1.52
7	646.05	651.72	0.57	1.75	0.57	1.75	1	2	0	1.52
7	647.05	697.19	1.00	1.00	1.00	1.00	1	0	0	1.52
7	648.05	694.93	0.88	1.14	0.88	1.14	1	0	0	1.10
7	649.05	102.77	0.88	1.14	0.88	1.14	1	0	0	1.00
7	650.05	531.93	0.91	1.10	0.91	1.10	1	0	0	1.14
7	651.05	933.76	0.87	1.15	0.87	1.15	1	0	0	1.14
7	655.05	721.59	0.87	1.15	0.87	1.15	1	0	0	1.15
7	656.05	770.43	1.35	0.74	1.35	0.74	1	0	0	1.40
7	657.05	1072.34	0.71	1.40	0.71	1.40	1	0	0	1.15
7	658.05	979.98	0.92	1.08	0.92	1.08	1	0	0	0.74
7	659.05	1252.95	0.92	1.09	0.92	1.09	1	0	0	1.08
7	661.05	1010.74	0.69	1.45	0.69	1.45	1	0	0	1.09
7	662.05	1222.05	0.72	1.39	0.69	1.45	0		1	.
7	663.05	1049.52	0.87	1.15	0.87	1.15	1	0	0	1.45
7	664.05	142.65	0.95	1.06	0.95	1.06	1	0	0	1.15
7	666.05	183.65	0.26	3.85	0.26	3.85	1	1	0	4.05
7	667.05	181.41	0.26	3.82	0.26	3.85	0		1	.
7	93.06	84.08	1.25	0.80	1.25	0.80	1	0	0	0.92
7	95.06	100.43	1.09	0.92	1.09	0.92	1	0	0	.
7	162.06	76.41	0.88	1.14	0.88	1.14	1	0	0	1.21
7	163.06	131.69	0.83	1.21	0.83	1.21	1	0	0	0.80
7	169.06	314.04	0.80	1.24	0.80	1.24	1	0	0	1.14
7	171.06	289.33	0.81	1.23	0.80	1.24	0		1	.
7	173.06	291.56	0.79	1.27	0.79	1.27	1	0	0	1.24
7	200.06	57.02	0.68	1.47	0.68	1.47	1	0	0	1.27
7	201.06	121.89	0.68	1.47	0.68	1.47	0		1	.
7	212.06	95.69	0.51	1.96	0.49	2.04	0		1	.
7	213.06	295.72	0.49	2.04	0.49	2.04	1	0	0	1.47
7	220.06	66.84	0.54	1.85	0.54	1.85	1	3	0	2.04
7	221.06	141.71	0.54	1.86	0.54	1.86	1	1	0	2.04
7	225.06	104.14	0.51	1.96	0.51	1.96	1	1	0	1.86
7	226.06	149.85	0.56	1.80	0.56	1.80	1	2	0	2.04
7	242.06	71.81	0.71	1.41	0.71	1.41	1	2	0	1.96
7	243.06	76.04	0.63	1.59	0.63	1.59	1	3	0	1.96
7	244.06	166.00	0.59	1.70	0.59	1.70	1	3	0	1.43
7	252.06	209.27	0.69	1.46	0.69	1.46	1	1	0	1.96

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	255.06	0	.	0	0	1	255	0	1.09	0	84.18
7	270.06	0	.	0	0	1	270	0	2.02	0	33.18
7	273.06	0	.	1	0	1	273	0	1.87	0	53.58
7	276.06	1	0	1	0	1	280	0	2.02	0	22.98
7	277.06	1	0	0	0	1	280	0	1.55	2	22.98
7	278.06	0	.	1	0	1	278	0	1.71	1	53.58
7	280.06	0	.	1	0	1	280	0	1.87	1	43.38
7	282.06	0	.	0	0	1	282	0	1.71	0	22.98
7	285.06	0	0	0	0	1	280	0	2.02	1	53.58
7	287.06	1	1	1	0	1	280	0	2.02	1	53.58
7	288.06	1	.	1	0	1	288	0	1.24	0	33.18
7	296.06	0	.	1	0	1	296	1	1.40	1	12.78
7	298.06	0	.	0	1	1	298	1	1.55	2	53.58
7	299.06	0	0	1	0	1	296	1	1.71	1	33.18
7	300.06	1	1	0	0	1	296	1	1.71	1	22.98
7	301.06	0	0	1	0	1	298	1	1.87	2	53.58
7	302.06	0	.	1	0	1	302	0	1.87	0	53.58
7	306.06	1	.	1	0	1	306	0	2.02	2	43.38
7	307.06	1	.	1	0	1	307	0	2.18	2	43.38
7	308.06	1	.	1	0	1	308	0	1.87	2	53.58
7	309.06	1	.	1	0	1	309	0	1.87	0	53.58
7	310.06	1	.	1	0	1	310	0	1.87	0	43.38
7	315.06	1	.	1	0	1	315	0	1.40	2	53.58
7	318.06	1	.	1	0	1	318	1	1.87	2	53.58
7	319.06	1	0	1	0	1	318	1	2.18	2	53.58
7	320.06	1	.	1	0	1	320	0	2.02	1	33.18
7	321.06	1	.	0	1	1	321	1	2.33	2	43.38
7	323.06	1	.	1	0	1	323	0	2.33	0	53.58
7	324.06	1	.	1	0	1	324	1	1.87	0	43.38
7	325.06	0	1	0	0	2	324	1	1.87	0	43.38
7	326.06	1	.	1	0	1	326	1	2.33	2	53.58
7	328.06	0	.	0	0	1	328	0	1.87	1	43.38
7	329.06	0	.	0	0	1	329	1	2.49	2	53.58
7	330.06	0	0	0	1	1	329	1	2.49	2	53.58
7	331.06	1	1	1	0	1	329	1	2.64	2	53.58
7	332.06	0	1	0	1	1	329	1	2.95	2	53.58
7	335.06	1	1	1	0	1	329	1	2.49	2	43.38
7	336.06	0	.	1	0	1	336	0	2.02	1	33.18
7	337.06	0	.	0	0	1	337	0	2.18	1	33.18
7	338.06	1	.	0	0	2	338	0	2.02	1	43.38
7	339.06	1	.	1	0	1	339	1	2.18	0	53.58
7	340.06	1	.	1	0	1	340	1	1.55	1	53.58
7	341.06	1	.	1	0	1	341	1	2.49	1	53.58
7	342.06	1	.	1	0	1	342	1	2.80	0	43.38
7	343.06	1	.	1	0	1	343	0	1.24	2	22.98
7	344.06	0	.	1	0	1	344	0	1.40	2	22.98
7	345.06	1	.	1	1	1	345	1	2.49	2	53.58
7	347.06	0	1	0	0	1	345	1	2.33	2	53.58
7	349.06	1	.	1	0	1	349	1	2.64	0	53.58
7	351.06	0	1	1	0	1	361	1	2.49	1	43.38

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	255.06	165.36	0.70	1.43	0.70	1.43	1	1	0	1.46
7	270.06	423.06	0.50	1.99	0.50	1.99	1	1	0	1.43
7	273.06	309.54	0.50	1.99	0.50	1.99	1	2	0	1.43
7	276.06	118.85	0.54	1.87	0.51	1.96	0		0	.
7	277.06	83.52	0.53	1.90	0.51	1.96	0		0	.
7	278.06	236.83	0.47	2.14	0.47	2.14	1	3	0	1.43
7	280.06	229.26	0.51	1.96	0.51	1.96	1	1	0	1.99
7	282.06	195.63	0.49	2.03	0.49	2.03	1	4	0	1.96
7	285.06	244.24	0.51	1.95	0.51	1.96	0		1	.
7	287.06	122.25	0.51	1.95	0.51	1.96	0		0	.
7	288.06	264.36	0.37	2.68	0.37	2.68	1	2	0	2.03
7	296.06	208.61	0.37	2.72	0.37	2.72	1	3	0	2.03
7	298.06	123.79	0.42	2.40	0.42	2.40	1	2	0	2.03
7	299.06	124.69	0.36	2.75	0.37	2.72	0		1	.
7	300.06	92.16	0.36	2.76	0.37	2.72	0		0	.
7	301.06	94.56	0.39	2.56	0.42	2.40	0		1	.
7	302.06	188.42	0.37	2.69	0.37	2.69	1	4	0	2.03
7	306.06	97.13	0.38	2.64	0.38	2.64	1	2	0	3.01
7	307.06	102.00	0.35	2.86	0.35	2.86	1	4	0	2.69
7	308.06	102.94	0.40	2.53	0.40	2.53	1	2	0	3.01
7	309.06	103.57	0.38	2.64	0.38	2.64	1	3	0	3.01
7	310.06	402.73	0.34	2.96	0.34	2.96	1	3	0	3.01
7	315.06	242.74	0.35	2.83	0.35	2.83	1	2	0	3.00
7	318.06	111.91	0.36	2.80	0.36	2.80	1	2	0	3.00
7	319.06	130.26	0.35	2.83	0.36	2.80	0		1	.
7	320.06	116.75	0.33	3.01	0.33	3.01	1	4	0	2.86
7	321.06	231.20	0.32	3.08	0.32	3.08	1	2	0	3.38
7	323.06	111.45	0.34	2.93	0.34	2.93	1	3	0	3.01
7	324.06	113.08	0.31	3.26	0.31	3.26	1	3	0	3.38
7	325.06	115.88	0.31	3.24	0.31	3.26	0		1	.
7	326.06	306.54	0.32	3.15	0.32	3.15	1	4	0	3.38
7	328.06	124.43	0.33	3.00	0.33	3.00	1	4	0	3.01
7	329.06	125.89	0.32	3.16	0.32	3.16	1	4	0	3.15
7	330.06	129.10	0.31	3.18	0.32	3.16	0		1	.
7	331.06	131.00	0.32	3.15	0.32	3.16	0		0	.
7	332.06	360.16	0.31	3.18	0.32	3.16	0		0	.
7	335.06	131.99	0.31	3.20	0.32	3.16	0		0	.
7	336.06	133.36	0.31	3.22	0.31	3.22	1	3	0	3.01
7	337.06	98.23	0.29	3.40	0.29	3.40	1	3	0	3.01
7	338.06	110.18	0.30	3.34	0.30	3.34	1	2	0	3.01
7	339.06	104.31	0.33	3.03	0.33	3.03	1	2	0	3.00
7	340.06	122.46	0.31	3.20	0.31	3.20	1	3	0	3.00
7	341.06	129.33	0.26	3.87	0.26	3.87	1	2	0	3.16
7	342.06	81.31	0.27	3.66	0.27	3.66	1	4	0	3.16
7	343.06	76.81	0.33	3.07	0.33	3.07	1	3	0	2.03
7	344.06	132.13	0.32	3.09	0.32	3.09	1	3	0	2.03
7	345.06	243.87	0.26	3.81	0.26	3.81	1	4	0	3.66
7	347.06	315.48	0.27	3.68	0.26	3.81	0		0	.
7	349.06	248.51	0.24	4.11	0.24	4.11	1	3	0	3.81
7	351.06	106.61	0.25	4.04	0.25	4.03	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	352.06	1	.	1	0	2	352	1	2.02	1	53.58
7	353.06	0	.	1	0	1	353	1	2.33	2	84.18
7	355.06	0	.	1	0	1	355	1	2.64	0	73.98
7	356.06	0	.	1	0	1	356	1	2.49	1	22.98
7	358.06	0	.	0	0	1	358	1	2.64	1	84.18
7	361.06	1	.	1	1	1	361	1	2.49	1	43.38
7	363.06	0	.	1	0	1	363	1	2.49	1	43.38
7	366.06	1	1	1	0	1	361	1	2.33	1	43.38
7	370.06	0	.	0	0	1	370	1	2.49	1	43.38
7	372.06	1	.	1	0	1	372	1	2.64	2	53.58
7	373.06	0	0	0	0	1	370	1	2.18	1	53.58
7	375.06	0	.	0	0	2	375	1	2.49	1	53.58
7	378.06	1	.	1	0	1	378	1	2.64	1	43.38
7	379.06	1	1	1	0	1	363	1	2.49	2	43.38
7	383.06	1	0	0	0	1	372	1	2.02	2	94.38
7	384.06	0	.	1	0	1	384	1	2.80	0	84.18
7	385.06	0	.	1	0	1	385	1	2.33	2	43.38
7	388.06	1	1	0	0	1	385	1	2.33	2	12.78
7	390.06	1	0	1	1	1	385	1	2.33	2	33.18
7	391.06	0	.	1	0	1	391	1	2.02	1	43.38
7	392.06	1	0	1	0	1	385	1	2.64	2	63.78
7	393.06	1	1	1	0	1	391	1	2.02	1	43.38
7	394.06	0	1	1	0	1	391	1	2.18	1	12.78
7	395.06	1	1	1	0	1	391	1	2.33	1	12.78
7	396.06	1	0	1	1	1	385	1	2.49	2	43.38
7	397.06	1	0	1	1	1	385	1	2.64	2	43.38
7	398.06	0	1	0	0	1	385	1	2.49	2	22.98
7	400.06	1	1	0	0	1	385	1	2.95	2	22.98
7	401.06	1	.	1	0	1	401	1	2.49	1	12.78
7	402.06	1	0	1	0	1	401	1	2.64	1	12.78
7	403.06	0	.	1	0	1	403	1	1.87	1	53.58
7	404.06	0	1	1	0	1	401	1	2.80	1	12.78
7	405.06	1	0	0	0	1	401	1	2.64	1	12.78
7	406.06	0	0	1	0	1	401	1	2.80	1	84.18
7	409.06	1	.	1	0	1	409	1	2.95	1	53.58
7	410.06	0	1	0	0	1	409	1	2.18	1	53.58
7	411.06	0	.	1	0	1	411	0	2.33	1	53.58
7	412.06	1	1	1	0	1	411	0	2.49	1	53.58
7	413.06	0	1	0	0	2	411	0	2.33	1	53.58
7	415.06	0	.	0	0	1	415	0	2.18	1	53.58
7	416.06	0	0	0	0	2	415	0	2.18	1	53.58
7	417.06	0	0	0	0	1	415	0	2.18	2	53.58
7	418.06	0	0	1	1	2	415	0	1.71	2	63.78
7	419.06	1	1	1	0	1	415	0	2.02	1	53.58
7	420.06	1	0	1	0	1	415	0	2.02	2	63.78
7	421.06	1	0	1	0	1	415	0	2.02	1	63.78
7	422.06	1	0	1	0	1	415	0	2.02	2	84.18
7	423.06	1	0	1	0	1	415	0	1.87	1	63.78
7	424.06	1	0	0	0	1	415	0	1.71	1	84.18
7	425.06	1	0	1	0	1	415	0	2.33	2	94.38

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	352.06	62.80	0.30	3.38	0.30	3.38	1	4	0	3.00
7	353.06	251.82	0.28	3.54	0.28	3.54	1	2	0	3.81
7	355.06	184.61	0.28	3.55	0.28	3.55	1	2	0	3.81
7	356.06	328.86	0.25	3.92	0.25	3.92	1	3	0	3.81
7	358.06	331.03	0.26	3.85	0.26	3.85	1	4	0	3.81
7	361.06	255.19	0.25	4.03	0.25	4.03	1	3	0	3.66
7	363.06	379.24	0.22	4.49	0.22	4.49	1	3	0	3.81
7	366.06	263.79	0.25	4.04	0.25	4.03	0		0	.
7	370.06	277.11	0.26	3.80	0.26	3.80	1	3	0	3.16
7	372.06	114.52	0.26	3.92	0.26	3.92	1	1	0	3.85
7	373.06	273.54	0.26	3.81	0.26	3.80	0		1	.
7	375.06	281.95	0.25	4.00	0.25	4.00	1	3	0	3.16
7	378.06	137.67	0.22	4.65	0.22	4.65	1	3	0	3.81
7	379.06	283.65	0.22	4.45	0.22	4.49	0		1	.
7	383.06	77.98	0.25	3.94	0.26	3.92	0		1	.
7	384.06	148.08	0.24	4.19	0.24	4.19	1	4	0	3.92
7	385.06	322.72	0.27	3.68	0.27	3.68	1	2	0	4.19
7	388.06	326.06	0.27	3.71	0.27	3.68	0		1	.
7	390.06	141.28	0.26	3.78	0.27	3.68	0		0	.
7	391.06	116.98	0.25	3.99	0.25	3.99	1	3	0	4.19
7	392.06	145.65	0.26	3.91	0.27	3.68	0		0	.
7	393.06	248.98	0.25	3.94	0.25	3.99	0		1	.
7	394.06	251.22	0.26	3.87	0.25	3.99	0		0	.
7	395.06	154.39	0.26	3.87	0.25	3.99	0		0	.
7	396.06	151.39	0.25	4.07	0.27	3.68	0		0	.
7	397.06	205.27	0.24	4.18	0.27	3.68	0		0	.
7	398.06	337.00	0.25	4.07	0.27	3.68	0		0	.
7	400.06	252.32	0.25	4.07	0.27	3.68	0		0	.
7	401.06	255.65	0.25	4.06	0.25	4.06	1	3	0	4.19
7	402.06	113.01	0.24	4.23	0.25	4.06	0		1	.
7	403.06	264.10	0.31	3.28	0.31	3.28	1	3	0	3.00
7	404.06	261.16	0.23	4.31	0.25	4.06	0		0	.
7	405.06	37.70	0.23	4.32	0.25	4.06	0		0	.
7	406.06	353.82	0.23	4.32	0.25	4.06	0		0	.
7	409.06	152.42	0.22	4.53	0.22	4.53	1	3	0	4.19
7	410.06	154.76	0.22	4.50	0.22	4.53	0		1	.
7	411.06	156.76	0.22	4.46	0.22	4.46	1	1	0	4.19
7	412.06	160.46	0.22	4.48	0.22	4.46	0		1	.
7	413.06	379.38	0.22	4.50	0.22	4.46	0		0	.
7	415.06	163.93	0.22	4.62	0.22	4.62	1	4	0	4.46
7	416.06	165.13	0.22	4.62	0.22	4.62	0		1	.
7	417.06	117.92	0.21	4.66	0.22	4.62	0		0	.
7	418.06	167.60	0.22	4.63	0.22	4.62	0		0	.
7	419.06	122.12	0.23	4.37	0.22	4.62	0		0	.
7	420.06	123.06	0.26	3.91	0.22	4.62	0		0	.
7	421.06	99.27	0.25	3.99	0.22	4.62	0		0	.
7	422.06	124.16	0.25	4.02	0.22	4.62	0		0	.
7	423.06	100.87	0.25	4.01	0.22	4.62	0		0	.
7	424.06	102.97	0.25	4.00	0.22	4.62	0		0	.
7	425.06	101.27	0.25	4.07	0.22	4.62	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	426.06	1	0	1	0	1	415	0	2.02	1	94.38
7	427.06	1	.	1	1	1	427	1	2.49	2	104.58
7	428.06	0	.	1	0	1	428	1	2.33	1	94.38
7	429.06	1	1	1	0	1	428	1	2.64	1	94.38
7	430.06	1	0	1	0	1	427	1	2.33	2	104.58
7	431.06	1	0	1	0	1	427	1	2.18	2	104.58
7	433.06	0	1	0	0	1	427	1	3.11	2	104.58
7	435.06	0	0	1	0	1	427	1	3.11	2	73.98
7	436.06	0	.	1	0	1	436	1	2.80	1	53.58
7	437.06	0	0	0	0	1	436	1	2.64	1	53.58
7	438.06	1	1	0	0	1	440	1	2.95	0	104.58
7	439.06	1	1	1	0	1	436	1	2.49	1	53.58
7	440.06	0	.	0	0	1	440	1	2.49	0	84.18
7	441.06	0	.	1	0	1	441	0	2.95	2	43.38
7	442.06	1	.	1	0	1	442	1	2.64	1	73.98
7	443.06	1	0	1	0	1	452	0	2.02	2	124.98
7	444.06	1	.	1	0	1	444	1	2.49	2	124.98
7	445.06	1	0	1	0	1	452	0	2.33	2	53.58
7	446.06	1	0	1	0	2	444	1	2.49	2	104.58
7	448.06	0	1	0	1	1	444	1	2.18	2	104.58
7	451.06	0	0	0	0	1	444	1	2.33	2	104.58
7	452.06	0	.	1	0	2	452	0	3.26	1	104.58
7	453.06	1	1	1	0	1	452	0	3.11	1	33.18
7	454.06	1	0	1	0	1	466	0	2.18	2	114.78
7	455.06	1	0	1	0	1	452	0	2.80	1	43.38
7	456.06	1	0	1	0	2	466	0	2.18	2	94.38
7	457.06	0	1	1	0	1	452	0	2.18	1	124.98
7	458.06	0	1	1	0	1	466	0	2.49	1	53.58
7	459.06	1	0	1	0	1	466	0	2.18	1	53.58
7	460.06	1	.	0	0	1	460	1	2.49	1	43.38
7	461.06	1	0	1	0	1	460	1	2.49	1	43.38
7	462.06	1	1	1	0	1	466	0	2.18	1	43.38
7	463.06	0	1	0	0	1	460	1	2.49	1	43.38
7	464.06	0	0	1	0	1	460	1	2.33	1	104.58
7	465.06	0	0	0	0	1	460	1	2.33	1	124.98
7	466.06	1	.	1	0	1	466	0	2.33	1	43.38
7	467.06	1	1	0	0	1	466	0	2.64	0	43.38
7	468.06	0	1	1	0	1	466	0	2.64	1	53.58
7	470.06	1	1	1	0	1	466	0	2.64	2	124.98
7	472.06	0	1	0	0	1	466	0	1.87	2	43.38
7	473.06	0	1	1	0	1	466	0	2.49	2	43.38
7	475.06	1	1	1	0	1	479	0	2.18	2	94.38
7	476.06	1	.	0	0	1	476	0	2.18	1	33.18
7	477.06	1	0	1	0	1	479	0	2.64	2	94.38
7	478.06	1	0	1	0	1	479	0	2.18	1	94.38
7	479.06	0	.	0	0	1	479	0	2.18	1	94.38
7	480.06	1	.	0	0	1	480	0	2.33	1	22.98
7	481.06	0	1	0	0	1	480	0	2.18	2	22.98
7	482.06	0	.	1	0	1	482	1	2.02	2	94.38
7	483.06	0	0	1	0	1	480	0	2.33	1	63.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	426.06	86.28	0.25	4.05	0.22	4.62	0		0	.
7	427.06	106.01	0.25	3.93	0.25	3.93	1	2	0	4.62
7	428.06	107.98	0.24	4.14	0.24	4.14	1	3	0	4.62
7	429.06	87.85	0.25	4.02	0.24	4.14	0		1	.
7	430.06	88.82	0.26	3.88	0.25	3.93	0		1	.
7	431.06	409.47	0.29	3.43	0.25	3.93	0		0	.
7	433.06	407.20	0.30	3.34	0.25	3.93	0		0	.
7	435.06	181.68	0.27	3.66	0.25	3.93	0		0	.
7	436.06	183.92	0.23	4.27	0.23	4.27	1	3	0	4.62
7	437.06	94.13	0.24	4.11	0.23	4.27	0		1	.
7	438.06	185.79	0.26	3.82	0.26	3.92	0		1	.
7	439.06	66.70	0.24	4.11	0.23	4.27	0		0	.
7	440.06	199.17	0.26	3.92	0.26	3.92	1	1	0	4.62
7	441.06	152.39	0.26	3.91	0.26	3.91	1	4	0	3.92
7	442.06	66.33	0.24	4.10	0.24	4.10	1	3	0	3.92
7	443.06	62.99	0.23	4.33	0.23	4.29	0		0	.
7	444.06	202.70	0.22	4.52	0.22	4.52	1	2	0	4.29
7	445.06	105.17	0.22	4.45	0.23	4.29	0		0	.
7	446.06	422.35	0.22	4.53	0.22	4.52	0		1	.
7	448.06	423.79	0.24	4.14	0.22	4.52	0		0	.
7	451.06	98.26	0.25	4.05	0.22	4.52	0		0	.
7	452.06	245.41	0.23	4.29	0.23	4.29	1	4	0	3.91
7	453.06	112.94	0.23	4.32	0.23	4.29	0		1	.
7	454.06	197.53	0.25	4.02	0.25	4.08	0		1	.
7	455.06	144.24	0.22	4.45	0.23	4.29	0		0	.
7	456.06	64.56	0.25	4.00	0.25	4.08	0		0	.
7	457.06	214.35	0.22	4.56	0.23	4.29	0		0	.
7	458.06	211.48	0.24	4.11	0.25	4.08	0		0	.
7	459.06	202.40	0.25	4.08	0.25	4.08	0		0	.
7	460.06	204.74	0.22	4.59	0.22	4.59	1	3	0	4.29
7	461.06	220.79	0.22	4.59	0.22	4.59	0		1	.
7	462.06	206.41	0.26	3.80	0.25	4.08	0		0	.
7	463.06	99.93	0.22	4.57	0.22	4.59	0		0	.
7	464.06	73.67	0.24	4.16	0.22	4.59	0		0	.
7	465.06	214.15	0.23	4.32	0.22	4.59	0		0	.
7	466.06	224.13	0.25	4.08	0.25	4.08	1	1	0	4.29
7	467.06	215.25	0.24	4.08	0.25	4.08	0		0	.
7	468.06	590.76	0.24	4.14	0.25	4.08	0		0	.
7	470.06	592.06	0.24	4.19	0.25	4.08	0		0	.
7	472.06	225.56	0.27	3.77	0.25	4.08	0		0	.
7	473.06	476.01	0.26	3.91	0.25	4.08	0		0	.
7	475.06	289.05	0.28	3.57	0.27	3.70	0		1	.
7	476.06	152.45	0.26	3.83	0.26	3.83	1	4	0	4.08
7	477.06	154.49	0.28	3.62	0.27	3.70	0		0	.
7	478.06	149.82	0.27	3.65	0.27	3.70	0		0	.
7	479.06	300.56	0.27	3.70	0.27	3.70	1	1	0	3.83
7	480.06	302.43	0.28	3.62	0.28	3.62	1	1	0	3.70
7	481.06	160.79	0.28	3.62	0.28	3.62	0		1	.
7	482.06	184.35	0.28	3.62	0.28	3.62	1	2	0	3.62
7	483.06	127.22	0.28	3.63	0.28	3.62	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	484.06	0	.	0	0	1	484	1	2.18	1	104.58
7	485.06	1	1	1	0	1	482	1	2.18	2	124.98
7	486.06	1	1	0	1	1	484	1	2.33	1	84.18
7	487.06	0	1	0	1	1	488	0	2.64	2	94.38
7	488.06	1	.	1	0	1	488	0	2.33	1	104.58
7	489.06	0	1	0	0	1	488	0	2.49	2	124.98
7	490.06	1	1	1	0	1	488	0	2.49	1	104.58
7	491.06	0	1	1	0	1	488	0	2.33	2	124.98
7	492.06	0	0	1	0	1	488	0	2.80	1	104.58
7	493.06	0	0	1	0	1	488	0	2.02	2	124.98
7	494.06	1	1	0	0	1	488	0	1.87	1	124.98
7	495.06	1	1	1	0	1	488	0	2.33	1	53.58
7	496.06	1	0	0	0	1	488	0	2.18	1	22.98
7	497.06	1	1	1	0	1	488	0	2.18	1	104.58
7	498.06	0	1	0	1	2	488	0	2.18	1	114.78
7	499.06	1	0	1	0	1	488	0	2.02	2	124.98
7	500.06	1	0	1	0	1	488	0	1.87	1	124.98
7	501.06	1	0	1	0	2	488	0	2.02	1	84.18
7	502.06	0	1	0	0	1	488	0	2.18	2	84.18
7	503.06	1	1	1	0	1	504	0	2.33	1	104.58
7	504.06	0	.	0	0	1	504	0	2.02	2	104.58
7	505.06	0	1	0	0	2	504	0	2.33	1	124.98
7	506.06	0	0	1	0	1	504	0	2.18	2	124.98
7	507.06	1	.	1	0	1	507	1	2.33	1	114.78
7	508.06	0	.	1	0	1	508	1	2.64	2	114.78
7	509.06	1	1	1	0	1	508	1	2.02	2	124.98
7	510.06	0	0	1	0	1	508	1	1.87	2	114.78
7	511.06	1	0	0	0	1	508	1	2.33	2	124.98
7	512.06	1	0	1	0	1	508	1	2.33	2	155.58
7	513.06	1	0	1	0	1	508	1	2.49	2	124.98
7	514.06	1	0	1	0	1	508	1	2.80	2	114.78
7	515.06	1	0	1	0	1	508	1	2.49	2	114.78
7	516.06	0	1	0	1	1	518	1	2.49	1	22.98
7	517.06	1	0	1	1	1	508	1	3.11	2	114.78
7	518.06	1	.	1	0	1	518	1	2.33	1	155.58
7	519.06	0	1	1	1	1	508	1	2.49	2	114.78
7	520.06	1	1	1	0	1	508	1	2.80	2	114.78
7	521.06	1	0	1	0	1	508	1	2.80	2	53.58
7	522.06	1	0	1	0	1	518	1	2.80	1	53.58
7	523.06	1	0	1	0	2	518	1	2.64	1	53.58
7	524.06	0	1	1	0	1	541	0	1.87	2	155.58
7	525.06	0	0	1	0	1	541	0	1.87	1	155.58
7	526.06	0	0	1	0	1	518	1	3.11	1	22.98
7	530.06	1	1	1	0	1	518	1	2.49	1	84.18
7	531.06	0	1	0	0	1	518	1	2.02	1	84.18
7	532.06	1	.	1	0	3	532	0	2.18	1	84.18
7	533.06	0	0	1	0	1	518	1	2.49	1	124.98
7	534.06	0	0	0	0	1	518	1	2.49	1	124.98
7	535.06	1	1	1	0	1	518	1	2.49	1	114.78
7	536.06	1	0	1	0	1	518	1	2.49	1	73.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	484.06	115.35	0.27	3.67	0.27	3.67	1	3	0	3.62
7	485.06	156.16	0.27	3.67	0.28	3.62	0		1	.
7	486.06	162.66	0.27	3.71	0.27	3.67	0		1	.
7	487.06	129.86	0.27	3.75	0.27	3.74	0		1	.
7	488.06	110.27	0.27	3.74	0.27	3.74	1	1	0	3.62
7	489.06	131.80	0.27	3.76	0.27	3.74	0		0	.
7	490.06	118.58	0.27	3.76	0.27	3.74	0		0	.
7	491.06	132.73	0.26	3.80	0.27	3.74	0		0	.
7	492.06	112.94	0.26	3.83	0.27	3.74	0		0	.
7	493.06	111.21	0.24	4.08	0.27	3.74	0		0	.
7	494.06	240.51	0.24	4.09	0.27	3.74	0		0	.
7	495.06	360.96	0.26	3.78	0.27	3.74	0		0	.
7	496.06	134.83	0.28	3.60	0.27	3.74	0		0	.
7	497.06	133.66	0.26	3.82	0.27	3.74	0		0	.
7	498.06	122.62	0.26	3.87	0.27	3.74	0		0	.
7	499.06	116.98	0.28	3.59	0.27	3.74	0		0	.
7	500.06	162.56	0.28	3.60	0.27	3.74	0		0	.
7	501.06	172.41	0.26	3.77	0.27	3.74	0		0	.
7	502.06	140.84	0.28	3.59	0.27	3.74	0		0	.
7	503.06	144.61	0.28	3.57	0.28	3.56	0		1	.
7	504.06	123.22	0.28	3.56	0.28	3.56	1	1	0	3.74
7	505.06	124.52	0.28	3.54	0.28	3.56	0		0	.
7	506.06	153.78	0.28	3.55	0.28	3.56	0		0	.
7	507.06	152.85	0.27	3.65	0.27	3.65	1	3	0	3.56
7	508.06	135.43	0.28	3.58	0.28	3.58	1	2	0	3.56
7	509.06	155.35	0.28	3.54	0.28	3.58	0		0	.
7	510.06	136.57	0.28	3.57	0.28	3.58	0		1	.
7	511.06	111.84	0.31	3.28	0.28	3.58	0		0	.
7	512.06	138.27	0.31	3.25	0.28	3.58	0		0	.
7	513.06	171.10	0.31	3.20	0.28	3.58	0		0	.
7	514.06	174.17	0.31	3.26	0.28	3.58	0		0	.
7	515.06	397.76	0.30	3.38	0.28	3.58	0		0	.
7	516.06	167.53	0.27	3.67	0.25	4.02	0		0	.
7	517.06	110.71	0.30	3.30	0.28	3.58	0		0	.
7	518.06	175.24	0.25	4.02	0.25	4.02	1	3	0	3.56
7	519.06	169.67	0.29	3.40	0.28	3.58	0		0	.
7	520.06	315.58	0.29	3.41	0.28	3.58	0		0	.
7	521.06	313.42	0.30	3.32	0.28	3.58	0		0	.
7	522.06	312.51	0.28	3.51	0.25	4.02	0		0	.
7	523.06	115.48	0.28	3.63	0.25	4.02	0		0	.
7	524.06	114.05	0.30	3.28	0.30	3.35	0		0	.
7	525.06	401.53	0.30	3.29	0.30	3.35	0		0	.
7	526.06	538.54	0.27	3.68	0.25	4.02	0		0	.
7	530.06	188.96	0.27	3.66	0.25	4.02	0		0	.
7	531.06	215.75	0.25	4.00	0.25	4.02	0		1	.
7	532.06	95.29	0.29	3.45	0.29	3.45	1	0	0	3.56
7	533.06	96.63	0.27	3.66	0.25	4.02	0		0	.
7	534.06	163.23	0.27	3.68	0.25	4.02	0		0	.
7	535.06	234.60	0.28	3.63	0.25	4.02	0		0	.
7	536.06	164.46	0.27	3.68	0.25	4.02	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	537.06	0	1	1	0	1	518	1	3.11	1	114.78
7	538.06	0	0	0	0	1	518	1	2.80	1	114.78
7	539.06	1	1	1	0	1	518	1	2.80	1	114.78
7	540.06	1	0	1	0	1	541	0	1.71	1	63.78
7	541.06	1	.	1	0	2	541	0	1.87	1	63.78
7	542.06	1	1	1	0	1	541	0	2.02	1	155.58
7	543.06	1	0	1	0	2	541	0	2.02	1	104.58
7	544.06	1	0	1	0	1	541	0	2.18	1	155.58
7	545.06	1	0	1	0	1	541	0	2.33	2	155.58
7	546.06	0	0	0	0	1	541	0	2.64	2	155.58
7	547.06	0	1	0	0	2	541	0	2.49	1	73.98
7	548.06	0	0	1	0	1	541	0	2.49	1	73.98
7	549.06	1	1	1	0	1	541	0	2.18	2	53.58
7	550.06	1	0	1	0	2	541	0	2.18	2	53.58
7	551.06	1	0	1	0	1	541	0	2.02	1	53.58
7	552.06	1	1	1	0	1	553	0	1.55	2	94.38
7	553.06	0	.	1	0	1	553	0	1.71	1	84.18
7	554.06	1	0	1	0	1	553	0	1.71	1	33.18
7	555.06	1	.	1	0	1	555	0	1.71	2	104.58
7	556.06	1	.	1	0	1	556	0	1.55	1	114.78
7	557.06	0	1	1	0	1	553	0	1.24	1	73.98
7	558.06	0	0	0	0	1	553	0	1.55	1	73.98
7	559.06	1	.	0	0	1	559	0	1.71	0	155.58
7	560.06	0	0	1	0	2	553	0	1.40	2	73.98
7	561.06	1	0	1	0	1	556	0	2.18	2	114.78
7	562.06	0	.	0	0	1	562	0	1.40	1	53.58
7	563.06	0	.	0	0	3	563	0	2.18	1	104.58
7	564.06	1	0	1	0	1	565	0	1.24	1	114.78
7	565.06	1	.	1	0	3	565	0	1.87	1	104.58
7	566.06	1	0	0	0	1	565	0	1.40	1	155.58
7	567.06	1	0	1	0	1	565	0	1.55	1	155.58
7	568.06	0	.	1	0	2	568	0	1.87	1	63.78
7	569.06	0	0	1	0	1	568	0	1.71	2	94.38
7	570.06	0	0	0	0	1	568	0	1.87	1	63.78
7	571.06	1	1	1	0	1	574	0	1.40	0	155.58
7	572.06	0	.	1	0	2	572	0	1.40	1	114.78
7	573.06	1	0	0	0	1	574	0	1.87	2	155.58
7	574.06	0	.	1	0	1	574	0	1.55	0	155.58
7	575.06	0	0	1	0	2	574	0	2.18	2	155.58
7	576.06	1	0	1	0	2	574	0	1.40	1	155.58
7	577.06	1	0	1	0	1	574	0	1.55	1	155.58
7	578.06	1	0	0	0	1	574	0	2.02	1	155.58
7	579.06	1	0	1	0	1	574	0	1.87	2	155.58
7	580.06	1	0	1	0	1	574	0	1.55	1	155.58
7	581.06	0	1	0	0	1	574	0	2.02	1	53.58
7	582.06	0	0	0	0	2	574	0	2.18	1	94.38
7	583.06	0	1	0	0	1	574	0	1.87	1	135.18
7	584.06	0	1	1	0	1	574	0	1.87	2	135.18
7	585.06	1	1	1	0	2	574	0	2.02	0	155.58
7	586.06	1	0	1	0	1	574	0	1.87	0	155.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	537.06	165.80	0.27	3.66	0.25	4.02	0		0	.
7	538.06	172.77	0.27	3.68	0.25	4.02	0		0	.
7	539.06	254.05	0.27	3.67	0.25	4.02	0		0	.
7	540.06	252.09	0.30	3.33	0.30	3.35	0		1	.
7	541.06	118.18	0.30	3.35	0.30	3.35	1	1	0	3.45
7	542.06	188.89	0.31	3.25	0.30	3.35	0		0	.
7	543.06	125.02	0.31	3.24	0.30	3.35	0		0	.
7	544.06	126.33	0.31	3.24	0.30	3.35	0		0	.
7	545.06	126.83	0.31	3.22	0.30	3.35	0		0	.
7	546.06	222.49	0.31	3.21	0.30	3.35	0		0	.
7	547.06	225.19	0.31	3.24	0.30	3.35	0		0	.
7	548.06	348.65	0.31	3.25	0.30	3.35	0		0	.
7	549.06	336.30	0.31	3.24	0.30	3.35	0		0	.
7	550.06	355.59	0.31	3.27	0.30	3.35	0		0	.
7	551.06	228.50	0.31	3.28	0.30	3.35	0		0	.
7	552.06	230.63	0.31	3.25	0.31	3.24	0		1	.
7	553.06	452.62	0.31	3.24	0.31	3.24	1	0	0	3.35
7	554.06	192.52	0.31	3.25	0.31	3.24	0		0	.
7	555.06	217.11	0.41	2.45	0.41	2.45	1	2	0	3.24
7	556.06	274.31	0.39	2.59	0.39	2.59	1	1	0	3.24
7	557.06	276.34	0.39	2.53	0.31	3.24	0		0	.
7	558.06	130.30	0.39	2.54	0.31	3.24	0		0	.
7	559.06	268.20	0.44	2.27	0.44	2.27	1	2	0	2.59
7	560.06	220.45	0.39	2.56	0.31	3.24	0		0	.
7	561.06	364.13	0.40	2.53	0.39	2.59	0		1	.
7	562.06	210.54	0.38	2.60	0.38	2.60	1	3	0	3.24
7	563.06	207.64	0.39	2.55	0.39	2.55	1	3	0	2.59
7	564.06	191.22	0.38	2.60	0.39	2.60	0		1	.
7	565.06	133.73	0.39	2.60	0.39	2.60	1	0	0	2.59
7	566.06	132.73	0.39	2.59	0.39	2.60	0		0	.
7	567.06	292.79	0.39	2.59	0.39	2.60	0		0	.
7	568.06	256.19	0.38	2.62	0.38	2.62	1	0	0	2.60
7	569.06	297.36	0.38	2.61	0.38	2.62	0		0	.
7	570.06	168.33	0.39	2.58	0.38	2.62	0		1	.
7	571.06	222.72	0.39	2.55	0.40	2.49	0		1	.
7	572.06	178.74	0.39	2.58	0.39	2.58	1	1	0	2.62
7	573.06	170.87	0.40	2.50	0.40	2.49	0		0	.
7	574.06	180.71	0.40	2.49	0.40	2.49	1	0	0	2.58
7	575.06	174.14	0.39	2.55	0.40	2.49	0		0	.
7	576.06	172.77	0.40	2.51	0.40	2.49	0		0	.
7	577.06	178.18	0.40	2.49	0.40	2.49	0		0	.
7	578.06	176.28	0.40	2.53	0.40	2.49	0		0	.
7	579.06	176.11	0.40	2.50	0.40	2.49	0		0	.
7	580.06	431.83	0.39	2.53	0.40	2.49	0		0	.
7	581.06	278.18	0.40	2.52	0.40	2.49	0		0	.
7	582.06	223.92	0.40	2.51	0.40	2.49	0		0	.
7	583.06	225.96	0.40	2.50	0.40	2.49	0		0	.
7	584.06	188.42	0.40	2.49	0.40	2.49	0		0	.
7	585.06	187.85	0.40	2.48	0.40	2.49	0		0	.
7	586.06	272.87	0.40	2.48	0.40	2.49	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	587.06	1	1	1	0	1	588	1	2.18	2	114.78
7	588.06	0	.	0	0	1	588	1	2.02	2	155.58
7	589.06	1	1	1	0	1	574	0	2.02	1	53.58
7	590.06	0	0	1	0	1	591	1	1.87	1	104.58
7	591.06	0	.	1	0	1	591	1	2.02	1	94.38
7	592.06	0	.	1	1	1	592	1	1.71	2	155.58
7	593.06	1	.	1	0	2	593	1	1.87	1	155.58
7	594.06	0	0	0	0	1	592	1	1.71	2	155.58
7	595.06	1	0	1	0	1	593	1	1.71	1	155.58
7	596.06	0	0	0	0	1	592	1	2.02	2	124.98
7	597.06	1	0	1	0	1	593	1	1.55	1	155.58
7	598.06	0	1	0	0	1	593	1	1.87	1	155.58
7	599.06	1	1	1	0	1	593	1	2.02	1	155.58
7	600.06	1	1	1	0	1	603	0	1.71	2	155.58
7	601.06	1	0	1	0	2	593	1	2.02	1	155.58
7	603.06	0	.	1	0	1	603	0	2.02	1	155.58
7	604.06	1	.	1	0	1	604	1	1.87	0	155.58
7	605.06	0	.	1	0	1	605	0	2.02	2	155.58
7	606.06	1	0	1	0	1	604	1	2.18	0	94.38
7	607.06	0	.	1	0	1	607	1	1.87	2	84.18
7	608.06	1	1	1	0	1	607	1	1.87	2	124.98
7	609.06	0	1	1	0	1	604	1	2.02	0	155.58
7	610.06	1	.	1	0	1	610	1	1.87	1	155.58
7	611.06	1	.	0	0	1	611	1	1.87	2	155.58
7	612.06	0	.	1	0	1	612	1	2.33	0	155.58
7	613.06	0	.	1	0	1	613	1	2.18	2	124.98
7	614.06	1	.	1	0	1	614	1	2.02	2	155.58
7	615.06	1	.	1	0	1	615	1	2.02	0	155.58
7	616.06	1	0	1	0	1	615	1	1.87	0	155.58
7	617.06	0	.	1	0	1	617	0	1.87	2	124.98
7	618.06	1	0	1	0	1	620	0	1.71	2	124.98
7	619.06	1	0	1	0	1	620	0	1.71	0	53.58
7	620.06	1	.	0	0	1	620	0	1.71	2	53.58
7	621.06	1	.	1	0	1	621	0	2.02	1	114.78
7	622.06	1	.	1	0	1	622	0	1.87	1	114.78
7	623.06	1	.	1	0	1	623	0	2.18	1	53.58
7	624.06	1	.	1	1	1	624	0	2.02	1	53.58
7	625.06	1	0	1	0	2	624	0	2.02	1	73.98
7	626.06	1	.	1	0	1	626	0	1.87	2	124.98
7	627.06	1	0	1	0	1	626	0	1.71	0	124.98
7	628.06	1	.	1	0	1	628	0	1.71	1	53.58
7	629.06	1	.	1	0	1	629	0	1.71	1	53.58
7	630.06	1	.	0	0	2	630	0	1.87	1	94.38
7	631.06	0	.	0	0	2	631	0	1.87	2	155.58
7	632.06	1	1	1	0	1	631	0	1.55	1	155.58
7	634.06	0	.	1	0	2	634	0	2.18	1	124.98
7	635.06	1	.	1	0	2	635	0	2.18	0	124.98
7	636.06	0	.	0	0	3	636	0	2.02	1	155.58
7	637.06	0	0	0	0	1	636	0	2.02	2	155.58
7	638.06	0	0	0	0	1	636	0	1.87	1	84.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	587.06	193.66	0.42	2.37	0.43	2.33	0		1	.
7	588.06	437.41	0.43	2.33	0.43	2.33	1	2	0	2.49
7	589.06	223.49	0.40	2.49	0.40	2.49	0		0	.
7	590.06	288.36	0.42	2.41	0.41	2.43	0		1	.
7	591.06	201.83	0.41	2.43	0.41	2.43	1	3	0	2.49
7	592.06	184.18	0.43	2.30	0.43	2.30	1	2	0	2.49
7	593.06	213.98	0.41	2.44	0.41	2.44	1	3	0	2.49
7	594.06	186.62	0.44	2.25	0.43	2.30	0		1	.
7	595.06	250.38	0.41	2.44	0.41	2.44	0		1	.
7	596.06	191.79	0.46	2.18	0.43	2.30	0		0	.
7	597.06	195.03	0.41	2.45	0.41	2.44	0		0	.
7	598.06	199.03	0.40	2.47	0.41	2.44	0		0	.
7	599.06	232.23	0.41	2.46	0.41	2.44	0		0	.
7	600.06	197.83	0.39	2.54	0.39	2.59	0		1	.
7	601.06	670.90	0.40	2.47	0.41	2.44	0		0	.
7	603.06	240.27	0.39	2.59	0.39	2.59	1	4	0	2.49
7	604.06	217.32	0.47	2.15	0.47	2.15	1	1	0	2.36
7	605.06	341.14	0.43	2.35	0.43	2.35	1	1	0	2.59
7	606.06	311.71	0.51	1.96	0.47	2.15	0		1	.
7	607.06	262.63	0.42	2.36	0.42	2.36	1	4	0	2.35
7	608.06	241.01	0.42	2.36	0.42	2.36	0		1	.
7	609.06	210.14	0.46	2.15	0.47	2.15	0		0	.
7	610.06	207.07	0.41	2.42	0.41	2.42	1	3	0	2.15
7	611.06	256.86	0.39	2.54	0.39	2.54	1	3	0	2.15
7	612.06	273.34	0.50	1.98	0.50	1.98	1	2	0	2.15
7	613.06	242.54	0.46	2.17	0.46	2.17	1	3	0	2.15
7	614.06	213.01	0.48	2.10	0.48	2.10	1	2	0	2.15
7	615.06	215.21	0.39	2.58	0.39	2.58	1	3	0	2.15
7	616.06	308.94	0.40	2.53	0.39	2.58	0		1	.
7	617.06	306.67	0.50	2.01	0.50	2.01	1	2	0	2.00
7	618.06	505.24	0.49	2.02	0.50	2.00	0		0	.
7	619.06	530.50	0.49	2.06	0.50	2.00	0		1	.
7	620.06	302.10	0.50	2.00	0.50	2.00	1	1	0	2.15
7	621.06	302.00	0.36	2.76	0.36	2.76	1	3	0	2.00
7	622.06	496.47	0.35	2.89	0.35	2.89	1	3	0	2.00
7	623.06	498.27	0.35	2.84	0.35	2.84	1	1	0	2.00
7	624.06	501.80	0.35	2.87	0.35	2.87	1	0	0	2.84
7	625.06	313.38	0.35	2.86	0.35	2.87	0		1	.
7	626.06	311.14	0.43	2.33	0.43	2.33	1	2	0	2.66
7	627.06	509.04	0.42	2.40	0.43	2.33	0		1	.
7	628.06	529.46	0.38	2.63	0.38	2.63	1	1	0	2.87
7	629.06	353.25	0.38	2.66	0.38	2.66	1	0	0	2.63
7	630.06	273.81	0.37	2.68	0.37	2.68	1	3	0	2.66
7	631.06	272.34	0.39	2.54	0.39	2.54	1	0	0	2.66
7	632.06	818.55	0.39	2.58	0.39	2.54	0		1	.
7	634.06	323.92	0.31	3.25	0.31	3.25	1	3	0	2.54
7	635.06	306.07	0.40	2.47	0.40	2.47	1	2	0	2.54
7	636.06	307.37	0.39	2.56	0.39	2.56	1	0	0	2.54
7	637.06	415.95	0.39	2.56	0.39	2.56	0		1	.
7	638.06	460.16	0.39	2.54	0.39	2.56	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	639.06	0	.	0	0	2	639	0	1.71	1	155.58
7	640.06	0	.	0	0	3	640	0	1.24	2	104.58
7	641.06	1	.	1	0	1	641	0	2.02	1	114.78
7	642.06	1	.	1	0	3	642	0	1.71	1	104.58
7	643.06	1	.	1	0	.	643	0	0.47	1	114.78
7	645.06	0	.	0	0	1	645	0	0.62	1	84.18
7	646.06	0	.	1	0	.	646	0	0.62	2	84.18
7	647.06	0	.	0	0	.	647	0	0.31	2	145.38
7	648.06	0	0	1	0	1	650	0	0.78	2	135.18
7	649.06	0	.	0	0	.	649	0	0.47	2	135.18
7	650.06	0	.	0	0	2	650	0	0.78	1	84.18
7	651.06	0	.	0	0	1	651	0	0.31	1	114.78
7	655.06	0	.	1	0	.	655	0	0.31	1	22.98
7	656.06	0	.	1	0	.	656	0	0.31	2	84.18
7	657.06	0	.	1	0	.	657	0	0.31	1	135.18
7	658.06	1	.	1	0	.	658	0	0.31	0	53.58
7	659.06	0	.	1	0	.	659	0	0.47	1	145.38
7	661.06	0	.	0	0	.	661	0	0.31	1	135.18
7	662.06	0	0	0	0	1	661	0	0.62	2	135.18
7	663.06	1	.	1	0	.	663	0	0.31	1	145.38
7	664.06	1	.	1	0	.	664	0	0.31	1	155.58
7	666.06	1	.	1	0	1	666	1	2.49	1	22.98
7	667.06	1	0	1	0	1	666	1	2.80	1	22.98
7	670.06	1	.	0	0	1	670	1	1.87	1	2.58
7	671.06	1	0	1	0	1	670	1	1.71	1	2.58
7	672.06	1	.	1	0	2	672	0	1.40	1	114.78
7	93.07	1	.	0	0	.	93	0	0.31	2	2.58
7	95.07	0	.	0	0	.	95	0	0.31	2	2.58
7	200.07	0	.	0	0	2	200	0	0.78	0	2.58
7	201.07	0	0	1	0	2	200	0	0.78	1	2.58
7	221.07	0	.	0	0	1	221	0	0.93	1	22.98
7	242.07	1	.	1	0	2	242	0	0.47	1	22.98
7	243.07	0	.	0	0	1	243	0	0.47	0	22.98
7	244.07	0	.	1	0	1	244	0	0.93	1	22.98
7	252.07	0	.	1	0	1	252	0	1.09	0	63.78
7	255.07	0	.	0	0	2	255	0	1.09	1	63.78
7	270.07	0	.	0	0	1	270	0	1.24	2	12.78
7	273.07	0	.	1	0	1	273	0	0.93	2	33.18
7	276.07	1	.	1	0	2	276	0	1.24	1	2.58
7	277.07	1	0	0	0	1	276	0	1.24	1	2.58
7	278.07	0	.	1	0	1	278	0	0.62	1	33.18
7	280.07	0	.	1	0	1	280	0	1.40	2	22.98
7	282.07	0	.	0	0	2	282	0	1.55	1	2.58
7	285.07	0	.	0	0	1	285	0	1.09	1	33.18
7	287.07	1	1	1	0	1	285	0	1.09	1	33.18
7	288.07	1	.	1	0	1	288	0	1.40	2	12.78
7	298.07	0	.	0	1	1	298	1	1.24	2	33.18
7	299.07	0	.	1	0	2	299	0	1.40	1	12.78
7	300.07	1	1	0	0	1	299	0	1.40	1	2.58
7	301.07	0	.	1	0	2	301	1	1.24	1	33.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	639.06	430.26	0.38	2.63	0.38	2.63	1	0	0	2.62
7	640.06	343.64	0.48	2.09	0.48	2.09	1	2	0	2.63
7	641.06	422.65	0.25	4.00	0.25	4.00	1	3	0	2.63
7	642.06	594.89	0.38	2.62	0.38	2.62	1	0	0	2.56
7	643.06	883.41	0.43	2.35	0.43	2.35	1	0	0	2.63
7	645.06	595.33	0.37	2.70	0.37	2.70	1	3	0	2.35
7	646.06	651.72	0.36	2.76	0.36	2.76	1	3	0	2.35
7	647.06	697.19	0.97	1.03	0.97	1.03	1	0	0	2.35
7	648.06	694.93	0.82	1.22	0.80	1.24	0		1	.
7	649.06	102.77	0.87	1.14	0.87	1.14	1	0	0	1.03
7	650.06	531.93	0.80	1.24	0.80	1.24	1	0	0	1.14
7	651.06	933.76	0.12	8.65	0.12	8.65	1	3	0	.
7	655.06	721.59	1.03	0.97	1.03	0.97	1	0	0	1.24
7	656.06	770.43	1.45	0.69	1.45	0.69	1	0	0	1.50
7	657.06	1072.34	0.66	1.50	0.66	1.50	1	0	0	0.97
7	658.06	979.98	0.92	1.09	0.92	1.09	1	0	0	0.69
7	659.06	1252.95	0.98	1.02	0.98	1.02	1	0	0	1.09
7	661.06	1010.74	0.67	1.48	0.67	1.48	1	0	0	1.02
7	662.06	1222.05	0.65	1.55	0.67	1.48	0		1	.
7	663.06	1049.52	0.86	1.17	0.86	1.17	1	0	0	1.48
7	664.06	142.65	0.92	1.09	0.92	1.09	1	0	0	1.17
7	666.06	183.65	0.23	4.35	0.23	4.35	1	3	0	3.85
7	667.06	181.41	0.23	4.27	0.23	4.35	0		1	.
7	670.06	624.96	0.14	7.02	0.14	7.02	1	3	0	.
7	671.06	627.99	0.14	6.98	0.14	7.02	0		0	.
7	672.06	327.06	0.23	4.41	0.23	4.41	1	3	0	.
7	93.07	84.08	1.14	0.88	1.14	0.88	1	0	0	1.12
7	95.07	100.43	0.90	1.12	0.90	1.12	1	0	0	.
7	200.07	57.02	0.74	1.35	0.74	1.35	1	0	0	0.88
7	201.07	121.89	0.69	1.45	0.74	1.35	0		1	.
7	221.07	141.71	0.99	1.01	0.99	1.01	1	0	0	1.35
7	242.07	71.81	0.66	1.51	0.66	1.51	1	3	0	1.01
7	243.07	76.04	0.73	1.38	0.73	1.38	1	2	0	1.01
7	244.07	166.00	0.67	1.50	0.67	1.50	1	1	0	1.01
7	252.07	209.27	0.65	1.54	0.65	1.54	1	0	0	1.50
7	255.07	165.36	0.66	1.52	0.66	1.52	1	0	0	1.54
7	270.07	423.06	0.85	1.18	0.85	1.18	1	2	0	1.52
7	273.07	309.54	0.66	1.52	0.66	1.52	1	1	0	1.52
7	276.07	118.85	0.63	1.58	0.63	1.58	1	1	0	1.52
7	277.07	83.52	0.64	1.57	0.63	1.58	0		1	.
7	278.07	236.83	0.68	1.47	0.68	1.47	1	2	0	1.52
7	280.07	229.26	0.86	1.17	0.86	1.17	1	2	0	1.52
7	282.07	195.63	0.62	1.61	0.62	1.61	1	3	0	1.58
7	285.07	244.24	0.64	1.56	0.64	1.56	1	3	0	1.52
7	287.07	122.25	0.63	1.59	0.64	1.56	0		1	.
7	288.07	264.36	0.69	1.44	0.69	1.44	1	2	0	1.58
7	298.07	123.79	0.63	1.59	0.63	1.59	1	2	0	1.67
7	299.07	124.69	0.60	1.67	0.60	1.67	1	4	0	1.58
7	300.07	92.16	0.60	1.68	0.60	1.67	0		1	.
7	301.07	94.56	0.59	1.69	0.59	1.69	1	3	0	1.67

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	302.07	0	0	1	0	2	301	1	1.40	1	33.18
7	306.07	1	0	1	0	1	338	0	1.40	0	22.98
7	307.07	1	1	1	0	1	298	1	1.71	2	22.98
7	308.07	1	.	1	0	1	308	0	1.24	2	33.18
7	309.07	1	0	1	0	1	310	0	1.40	2	33.18
7	310.07	1	.	1	0	1	310	0	1.24	1	22.98
7	315.07	1	.	1	0	1	315	0	0.78	2	33.18
7	318.07	1	0	1	0	1	339	0	1.71	2	33.18
7	319.07	1	.	1	0	1	319	1	2.02	2	33.18
7	320.07	1	1	1	0	1	301	1	1.40	1	12.78
7	321.07	1	0	0	1	1	319	1	1.87	2	22.98
7	323.07	1	1	1	0	1	336	0	1.87	2	33.18
7	324.07	1	.	1	0	1	324	1	1.71	1	22.98
7	325.07	0	1	0	0	2	324	1	1.87	1	22.98
7	326.07	1	.	1	0	1	326	0	2.02	2	33.18
7	328.07	0	.	0	0	2	328	0	1.24	1	22.98
7	329.07	0	.	0	0	1	329	1	1.87	2	33.18
7	330.07	0	0	0	1	1	329	1	2.18	2	33.18
7	331.07	1	1	1	0	1	329	1	2.18	2	33.18
7	332.07	0	1	0	1	1	329	1	2.64	2	33.18
7	335.07	1	1	1	0	1	329	1	2.18	2	22.98
7	336.07	0	.	1	0	1	336	0	1.55	1	12.78
7	337.07	0	0	0	0	1	336	0	1.55	1	12.78
7	338.07	1	.	0	0	2	338	0	1.40	1	22.98
7	339.07	1	.	1	0	1	339	0	1.24	1	33.18
7	340.07	1	1	1	0	2	328	0	1.09	1	33.18
7	341.07	1	1	1	0	1	326	0	1.87	1	33.18
7	342.07	1	0	1	0	1	361	1	2.64	1	22.98
7	343.07	1	.	1	0	1	343	0	0.93	2	2.58
7	344.07	0	.	1	0	1	344	0	0.78	0	2.58
7	345.07	1	.	1	1	1	345	1	2.64	2	33.18
7	347.07	0	1	0	0	1	345	1	2.18	2	33.18
7	349.07	1	0	1	0	1	379	1	2.64	1	33.18
7	351.07	0	1	1	0	1	361	1	2.18	1	22.98
7	352.07	1	0	1	0	1	315	0	1.09	1	33.18
7	353.07	0	0	1	0	1	345	1	2.49	2	63.78
7	355.07	0	.	1	0	1	355	0	2.80	1	53.58
7	356.07	0	1	1	0	1	379	1	2.49	1	2.58
7	358.07	0	0	0	0	1	379	1	2.64	1	63.78
7	361.07	1	.	1	1	1	361	1	2.02	1	22.98
7	363.07	0	1	1	0	1	361	1	2.49	1	22.98
7	366.07	1	1	1	0	1	361	1	2.18	1	22.98
7	370.07	0	.	0	0	1	370	0	2.02	1	22.98
7	372.07	1	.	1	0	1	372	0	2.64	2	33.18
7	373.07	0	1	0	0	1	326	0	1.87	1	33.18
7	375.07	0	0	0	0	2	326	0	2.18	1	33.18
7	378.07	1	.	1	0	1	378	0	2.33	1	22.98
7	379.07	1	.	1	0	1	379	1	2.33	1	22.98
7	383.07	1	1	0	0	1	384	0	2.02	2	73.98
7	384.07	0	.	1	0	1	384	0	2.64	0	63.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	302.07	188.42	0.59	1.68	0.59	1.69	0		1	.
7	306.07	97.13	0.60	1.66	0.59	1.69	0		0	.
7	307.07	102.00	0.62	1.61	0.63	1.59	0		1	.
7	308.07	102.94	0.54	1.85	0.54	1.85	1	3	0	1.69
7	309.07	103.57	0.57	1.75	0.62	1.61	0		1	.
7	310.07	402.73	0.62	1.61	0.62	1.61	1	2	0	1.69
7	315.07	242.74	0.58	1.72	0.58	1.72	1	3	0	1.80
7	318.07	111.91	0.57	1.75	0.55	1.82	0		1	.
7	319.07	130.26	0.56	1.78	0.56	1.78	1	2	0	1.82
7	320.07	116.75	0.59	1.69	0.59	1.69	0		0	.
7	321.07	231.20	0.56	1.78	0.56	1.78	0		1	.
7	323.07	111.45	0.60	1.66	0.59	1.68	0		0	.
7	324.07	113.08	0.54	1.84	0.54	1.84	1	3	0	1.82
7	325.07	115.88	0.53	1.89	0.54	1.84	0		1	.
7	326.07	306.54	0.52	1.91	0.52	1.91	1	1	0	1.93
7	328.07	124.43	0.55	1.80	0.55	1.80	1	1	0	1.69
7	329.07	125.89	0.52	1.91	0.52	1.91	1	2	0	1.91
7	330.07	129.10	0.51	1.95	0.52	1.91	0		1	.
7	331.07	131.00	0.50	2.01	0.52	1.91	0		0	.
7	332.07	360.16	0.50	2.02	0.52	1.91	0		0	.
7	335.07	131.99	0.49	2.03	0.52	1.91	0		0	.
7	336.07	133.36	0.59	1.68	0.59	1.68	1	1	0	1.67
7	337.07	98.23	0.59	1.71	0.59	1.68	0		1	.
7	338.07	110.18	0.59	1.69	0.59	1.69	1	0	0	1.68
7	339.07	104.31	0.55	1.82	0.55	1.82	1	1	0	1.80
7	340.07	122.46	0.55	1.81	0.55	1.80	0		1	.
7	341.07	129.33	0.49	2.03	0.52	1.91	0		0	.
7	342.07	81.31	0.48	2.09	0.47	2.12	0		0	.
7	343.07	76.81	0.36	2.74	0.36	2.74	1	3	0	1.52
7	344.07	132.13	0.33	3.03	0.33	3.03	1	3	0	1.52
7	345.07	243.87	0.43	2.34	0.43	2.34	1	3	0	2.07
7	347.07	315.48	0.41	2.45	0.43	2.34	0		1	.
7	349.07	248.51	0.46	2.19	0.48	2.09	0		1	.
7	351.07	106.61	0.47	2.13	0.47	2.12	0		1	.
7	352.07	62.80	0.57	1.76	0.58	1.72	0		1	.
7	353.07	251.82	0.37	2.69	0.43	2.34	0		0	.
7	355.07	184.61	0.37	2.67	0.37	2.67	1	2	0	2.07
7	356.07	328.86	0.39	2.57	0.48	2.09	0		0	.
7	358.07	331.03	0.38	2.65	0.48	2.09	0		0	.
7	361.07	255.19	0.47	2.12	0.47	2.12	1	3	0	1.91
7	363.07	379.24	0.47	2.11	0.47	2.12	0		0	.
7	366.07	263.79	0.47	2.13	0.47	2.12	0		0	.
7	370.07	277.11	0.52	1.93	0.52	1.93	1	1	0	1.82
7	372.07	114.52	0.36	2.78	0.36	2.78	1	3	0	2.07
7	373.07	273.54	0.52	1.94	0.52	1.91	0		1	.
7	375.07	281.95	0.50	2.02	0.52	1.91	0		0	.
7	378.07	137.67	0.48	2.07	0.48	2.07	1	1	0	1.91
7	379.07	283.65	0.48	2.09	0.48	2.09	1	2	0	2.07
7	383.07	77.98	0.37	2.68	0.37	2.70	0		1	.
7	384.07	148.08	0.37	2.70	0.37	2.70	1	1	0	2.07

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	385.07	0	1	1	0	2	384	0	1.87	0	22.98
7	390.07	1	.	1	1	1	390	0	2.02	0	12.78
7	391.07	0	1	1	0	1	384	0	1.87	1	22.98
7	392.07	1	.	1	0	1	392	0	2.18	2	43.38
7	393.07	1	1	1	0	2	384	0	1.87	1	22.98
7	396.07	1	.	1	1	2	396	0	2.18	0	22.98
7	397.07	1	.	1	1	1	397	0	2.18	0	22.98
7	398.07	0	.	0	0	1	398	0	2.33	2	2.58
7	400.07	1	1	0	0	1	410	0	2.33	0	2.58
7	403.07	0	.	1	0	1	403	0	1.24	0	33.18
7	406.07	0	.	1	0	1	406	0	2.18	1	63.78
7	409.07	1	0	1	0	1	396	0	2.33	1	33.18
7	410.07	0	.	0	0	1	410	0	2.02	0	33.18
7	411.07	0	.	1	0	1	411	0	2.33	1	33.18
7	412.07	1	1	1	0	1	411	0	2.49	1	33.18
7	413.07	0	1	0	0	1	411	0	2.49	1	33.18
7	415.07	0	0	0	0	1	411	0	2.18	1	33.18
7	416.07	0	0	0	0	2	411	0	2.33	1	33.18
7	417.07	0	0	0	0	1	411	0	2.18	2	33.18
7	418.07	0	0	1	1	1	411	0	1.87	2	43.38
7	419.07	1	1	1	0	1	411	0	2.18	1	33.18
7	420.07	1	0	1	0	1	411	0	2.02	2	43.38
7	421.07	1	0	1	0	1	411	0	2.02	1	43.38
7	422.07	1	.	1	0	1	422	0	1.87	2	63.78
7	423.07	1	0	1	0	1	411	0	1.87	1	43.38
7	424.07	1	.	0	0	1	424	0	1.71	1	63.78
7	425.07	1	0	1	0	1	426	0	2.49	2	73.98
7	426.07	1	.	1	0	1	426	0	2.02	1	73.98
7	427.07	1	1	1	1	1	426	0	2.80	2	84.18
7	428.07	0	1	1	0	1	426	0	2.49	1	73.98
7	429.07	1	0	1	0	1	426	0	2.80	1	73.98
7	430.07	1	0	1	0	1	426	0	2.80	2	84.18
7	431.07	1	.	1	0	1	431	1	2.64	2	84.18
7	433.07	0	1	0	0	1	431	1	2.95	2	84.18
7	435.07	0	0	1	0	1	431	1	2.95	2	53.58
7	436.07	0	1	1	0	1	426	0	2.80	1	33.18
7	437.07	0	.	0	0	1	437	1	2.64	1	33.18
7	438.07	1	.	0	0	1	438	0	2.80	1	84.18
7	439.07	1	1	1	0	1	437	1	2.64	1	33.18
7	440.07	0	1	0	0	1	437	1	2.80	1	63.78
7	441.07	0	0	1	0	1	438	0	2.80	2	22.98
7	442.07	1	0	1	0	1	437	1	2.64	1	53.58
7	443.07	1	.	1	0	1	443	0	2.18	2	104.58
7	444.07	1	0	1	0	1	445	0	2.80	2	104.58
7	445.07	1	.	1	0	1	445	0	2.64	2	33.18
7	446.07	1	0	1	0	1	445	0	2.80	2	84.18
7	448.07	0	0	0	1	1	445	0	2.64	2	84.18
7	451.07	0	0	0	0	1	445	0	2.33	2	84.18
7	452.07	0	1	1	0	1	438	0	2.80	1	84.18
7	453.07	1	1	1	0	1	438	0	2.49	1	12.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	385.07	322.72	0.33	3.00	0.37	2.70	0		0	.
7	390.07	141.28	0.31	3.22	0.31	3.22	1	4	0	2.70
7	391.07	116.98	0.35	2.90	0.37	2.70	0		0	.
7	392.07	145.65	0.30	3.29	0.30	3.29	1	4	0	3.22
7	393.07	248.98	0.34	2.95	0.37	2.70	0		0	.
7	396.07	151.39	0.28	3.52	0.28	3.52	1	1	0	3.37
7	397.07	205.27	0.30	3.37	0.30	3.37	1	4	0	3.29
7	398.07	337.00	0.29	3.41	0.29	3.41	1	2	0	3.52
7	400.07	252.32	0.28	3.58	0.27	3.66	0		1	.
7	403.07	264.10	0.63	1.59	0.63	1.59	1	2	0	1.80
7	406.07	353.82	0.12	8.35	0.12	8.35	1	3	0	.
7	409.07	152.42	0.28	3.54	0.28	3.52	0		1	.
7	410.07	154.76	0.27	3.66	0.27	3.66	1	3	0	3.52
7	411.07	156.76	0.28	3.59	0.28	3.59	1	1	0	3.52
7	412.07	160.46	0.28	3.61	0.28	3.59	0		1	.
7	413.07	379.38	0.28	3.63	0.28	3.59	0		0	.
7	415.07	163.93	0.27	3.64	0.28	3.59	0		0	.
7	416.07	165.13	0.27	3.65	0.28	3.59	0		0	.
7	417.07	117.92	0.27	3.65	0.28	3.59	0		0	.
7	418.07	167.60	0.27	3.72	0.28	3.59	0		0	.
7	419.07	122.12	0.25	3.98	0.28	3.59	0		0	.
7	420.07	123.06	0.23	4.39	0.28	3.59	0		0	.
7	421.07	99.27	0.23	4.39	0.28	3.59	0		0	.
7	422.07	124.16	0.23	4.35	0.23	4.35	1	2	0	3.59
7	423.07	100.87	0.23	4.42	0.28	3.59	0		0	.
7	424.07	102.97	0.22	4.48	0.22	4.48	1	3	0	3.59
7	425.07	101.27	0.22	4.47	0.22	4.51	0		1	.
7	426.07	86.28	0.22	4.51	0.22	4.51	1	1	0	3.59
7	427.07	106.01	0.21	4.65	0.22	4.51	0		0	.
7	428.07	107.98	0.22	4.49	0.22	4.51	0		0	.
7	429.07	87.85	0.22	4.62	0.22	4.51	0		0	.
7	430.07	88.82	0.21	4.69	0.22	4.51	0		0	.
7	431.07	409.47	0.19	5.16	0.19	5.16	1	3	0	4.51
7	433.07	407.20	0.19	5.24	0.19	5.16	0		1	.
7	435.07	181.68	0.19	5.24	0.19	5.16	0		0	.
7	436.07	183.92	0.21	4.66	0.22	4.51	0		0	.
7	437.07	94.13	0.20	4.95	0.20	4.95	1	2	0	4.51
7	438.07	185.79	0.20	5.07	0.20	5.07	1	1	0	4.51
7	439.07	66.70	0.20	4.96	0.20	4.95	0		1	.
7	440.07	199.17	0.20	4.99	0.20	4.95	0		0	.
7	441.07	152.39	0.20	5.04	0.20	5.07	0		0	.
7	442.07	66.33	0.20	5.00	0.20	4.95	0		0	.
7	443.07	62.99	0.22	4.48	0.22	4.48	1	2	0	5.07
7	444.07	202.70	0.22	4.49	0.22	4.49	0		0	.
7	445.07	105.17	0.22	4.49	0.22	4.49	1	1	0	5.07
7	446.07	422.35	0.22	4.51	0.22	4.49	0		0	.
7	448.07	423.79	0.21	4.87	0.22	4.49	0		0	.
7	451.07	98.26	0.20	5.00	0.22	4.49	0		0	.
7	452.07	245.41	0.20	5.08	0.20	5.07	0		1	.
7	453.07	112.94	0.20	5.01	0.20	5.07	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	454.07	1	0	1	0	1	445	0	2.02	2	94.38
7	455.07	1	.	1	0	1	455	0	2.64	1	22.98
7	456.07	1	.	1	0	1	456	0	2.18	2	73.98
7	457.07	0	1	1	0	1	445	0	2.49	1	104.58
7	458.07	0	.	1	0	1	458	0	2.49	1	33.18
7	459.07	1	.	1	0	1	459	0	2.33	1	33.18
7	460.07	1	1	0	0	1	445	0	2.64	1	22.98
7	461.07	1	0	1	0	1	445	0	2.80	1	22.98
7	462.07	1	1	1	0	1	458	0	2.64	1	22.98
7	463.07	0	1	0	0	1	445	0	2.80	1	22.98
7	464.07	0	0	1	0	1	445	0	2.49	1	84.18
7	465.07	0	0	0	0	1	445	0	2.80	1	104.58
7	466.07	1	1	1	0	1	445	0	2.64	1	22.98
7	467.07	1	1	0	0	1	458	0	2.64	1	22.98
7	468.07	0	1	1	0	1	458	0	2.64	1	33.18
7	470.07	1	1	1	0	1	458	0	2.64	2	104.58
7	472.07	0	1	0	0	1	458	0	2.02	2	22.98
7	473.07	0	1	1	0	1	458	0	2.64	2	22.98
7	475.07	1	.	1	0	1	475	1	2.02	2	73.98
7	476.07	1	1	0	0	1	458	0	2.33	1	12.78
7	477.07	1	0	1	0	1	475	1	2.18	2	73.98
7	478.07	1	.	1	0	1	478	1	2.18	1	73.98
7	479.07	0	.	0	0	2	479	0	2.33	1	73.98
7	480.07	1	0	0	0	1	478	1	2.33	1	2.58
7	481.07	0	.	0	0	1	481	0	2.49	0	2.58
7	482.07	0	.	1	0	1	482	1	2.02	2	73.98
7	483.07	0	0	1	0	1	481	0	2.02	1	43.38
7	484.07	0	.	0	0	1	484	1	2.18	1	84.18
7	485.07	1	1	1	0	1	482	1	2.64	2	104.58
7	486.07	1	1	0	1	1	484	1	2.64	1	63.78
7	487.07	0	1	0	1	1	482	1	2.80	2	73.98
7	488.07	1	0	1	0	1	484	1	2.80	1	84.18
7	489.07	0	0	0	0	1	482	1	2.49	2	104.58
7	490.07	1	0	1	0	1	484	1	3.11	1	84.18
7	491.07	0	0	1	0	1	482	1	2.33	2	104.58
7	492.07	0	1	1	0	1	484	1	3.26	1	84.18
7	493.07	0	.	1	0	1	493	1	1.71	0	104.58
7	494.07	1	.	0	0	1	494	1	1.71	1	104.58
7	495.07	1	1	1	0	1	484	1	2.64	1	33.18
7	496.07	1	.	0	0	1	496	1	2.33	1	2.58
7	497.07	1	0	1	0	1	484	1	2.33	1	84.18
7	498.07	0	1	0	1	1	484	1	2.02	0	94.38
7	499.07	1	.	1	0	1	499	1	1.87	2	104.58
7	500.07	1	.	1	0	1	500	1	1.55	1	104.58
7	501.07	1	.	1	0	2	501	1	2.02	1	63.78
7	502.07	0	.	0	0	1	502	1	2.18	0	63.78
7	503.07	1	1	1	0	1	504	0	2.02	1	84.18
7	504.07	0	.	0	0	1	504	0	2.02	2	84.18
7	505.07	0	0	0	0	2	504	0	2.33	1	104.58
7	506.07	0	0	1	0	1	504	0	2.49	2	104.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	454.07	197.53	0.20	4.91	0.22	4.49	0		0	.
7	455.07	144.24	0.22	4.58	0.22	4.58	1	3	0	5.07
7	456.07	64.56	0.20	4.94	0.20	4.94	1	2	0	4.49
7	457.07	214.35	0.22	4.50	0.22	4.49	0		1	.
7	458.07	211.48	0.20	4.96	0.20	4.96	1	1	0	4.49
7	459.07	202.40	0.20	5.03	0.20	5.03	1	3	0	4.49
7	460.07	204.74	0.22	4.47	0.22	4.49	0		0	.
7	461.07	220.79	0.22	4.51	0.22	4.49	0		0	.
7	462.07	206.41	0.19	5.36	0.20	4.96	0		0	.
7	463.07	99.93	0.22	4.54	0.22	4.49	0		0	.
7	464.07	73.67	0.20	5.05	0.22	4.49	0		0	.
7	465.07	214.15	0.21	4.81	0.22	4.49	0		0	.
7	466.07	224.13	0.20	5.01	0.22	4.49	0		0	.
7	467.07	215.25	0.20	5.04	0.20	4.96	0		0	.
7	468.07	590.76	0.20	5.01	0.20	4.96	0		0	.
7	470.07	592.06	0.20	4.98	0.20	4.96	0		1	.
7	472.07	225.56	0.18	5.44	0.20	4.96	0		0	.
7	473.07	476.01	0.19	5.32	0.20	4.96	0		0	.
7	475.07	289.05	0.20	5.06	0.20	5.06	1	2	0	5.50
7	476.07	152.45	0.18	5.42	0.20	4.96	0		0	.
7	477.07	154.49	0.20	5.02	0.20	5.06	0		1	.
7	478.07	149.82	0.19	5.25	0.19	5.25	1	3	0	5.50
7	479.07	300.56	0.18	5.50	0.18	5.50	1	0	0	4.96
7	480.07	302.43	0.19	5.19	0.19	5.25	0		1	.
7	481.07	160.79	0.19	5.14	0.19	5.14	1	1	0	5.50
7	482.07	184.35	0.19	5.14	0.19	5.14	1	3	0	5.14
7	483.07	127.22	0.20	5.12	0.19	5.14	0		1	.
7	484.07	115.35	0.20	5.10	0.20	5.10	1	2	0	5.14
7	485.07	156.16	0.19	5.16	0.19	5.14	0		1	.
7	486.07	162.66	0.20	5.11	0.20	5.10	0		1	.
7	487.07	129.86	0.19	5.14	0.19	5.14	0		0	.
7	488.07	110.27	0.20	5.09	0.20	5.10	0		0	.
7	489.07	131.80	0.19	5.15	0.19	5.14	0		0	.
7	490.07	118.58	0.20	5.10	0.20	5.10	0		0	.
7	491.07	132.73	0.19	5.15	0.19	5.14	0		0	.
7	492.07	112.94	0.20	5.10	0.20	5.10	0		0	.
7	493.07	111.21	0.24	4.12	0.24	4.12	1	2	0	5.14
7	494.07	240.51	0.23	4.26	0.23	4.26	1	3	0	5.14
7	495.07	360.96	0.20	5.07	0.20	5.10	0		0	.
7	496.07	134.83	0.26	3.83	0.26	3.83	1	2	0	3.99
7	497.07	133.66	0.20	5.04	0.20	5.10	0		0	.
7	498.07	122.62	0.24	4.17	0.20	5.10	0		0	.
7	499.07	116.98	0.25	3.99	0.25	3.99	1	1	0	3.98
7	500.07	162.56	0.25	3.98	0.25	3.98	1	1	0	5.14
7	501.07	172.41	0.21	4.86	0.21	4.86	1	3	0	5.14
7	502.07	140.84	0.25	4.00	0.25	4.00	1	3	0	3.99
7	503.07	144.61	0.25	3.95	0.25	3.98	0		1	.
7	504.07	123.22	0.25	3.98	0.25	3.98	1	0	0	3.99
7	505.07	124.52	0.25	4.00	0.25	3.98	0		0	.
7	506.07	153.78	0.25	3.95	0.25	3.98	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	507.07	1	1	1	0	1	504	0	2.95	1	94.38
7	508.07	0	1	1	0	1	504	0	3.26	2	94.38
7	509.07	1	.	1	0	1	509	1	2.33	2	104.58
7	510.07	0	1	1	0	1	504	0	2.18	2	94.38
7	511.07	1	0	0	0	1	509	1	2.49	2	104.58
7	512.07	1	0	1	0	1	509	1	2.33	2	135.18
7	513.07	1	0	1	0	1	509	1	2.33	2	104.58
7	514.07	1	0	1	0	1	509	1	2.49	2	94.38
7	515.07	1	1	1	0	1	537	0	2.64	2	94.38
7	516.07	0	.	0	1	1	516	0	2.33	1	2.58
7	517.07	1	.	1	1	1	517	0	2.64	2	94.38
7	518.07	1	1	1	0	1	504	0	2.95	1	135.18
7	519.07	0	0	1	1	1	537	0	2.95	2	94.38
7	520.07	1	.	1	0	1	520	1	2.33	2	94.38
7	521.07	1	.	1	0	1	521	1	3.11	2	33.18
7	522.07	1	0	1	0	1	539	1	3.11	1	33.18
7	523.07	1	0	1	0	2	539	1	2.95	1	33.18
7	524.07	0	0	1	0	1	541	0	1.87	2	135.18
7	525.07	0	1	1	0	1	541	0	1.87	1	135.18
7	526.07	0	1	1	0	1	537	0	2.80	1	2.58
7	530.07	1	1	1	0	1	531	1	2.33	1	63.78
7	531.07	0	.	0	0	1	531	1	1.87	1	63.78
7	532.07	1	.	1	0	3	532	0	3.11	1	63.78
7	533.07	0	0	1	0	1	531	1	2.33	1	104.58
7	534.07	0	0	0	0	1	531	1	2.33	1	104.58
7	535.07	1	.	1	0	1	535	0	2.33	1	94.38
7	536.07	1	0	1	0	1	531	1	2.49	1	53.58
7	537.07	0	.	1	0	1	537	0	2.80	1	94.38
7	538.07	0	0	0	0	1	537	0	2.49	1	94.38
7	539.07	1	.	1	0	1	539	1	2.64	1	94.38
7	540.07	1	0	1	0	1	541	0	1.87	1	43.38
7	541.07	1	.	1	0	2	541	0	2.95	1	43.38
7	542.07	1	1	1	0	1	541	0	2.02	1	135.18
7	543.07	1	0	1	0	2	541	0	2.18	1	84.18
7	544.07	1	0	1	0	1	541	0	2.18	1	135.18
7	545.07	1	0	1	0	1	541	0	2.18	2	135.18
7	546.07	0	0	0	0	1	541	0	2.80	2	135.18
7	547.07	0	1	0	0	1	541	0	2.49	1	53.58
7	548.07	0	0	1	0	1	541	0	2.64	1	53.58
7	549.07	1	1	1	0	1	541	0	2.33	2	33.18
7	550.07	1	0	1	0	2	541	0	2.49	1	33.18
7	551.07	1	0	1	0	1	541	0	2.18	1	33.18
7	552.07	1	1	1	0	1	541	0	1.87	2	73.98
7	553.07	0	1	1	0	1	541	0	2.02	1	63.78
7	554.07	1	0	1	0	1	541	0	1.87	1	12.78
7	555.07	1	1	1	0	1	562	0	2.02	2	84.18
7	556.07	1	0	1	0	1	562	0	1.87	0	94.38
7	557.07	0	1	1	0	1	541	0	1.71	1	53.58
7	558.07	0	.	0	0	1	558	0	1.87	1	53.58
7	559.07	1	.	0	0	1	559	0	1.87	0	135.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	507.07	152.85	0.25	3.99	0.25	3.98	0		0	.
7	508.07	135.43	0.25	3.98	0.25	3.98	0		0	.
7	509.07	155.35	0.25	4.08	0.25	4.08	1	3	0	3.98
7	510.07	136.57	0.25	4.02	0.25	3.98	0		0	.
7	511.07	111.84	0.23	4.38	0.25	4.08	0		1	.
7	512.07	138.27	0.23	4.42	0.25	4.08	0		0	.
7	513.07	171.10	0.23	4.43	0.25	4.08	0		0	.
7	514.07	174.17	0.23	4.39	0.25	4.08	0		0	.
7	515.07	397.76	0.27	3.65	0.27	3.69	0		1	.
7	516.07	167.53	0.25	4.05	0.25	4.05	1	1	0	3.98
7	517.07	110.71	0.27	3.66	0.27	3.66	1	2	0	4.05
7	518.07	175.24	0.25	4.00	0.25	3.98	0		0	.
7	519.07	169.67	0.27	3.67	0.27	3.69	0		0	.
7	520.07	315.58	0.27	3.74	0.27	3.74	1	3	0	3.69
7	521.07	313.42	0.26	3.80	0.26	3.80	1	3	0	3.69
7	522.07	312.51	0.27	3.69	0.28	3.61	0		0	.
7	523.07	115.48	0.27	3.64	0.28	3.61	0		1	.
7	524.07	114.05	0.27	3.65	0.27	3.74	0		0	.
7	525.07	401.53	0.27	3.76	0.27	3.74	0		0	.
7	526.07	538.54	0.27	3.66	0.27	3.69	0		0	.
7	530.07	188.96	0.23	4.31	0.25	3.97	0		0	.
7	531.07	215.75	0.25	3.97	0.25	3.97	1	2	0	3.98
7	532.07	95.29	0.28	3.62	0.28	3.62	1	0	0	3.69
7	533.07	96.63	0.23	4.33	0.25	3.97	0		1	.
7	534.07	163.23	0.23	4.33	0.25	3.97	0		0	.
7	535.07	234.60	0.25	4.01	0.25	4.01	1	3	0	4.05
7	536.07	164.46	0.23	4.32	0.25	3.97	0		0	.
7	537.07	165.80	0.27	3.69	0.27	3.69	1	1	0	4.05
7	538.07	172.77	0.27	3.68	0.27	3.69	0		0	.
7	539.07	254.05	0.28	3.61	0.28	3.61	1	2	0	3.69
7	540.07	252.09	0.27	3.75	0.27	3.74	0		1	.
7	541.07	118.18	0.27	3.74	0.27	3.74	1	0	0	3.62
7	542.07	188.89	0.27	3.73	0.27	3.74	0		0	.
7	543.07	125.02	0.27	3.76	0.27	3.74	0		0	.
7	544.07	126.33	0.27	3.74	0.27	3.74	0		0	.
7	545.07	126.83	0.27	3.77	0.27	3.74	0		0	.
7	546.07	222.49	0.26	3.79	0.27	3.74	0		0	.
7	547.07	225.19	0.27	3.74	0.27	3.74	0		0	.
7	548.07	348.65	0.27	3.74	0.27	3.74	0		0	.
7	549.07	336.30	0.27	3.77	0.27	3.74	0		0	.
7	550.07	355.59	0.27	3.75	0.27	3.74	0		0	.
7	551.07	228.50	0.27	3.74	0.27	3.74	0		0	.
7	552.07	230.63	0.26	3.83	0.27	3.74	0		0	.
7	553.07	452.62	0.26	3.82	0.27	3.74	0		0	.
7	554.07	192.52	0.26	3.83	0.27	3.74	0		0	.
7	555.07	217.11	0.22	4.57	0.22	4.59	0		1	.
7	556.07	274.31	0.26	3.84	0.22	4.59	0		0	.
7	557.07	276.34	0.22	4.53	0.27	3.74	0		0	.
7	558.07	130.30	0.22	4.55	0.22	4.55	1	2	0	3.74
7	559.07	268.20	0.31	3.27	0.31	3.27	1	2	0	3.81

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	560.07	0	.	1	0	2	560	0	2.02	2	53.58
7	561.07	1	0	1	0	1	562	0	2.18	1	94.38
7	562.07	0	.	0	0	1	562	0	1.87	1	33.18
7	563.07	0	.	0	0	1	563	0	2.18	1	84.18
7	564.07	1	0	1	0	1	565	0	1.71	1	94.38
7	565.07	1	.	1	0	3	565	0	2.18	1	84.18
7	566.07	1	0	0	0	1	565	0	1.87	1	135.18
7	567.07	1	0	1	0	1	565	0	2.18	1	135.18
7	568.07	0	1	1	0	1	565	0	2.18	1	43.38
7	569.07	0	0	1	0	1	570	0	2.18	2	73.98
7	570.07	0	.	0	0	1	570	0	2.18	1	43.38
7	571.07	1	.	1	0	3	571	0	1.55	1	135.18
7	572.07	0	.	1	0	2	572	0	1.71	0	94.38
7	573.07	1	0	0	0	1	574	0	2.02	2	135.18
7	574.07	0	.	1	0	1	574	0	1.55	1	135.18
7	575.07	0	1	1	0	1	574	0	2.18	2	135.18
7	576.07	1	0	1	0	2	574	0	1.24	1	135.18
7	577.07	1	1	1	0	2	574	0	1.24	1	135.18
7	578.07	1	0	0	0	1	574	0	2.02	1	135.18
7	579.07	1	0	1	0	1	574	0	1.87	2	135.18
7	580.07	1	0	1	0	1	574	0	1.55	1	135.18
7	581.07	0	0	0	0	1	574	0	2.18	1	33.18
7	582.07	0	0	0	0	2	574	0	2.33	1	73.98
7	583.07	0	.	0	0	1	583	0	1.87	1	114.78
7	584.07	0	.	1	0	1	584	0	2.18	2	114.78
7	585.07	1	.	1	0	1	585	0	2.02	0	135.18
7	586.07	1	.	1	0	1	586	0	2.18	2	135.18
7	587.07	1	1	1	0	1	583	0	2.49	2	94.38
7	588.07	0	0	0	0	1	583	0	2.18	2	135.18
7	589.07	1	.	1	0	1	589	0	2.33	1	33.18
7	590.07	0	0	1	0	1	583	0	2.02	1	84.18
7	591.07	0	0	1	0	1	583	0	2.02	1	73.98
7	592.07	0	.	1	1	1	592	1	1.71	2	135.18
7	593.07	1	0	1	0	2	583	0	1.87	1	135.18
7	594.07	0	0	0	0	1	592	1	1.87	2	135.18
7	595.07	1	0	1	0	1	583	0	2.18	1	135.18
7	596.07	0	0	0	0	1	592	1	1.71	2	104.58
7	597.07	1	.	1	0	1	597	1	2.02	1	135.18
7	598.07	0	.	0	0	1	598	1	2.18	1	135.18
7	599.07	1	1	1	0	1	598	1	2.33	1	135.18
7	600.07	1	1	1	0	1	592	1	1.71	2	135.18
7	601.07	1	0	1	0	2	598	1	2.64	1	135.18
7	603.07	0	1	1	0	1	598	1	1.87	1	135.18
7	604.07	1	0	1	0	1	605	1	2.33	2	135.18
7	605.07	0	.	1	0	1	605	1	1.87	2	135.18
7	606.07	1	1	1	0	1	605	1	2.64	2	73.98
7	607.07	0	0	1	0	1	605	1	2.18	2	63.78
7	608.07	1	1	1	0	1	605	1	2.49	2	104.58
7	609.07	0	1	1	0	1	605	1	2.95	2	135.18
7	610.07	1	0	1	0	1	611	1	1.71	1	135.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	560.07	220.45	0.21	4.67	0.21	4.67	1	3	0	3.74
7	561.07	364.13	0.26	3.83	0.22	4.59	0		0	.
7	562.07	210.54	0.22	4.59	0.22	4.59	1	1	0	3.74
7	563.07	207.64	0.26	3.81	0.26	3.81	1	0	0	4.59
7	564.07	191.22	0.27	3.73	0.27	3.75	0		1	.
7	565.07	133.73	0.27	3.75	0.27	3.75	1	3	0	3.81
7	566.07	132.73	0.27	3.72	0.27	3.75	0		0	.
7	567.07	292.79	0.27	3.73	0.27	3.75	0		0	.
7	568.07	256.19	0.27	3.76	0.27	3.75	0		0	.
7	569.07	297.36	0.27	3.70	0.27	3.70	0		1	.
7	570.07	168.33	0.27	3.70	0.27	3.70	1	1	0	3.81
7	571.07	222.72	0.27	3.74	0.27	3.74	1	0	0	3.59
7	572.07	178.74	0.27	3.67	0.27	3.67	1	0	0	3.70
7	573.07	170.87	0.28	3.59	0.28	3.59	0		0	.
7	574.07	180.71	0.28	3.59	0.28	3.59	1	1	0	3.67
7	575.07	174.14	0.28	3.60	0.28	3.59	0		0	.
7	576.07	172.77	0.28	3.59	0.28	3.59	0		0	.
7	577.07	178.18	0.28	3.62	0.28	3.59	0		1	.
7	578.07	176.28	0.28	3.60	0.28	3.59	0		0	.
7	579.07	176.11	0.28	3.60	0.28	3.59	0		0	.
7	580.07	431.83	0.28	3.59	0.28	3.59	0		0	.
7	581.07	278.18	0.28	3.60	0.28	3.59	0		0	.
7	582.07	223.92	0.28	3.60	0.28	3.59	0		0	.
7	583.07	225.96	0.28	3.59	0.28	3.59	1	1	0	3.74
7	584.07	188.42	0.28	3.57	0.28	3.57	1	2	0	3.74
7	585.07	187.85	0.29	3.50	0.29	3.50	1	2	0	3.74
7	586.07	272.87	0.27	3.71	0.27	3.71	1	3	0	3.74
7	587.07	193.66	0.33	3.01	0.28	3.59	0		0	.
7	588.07	437.41	0.33	3.01	0.28	3.59	0		0	.
7	589.07	223.49	0.27	3.73	0.27	3.73	1	3	0	3.74
7	590.07	288.36	0.33	2.99	0.28	3.59	0		0	.
7	591.07	201.83	0.33	2.99	0.28	3.59	0		1	.
7	592.07	184.18	0.38	2.65	0.38	2.65	1	2	0	3.59
7	593.07	213.98	0.33	3.02	0.28	3.59	0		0	.
7	594.07	186.62	0.37	2.68	0.38	2.65	0		1	.
7	595.07	250.38	0.33	3.02	0.28	3.59	0		0	.
7	596.07	191.79	0.37	2.73	0.38	2.65	0		0	.
7	597.07	195.03	0.33	3.05	0.33	3.05	1	3	0	3.59
7	598.07	199.03	0.33	3.03	0.33	3.03	1	3	0	3.59
7	599.07	232.23	0.33	3.04	0.33	3.03	0		1	.
7	600.07	197.83	0.38	2.64	0.38	2.65	0		0	.
7	601.07	670.90	0.33	3.03	0.33	3.03	0		0	.
7	603.07	240.27	0.33	2.99	0.33	3.03	0		0	.
7	604.07	217.32	0.43	2.33	0.45	2.21	0		0	.
7	605.07	341.14	0.45	2.21	0.45	2.21	1	2	0	3.59
7	606.07	311.71	0.43	2.35	0.45	2.21	0		0	.
7	607.07	262.63	0.46	2.18	0.45	2.21	0		1	.
7	608.07	241.01	0.45	2.20	0.45	2.21	0		0	.
7	609.07	210.14	0.43	2.35	0.45	2.21	0		0	.
7	610.07	207.07	0.38	2.61	0.31	3.27	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	611.07	1	.	0	0	1	611	1	1.71	1	135.18
7	612.07	0	0	1	0	1	605	1	2.33	2	135.18
7	613.07	0	1	1	0	1	605	1	2.33	2	104.58
7	614.07	1	1	1	0	1	605	1	2.02	2	135.18
7	615.07	1	0	1	0	1	611	1	2.18	1	135.18
7	616.07	1	0	1	0	1	611	1	2.18	1	135.18
7	617.07	0	.	1	0	1	617	1	1.71	2	104.58
7	618.07	1	0	1	0	2	618	1	1.55	2	104.58
7	619.07	1	0	1	0	1	611	1	2.33	1	33.18
7	620.07	1	0	0	0	1	605	1	2.02	2	33.18
7	621.07	1	0	1	0	1	611	1	2.49	1	94.38
7	622.07	1	0	1	0	1	611	1	2.33	1	94.38
7	623.07	1	0	1	0	1	611	1	2.80	1	33.18
7	624.07	1	0	1	1	1	611	1	2.95	1	33.18
7	625.07	1	0	1	0	2	611	1	2.64	1	53.58
7	626.07	1	.	1	0	1	626	1	1.71	2	104.58
7	627.07	1	0	1	0	1	634	1	1.71	1	104.58
7	628.07	1	0	1	0	1	611	1	1.87	1	33.18
7	629.07	1	0	1	0	1	611	1	1.55	1	33.18
7	630.07	1	1	0	0	1	634	1	1.40	1	73.98
7	631.07	0	1	0	0	2	672	0	1.71	2	135.18
7	632.07	1	1	1	0	1	672	0	1.40	1	135.18
7	634.07	0	.	1	0	3	634	1	1.55	1	104.58
7	635.07	1	0	1	0	2	672	0	1.87	1	104.58
7	636.07	0	.	0	0	3	636	0	1.71	1	135.18
7	637.07	0	0	0	0	1	636	0	1.55	2	135.18
7	638.07	0	.	0	0	2	638	0	1.40	1	63.78
7	639.07	0	.	0	0	2	639	0	1.40	1	135.18
7	640.07	0	.	0	0	1	640	0	0.62	2	84.18
7	641.07	1	1	1	0	2	672	0	1.71	1	94.38
7	642.07	1	.	1	0	3	642	0	1.40	1	84.18
7	643.07	1	.	1	0	.	643	0	0.31	0	94.38
7	645.07	0	0	0	0	1	646	0	0.62	1	63.78
7	646.07	0	.	1	0	.	646	0	0.31	2	63.78
7	647.07	0	.	0	0	.	647	0	0.62	2	124.98
7	648.07	0	.	1	0	1	648	0	0.78	2	114.78
7	649.07	0	.	0	0	.	649	0	0.47	1	114.78
7	650.07	0	.	0	0	1	650	0	0.78	0	63.78
7	651.07	0	.	0	0	1	651	0	0.31	1	94.38
7	655.07	0	.	1	0	.	655	0	0.31	1	2.58
7	656.07	0	.	1	0	.	656	0	0.31	0	63.78
7	657.07	0	.	1	0	.	657	0	0.31	1	114.78
7	658.07	1	.	1	0	.	658	0	0.31	2	33.18
7	659.07	0	.	1	0	.	659	0	0.31	0	124.98
7	661.07	0	.	0	0	.	661	0	0.31	1	114.78
7	662.07	0	0	0	0	1	661	0	0.62	2	114.78
7	663.07	1	.	1	0	.	663	0	0.31	1	124.98
7	664.07	1	.	1	0	.	664	0	0.31	1	135.18
7	666.07	1	0	1	0	1	379	1	2.49	1	2.58
7	667.07	1	0	1	0	1	379	1	2.49	1	2.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	611.07	256.86	0.31	3.27	0.31	3.27	1	3	0	3.59
7	612.07	273.34	0.43	2.31	0.45	2.21	0		0	.
7	613.07	242.54	0.43	2.34	0.45	2.21	0		0	.
7	614.07	213.01	0.44	2.29	0.45	2.21	0		0	.
7	615.07	215.21	0.38	2.61	0.31	3.27	0		0	.
7	616.07	308.94	0.38	2.60	0.31	3.27	0		0	.
7	617.07	306.67	0.45	2.24	0.45	2.24	1	2	0	3.59
7	618.07	505.24	0.46	2.17	0.46	2.17	0		0	3.59
7	619.07	530.50	0.39	2.59	0.31	3.27	0		0	.
7	620.07	302.10	0.41	2.41	0.45	2.21	0		0	.
7	621.07	302.00	0.39	2.57	0.31	3.27	0		0	.
7	622.07	496.47	0.39	2.53	0.31	3.27	0		0	.
7	623.07	498.27	0.39	2.56	0.31	3.27	0		0	.
7	624.07	501.80	0.39	2.56	0.31	3.27	0		0	.
7	625.07	313.38	0.39	2.57	0.31	3.27	0		0	.
7	626.07	311.14	0.39	2.55	0.39	2.55	1	2	0	3.59
7	627.07	509.04	0.39	2.58	0.38	2.66	0		0	.
7	628.07	529.46	0.37	2.72	0.31	3.27	0		0	.
7	629.07	353.25	0.37	2.73	0.31	3.27	0		0	.
7	630.07	273.81	0.38	2.64	0.38	2.66	0		1	.
7	631.07	272.34	0.40	2.53	0.40	2.53	0		0	.
7	632.07	818.55	0.39	2.54	0.40	2.53	0		1	.
7	634.07	323.92	0.38	2.66	0.38	2.66	1	3	0	3.59
7	635.07	306.07	0.40	2.51	0.40	2.53	0		0	.
7	636.07	307.37	0.40	2.51	0.40	2.51	1	0	0	2.53
7	637.07	415.95	0.40	2.51	0.40	2.51	0		1	.
7	638.07	460.16	0.41	2.46	0.41	2.46	1	1	0	2.51
7	639.07	430.26	0.41	2.42	0.41	2.42	1	1	0	2.45
7	640.07	343.64	0.54	1.87	0.54	1.87	1	0	0	1.82
7	641.07	422.65	0.40	2.51	0.40	2.53	0		0	.
7	642.07	594.89	0.41	2.45	0.41	2.45	1	0	0	2.46
7	643.07	883.41	0.72	1.39	0.72	1.39	1	0	0	1.52
7	645.07	595.33	0.67	1.49	0.66	1.52	0		1	.
7	646.07	651.72	0.66	1.52	0.66	1.52	1	0	0	1.87
7	647.07	697.19	0.95	1.05	0.95	1.05	1	2	0	1.39
7	648.07	694.93	0.71	1.41	0.71	1.41	1	1	0	2.59
7	649.07	102.77	0.76	1.32	0.76	1.32	1	2	0	2.59
7	650.07	531.93	0.42	2.41	0.42	2.41	1	3	0	2.59
7	651.07	933.76	0.55	1.82	0.55	1.82	1	1	0	2.42
7	655.07	721.59	1.22	0.82	1.22	0.82	1	0	0	1.41
7	656.07	770.43	0.08	12.69	0.08	12.69	1	3	0	.
7	657.07	1072.34	0.60	1.67	0.60	1.67	1	0	0	0.82
7	658.07	979.98	1.00	1.00	1.00	1.00	1	0	0	1.67
7	659.07	1252.95	0.98	1.02	0.98	1.02	1	0	0	1.00
7	661.07	1010.74	0.66	1.51	0.66	1.51	1	0	0	1.02
7	662.07	1222.05	0.66	1.50	0.66	1.51	0		1	.
7	663.07	1049.52	0.85	1.17	0.85	1.17	1	0	0	1.51
7	664.07	142.65	0.90	1.11	0.90	1.11	1	0	0	1.17
7	666.07	183.65	0.42	2.39	0.48	2.09	0		0	.
7	667.07	181.41	0.40	2.50	0.48	2.09	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	672.07	1	.	1	0	2	672	0	1.55	0	94.38
7	674.07	1	.	1	0	3	674	0	0.31	1	104.58
7	675.07	0	.	0	0	1	675	0	0.62	1	104.58
7	221.08	0	.	0	0	1	221	0	0.62	0	2.58
7	242.08	1	.	1	0	.	242	0	0.31	1	2.58
7	243.08	0	1	0	0	1	242	0	0.78	2	2.58
7	244.08	0	.	1	0	1	244	0	0.78	1	2.58
7	252.08	0	0	1	0	1	244	0	1.24	2	43.38
7	255.08	0	.	0	0	2	255	0	1.24	0	43.38
7	273.08	0	0	1	0	2	278	0	0.78	0	12.78
7	278.08	0	.	1	0	.	278	0	0.47	0	12.78
7	280.08	0	.	1	0	1	280	0	1.24	2	2.58
7	285.08	0	.	0	0	.	285	0	0.62	1	12.78
7	287.08	1	1	1	0	1	285	0	0.78	1	12.78
7	298.08	0	0	0	1	1	301	0	1.24	2	12.78
7	301.08	0	.	1	0	2	301	0	1.24	1	12.78
7	302.08	0	0	1	0	1	301	0	1.55	1	12.78
7	306.08	1	0	1	0	2	323	0	1.40	1	2.58
7	307.08	1	.	1	0	1	307	0	1.71	0	2.58
7	308.08	1	0	1	0	1	323	0	1.24	2	12.78
7	309.08	1	0	1	0	1	323	0	1.24	2	12.78
7	310.08	1	0	1	0	1	323	0	1.24	1	2.58
7	315.08	1	.	1	0	1	315	1	1.09	2	12.78
7	318.08	1	.	1	0	1	318	1	1.87	2	12.78
7	319.08	1	0	1	0	1	318	1	2.18	2	12.78
7	321.08	1	.	0	1	1	321	1	2.49	0	2.58
7	323.08	1	.	1	0	1	323	0	1.55	2	12.78
7	324.08	1	.	1	0	1	324	1	1.71	1	2.58
7	325.08	0	1	0	0	2	324	1	2.18	1	2.58
7	326.08	1	.	1	0	1	326	1	2.33	2	12.78
7	328.08	0	1	0	0	2	323	0	1.55	1	2.58
7	329.08	0	1	0	0	1	326	1	1.55	2	12.78
7	330.08	0	0	0	1	1	326	1	1.87	2	12.78
7	331.08	1	1	1	0	1	326	1	2.02	2	12.78
7	332.08	0	1	0	1	1	326	1	2.18	2	12.78
7	335.08	1	.	1	0	1	335	1	2.02	0	2.58
7	338.08	1	0	0	0	1	323	0	1.71	1	2.58
7	339.08	1	.	1	0	1	339	1	1.24	0	12.78
7	340.08	1	1	1	0	2	323	0	1.24	1	12.78
7	341.08	1	0	1	0	1	326	1	1.87	2	12.78
7	342.08	1	0	1	0	1	375	1	2.18	1	2.58
7	345.08	1	.	1	1	1	345	1	2.33	2	12.78
7	347.08	0	.	0	0	1	347	1	2.18	2	12.78
7	349.08	1	.	1	0	1	349	1	2.33	1	12.78
7	351.08	0	1	1	0	1	375	1	1.87	1	2.58
7	352.08	1	.	1	0	1	352	1	1.24	1	12.78
7	353.08	0	.	1	0	1	353	1	2.49	2	43.38
7	355.08	0	.	1	0	1	355	1	2.64	0	33.18
7	358.08	0	.	0	0	1	358	1	2.49	1	43.38
7	361.08	1	1	1	1	2	375	1	1.87	1	2.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	672.07	327.06	0.40	2.53	0.40	2.53	1	1	0	3.59
7	674.07	261.23	0.36	2.80	0.36	2.80	1	3	0	1.39
7	675.07	268.80	0.39	2.59	0.39	2.59	1	1	0	1.39
7	221.08	141.71	1.02	0.98	1.02	0.98	1	1	0	.
7	242.08	71.81	0.67	1.48	0.67	1.48	1	0	0	0.98
7	243.08	76.04	0.69	1.44	0.67	1.48	0		1	.
7	244.08	166.00	0.76	1.32	0.76	1.32	1	1	0	1.48
7	252.08	209.27	0.77	1.30	0.76	1.32	0		1	.
7	255.08	165.36	0.78	1.28	0.78	1.28	1	1	0	1.32
7	273.08	309.54	0.83	1.21	0.80	1.25	0		1	.
7	278.08	236.83	0.80	1.25	0.80	1.25	1	0	0	1.28
7	280.08	229.26	0.70	1.42	0.70	1.42	1	1	0	1.23
7	285.08	244.24	0.81	1.23	0.81	1.23	1	0	0	1.25
7	287.08	122.25	0.81	1.24	0.81	1.23	0		1	.
7	298.08	123.79	0.60	1.66	0.59	1.69	0		1	.
7	301.08	94.56	0.59	1.69	0.59	1.69	1	0	0	1.42
7	302.08	188.42	0.60	1.66	0.59	1.69	0		0	.
7	306.08	97.13	0.53	1.90	0.54	1.84	0		0	.
7	307.08	102.00	0.57	1.76	0.57	1.76	1	4	0	1.69
7	308.08	102.94	0.53	1.88	0.54	1.84	0		0	.
7	309.08	103.57	0.54	1.87	0.54	1.84	0		0	.
7	310.08	402.73	0.53	1.87	0.54	1.84	0		0	.
7	315.08	242.74	0.50	2.01	0.50	2.01	1	2	0	1.84
7	318.08	111.91	0.53	1.90	0.53	1.90	1	2	0	1.84
7	319.08	130.26	0.53	1.90	0.53	1.90	0		1	.
7	321.08	231.20	0.49	2.04	0.49	2.04	1	2	0	1.84
7	323.08	111.45	0.54	1.84	0.54	1.84	1	4	0	1.76
7	324.08	113.08	0.46	2.15	0.46	2.15	1	3	0	1.84
7	325.08	115.88	0.46	2.18	0.46	2.15	0		1	.
7	326.08	306.54	0.49	2.05	0.49	2.05	1	0	0	1.84
7	328.08	124.43	0.53	1.89	0.54	1.84	0		0	.
7	329.08	125.89	0.49	2.04	0.49	2.05	0		0	.
7	330.08	129.10	0.50	2.01	0.49	2.05	0		0	.
7	331.08	131.00	0.49	2.03	0.49	2.05	0		0	.
7	332.08	360.16	0.49	2.04	0.49	2.05	0		0	.
7	335.08	131.99	0.48	2.09	0.48	2.09	1	1	0	2.03
7	338.08	110.18	0.53	1.90	0.54	1.84	0		1	.
7	339.08	104.31	0.49	2.06	0.49	2.06	1	3	0	1.84
7	340.08	122.46	0.53	1.89	0.54	1.84	0		0	.
7	341.08	129.33	0.51	1.97	0.49	2.05	0		1	.
7	342.08	81.31	0.47	2.13	0.49	2.03	0		0	.
7	345.08	243.87	0.47	2.12	0.47	2.12	1	3	0	2.09
7	347.08	315.48	0.49	2.05	0.49	2.05	1	3	0	2.01
7	349.08	248.51	0.52	1.92	0.52	1.92	1	2	0	2.01
7	351.08	106.61	0.47	2.13	0.49	2.03	0		0	.
7	352.08	62.80	0.48	2.09	0.48	2.09	1	3	0	1.84
7	353.08	251.82	0.49	2.03	0.49	2.03	1	2	0	2.01
7	355.08	184.61	0.52	1.94	0.52	1.94	1	1	0	2.01
7	358.08	331.03	0.47	2.11	0.47	2.11	1	3	0	2.01
7	361.08	255.19	0.47	2.12	0.49	2.03	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	363.08	0	1	1	0	1	375	1	2.02	1	2.58
7	366.08	1	1	1	0	1	375	1	1.87	1	2.58
7	370.08	0	0	0	0	1	324	1	2.33	1	2.58
7	372.08	1	1	1	0	1	353	1	2.33	2	12.78
7	373.08	0	0	0	0	1	324	1	2.33	1	12.78
7	375.08	0	.	0	0	2	375	1	2.33	0	12.78
7	378.08	1	.	1	0	1	378	1	2.18	1	2.58
7	379.08	1		1	0	1	379	1	2.18	1	2.58
7	383.08	1	1	0	0	2	384	1	2.18	2	53.58
7	384.08	0	.	1	0	1	384	1	2.18	2	43.38
7	385.08	0	1	1	0	1	391	1	2.02	1	2.58
7	391.08	0	.	1	0	1	391	1	2.33	1	2.58
7	392.08	1	.	1	0	1	392	1	2.02	2	22.98
7	393.08	1	1	1	0	1	391	1	2.33	1	2.58
7	396.08	1	0	1	1	2	397	1	1.87	1	2.58
7	397.08	1	.	1	1	1	397	1	2.02	1	2.58
7	403.08	0	1	1	0	1	315	1	1.71	2	12.78
7	406.08	0	0	1	0	1	244	0	1.24	1	43.38
7	409.08	1	.	1	0	1	409	0	1.87	1	12.78
7	410.08	0	1	0	0	1	409	0	2.18	0	12.78
7	411.08	0	.	1	0	1	411	0	2.02	1	12.78
7	412.08	1	1	1	0	1	411	0	2.18	1	12.78
7	413.08	0	1	0	0	1	411	0	2.18	1	12.78
7	415.08	0	0	0	0	1	411	0	1.87	1	12.78
7	416.08	0	0	0	0	1	411	0	2.02	1	12.78
7	417.08	0	0	0	0	1	411	0	1.87	2	12.78
7	418.08	0	0	1	1	1	411	0	2.02	2	22.98
7	419.08	1	1	1	0	1	411	0	2.18	1	12.78
7	420.08	1	0	1	0	1	411	0	2.02	2	22.98
7	421.08	1	0	1	0	1	411	0	1.87	1	22.98
7	422.08	1	.	1	0	1	422	0	1.87	2	43.38
7	423.08	1	0	1	0	1	411	0	2.02	1	22.98
7	424.08	1	.	0	0	1	424	0	1.87	1	43.38
7	425.08	1	0	1	0	1	426	0	2.33	2	53.58
7	426.08	1	.	1	0	1	426	0	2.02	1	53.58
7	427.08	1	.	1	1	1	427	1	2.49	2	63.78
7	428.08	0	1	1	0	1	426	0	2.33	1	53.58
7	429.08	1	.	1	0	1	429	1	2.33	1	53.58
7	430.08	1	0	1	0	1	427	1	2.64	2	63.78
7	431.08	1	0	1	0	1	427	1	2.49	2	63.78
7	433.08	0	.	0	0	1	433	1	2.64	2	63.78
7	435.08	0	1	1	0	1	442	0	2.49	2	33.18
7	436.08	0	1	1	0	1	429	1	2.18	1	12.78
7	437.08	0	0	0	0	1	429	1	2.49	1	12.78
7	438.08	1	1	0	0	2	442	0	2.33	1	63.78
7	439.08	1	.	1	0	1	439	1	2.49	1	12.78
7	440.08	0	0	0	0	1	442	0	2.64	1	43.38
7	441.08	0	.	1	0	1	441	1	1.87	2	2.58
7	442.08	1	.	1	0	1	442	0	2.33	1	33.18
7	443.08	1	1	1	0	1	441	1	2.02	2	84.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	363.08	379.24	0.47	2.12	0.49	2.03	0		0	.
7	366.08	263.79	0.47	2.13	0.49	2.03	0		0	.
7	370.08	277.11	0.46	2.17	0.46	2.15	0		0	.
7	372.08	114.52	0.50	2.02	0.49	2.03	0		1	.
7	373.08	273.54	0.48	2.08	0.46	2.15	0		0	.
7	375.08	281.95	0.49	2.03	0.49	2.03	1	1	0	2.05
7	378.08	137.67	0.49	2.02	0.49	2.02	1	2	0	2.09
7	379.08	283.65	0.50	2.01	0.50	2.01	0		0	2.09
7	383.08	77.98	0.52	1.93	0.52	1.93	0		0	.
7	384.08	148.08	0.52	1.93	0.52	1.93	1	1	0	1.94
7	385.08	322.72	0.43	2.31	0.43	2.31	0		0	.
7	391.08	116.98	0.43	2.31	0.43	2.31	1	3	0	1.93
7	392.08	145.65	0.48	2.07	0.48	2.07	1	2	0	1.93
7	393.08	248.98	0.43	2.31	0.43	2.31	0		0	.
7	396.08	151.39	0.43	2.31	0.43	2.31	0		1	.
7	397.08	205.27	0.43	2.31	0.43	2.31	1	3	0	1.93
7	403.08	264.10	0.52	1.92	0.50	2.01	0		1	.
7	406.08	353.82	0.77	1.30	0.76	1.32	0		0	.
7	409.08	152.42	0.43	2.32	0.43	2.32	1	1	0	1.93
7	410.08	154.76	0.45	2.24	0.43	2.32	0		1	.
7	411.08	156.76	0.42	2.39	0.42	2.39	1	4	0	2.32
7	412.08	160.46	0.42	2.41	0.42	2.39	0		1	.
7	413.08	379.38	0.42	2.41	0.42	2.39	0		0	.
7	415.08	163.93	0.42	2.41	0.42	2.39	0		0	.
7	416.08	165.13	0.41	2.42	0.42	2.39	0		0	.
7	417.08	117.92	0.41	2.43	0.42	2.39	0		0	.
7	418.08	167.60	0.41	2.45	0.42	2.39	0		0	.
7	419.08	122.12	0.41	2.42	0.42	2.39	0		0	.
7	420.08	123.06	0.40	2.51	0.42	2.39	0		0	.
7	421.08	99.27	0.41	2.43	0.42	2.39	0		0	.
7	422.08	124.16	0.39	2.55	0.39	2.55	1	3	0	2.39
7	423.08	100.87	0.41	2.44	0.42	2.39	0		0	.
7	424.08	102.97	0.41	2.44	0.41	2.44	1	2	0	2.39
7	425.08	101.27	0.41	2.45	0.41	2.42	0		1	.
7	426.08	86.28	0.41	2.42	0.41	2.42	1	1	0	2.39
7	427.08	106.01	0.43	2.34	0.43	2.34	1	2	0	2.42
7	428.08	107.98	0.41	2.46	0.41	2.42	0		0	.
7	429.08	87.85	0.40	2.48	0.40	2.48	1	3	0	2.42
7	430.08	88.82	0.42	2.38	0.43	2.34	0		1	.
7	431.08	409.47	0.42	2.40	0.43	2.34	0		0	.
7	433.08	407.20	0.41	2.44	0.41	2.44	1	1	0	2.42
7	435.08	181.68	0.41	2.43	0.41	2.46	0		1	.
7	436.08	183.92	0.41	2.46	0.40	2.48	0		1	.
7	437.08	94.13	0.40	2.48	0.40	2.48	0		0	.
7	438.08	185.79	0.40	2.48	0.41	2.46	0		0	.
7	439.08	66.70	0.40	2.48	0.40	2.48	1	3	0	2.44
7	440.08	199.17	0.40	2.47	0.41	2.46	0		0	.
7	441.08	152.39	0.41	2.44	0.41	2.44	1	2	0	2.46
7	442.08	66.33	0.41	2.46	0.41	2.46	1	1	0	2.44
7	443.08	62.99	0.33	2.99	0.41	2.44	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	444.08	1	.	1	0	1	444	1	2.49	2	84.18
7	445.08	1	.	1	0	1	445	1	2.33	2	12.78
7	446.08	1	0	1	0	1	444	1	2.64	2	63.78
7	448.08	0	1	0	1	1	444	1	2.49	2	63.78
7	451.08	0	0	0	0	1	444	1	2.33	2	63.78
7	452.08	0	1	1	0	1	442	0	2.02	0	63.78
7	454.08	1	.	1	0	1	454	0	2.18	2	73.98
7	455.08	1	.	1	0	1	455	1	2.02	1	2.58
7	456.08	1	.	1	0	1	456	1	2.33	2	53.58
7	457.08	0	.	1	0	1	457	1	2.02	1	84.18
7	458.08	0	.	1	0	1	458	1	2.33	1	12.78
7	459.08	1	0	1	0	1	454	0	2.18	1	12.78
7	460.08	1	1	0	0	1	457	1	2.18	1	2.58
7	461.08	1	0	1	0	1	457	1	2.49	1	2.58
7	462.08	1	.	1	0	1	462	0	2.49	1	2.58
7	463.08	0	1	0	0	1	457	1	2.80	1	2.58
7	464.08	0	0	1	0	1	457	1	2.64	1	63.78
7	465.08	0	0	0	0	1	457	1	2.64	1	84.18
7	466.08	1	1	1	0	1	457	1	2.49	1	2.58
7	467.08	1	.	0	0	1	467	0	2.18	1	2.58
7	468.08	0	0	1	0	1	458	1	2.33	1	12.78
7	470.08	1	0	1	0	1	456	1	2.18	2	84.18
7	472.08	0	.	0	0	1	472	0	2.49	0	2.58
7	473.08	0	1	1	0	1	467	0	2.49	0	2.58
7	475.08	1	0	1	0	1	479	0	2.02	2	53.58
7	477.08	1	.	1	0	1	477	0	1.87	2	53.58
7	478.08	1	1	1	0	1	479	0	2.49	1	53.58
7	479.08	0	.	0	0	2	479	0	2.64	1	53.58
7	482.08	0	0	1	0	1	483	0	2.18	2	53.58
7	483.08	0	.	1	0	1	483	0	1.71	1	22.98
7	484.08	0	0	0	0	1	483	0	2.02	1	63.78
7	485.08	1	1	1	0	1	483	0	2.95	2	84.18
7	486.08	1	0	0	1	1	483	0	2.64	1	43.38
7	487.08	0	1	0	1	1	483	0	2.80	2	53.58
7	488.08	1	0	1	0	1	483	0	2.95	1	63.78
7	489.08	0	1	0	0	1	483	0	2.49	2	84.18
7	490.08	1	1	1	0	2	483	0	3.26	1	63.78
7	491.08	0	0	1	0	1	483	0	2.33	2	84.18
7	492.08	0	0	1	0	1	483	0	3.26	1	63.78
7	493.08	0	.	1	0	1	493	0	1.87	1	84.18
7	494.08	1	.	0	0	2	494	0	2.02	1	84.18
7	495.08	1	1	1	0	1	483	0	2.95	1	12.78
7	497.08	1	0	1	0	2	483	0	2.49	1	63.78
7	498.08	0	1	0	1	1	483	0	2.02	1	73.98
7	499.08	1	0	1	0	1	493	0	1.87	0	84.18
7	500.08	1	1	1	0	2	493	0	1.71	1	84.18
7	501.08	1	0	1	0	2	483	0	2.18	1	43.38
7	502.08	0	1	0	0	1	493	0	2.18	1	43.38
7	503.08	1	1	1	0	1	504	0	1.87	1	63.78
7	504.08	0	.	0	0	1	504	0	2.02	2	63.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	444.08	202.70	0.33	3.00	0.33	3.00	1	2	0	2.46
7	445.08	105.17	0.33	2.99	0.33	2.99	1	2	0	2.46
7	446.08	422.35	0.34	2.95	0.33	3.00	0		1	.
7	448.08	423.79	0.33	2.99	0.33	3.00	0		0	.
7	451.08	98.26	0.33	3.05	0.33	3.00	0		0	.
7	452.08	245.41	0.40	2.52	0.41	2.46	0		0	.
7	454.08	197.53	0.31	3.20	0.31	3.20	1	1	0	2.46
7	455.08	144.24	0.32	3.14	0.32	3.14	1	3	0	2.46
7	456.08	64.56	0.32	3.12	0.32	3.12	1	2	0	3.20
7	457.08	214.35	0.31	3.19	0.31	3.19	1	3	0	2.46
7	458.08	211.48	0.30	3.32	0.30	3.32	1	3	0	3.20
7	459.08	202.40	0.31	3.23	0.31	3.20	0		1	.
7	460.08	204.74	0.31	3.19	0.31	3.19	0		1	.
7	461.08	220.79	0.32	3.17	0.31	3.19	0		0	.
7	462.08	206.41	0.30	3.36	0.30	3.36	1	3	0	3.18
7	463.08	99.93	0.32	3.16	0.31	3.19	0		0	.
7	464.08	73.67	0.32	3.12	0.31	3.19	0		0	.
7	465.08	214.15	0.32	3.17	0.31	3.19	0		0	.
7	466.08	224.13	0.32	3.16	0.31	3.19	0		0	.
7	467.08	215.25	0.31	3.18	0.31	3.18	1	1	0	3.20
7	468.08	590.76	0.30	3.30	0.30	3.32	0		1	.
7	470.08	592.06	0.32	3.15	0.32	3.12	0		1	.
7	472.08	225.56	0.13	7.42	0.13	7.42	1	3	0	.
7	473.08	476.01	0.32	3.09	0.31	3.18	0		1	.
7	475.08	289.05	0.27	3.75	0.28	3.62	0		0	.
7	477.08	154.49	0.27	3.77	0.27	3.77	1	4	0	3.31
7	478.08	149.82	0.28	3.62	0.28	3.62	0		1	.
7	479.08	300.56	0.30	3.31	0.28	3.62	1	4	0	3.18
7	482.08	184.35	0.26	3.87	0.26	3.88	0		1	.
7	483.08	127.22	0.26	3.88	0.26	3.88	1	4	0	3.77
7	484.08	115.35	0.26	3.88	0.26	3.88	0		0	.
7	485.08	156.16	0.26	3.85	0.26	3.88	0		0	.
7	486.08	162.66	0.26	3.87	0.26	3.88	0		0	.
7	487.08	129.86	0.26	3.87	0.26	3.88	0		0	.
7	488.08	110.27	0.26	3.89	0.26	3.88	0		0	.
7	489.08	131.80	0.26	3.83	0.26	3.88	0		0	.
7	490.08	118.58	0.26	3.85	0.26	3.88	0		0	.
7	491.08	132.73	0.26	3.86	0.26	3.88	0		0	.
7	492.08	112.94	0.26	3.83	0.26	3.88	0		0	.
7	493.08	111.21	0.21	4.72	0.21	4.72	1	0	0	4.69
7	494.08	240.51	0.21	4.69	0.21	4.69	1	0	0	3.88
7	495.08	360.96	0.26	3.87	0.26	3.88	0		0	.
7	497.08	133.66	0.26	3.91	0.26	3.88	0		0	.
7	498.08	122.62	0.21	4.67	0.26	3.88	0		0	.
7	499.08	116.98	0.18	5.52	0.21	4.72	0		0	.
7	500.08	162.56	0.18	5.52	0.21	4.72	0		1	.
7	501.08	172.41	0.21	4.74	0.26	3.88	0		0	.
7	502.08	140.84	0.18	5.52	0.21	4.72	0		0	.
7	503.08	144.61	0.18	5.61	0.18	5.59	0		1	.
7	504.08	123.22	0.18	5.59	0.18	5.59	1	4	0	4.72

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	505.08	0	1	0	0	1	504	0	2.33	1	84.18
7	506.08	0	0	1	0	1	504	0	2.33	2	84.18
7	507.08	1	1	1	0	1	504	0	2.64	1	73.98
7	508.08	0	1	1	0	1	504	0	2.95	2	73.98
7	509.08	1	1	1	0	1	510	1	2.64	2	84.18
7	510.08	0	.	1	0	1	510	1	2.33	2	73.98
7	511.08	1	0	0	0	1	510	1	2.64	2	84.18
7	512.08	1	0	1	0	1	512	1	2.49	2	114.78
7	513.08	1	.	1	0	1	513	0	2.49	2	84.18
7	514.08	1	.	1	0	1	514	1	2.02	2	73.98
7	515.08	1	.	1	0	1	515	1	2.33	2	73.98
7	517.08	1	0	1	1	1	514	1	1.87	2	73.98
7	518.08	1	.	1	0	1	518	1	3.26	1	114.78
7	519.08	0	.	1	1	1	519	1	2.80	2	73.98
7	520.08	1	1	1	0	1	538	1	2.02	1	73.98
7	521.08	1	.	1	0	1	521	1	2.64	2	12.78
7	522.08	1	.	1	0	1	522	1	2.95	1	12.78
7	523.08	1	.	1	0	1	523	1	2.49	1	12.78
7	524.08	0	0	1	0	2	525	0	1.55	1	114.78
7	525.08	0	.	1	0	2	525	0	1.87	1	114.78
7	530.08	1	.	1	0	1	530	0	2.18	0	43.38
7	531.08	0	1	0	0	1	518	1	2.64	1	43.38
7	532.08	1	.	1	0	2	532	0	2.95	1	43.38
7	533.08	0	0	1	0	1	518	1	2.49	1	84.18
7	534.08	0	.	0	0	1	534	0	2.64	0	84.18
7	535.08	1	.	1	0	1	535	1	2.64	1	73.98
7	536.08	1	.	1	0	1	536	1	2.64	1	33.18
7	537.08	0	1	1	0	1	535	1	2.18	1	73.98
7	538.08	0	.	0	0	1	538	1	2.02	1	73.98
7	539.08	1	0	1	0	1	538	1	2.64	1	73.98
7	540.08	1	0	1	0	1	532	0	1.87	1	22.98
7	541.08	1	0	1	0	2	532	0	2.95	1	22.98
7	542.08	1	1	1	0	1	525	0	1.71	1	114.78
7	543.08	1	.	1	0	2	543	0	2.02	1	63.78
7	544.08	1	0	1	0	1	543	0	2.33	1	114.78
7	545.08	1	0	1	0	2	543	0	2.02	2	114.78
7	546.08	0	.	0	0	2	546	1	2.18	2	114.78
7	547.08	0	.	0	0	1	547	1	2.49	1	33.18
7	548.08	0	0	1	0	1	547	1	2.49	1	33.18
7	549.08	1	1	1	0	1	546	1	2.18	0	12.78
7	550.08	1	.	1	0	1	550	1	2.64	0	12.78
7	551.08	1	.	1	0	1	551	1	2.02	1	12.78
7	552.08	1	.	1	0	1	552	1	2.02	0	53.58
7	553.08	0	1	1	0	1	551	1	1.87	1	43.38
7	555.08	1	1	1	0	1	560	1	2.02	2	63.78
7	556.08	1	.	1	0	1	556	0	2.33	2	73.98
7	557.08	0	.	1	0	1	557	1	2.18	1	33.18
7	558.08	0	0	0	0	1	557	1	2.18	1	33.18
7	559.08	1	.	0	0	1	559	0	2.49	1	114.78
7	560.08	0	.	1	0	2	560	1	2.49	2	33.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	505.08	124.52	0.18	5.56	0.18	5.59	0		0	.
7	506.08	153.78	0.18	5.63	0.18	5.59	0		0	.
7	507.08	152.85	0.19	5.39	0.18	5.59	0		0	.
7	508.08	135.43	0.19	5.37	0.18	5.59	0		0	.
7	509.08	155.35	0.22	4.56	0.19	5.18	0		1	.
7	510.08	136.57	0.19	5.18	0.19	5.18	1	3	0	5.59
7	511.08	111.84	0.22	4.57	0.19	5.18	0		0	.
7	512.08	138.27	0.22	4.57	0.22	4.57	0		0	5.59
7	513.08	171.10	0.23	4.43	0.23	4.43	1	1	0	4.38
7	514.08	174.17	0.23	4.33	0.23	4.33	1	2	0	4.31
7	515.08	397.76	0.20	5.01	0.20	5.01	1	2	0	4.95
7	517.08	110.71	0.20	5.09	0.23	4.33	0		1	.
7	518.08	175.24	0.24	4.21	0.24	4.21	1	2	0	5.59
7	519.08	169.67	0.20	5.04	0.20	5.04	1	2	0	4.95
7	520.08	315.58	0.19	5.34	0.19	5.35	0		1	.
7	521.08	313.42	0.19	5.16	0.19	5.16	1	2	0	5.25
7	522.08	312.51	0.19	5.26	0.19	5.26	1	3	0	5.25
7	523.08	115.48	0.19	5.25	0.19	5.25	1	1	0	4.95
7	524.08	114.05	0.22	4.64	0.21	4.65	0		1	.
7	525.08	401.53	0.21	4.65	0.21	4.65	1	1	0	5.39
7	530.08	188.96	0.23	4.31	0.23	4.31	1	1	0	4.43
7	531.08	215.75	0.24	4.24	0.24	4.21	0		1	.
7	532.08	95.29	0.19	5.39	0.19	5.39	1	0	0	5.25
7	533.08	96.63	0.23	4.27	0.24	4.21	0		0	.
7	534.08	163.23	0.23	4.38	0.23	4.38	1	1	0	5.59
7	535.08	234.60	0.20	4.95	0.20	4.95	1	4	0	4.31
7	536.08	164.46	0.22	4.50	0.22	4.50	1	3	0	4.31
7	537.08	165.80	0.19	5.26	0.20	4.95	0		1	.
7	538.08	172.77	0.19	5.35	0.19	5.35	1	3	0	4.95
7	539.08	254.05	0.19	5.35	0.19	5.35	0		0	.
7	540.08	252.09	0.21	4.69	0.19	5.39	0		0	.
7	541.08	118.18	0.21	4.68	0.19	5.39	0		1	.
7	542.08	188.89	0.22	4.63	0.21	4.65	0		0	.
7	543.08	125.02	0.22	4.60	0.22	4.60	1	1	0	4.65
7	544.08	126.33	0.22	4.60	0.22	4.60	0		1	.
7	545.08	126.83	0.22	4.58	0.22	4.60	0		0	.
7	546.08	222.49	0.22	4.59	0.22	4.59	1	2	0	4.60
7	547.08	225.19	0.13	7.63	0.13	7.63	1	3	0	4.60
7	548.08	348.65	0.13	7.48	0.13	7.63	0		1	.
7	549.08	336.30	0.22	4.62	0.22	4.59	0		1	.
7	550.08	355.59	0.21	4.83	0.21	4.83	1	3	0	4.60
7	551.08	228.50	0.23	4.40	0.23	4.40	1	2	0	4.60
7	552.08	230.63	0.21	4.70	0.21	4.70	1	3	0	4.60
7	553.08	452.62	0.26	3.79	0.23	4.40	0		1	.
7	555.08	217.11	0.21	4.79	0.20	5.01	0		1	.
7	556.08	274.31	0.21	4.75	0.21	4.75	1	1	0	4.60
7	557.08	276.34	0.26	3.86	0.26	3.86	1	2	0	4.60
7	558.08	130.30	0.26	3.86	0.26	3.86	0		1	.
7	559.08	268.20	0.18	5.67	0.18	5.67	1	3	0	4.57
7	560.08	220.45	0.20	5.01	0.20	5.01	1	3	0	4.60

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	561.08	1	.	1	0	1	561	0	2.49	1	73.98
7	562.08	0	0	0	0	1	557	1	2.33	1	12.78
7	563.08	0	.	0	0	1	563	0	2.49	1	63.78
7	564.08	1	0	1	0	1	565	0	1.71	1	73.98
7	565.08	1	.	1	0	3	565	0	1.71	1	63.78
7	566.08	1	0	0	0	1	565	0	1.87	1	114.78
7	567.08	1	0	1	0	1	565	0	2.02	1	114.78
7	568.08	0	1	1	0	1	565	0	2.02	1	22.98
7	569.08	0	0	1	0	1	570	0	2.33	2	53.58
7	570.08	0	.	0	0	1	570	0	2.02	1	22.98
7	571.08	1	.	1	0	2	571	0	1.71	1	114.78
7	572.08	0	0	1	0	2	570	0	1.87	2	73.98
7	573.08	1	0	0	0	1	574	0	2.18	2	114.78
7	574.08	0	.	1	0	3	574	0	1.40	1	114.78
7	575.08	0	.	1	0	1	575	1	2.49	2	114.78
7	576.08	1	0	1	0	2	574	0	1.24	1	114.78
7	577.08	1	1	1	0	2	574	0	1.24	1	114.78
7	578.08	1	0	0	0	1	574	0	1.87	1	114.78
7	579.08	1	0	1	0	1	574	0	1.71	2	114.78
7	580.08	1	0	1	0	1	574	0	1.55	1	114.78
7	581.08	0	.	0	0	1	581	1	2.33	1	12.78
7	582.08	0	0	0	0	2	581	1	2.49	1	53.58
7	583.08	0	0	0	0	1	585	0	2.02	1	94.38
7	584.08	0	1	1	0	1	585	0	2.18	2	94.38
7	585.08	1	.	1	0	1	585	0	2.02	1	114.78
7	586.08	1	1	1	0	1	575	1	2.33	2	114.78
7	587.08	1	.	1	0	1	587	1	2.33	2	73.98
7	588.08	0	.	0	0	1	588	1	1.87	2	114.78
7	589.08	1	1	1	0	1	581	1	2.80	1	12.78
7	590.08	0	.	1	0	1	590	1	2.33	0	63.78
7	591.08	0	.	1	0	2	591	1	1.87	1	53.58
7	592.08	0	1	1	1	1	598	0	2.02	2	114.78
7	593.08	1	.	1	0	1	593	1	1.71	1	114.78
7	594.08	0	0	0	0	1	598	0	1.87	2	114.78
7	595.08	1	0	1	0	1	593	1	2.18	1	114.78
7	596.08	0	0	0	0	1	598	0	1.71	2	84.18
7	597.08	1	.	1	0	1	597	0	2.18	1	114.78
7	598.08	0	.	0	0	1	598	0	2.33	1	114.78
7	599.08	1	1	1	0	2	598	0	2.49	1	114.78
7	600.08	1	0	1	0	2	598	0	1.87	2	114.78
7	601.08	1	0	1	0	2	598	0	2.64	1	114.78
7	603.08	0	0	1	0	1	598	0	1.71	1	114.78
7	604.08	1	0	1	0	1	608	1	2.64	2	114.78
7	605.08	0	1	1	0	1	598	0	1.55	2	114.78
7	606.08	1	.	1	0	1	606	1	2.64	0	53.58
7	607.08	0	1	1	0	1	598	0	2.18	2	43.38
7	608.08	1	.	1	0	1	608	1	2.33	2	84.18
7	609.08	0	.	1	0	1	609	1	3.11	2	114.78
7	610.08	1	1	1	0	1	598	0	1.87	1	114.78
7	611.08	1	1	0	0	1	598	0	1.55	1	114.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	561.08	364.13	0.21	4.68	0.21	4.68	1	1	0	4.75
7	562.08	210.54	0.26	3.88	0.26	3.86	0		0	.
7	563.08	207.64	0.21	4.70	0.21	4.70	1	1	0	4.68
7	564.08	191.22	0.23	4.31	0.22	4.57	0		1	.
7	565.08	133.73	0.22	4.57	0.22	4.57	1	0	0	4.70
7	566.08	132.73	0.23	4.29	0.22	4.57	0		0	.
7	567.08	292.79	0.23	4.26	0.22	4.57	0		0	.
7	568.08	256.19	0.24	4.23	0.22	4.57	0		0	.
7	569.08	297.36	0.24	4.22	0.23	4.27	0		1	.
7	570.08	168.33	0.23	4.27	0.23	4.27	1	1	0	4.57
7	571.08	222.72	0.23	4.26	0.23	4.26	1	0	0	4.27
7	572.08	178.74	0.24	4.24	0.23	4.27	0		0	.
7	573.08	170.87	0.29	3.50	0.24	4.15	0		0	.
7	574.08	180.71	0.24	4.15	0.24	4.15	1	0	0	4.26
7	575.08	174.14	0.29	3.48	0.29	3.48	1	2	0	4.15
7	576.08	172.77	0.28	3.51	0.24	4.15	0		0	.
7	577.08	178.18	0.29	3.49	0.24	4.15	0		1	.
7	578.08	176.28	0.29	3.48	0.24	4.15	0		0	.
7	579.08	176.11	0.29	3.50	0.24	4.15	0		0	.
7	580.08	431.83	0.29	3.48	0.24	4.15	0		0	.
7	581.08	278.18	0.29	3.49	0.29	3.49	1	3	0	4.15
7	582.08	223.92	0.29	3.44	0.29	3.49	0		1	.
7	583.08	225.96	0.29	3.43	0.29	3.45	0		0	.
7	584.08	188.42	0.29	3.39	0.29	3.45	0		1	.
7	585.08	187.85	0.29	3.45	0.29	3.45	1	1	0	4.15
7	586.08	272.87	0.30	3.32	0.29	3.48	0		1	.
7	587.08	193.66	0.27	3.76	0.27	3.76	1	2	0	3.45
7	588.08	437.41	0.27	3.76	0.27	3.76	1	2	0	3.45
7	589.08	223.49	0.29	3.48	0.29	3.49	0		0	.
7	590.08	288.36	0.12	8.22	0.12	8.22	1	3	0	.
7	591.08	201.83	0.25	3.97	0.25	3.97	1	3	0	3.45
7	592.08	184.18	0.25	3.98	0.25	4.00	0		0	.
7	593.08	213.98	0.25	4.02	0.25	4.02	1	3	0	3.45
7	594.08	186.62	0.25	4.00	0.25	4.00	0		0	.
7	595.08	250.38	0.25	4.00	0.25	4.02	0		1	.
7	596.08	191.79	0.25	4.02	0.25	4.00	0		0	.
7	597.08	195.03	0.25	4.00	0.25	4.00	1	1	0	3.45
7	598.08	199.03	0.25	4.00	0.25	4.00	1	0	0	4.00
7	599.08	232.23	0.25	3.96	0.25	4.00	0		1	.
7	600.08	197.83	0.25	4.07	0.25	4.00	0		0	.
7	601.08	670.90	0.25	3.95	0.25	4.00	0		0	.
7	603.08	240.27	0.25	3.95	0.25	4.00	0		0	.
7	604.08	217.32	0.28	3.53	0.27	3.75	0		1	.
7	605.08	341.14	0.22	4.63	0.25	4.00	0		0	.
7	606.08	311.71	0.27	3.69	0.27	3.69	1	2	0	4.00
7	607.08	262.63	0.22	4.56	0.25	4.00	0		0	.
7	608.08	241.01	0.27	3.75	0.27	3.75	1	2	0	4.00
7	609.08	210.14	0.28	3.54	0.28	3.54	1	2	0	4.00
7	610.08	207.07	0.22	4.62	0.25	4.00	0		0	.
7	611.08	256.86	0.25	4.02	0.25	4.00	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	612.08	0	0	1	0	1	613	1	2.33	2	114.78
7	613.08	0	.	1	0	1	613	1	2.64	2	84.18
7	614.08	1	1	1	0	1	613	1	1.87	2	114.78
7	615.08	1	1	1	0	1	598	0	2.02	1	114.78
7	616.08	1	.	1	0	1	616	1	2.02	1	114.78
7	617.08	0	.	1	0	1	617	0	1.55	1	84.18
7	618.08	1	.	1	0	1	618	0	1.55	2	84.18
7	619.08	1	0	1	0	1	623	1	2.49	1	12.78
7	620.08	1	0	0	0	1	613	1	1.87	2	12.78
7	621.08	1	.	1	0	1	621	1	2.02	0	73.98
7	622.08	1	0	1	0	1	621	1	2.18	0	73.98
7	623.08	1	.	1	0	1	623	1	2.49	1	12.78
7	624.08	1	0	1	1	1	623	1	2.80	1	12.78
7	625.08	1	0	1	0	2	623	1	2.49	1	33.18
7	626.08	1	0	1	0	1	617	0	1.87	2	84.18
7	627.08	1	1	1	0	2	617	0	1.87	1	84.18
7	628.08	1	0	1	0	1	623	1	2.18	1	12.78
7	629.08	1	.	1	0	1	629	1	1.55	0	12.78
7	630.08	1	.	0	0	1	630	0	1.40	1	53.58
7	631.08	0	1	0	0	2	672	0	1.55	2	114.78
7	632.08	1	0	1	0	1	672	0	1.24	1	114.78
7	634.08	0	.	1	0	1	634	1	1.71	1	84.18
7	635.08	1	0	1	0	1	672	0	1.55	0	84.18
7	636.08	0	.	0	0	2	636	0	1.55	1	114.78
7	637.08	0	0	0	0	1	636	0	1.55	2	114.78
7	638.08	0	.	0	0	3	638	0	1.24	1	43.38
7	639.08	0	.	0	0	3	639	0	0.93	1	114.78
7	640.08	0	.	0	0	1	640	0	0.62	2	63.78
7	641.08	1	1	1	0	2	672	0	1.24	1	73.98
7	642.08	1	.	1	0	3	642	0	0.93	1	63.78
7	643.08	1	.	1	0	.	643	0	0.31	1	73.98
7	645.08	0	.	0	0	2	645	0	0.62	1	43.38
7	646.08	0	.	1	0	.	646	0	0.31	2	43.38
7	647.08	0	.	0	0	.	647	0	0.62	2	104.58
7	648.08	0	0	1	0	1	649	0	0.62	2	94.38
7	649.08	0	.	0	0	.	649	0	0.31	1	94.38
7	650.08	0	0	0	0	1	656	0	0.62	2	43.38
7	651.08	0	.	0	0	3	651	0	0.62	1	73.98
7	656.08	0	.	1	0	.	656	0	0.31	1	43.38
7	657.08	0	.	1	0	.	657	0	0.31	1	94.38
7	658.08	1	.	1	0	.	658	0	0.31	2	12.78
7	659.08	0	.	1	0	.	659	0	0.31	2	104.58
7	661.08	0	.	0	0	.	661	0	0.31	1	94.38
7	662.08	0	0	0	0	1	661	0	0.62	2	94.38
7	663.08	1	.	1	0	.	663	0	0.31	1	104.58
7	664.08	1	.	1	0	.	664	0	0.31	1	114.78
7	672.08	1	.	1	0	2	672	0	1.71	0	73.98
7	674.08	1	.	1	0	.	674	0	0.31	2	84.18
7	675.08	0	.	0	0	1	675	0	0.62	1	84.18
7	252.09	0	.	1	0	1	252	0	0.93	2	22.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	612.08	273.34	0.28	3.62	0.28	3.59	0		0	.
7	613.08	242.54	0.28	3.59	0.28	3.59	1	2	0	4.00
7	614.08	213.01	0.28	3.56	0.28	3.59	0		0	.
7	615.08	215.21	0.22	4.54	0.25	4.00	0		0	.
7	616.08	308.94	0.22	4.49	0.22	4.49	1	3	0	4.00
7	617.08	306.67	0.26	3.82	0.26	3.82	1	1	0	4.00
7	618.08	505.24	0.27	3.74	0.27	3.74	1	2	0	4.00
7	619.08	530.50	0.25	3.94	0.22	4.60	0		0	.
7	620.08	302.10	0.28	3.56	0.28	3.59	0		0	.
7	621.08	302.00	0.22	4.65	0.22	4.65	1	3	0	4.00
7	622.08	496.47	0.22	4.56	0.22	4.65	0		1	.
7	623.08	498.27	0.22	4.60	0.22	4.60	1	3	0	4.00
7	624.08	501.80	0.24	4.18	0.22	4.60	0		1	.
7	625.08	313.38	0.25	4.06	0.22	4.60	0		0	.
7	626.08	311.14	0.26	3.82	0.26	3.82	0		0	.
7	627.08	509.04	0.26	3.81	0.26	3.82	0		1	.
7	628.08	529.46	0.25	3.95	0.22	4.60	0		0	.
7	629.08	353.25	0.28	3.62	0.28	3.62	1	2	0	4.00
7	630.08	273.81	0.26	3.86	0.26	3.86	1	3	0	4.00
7	631.08	272.34	0.26	3.79	0.26	3.83	0		0	.
7	632.08	818.55	0.26	3.79	0.26	3.83	0		1	.
7	634.08	323.92	0.25	3.96	0.25	3.96	1	3	0	4.00
7	635.08	306.07	0.26	3.89	0.26	3.83	0		0	.
7	636.08	307.37	0.26	3.90	0.26	3.90	1	0	0	3.83
7	637.08	415.95	0.25	3.92	0.26	3.90	0		1	.
7	638.08	460.16	0.26	3.83	0.26	3.83	1	0	0	3.90
7	639.08	430.26	0.31	3.26	0.31	3.26	1	0	0	3.48
7	640.08	343.64	0.54	1.86	0.54	1.86	1	3	0	3.26
7	641.08	422.65	0.26	3.81	0.26	3.83	0		0	.
7	642.08	594.89	0.29	3.48	0.29	3.48	1	0	0	3.83
7	643.08	883.41	0.66	1.51	0.66	1.51	1	0	0	1.56
7	645.08	595.33	0.64	1.56	0.64	1.56	1	1	0	1.63
7	646.08	651.72	0.62	1.63	0.62	1.63	1	0	0	3.26
7	647.08	697.19	0.84	1.19	0.84	1.19	1	2	0	2.42
7	648.08	694.93	0.81	1.23	0.80	1.24	0		1	.
7	649.08	102.77	0.80	1.24	0.80	1.24	1	0	0	1.20
7	650.08	531.93	0.85	1.18	0.83	1.20	0		1	.
7	651.08	933.76	0.59	1.70	0.59	1.70	1	2	0	3.26
7	656.08	770.43	0.83	1.20	0.83	1.20	1	0	0	2.42
7	657.08	1072.34	0.68	1.48	0.68	1.48	1	0	0	1.24
7	658.08	979.98	0.95	1.05	0.95	1.05	1	0	0	1.48
7	659.08	1252.95	1.02	0.98	1.02	0.98	1	0	0	1.05
7	661.08	1010.74	0.67	1.49	0.67	1.49	1	0	0	0.98
7	662.08	1222.05	0.66	1.51	0.67	1.49	0		1	.
7	663.08	1049.52	0.87	1.15	0.87	1.15	1	0	0	1.49
7	664.08	142.65	0.79	1.26	0.79	1.26	1	0	0	1.15
7	672.08	327.06	0.26	3.83	0.26	3.83	1	0	0	3.82
7	674.08	261.23	0.41	2.42	0.41	2.42	1	0	0	1.51
7	675.08	268.80	0.42	2.40	0.42	2.40	1	3	0	2.42
7	252.09	209.27	0.97	1.03	0.97	1.03	1	2	0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	255.09	0	.	0	0	.	255	0	0.93	0	22.98
7	353.09	0	.	1	0	1	353	0	1.71	0	22.98
7	355.09	0	.	1	0	1	355	0	1.87	0	12.78
7	358.09	0	.	0	0	2	358	0	1.40	1	22.98
7	383.09	1	.	0	0	1	383	0	1.71	2	33.18
7	384.09	0	.	1	0	1	384	0	1.40	2	22.98
7	392.09	1	.	1	0	2	392	0	1.40	0	2.58
7	406.09	0	.	1	0	1	406	0	0.62	1	22.98
7	418.09	0	.	1	1	1	418	0	1.40	1	2.58
7	420.09	1	0	1	0	1	421	0	1.40	2	2.58
7	421.09	1	.	1	0	1	421	0	1.24	1	2.58
7	422.09	1	.	1	0	1	422	0	1.71	2	22.98
7	423.09	1	0	1	0	1	421	0	1.55	1	2.58
7	424.09	1	0	0	0	1	422	0	1.55	1	22.98
7	425.09	1	0	1	0	1	426	0	1.71	2	33.18
7	426.09	1	.	1	0	1	426	0	1.71	1	33.18
7	427.09	1	.	1	1	1	427	0	1.24	2	43.38
7	428.09	0	.	1	0	1	428	0	1.40	1	33.18
7	429.09	1	1	1	0	1	428	0	1.40	1	33.18
7	430.09	1	.	1	0	1	430	0	1.71	2	43.38
7	431.09	1	.	1	0	1	431	1	1.40	0	43.38
7	433.09	0	.	0	0	1	433	1	1.71	1	43.38
7	435.09	0	1	1	0	1	442	0	1.87	2	12.78
7	438.09	1	1	0	0	2	442	0	1.71	1	43.38
7	440.09	0	0	0	0	1	442	0	1.71	1	22.98
7	442.09	1	.	1	0	2	442	0	1.55	1	12.78
7	443.09	1	1	1	0	1	457	0	1.24	1	63.78
7	444.09	1	.	1	0	1	444	0	1.40	1	63.78
7	446.09	1	.	1	0	1	446	0	1.87	2	43.38
7	448.09	0	0	0	1	1	446	0	1.87	2	43.38
7	451.09	0	.	0	0	1	451	0	2.02	0	43.38
7	452.09	0	.	1	0	1	452	0	1.40	1	43.38
7	454.09	1	1	1	0	1	451	0	2.02	0	53.58
7	456.09	1	.	1	0	1	456	0	1.87	1	33.18
7	457.09	0	.	1	0	1	457	0	1.09	1	63.78
7	464.09	0	1	1	0	1	446	0	1.87	1	43.38
7	465.09	0	.	0	0	1	465	0	1.71	2	63.78
7	470.09	1	.	1	0	1	470	0	1.87	0	63.78
7	475.09	1	0	1	0	1	479	0	1.71	2	33.18
7	477.09	1	0	1	0	1	479	0	1.71	2	33.18
7	478.09	1	1	1	0	1	479	0	1.55	1	33.18
7	479.09	0	.	0	0	2	479	0	1.55	1	33.18
7	482.09	0	.	1	0	1	482	1	2.18	2	33.18
7	483.09	0	1	1	0	1	479	0	1.40	1	2.58
7	484.09	0	.	0	0	1	484	1	2.02	1	43.38
7	485.09	1	1	1	0	1	482	1	2.02	2	63.78
7	486.09	1	1	0	1	1	484	1	2.02	1	22.98
7	487.09	0	.	0	1	1	487	1	1.71	0	33.18
7	488.09	1	0	1	0	1	484	1	2.02	1	43.38
7	489.09	0	.	0	0	1	489	1	2.02	2	63.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	255.09	165.36	0.95	1.06	0.95	1.06	1	0	0	.
7	353.09	251.82	0.46	2.17	0.46	2.17	1	1	0	2.22
7	355.09	184.61	0.44	2.28	0.44	2.28	1	4	0	2.17
7	358.09	331.03	0.45	2.22	0.45	2.22	1	1	0	1.06
7	383.09	77.98	0.55	1.82	0.55	1.82	1	1	0	2.07
7	384.09	148.08	0.48	2.07	0.48	2.07	1	1	0	2.28
7	392.09	145.65	0.50	2.01	0.50	2.01	1	4	0	1.82
7	406.09	353.82	0.89	1.12	0.89	1.12	1	3	0	.
7	418.09	167.60	0.39	2.56	0.39	2.56	1	4	0	2.01
7	420.09	123.06	0.40	2.51	0.40	2.51	0		1	.
7	421.09	99.27	0.40	2.51	0.40	2.51	1	1	0	2.56
7	422.09	124.16	0.41	2.44	0.41	2.44	1	1	0	2.51
7	423.09	100.87	0.40	2.50	0.40	2.51	0		0	.
7	424.09	102.97	0.40	2.49	0.41	2.44	0		1	.
7	425.09	101.27	0.41	2.45	0.41	2.46	0		1	.
7	426.09	86.28	0.41	2.46	0.41	2.46	1	1	0	2.44
7	427.09	106.01	0.50	1.99	0.50	1.99	1	1	0	2.16
7	428.09	107.98	0.46	2.16	0.46	2.16	1	1	0	2.46
7	429.09	87.85	0.46	2.17	0.46	2.16	0		1	.
7	430.09	88.82	0.53	1.89	0.53	1.89	1	2	0	1.99
7	431.09	409.47	0.50	2.02	0.50	2.02	1	3	0	1.99
7	433.09	407.20	0.50	2.02	0.50	2.02	1	4	0	1.99
7	435.09	181.68	0.52	1.91	0.50	1.98	0		1	.
7	438.09	185.79	0.51	1.95	0.50	1.98	0		0	.
7	440.09	199.17	0.52	1.94	0.50	1.98	0		0	.
7	442.09	66.33	0.50	1.98	0.50	1.98	1	1	0	2.02
7	443.09	62.99	0.56	1.77	0.56	1.79	0		1	.
7	444.09	202.70	0.52	1.94	0.52	1.94	1	2	0	1.79
7	446.09	422.35	0.49	2.03	0.49	2.03	1	1	0	1.79
7	448.09	423.79	0.49	2.04	0.49	2.03	0		0	.
7	451.09	98.26	0.48	2.08	0.48	2.08	1	4	0	2.03
7	452.09	245.41	0.53	1.90	0.53	1.90	1	1	0	1.98
7	454.09	197.53	0.47	2.13	0.48	2.08	0		1	.
7	456.09	64.56	0.45	2.21	0.45	2.21	1	4	0	2.08
7	457.09	214.35	0.56	1.79	0.56	1.79	1	1	0	1.90
7	464.09	73.67	0.49	2.02	0.49	2.03	0		1	.
7	465.09	214.15	0.49	2.05	0.49	2.05	1	3	0	1.79
7	470.09	592.06	0.45	2.24	0.45	2.24	1	4	0	2.21
7	475.09	289.05	0.44	2.27	0.44	2.29	0		0	.
7	477.09	154.49	0.44	2.29	0.44	2.29	0		0	.
7	478.09	149.82	0.43	2.32	0.44	2.29	0		1	.
7	479.09	300.56	0.44	2.29	0.44	2.29	1	4	0	2.24
7	482.09	184.35	0.47	2.13	0.47	2.13	1	2	0	2.29
7	483.09	127.22	0.43	2.31	0.44	2.29	0		0	.
7	484.09	115.35	0.43	2.33	0.43	2.33	1	3	0	2.29
7	485.09	156.16	0.49	2.02	0.47	2.13	0		1	.
7	486.09	162.66	0.43	2.33	0.43	2.33	0		1	.
7	487.09	129.86	0.47	2.11	0.47	2.11	1	2	0	2.29
7	488.09	110.27	0.43	2.34	0.43	2.33	0		0	.
7	489.09	131.80	0.47	2.14	0.47	2.14	1	2	0	2.29

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	490.09	1	.	1	0	2	490	1	2.02	1	43.38
7	491.09	0	0	1	0	1	489	1	1.71	2	63.78
7	492.09	0	1	1	0	1	490	1	2.02	1	43.38
7	493.09	0	1	1	0	1	498	0	1.71	1	63.78
7	494.09	1	1	0	0	2	498	0	1.55	1	63.78
7	497.09	1	.	1	0	1	497	1	1.87	1	43.38
7	498.09	0	.	0	1	2	498	0	1.55	1	53.58
7	499.09	1	.	1	0	1	499	0	1.71	2	63.78
7	500.09	1	1	1	0	1	498	0	1.55	1	63.78
7	501.09	1	.	1	0	2	501	0	1.71	1	22.98
7	502.09	0	1	0	0	1	499	0	1.87	1	22.98
7	503.09	1	1	1	0	1	499	0	1.71	1	43.38
7	504.09	0	0	0	0	1	499	0	1.87	2	43.38
7	505.09	0	1	0	0	1	499	0	1.87	1	63.78
7	506.09	0	0	1	0	1	499	0	2.02	2	63.78
7	507.09	1	.	1	0	1	507	1	2.18	1	53.58
7	508.09	0	.	1	0	1	508	1	2.18	2	53.58
7	509.09	1	1	1	0	1	547	0	2.02	2	63.78
7	510.09	0	0	1	0	1	508	1	2.02	2	53.58
7	511.09	1	.	0	0	1	511	0	2.02	0	63.78
7	512.09	1	.	1	0	1	512	0	2.02	2	94.38
7	513.09	1	1	1	0	1	531	0	2.18	2	63.78
7	514.09	1	.	1	0	1	514	0	1.55	2	53.58
7	515.09	1	0	1	0	1	517	0	1.71	1	53.58
7	517.09	1	.	1	1	1	517	0	1.71	0	53.58
7	518.09	1	.	1	0	1	518	0	2.18	2	94.38
7	519.09	0	1	1	1	1	517	0	1.71	2	53.58
7	520.09	1	0	1	0	1	517	0	1.71	1	53.58
7	524.09	0	0	1	0	2	525	0	1.55	1	94.38
7	525.09	0	.	1	0	2	525	0	1.87	1	94.38
7	530.09	1	0	1	0	1	531	0	1.87	2	22.98
7	531.09	0	.	0	0	1	531	0	2.49	1	22.98
7	532.09	1	.	1	0	1	532	0	2.02	0	22.98
7	533.09	0	0	1	0	1	531	0	2.02	1	63.78
7	534.09	0	0	0	0	1	531	0	2.33	2	63.78
7	535.09	1	.	1	0	2	535	0	2.33	1	53.58
7	536.09	1	0	1	0	1	531	0	2.49	1	12.78
7	537.09	0	.	1	0	1	537	0	1.55	1	53.58
7	538.09	0	0	0	0	1	537	0	1.40	1	53.58
7	539.09	1	0	1	0	2	517	0	1.87	1	53.58
7	540.09	1	.	1	0	1	540	0	1.71	1	2.58
7	541.09	1	.	1	0	1	541	0	1.71	1	2.58
7	542.09	1	1	1	0	1	525	0	1.55	1	94.38
7	543.09	1	.	1	0	2	543	0	1.55	1	43.38
7	544.09	1	.	1	0	1	544	0	1.87	1	94.38
7	545.09	1	.	1	0	1	545	0	1.87	2	94.38
7	546.09	0	.	0	0	2	546	0	1.71	2	94.38
7	547.09	0	.	0	0	1	547	0	2.18	1	12.78
7	548.09	0	.	1	0	1	548	0	2.02	1	12.78
7	552.09	1	.	1	0	1	552	0	1.55	1	33.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	490.09	118.58	0.43	2.33	0.43	2.33	1	3	0	2.29
7	491.09	132.73	0.45	2.21	0.47	2.14	0		1	.
7	492.09	112.94	0.44	2.26	0.43	2.33	0		1	.
7	493.09	111.21	0.42	2.36	0.43	2.33	0		0	.
7	494.09	240.51	0.43	2.35	0.43	2.33	0		1	.
7	497.09	133.66	0.43	2.35	0.43	2.35	1	3	0	2.29
7	498.09	122.62	0.43	2.33	0.43	2.33	1	1	0	2.31
7	499.09	116.98	0.42	2.39	0.42	2.39	1	1	0	2.33
7	500.09	162.56	0.42	2.36	0.43	2.33	0		0	.
7	501.09	172.41	0.43	2.31	0.43	2.31	1	1	0	2.29
7	502.09	140.84	0.42	2.41	0.42	2.39	0		1	.
7	503.09	144.61	0.42	2.37	0.42	2.39	0		0	.
7	504.09	123.22	0.42	2.38	0.42	2.39	0		0	.
7	505.09	124.52	0.41	2.43	0.42	2.39	0		0	.
7	506.09	153.78	0.42	2.40	0.42	2.39	0		0	.
7	507.09	152.85	0.39	2.58	0.39	2.58	1	2	0	2.39
7	508.09	135.43	0.37	2.69	0.37	2.69	1	3	0	2.39
7	509.09	155.35	0.30	3.35	0.30	3.33	0		1	.
7	510.09	136.57	0.35	2.88	0.37	2.69	0		1	.
7	511.09	111.84	0.32	3.16	0.32	3.16	1	2	0	3.33
7	512.09	138.27	0.29	3.43	0.29	3.43	1	3	0	3.33
7	513.09	171.10	0.30	3.33	0.30	3.34	0		0	.
7	514.09	174.17	0.33	3.06	0.33	3.06	1	2	0	3.24
7	515.09	397.76	0.33	3.08	0.32	3.09	0		0	.
7	517.09	110.71	0.32	3.09	0.32	3.09	1	1	0	3.24
7	518.09	175.24	0.29	3.39	0.29	3.39	1	1	0	3.33
7	519.09	169.67	0.32	3.09	0.32	3.09	0		0	.
7	520.09	315.58	0.33	3.07	0.32	3.09	0		1	.
7	524.09	114.05	0.24	4.21	0.24	4.16	0		1	.
7	525.09	401.53	0.24	4.16	0.24	4.16	1	0	0	4.13
7	530.09	188.96	0.30	3.37	0.30	3.34	0		0	.
7	531.09	215.75	0.30	3.34	0.30	3.34	1	1	0	3.39
7	532.09	95.29	0.31	3.20	0.31	3.20	1	2	0	3.09
7	533.09	96.63	0.30	3.33	0.30	3.34	0		0	.
7	534.09	163.23	0.30	3.34	0.30	3.34	0		1	.
7	535.09	234.60	0.31	3.24	0.31	3.24	1	1	0	3.34
7	536.09	164.46	0.30	3.37	0.30	3.34	0		0	.
7	537.09	165.80	0.31	3.22	0.31	3.22	1	3	0	3.24
7	538.09	172.77	0.31	3.22	0.31	3.22	0		1	.
7	539.09	254.05	0.33	3.07	0.32	3.09	0		0	.
7	540.09	252.09	0.24	4.13	0.24	4.13	1	1	0	3.09
7	541.09	118.18	0.24	4.11	0.24	4.11	1	3	0	3.09
7	542.09	188.89	0.24	4.19	0.24	4.16	0		0	.
7	543.09	125.02	0.24	4.19	0.24	4.19	1	0	0	4.16
7	544.09	126.33	0.24	4.19	0.24	4.19	1	2	0	4.19
7	545.09	126.83	0.24	4.24	0.24	4.24	1	3	0	4.19
7	546.09	222.49	0.24	4.20	0.24	4.20	1	4	0	4.19
7	547.09	225.19	0.30	3.33	0.30	3.33	1	1	0	2.39
7	548.09	348.65	0.30	3.38	0.30	3.38	1	3	0	3.33
7	552.09	230.63	0.24	4.21	0.24	4.21	1	1	0	4.28

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	553.09	0	.	1	0	1	553	1	1.24	1	22.98
7	555.09	1	.	1	0	1	555	1	1.71	2	43.38
7	556.09	1	.	1	0	1	556	1	2.33	2	53.58
7	557.09	0	0	1	0	1	553	1	1.71	1	12.78
7	558.09	0	0	0	0	1	553	1	1.71	1	12.78
7	559.09	1	.	0	0	1	559	1	1.71	0	94.38
7	560.09	0	.	1	0	2	560	0	1.87	2	12.78
7	561.09	1	.	1	0	2	556	1	2.33	2	53.58
7	563.09	0	.	0	0	1	563	0	2.33	0	43.38
7	564.09	1	0	1	0	1	565	0	1.24	1	53.58
7	565.09	1	.	1	0	3	565	0	1.24	1	43.38
7	566.09	1	0	0	0	1	565	0	1.40	1	94.38
7	567.09	1	.	1	0	1	567	0	1.55	1	94.38
7	568.09	0	.	1	0	2	568	0	1.87	1	2.58
7	569.09	0	0	1	0	1	570	0	2.02	2	33.18
7	570.09	0	.	0	0	2	570	0	2.02	1	2.58
7	571.09	1	1	1	0	2	570	0	1.55	1	94.38
7	572.09	0	0	1	0	2	570	0	1.71	1	53.58
7	573.09	1	0	0	0	2	574	0	2.18	2	94.38
7	574.09	0	.	1	0	3	574	0	1.40	1	94.38
7	575.09	0	.	1	0	1	575	0	2.49	2	94.38
7	576.09	1	0	1	0	1	574	0	1.40	1	94.38
7	577.09	1	1	1	0	2	574	0	1.40	1	94.38
7	578.09	1	0	0	0	1	574	0	1.87	1	94.38
7	579.09	1	0	1	0	1	574	0	1.71	2	94.38
7	580.09	1	0	1	0	1	574	0	1.55	1	94.38
7	582.09	0	.	0	0	2	582	0	2.18	1	33.18
7	583.09	0	0	0	0	1	586	0	1.87	1	73.98
7	584.09	0	1	1	0	1	586	0	1.87	2	73.98
7	585.09	1	0	1	0	1	586	0	2.02	1	94.38
7	586.09	1	.	1	0	1	586	0	2.02	2	94.38
7	587.09	1	.	1	0	1	587	0	2.02	2	53.58
7	588.09	0	.	0	0	1	588	0	1.55	2	94.38
7	590.09	0	1	1	0	1	555	1	1.87	2	43.38
7	591.09	0	.	1	0	1	591	0	1.40	1	33.18
7	592.09	0	.	1	1	1	592	0	1.87	2	94.38
7	593.09	1	1	1	0	1	591	0	1.55	1	94.38
7	594.09	0	0	0	0	1	592	0	1.71	2	94.38
7	595.09	1	.	1	0	1	595	0	1.71	1	94.38
7	596.09	0	0	0	0	1	592	0	1.55	2	63.78
7	597.09	1	.	1	0	1	597	0	1.71	1	94.38
7	598.09	0	1	0	0	1	597	0	2.02	1	94.38
7	599.09	1	1	1	0	1	597	0	2.02	1	94.38
7	600.09	1	.	1	0	1	600	1	1.71	2	94.38
7	601.09	1	0	1	0	1	597	0	2.02	1	94.38
7	603.09	0	0	1	0	1	592	0	1.87	1	94.38
7	604.09	1	.	1	0	1	604	0	2.49	2	94.38
7	605.09	0	1	1	0	1	600	1	1.71	2	94.38
7	606.09	1	.	1	0	1	606	0	2.80	1	33.18
7	607.09	0	1	1	0	1	611	1	1.55	1	22.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	553.09	452.62	0.20	4.99	0.20	4.99	1	3	0	4.21
7	555.09	217.11	0.24	4.20	0.24	4.20	1	2	0	4.21
7	556.09	274.31	0.24	4.21	0.24	4.21	1	2	0	4.21
7	557.09	276.34	0.20	5.04	0.20	4.99	0		1	.
7	558.09	130.30	0.20	5.04	0.20	4.99	0		0	.
7	559.09	268.20	0.20	4.97	0.20	4.97	1	3	0	4.21
7	560.09	220.45	0.23	4.28	0.23	4.28	1	4	0	4.20
7	561.09	364.13	0.24	4.22	0.24	4.21	1	0	0	.
7	563.09	207.64	0.21	4.67	0.21	4.67	1	3	0	4.21
7	564.09	191.22	0.18	5.57	0.19	5.29	0		1	.
7	565.09	133.73	0.19	5.29	0.19	5.29	1	3	0	4.21
7	566.09	132.73	0.18	5.59	0.19	5.29	0		0	.
7	567.09	292.79	0.18	5.61	0.18	5.61	1	1	0	4.21
7	568.09	256.19	0.18	5.59	0.18	5.59	1	1	0	5.61
7	569.09	297.36	0.18	5.54	0.18	5.50	0		1	.
7	570.09	168.33	0.18	5.50	0.18	5.50	1	1	0	5.59
7	571.09	222.72	0.20	5.05	0.18	5.50	0		0	.
7	572.09	178.74	0.18	5.55	0.18	5.50	0		0	.
7	573.09	170.87	0.18	5.44	0.21	4.82	0		0	.
7	574.09	180.71	0.21	4.82	0.21	4.82	1	0	0	5.50
7	575.09	174.14	0.18	5.46	0.18	5.46	1	4	0	4.82
7	576.09	172.77	0.18	5.45	0.21	4.82	0		0	.
7	577.09	178.18	0.18	5.44	0.21	4.82	0		1	.
7	578.09	176.28	0.18	5.44	0.21	4.82	0		0	.
7	579.09	176.11	0.18	5.44	0.21	4.82	0		0	.
7	580.09	431.83	0.18	5.44	0.21	4.82	0		0	.
7	582.09	223.92	0.18	5.51	0.18	5.51	1	3	0	5.46
7	583.09	225.96	0.18	5.52	0.18	5.49	0		0	.
7	584.09	188.42	0.18	5.49	0.18	5.49	0		0	.
7	585.09	187.85	0.18	5.53	0.18	5.49	0		1	.
7	586.09	272.87	0.18	5.49	0.18	5.49	1	4	0	5.46
7	587.09	193.66	0.23	4.26	0.23	4.26	1	2	0	4.67
7	588.09	437.41	0.18	5.64	0.18	5.64	1	3	0	5.23
7	590.09	288.36	0.22	4.65	0.24	4.20	0		1	.
7	591.09	201.83	0.19	5.23	0.19	5.23	1	1	0	5.49
7	592.09	184.18	0.22	4.56	0.22	4.56	1	1	0	4.67
7	593.09	213.98	0.21	4.75	0.19	5.23	0		1	.
7	594.09	186.62	0.22	4.55	0.22	4.56	0		0	.
7	595.09	250.38	0.21	4.67	0.21	4.67	1	1	0	5.23
7	596.09	191.79	0.22	4.53	0.22	4.56	0		0	.
7	597.09	195.03	0.21	4.68	0.21	4.68	1	3	0	4.67
7	598.09	199.03	0.21	4.69	0.21	4.68	0		1	.
7	599.09	232.23	0.21	4.72	0.21	4.68	0		0	.
7	600.09	197.83	0.27	3.75	0.27	3.75	1	2	0	4.56
7	601.09	670.90	0.21	4.75	0.21	4.68	0		0	.
7	603.09	240.27	0.22	4.61	0.22	4.56	0		1	.
7	604.09	217.32	0.22	4.60	0.22	4.60	1	2	0	4.56
7	605.09	341.14	0.27	3.67	0.27	3.75	0		1	.
7	606.09	311.71	0.21	4.81	0.21	4.81	1	3	0	4.56
7	607.09	262.63	0.24	4.15	0.22	4.47	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	608.09	1	.	1	0	1	608	1	2.02	0	63.78
7	609.09	0	1	1	0	1	606	0	2.64	0	94.38
7	610.09	1	0	1	0	1	611	1	1.55	1	94.38
7	611.09	1	.	0	0	1	611	1	1.55	1	94.38
7	612.09	0	.	1	0	1	612	1	2.18	2	94.38
7	613.09	0	.	1	0	1	613	0	2.49	2	63.78
7	614.09	1	1	1	0	1	612	1	2.02	2	94.38
7	615.09	1	1	1	0	1	611	1	1.55	1	94.38
7	616.09	1	0	1	0	1	611	1	1.87	1	94.38
7	617.09	0	1	1	0	1	618	0	1.87	1	63.78
7	618.09	1	.	1	0	1	618	0	2.02	2	63.78
7	621.09	1	1	1	0	1	600	1	2.18	2	53.58
7	622.09	1	.	1	0	1	622	1	2.18	0	53.58
7	626.09	1	0	1	0	1	618	0	2.02	2	63.78
7	627.09	1	1	1	0	1	618	0	2.18	1	63.78
7	630.09	1	.	0	0	1	630	1	1.87	1	33.18
7	631.09	0	1	0	0	2	618	0	1.24	2	94.38
7	632.09	1	0	1	0	1	618	0	0.93	0	94.38
7	634.09	0	.	1	0	1	634	1	2.18	1	63.78
7	635.09	1	.	1	0	1	635	0	1.55	2	63.78
7	636.09	0	.	0	0	2	636	0	1.55	1	94.38
7	637.09	0	0	0	0	1	636	0	1.87	2	94.38
7	638.09	0	.	0	0	3	638	0	1.55	1	22.98
7	639.09	0	.	0	0	.	639	0	0.62	1	94.38
7	640.09	0	.	0	0	1	640	0	1.40	0	43.38
7	641.09	1	1	1	0	2	618	0	1.24	0	53.58
7	642.09	1	.	1	0	3	642	0	0.93	1	43.38
7	643.09	1	.	1	0	.	643	0	0.47	1	53.58
7	645.09	0	.	0	0	1	645	0	0.62	0	22.98
7	646.09	0	.	1	0	1	646	0	0.62	2	22.98
7	647.09	0	.	0	0	.	647	0	0.31	2	84.18
7	648.09	0	0	1	0	1	649	0	0.62	2	73.98
7	649.09	0	.	0	0	.	649	0	0.31	1	73.98
7	650.09	0	0	0	0	1	656	0	0.62	2	22.98
7	651.09	0	.	0	0	3	651	0	0.93	1	53.58
7	656.09	0	.	1	0	.	656	0	0.31	1	22.98
7	657.09	0	.	1	0	.	657	0	0.31	1	73.98
7	659.09	0	.	1	0	.	659	0	0.31	2	84.18
7	661.09	0	.	0	0	.	661	0	0.31	1	73.98
7	662.09	0	0	0	0	1	661	0	0.62	2	73.98
7	663.09	1	.	1	0	.	663	0	0.31	1	84.18
7	664.09	1	.	1	0	.	664	0	0.31	1	94.38
7	672.09	1	0	1	0	2	618	0	2.18	2	53.58
7	674.09	1	.	1	0	2	674	0	1.40	0	63.78
7	675.09	0	.	0	0	.	675	0	0.62	1	63.78
7	678.09	1	0	0	0	1	507	1	2.02	1	22.98
7	679.09	1	.	0	0	1	679	0	2.49	1	94.38
7	681.09	1	.	0	0	.	681	0	0.47	1	94.38
7	252.1	0	.	1	0	2	252	0	0.62	2	2.58
7	255.1	0	.	0	0	2	255	0	0.78	1	2.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	608.09	241.01	0.22	4.64	0.22	4.64	1	3	0	4.56
7	609.09	210.14	0.21	4.74	0.21	4.81	0		1	.
7	610.09	207.07	0.24	4.15	0.22	4.47	0		1	.
7	611.09	256.86	0.22	4.47	0.22	4.47	1	3	0	4.56
7	612.09	273.34	0.24	4.25	0.24	4.25	1	1	0	4.70
7	613.09	242.54	0.21	4.70	0.21	4.70	1	4	0	4.56
7	614.09	213.01	0.24	4.23	0.24	4.25	0		0	.
7	615.09	215.21	0.25	4.05	0.22	4.47	0		0	.
7	616.09	308.94	0.24	4.09	0.22	4.47	0		0	.
7	617.09	306.67	0.23	4.38	0.23	4.44	0		1	.
7	618.09	505.24	0.23	4.44	0.23	4.44	1	1	0	4.25
7	621.09	302.00	0.26	3.83	0.27	3.75	0		0	.
7	622.09	496.47	0.25	4.03	0.25	4.03	1	2	0	4.56
7	626.09	311.14	0.23	4.44	0.23	4.44	0		0	.
7	627.09	509.04	0.23	4.41	0.23	4.44	0		0	.
7	630.09	273.81	0.22	4.50	0.22	4.50	1	3	0	4.25
7	631.09	272.34	0.26	3.89	0.23	4.44	0		0	.
7	632.09	818.55	0.24	4.11	0.23	4.44	0		0	.
7	634.09	323.92	0.20	4.89	0.20	4.89	1	3	0	4.25
7	635.09	306.07	0.30	3.29	0.30	3.29	1	1	0	4.44
7	636.09	307.37	0.30	3.28	0.30	3.28	1	1	0	3.29
7	637.09	415.95	0.30	3.28	0.30	3.28	0		1	.
7	638.09	460.16	0.29	3.40	0.29	3.40	1	0	0	3.28
7	639.09	430.26	0.65	1.53	0.65	1.53	1	0	0	3.51
7	640.09	343.64	0.15	6.68	0.15	6.68	1	3	0	.
7	641.09	422.65	0.28	3.54	0.23	4.44	0		0	.
7	642.09	594.89	0.28	3.51	0.28	3.51	1	0	0	3.40
7	643.09	883.41	0.67	1.48	0.67	1.48	1	0	0	2.18
7	645.09	595.33	0.46	2.18	0.46	2.18	1	0	0	2.05
7	646.09	651.72	0.49	2.05	0.49	2.05	1	0	0	2.57
7	647.09	697.19	1.01	0.99	1.01	0.99	1	0	0	1.48
7	648.09	694.93	0.87	1.15	0.86	1.17	0		1	.
7	649.09	102.77	0.86	1.17	0.86	1.17	1	0	0	1.12
7	650.09	531.93	0.91	1.10	0.89	1.12	0		1	.
7	651.09	933.76	0.39	2.57	0.39	2.57	1	0	0	2.56
7	656.09	770.43	0.89	1.12	0.89	1.12	1	0	0	0.99
7	657.09	1072.34	0.74	1.35	0.74	1.35	1	0	0	1.17
7	659.09	1252.95	1.10	0.91	1.10	0.91	1	0	0	1.35
7	661.09	1010.74	0.64	1.57	0.64	1.57	1	0	0	0.91
7	662.09	1222.05	0.64	1.55	0.64	1.57	0		1	.
7	663.09	1049.52	0.86	1.17	0.86	1.17	1	0	0	1.57
7	664.09	142.65	0.83	1.21	0.83	1.21	1	0	0	1.17
7	672.09	327.06	0.23	4.41	0.23	4.44	0		0	.
7	674.09	261.23	0.42	2.41	0.42	2.41	1	2	0	1.48
7	675.09	268.80	0.36	2.78	0.36	2.78	1	3	0	1.48
7	678.09	65.83	0.38	2.66	0.39	2.58	0		1	.
7	679.09	184.78	0.19	5.40	0.19	5.40	1	2	0	5.46
7	681.09	383.15	0.39	2.56	0.39	2.56	1	0	0	1.53
7	252.1	209.27	1.18	0.85	1.18	0.85	1	0	0	0.86
7	255.1	165.36	1.14	0.88	1.14	0.88	1	0	0	0.85

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	353.1	0	.	1	0	3	353	0	0.62	1	2.58
7	358.1	0	.	0	0	.	358	0	0.31	1	2.58
7	383.1	1	.	0	0	1	383	0	0.62	2	12.78
7	384.1	0	.	1	0	.	384	0	0.31	2	2.58
7	406.1	0	.	1	0	.	406	0	0.31	1	2.58
7	422.1	1	.	1	0	3	422	0	1.09	2	2.58
7	424.1	1	0	0	0	1	422	0	0.93	1	2.58
7	425.1	1	0	1	0	1	426	0	1.40	2	12.78
7	426.1	1	.	1	0	1	426	0	1.09	0	12.78
7	427.1	1	.	1	1	.	427	0	0.47	2	22.98
7	428.1	0	.	1	0	.	428	0	0.62	1	12.78
7	429.1	1	1	1	0	1	428	0	0.78	0	12.78
7	430.1	1	0	1	0	1	431	0	0.93	0	22.98
7	431.1	1	.	1	0	2	431	0	0.93	0	22.98
7	433.1	0	1	0	0	1	431	0	1.24	1	22.98
7	438.1	1	.	0	0	2	438	0	0.93	1	22.98
7	440.1	0	.	0	0	1	440	0	0.93	2	2.58
7	443.1	1	.	1	0	1	443	0	0.93	0	43.38
7	444.1	1	.	1	0	1	444	0	0.93	1	43.38
7	446.1	1	.	1	0	1	446	0	1.71	2	22.98
7	448.1	0	.	0	1	1	448	0	2.02	1	22.98
7	451.1	0	0	0	0	1	448	0	2.02	1	22.98
7	452.1	0	.	1	0	3	452	0	1.09	1	22.98
7	454.1	1	.	1	0	2	454	0	1.55	1	33.18
7	456.1	1	.	1	0	2	456	0	1.24	1	12.78
7	457.1	0	.	1	0	.	457	0	0.78	1	43.38
7	464.1	0	.	1	0	1	464	0	1.40	1	22.98
7	465.1	0	.	0	0	1	465	0	1.40	0	43.38
7	470.1	1	0	1	0	1	456	0	1.24	0	43.38
7	475.1	1	0	1	0	1	478	0	1.24	0	12.78
7	477.1	1	.	1	0	1	477	0	1.24	1	12.78
7	478.1	1	.	1	0	1	478	0	1.09	0	12.78
7	479.1	0	.	0	0	.	479	0	0.78	1	12.78
7	482.1	0	.	1	0	1	482	0	1.87	1	12.78
7	484.1	0	.	0	0	2	484	0	1.71	1	22.98
7	485.1	1	.	1	0	1	485	0	1.55	2	43.38
7	486.1	1	.	0	1	1	486	0	1.71	1	2.58
7	487.1	0	.	0	1	1	487	0	1.55	1	12.78
7	488.1	1	0	1	0	1	486	0	1.71	1	22.98
7	489.1	0	.	0	0	1	489	1	1.71	2	43.38
7	490.1	1	1	1	0	2	482	0	1.40	0	22.98
7	491.1	0	0	1	0	1	489	1	1.87	2	43.38
7	492.1	0	0	1	0	1	487	0	1.71	0	22.98
7	493.1	0	.	1	0	1	493	0	1.71	1	43.38
7	494.1	1	.	0	0	1	494	0	1.24	1	43.38
7	497.1	1	.	1	0	1	497	1	1.55	1	22.98
7	498.1	0	1	0	1	2	497	1	1.24	1	33.18
7	499.1	1	.	1	0	1	499	0	2.18	2	43.38
7	500.1	1	1	1	0	1	493	0	2.02	1	43.38
7	501.1	1	0	1	0	3	497	1	1.55	1	2.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	353.1	251.82	0.56	1.78	0.56	1.78	1	0	0	1.81
7	358.1	331.03	0.55	1.81	0.55	1.81	1	0	0	0.88
7	383.1	77.98	1.01	0.99	1.01	0.99	1	0	0	1.52
7	384.1	148.08	0.66	1.52	0.66	1.52	1	0	0	1.78
7	406.1	353.82	1.16	0.86	1.16	0.86	1	0	0	.
7	422.1	124.16	0.73	1.37	0.73	1.37	1	0	0	0.99
7	424.1	102.97	0.75	1.33	0.73	1.37	0		1	.
7	425.1	101.27	0.73	1.37	0.71	1.42	0		1	.
7	426.1	86.28	0.71	1.42	0.71	1.42	1	0	0	1.37
7	427.1	106.01	0.70	1.43	0.70	1.43	1	0	0	1.56
7	428.1	107.98	0.64	1.56	0.64	1.56	1	0	0	1.42
7	429.1	87.85	0.65	1.55	0.64	1.56	0		1	.
7	430.1	88.82	0.67	1.49	0.67	1.49	0		1	.
7	431.1	409.47	0.67	1.49	0.67	1.49	1	0	0	1.43
7	433.1	407.20	0.68	1.48	0.67	1.49	0		0	.
7	438.1	185.79	0.63	1.59	0.63	1.59	1	1	0	1.49
7	440.1	199.17	0.23	4.27	0.23	4.27	1	3	0	.
7	443.1	62.99	0.63	1.59	0.63	1.59	1	1	0	1.69
7	444.1	202.70	0.58	1.73	0.58	1.73	1	3	0	1.59
7	446.1	422.35	0.62	1.62	0.62	1.62	1	2	0	1.59
7	448.1	423.79	0.60	1.67	0.60	1.67	1	1	0	1.59
7	451.1	98.26	0.61	1.63	0.60	1.67	0		1	.
7	452.1	245.41	0.63	1.57	0.63	1.57	1	0	0	1.59
7	454.1	197.53	0.61	1.63	0.61	1.63	1	1	0	1.67
7	456.1	64.56	0.63	1.59	0.63	1.59	1	1	0	1.63
7	457.1	214.35	0.59	1.69	0.59	1.69	1	0	0	1.57
7	464.1	73.67	0.56	1.79	0.56	1.79	1	3	0	1.59
7	465.1	214.15	0.65	1.55	0.65	1.55	1	2	0	1.59
7	470.1	592.06	0.62	1.60	0.63	1.59	0		1	.
7	475.1	289.05	0.66	1.52	0.67	1.49	0		1	.
7	477.1	154.49	0.59	1.70	0.59	1.70	1	3	0	1.49
7	478.1	149.82	0.67	1.49	0.67	1.49	1	1	0	1.60
7	479.1	300.56	0.63	1.60	0.63	1.60	1	0	0	1.59
7	482.1	184.35	0.65	1.55	0.65	1.55	1	1	0	1.62
7	484.1	115.35	0.62	1.62	0.62	1.62	1	4	0	1.49
7	485.1	156.16	0.71	1.41	0.71	1.41	1	2	0	1.55
7	486.1	162.66	0.61	1.64	0.61	1.64	1	3	0	1.62
7	487.1	129.86	0.63	1.58	0.63	1.58	1	3	0	1.55
7	488.1	110.27	0.63	1.59	0.61	1.64	0		1	.
7	489.1	131.80	0.74	1.35	0.74	1.35	1	2	0	1.55
7	490.1	118.58	0.64	1.56	0.65	1.55	0		1	.
7	491.1	132.73	0.74	1.34	0.74	1.35	0		1	.
7	492.1	112.94	0.62	1.60	0.63	1.58	0		1	.
7	493.1	111.21	0.61	1.65	0.61	1.65	1	1	0	1.64
7	494.1	240.51	0.61	1.64	0.61	1.64	1	1	0	1.55
7	497.1	133.66	0.60	1.67	0.60	1.67	1	3	0	1.55
7	498.1	122.62	0.60	1.65	0.60	1.67	0		0	.
7	499.1	116.98	0.60	1.66	0.60	1.66	1	0	0	1.65
7	500.1	162.56	0.59	1.71	0.61	1.65	0		1	.
7	501.1	172.41	0.61	1.63	0.60	1.67	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	502.1	0	1	0	0	1	499	0	1.87	1	2.58
7	503.1	1	1	1	0	1	499	0	1.87	1	22.98
7	504.1	0	0	0	0	1	499	0	2.02	2	22.98
7	505.1	0	1	0	0	2	499	0	1.71	1	43.38
7	506.1	0	0	1	0	1	499	0	1.71	2	43.38
7	507.1	1	1	1	0	1	499	0	2.02	1	33.18
7	508.1	0	0	1	0	1	499	0	1.71	2	33.18
7	509.1	1	.	1	0	1	509	0	1.55	2	43.38
7	510.1	0	1	1	0	1	499	0	1.71	2	33.18
7	511.1	1	0	0	0	1	518	0	1.55	1	43.38
7	512.1	1	0	1	0	1	509	0	1.71	2	73.98
7	513.1	1	.	1	0	1	513	0	1.40	2	43.38
7	514.1	1	.	1	0	2	514	0	1.09	2	33.18
7	515.1	1	0	1	0	1	514	0	1.55	1	33.18
7	517.1	1	0	1	1	1	514	0	1.40	1	33.18
7	518.1	1	.	1	0	2	518	0	1.55	0	73.98
7	519.1	0	1	1	1	1	514	0	1.55	1	33.18
7	520.1	1	0	1	0	1	514	0	1.40	1	33.18
7	524.1	0	0	1	0	1	525	0	1.71	0	73.98
7	525.1	0	.	1	0	2	525	0	1.71	1	73.98
7	530.1	1	.	1	0	1	530	0	1.55	0	2.58
7	531.1	0	.	0	0	2	531	0	1.87	1	2.58
7	532.1	1	.	1	0	1	532	0	1.87	1	2.58
7	533.1	0	0	1	0	1	531	0	1.24	1	43.38
7	534.1	0	0	0	0	1	531	0	1.55	2	43.38
7	535.1	1	.	1	0	3	535	0	1.24	1	33.18
7	537.1	0	.	1	0	2	537	0	1.24	1	33.18
7	538.1	0	0	0	0	1	537	0	1.24	1	33.18
7	539.1	1	0	1	0	2	514	0	1.40	1	33.18
7	542.1	1	1	1	0	1	525	0	1.71	1	73.98
7	543.1	1	0	1	0	2	525	0	1.55	1	22.98
7	544.1	1	0	1	0	1	525	0	1.24	1	73.98
7	545.1	1	0	1	0	1	525	0	1.40	2	73.98
7	546.1	0	1	0	0	2	525	0	1.55	0	73.98
7	552.1	1	.	1	0	2	552	0	1.24	1	12.78
7	553.1	0	1	1	0	1	552	0	1.40	1	2.58
7	555.1	1	.	1	0	2	555	0	1.24	2	22.98
7	556.1	1	.	1	0	1	556	0	1.87	1	33.18
7	559.1	1	.	0	0	2	559	1	1.40	2	73.98
7	561.1	1	.	1	0	2	561	0	1.87	1	33.18
7	563.1	0	.	0	0	1	563	1	1.71	1	22.98
7	564.1	1	0	1	0	1	565	1	1.09	0	33.18
7	565.1	1	.	1	0	1	565	1	0.78	1	22.98
7	566.1	1	0	0	0	1	565	1	1.40	1	73.98
7	567.1	1	.	1	0	1	567	1	1.71	1	73.98
7	569.1	0	.	1	0	1	569	0	1.87	2	12.78
7	571.1	1	.	1	0	2	571	0	1.09	1	73.98
7	572.1	0	.	1	0	2	572	0	1.87	1	33.18
7	573.1	1	0	0	0	1	574	0	1.87	2	73.98
7	574.1	0	.	1	0	2	574	0	1.24	1	73.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	502.1	140.84	0.60	1.65	0.60	1.66	0		1	.
7	503.1	144.61	0.59	1.69	0.60	1.66	0		0	.
7	504.1	123.22	0.59	1.70	0.60	1.66	0		0	.
7	505.1	124.52	0.59	1.69	0.60	1.66	0		0	.
7	506.1	153.78	0.60	1.66	0.60	1.66	0		0	.
7	507.1	152.85	0.60	1.65	0.60	1.66	0		0	.
7	508.1	135.43	0.61	1.65	0.60	1.66	0		0	.
7	509.1	155.35	0.58	1.72	0.58	1.72	1	2	0	1.66
7	510.1	136.57	0.61	1.65	0.60	1.66	0		0	.
7	511.1	111.84	0.49	2.02	0.50	1.98	0		1	.
7	512.1	138.27	0.57	1.74	0.58	1.72	0		1	.
7	513.1	171.10	0.55	1.82	0.55	1.82	1	1	0	1.92
7	514.1	174.17	0.54	1.84	0.54	1.84	1	1	0	1.90
7	515.1	397.76	0.53	1.87	0.54	1.84	0		0	.
7	517.1	110.71	0.53	1.87	0.54	1.84	0		1	.
7	518.1	175.24	0.50	1.98	0.50	1.98	1	3	0	1.66
7	519.1	169.67	0.54	1.86	0.54	1.84	0		0	.
7	520.1	315.58	0.53	1.89	0.54	1.84	0		0	.
7	524.1	114.05	0.52	1.93	0.52	1.93	0		1	.
7	525.1	401.53	0.52	1.93	0.52	1.93	1	4	0	1.91
7	530.1	188.96	0.54	1.84	0.54	1.84	1	4	0	1.82
7	531.1	215.75	0.52	1.92	0.52	1.92	1	1	0	1.66
7	532.1	95.29	0.52	1.91	0.52	1.91	1	4	0	1.84
7	533.1	96.63	0.54	1.87	0.52	1.92	0		0	.
7	534.1	163.23	0.55	1.83	0.52	1.92	0		1	.
7	535.1	234.60	0.54	1.86	0.54	1.86	1	0	1	1.84
7	537.1	165.80	0.53	1.90	0.53	1.90	1	0	0	1.86
7	538.1	172.77	0.52	1.91	0.53	1.90	0		0	.
7	539.1	254.05	0.53	1.89	0.54	1.84	0		0	.
7	542.1	188.89	0.52	1.94	0.52	1.93	0		0	.
7	543.1	125.02	0.51	1.95	0.52	1.93	0		0	.
7	544.1	126.33	0.54	1.86	0.52	1.93	0		0	.
7	545.1	126.83	0.52	1.92	0.52	1.93	0		0	.
7	546.1	222.49	0.54	1.85	0.52	1.93	0		0	.
7	552.1	230.63	0.50	2.00	0.50	2.00	1	4	0	1.93
7	553.1	452.62	0.50	2.00	0.50	2.00	0		1	.
7	555.1	217.11	0.53	1.89	0.53	1.89	1	4	0	2.00
7	556.1	274.31	0.47	2.12	0.47	2.12	1	1	0	1.89
7	559.1	268.20	0.58	1.73	0.58	1.73	1	2	0	1.89
7	561.1	364.13	0.44	2.26	0.44	2.26	1	4	0	2.12
7	563.1	207.64	0.46	2.18	0.46	2.18	1	3	0	1.89
7	564.1	191.22	0.43	2.35	0.44	2.27	0		1	.
7	565.1	133.73	0.44	2.27	0.44	2.27	1	3	0	1.89
7	566.1	132.73	0.42	2.37	0.44	2.27	0		0	.
7	567.1	292.79	0.43	2.31	0.43	2.31	1	3	0	1.89
7	569.1	297.36	0.44	2.25	0.44	2.25	1	2	0	2.26
7	571.1	222.72	0.37	2.69	0.37	2.69	1	1	0	2.26
7	572.1	178.74	0.41	2.44	0.41	2.44	1	3	0	2.26
7	573.1	170.87	0.32	3.10	0.32	3.08	0		0	.
7	574.1	180.71	0.32	3.08	0.32	3.08	1	0	0	2.69

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	575.1	0	1	1	0	1	574	0	2.02	2	73.98
7	576.1	1	0	1	0	1	574	0	1.40	1	73.98
7	577.1	1	1	1	0	2	574	0	1.40	1	73.98
7	578.1	1	0	0	0	1	574	0	1.71	1	73.98
7	579.1	1	0	1	0	2	574	0	1.55	2	73.98
7	580.1	1	0	1	0	1	574	0	1.40	1	73.98
7	582.1	0	.	0	0	2	582	0	1.71	0	12.78
7	583.1	0	0	0	0	1	582	0	1.71	1	53.58
7	584.1	0	1	1	0	1	582	0	1.87	2	53.58
7	585.1	1	0	1	0	1	582	0	1.71	1	73.98
7	586.1	1	0	1	0	1	582	0	1.71	2	73.98
7	587.1	1	.	1	0	1	587	0	1.71	1	33.18
7	588.1	0	.	0	0	2	588	0	1.24	2	73.98
7	590.1	0	.	1	0	1	590	1	1.55	2	22.98
7	591.1	0	.	1	0	1	591	0	1.40	1	12.78
7	592.1	0	1	1	1	2	587	0	1.55	2	73.98
7	593.1	1	.	1	0	1	593	0	1.09	1	73.98
7	594.1	0	0	0	0	1	587	0	1.71	2	73.98
7	595.1	1	0	1	0	1	593	0	1.24	1	73.98
7	596.1	0	.	0	0	1	596	0	1.24	2	43.38
7	597.1	1	.	1	0	2	597	0	1.24	1	73.98
7	598.1	0	1	0	0	1	597	0	1.55	1	73.98
7	599.1	1	1	1	0	1	597	0	1.55	1	73.98
7	600.1	1	.	1	0	1	600	0	1.55	2	73.98
7	601.1	1	0	1	0	1	597	0	1.55	1	73.98
7	603.1	0	0	1	0	1	587	0	1.87	1	73.98
7	604.1	1	0	1	0	1	621	1	2.33	2	73.98
7	605.1	0	1	1	0	1	600	0	1.71	0	73.98
7	606.1	1	0	1	0	1	622	1	2.49	1	12.78
7	607.1	0	1	1	0	2	610	0	1.40	1	2.58
7	608.1	1	1	1	0	2	600	0	2.02	1	43.38
7	609.1	0	1	1	0	1	622	1	2.33	1	73.98
7	610.1	1	.	1	0	2	610	0	1.40	1	73.98
7	611.1	1	.	0	0	2	611	0	1.24	1	73.98
7	612.1	0	.	1	0	1	612	1	1.40	2	73.98
7	613.1	0	.	1	0	1	613	1	1.55	2	43.38
7	614.1	1	1	1	0	1	612	1	1.55	2	73.98
7	615.1	1	0	1	0	1	600	0	1.24	1	73.98
7	616.1	1	0	1	0	1	600	0	1.71	1	73.98
7	617.1	0	.	1	0	1	617	1	1.87	0	43.38
7	618.1	1	.	1	0	1	618	1	1.71	0	43.38
7	621.1	1	.	1	0	1	621	1	2.18	2	33.18
7	622.1	1	.	1	0	1	622	1	2.18	1	33.18
7	626.1	1	.	1	0	1	626	1	2.02	2	43.38
7	627.1	1	.	1	0	1	627	1	2.18	0	43.38
7	630.1	1	.	0	0	1	630	1	1.40	1	12.78
7	631.1	0	1	0	0	1	672	1	1.24	1	73.98
7	632.1	1	0	1	0	1	672	1	1.09	1	73.98
7	634.1	0	.	1	0	1	634	1	1.71	1	43.38
7	635.1	1	0	1	0	2	641	0	1.71	1	43.38

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	575.1	174.14	0.32	3.10	0.32	3.08	0		0	.
7	576.1	172.77	0.32	3.10	0.32	3.08	0		0	.
7	577.1	178.18	0.32	3.10	0.32	3.08	0		1	.
7	578.1	176.28	0.33	3.05	0.32	3.08	0		0	.
7	579.1	176.11	0.32	3.09	0.32	3.08	0		0	.
7	580.1	431.83	0.32	3.09	0.32	3.08	0		0	.
7	582.1	223.92	0.32	3.10	0.32	3.10	1	1	0	3.08
7	583.1	225.96	0.32	3.12	0.32	3.10	0		0	.
7	584.1	188.42	0.32	3.13	0.32	3.10	0		0	.
7	585.1	187.85	0.32	3.10	0.32	3.10	0		0	.
7	586.1	272.87	0.33	3.07	0.32	3.10	0		0	.
7	587.1	193.66	0.28	3.56	0.28	3.56	1	1	0	3.59
7	588.1	437.41	0.32	3.11	0.32	3.11	1	2	0	3.10
7	590.1	288.36	0.60	1.66	0.60	1.66	1	2	0	1.89
7	591.1	201.83	0.29	3.40	0.29	3.40	1	3	0	3.10
7	592.1	184.18	0.28	3.60	0.28	3.56	0		1	.
7	593.1	213.98	0.28	3.59	0.28	3.59	1	1	0	3.10
7	594.1	186.62	0.28	3.60	0.28	3.56	0		0	.
7	595.1	250.38	0.27	3.67	0.28	3.59	0		1	.
7	596.1	191.79	0.30	3.33	0.30	3.33	1	2	0	3.56
7	597.1	195.03	0.28	3.59	0.28	3.59	1	1	0	3.59
7	598.1	199.03	0.28	3.61	0.28	3.59	0		1	.
7	599.1	232.23	0.28	3.62	0.28	3.59	0		0	.
7	600.1	197.83	0.26	3.83	0.26	3.83	1	1	0	3.86
7	601.1	670.90	0.28	3.61	0.28	3.59	0		0	.
7	603.1	240.27	0.28	3.62	0.28	3.56	0		0	.
7	604.1	217.32	0.25	3.95	0.26	3.88	0		1	.
7	605.1	341.14	0.26	3.87	0.26	3.83	0		0	.
7	606.1	311.71	0.26	3.91	0.26	3.87	0		1	.
7	607.1	262.63	0.25	3.92	0.26	3.86	0		1	.
7	608.1	241.01	0.26	3.88	0.26	3.83	0		0	.
7	609.1	210.14	0.26	3.92	0.26	3.87	0		0	.
7	610.1	207.07	0.26	3.86	0.26	3.86	1	1	0	3.56
7	611.1	256.86	0.28	3.55	0.28	3.55	1	3	0	3.56
7	612.1	273.34	0.25	4.02	0.25	4.02	1	2	0	3.83
7	613.1	242.54	0.28	3.58	0.28	3.58	1	2	0	3.83
7	614.1	213.01	0.24	4.11	0.25	4.02	0		1	.
7	615.1	215.21	0.26	3.88	0.26	3.83	0		1	.
7	616.1	308.94	0.25	3.94	0.26	3.83	0		0	.
7	617.1	306.67	0.29	3.42	0.29	3.42	1	3	0	3.83
7	618.1	505.24	0.30	3.31	0.30	3.31	1	2	0	3.83
7	621.1	302.00	0.26	3.88	0.26	3.88	1	3	0	3.83
7	622.1	496.47	0.26	3.87	0.26	3.87	1	2	0	3.83
7	626.1	311.14	0.30	3.36	0.30	3.36	1	2	0	3.83
7	627.1	509.04	0.29	3.40	0.29	3.40	1	3	0	3.83
7	630.1	273.81	0.23	4.44	0.23	4.44	1	3	0	3.83
7	631.1	272.34	0.23	4.40	0.26	3.89	0		0	.
7	632.1	818.55	0.24	4.25	0.26	3.89	0		1	.
7	634.1	323.92	0.25	4.06	0.25	4.06	1	3	0	3.83
7	635.1	306.07	0.21	4.73	0.22	4.57	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	636.1	0	.	0	0	3	636	0	1.71	1	73.98
7	637.1	0	0	0	0	1	636	0	1.71	2	73.98
7	638.1	0	.	0	0	3	638	0	1.24	1	2.58
7	639.1	0	.	0	0	.	639	0	0.62	0	73.98
7	640.1	0	.	0	0	3	640	0	1.55	1	22.98
7	641.1	1	.	1	0	2	641	0	1.71	1	33.18
7	642.1	1	.	1	0	3	642	0	0.93	1	22.98
7	643.1	1	.	1	0	.	643	0	0.62	1	33.18
7	645.1	0	.	0	0	1	645	0	0.62	1	2.58
7	646.1	0	.	1	0	1	646	0	0.93	2	2.58
7	647.1	0	.	0	0	.	647	0	0.47	2	63.78
7	648.1	0	.	1	0	2	648	0	0.62	2	53.58
7	649.1	0	.	0	0	.	649	0	0.31	1	53.58
7	650.1	0	.	0	0	2	650	0	0.93	1	2.58
7	651.1	0	.	0	0	.	651	0	0.78	1	33.18
7	656.1	0	.	1	0	1	656	0	0.62	0	2.58
7	657.1	0	.	1	0	.	657	0	0.31	1	53.58
7	659.1	0	.	1	0	.	659	0	0.31	2	63.78
7	661.1	0	.	0	0	.	661	0	0.31	1	53.58
7	662.1	0	0	0	0	1	661	0	0.62	2	53.58
7	663.1	1	.	1	0	.	663	0	0.31	1	63.78
7	664.1	1	.	1	0	.	664	0	0.31	1	73.98
7	672.1	1	.	1	0	2	672	1	1.87	0	33.18
7	674.1	1	1	1	0	2	675	0	1.71	1	43.38
7	675.1	0	.	0	0	.	675	0	0.62	1	43.38
7	677.1	0	.	0	0	1	677	0	1.71	2	12.78
7	678.1	1	.	0	0	2	678	0	1.24	1	2.58
7	679.1	1	1	0	0	1	582	0	1.87	1	73.98
7	680.1	1	1	0	0	1	582	0	1.71	2	73.98
7	681.1	1	.	0	0	.	681	0	0.78	1	73.98
7	427.11	1	.	1	1	.	427	0	0.47	2	2.58
7	430.11	1	.	1	0	1	430	0	0.78	1	2.58
7	431.11	1	.	1	0	1	431	0	1.09	2	2.58
7	433.11	0	.	0	0	2	433	0	1.40	1	2.58
7	438.11	1	.	0	0	.	438	0	0.62	1	2.58
7	443.11	1	1	1	0	1	464	0	1.40	2	22.98
7	444.11	1	.	1	0	1	444	0	0.78	1	22.98
7	446.11	1	1	1	0	1	464	0	1.71	2	2.58
7	448.11	0	.	0	1	2	448	0	1.40	1	2.58
7	451.11	0	0	0	0	2	448	0	1.40	1	2.58
7	452.11	0	.	1	0	.	452	0	0.93	1	2.58
7	454.11	1	.	1	0	3	454	0	1.24	1	12.78
7	457.11	0	.	1	0	1	457	0	1.09	0	22.98
7	464.11	0	.	1	0	1	464	0	1.24	1	2.58
7	465.11	0	1	0	0	1	464	0	1.40	1	22.98
7	470.11	1	.	1	0	1	470	0	0.78	0	22.98
7	484.11	0	.	0	0	2	484	0	0.93	1	2.58
7	485.11	1	.	1	0	1	485	1	1.71	2	22.98
7	488.11	1	.	1	0	2	488	0	1.24	1	2.58
7	489.11	0	.	0	0	1	489	1	1.55	0	22.98

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	636.1	307.37	0.23	4.43	0.23	4.43	1	0	0	4.57
7	637.1	415.95	0.24	4.25	0.23	4.43	0		1	.
7	638.1	460.16	0.27	3.73	0.27	3.73	1	0	0	4.43
7	639.1	430.26	0.83	1.21	0.83	1.21	1	0	0	2.17
7	640.1	343.64	0.48	2.08	0.48	2.08	1	0	0	3.73
7	641.1	422.65	0.22	4.57	0.22	4.57	1	1	0	3.83
7	642.1	594.89	0.46	2.17	0.46	2.17	1	0	0	2.08
7	643.1	883.41	0.66	1.50	0.66	1.50	1	0	0	1.43
7	645.1	595.33	0.64	1.56	0.64	1.56	1	3	0	1.43
7	646.1	651.72	0.70	1.43	0.70	1.43	1	1	0	1.38
7	647.1	697.19	1.05	0.96	1.05	0.96	1	0	0	1.50
7	648.1	694.93	0.97	1.03	0.97	1.03	1	1	0	1.07
7	649.1	102.77	0.94	1.07	0.94	1.07	1	0	0	1.15
7	650.1	531.93	0.87	1.15	0.87	1.15	1	1	0	1.08
7	651.1	933.76	0.73	1.38	0.73	1.38	1	0	0	2.40
7	656.1	770.43	0.92	1.08	0.92	1.08	1	0	0	0.96
7	657.1	1072.34	0.73	1.37	0.73	1.37	1	0	0	1.03
7	659.1	1252.95	1.08	0.93	1.08	0.93	1	0	0	1.37
7	661.1	1010.74	0.67	1.48	0.67	1.48	1	0	0	0.93
7	662.1	1222.05	0.68	1.47	0.67	1.48	0		1	.
7	663.1	1049.52	0.94	1.06	0.94	1.06	1	0	0	1.48
7	664.1	142.65	0.99	1.01	0.99	1.01	1	0	0	1.06
7	672.1	327.06	0.26	3.89	0.26	3.89	1	3	0	3.83
7	674.1	261.23	0.07	15.06	0.07	15.07	0		1	.
7	675.1	268.80	0.07	15.07	0.07	15.07	1	3	0	.
7	677.1	159.49	0.70	1.42	0.70	1.42	1	2	0	1.62
7	678.1	65.83	0.13	7.60	0.13	7.60	1	3	0	.
7	679.1	184.78	0.33	3.07	0.32	3.10	0		1	.
7	680.1	185.42	0.32	3.15	0.32	3.10	0		0	.
7	681.1	383.15	0.42	2.40	0.42	2.40	1	0	0	1.21
7	427.11	106.01	0.70	1.43	0.70	1.43	1	0	0	.
7	430.11	88.82	0.66	1.51	0.66	1.51	1	3	0	1.43
7	431.11	409.47	0.71	1.41	0.71	1.41	1	2	0	1.43
7	433.11	407.20	0.69	1.45	0.69	1.45	1	1	0	1.43
7	438.11	185.79	0.67	1.50	0.67	1.50	1	0	0	1.45
7	443.11	62.99	0.64	1.57	0.60	1.66	0		1	.
7	444.11	202.70	0.60	1.66	0.60	1.66	1	3	0	1.42
7	446.11	422.35	0.66	1.53	0.60	1.66	0		0	.
7	448.11	423.79	0.68	1.46	0.68	1.46	1	1	0	1.66
7	451.11	98.26	0.67	1.48	0.68	1.46	0		1	.
7	452.11	245.41	0.70	1.42	0.70	1.42	1	0	0	1.50
7	454.11	197.53	0.69	1.46	0.69	1.46	1	0	0	1.46
7	457.11	214.35	0.67	1.48	0.67	1.48	1	2	0	1.42
7	464.11	73.67	0.60	1.66	0.60	1.66	1	1	0	1.42
7	465.11	214.15	0.63	1.59	0.60	1.66	0		0	.
7	470.11	592.06	0.71	1.41	0.71	1.41	1	1	0	1.46
7	484.11	115.35	0.70	1.43	0.70	1.43	1	1	0	1.41
7	485.11	156.16	0.75	1.33	0.75	1.33	1	2	0	1.59
7	488.11	110.27	0.67	1.49	0.67	1.49	1	1	0	1.43
7	489.11	131.80	0.66	1.52	0.66	1.52	1	2	0	1.59

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	490.11	1	.	1	0	2	490	0	1.09	0	2.58
7	491.11	0	0	1	0	1	489	1	2.18	2	22.98
7	492.11	0	.	1	0	1	492	0	1.55	0	2.58
7	493.11	0	1	1	0	1	498	1	1.87	1	22.98
7	494.11	1	1	0	0	1	498	1	1.55	1	22.98
7	497.11	1	1	1	0	1	492	0	1.55	1	2.58
7	498.11	0	.	0	1	2	498	1	1.40	1	12.78
7	499.11	1	0	1	0	1	500	0	2.33	2	22.98
7	500.11	1	.	1	0	1	500	0	2.33	1	22.98
7	503.11	1	.	1	0	1	503	0	2.18	1	2.58
7	504.11	0	1	0	0	1	503	0	2.18	2	2.58
7	505.11	0	0	0	0	2	503	0	1.71	1	22.98
7	506.11	0	0	1	0	1	503	0	1.55	0	22.98
7	507.11	1	1	1	0	1	503	0	1.71	1	12.78
7	508.11	0	0	1	0	1	503	0	1.40	2	12.78
7	509.11	1	.	1	0	1	509	0	1.40	2	22.98
7	510.11	0	1	1	0	1	503	0	1.40	2	12.78
7	511.11	1	.	0	0	1	511	0	1.55	0	22.98
7	512.11	1	.	1	0	1	512	0	2.18	2	53.58
7	513.11	1	.	1	0	1	513	0	1.55	2	22.98
7	514.11	1	.	1	0	1	514	0	1.71	2	12.78
7	515.11	1	0	1	0	1	520	0	2.02	1	12.78
7	517.11	1	.	1	1	1	517	0	1.87	1	12.78
7	518.11	1	.	1	0	2	518	0	1.24	2	53.58
7	519.11	0	1	1	1	1	520	0	1.87	1	12.78
7	520.11	1	.	1	0	2	520	0	1.71	1	12.78
7	524.11	0	0	1	0	1	525	0	1.55	1	53.58
7	525.11	0	.	1	0	2	525	0	1.71	1	53.58
7	533.11	0	.	1	0	1	533	0	1.09	1	22.98
7	534.11	0	0	0	0	1	533	0	1.55	0	22.98
7	535.11	1	.	1	0	1	535	0	1.09	1	12.78
7	537.11	0	1	1	0	1	535	0	1.71	1	12.78
7	538.11	0	0	0	0	1	535	0	1.87	1	12.78
7	539.11	1	0	1	0	2	520	0	1.87	1	12.78
7	542.11	1	1	1	0	1	525	0	1.55	1	53.58
7	543.11	1	.	1	0	2	543	0	1.09	1	2.58
7	544.11	1	.	1	0	1	544	0	1.24	2	53.58
7	545.11	1	.	1	0	1	545	0	1.40	2	53.58
7	546.11	0	1	0	0	2	544	0	1.55	0	53.58
7	555.11	1	.	1	0	1	555	0	0.93	1	2.58
7	556.11	1	.	1	0	2	556	0	0.93	1	12.78
7	559.11	1	.	0	0	2	559	0	1.24	2	53.58
7	561.11	1	.	1	0	2	561	0	1.24	1	12.78
7	563.11	0	.	0	0	2	563	0	1.55	1	2.58
7	564.11	1	.	1	0	1	564	0	1.24	1	12.78
7	565.11	1	.	1	0	1	565	0	0.78	1	2.58
7	566.11	1	0	0	0	1	564	0	1.24	2	53.58
7	567.11	1	.	1	0	1	567	0	1.24	1	53.58
7	571.11	1	.	1	0	.	571	0	0.47	1	53.58
7	572.11	0	.	1	0	2	572	0	1.24	1	12.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	490.11	118.58	0.65	1.55	0.65	1.55	1	1	0	1.49
7	491.11	132.73	0.65	1.55	0.66	1.52	0		1	.
7	492.11	112.94	0.63	1.59	0.63	1.59	1	4	0	1.55
7	493.11	111.21	0.57	1.75	0.57	1.75	0		0	.
7	494.11	240.51	0.57	1.76	0.57	1.75	0		1	.
7	497.11	133.66	0.64	1.56	0.63	1.59	0		1	.
7	498.11	122.62	0.57	1.75	0.57	1.75	1	3	0	1.59
7	499.11	116.98	0.66	1.52	0.64	1.56	0		1	.
7	500.11	162.56	0.64	1.56	0.64	1.56	1	1	0	1.59
7	503.11	144.61	0.61	1.64	0.61	1.64	1	4	0	1.56
7	504.11	123.22	0.64	1.57	0.61	1.64	0		1	.
7	505.11	124.52	0.63	1.58	0.61	1.64	0		0	.
7	506.11	153.78	0.63	1.58	0.61	1.64	0		0	.
7	507.11	152.85	0.64	1.57	0.61	1.64	0		0	.
7	508.11	135.43	0.63	1.58	0.61	1.64	0		0	.
7	509.11	155.35	0.71	1.40	0.71	1.40	1	3	0	1.46
7	510.11	136.57	0.64	1.56	0.61	1.64	0		0	.
7	511.11	111.84	0.76	1.32	0.76	1.32	1	2	0	1.46
7	512.11	138.27	0.75	1.33	0.75	1.33	1	1	0	1.46
7	513.11	171.10	0.76	1.32	0.76	1.32	1	2	0	1.53
7	514.11	174.17	0.60	1.66	0.60	1.66	1	2	0	1.53
7	515.11	397.76	0.55	1.81	0.57	1.76	0		0	.
7	517.11	110.71	0.56	1.79	0.56	1.79	1	3	0	1.53
7	518.11	175.24	0.68	1.46	0.68	1.46	1	1	0	1.64
7	519.11	169.67	0.55	1.80	0.57	1.76	0		0	.
7	520.11	315.58	0.57	1.76	0.57	1.76	1	1	0	1.53
7	524.11	114.05	0.53	1.88	0.52	1.91	0		1	.
7	525.11	401.53	0.52	1.91	0.52	1.91	1	4	0	1.76
7	533.11	96.63	0.65	1.53	0.65	1.53	1	4	0	1.33
7	534.11	163.23	0.68	1.47	0.65	1.53	0		1	.
7	535.11	234.60	0.59	1.70	0.59	1.70	1	3	0	1.53
7	537.11	165.80	0.59	1.68	0.59	1.70	0		1	.
7	538.11	172.77	0.59	1.69	0.59	1.70	0		0	.
7	539.11	254.05	0.57	1.77	0.57	1.76	0		1	.
7	542.11	188.89	0.53	1.90	0.52	1.91	0		0	.
7	543.11	125.02	0.59	1.68	0.59	1.68	1	1	0	1.91
7	544.11	126.33	0.62	1.61	0.62	1.61	1	1	0	1.60
7	545.11	126.83	0.62	1.60	0.62	1.60	1	1	0	1.68
7	546.11	222.49	0.63	1.59	0.62	1.61	0		1	.
7	555.11	217.11	0.43	2.33	0.43	2.33	1	3	0	1.61
7	556.11	274.31	0.53	1.87	0.53	1.87	1	3	0	1.94
7	559.11	268.20	0.46	2.18	0.46	2.18	1	3	0	1.61
7	561.11	364.13	0.59	1.69	0.59	1.69	1	1	0	1.94
7	563.11	207.64	0.52	1.94	0.52	1.94	1	1	0	1.98
7	564.11	191.22	0.55	1.82	0.55	1.82	1	2	0	1.61
7	565.11	133.73	0.40	2.48	0.40	2.48	1	3	0	1.61
7	566.11	132.73	0.53	1.89	0.55	1.82	0		1	.
7	567.11	292.79	0.50	1.98	0.50	1.98	1	1	0	1.61
7	571.11	222.72	0.63	1.58	0.63	1.58	1	0	0	1.68
7	572.11	178.74	0.60	1.68	0.60	1.68	1	1	0	1.69

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	573.11	1	0	0	0	1	574	0	1.40	2	53.58
7	574.11	0	.	1	0	2	574	0	0.78	1	53.58
7	575.11	0	1	1	0	2	574	0	1.71	2	53.58
7	576.11	1	0	1	0	1	574	0	1.09	1	53.58
7	577.11	1	1	1	0	2	574	0	1.09	1	53.58
7	578.11	1	0	0	0	1	574	0	1.40	1	53.58
7	579.11	1	0	1	0	2	574	0	1.24	2	53.58
7	580.11	1	0	1	0	1	574	0	1.24	1	53.58
7	583.11	0	0	0	0	1	585	0	1.40	1	33.18
7	584.11	0	1	1	0	1	585	0	1.55	2	33.18
7	585.11	1	.	1	0	1	585	0	0.93	1	53.58
7	586.11	1	0	1	0	1	585	0	1.24	2	53.58
7	587.11	1	.	1	0	2	587	0	1.24	1	12.78
7	588.11	0	.	0	0	1	588	0	0.93	2	53.58
7	590.11	0	.	1	0	1	590	0	1.40	0	2.58
7	592.11	0	1	1	1	2	587	0	1.24	2	53.58
7	593.11	1	.	1	0	.	593	0	0.47	1	53.58
7	594.11	0	.	0	0	2	594	0	1.40	2	53.58
7	595.11	1	.	1	0	1	595	0	0.78	1	53.58
7	596.11	0	.	0	0	1	596	0	1.09	2	22.98
7	597.11	1	.	1	0	.	597	0	0.93	1	53.58
7	598.11	0	1	0	0	1	597	0	1.09	1	53.58
7	599.11	1	1	1	0	1	597	0	1.09	1	53.58
7	600.11	1	.	1	0	1	600	0	1.55	2	53.58
7	601.11	1	0	1	0	1	597	0	1.24	1	53.58
7	603.11	0	0	1	0	1	587	0	1.55	1	53.58
7	604.11	1	.	1	0	1	604	0	1.40	2	53.58
7	605.11	0	1	1	0	1	616	0	1.40	1	53.58
7	608.11	1	.	1	0	2	608	0	1.55	1	22.98
7	609.11	0	.	1	0	1	609	0	1.09	0	53.58
7	610.11	1	.	1	0	2	610	0	1.09	1	53.58
7	611.11	1	.	0	0	.	611	0	0.78	1	53.58
7	612.11	0	.	1	0	1	612	0	1.09	2	53.58
7	613.11	0	.	1	0	1	613	0	0.78	0	22.98
7	614.11	1	.	1	0	2	614	0	1.09	0	53.58
7	615.11	1	.	1	0	1	615	0	1.09	1	53.58
7	616.11	1	.	1	0	2	616	0	1.40	1	53.58
7	617.11	0	0	1	0	1	632	0	1.55	2	22.98
7	618.11	1	1	1	0	1	632	0	1.24	1	22.98
7	621.11	1	.	1	0	1	621	0	1.24	2	12.78
7	622.11	1	0	1	0	1	621	0	1.24	1	12.78
7	626.11	1	.	1	0	1	626	0	1.71	2	22.98
7	627.11	1	0	1	0	1	626	0	1.55	1	22.98
7	631.11	0	1	0	0	1	632	0	1.24	1	53.58
7	632.11	1	.	1	0	2	632	0	1.09	1	53.58
7	634.11	0	.	1	0	3	634	0	1.09	1	22.98
7	635.11	1	.	1	0	2	635	0	1.09	1	22.98
7	636.11	0	.	0	0	3	636	0	1.09	1	53.58
7	637.11	0	0	0	0	2	636	0	1.09	1	53.58
7	639.11	0	.	0	0	.	639	0	0.47	1	53.58

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	573.11	170.87	0.63	1.59	0.65	1.55	0		0	.
7	574.11	180.71	0.65	1.55	0.65	1.55	1	1	0	1.58
7	575.11	174.14	0.63	1.59	0.65	1.55	0		0	.
7	576.11	172.77	0.64	1.55	0.65	1.55	0		0	.
7	577.11	178.18	0.64	1.57	0.65	1.55	0		1	.
7	578.11	176.28	0.64	1.57	0.65	1.55	0		0	.
7	579.11	176.11	0.63	1.60	0.65	1.55	0		0	.
7	580.11	431.83	0.62	1.60	0.65	1.55	0		0	.
7	583.11	225.96	0.61	1.63	0.63	1.60	0		0	.
7	584.11	188.42	0.62	1.62	0.63	1.60	0		0	.
7	585.11	187.85	0.63	1.60	0.63	1.60	1	1	0	1.66
7	586.11	272.87	0.61	1.64	0.63	1.60	0		1	.
7	587.11	193.66	0.55	1.80	0.55	1.80	1	0	0	1.78
7	588.11	437.41	0.73	1.37	0.73	1.37	1	2	0	1.60
7	590.11	288.36	0.73	1.37	0.73	1.37	1	2	0	1.94
7	592.11	184.18	0.57	1.77	0.55	1.80	0		1	.
7	593.11	213.98	0.56	1.79	0.56	1.79	1	3	0	1.60
7	594.11	186.62	0.59	1.71	0.59	1.71	1	1	0	1.80
7	595.11	250.38	0.55	1.81	0.55	1.81	1	1	0	1.60
7	596.11	191.79	0.62	1.61	0.62	1.61	1	2	0	1.84
7	597.11	195.03	0.56	1.78	0.56	1.78	1	0	0	1.81
7	598.11	199.03	0.57	1.77	0.56	1.78	0		1	.
7	599.11	232.23	0.57	1.77	0.56	1.78	0		0	.
7	600.11	197.83	0.56	1.80	0.56	1.80	1	2	0	1.84
7	601.11	670.90	0.56	1.79	0.56	1.78	0		0	.
7	603.11	240.27	0.57	1.76	0.55	1.80	0		0	.
7	604.11	217.32	0.57	1.74	0.57	1.74	1	2	0	1.90
7	605.11	341.14	0.49	2.03	0.50	2.02	0		1	.
7	608.11	241.01	0.50	2.00	0.50	2.00	1	1	0	2.02
7	609.11	210.14	0.53	1.88	0.53	1.88	1	3	0	1.90
7	610.11	207.07	0.52	1.92	0.52	1.92	1	3	0	1.84
7	611.11	256.86	0.54	1.84	0.54	1.84	1	0	0	1.71
7	612.11	273.34	0.60	1.66	0.60	1.66	1	2	0	1.74
7	613.11	242.54	0.57	1.74	0.57	1.74	1	1	0	1.79
7	614.11	213.01	0.56	1.79	0.56	1.79	1	3	0	1.74
7	615.11	215.21	0.48	2.06	0.48	2.06	1	3	0	1.84
7	616.11	308.94	0.50	2.02	0.50	2.02	1	1	0	1.84
7	617.11	306.67	0.48	2.09	0.46	2.17	0		0	.
7	618.11	505.24	0.47	2.14	0.46	2.17	0		0	.
7	621.11	302.00	0.53	1.90	0.53	1.90	1	1	0	2.00
7	622.11	496.47	0.53	1.90	0.53	1.90	0		1	.
7	626.11	311.14	0.49	2.06	0.49	2.06	1	1	0	2.17
7	627.11	509.04	0.50	2.02	0.49	2.06	0		1	.
7	631.11	272.34	0.46	2.15	0.46	2.17	0		1	.
7	632.11	818.55	0.46	2.17	0.46	2.17	1	1	0	2.25
7	634.11	323.92	0.56	1.79	0.56	1.79	1	0	0	1.90
7	635.11	306.07	0.51	1.95	0.51	1.95	1	1	0	2.04
7	636.11	307.37	0.48	2.08	0.48	2.08	1	0	0	1.95
7	637.11	415.95	0.44	2.26	0.48	2.08	0		1	.
7	639.11	430.26	0.73	1.36	0.73	1.36	1	2	0	2.08

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	640.11	0	.	0	0	.	640	0	0.62	2	2.58
7	641.11	1	.	1	0	2	641	0	1.55	1	12.78
7	642.11	1	.	1	0	3	642	0	0.47	1	2.58
7	643.11	1	.	1	0	.	643	0	0.47	1	12.78
7	647.11	0	.	0	0	.	647	0	0.47	2	43.38
7	648.11	0	.	1	0	2	648	0	0.62	2	33.18
7	649.11	0	.	0	0	.	649	0	0.31	2	33.18
7	651.11	0	.	0	0	.	651	0	0.47	1	12.78
7	657.11	0	.	1	0	.	657	0	0.31	1	33.18
7	659.11	0	.	1	0	.	659	0	0.31	1	43.38
7	661.11	0	.	0	0	.	661	0	0.31	1	33.18
7	662.11	0	0	0	0	1	661	0	0.62	2	33.18
7	663.11	1	.	1	0	.	663	0	0.47	0	43.38
7	664.11	1	.	1	0	1	664	0	0.31	1	53.58
7	672.11	1	.	1	0	2	672	0	1.24	1	12.78
7	674.11	1	.	1	0	1	674	0	0.93	1	22.98
7	675.11	0	.	0	0	.	675	0	0.62	1	22.98
7	679.11	1	.	0	0	2	679	0	1.40	1	53.58
7	680.11	1	.	0	0	1	680	0	1.40	2	53.58
7	681.11	1	.	0	0	.	681	0	0.62	1	53.58
7	443.12	1	.	1	0	2	443	0	1.24	0	2.58
7	444.12	1	.	1	0	1	444	0	0.47	1	2.58
7	457.12	0	1	1	0	1	444	0	0.93	0	2.58
7	465.12	0	.	0	0	1	465	0	0.78	0	2.58
7	470.12	1	.	1	0	.	470	0	0.31	2	2.58
7	485.12	1	.	1	0	1	485	0	1.09	2	2.58
7	489.12	0	.	0	0	1	489	0	0.78	1	2.58
7	491.12	0	.	1	0	2	491	0	1.40	2	2.58
7	493.12	0	.	1	0	1	493	0	1.24	2	2.58
7	494.12	1	.	0	0	1	494	0	1.09	1	2.58
7	499.12	1	.	1	0	1	499	0	1.09	1	2.58
7	500.12	1	.	1	0	2	500	0	1.24	1	2.58
7	505.12	0	.	0	0	1	505	0	0.93	1	2.58
7	506.12	0	0	1	0	1	505	0	1.09	1	2.58
7	509.12	1	.	1	0	1	509	0	0.62	0	2.58
7	511.12	1	0	0	0	1	509	0	1.09	2	2.58
7	512.12	1	0	1	0	1	509	0	1.71	0	33.18
7	513.12	1	.	1	0	1	513	0	1.71	2	2.58
7	518.12	1	.	1	0	.	518	0	0.47	2	33.18
7	524.12	0	0	1	0	1	525	0	0.93	0	33.18
7	525.12	0	.	1	0	2	525	0	1.09	1	33.18
7	533.12	0	.	1	0	1	533	0	0.62	0	2.58
7	534.12	0	0	0	0	1	533	0	1.09	1	2.58
7	542.12	1	1	1	0	1	525	0	0.93	1	33.18
7	544.12	1	.	1	0	1	544	0	0.93	1	33.18
7	545.12	1	.	1	0	1	545	0	0.93	2	33.18
7	546.12	0	.	0	0	2	546	0	1.24	1	33.18
7	559.12	1	.	0	0	.	559	0	0.47	0	33.18
7	566.12	1	.	0	0	1	566	0	0.78	2	33.18
7	567.12	1	0	1	0	1	566	0	0.78	1	33.18

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	640.11	343.64	0.88	1.14	0.88	1.14	1	2	0	2.08
7	641.11	422.65	0.49	2.04	0.49	2.04	1	1	0	2.06
7	642.11	594.89	0.63	1.58	0.63	1.58	1	3	0	2.08
7	643.11	883.41	0.74	1.35	0.74	1.35	1	0	0	1.09
7	647.11	697.19	0.98	1.02	0.98	1.02	1	0	0	1.35
7	648.11	694.93	0.97	1.03	0.97	1.03	1	0	0	0.96
7	649.11	102.77	1.04	0.96	1.04	0.96	1	0	0	1.02
7	651.11	933.76	0.92	1.09	0.92	1.09	1	0	0	2.08
7	657.11	1072.34	0.70	1.42	0.70	1.42	1	0	0	1.03
7	659.11	1252.95	1.06	0.94	1.06	0.94	1	0	0	1.42
7	661.11	1010.74	0.65	1.55	0.65	1.55	1	0	0	0.94
7	662.11	1222.05	0.68	1.47	0.65	1.55	0		1	.
7	663.11	1049.52	0.96	1.04	0.96	1.04	1	0	0	1.55
7	664.11	142.65	0.39	2.57	0.39	2.57	1	0	0	1.04
7	672.11	327.06	0.44	2.25	0.44	2.25	1	1	0	2.40
7	674.11	261.23	0.42	2.40	0.42	2.40	1	1	0	1.74
7	675.11	268.80	0.40	2.50	0.40	2.50	1	3	0	1.74
7	679.11	184.78	0.60	1.66	0.60	1.66	1	0	0	1.55
7	680.11	185.42	0.63	1.60	0.63	1.60	1	1	0	1.60
7	681.11	383.15	0.39	2.55	0.39	2.55	1	3	0	2.08
7	443.12	62.99	0.58	1.71	0.58	1.71	1	4	0	1.78
7	444.12	202.70	0.56	1.78	0.56	1.78	1	1	0	.
7	457.12	214.35	0.57	1.76	0.56	1.78	0		1	.
7	465.12	214.15	0.66	1.53	0.66	1.53	1	2	0	1.71
7	470.12	592.06	0.77	1.30	0.77	1.30	1	0	0	1.71
7	485.12	156.16	0.77	1.30	0.77	1.30	1	1	0	1.34
7	489.12	131.80	0.63	1.60	0.63	1.60	1	3	0	1.30
7	491.12	132.73	0.81	1.24	0.81	1.24	1	2	0	1.30
7	493.12	111.21	0.74	1.34	0.74	1.34	1	1	0	1.38
7	494.12	240.51	0.73	1.38	0.73	1.38	1	1	0	1.30
7	499.12	116.98	0.84	1.20	0.84	1.20	1	1	0	1.30
7	500.12	162.56	0.73	1.38	0.73	1.38	1	3	0	1.30
7	505.12	124.52	0.77	1.30	0.77	1.30	1	4	0	1.20
7	506.12	153.78	0.76	1.31	0.77	1.30	0		1	.
7	509.12	155.35	0.78	1.28	0.78	1.28	1	0	0	1.20
7	511.12	111.84	0.78	1.29	0.78	1.28	0		1	.
7	512.12	138.27	0.76	1.32	0.78	1.28	0		0	.
7	513.12	171.10	0.64	1.56	0.64	1.56	1	1	0	1.28
7	518.12	175.24	0.84	1.20	0.84	1.20	1	0	0	1.30
7	524.12	114.05	0.56	1.77	0.57	1.75	0		1	.
7	525.12	401.53	0.57	1.75	0.57	1.75	1	1	0	1.56
7	533.12	96.63	0.30	3.33	0.30	3.33	1	3	0	.
7	534.12	163.23	0.30	3.39	0.30	3.33	0		1	.
7	542.12	188.89	0.57	1.74	0.57	1.75	0		0	.
7	544.12	126.33	0.57	1.74	0.57	1.74	1	3	0	1.75
7	545.12	126.83	0.60	1.66	0.60	1.66	1	2	0	1.75
7	546.12	222.49	0.59	1.70	0.59	1.70	1	1	0	1.75
7	559.12	268.20	0.55	1.83	0.55	1.83	1	0	0	1.70
7	566.12	132.73	0.55	1.81	0.55	1.81	1	1	0	1.83
7	567.12	292.79	0.55	1.81	0.55	1.81	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	571.12	1	.	1	0	.	571	0	0.31	1	33.18
7	573.12	1	0	0	0	1	574	0	1.40	2	33.18
7	574.12	0	.	1	0	2	574	0	0.62	1	33.18
7	575.12	0	1	1	0	1	574	0	1.55	2	33.18
7	576.12	1	0	1	0	1	574	0	1.09	0	33.18
7	577.12	1	1	1	0	2	574	0	0.93	1	33.18
7	578.12	1	1	0	0	1	574	0	1.40	1	33.18
7	579.12	1	0	1	0	2	574	0	1.40	2	33.18
7	580.12	1	0	1	0	1	574	0	1.24	1	33.18
7	583.12	0	0	0	0	1	584	0	1.09	0	12.78
7	584.12	0	.	1	0	1	584	0	1.40	2	12.78
7	585.12	1	0	1	0	1	586	0	0.62	1	33.18
7	586.12	1	.	1	0	3	586	0	0.62	2	33.18
7	588.12	0	.	0	0	1	588	0	1.09	2	33.18
7	592.12	0	.	1	1	2	592	0	1.09	2	33.18
7	593.12	1	.	1	0	1	593	0	0.62	1	33.18
7	594.12	0	.	0	0	1	594	0	0.93	2	33.18
7	595.12	1	.	1	0	1	595	0	0.93	1	33.18
7	596.12	0	1	0	0	1	615	0	1.09	2	2.58
7	597.12	1	.	1	0	.	597	0	0.93	1	33.18
7	598.12	0	.	0	0	2	598	0	1.09	1	33.18
7	599.12	1	.	1	0	1	599	0	1.09	2	33.18
7	600.12	1	1	1	0	1	615	0	1.40	2	33.18
7	601.12	1	.	1	0	1	601	0	1.09	1	33.18
7	603.12	0	0	1	0	1	592	0	1.24	1	33.18
7	604.12	1	.	1	0	2	604	0	1.09	2	33.18
7	605.12	0	1	1	0	1	615	0	1.24	1	33.18
7	608.12	1	.	1	0	2	608	0	1.09	1	2.58
7	609.12	0	.	1	0	1	609	0	0.93	2	33.18
7	610.12	1	0	1	0	2	611	0	0.62	1	33.18
7	611.12	1	.	0	0	.	611	0	0.78	1	33.18
7	612.12	0	1	1	0	1	614	0	1.55	2	33.18
7	613.12	0	.	1	0	2	613	0	0.93	1	2.58
7	614.12	1	.	1	0	1	614	0	1.40	1	33.18
7	615.12	1	.	1	0	2	615	0	1.24	1	33.18
7	616.12	1	1	1	0	2	615	0	1.40	1	33.18
7	617.12	0	.	1	0	1	617	0	0.93	2	2.58
7	618.12	1	.	1	0	2	618	0	0.62	1	2.58
7	626.12	1	0	1	0	1	627	0	1.09	2	2.58
7	627.12	1	.	1	0	1	627	0	0.78	1	2.58
7	631.12	0	.	0	0	1	631	0	0.78	1	33.18
7	632.12	1	.	1	0	.	632	0	0.47	1	33.18
7	634.12	0	.	1	0	2	634	0	0.93	1	2.58
7	635.12	1	.	1	0	.	635	0	0.31	1	2.58
7	636.12	0	.	0	0	.	636	0	0.31	2	33.18
7	637.12	0	0	0	0	2	636	0	0.62	1	33.18
7	639.12	0	.	0	0	.	639	0	0.31	1	33.18
7	647.12	0	.	0	0	.	647	0	0.31	2	22.98
7	648.12	0	0	1	0	1	649	0	0.62	2	12.78
7	649.12	0	.	0	0	.	649	0	0.31	1	12.78

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	571.12	222.72	0.66	1.52	0.66	1.52	1	0	0	1.81
7	573.12	170.87	0.63	1.58	0.65	1.55	0		0	.
7	574.12	180.71	0.65	1.55	0.65	1.55	1	0	0	1.52
7	575.12	174.14	0.63	1.59	0.65	1.55	0		0	.
7	576.12	172.77	0.64	1.57	0.65	1.55	0		0	.
7	577.12	178.18	0.64	1.56	0.65	1.55	0		1	.
7	578.12	176.28	0.62	1.60	0.65	1.55	0		0	.
7	579.12	176.11	0.63	1.58	0.65	1.55	0		0	.
7	580.12	431.83	0.63	1.59	0.65	1.55	0		0	.
7	583.12	225.96	0.72	1.39	0.77	1.29	0		1	.
7	584.12	188.42	0.77	1.29	0.77	1.29	1	1	0	1.45
7	585.12	187.85	0.70	1.43	0.69	1.45	0		1	.
7	586.12	272.87	0.69	1.45	0.69	1.45	1	0	0	1.59
7	588.12	437.41	0.61	1.63	0.61	1.63	1	2	0	1.29
7	592.12	184.18	0.55	1.81	0.55	1.81	1	1	0	1.72
7	593.12	213.98	0.54	1.84	0.54	1.84	1	3	0	1.29
7	594.12	186.62	0.63	1.57	0.63	1.57	1	2	0	1.81
7	595.12	250.38	0.58	1.73	0.58	1.73	1	3	0	1.29
7	596.12	191.79	0.53	1.88	0.52	1.94	0		1	.
7	597.12	195.03	0.58	1.73	0.58	1.73	1	0	0	1.29
7	598.12	199.03	0.58	1.72	0.58	1.72	1	1	0	1.73
7	599.12	232.23	0.59	1.69	0.59	1.69	1	2	0	1.72
7	600.12	197.83	0.53	1.88	0.52	1.94	0		0	.
7	601.12	670.90	0.56	1.78	0.56	1.78	1	3	0	1.72
7	603.12	240.27	0.55	1.82	0.55	1.81	0		1	.
7	604.12	217.32	0.64	1.57	0.64	1.57	1	2	0	1.81
7	605.12	341.14	0.53	1.90	0.52	1.94	0		0	.
7	608.12	241.01	0.55	1.81	0.55	1.81	1	1	0	1.94
7	609.12	210.14	0.65	1.54	0.65	1.54	1	2	0	1.81
7	610.12	207.07	0.51	1.94	0.52	1.94	0		1	.
7	611.12	256.86	0.52	1.94	0.52	1.94	1	3	0	1.81
7	612.12	273.34	0.45	2.22	0.45	2.24	0		1	.
7	613.12	242.54	0.43	2.31	0.43	2.31	1	1	0	1.81
7	614.12	213.01	0.45	2.24	0.45	2.24	1	1	0	2.30
7	615.12	215.21	0.52	1.94	0.52	1.94	1	1	0	1.81
7	616.12	308.94	0.52	1.92	0.52	1.94	0		0	.
7	617.12	306.67	0.73	1.36	0.73	1.36	1	2	0	1.83
7	618.12	505.24	0.64	1.56	0.64	1.56	1	3	0	1.83
7	626.12	311.14	0.72	1.40	0.68	1.47	0		1	.
7	627.12	509.04	0.68	1.47	0.68	1.47	1	0	0	1.83
7	631.12	272.34	0.55	1.83	0.55	1.83	1	1	0	1.81
7	632.12	818.55	0.55	1.81	0.55	1.81	1	0	0	2.24
7	634.12	323.92	0.50	2.02	0.50	2.02	1	3	0	1.81
7	635.12	306.07	0.80	1.25	0.80	1.25	1	0	0	1.47
7	636.12	307.37	0.84	1.19	0.84	1.19	1	0	0	1.25
7	637.12	415.95	0.84	1.19	0.84	1.19	0		1	.
7	639.12	430.26	1.08	0.93	1.08	0.93	1	0	0	2.35
7	647.12	697.19	0.94	1.07	0.94	1.07	1	0	0	0.93
7	648.12	694.93	0.86	1.16	0.86	1.16	0		1	.
7	649.12	102.77	0.86	1.16	0.86	1.16	1	0	0	1.07

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	657.12	0	.	1	0	.	657	0	0.31	1	12.78
7	659.12	0	.	1	0	.	659	0	0.31	2	22.98
7	661.12	0	.	0	0	.	661	0	0.31	1	12.78
7	662.12	0	0	0	0	1	661	0	0.62	2	12.78
7	663.12	1	.	1	0	.	663	0	0.47	1	22.98
7	674.12	1	.	1	0	1	674	0	0.93	1	2.58
7	675.12	0	.	0	0	.	675	0	0.62	1	2.58
7	679.12	1	.	0	0	3	679	0	1.24	1	33.18
7	680.12	1	.	0	0	1	680	0	1.09	0	33.18
7	681.12	1	.	0	0	.	681	0	0.31	1	33.18
7	512.13	1	.	1	0	1	512	0	0.98	1	12.45
7	518.13	1	.	1	0	.	518	0	0.33	2	12.45
7	524.13	0	0	1	0	1	525	0	0.81	2	12.45
7	525.13	0	.	1	0	.	525	0	0.65	1	12.45
7	542.13	1	.	1	0	2	542	0	0.65	1	12.45
7	544.13	1	.	1	0	1	544	0	0.49	1	12.45
7	545.13	1	0	1	0	1	544	0	0.49	2	12.45
7	546.13	0	.	0	0	3	546	0	0.98	1	12.45
7	559.13	1	.	0	0	.	559	0	0.98	1	12.45
7	566.13	1	.	0	0	1	566	0	0.81	2	12.45
7	567.13	1	0	1	0	1	566	0	0.81	1	12.45
7	571.13	1	.	1	0	.	571	0	0.33	1	12.45
7	573.13	1	.	0	0	2	573	0	1.47	2	12.45
7	574.13	0	.	1	0	2	574	0	0.65	1	12.45
7	575.13	0	.	1	0	1	575	0	1.63	2	12.45
7	576.13	1	0	1	0	1	577	0	1.14	0	12.45
7	577.13	1	.	1	0	2	577	0	0.81	1	12.45
7	578.13	1	.	0	0	1	578	0	1.47	1	12.45
7	579.13	1	.	1	0	2	579	0	1.47	2	12.45
7	580.13	1	0	1	0	1	579	0	1.14	1	12.45
7	585.13	1	.	1	0	1	585	0	1.14	2	12.45
7	586.13	1	.	1	0	1	586	0	0.98	2	12.45
7	588.13	0	.	0	0	1	588	0	1.14	1	12.45
7	592.13	0	.	1	1	3	592	0	1.30	2	12.45
7	593.13	1	.	1	0	1	593	0	0.81	1	12.45
7	594.13	0	.	0	0	1	594	0	0.98	2	12.45
7	595.13	1	.	1	0	1	595	0	1.30	1	12.45
7	597.13	1	.	1	0	3	597	0	1.14	1	12.45
7	598.13	0	.	0	0	2	598	0	1.14	1	12.45
7	599.13	1	0	1	0	1	601	0	1.14	2	12.45
7	600.13	1	.	1	0	1	600	0	0.81	2	12.45
7	601.13	1	.	1	0	2	601	0	0.98	1	12.45
7	603.13	0	0	1	0	1	592	0	1.14	1	12.45
7	604.13	1	.	1	0	1	604	0	0.98	1	12.45
7	605.13	0	1	1	0	1	616	0	1.30	0	12.45
7	609.13	0	.	1	0	1	609	0	1.14	2	12.45
7	610.13	1	.	1	0	2	610	0	0.65	1	12.45
7	611.13	1	.	0	0	.	611	0	0.81	1	12.45
7	612.13	0	.	1	0	1	612	0	1.14	2	12.45
7	614.13	1	0	1	0	1	604	0	1.30	1	12.45

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	657.12	1072.34	0.65	1.54	0.65	1.54	1	0	0	1.16
7	659.12	1252.95	1.03	0.97	1.03	0.97	1	0	0	1.54
7	661.12	1010.74	0.26	3.83	0.26	3.83	1	0	0	.
7	662.12	1222.05	0.26	3.92	0.26	3.83	0		1	.
7	663.12	1049.52	0.97	1.03	0.97	1.03	1	0	0	0.97
7	674.12	261.23	0.44	2.30	0.44	2.30	1	1	0	2.31
7	675.12	268.80	0.42	2.40	0.42	2.40	1	3	0	1.81
7	679.12	184.78	0.63	1.59	0.63	1.59	1	0	0	1.55
7	680.12	185.42	0.75	1.33	0.75	1.33	1	2	0	1.29
7	681.12	383.15	0.43	2.35	0.43	2.35	1	0	0	1.19
7	512.13	138.27	0.79	1.26	0.79	1.26	1	4	0	1.18
7	518.13	175.24	0.85	1.18	0.85	1.18	1	0	0	.
7	524.13	114.05	0.68	1.48	0.68	1.48	0		0	.
7	525.13	401.53	0.68	1.48	0.68	1.48	1	0	0	1.26
7	542.13	188.89	0.69	1.45	0.69	1.45	1	1	0	1.48
7	544.13	126.33	0.62	1.62	0.62	1.62	1	0	0	1.45
7	545.13	126.83	0.62	1.61	0.62	1.62	0		1	.
7	546.13	222.49	0.60	1.68	0.60	1.68	1	0	0	1.62
7	559.13	268.20	0.59	1.68	0.59	1.68	1	0	0	1.68
7	566.13	132.73	0.58	1.73	0.58	1.73	1	0	0	1.68
7	567.13	292.79	0.56	1.79	0.58	1.73	0		1	.
7	571.13	222.72	0.63	1.59	0.63	1.59	1	0	0	1.73
7	573.13	170.87	0.67	1.49	0.67	1.49	1	2	0	1.50
7	574.13	180.71	0.64	1.57	0.64	1.57	1	1	0	1.59
7	575.13	174.14	0.67	1.49	0.67	1.49	1	1	0	1.50
7	576.13	172.77	0.65	1.55	0.65	1.54	0		1	.
7	577.13	178.18	0.65	1.54	0.65	1.54	1	1	0	1.57
7	578.13	176.28	0.64	1.57	0.64	1.57	1	3	0	1.50
7	579.13	176.11	0.67	1.50	0.67	1.50	1	1	0	1.54
7	580.13	431.83	0.67	1.50	0.67	1.50	0		1	.
7	585.13	187.85	0.69	1.45	0.69	1.45	1	2	0	1.47
7	586.13	272.87	0.67	1.49	0.67	1.49	1	2	0	1.47
7	588.13	437.41	0.59	1.70	0.59	1.70	1	2	0	1.93
7	592.13	184.18	0.53	1.89	0.53	1.89	1	0	0	1.85
7	593.13	213.98	0.53	1.90	0.53	1.90	1	4	0	1.47
7	594.13	186.62	0.57	1.74	0.57	1.74	1	1	0	1.84
7	595.13	250.38	0.52	1.93	0.52	1.93	1	1	0	1.90
7	597.13	195.03	0.51	1.95	0.51	1.95	1	3	0	1.93
7	598.13	199.03	0.54	1.86	0.54	1.86	1	0	0	1.93
7	599.13	232.23	0.54	1.85	0.54	1.85	0		1	.
7	600.13	197.83	0.76	1.31	0.76	1.31	1	0	0	1.87
7	601.13	670.90	0.54	1.85	0.54	1.85	1	1	0	1.86
7	603.13	240.27	0.53	1.88	0.53	1.89	0		1	.
7	604.13	217.32	0.55	1.80	0.55	1.80	1	4	0	1.73
7	605.13	341.14	0.53	1.89	0.53	1.87	0		1	.
7	609.13	210.14	0.58	1.73	0.58	1.73	1	0	0	1.31
7	610.13	207.07	0.54	1.84	0.54	1.84	1	1	0	1.86
7	611.13	256.86	0.54	1.86	0.54	1.86	1	0	0	1.89
7	612.13	273.34	0.78	1.28	0.78	1.28	1	1	0	1.80
7	614.13	213.01	0.56	1.79	0.55	1.80	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
7	615.13	1	1	1	0	1	594	0	1.30	1	12.45
7	616.13	1	.	1	0	1	616	0	1.47	1	12.45
7	631.13	0	.	0	0	2	631	0	0.65	1	12.45
7	632.13	1	.	1	0	.	632	0	0.33	1	12.45
7	636.13	0	.	0	0	.	636	0	0.33	2	12.45
7	637.13	0	0	0	0	2	636	0	0.65	0	12.45
7	639.13	0	.	0	0	.	639	0	0.33	1	12.45
7	647.13	0	.	0	0	.	647	0	0.33	2	2.25
7	659.13	0	.	1	0	.	659	0	0.33	0	2.25
7	663.13	1	.	1	0	.	663	0	0.33	1	2.25
7	664.13	1	.	1	0	.	664	0	0.33	1	12.45
7	679.13	1	.	0	0	.	679	0	1.14	0	12.45
7	680.13	1	0	0	0	1	593	0	1.14	1	12.45
7	681.13	1	.	0	0	.	681	0	0.33	1	12.45
8	1	0	.	1	0	.	1	0	0.36	1	4.01
8	2	1	.	1	0	.	2	0	0.53	1	4.01
8	3	1	.	0	0	2	3	0	0.89	1	4.01
8	4	1	.	1	0	2	4	0	1.07	1	4.01
8	5	1	.	1	0	2	5	0	1.25	1	4.01
8	6	1	.	0	1	.	6	0	0.89	1	4.01
8	7	1	.	0	0	2	7	0	1.07	1	4.01
8	8	1	.	1	0	.	8	0	1.07	1	17.65
8	9	0	.	0	0	.	9	0	1.07	1	4.01
8	10	0	.	0	0	.	10	0	1.07	1	4.01
8	11	0	.	1	0	.	11	0	0.89	0	4.01
8	12	1	.	1	0	.	12	0	0.36	0	17.65
8	13	1	.	0	0	.	13	0	0.36	1	4.01
8	15	0	.	0	0	2	15	0	0.71	1	4.01
8	17	1	.	1	0	.	17	0	0.36	1	58.59
8	18	0	.	1	0	3	18	0	0.71	1	99.53
8	19	0	.	0	0	.	19	0	1.07	0	99.53
8	20	0	.	0	0	.	20	0	0.89	1	99.53
8	21	1	.	0	0	.	21	0	0.53	1	17.65
8	22	0	.	0	0	.	22	0	0.71	1	17.65
8	23	0	0	0	1	2	22	0	0.89	1	99.53
8	24	0	.	1	0	3	24	0	0.89	1	17.65
8	25	0	.	0	0	.	25	0	1.07	1	99.53
8	26	0	.	0	1	2	26	0	1.07	0	99.53
8	27	0	.	1	0	.	27	0	0.71	1	31.30
8	28	1	1	1	0	1	27	0	1.07	2	31.30
8	29	0	1	0	0	1	27	0	1.25	1	58.59
8	30	0	.	0	0	.	30	0	1.43	1	31.30
8	31	1	.	1	0	.	31	0	1.25	1	31.30
8	32	1	.	1	0	2	32	0	1.43	1	58.59
8	33	1	.	0	0	2	33	0	1.43	1	58.59
8	34	0	1	0	0	2	33	0	1.43	0	58.59
8	35	0	.	0	0	.	35	0	1.07	1	99.53
8	36	1	.	0	0	.	36	0	1.25	1	99.53
8	37	0	.	0	0	2	37	0	1.25	1	99.53
8	38	1	1	0	0	1	37	0	1.25	1	17.65

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
7	615.13	215.21	0.55	1.81	0.57	1.74	0		1	.
7	616.13	308.94	0.53	1.87	0.53	1.87	1	4	0	1.74
7	631.13	272.34	0.83	1.21	0.83	1.21	1	0	0	1.21
7	632.13	818.55	0.83	1.21	0.83	1.21	1	0	0	1.28
7	636.13	307.37	0.85	1.18	0.85	1.18	1	0	0	1.21
7	637.13	415.95	0.84	1.19	0.85	1.18	0		1	.
7	639.13	430.26	1.23	0.81	1.23	0.81	1	0	0	2.09
7	647.13	697.19	0.99	1.01	0.99	1.01	1	0	0	0.81
7	659.13	1252.95	1.01	0.99	1.01	0.99	1	0	0	1.01
7	663.13	1049.52	1.06	0.95	1.06	0.95	1	0	0	0.99
7	664.13	142.65	0.47	2.12	0.47	2.12	1	0	0	.
7	679.13	184.78	0.68	1.47	0.68	1.47	1	0	0	1.49
7	680.13	185.42	0.52	1.91	0.53	1.90	0		1	.
7	681.13	383.15	0.48	2.09	0.48	2.09	1	0	0	1.18
8	1	38.17	1.39	0.72	1.39	0.72	1	0	0	.
8	2	40.04	0.81	1.23	0.81	1.23	1	0	0	0.72
8	3	41.67	0.80	1.24	0.80	1.24	1	0	0	1.23
8	4	42.64	0.83	1.20	0.83	1.20	1	0	0	1.24
8	5	43.91	0.83	1.20	0.83	1.20	1	0	0	1.20
8	6	45.54	0.77	1.29	0.77	1.29	1	0	0	1.20
8	7	47.21	0.78	1.29	0.78	1.29	1	0	0	1.29
8	8	50.40	0.78	1.28	0.78	1.28	1	1	0	1.29
8	9	50.85	0.78	1.29	0.78	1.29	1	0	0	1.28
8	10	52.58	0.77	1.30	0.77	1.30	1	0	0	1.29
8	11	54.48	0.80	1.25	0.80	1.25	1	1	0	1.30
8	12	62.02	0.87	1.15	0.87	1.15	1	0	0	1.25
8	13	72.37	0.88	1.14	0.88	1.14	1	0	0	1.15
8	15	73.44	0.82	1.22	0.82	1.22	1	1	0	1.14
8	17	35.14	0.92	1.09	0.92	1.09	1	0	0	1.22
8	18	29.49	0.92	1.08	0.92	1.08	1	0	0	1.09
8	19	30.03	0.96	1.05	0.96	1.05	1	0	0	1.08
8	20	32.43	1.04	0.96	1.04	0.96	1	1	0	1.05
8	21	97.69	1.00	1.00	1.00	1.00	1	0	0	0.96
8	22	100.46	1.03	0.97	1.03	0.97	1	0	0	1.00
8	23	34.10	1.04	0.96	1.04	0.96	0		1	.
8	24	103.87	1.05	0.95	1.05	0.95	1	0	0	0.97
8	25	36.87	1.07	0.93	1.07	0.93	1	0	0	0.95
8	26	41.41	1.12	0.89	1.12	0.89	1	0	0	0.93
8	27	84.15	1.12	0.89	1.12	0.89	1	0	0	0.89
8	28	85.99	1.11	0.90	1.12	0.89	0		1	.
8	29	67.77	1.13	0.88	1.12	0.89	0		0	.
8	30	88.56	1.13	0.89	1.13	0.89	1	0	0	0.89
8	31	90.19	1.10	0.91	1.10	0.91	1	0	0	0.89
8	32	68.97	1.10	0.91	1.10	0.91	1	1	0	0.91
8	33	70.41	1.10	0.91	1.10	0.91	1	1	0	0.91
8	34	72.81	1.11	0.90	1.10	0.91	0		1	.
8	35	44.24	1.07	0.93	1.07	0.93	1	0	0	0.91
8	36	48.05	1.06	0.94	1.06	0.94	1	0	0	0.93
8	37	50.65	1.05	0.95	1.05	0.95	1	0	0	0.94
8	38	136.00	1.07	0.94	1.05	0.95	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	39	1	.	1	0	.	39	0	1.25	1	99.53
8	40	1	.	1	0	2	40	0	1.25	1	99.53
8	41	0	.	0	0	.	41	0	1.07	1	17.65
8	42	1	.	1	0	.	42	0	0.36	0	58.59
8	43	1	.	0	0	.	43	0	0.71	1	58.59
8	44	1	0	1	0	1	43	0	0.89	1	99.53
8	45	0	.	0	0	2	45	0	1.25	0	58.59
8	46	1	1	1	0	2	45	0	1.25	1	58.59
8	47	1	0	1	0	1	45	0	1.43	1	99.53
8	48	1	.	1	0	.	48	0	1.25	1	99.53
8	49	1	.	1	0	2	49	0	1.25	1	58.59
8	50	0	.	0	0	3	50	0	1.25	1	58.59
8	51	1	.	1	0	2	51	0	1.25	1	99.53
8	52	1	.	1	1	.	52	0	1.07	1	58.59
8	53	1	0	0	0	1	52	0	1.25	2	58.59
8	54	1	.	1	0	.	54	0	1.25	1	85.88
8	55	0	.	0	1	3	55	0	1.25	1	58.59
8	56	0	0	0	1	1	55	0	1.25	1	58.59
8	57	1	.	1	1	.	57	0	1.25	1	58.59
8	58	1	.	1	0	2	58	0	1.07	1	58.59
8	59	1	.	1	0	.	59	0	0.71	0	85.88
8	60	1	.	0	1	.	60	0	0.89	1	85.88
8	61	0	.	1	0	.	61	0	0.89	1	58.59
8	62	0	0	0	0	2	61	0	1.07	1	58.59
8	63	0	.	0	0	.	63	0	0.89	1	99.53
8	64	0	0	1	0	1	63	0	1.07	0	99.53
8	65	1	.	1	0	2	65	0	1.07	1	99.53
8	66	0	.	0	0	2	66	0	1.25	0	58.59
8	67	1	.	1	0	1	67	0	1.25	1	31.30
8	68	0	1	1	0	1	67	0	1.60	2	31.30
8	69	1	.	1	0	.	69	0	0.71	0	99.53
8	70	1	.	1	0	.	70	0	0.71	1	99.53
8	71	0	1	0	0	2	70	0	0.89	1	99.53
8	72	1	.	1	0	2	72	0	1.25	0	99.53
8	73	1	.	1	0	3	73	0	1.25	1	85.88
8	74	0	.	1	0	1	74	0	1.25	1	85.88
8	75	0	.	0	0	2	75	0	1.43	1	113.17
8	76	0	0	1	0	1	75	0	1.25	1	99.53
8	77	0	.	0	0	3	77	0	1.43	1	85.88
8	78	0	0	0	0	2	77	0	1.25	1	99.53
8	79	1	.	1	0	2	79	0	1.25	1	99.53
8	80	1	.	0	0	.	80	0	1.25	0	113.17
8	81	0	.	1	0	3	81	0	1.25	0	58.59
8	82	1	.	1	0	.	82	0	1.07	1	85.88
8	83	1	.	1	0	.	83	0	0.89	1	113.17
8	84	1	0	0	0	1	83	0	1.25	1	85.88
8	85	0	.	0	0	.	85	0	1.07	1	99.53
8	86	0	0	0	1	2	85	0	1.07	1	99.53
8	87	1	1	1	0	2	85	0	1.43	1	99.53
8	88	0	.	0	0	3	88	0	1.07	1	113.17

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	39	52.55	1.06	0.94	1.06	0.94	1	0	0	0.95
8	40	54.82	1.06	0.94	1.06	0.94	1	1	0	0.94
8	41	142.10	1.04	0.96	1.04	0.96	1	0	0	0.94
8	42	82.85	0.74	1.34	0.74	1.34	1	0	0	0.96
8	43	84.75	0.73	1.37	0.73	1.37	1	0	0	1.34
8	44	57.52	0.75	1.33	0.73	1.37	0		1	.
8	45	86.46	0.75	1.34	0.75	1.34	1	0	0	1.37
8	46	89.26	0.74	1.34	0.75	1.34	0		1	.
8	47	59.29	0.75	1.33	0.75	1.34	0		0	.
8	48	60.92	0.76	1.32	0.76	1.32	1	0	0	1.34
8	49	93.40	0.75	1.33	0.75	1.33	1	0	0	1.32
8	50	95.90	0.76	1.32	0.76	1.32	1	0	0	1.33
8	51	63.19	0.78	1.29	0.78	1.29	1	0	0	1.32
8	52	100.57	0.78	1.28	0.78	1.28	1	0	0	1.29
8	53	104.54	0.78	1.29	0.78	1.28	0		1	.
8	54	70.43	0.78	1.29	0.78	1.29	1	0	0	1.28
8	55	108.78	0.77	1.29	0.77	1.29	1	0	0	1.29
8	56	110.91	0.78	1.28	0.77	1.29	0		1	.
8	57	112.78	0.77	1.30	0.77	1.30	1	0	0	1.29
8	58	114.68	0.79	1.27	0.79	1.27	1	1	0	1.30
8	59	72.07	0.76	1.32	0.76	1.32	1	0	0	1.27
8	60	73.47	0.77	1.29	0.77	1.29	1	0	0	1.32
8	61	120.12	0.78	1.29	0.79	1.27	1	0	0	1.29
8	62	125.06	0.79	1.27	0.79	1.27	0		1	.
8	63	70.47	0.81	1.23	0.81	1.23	1	0	0	1.29
8	64	71.24	0.79	1.27	0.81	1.23	0		1	.
8	65	73.10	0.78	1.28	0.78	1.28	1	0	0	1.23
8	66	127.20	0.80	1.25	0.80	1.25	1	1	0	1.28
8	67	188.53	0.81	1.24	0.81	1.24	1	0	0	1.25
8	68	190.29	0.80	1.25	0.81	1.24	0		1	.
8	69	66.90	0.83	1.20	0.83	1.20	1	0	0	1.24
8	70	65.63	0.81	1.24	0.81	1.24	1	0	0	1.20
8	71	75.51	0.83	1.21	0.81	1.24	0		1	.
8	72	77.44	0.83	1.20	0.83	1.20	1	1	0	1.24
8	73	81.21	0.82	1.21	0.82	1.21	1	0	0	1.20
8	74	83.01	0.85	1.18	0.85	1.18	1	1	0	1.21
8	75	56.75	0.84	1.20	0.84	1.20	1	0	0	1.18
8	76	82.38	0.84	1.18	0.84	1.20	0		1	.
8	77	89.19	0.85	1.17	0.85	1.17	1	0	0	1.20
8	78	84.65	0.87	1.15	0.85	1.17	0		1	.
8	79	87.38	0.87	1.15	0.87	1.15	1	0	0	1.17
8	80	59.99	0.86	1.16	0.86	1.16	1	0	0	1.15
8	81	149.85	0.88	1.13	0.88	1.13	1	0	0	1.16
8	82	94.29	0.86	1.16	0.86	1.16	1	0	0	1.13
8	83	61.19	0.77	1.30	0.77	1.30	1	0	0	1.16
8	84	97.16	0.79	1.27	0.77	1.30	0		1	.
8	85	96.39	0.81	1.24	0.81	1.24	1	0	0	1.30
8	86	94.89	0.82	1.22	0.81	1.24	0		1	.
8	87	98.66	0.84	1.20	0.81	1.24	0		0	.
8	88	58.05	0.87	1.15	0.87	1.15	1	0	0	1.24

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	89	0	0	0	0	2	88	0	1.25	0	113.17
8	90	0	0	0	0	2	88	0	1.60	1	113.17
8	91	0	.	0	0	2	91	0	1.60	1	113.17
8	93	0	.	0	1	.	93	0	1.43	0	113.17
8	94	1	1	0	0	1	93	0	1.60	1	113.17
8	95	0	.	0	0	2	95	0	1.60	1	113.17
8	96	0	.	1	0	.	96	0	1.43	1	85.88
8	97	1	.	1	0	2	97	0	1.43	1	113.17
8	98	1	.	0	0	.	98	0	1.25	1	126.82
8	99	0	.	0	1	.	99	0	1.25	1	126.82
8	100	1	.	1	0	.	100	0	1.25	0	126.82
8	101	1	.	1	0	1	101	0	1.43	1	113.17
8	102	1	0	1	0	2	101	0	1.43	0	113.17
8	103	0	.	0	0	2	103	0	1.43	1	126.82
8	104	0	.	0	1	1	104	0	1.43	1	113.17
8	105	0	0	0	1	2	104	0	1.60	1	113.17
8	106	0	0	1	0	2	104	0	1.60	1	126.82
8	107	1	.	0	0	.	107	0	1.43	0	126.82
8	109	1	.	1	0	.	109	0	1.43	1	126.82
8	110	0	1	0	0	2	109	0	1.60	2	126.82
8	111	0	0	0	0	1	109	0	1.78	1	126.82
8	112	0	.	1	0	1	112	0	1.78	0	72.24
8	113	0	.	0	0	1	113	0	1.96	1	85.88
8	114	0	.	1	0	.	114	0	1.60	1	113.17
8	115	1	1	1	0	1	114	0	1.60	1	126.82
8	116	1	.	0	0	.	116	0	1.43	1	113.17
8	117	0	.	1	0	.	117	0	1.60	1	113.17
8	118	0	.	0	0	.	118	0	1.25	1	113.17
8	119	1	1	1	0	1	118	0	1.43	1	113.17
8	120	0	1	0	0	1	118	0	1.60	1	85.88
8	121	1	1	1	0	1	118	0	1.60	1	113.17
8	122	0	.	1	0	.	122	0	1.60	1	113.17
8	123	1	.	1	0	.	123	0	1.25	1	154.11
8	124	1	.	0	0	.	124	0	1.43	1	154.11
8	125	0	1	1	1	1	124	0	1.43	0	154.11
8	126	0	0	0	1	2	124	0	1.60	1	113.17
8	127	1	.	0	0	.	127	0	1.60	1	154.11
8	128	1	0	0	0	2	127	0	1.60	1	113.17
8	129	0	.	1	0	2	129	0	1.60	1	72.24
8	130	1	.	0	0	.	130	0	1.43	1	85.88
8	131	0	1	0	0	1	130	0	1.60	2	72.24
8	132	1	1	1	0	1	130	0	1.78	1	181.40
8	133	0	.	1	0	.	133	0	1.60	1	154.11
8	134	1	.	1	0	.	134	0	1.60	0	154.11
8	135	0	1	1	0	1	134	0	1.60	0	154.11
8	136	1	.	1	0	.	136	0	1.60	1	154.11
8	137	1	.	1	0	.	137	0	1.25	1	113.17
8	138	0	1	1	0	2	137	0	1.25	1	113.17
8	139	0	0	0	0	2	137	0	1.43	1	181.40
8	140	1	.	1	0	.	140	0	1.43	1	181.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	89	66.06	0.86	1.16	0.87	1.15	0		1	.
8	90	64.93	0.88	1.14	0.87	1.15	0		0	.
8	91	67.46	0.89	1.12	0.89	1.12	1	0	0	1.15
8	93	69.20	0.83	1.21	0.83	1.21	1	0	0	1.12
8	94	70.73	0.82	1.22	0.83	1.21	0		1	.
8	95	71.90	0.84	1.19	0.84	1.19	1	1	0	1.21
8	96	112.84	0.84	1.19	0.84	1.19	1	0	0	1.19
8	97	75.41	0.86	1.16	0.86	1.16	1	0	0	1.19
8	98	73.37	0.89	1.13	0.89	1.13	1	0	0	1.16
8	99	71.23	0.88	1.13	0.88	1.13	1	0	0	1.13
8	100	69.40	0.85	1.18	0.85	1.18	1	0	0	1.13
8	101	79.11	0.86	1.16	0.86	1.16	1	0	0	1.18
8	102	80.84	0.87	1.15	0.86	1.16	0		1	.
8	103	78.01	0.90	1.11	0.90	1.11	1	0	0	1.16
8	104	82.68	0.91	1.09	0.91	1.09	1	0	0	1.11
8	105	84.61	0.94	1.06	0.91	1.09	0		1	.
8	106	80.11	0.96	1.05	0.91	1.09	0		0	.
8	107	81.81	0.92	1.09	0.92	1.09	1	0	0	1.09
8	109	82.78	0.90	1.12	0.90	1.12	1	0	0	1.09
8	110	85.48	0.89	1.12	0.90	1.12	0		1	.
8	111	90.95	0.91	1.10	0.90	1.12	0		0	.
8	112	226.76	0.91	1.09	0.91	1.09	1	1	0	1.12
8	113	154.08	0.92	1.09	0.92	1.09	1	1	0	1.09
8	114	91.09	0.93	1.07	0.93	1.07	1	0	0	1.09
8	115	93.06	0.95	1.05	0.93	1.07	0		1	.
8	116	96.03	0.92	1.09	0.92	1.09	1	0	0	1.07
8	117	85.88	0.90	1.11	0.90	1.11	1	0	0	1.09
8	118	99.93	0.86	1.16	0.86	1.16	1	0	0	1.11
8	119	102.47	0.87	1.15	0.86	1.16	0		1	.
8	120	173.47	0.89	1.13	0.86	1.16	0		0	.
8	121	107.10	0.90	1.11	0.86	1.16	0		0	.
8	122	104.93	0.92	1.09	0.92	1.09	1	1	0	1.16
8	123	69.86	0.88	1.13	0.88	1.13	1	0	0	1.09
8	124	71.27	0.86	1.16	0.86	1.16	1	0	0	1.13
8	125	73.10	0.86	1.17	0.86	1.16	0		1	.
8	126	112.28	0.86	1.16	0.86	1.16	0		0	.
8	127	75.00	0.86	1.16	0.86	1.16	1	0	0	1.16
8	128	115.95	0.87	1.15	0.86	1.16	0		1	.
8	129	257.23	0.89	1.12	0.89	1.12	1	1	0	1.16
8	130	166.53	0.84	1.18	0.84	1.18	1	0	0	1.12
8	131	259.13	0.84	1.19	0.84	1.18	0		1	.
8	132	58.46	0.85	1.18	0.84	1.18	0		0	.
8	133	79.81	0.85	1.17	0.85	1.17	1	0	0	1.18
8	134	87.15	0.83	1.21	0.83	1.21	1	0	0	1.17
8	135	78.14	0.85	1.17	0.83	1.21	0		1	.
8	136	89.28	0.84	1.19	0.84	1.19	1	0	0	1.21
8	137	129.59	0.82	1.22	0.82	1.22	1	0	0	1.19
8	138	132.20	0.84	1.20	0.82	1.22	0		1	.
8	139	67.53	0.85	1.17	0.82	1.22	0		0	.
8	140	69.50	0.85	1.17	0.85	1.17	1	0	0	1.22

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	141	0	.	0	0	1	141	0	1.25	1	181.40
8	142	0	0	0	0	2	141	0	1.43	0	181.40
8	143	1	.	1	0	2	143	0	1.43	1	181.40
8	144	1	.	1	0	.	144	0	1.43	1	181.40
8	145	0	1	1	0	1	144	0	1.43	0	181.40
8	146	1	1	1	0	1	144	0	1.60	1	99.53
8	147	0	.	0	0	1	147	0	1.43	1	195.05
8	148	0	0	0	0	1	147	0	1.25	0	195.05
8	149	0	.	0	0	1	149	0	1.43	1	126.82
8	150	1	1	1	0	2	149	0	1.25	0	126.82
8	151	0	.	0	0	1	151	0	1.25	1	181.40
8	152	1	1	1	0	1	151	0	1.60	2	181.40
8	153	0	1	1	0	1	151	0	1.78	1	113.17
8	154	0	.	0	0	2	154	0	1.78	1	154.11
8	155	1	1	1	0	1	154	0	1.60	0	154.11
8	156	1	.	1	0	.	156	0	1.43	1	85.88
8	157	1	0	0	0	1	156	0	1.78	2	72.24
8	158	1	0	1	1	1	156	0	1.96	1	85.88
8	159	1	.	1	0	.	159	0	1.43	1	195.05
8	160	1	0	0	0	1	159	0	1.78	2	181.40
8	161	0	1	0	0	1	159	0	1.78	1	181.40
8	162	0	.	0	0	1	162	0	1.78	0	195.05
8	163	1	1	0	0	2	162	0	1.60	1	181.40
8	164	1	.	1	0	1	164	0	1.60	1	195.05
8	165	0	1	0	0	2	164	0	1.60	1	181.40
8	166	1	1	0	0	2	164	0	1.60	0	181.40
8	167	0	.	1	0	.	167	0	1.07	1	154.11
8	168	1	.	1	0	.	168	0	1.25	0	154.11
8	169	0	1	1	0	1	168	0	1.43	1	154.11
8	170	0	.	0	0	3	170	0	1.25	0	167.75
8	171	0	0	0	0	1	170	0	1.25	1	235.98
8	172	0	.	0	0	1	172	0	1.43	1	235.98
8	173	0	.	0	0	.	173	0	1.43	1	181.40
8	174	0	0	0	0	1	173	0	1.43	2	181.40
8	175	0	0	1	0	1	173	0	1.60	1	113.17
8	176	1	.	0	0	.	176	0	1.60	1	167.75
8	177	1	0	0	0	1	176	0	1.60	1	167.75
8	178	1	0	0	0	1	176	0	1.78	0	167.75
8	179	1	0	1	0	1	176	0	1.96	1	167.75
8	180	0	1	1	1	2	176	0	1.78	1	113.17
8	181	0	.	1	0	2	181	0	1.60	1	181.40
8	182	1	.	1	0	2	182	0	1.78	1	249.63
8	183	0	1	0	0	1	182	0	1.78	1	249.63
8	184	1	.	1	0	1	184	0	1.78	2	249.63
8	185	1	.	0	0	.	185	0	1.43	1	167.75
8	186	1	.	1	0	.	186	0	1.43	1	208.69
8	187	0	1	0	0	2	186	0	1.43	1	208.69
8	188	0	.	0	0	3	188	0	1.43	1	167.75
8	189	1	.	1	0	.	189	0	1.25	1	167.75
8	190	0	.	1	0	.	190	0	1.25	1	181.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	141	70.94	0.88	1.13	0.88	1.13	1	1	0	1.17
8	142	72.17	0.86	1.17	0.88	1.13	0		0	.
8	143	74.04	0.86	1.16	0.86	1.16	1	0	0	1.13
8	144	75.91	0.83	1.21	0.83	1.21	1	0	0	1.16
8	145	77.28	0.83	1.20	0.83	1.21	0		1	.
8	146	250.95	0.84	1.19	0.83	1.21	0		0	.
8	147	50.62	0.86	1.16	0.86	1.16	1	0	0	1.21
8	148	51.92	0.87	1.15	0.86	1.16	0		1	.
8	149	146.21	0.87	1.15	0.87	1.15	1	0	0	1.16
8	150	147.74	0.88	1.14	0.87	1.15	0		1	.
8	151	88.42	0.87	1.15	0.87	1.15	1	0	0	1.15
8	152	87.52	0.88	1.13	0.87	1.15	0		1	.
8	153	158.59	0.88	1.14	0.87	1.15	0		0	.
8	154	130.16	0.88	1.13	0.88	1.13	1	0	0	1.15
8	155	113.71	0.88	1.14	0.88	1.13	0		1	.
8	156	269.80	0.79	1.27	0.79	1.27	1	0	0	1.13
8	157	303.07	0.79	1.27	0.79	1.27	0		1	.
8	158	271.27	0.80	1.24	0.79	1.27	0		0	.
8	159	69.14	0.79	1.26	0.79	1.26	1	0	0	1.27
8	160	96.30	0.80	1.25	0.79	1.26	0		1	.
8	161	97.80	0.81	1.24	0.79	1.26	0		0	.
8	162	70.40	0.81	1.23	0.81	1.23	1	0	0	1.26
8	163	101.10	0.82	1.22	0.81	1.23	0		1	.
8	164	72.01	0.83	1.21	0.83	1.21	1	0	0	1.23
8	165	105.67	0.84	1.19	0.83	1.21	0		1	.
8	166	104.94	0.85	1.18	0.83	1.21	0		0	.
8	167	139.80	0.86	1.17	0.86	1.17	1	0	0	1.21
8	168	140.24	0.84	1.20	0.84	1.20	1	0	0	1.17
8	169	142.07	0.84	1.19	0.84	1.20	0		1	.
8	170	107.94	0.85	1.17	0.85	1.17	1	0	0	1.20
8	171	57.30	0.88	1.14	0.85	1.17	0		1	.
8	172	58.66	0.88	1.13	0.88	1.13	1	0	0	1.17
8	173	110.54	0.85	1.17	0.85	1.17	1	0	0	1.13
8	174	112.58	0.84	1.19	0.85	1.17	0		1	.
8	175	223.92	0.85	1.18	0.85	1.17	0		0	.
8	176	119.62	0.84	1.19	0.84	1.19	1	0	0	1.17
8	177	114.18	0.85	1.18	0.84	1.19	0		1	.
8	178	117.15	0.84	1.19	0.84	1.19	0		0	.
8	179	122.22	0.83	1.20	0.84	1.19	0		0	.
8	180	267.80	0.84	1.20	0.84	1.19	0		0	.
8	181	114.21	0.84	1.19	0.84	1.19	1	1	0	1.19
8	182	40.47	0.85	1.18	0.85	1.18	1	0	0	1.19
8	183	41.51	0.86	1.17	0.85	1.18	0		1	.
8	184	42.71	0.86	1.17	0.86	1.17	1	0	0	1.18
8	185	125.76	0.85	1.18	0.85	1.18	1	0	0	1.17
8	186	92.73	0.84	1.19	0.84	1.19	1	0	0	1.18
8	187	94.33	0.86	1.17	0.84	1.19	0		1	.
8	188	128.43	0.84	1.19	0.84	1.19	1	0	0	1.19
8	189	131.63	0.85	1.17	0.85	1.17	1	0	0	1.19
8	190	128.79	0.84	1.20	0.84	1.20	1	0	0	1.17

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	191	1	.	1	0	1	191	0	1.25	1	195.05
8	192	1	.	1	0	2	192	0	1.43	1	208.69
8	193	0	.	0	0	.	193	0	1.43	1	235.98
8	194	0	0	0	0	2	193	0	1.43	0	235.98
8	195	1	.	1	0	2	195	0	1.43	1	181.40
8	196	1	.	1	0	2	196	0	1.43	1	181.40
8	197	0	.	0	0	2	197	0	1.43	1	235.98
8	198	0	.	1	1	2	198	0	1.43	1	235.98
8	199	0	0	0	0	2	198	0	1.25	1	181.40
8	200	1	.	1	0	2	200	0	1.25	1	181.40
8	201	1	.	1	0	1	201	0	1.43	0	181.40
8	202	1	0	1	0	1	201	0	1.60	1	181.40
8	203	1	.	1	0	2	203	0	1.60	1	181.40
8	204	0	.	1	1	.	204	0	1.43	1	235.98
8	205	1	.	1	0	1	205	0	1.60	1	167.75
8	206	0	1	1	0	2	205	0	1.43	1	195.05
8	207	1	.	0	0	.	207	0	1.25	2	249.63
8	208	1	0	1	0	1	207	0	1.25	1	85.88
8	209	1	.	1	0	1	209	0	1.60	2	85.88
8	210	1	.	0	0	.	210	0	1.43	1	208.69
8	211	0	1	1	0	1	210	0	1.43	1	222.34
8	212	0	0	0	0	1	210	0	1.78	2	222.34
8	213	1	1	1	0	1	210	0	1.78	1	195.05
8	214	0	1	0	0	2	210	0	1.78	1	222.34
8	215	1	1	1	0	1	210	0	1.60	2	222.34
8	216	0	.	0	1	1	216	0	1.78	1	235.98
8	217	0	.	0	1	2	217	0	1.43	0	235.98
8	218	0	.	1	1	1	218	0	1.25	0	235.98
8	219	0	0	0	0	2	218	0	1.25	1	249.63
8	220	1	.	1	0	.	220	0	1.07	1	263.27
8	221	0	.	1	0	2	221	0	1.25	1	85.88
8	222	1	.	1	0	.	222	0	1.07	1	222.34
8	223	1	.	0	0	.	223	0	0.89	1	222.34
8	224	0	1	0	0	1	223	0	1.25	1	222.34
8	225	0	.	1	1	2	225	0	1.43	0	222.34
8	226	1	.	1	0	.	226	0	1.25	1	249.63
8	227	1	.	1	0	1	227	0	1.25	2	249.63
8	228	0	.	1	0	.	228	0	1.43	1	249.63
8	229	0	0	1	0	1	228	0	1.43	0	249.63
8	230	0	0	1	0	2	228	0	1.60	1	167.75
8	231	0	.	1	0	2	231	0	1.43	1	235.98
8	232	0	.	1	0	2	232	0	1.25	0	235.98
8	233	0	.	1	0	2	233	0	1.25	1	58.59
8	234	0	.	0	0	3	234	0	1.25	1	181.40
8	235	1	.	1	0	1	235	0	1.25	2	181.40
8	237	0	.	0	0	.	237	0	0.89	1	263.27
8	238	1	.	1	0	.	238	0	0.53	1	140.46
8	239	0	.	1	0	.	239	0	0.36	1	263.27
8	240	0	0	1	0	2	239	0	0.71	0	263.27
8	241	0	.	1	0	.	241	0	0.36	1	44.94

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	191	95.43	0.86	1.17	0.86	1.17	1	1	0	1.20
8	192	95.93	0.85	1.17	0.85	1.17	1	0	0	1.17
8	193	72.88	0.86	1.16	0.86	1.16	1	0	0	1.17
8	194	74.15	0.86	1.16	0.86	1.16	0		1	.
8	195	139.01	0.86	1.16	0.86	1.16	1	0	0	1.16
8	196	141.31	0.87	1.14	0.87	1.14	1	0	0	1.16
8	197	75.85	0.88	1.13	0.88	1.13	1	0	0	1.14
8	198	77.92	0.89	1.13	0.89	1.13	1	0	0	1.13
8	199	148.68	0.91	1.10	0.89	1.13	0		1	.
8	200	150.05	0.91	1.10	0.91	1.10	1	0	0	1.13
8	201	151.42	0.90	1.11	0.90	1.11	1	0	0	1.10
8	202	152.92	0.92	1.09	0.90	1.11	0		1	.
8	203	154.25	0.90	1.11	0.90	1.11	1	0	0	1.11
8	204	81.65	0.86	1.17	0.86	1.17	1	0	0	1.11
8	205	159.89	0.85	1.18	0.85	1.18	1	0	0	1.17
8	206	114.25	0.86	1.16	0.85	1.18	0		1	.
8	207	69.53	0.82	1.22	0.82	1.22	1	0	0	1.18
8	208	354.12	0.77	1.30	0.82	1.22	0		1	.
8	209	356.62	0.79	1.26	0.79	1.26	1	1	0	1.22
8	210	113.88	0.77	1.30	0.77	1.30	1	0	0	1.26
8	211	99.37	0.78	1.28	0.77	1.30	0		1	.
8	212	97.87	0.77	1.30	0.77	1.30	0		0	.
8	213	129.26	0.78	1.29	0.77	1.30	0		0	.
8	214	100.87	0.78	1.28	0.77	1.30	0		0	.
8	215	102.14	0.79	1.26	0.77	1.30	0		0	.
8	216	112.95	0.80	1.25	0.80	1.25	1	0	0	1.30
8	217	116.69	0.81	1.24	0.81	1.24	1	0	0	1.25
8	218	118.56	0.81	1.24	0.81	1.24	1	0	0	1.24
8	219	113.68	0.82	1.22	0.81	1.24	0		1	.
8	220	114.58	0.85	1.18	0.85	1.18	1	0	0	1.24
8	221	379.38	0.85	1.17	0.85	1.17	1	0	0	1.18
8	222	137.14	0.84	1.19	0.84	1.19	1	0	0	1.17
8	223	139.31	0.82	1.22	0.82	1.22	1	0	0	1.19
8	224	142.51	0.83	1.20	0.82	1.22	0		1	.
8	225	144.05	0.83	1.20	0.83	1.20	1	0	0	1.22
8	226	117.62	0.80	1.24	0.80	1.24	1	0	0	1.20
8	227	119.15	0.79	1.26	0.79	1.26	1	1	0	1.24
8	228	120.15	0.78	1.28	0.78	1.28	1	0	0	1.26
8	229	139.50	0.79	1.26	0.78	1.28	0		1	.
8	230	228.16	0.80	1.24	0.78	1.28	0		0	.
8	231	193.00	0.81	1.23	0.81	1.23	1	0	0	1.28
8	232	194.83	0.82	1.22	0.82	1.22	1	0	0	1.23
8	233	436.61	0.82	1.22	0.82	1.22	1	0	0	1.22
8	234	243.94	0.83	1.21	0.83	1.21	1	0	0	1.22
8	235	282.72	0.83	1.20	0.83	1.20	1	0	0	1.21
8	237	274.17	0.85	1.17	0.85	1.17	1	0	0	1.20
8	238	439.33	1.13	0.89	1.13	0.89	1	0	0	1.17
8	239	424.76	1.22	0.82	1.22	0.82	1	0	0	0.89
8	240	426.36	1.23	0.81	1.22	0.82	0		1	.
8	241	733.20	0.94	1.07	0.94	1.07	1	0	0	0.82

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	243	0	.	1	0	.	243	0	0.36	1	85.88
8	244	0	.	1	0	.	244	0	0.71	1	126.82
8	245	0	.	1	0	.	245	0	0.36	1	4.01
8	248	0	.	1	0	.	248	0	0.36	0	72.24
8	17.01	1	.	1	0	.	17	0	0.36	1	31.30
8	18.01	0	.	1	0	.	18	0	0.53	1	72.24
8	19.01	0	.	0	0	.	19	0	0.89	1	72.24
8	20.01	0	.	0	0	.	20	0	0.53	1	72.24
8	23.01	0	.	0	1	2	23	0	0.89	1	72.24
8	25.01	0	.	0	0	2	25	0	1.25	1	72.24
8	26.01	0	0	0	1	2	25	0	1.25	0	72.24
8	27.01	0	.	1	0	.	27	0	1.07	1	4.01
8	28.01	1	.	1	0	1	28	0	1.25	2	4.01
8	29.01	0	.	0	0	.	29	0	1.25	1	31.30
8	30.01	0	.	0	0	.	30	0	1.43	1	4.01
8	31.01	1	.	1	0	2	31	0	1.60	1	4.01
8	32.01	1	.	1	0	.	32	0	1.78	1	31.30
8	33.01	1	.	0	0	2	33	0	1.78	1	31.30
8	34.01	0	1	0	0	2	33	0	1.78	1	31.30
8	35.01	0	.	0	0	.	35	0	1.43	1	72.24
8	36.01	1	1	0	0	2	35	0	1.43	1	72.24
8	37.01	0	1	0	0	2	35	0	1.43	1	72.24
8	39.01	1	.	1	0	2	39	0	1.60	1	72.24
8	40.01	1	.	1	0	3	40	0	1.60	1	72.24
8	42.01	1	.	1	0	.	42	0	0.36	1	31.30
8	43.01	1	.	0	0	.	43	0	0.71	1	31.30
8	44.01	1	0	1	0	1	43	0	1.07	1	72.24
8	45.01	0	1	0	0	1	43	0	1.43	0	31.30
8	46.01	1	1	1	0	1	43	0	1.60	1	31.30
8	47.01	1	0	1	0	1	43	0	1.78	0	72.24
8	48.01	1	.	1	0	2	48	0	1.78	1	72.24
8	49.01	1	.	1	0	2	49	0	1.78	1	31.30
8	50.01	0	.	0	0	3	50	0	1.78	1	31.30
8	51.01	1	.	1	0	.	51	0	1.78	1	72.24
8	52.01	1	.	1	1	.	52	0	1.60	1	31.30
8	53.01	1	0	0	0	1	52	0	1.96	2	31.30
8	54.01	1	0	1	0	2	52	0	1.96	1	58.59
8	55.01	0	.	0	1	3	55	0	2.14	1	31.30
8	56.01	0	0	0	1	1	55	0	2.14	1	31.30
8	57.01	1	.	1	1	.	57	0	1.60	1	31.30
8	58.01	1	.	1	0	.	58	0	1.25	1	31.30
8	59.01	1	.	1	0	.	59	0	1.07	1	58.59
8	60.01	1	.	0	1	.	60	0	1.07	1	58.59
8	61.01	0	.	1	0	.	61	0	1.07	1	31.30
8	62.01	0	.	0	0	.	62	0	1.07	1	31.30
8	63.01	0	.	0	0	.	63	0	1.07	1	72.24
8	64.01	0	0	1	0	1	63	0	1.43	2	72.24
8	65.01	1	1	1	0	2	63	0	1.43	1	72.24
8	66.01	0	.	0	0	.	66	0	1.43	0	31.30
8	67.01	1	1	1	0	1	66	0	1.43	1	4.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	243	945.18	1.29	0.78	1.29	0.78	1	0	0	1.07
8	244	721.68	1.26	0.80	1.26	0.80	1	0	0	0.78
8	245	1207.40	1.14	0.88	1.14	0.88	1	0	0	0.80
8	248	1252.16	0.69	1.46	0.69	1.46	1	0	0	0.88
8	17.01	35.14	1.01	0.99	1.01	0.99	1	0	0	.
8	18.01	29.49	1.17	0.85	1.17	0.85	1	0	0	0.99
8	19.01	30.03	1.24	0.80	1.24	0.80	1	0	0	0.85
8	20.01	32.43	1.43	0.70	1.43	0.70	1	0	0	0.80
8	23.01	34.10	1.10	0.91	1.10	0.91	1	1	0	0.70
8	25.01	36.87	1.01	0.99	1.01	0.99	1	1	0	0.91
8	26.01	41.41	0.95	1.05	1.01	0.99	0		0	.
8	27.01	84.15	0.72	1.39	0.72	1.39	1	0	0	0.99
8	28.01	85.99	0.73	1.37	0.73	1.37	1	1	0	1.39
8	29.01	67.77	0.72	1.39	0.72	1.39	1	1	0	1.37
8	30.01	88.56	0.73	1.38	0.73	1.38	1	0	0	1.39
8	31.01	90.19	0.73	1.37	0.73	1.37	1	0	0	1.38
8	32.01	68.97	0.73	1.38	0.73	1.38	1	0	0	1.37
8	33.01	70.41	0.72	1.38	0.72	1.38	1	0	0	1.38
8	34.01	72.81	0.72	1.38	0.72	1.38	0		1	.
8	35.01	44.24	0.75	1.34	0.75	1.34	1	0	0	1.38
8	36.01	48.05	0.75	1.34	0.75	1.34	0		1	.
8	37.01	50.65	0.75	1.33	0.75	1.34	0		0	.
8	39.01	52.55	0.72	1.39	0.72	1.39	1	0	0	1.34
8	40.01	54.82	0.73	1.37	0.73	1.37	1	0	0	1.39
8	42.01	82.85	0.68	1.46	0.68	1.46	1	0	0	1.37
8	43.01	84.75	0.67	1.49	0.67	1.49	1	0	0	1.46
8	44.01	57.52	0.66	1.51	0.67	1.49	0		1	.
8	45.01	86.46	0.66	1.51	0.67	1.49	0		0	.
8	46.01	89.26	0.67	1.50	0.67	1.49	0		0	.
8	47.01	59.29	0.67	1.50	0.67	1.49	0		0	.
8	48.01	60.92	0.70	1.43	0.70	1.43	1	0	0	1.49
8	49.01	93.40	0.76	1.31	0.76	1.31	1	1	0	1.43
8	50.01	95.90	0.87	1.15	0.87	1.15	1	0	0	1.31
8	51.01	63.19	0.84	1.19	0.84	1.19	1	1	0	1.15
8	52.01	100.57	0.83	1.20	0.83	1.20	1	0	0	1.19
8	53.01	104.54	0.82	1.22	0.83	1.20	0		1	.
8	54.01	70.43	0.82	1.22	0.83	1.20	0		0	.
8	55.01	108.78	0.82	1.22	0.82	1.22	1	0	0	1.20
8	56.01	110.91	0.82	1.22	0.82	1.22	0		1	.
8	57.01	112.78	0.85	1.18	0.85	1.18	1	0	0	1.22
8	58.01	114.68	0.85	1.18	0.85	1.18	1	0	0	1.18
8	59.01	72.07	0.85	1.18	0.85	1.18	1	0	0	1.18
8	60.01	73.47	0.84	1.18	0.84	1.18	1	0	0	1.18
8	61.01	120.12	0.88	1.14	0.88	1.14	1	1	0	1.18
8	62.01	125.06	0.91	1.10	0.91	1.10	1	1	0	1.14
8	63.01	70.47	0.88	1.14	0.88	1.14	1	0	0	1.10
8	64.01	71.24	0.88	1.13	0.88	1.14	0		1	.
8	65.01	73.10	0.92	1.09	0.88	1.14	0		0	.
8	66.01	127.20	0.93	1.08	0.93	1.08	1	0	0	1.14
8	67.01	188.53	0.90	1.11	0.93	1.08	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	68.01	0	1	1	0	1	66	0	1.78	2	4.01
8	69.01	1	.	1	0	.	69	0	1.25	0	72.24
8	70.01	1	0	1	0	1	69	0	1.25	1	72.24
8	71.01	0	1	0	0	2	69	0	1.43	1	72.24
8	72.01	1	.	1	0	3	72	0	1.60	1	72.24
8	73.01	1	.	1	0	2	73	0	1.78	1	58.59
8	74.01	0	.	1	0	2	74	0	1.78	1	58.59
8	75.01	0	.	0	0	2	75	0	1.78	1	85.88
8	76.01	0	0	1	0	1	75	0	1.78	1	72.24
8	77.01	0	.	0	0	2	77	0	1.78	1	58.59
8	78.01	0	0	0	0	2	77	0	1.96	1	72.24
8	79.01	1	1	1	0	1	77	0	1.96	1	72.24
8	80.01	1	.	0	0	3	80	0	1.78	0	85.88
8	81.01	0	.	1	0	2	81	0	1.78	0	31.30
8	82.01	1	1	1	0	2	81	0	1.78	1	58.59
8	83.01	1	.	1	0	3	83	0	1.43	1	85.88
8	84.01	1	0	0	0	1	83	0	1.78	1	58.59
8	85.01	0	.	0	0	.	85	0	1.43	1	72.24
8	86.01	0	0	0	1	1	85	0	1.43	0	72.24
8	87.01	1	1	1	0	2	85	0	1.60	1	72.24
8	88.01	0	.	0	0	3	88	0	1.43	1	85.88
8	89.01	0	0	0	0	2	88	0	1.78	1	85.88
8	90.01	0	.	0	0	2	90	0	1.96	1	85.88
8	91.01	0	0	0	0	2	90	0	1.96	1	85.88
8	93.01	0	0	0	1	1	90	0	1.96	2	85.88
8	94.01	1	1	0	0	1	90	0	2.14	1	85.88
8	95.01	0	.	0	0	3	95	0	2.14	1	85.88
8	96.01	0	0	1	0	2	95	0	1.96	1	58.59
8	97.01	1	1	1	0	2	95	0	1.96	1	85.88
8	98.01	1	.	0	0	.	98	0	1.78	1	99.53
8	99.01	0	1	0	1	2	98	0	1.78	1	99.53
8	100.01	1	.	1	0	1	100	0	1.78	2	99.53
8	101.01	1	0	1	0	1	100	0	1.96	1	85.88
8	102.01	1	.	1	0	2	102	0	1.96	1	85.88
8	103.01	0	.	0	0	2	103	0	1.78	1	99.53
8	104.01	0	0	0	1	1	103	0	1.96	1	85.88
8	105.01	0	0	0	1	1	103	0	1.96	1	85.88
8	106.01	0	0	1	0	2	103	0	1.96	1	99.53
8	107.01	1	.	0	0	3	107	0	1.96	0	99.53
8	109.01	1	.	1	0	2	109	0	1.96	1	99.53
8	110.01	0	1	0	0	1	109	0	2.14	2	99.53
8	111.01	0	0	0	0	1	109	0	2.14	1	99.53
8	112.01	0	0	1	0	1	109	0	2.14	0	44.94
8	113.01	0	0	0	0	1	109	0	2.32	1	58.59
8	114.01	0	.	1	0	2	114	0	2.14	1	85.88
8	115.01	1	1	1	0	2	114	0	2.14	1	99.53
8	116.01	1	.	0	0	.	116	0	2.14	1	85.88
8	117.01	0	1	1	0	2	116	0	1.96	1	85.88
8	118.01	0	.	0	0	2	118	0	1.78	1	85.88
8	119.01	1	1	1	0	1	118	0	1.78	1	85.88

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	68.01	190.29	0.91	1.10	0.93	1.08	0		0	.
8	69.01	66.90	0.81	1.23	0.81	1.23	1	0	0	1.08
8	70.01	65.63	0.80	1.25	0.81	1.23	0		1	.
8	71.01	75.51	0.80	1.24	0.81	1.23	0		0	.
8	72.01	77.44	0.80	1.25	0.80	1.25	1	0	0	1.23
8	73.01	81.21	0.81	1.23	0.81	1.23	1	0	0	1.25
8	74.01	83.01	0.81	1.23	0.81	1.23	1	0	0	1.23
8	75.01	56.75	0.80	1.25	0.80	1.25	1	1	0	1.23
8	76.01	82.38	0.80	1.25	0.80	1.25	0		1	.
8	77.01	89.19	0.80	1.26	0.80	1.26	1	0	0	1.25
8	78.01	84.65	0.79	1.27	0.80	1.26	0		1	.
8	79.01	87.38	0.78	1.28	0.80	1.26	0		0	.
8	80.01	59.99	0.77	1.31	0.77	1.31	1	0	0	1.26
8	81.01	149.85	0.76	1.32	0.76	1.32	1	0	0	1.31
8	82.01	94.29	0.75	1.34	0.76	1.32	0		1	.
8	83.01	61.19	0.75	1.34	0.75	1.34	1	0	0	1.32
8	84.01	97.16	0.74	1.35	0.75	1.34	0		1	.
8	85.01	96.39	0.73	1.37	0.73	1.37	1	0	0	1.34
8	86.01	94.89	0.72	1.38	0.73	1.37	0		1	.
8	87.01	98.66	0.71	1.41	0.73	1.37	0		0	.
8	88.01	58.05	0.70	1.43	0.70	1.43	1	0	0	1.37
8	89.01	66.06	0.71	1.40	0.70	1.43	0		1	.
8	90.01	64.93	0.72	1.39	0.72	1.39	1	1	0	1.43
8	91.01	67.46	0.72	1.39	0.72	1.39	0		1	.
8	93.01	69.20	0.74	1.36	0.72	1.39	0		0	.
8	94.01	70.73	0.73	1.36	0.72	1.39	0		0	.
8	95.01	71.90	0.74	1.34	0.74	1.34	1	0	0	1.39
8	96.01	112.84	0.73	1.36	0.74	1.34	0		1	.
8	97.01	75.41	0.73	1.38	0.74	1.34	0		0	.
8	98.01	73.37	0.71	1.40	0.71	1.40	1	0	0	1.34
8	99.01	71.23	0.71	1.42	0.71	1.40	0		1	.
8	100.01	69.40	0.72	1.38	0.72	1.38	1	1	0	1.40
8	101.01	79.11	0.72	1.40	0.72	1.38	0		1	.
8	102.01	80.84	0.72	1.39	0.72	1.39	1	1	0	1.38
8	103.01	78.01	0.70	1.43	0.70	1.43	1	1	0	1.39
8	104.01	82.68	0.69	1.46	0.70	1.43	0		1	.
8	105.01	84.61	0.67	1.48	0.70	1.43	0		0	.
8	106.01	80.11	0.68	1.48	0.70	1.43	0		0	.
8	107.01	81.81	0.68	1.46	0.68	1.46	1	0	0	1.43
8	109.01	82.78	0.67	1.50	0.67	1.50	1	1	0	1.46
8	110.01	85.48	0.66	1.51	0.67	1.50	0		1	.
8	111.01	90.95	0.66	1.51	0.67	1.50	0		0	.
8	112.01	226.76	0.67	1.50	0.67	1.50	0		0	.
8	113.01	154.08	0.67	1.49	0.67	1.50	0		0	.
8	114.01	91.09	0.67	1.50	0.67	1.50	1	1	0	1.50
8	115.01	93.06	0.66	1.50	0.67	1.50	0		1	.
8	116.01	96.03	0.66	1.51	0.66	1.51	1	0	0	1.50
8	117.01	85.88	0.66	1.52	0.66	1.51	0		1	.
8	118.01	99.93	0.66	1.52	0.66	1.52	1	1	0	1.51
8	119.01	102.47	0.66	1.52	0.66	1.52	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	120.01	0	1	0	0	2	118	0	1.96	1	58.59
8	121.01	1	1	1	0	1	118	0	1.96	1	85.88
8	122.01	0	.	1	0	.	122	0	1.96	1	85.88
8	123.01	1	.	1	0	.	123	0	1.78	1	126.82
8	124.01	1	0	0	0	1	123	0	1.78	1	126.82
8	125.01	0	1	1	1	1	123	0	1.96	1	126.82
8	126.01	0	0	0	1	2	123	0	1.96	1	85.88
8	127.01	1	.	0	0	2	127	0	2.14	1	126.82
8	128.01	1	0	0	0	2	127	0	2.14	1	85.88
8	129.01	0	.	1	0	2	129	0	2.14	1	44.94
8	130.01	1	1	0	0	1	129	0	2.14	1	58.59
8	131.01	0	1	0	0	1	129	0	2.49	2	44.94
8	132.01	1	1	1	0	1	129	0	2.49	1	154.11
8	133.01	0	1	1	0	2	129	0	2.49	1	126.82
8	134.01	1	.	1	0	1	134	0	2.32	0	126.82
8	135.01	0	1	1	0	1	134	0	2.49	0	126.82
8	136.01	1	1	1	0	1	134	0	2.32	1	126.82
8	137.01	1	.	1	0	2	137	0	1.78	1	85.88
8	138.01	0	1	1	0	2	137	0	1.78	1	85.88
8	139.01	0	0	0	0	2	137	0	1.78	1	154.11
8	140.01	1	1	1	0	1	137	0	2.14	1	154.11
8	141.01	0	.	0	0	2	141	0	1.96	1	154.11
8	142.01	0	0	0	0	1	141	0	1.96	2	154.11
8	143.01	1	1	1	0	2	141	0	2.14	1	154.11
8	144.01	1	.	1	0	3	144	0	2.14	1	154.11
8	145.01	0	1	1	0	1	144	0	2.32	2	154.11
8	146.01	1	1	1	0	1	144	0	2.32	1	72.24
8	147.01	0	1	0	0	1	144	0	2.14	1	167.75
8	148.01	0	0	0	0	1	144	0	1.96	1	167.75
8	149.01	0	0	0	0	1	144	0	2.14	1	99.53
8	150.01	1	1	1	0	2	144	0	1.96	0	99.53
8	151.01	0	1	0	0	1	144	0	1.78	1	154.11
8	152.01	1	1	1	0	1	144	0	2.14	2	154.11
8	153.01	0	1	1	0	1	144	0	2.49	1	85.88
8	154.01	0	0	0	0	2	144	0	2.49	1	126.82
8	155.01	1	1	1	0	1	144	0	2.67	2	126.82
8	156.01	1	0	1	0	1	144	0	2.67	1	58.59
8	157.01	1	0	0	0	1	144	0	2.85	1	44.94
8	158.01	1	0	1	1	1	144	0	2.85	1	58.59
8	159.01	1	.	1	0	3	159	0	2.14	1	167.75
8	160.01	1	0	0	0	1	159	0	2.49	0	154.11
8	161.01	0	1	0	0	1	159	0	2.32	1	154.11
8	162.01	0	0	0	0	1	159	0	2.32	2	167.75
8	163.01	1	1	0	0	1	159	0	2.32	1	154.11
8	164.01	1	0	1	0	1	159	0	2.32	1	167.75
8	165.01	0	1	0	0	2	159	0	2.49	1	154.11
8	166.01	1	1	0	0	1	159	0	2.49	0	154.11
8	167.01	0	.	1	0	.	167	0	1.43	1	126.82
8	168.01	1	1	1	0	1	167	0	1.60	2	126.82
8	169.01	0	1	1	0	1	167	0	1.96	1	126.82

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	120.01	173.47	0.66	1.52	0.66	1.52	0		0	.
8	121.01	107.10	0.65	1.53	0.66	1.52	0		0	.
8	122.01	104.93	0.68	1.48	0.68	1.48	1	0	0	1.52
8	123.01	69.86	0.67	1.49	0.67	1.49	1	1	0	1.48
8	124.01	71.27	0.68	1.48	0.67	1.49	0		1	.
8	125.01	73.10	0.68	1.48	0.67	1.49	0		0	.
8	126.01	112.28	0.67	1.49	0.67	1.49	0		0	.
8	127.01	75.00	0.68	1.48	0.68	1.48	1	1	0	1.49
8	128.01	115.95	0.67	1.49	0.68	1.48	0		1	.
8	129.01	257.23	0.67	1.50	0.67	1.50	1	0	0	1.48
8	130.01	166.53	0.66	1.52	0.67	1.50	0		1	.
8	131.01	259.13	0.66	1.51	0.67	1.50	0		0	.
8	132.01	58.46	0.66	1.52	0.67	1.50	0		0	.
8	133.01	79.81	0.65	1.55	0.67	1.50	0		0	.
8	134.01	87.15	0.66	1.50	0.66	1.50	1	1	0	1.50
8	135.01	78.14	0.65	1.53	0.66	1.50	0		1	.
8	136.01	89.28	0.66	1.52	0.66	1.50	0		0	.
8	137.01	129.59	0.66	1.52	0.66	1.52	1	0	0	1.50
8	138.01	132.20	0.66	1.52	0.66	1.52	0		1	.
8	139.01	67.53	0.65	1.55	0.66	1.52	0		0	.
8	140.01	69.50	0.64	1.55	0.66	1.52	0		0	.
8	141.01	70.94	0.63	1.59	0.63	1.59	1	0	0	1.52
8	142.01	72.17	0.64	1.56	0.63	1.59	0		1	.
8	143.01	74.04	0.64	1.57	0.63	1.59	0		0	.
8	144.01	75.91	0.63	1.59	0.63	1.59	1	0	0	1.59
8	145.01	77.28	0.63	1.58	0.63	1.59	0		1	.
8	146.01	250.95	0.63	1.60	0.63	1.59	0		0	.
8	147.01	50.62	0.62	1.61	0.63	1.59	0		0	.
8	148.01	51.92	0.63	1.58	0.63	1.59	0		0	.
8	149.01	146.21	0.63	1.58	0.63	1.59	0		0	.
8	150.01	147.74	0.64	1.57	0.63	1.59	0		0	.
8	151.01	88.42	0.63	1.60	0.63	1.59	0		0	.
8	152.01	87.52	0.63	1.59	0.63	1.59	0		0	.
8	153.01	158.59	0.63	1.60	0.63	1.59	0		0	.
8	154.01	130.16	0.63	1.60	0.63	1.59	0		0	.
8	155.01	113.71	0.62	1.60	0.63	1.59	0		0	.
8	156.01	269.80	0.64	1.57	0.63	1.59	0		0	.
8	157.01	303.07	0.65	1.55	0.63	1.59	0		0	.
8	158.01	271.27	0.64	1.55	0.63	1.59	0		0	.
8	159.01	69.14	0.65	1.55	0.65	1.55	1	0	0	1.59
8	160.01	96.30	0.64	1.56	0.65	1.55	0		1	.
8	161.01	97.80	0.64	1.57	0.65	1.55	0		0	.
8	162.01	70.40	0.62	1.60	0.65	1.55	0		0	.
8	163.01	101.10	0.63	1.60	0.65	1.55	0		0	.
8	164.01	72.01	0.61	1.63	0.65	1.55	0		0	.
8	165.01	105.67	0.65	1.53	0.65	1.55	0		0	.
8	166.01	104.94	0.65	1.54	0.65	1.55	0		0	.
8	167.01	139.80	0.65	1.53	0.65	1.53	1	0	0	1.55
8	168.01	140.24	0.63	1.59	0.65	1.53	0		1	.
8	169.01	142.07	0.64	1.56	0.65	1.53	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	170.01	0	.	0	0	.	170	0	1.60	0	140.46
8	171.01	0	0	0	0	1	170	0	1.78	1	208.69
8	172.01	0	0	0	0	1	170	0	1.78	1	208.69
8	173.01	0	0	0	0	1	170	0	1.96	1	154.11
8	174.01	0	0	0	0	1	170	0	1.96	2	154.11
8	175.01	0	0	1	0	1	170	0	2.14	1	85.88
8	176.01	1	1	0	0	2	170	0	2.14	1	140.46
8	177.01	1	0	0	0	1	170	0	2.32	1	140.46
8	178.01	1	0	0	0	1	170	0	2.49	0	140.46
8	179.01	1	0	1	0	1	170	0	2.67	1	140.46
8	180.01	0	1	1	1	2	170	0	2.85	1	85.88
8	181.01	0	.	1	0	2	181	0	2.49	1	154.11
8	182.01	1	1	1	0	1	181	0	2.49	1	222.34
8	183.01	0	1	0	0	1	181	0	2.49	1	222.34
8	184.01	1	1	1	0	1	181	0	2.49	2	222.34
8	185.01	1	0	0	0	1	181	0	2.32	1	140.46
8	186.01	1	0	1	0	1	181	0	2.32	1	181.40
8	187.01	0	1	0	0	2	181	0	2.32	1	181.40
8	188.01	0	.	0	0	2	188	0	2.32	1	140.46
8	189.01	1	.	1	0	2	189	0	1.96	1	140.46
8	190.01	0	1	1	0	1	189	0	1.96	1	154.11
8	191.01	1	.	1	0	1	191	0	1.96	1	167.75
8	192.01	1	0	1	0	1	191	0	1.96	1	181.40
8	193.01	0	1	0	0	2	191	0	2.14	1	208.69
8	194.01	0	0	0	0	1	191	0	2.14	0	208.69
8	195.01	1	1	1	0	1	191	0	2.14	1	154.11
8	196.01	1	0	1	0	1	191	0	2.14	1	154.11
8	197.01	0	.	0	0	2	197	0	2.14	1	208.69
8	198.01	0	.	1	1	2	198	0	2.14	1	208.69
8	199.01	0	0	0	0	2	198	0	1.78	1	154.11
8	200.01	1	.	1	0	2	200	0	1.78	1	154.11
8	201.01	1	0	1	0	1	200	0	1.96	2	154.11
8	202.01	1	0	1	0	1	200	0	2.14	1	154.11
8	203.01	1	0	1	0	2	200	0	2.14	1	154.11
8	204.01	0	1	1	1	2	200	0	2.14	1	208.69
8	205.01	1	1	1	0	1	200	0	2.32	1	140.46
8	206.01	0	.	1	0	2	206	0	1.96	1	167.75
8	207.01	1	1	0	0	1	206	0	1.96	0	222.34
8	208.01	1	0	1	0	1	206	0	1.78	1	58.59
8	209.01	1	0	1	0	1	206	0	2.14	2	58.59
8	210.01	1	.	0	0	2	210	0	2.14	1	181.40
8	211.01	0	.	1	0	2	211	0	2.14	1	195.05
8	212.01	0	0	0	0	1	211	0	2.32	2	195.05
8	213.01	1	1	1	0	1	211	0	2.49	1	167.75
8	214.01	0	1	0	0	2	211	0	2.32	1	195.05
8	215.01	1	1	1	0	1	211	0	2.14	0	195.05
8	216.01	0	1	0	1	1	211	0	2.32	0	208.69
8	217.01	0	0	0	1	2	211	0	1.96	0	208.69
8	218.01	0	0	1	1	1	211	0	1.78	1	208.69
8	219.01	0	0	0	0	2	211	0	1.60	1	222.34

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	170.01	107.94	0.64	1.56	0.64	1.56	1	0	0	1.53
8	171.01	57.30	0.63	1.58	0.64	1.56	0		1	.
8	172.01	58.66	0.64	1.55	0.64	1.56	0		0	.
8	173.01	110.54	0.65	1.54	0.64	1.56	0		0	.
8	174.01	112.58	0.66	1.52	0.64	1.56	0		0	.
8	175.01	223.92	0.65	1.53	0.64	1.56	0		0	.
8	176.01	119.62	0.66	1.52	0.64	1.56	0		0	.
8	177.01	114.18	0.66	1.52	0.64	1.56	0		0	.
8	178.01	117.15	0.67	1.49	0.64	1.56	0		0	.
8	179.01	122.22	0.68	1.48	0.64	1.56	0		0	.
8	180.01	267.80	0.67	1.49	0.64	1.56	0		0	.
8	181.01	114.21	0.67	1.48	0.67	1.48	1	0	0	1.56
8	182.01	40.47	0.67	1.49	0.67	1.48	0		1	.
8	183.01	41.51	0.67	1.49	0.67	1.48	0		0	.
8	184.01	42.71	0.67	1.48	0.67	1.48	0		0	.
8	185.01	125.76	0.67	1.49	0.67	1.48	0		0	.
8	186.01	92.73	0.67	1.50	0.67	1.48	0		0	.
8	187.01	94.33	0.67	1.49	0.67	1.48	0		0	.
8	188.01	128.43	0.66	1.50	0.66	1.50	1	0	0	1.48
8	189.01	131.63	0.66	1.52	0.66	1.52	1	0	0	1.50
8	190.01	128.79	0.66	1.50	0.66	1.52	0		1	.
8	191.01	95.43	0.66	1.52	0.66	1.52	1	0	0	1.52
8	192.01	95.93	0.66	1.52	0.66	1.52	0		1	.
8	193.01	72.88	0.66	1.52	0.66	1.52	0		0	.
8	194.01	74.15	0.66	1.51	0.66	1.52	0		0	.
8	195.01	139.01	0.66	1.51	0.66	1.52	0		0	.
8	196.01	141.31	0.65	1.53	0.66	1.52	0		0	.
8	197.01	75.85	0.65	1.54	0.65	1.54	1	1	0	1.52
8	198.01	77.92	0.65	1.53	0.65	1.53	1	1	0	1.54
8	199.01	148.68	0.64	1.56	0.65	1.53	0		1	.
8	200.01	150.05	0.64	1.57	0.64	1.57	1	1	0	1.53
8	201.01	151.42	0.65	1.55	0.64	1.57	0		1	.
8	202.01	152.92	0.65	1.55	0.64	1.57	0		0	.
8	203.01	154.25	0.66	1.52	0.64	1.57	0		0	.
8	204.01	81.65	0.66	1.52	0.64	1.57	0		0	.
8	205.01	159.89	0.66	1.51	0.64	1.57	0		0	.
8	206.01	114.25	0.66	1.51	0.66	1.51	1	1	0	1.57
8	207.01	69.53	0.66	1.51	0.66	1.51	0		1	.
8	208.01	354.12	0.66	1.53	0.66	1.51	0		0	.
8	209.01	356.62	0.66	1.53	0.66	1.51	0		0	.
8	210.01	113.88	0.64	1.55	0.64	1.55	1	1	0	1.51
8	211.01	99.37	0.65	1.53	0.65	1.53	1	1	0	1.55
8	212.01	97.87	0.65	1.55	0.65	1.53	0		1	.
8	213.01	129.26	0.65	1.54	0.65	1.53	0		0	.
8	214.01	100.87	0.65	1.53	0.65	1.53	0		0	.
8	215.01	102.14	0.65	1.55	0.65	1.53	0		0	.
8	216.01	112.95	0.67	1.50	0.65	1.53	0		0	.
8	217.01	116.69	0.66	1.52	0.65	1.53	0		0	.
8	218.01	118.56	0.66	1.52	0.65	1.53	0		0	.
8	219.01	113.68	0.65	1.54	0.65	1.53	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	220.01	1	.	1	0	.	220	0	1.43	1	235.98
8	221.01	0	1	1	0	2	220	0	1.60	0	58.59
8	222.01	1	1	1	0	2	220	0	1.78	1	195.05
8	223.01	1	0	0	0	2	220	0	1.43	1	195.05
8	224.01	0	1	0	0	1	220	0	1.78	1	195.05
8	225.01	0	0	1	1	1	220	0	1.96	1	195.05
8	226.01	1	.	1	0	1	226	0	1.96	1	222.34
8	227.01	1	0	1	0	1	226	0	1.96	2	222.34
8	228.01	0	1	1	0	2	226	0	2.14	1	222.34
8	229.01	0	0	1	0	1	226	0	2.14	0	222.34
8	230.01	0	0	1	0	1	226	0	2.14	0	140.46
8	231.01	0	.	1	0	2	231	0	2.14	1	208.69
8	232.01	0	0	1	0	2	231	0	1.78	0	208.69
8	233.01	0	0	1	0	2	231	0	1.96	1	31.30
8	234.01	0	.	0	0	2	234	0	1.78	1	154.11
8	235.01	1	1	1	0	1	234	0	1.78	2	154.11
8	237.01	0	.	0	0	.	237	0	0.89	0	235.98
8	238.01	1	.	1	0	.	238	0	0.36	0	113.17
8	239.01	0	.	1	0	.	239	0	0.36	1	235.98
8	240.01	0	0	1	0	2	239	0	0.71	1	235.98
8	241.01	0	.	1	0	.	241	0	0.36	1	17.65
8	243.01	0	.	1	0	.	243	0	0.36	1	58.59
8	244.01	0	0	1	0	2	243	0	0.71	1	99.53
8	248.01	0	.	1	0	.	248	0	0.36	1	44.94
8	17.02	1	.	1	0	.	17	0	0.36	1	4.01
8	18.02	0	.	1	0	.	18	0	0.36	1	44.94
8	19.02	0	.	0	0	.	19	0	0.71	1	44.94
8	20.02	0	.	0	0	.	20	0	0.53	1	44.94
8	23.02	0	.	0	1	3	23	0	0.71	1	44.94
8	25.02	0	.	0	0	3	25	0	1.07	1	44.94
8	26.02	0	.	0	1	.	26	0	0.89	1	44.94
8	29.02	0	.	0	0	.	29	0	0.89	1	4.01
8	32.02	1	.	1	0	.	32	0	1.25	1	4.01
8	33.02	1	.	0	0	.	33	0	1.78	1	4.01
8	34.02	0	1	0	0	2	33	0	1.60	1	4.01
8	35.02	0	.	0	0	.	35	0	0.89	1	44.94
8	36.02	1	.	0	0	2	36	0	1.25	1	44.94
8	37.02	0	.	0	0	2	37	0	1.43	1	44.94
8	39.02	1	.	1	0	2	39	0	1.60	1	44.94
8	40.02	1	.	1	0	3	40	0	1.60	1	44.94
8	42.02	1	.	1	0	.	42	0	0.53	1	4.01
8	43.02	1	0	0	0	2	42	0	0.89	1	4.01
8	44.02	1	.	1	0	.	44	0	0.89	1	44.94
8	45.02	0	1	0	0	1	44	0	1.60	1	4.01
8	46.02	1	1	1	0	1	44	0	1.96	1	4.01
8	47.02	1	0	1	0	1	44	0	1.60	2	44.94
8	48.02	1	0	1	0	2	44	0	1.96	0	44.94
8	49.02	1	.	1	0	1	49	0	1.96	1	4.01
8	50.02	0	.	0	0	2	50	0	2.14	1	4.01
8	51.02	1	.	1	0	.	51	0	1.96	1	44.94

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	220.01	114.58	0.64	1.57	0.64	1.57	1	0	0	1.53
8	221.01	379.38	0.63	1.58	0.64	1.57	0		1	.
8	222.01	137.14	0.63	1.59	0.64	1.57	0		0	.
8	223.01	139.31	0.62	1.60	0.64	1.57	0		0	.
8	224.01	142.51	0.61	1.64	0.64	1.57	0		0	.
8	225.01	144.05	0.62	1.62	0.64	1.57	0		0	.
8	226.01	117.62	0.62	1.61	0.62	1.61	1	1	0	1.57
8	227.01	119.15	0.62	1.61	0.62	1.61	0		1	.
8	228.01	120.15	0.62	1.61	0.62	1.61	0		0	.
8	229.01	139.50	0.61	1.63	0.62	1.61	0		0	.
8	230.01	228.16	0.61	1.64	0.62	1.61	0		0	.
8	231.01	193.00	0.60	1.66	0.60	1.66	1	1	0	1.61
8	232.01	194.83	0.60	1.66	0.60	1.66	0		1	.
8	233.01	436.61	0.61	1.65	0.60	1.66	0		0	.
8	234.01	243.94	0.60	1.65	0.60	1.65	1	0	0	1.66
8	235.01	282.72	0.61	1.65	0.60	1.65	0		1	.
8	237.01	274.17	0.78	1.28	0.78	1.28	1	0	0	1.65
8	238.01	439.33	1.20	0.83	1.20	0.83	1	0	0	1.28
8	239.01	424.76	1.14	0.87	1.14	0.87	1	0	0	0.83
8	240.01	426.36	1.14	0.88	1.14	0.87	0		1	.
8	241.01	733.20	0.96	1.04	0.96	1.04	1	0	0	0.87
8	243.01	945.18	1.63	0.61	1.63	0.61	1	0	0	1.04
8	244.01	721.68	1.61	0.62	1.63	0.61	0		1	.
8	248.01	1252.16	1.55	0.65	1.55	0.65	1	0	0	0.61
8	17.02	35.14	1.06	0.94	1.06	0.94	1	0	0	.
8	18.02	29.49	1.47	0.68	1.47	0.68	1	0	0	0.94
8	19.02	30.03	1.46	0.68	1.46	0.68	1	0	0	0.68
8	20.02	32.43	1.30	0.77	1.30	0.77	1	0	0	0.68
8	23.02	34.10	1.32	0.76	1.32	0.76	1	0	0	0.77
8	25.02	36.87	1.30	0.77	1.30	0.77	1	0	0	0.76
8	26.02	41.41	1.56	0.64	1.56	0.64	1	1	0	0.77
8	29.02	67.77	1.33	0.75	1.33	0.75	1	0	0	0.64
8	32.02	68.97	1.16	0.86	1.16	0.86	1	0	0	0.75
8	33.02	70.41	1.24	0.81	1.24	0.81	1	1	0	0.86
8	34.02	72.81	1.20	0.83	1.24	0.81	0		1	.
8	35.02	44.24	1.13	0.89	1.13	0.89	1	0	0	0.81
8	36.02	48.05	1.13	0.89	1.13	0.89	1	1	0	0.89
8	37.02	50.65	1.09	0.92	1.09	0.92	1	1	0	0.89
8	39.02	52.55	1.10	0.91	1.10	0.91	1	1	0	0.92
8	40.02	54.82	1.08	0.93	1.08	0.93	1	0	0	0.91
8	42.02	82.85	0.70	1.42	0.70	1.42	1	0	0	0.93
8	43.02	84.75	0.69	1.46	0.70	1.42	0		1	.
8	44.02	57.52	0.68	1.47	0.68	1.47	1	1	0	1.42
8	45.02	86.46	0.70	1.43	0.68	1.47	0		1	.
8	46.02	89.26	0.68	1.46	0.68	1.47	0		0	.
8	47.02	59.29	0.68	1.47	0.68	1.47	0		0	.
8	48.02	60.92	0.64	1.57	0.68	1.47	0		0	.
8	49.02	93.40	0.59	1.68	0.59	1.68	1	0	0	1.47
8	50.02	95.90	0.54	1.84	0.54	1.84	1	0	0	1.68
8	51.02	63.19	0.54	1.86	0.54	1.86	1	0	0	1.84

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	52.02	1	.	1	1	1	52	0	1.96	1	4.01
8	53.02	1	0	0	0	1	52	0	2.14	0	4.01
8	54.02	1	0	1	0	2	52	0	2.32	1	31.30
8	55.02	0	.	0	1	2	55	0	2.32	1	4.01
8	56.02	0	0	0	1	1	55	0	2.49	1	4.01
8	57.02	1	.	1	1	2	57	0	2.14	1	4.01
8	58.02	1	.	1	0	.	58	0	1.96	1	4.01
8	59.02	1	.	1	0	3	59	0	1.78	1	31.30
8	60.02	1	.	0	1	.	60	0	1.60	1	31.30
8	61.02	0	.	1	0	.	61	0	1.60	1	4.01
8	62.02	0	.	0	0	.	62	0	1.60	1	4.01
8	63.02	0	.	0	0	.	63	0	1.60	1	44.94
8	64.02	0	0	1	0	1	63	0	2.14	2	44.94
8	65.02	1	.	1	0	1	65	0	1.96	1	44.94
8	66.02	0	.	0	0	.	66	0	2.14	0	4.01
8	69.02	1	.	1	0	.	69	0	1.96	2	44.94
8	70.02	1	.	1	0	1	70	0	2.14	1	44.94
8	71.02	0	.	0	0	2	71	0	2.14	1	44.94
8	72.02	1	.	1	0	1	72	0	2.32	1	44.94
8	73.02	1	0	1	0	2	72	0	2.14	1	31.30
8	74.02	0	1	1	0	1	72	0	1.96	1	31.30
8	75.02	0	.	0	0	2	75	0	1.96	0	58.59
8	76.02	0	0	1	0	1	75	0	1.96	1	44.94
8	77.02	0	0	0	0	2	75	0	1.96	1	31.30
8	78.02	0	0	0	0	1	75	0	2.32	1	44.94
8	79.02	1	1	1	0	1	75	0	2.32	1	44.94
8	80.02	1	.	0	0	1	80	0	2.14	0	58.59
8	81.02	0	1	1	0	1	80	0	2.14	0	4.01
8	82.02	1	1	1	0	1	80	0	2.14	1	31.30
8	83.02	1	.	1	0	1	83	0	1.96	1	58.59
8	84.02	1	0	0	0	1	83	0	2.14	1	31.30
8	85.02	0	.	0	0	.	85	0	2.14	1	44.94
8	86.02	0	0	0	1	1	85	0	2.14	0	44.94
8	87.02	1	1	1	0	2	85	0	2.14	1	44.94
8	88.02	0	.	0	0	2	88	0	1.96	1	58.59
8	89.02	0	0	0	0	1	88	0	2.14	1	58.59
8	90.02	0	.	0	0	1	90	0	2.32	1	58.59
8	91.02	0	0	0	0	2	90	0	2.49	1	58.59
8	93.02	0	0	0	1	1	90	0	2.67	0	58.59
8	94.02	1	1	0	0	1	90	0	2.14	1	58.59
8	95.02	0	.	0	0	2	95	0	1.96	1	58.59
8	96.02	0	.	1	0	2	96	0	1.96	1	31.30
8	97.02	1	1	1	0	2	96	0	1.96	1	58.59
8	98.02	1	.	0	0	.	98	0	1.96	1	72.24
8	99.02	0	1	0	1	2	98	0	1.96	1	72.24
8	100.02	1	.	1	0	3	100	0	1.96	1	72.24
8	101.02	1	.	1	0	2	101	0	1.96	1	58.59
8	102.02	1	.	1	0	2	102	0	1.96	1	58.59
8	103.02	0	.	0	0	2	103	0	1.78	1	72.24
8	104.02	0	0	0	1	2	103	0	1.96	1	58.59

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	52.02	100.57	0.56	1.79	0.56	1.79	1	0	0	1.86
8	53.02	104.54	0.57	1.75	0.56	1.79	0		1	.
8	54.02	70.43	0.57	1.75	0.56	1.79	0		0	.
8	55.02	108.78	0.57	1.75	0.57	1.75	1	0	0	1.79
8	56.02	110.91	0.57	1.76	0.57	1.75	0		1	.
8	57.02	112.78	0.55	1.82	0.55	1.82	1	0	0	1.75
8	58.02	114.68	0.55	1.83	0.55	1.83	1	0	0	1.82
8	59.02	72.07	0.54	1.85	0.54	1.85	1	0	0	1.83
8	60.02	73.47	0.54	1.86	0.54	1.86	1	0	0	1.85
8	61.02	120.12	0.52	1.92	0.52	1.92	1	0	0	1.86
8	62.02	125.06	0.55	1.82	0.55	1.82	1	2	0	1.92
8	63.02	70.47	0.49	2.03	0.49	2.03	1	3	0	1.92
8	64.02	71.24	0.49	2.03	0.49	2.03	0		1	.
8	65.02	73.10	0.51	1.98	0.51	1.98	1	1	0	1.92
8	66.02	127.20	0.50	1.99	0.50	1.99	1	0	0	1.98
8	69.02	66.90	0.31	3.27	0.31	3.27	1	3	0	1.99
8	70.02	65.63	0.30	3.36	0.30	3.36	1	3	0	1.99
8	71.02	75.51	0.45	2.23	0.45	2.23	1	1	0	1.99
8	72.02	77.44	0.45	2.20	0.45	2.20	1	0	0	2.23
8	73.02	81.21	0.45	2.21	0.45	2.20	0		1	.
8	74.02	83.01	0.45	2.21	0.45	2.20	0		0	.
8	75.02	56.75	0.46	2.16	0.46	2.16	1	0	0	2.20
8	76.02	82.38	0.46	2.16	0.46	2.16	0		1	.
8	77.02	89.19	0.47	2.15	0.46	2.16	0		0	.
8	78.02	84.65	0.47	2.12	0.46	2.16	0		0	.
8	79.02	87.38	0.49	2.06	0.46	2.16	0		0	.
8	80.02	59.99	0.48	2.08	0.48	2.08	1	0	0	2.16
8	81.02	149.85	0.47	2.12	0.48	2.08	0		1	.
8	82.02	94.29	0.48	2.10	0.48	2.08	0		0	.
8	83.02	61.19	0.58	1.73	0.58	1.73	1	0	0	2.08
8	84.02	97.16	0.74	1.35	0.58	1.73	0		1	.
8	85.02	96.39	0.76	1.31	0.76	1.31	1	0	0	1.73
8	86.02	94.89	0.76	1.31	0.76	1.31	0		1	.
8	87.02	98.66	0.76	1.32	0.76	1.31	0		0	.
8	88.02	58.05	0.76	1.32	0.76	1.32	1	0	0	1.31
8	89.02	66.06	0.76	1.32	0.76	1.32	0		1	.
8	90.02	64.93	0.76	1.31	0.76	1.31	1	0	0	1.32
8	91.02	67.46	0.77	1.30	0.76	1.31	0		1	.
8	93.02	69.20	0.78	1.28	0.76	1.31	0		0	.
8	94.02	70.73	0.79	1.27	0.76	1.31	0		0	.
8	95.02	71.90	0.77	1.29	0.77	1.29	1	0	0	1.31
8	96.02	112.84	0.80	1.25	0.80	1.25	1	1	0	1.29
8	97.02	75.41	0.80	1.25	0.80	1.25	0		1	.
8	98.02	73.37	0.80	1.25	0.80	1.25	1	0	0	1.25
8	99.02	71.23	0.80	1.25	0.80	1.25	0		1	.
8	100.02	69.40	0.78	1.28	0.78	1.28	1	0	0	1.25
8	101.02	79.11	0.78	1.28	0.78	1.28	1	1	0	1.28
8	102.02	80.84	0.77	1.30	0.77	1.30	1	0	0	1.28
8	103.02	78.01	0.77	1.30	0.77	1.30	1	0	0	1.30
8	104.02	82.68	0.77	1.31	0.77	1.30	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	105.02	0	0	0	1	1	103	0	1.78	1	58.59
8	106.02	0	.	1	0	2	106	0	1.78	1	72.24
8	107.02	1	.	0	0	.	107	0	1.78	1	72.24
8	109.02	1	.	1	0	1	109	0	1.78	1	72.24
8	110.02	0	1	0	0	1	109	0	1.78	2	72.24
8	111.02	0	0	0	0	1	109	0	1.78	1	72.24
8	112.02	0	0	1	0	2	109	0	1.78	0	17.65
8	113.02	0	0	0	0	1	109	0	1.96	1	31.30
8	114.02	0	.	1	0	.	114	0	1.96	1	58.59
8	115.02	1	1	1	0	2	114	0	1.78	1	72.24
8	116.02	1	.	0	0	.	116	0	1.78	1	58.59
8	117.02	0	1	1	0	2	116	0	1.60	1	58.59
8	118.02	0	.	0	0	2	118	0	1.60	1	58.59
8	119.02	1	1	1	0	2	118	0	1.60	1	58.59
8	120.02	0	1	0	0	2	118	0	1.78	1	31.30
8	121.02	1	1	1	0	2	118	0	1.78	1	58.59
8	122.02	0	.	1	0	3	122	0	1.78	1	58.59
8	123.02	1	.	1	0	.	123	0	1.60	1	99.53
8	124.02	1	0	0	0	.	123	0	1.43	0	99.53
8	125.02	0	1	1	1	1	123	0	1.78	1	99.53
8	126.02	0	0	0	1	2	123	0	1.78	1	58.59
8	127.02	1	.	0	0	3	127	0	1.96	1	99.53
8	128.02	1	0	0	0	2	127	0	2.14	1	58.59
8	129.02	0	.	1	0	2	129	0	1.96	1	17.65
8	130.02	1	1	0	0	1	129	0	1.96	1	31.30
8	131.02	0	1	0	0	1	129	0	2.32	2	17.65
8	132.02	1	1	1	0	1	129	0	2.32	1	126.82
8	133.02	0	.	1	0	.	133	0	2.32	1	99.53
8	134.02	1	.	1	0	2	134	0	2.14	0	99.53
8	135.02	0	.	1	0	1	135	0	1.96	0	99.53
8	136.02	1	1	1	0	1	135	0	1.78	1	99.53
8	137.02	1	.	1	0	2	137	0	1.60	1	58.59
8	138.02	0	1	1	0	1	137	0	1.60	1	58.59
8	139.02	0	.	0	0	2	139	0	1.60	1	126.82
8	140.02	1	1	1	0	2	139	0	1.96	1	126.82
8	141.02	0	1	0	0	2	139	0	1.96	1	126.82
8	142.02	0	0	0	0	1	139	0	1.96	2	126.82
8	143.02	1	1	1	0	1	139	0	1.96	1	126.82
8	144.02	1	.	1	0	2	144	0	2.14	1	126.82
8	145.02	0	1	1	0	1	144	0	2.32	2	126.82
8	146.02	1	.	1	0	1	146	0	2.32	1	44.94
8	147.02	0	1	0	0	2	146	0	2.14	1	140.46
8	148.02	0	0	0	0	2	146	0	2.14	1	140.46
8	149.02	0	0	0	0	1	146	0	1.96	1	72.24
8	150.02	1	.	1	0	2	150	0	1.78	1	72.24
8	151.02	0	.	0	0	.	151	0	1.60	1	126.82
8	152.02	1	1	1	0	1	151	0	1.78	2	126.82
8	153.02	0	1	1	0	1	151	0	2.14	1	58.59
8	154.02	0	.	0	0	.	154	0	1.96	1	99.53
8	155.02	1	1	1	0	1	154	0	2.32	2	99.53

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	105.02	84.61	0.77	1.30	0.77	1.30	0		0	.
8	106.02	80.11	0.77	1.30	0.77	1.30	1	1	0	1.30
8	107.02	81.81	0.81	1.24	0.81	1.24	1	0	0	1.30
8	109.02	82.78	0.80	1.25	0.80	1.25	1	0	0	1.24
8	110.02	85.48	0.79	1.26	0.80	1.25	0		1	.
8	111.02	90.95	0.79	1.26	0.80	1.25	0		0	.
8	112.02	226.76	0.78	1.28	0.80	1.25	0		0	.
8	113.02	154.08	0.79	1.27	0.80	1.25	0		0	.
8	114.02	91.09	0.79	1.26	0.79	1.26	1	0	0	1.25
8	115.02	93.06	0.79	1.26	0.79	1.26	0		1	.
8	116.02	96.03	0.79	1.27	0.79	1.27	1	0	0	1.26
8	117.02	85.88	0.79	1.26	0.79	1.27	0		1	.
8	118.02	99.93	0.81	1.24	0.81	1.24	1	0	0	1.27
8	119.02	102.47	0.80	1.25	0.81	1.24	0		1	.
8	120.02	173.47	0.79	1.27	0.81	1.24	0		0	.
8	121.02	107.10	0.79	1.27	0.81	1.24	0		0	.
8	122.02	104.93	0.74	1.35	0.74	1.35	1	0	0	1.24
8	123.02	69.86	0.77	1.29	0.77	1.29	1	0	0	1.35
8	124.02	71.27	0.73	1.38	0.77	1.29	0		1	.
8	125.02	73.10	0.73	1.37	0.77	1.29	0		0	.
8	126.02	112.28	0.73	1.37	0.77	1.29	0		0	.
8	127.02	75.00	0.72	1.38	0.72	1.38	1	0	0	1.29
8	128.02	115.95	0.73	1.36	0.72	1.38	0		1	.
8	129.02	257.23	0.73	1.36	0.73	1.36	1	1	0	1.38
8	130.02	166.53	0.74	1.36	0.73	1.36	0		1	.
8	131.02	259.13	0.73	1.37	0.73	1.36	0		0	.
8	132.02	58.46	0.74	1.36	0.73	1.36	0		0	.
8	133.02	79.81	0.75	1.33	0.75	1.33	1	1	0	1.36
8	134.02	87.15	0.72	1.39	0.72	1.39	1	0	0	1.33
8	135.02	78.14	0.72	1.38	0.72	1.38	1	1	0	1.39
8	136.02	89.28	0.74	1.36	0.72	1.38	0		1	.
8	137.02	129.59	0.74	1.36	0.74	1.36	1	1	0	1.38
8	138.02	132.20	0.73	1.37	0.74	1.36	0		1	.
8	139.02	67.53	0.75	1.34	0.75	1.34	1	1	0	1.36
8	140.02	69.50	0.74	1.36	0.75	1.34	0		1	.
8	141.02	70.94	0.75	1.33	0.75	1.34	0		0	.
8	142.02	72.17	0.75	1.33	0.75	1.34	0		0	.
8	143.02	74.04	0.75	1.34	0.75	1.34	0		0	.
8	144.02	75.91	0.76	1.32	0.76	1.32	1	0	0	1.34
8	145.02	77.28	0.74	1.34	0.76	1.32	0		1	.
8	146.02	250.95	0.75	1.33	0.75	1.33	1	1	0	1.32
8	147.02	50.62	0.75	1.34	0.75	1.33	0		1	.
8	148.02	51.92	0.73	1.38	0.75	1.33	0		0	.
8	149.02	146.21	0.72	1.39	0.75	1.33	0		0	.
8	150.02	147.74	0.71	1.41	0.71	1.41	1	1	0	1.33
8	151.02	88.42	0.73	1.36	0.73	1.36	1	1	0	1.41
8	152.02	87.52	0.75	1.34	0.73	1.36	0		1	.
8	153.02	158.59	0.74	1.35	0.73	1.36	0		0	.
8	154.02	130.16	0.74	1.34	0.74	1.34	1	1	0	1.36
8	155.02	113.71	0.75	1.34	0.74	1.34	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	156.02	1	0	1	0	1	154	0	2.32	1	31.30
8	157.02	1	.	0	0	.	157	0	2.14	1	17.65
8	158.02	1	.	1	1	1	158	0	2.14	1	31.30
8	159.02	1	.	1	0	.	159	0	1.78	1	140.46
8	160.02	1	0	0	0	1	159	0	1.96	0	126.82
8	161.02	0	1	0	0	1	159	0	1.96	1	126.82
8	162.02	0	0	0	0	1	159	0	2.14	2	140.46
8	163.02	1	1	0	0	1	159	0	2.14	1	126.82
8	164.02	1	0	1	0	2	159	0	2.32	1	140.46
8	165.02	0	.	0	0	2	165	0	2.14	1	126.82
8	166.02	1	1	0	0	1	165	0	2.32	2	126.82
8	167.02	0	.	1	0	.	167	0	1.07	1	99.53
8	168.02	1	1	1	0	1	167	0	1.43	2	99.53
8	169.02	0	1	1	0	2	167	0	1.43	1	99.53
8	170.02	0	.	0	0	.	170	0	1.43	0	113.17
8	171.02	0	0	0	0	1	170	0	1.78	1	181.40
8	172.02	0	.	0	0	2	172	0	1.43	1	181.40
8	173.02	0	0	0	0	2	172	0	1.60	1	126.82
8	174.02	0	0	0	0	1	172	0	1.78	2	126.82
8	175.02	0	0	1	0	1	172	0	1.96	1	58.59
8	176.02	1	1	0	0	2	172	0	2.14	1	113.17
8	177.02	1	0	0	0	1	172	0	2.14	1	113.17
8	178.02	1	0	0	0	1	172	0	2.32	1	113.17
8	179.02	1	0	1	0	1	172	0	2.49	1	113.17
8	180.02	0	1	1	1	2	172	0	2.49	1	58.59
8	181.02	0	0	1	0	1	172	0	2.32	1	126.82
8	182.02	1	1	1	0	1	172	0	2.49	1	195.05
8	183.02	0	1	0	0	1	172	0	2.49	1	195.05
8	184.02	1	1	1	0	1	172	0	2.49	2	195.05
8	185.02	1	0	0	0	1	172	0	2.49	1	113.17
8	186.02	1	0	1	0	1	172	0	2.49	1	154.11
8	187.02	0	1	0	0	2	172	0	2.49	1	154.11
8	188.02	0	.	0	0	.	188	0	2.32	1	113.17
8	189.02	1	1	1	0	2	188	0	1.96	1	113.17
8	190.02	0	1	1	0	1	188	0	1.96	1	126.82
8	191.02	1	1	1	0	1	188	0	1.96	1	140.46
8	192.02	1	0	1	0	1	188	0	1.96	1	154.11
8	193.02	0	.	0	0	2	193	0	1.96	1	181.40
8	194.02	0	0	0	0	1	193	0	2.14	1	181.40
8	195.02	1	1	1	0	1	193	0	2.14	1	126.82
8	196.02	1	0	1	0	1	193	0	2.14	1	126.82
8	197.02	0	.	0	0	2	197	0	2.14	1	181.40
8	198.02	0	.	1	1	3	198	0	2.14	1	181.40
8	199.02	0	0	0	0	2	198	0	1.78	1	126.82
8	200.02	1	.	1	0	3	200	0	1.78	1	126.82
8	201.02	1	0	1	0	1	200	0	1.78	0	126.82
8	202.02	1	0	1	0	1	200	0	2.14	1	126.82
8	203.02	1	.	1	0	2	203	0	2.14	1	126.82
8	204.02	0	1	1	1	2	203	0	2.14	1	181.40
8	205.02	1	1	1	0	1	203	0	2.14	1	113.17

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	156.02	269.80	0.73	1.36	0.74	1.34	0		0	.
8	157.02	303.07	0.75	1.33	0.75	1.33	1	1	0	1.34
8	158.02	271.27	0.74	1.34	0.74	1.34	1	1	0	1.33
8	159.02	69.14	0.75	1.33	0.75	1.33	1	0	0	1.34
8	160.02	96.30	0.75	1.33	0.75	1.33	0		1	.
8	161.02	97.80	0.76	1.32	0.75	1.33	0		0	.
8	162.02	70.40	0.77	1.30	0.75	1.33	0		0	.
8	163.02	101.10	0.79	1.27	0.75	1.33	0		0	.
8	164.02	72.01	0.78	1.28	0.75	1.33	0		0	.
8	165.02	105.67	0.72	1.39	0.72	1.39	1	1	0	1.33
8	166.02	104.94	0.70	1.43	0.72	1.39	0		1	.
8	167.02	139.80	0.72	1.38	0.72	1.38	1	0	0	1.39
8	168.02	140.24	0.73	1.38	0.72	1.38	0		1	.
8	169.02	142.07	0.72	1.38	0.72	1.38	0		0	.
8	170.02	107.94	0.72	1.39	0.72	1.39	1	0	0	1.38
8	171.02	57.30	0.72	1.38	0.72	1.39	0		1	.
8	172.02	58.66	0.71	1.40	0.71	1.40	1	1	0	1.39
8	173.02	110.54	0.71	1.41	0.71	1.40	0		1	.
8	174.02	112.58	0.71	1.42	0.71	1.40	0		0	.
8	175.02	223.92	0.71	1.42	0.71	1.40	0		0	.
8	176.02	119.62	0.71	1.41	0.71	1.40	0		0	.
8	177.02	114.18	0.71	1.41	0.71	1.40	0		0	.
8	178.02	117.15	0.71	1.42	0.71	1.40	0		0	.
8	179.02	122.22	0.71	1.42	0.71	1.40	0		0	.
8	180.02	267.80	0.71	1.41	0.71	1.40	0		0	.
8	181.02	114.21	0.71	1.41	0.71	1.40	0		0	.
8	182.02	40.47	0.71	1.42	0.71	1.40	0		0	.
8	183.02	41.51	0.70	1.43	0.71	1.40	0		0	.
8	184.02	42.71	0.70	1.43	0.71	1.40	0		0	.
8	185.02	125.76	0.70	1.43	0.71	1.40	0		0	.
8	186.02	92.73	0.70	1.43	0.71	1.40	0		0	.
8	187.02	94.33	0.70	1.43	0.71	1.40	0		0	.
8	188.02	128.43	0.69	1.44	0.69	1.44	1	1	0	1.40
8	189.02	131.63	0.70	1.44	0.69	1.44	0		1	.
8	190.02	128.79	0.69	1.45	0.69	1.44	0		0	.
8	191.02	95.43	0.69	1.45	0.69	1.44	0		0	.
8	192.02	95.93	0.69	1.45	0.69	1.44	0		0	.
8	193.02	72.88	0.68	1.47	0.68	1.47	1	1	0	1.44
8	194.02	74.15	0.68	1.47	0.68	1.47	0		1	.
8	195.02	139.01	0.67	1.48	0.68	1.47	0		0	.
8	196.02	141.31	0.68	1.47	0.68	1.47	0		0	.
8	197.02	75.85	0.67	1.48	0.67	1.48	1	0	0	1.47
8	198.02	77.92	0.67	1.50	0.67	1.50	1	0	0	1.48
8	199.02	148.68	0.67	1.49	0.67	1.50	0		1	.
8	200.02	150.05	0.68	1.48	0.68	1.48	1	0	0	1.50
8	201.02	151.42	0.67	1.49	0.68	1.48	0		1	.
8	202.02	152.92	0.67	1.49	0.68	1.48	0		0	.
8	203.02	154.25	0.66	1.52	0.66	1.52	1	1	0	1.48
8	204.02	81.65	0.66	1.51	0.66	1.52	0		1	.
8	205.02	159.89	0.66	1.52	0.66	1.52	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	206.02	0	.	1	0	3	206	0	1.96	1	140.46
8	207.02	1	1	0	0	1	206	0	1.96	0	195.05
8	208.02	1	.	1	0	1	208	0	1.78	1	31.30
8	209.02	1	.	1	0	1	209	0	2.14	2	31.30
8	210.02	1	.	0	0	.	210	0	1.96	1	154.11
8	211.02	0	.	1	0	3	211	0	1.96	1	167.75
8	212.02	0	0	0	0	1	211	0	1.96	2	167.75
8	213.02	1	1	1	0	1	211	0	2.32	1	140.46
8	214.02	0	.	0	0	2	214	0	1.96	1	167.75
8	215.02	1	1	1	0	1	214	0	2.14	2	167.75
8	216.02	0	1	0	1	1	214	0	2.14	1	181.40
8	217.02	0	.	0	1	2	217	0	1.96	0	181.40
8	218.02	0	0	1	1	1	217	0	1.96	1	181.40
8	219.02	0	0	0	0	1	217	0	1.78	1	195.05
8	220.02	1	.	1	0	.	220	0	1.60	1	208.69
8	221.02	0	1	1	0	2	220	0	1.60	0	31.30
8	222.02	1	.	1	0	2	222	0	1.78	1	167.75
8	223.02	1	.	0	0	2	223	0	1.43	1	167.75
8	224.02	0	1	0	0	1	223	0	1.78	1	167.75
8	225.02	0	0	1	1	1	223	0	1.78	1	167.75
8	226.02	1	.	1	0	.	226	0	1.78	1	195.05
8	227.02	1	0	1	0	1	226	0	1.96	2	195.05
8	228.02	0	.	1	0	.	228	0	1.96	1	195.05
8	229.02	0	.	1	0	1	229	0	1.96	2	195.05
8	230.02	0	0	1	0	1	229	0	1.96	1	113.17
8	231.02	0	.	1	0	3	231	0	1.78	1	181.40
8	232.02	0	0	1	0	2	231	0	1.78	0	181.40
8	233.02	0	0	1	0	2	231	0	1.96	1	4.01
8	234.02	0	0	0	0	2	231	0	1.78	1	126.82
8	235.02	1	1	1	0	2	231	0	1.78	2	126.82
8	237.02	0	.	0	0	.	237	0	0.53	0	208.69
8	238.02	1	.	1	0	.	238	0	0.53	0	85.88
8	239.02	0	.	1	0	.	239	0	0.36	1	208.69
8	240.02	0	0	1	0	2	239	0	0.71	1	208.69
8	243.02	0	.	1	0	.	243	0	0.36	1	31.30
8	244.02	0	0	1	0	2	243	0	0.71	1	72.24
8	248.02	0	.	1	0	.	248	0	0.36	1	17.65
8	18.03	0	.	1	0	.	18	0	0.36	1	17.65
8	19.03	0	.	0	0	.	19	0	0.71	1	17.65
8	20.03	0	.	0	0	.	20	0	0.89	1	17.65
8	23.03	0	.	0	1	2	23	0	1.07	1	17.65
8	25.03	0	.	0	0	.	25	0	1.07	1	17.65
8	26.03	0	.	0	1	.	26	0	0.71	0	17.65
8	35.03	0	.	0	0	.	35	0	0.71	1	17.65
8	36.03	1	.	0	0	.	36	0	1.07	1	17.65
8	37.03	0	.	0	0	.	37	0	1.25	1	17.65
8	39.03	1	.	1	0	3	39	0	1.25	1	17.65
8	40.03	1	.	1	0	3	40	0	1.43	1	17.65
8	44.03	1	.	1	0	.	44	0	0.89	1	17.65
8	47.03	1	.	1	0	1	47	0	1.25	0	17.65

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	206.02	114.25	0.65	1.53	0.65	1.53	1	0	0	1.52
8	207.02	69.53	0.66	1.50	0.65	1.53	0		1	.
8	208.02	354.12	0.67	1.50	0.67	1.50	1	1	0	1.53
8	209.02	356.62	0.66	1.53	0.66	1.53	1	3	0	1.50
8	210.02	113.88	0.68	1.47	0.68	1.47	1	0	0	1.50
8	211.02	99.37	0.68	1.48	0.68	1.48	1	0	0	1.47
8	212.02	97.87	0.69	1.46	0.68	1.48	0		1	.
8	213.02	129.26	0.68	1.47	0.68	1.48	0		0	.
8	214.02	100.87	0.66	1.51	0.66	1.51	1	1	0	1.48
8	215.02	102.14	0.67	1.50	0.66	1.51	0		1	.
8	216.02	112.95	0.65	1.55	0.66	1.51	0		0	.
8	217.02	116.69	0.65	1.53	0.65	1.53	1	1	0	1.51
8	218.02	118.56	0.66	1.51	0.65	1.53	0		1	.
8	219.02	113.68	0.65	1.54	0.65	1.53	0		0	.
8	220.02	114.58	0.65	1.54	0.65	1.54	1	0	0	1.53
8	221.02	379.38	0.65	1.54	0.65	1.54	0		1	.
8	222.02	137.14	0.65	1.55	0.65	1.55	1	1	0	1.54
8	223.02	139.31	0.65	1.54	0.65	1.54	1	1	0	1.55
8	224.02	142.51	0.66	1.51	0.65	1.54	0		1	.
8	225.02	144.05	0.66	1.52	0.65	1.54	0		0	.
8	226.02	117.62	0.65	1.54	0.65	1.54	1	1	0	1.54
8	227.02	119.15	0.65	1.54	0.65	1.54	0		1	.
8	228.02	120.15	0.67	1.50	0.67	1.50	1	1	0	1.54
8	229.02	139.50	0.67	1.49	0.67	1.49	1	1	0	1.50
8	230.02	228.16	0.66	1.50	0.67	1.49	0		1	.
8	231.02	193.00	0.67	1.49	0.67	1.49	1	0	0	1.49
8	232.02	194.83	0.67	1.50	0.67	1.49	0		1	.
8	233.02	436.61	0.65	1.54	0.67	1.49	0		0	.
8	234.02	243.94	0.65	1.54	0.67	1.49	0		0	.
8	235.02	282.72	0.63	1.58	0.67	1.49	0		0	.
8	237.02	274.17	0.98	1.02	0.98	1.02	1	0	0	1.49
8	238.02	439.33	1.22	0.82	1.22	0.82	1	0	0	1.02
8	239.02	424.76	1.08	0.93	1.08	0.93	1	0	0	0.82
8	240.02	426.36	1.11	0.90	1.08	0.93	0		1	.
8	243.02	945.18	1.61	0.62	1.61	0.62	1	0	0	0.93
8	244.02	721.68	1.63	0.62	1.61	0.62	0		1	.
8	248.02	1252.16	1.79	0.56	1.79	0.56	1	0	0	0.62
8	18.03	29.49	1.59	0.63	1.59	0.63	1	0	0	.
8	19.03	30.03	1.43	0.70	1.43	0.70	1	0	0	0.63
8	20.03	32.43	1.27	0.79	1.27	0.79	1	0	0	0.70
8	23.03	34.10	1.23	0.81	1.23	0.81	1	0	0	0.79
8	25.03	36.87	1.26	0.79	1.26	0.79	1	0	0	0.81
8	26.03	41.41	1.25	0.80	1.25	0.80	1	0	0	0.79
8	35.03	44.24	0.96	1.05	0.96	1.05	1	0	0	0.80
8	36.03	48.05	1.02	0.98	1.02	0.98	1	0	0	1.05
8	37.03	50.65	1.13	0.88	1.13	0.88	1	0	0	0.98
8	39.03	52.55	1.14	0.88	1.14	0.88	1	0	0	0.88
8	40.03	54.82	1.18	0.85	1.18	0.85	1	0	0	0.88
8	44.03	57.52	0.94	1.07	0.94	1.07	1	1	0	0.85
8	47.03	59.29	0.82	1.21	0.82	1.21	1	1	0	1.07

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	48.03	1	0	1	0	2	47	0	1.60	1	17.65
8	51.03	1	.	1	0	2	51	0	1.78	1	17.65
8	54.03	1	.	1	0	2	54	0	1.78	1	4.01
8	59.03	1	.	1	0	3	59	0	2.32	1	4.01
8	60.03	1	0	0	1	1	59	0	2.14	1	4.01
8	63.03	0	.	0	0	.	63	0	1.78	1	17.65
8	64.03	0	0	1	0	1	63	0	2.32	2	17.65
8	65.03	1	.	1	0	1	65	0	2.32	1	17.65
8	69.03	1	0	1	0	1	70	0	1.96	2	17.65
8	70.03	1	.	1	0	1	70	0	1.78	1	17.65
8	71.03	0	.	0	0	2	71	0	2.32	1	17.65
8	72.03	1	1	1	0	1	71	0	2.67	1	17.65
8	73.03	1	0	1	0	1	71	0	2.49	1	4.01
8	74.03	0	1	1	0	1	71	0	2.32	1	4.01
8	75.03	0	0	0	0	2	71	0	2.14	2	31.30
8	76.03	0	0	1	0	1	71	0	2.32	1	17.65
8	77.03	0	0	0	0	2	71	0	2.32	1	4.01
8	78.03	0	0	0	0	1	71	0	2.49	1	17.65
8	79.03	1	1	1	0	1	71	0	2.49	1	17.65
8	80.03	1	.	0	0	1	80	0	2.32	0	31.30
8	82.03	1	.	1	0	1	82	0	2.32	1	4.01
8	83.03	1	0	1	0	1	82	0	2.32	1	31.30
8	84.03	1	0	0	0	1	82	0	2.49	1	4.01
8	85.03	0	.	0	0	1	85	0	2.67	0	17.65
8	86.03	0	.	0	1	1	86	0	2.67	1	17.65
8	87.03	1	.	1	0	2	87	0	2.67	1	17.65
8	88.03	0	1	0	0	2	87	0	2.49	1	31.30
8	89.03	0	0	0	0	1	87	0	2.67	2	31.30
8	90.03	0	0	0	0	1	87	0	2.67	1	31.30
8	91.03	0	0	0	0	1	87	0	3.03	1	31.30
8	93.03	0	0	0	1	1	87	0	3.21	2	31.30
8	94.03	1	1	0	0	1	87	0	2.67	1	31.30
8	95.03	0	1	0	0	1	87	0	2.49	0	31.30
8	96.03	0	.	1	0	.	96	0	2.32	1	4.01
8	97.03	1	1	1	0	1	96	0	2.49	1	31.30
8	98.03	1	.	0	0	1	98	0	2.67	1	44.94
8	99.03	0	.	0	1	1	99	0	2.67	0	44.94
8	100.03	1	.	1	0	2	100	0	2.49	1	44.94
8	101.03	1	.	1	0	2	101	0	2.49	1	31.30
8	102.03	1	0	1	0	2	101	0	2.32	1	31.30
8	103.03	0	1	0	0	2	101	0	2.32	1	44.94
8	104.03	0	0	0	1	2	101	0	2.32	1	31.30
8	105.03	0	0	0	1	2	101	0	2.14	1	31.30
8	106.03	0	.	1	0	2	106	0	1.96	1	44.94
8	107.03	1	.	0	0	.	107	0	2.14	1	44.94
8	109.03	1	0	1	0	1	107	0	1.96	0	44.94
8	110.03	0	1	0	0	1	107	0	2.14	2	44.94
8	111.03	0	0	0	0	1	107	0	2.14	0	44.94
8	113.03	0	.	0	0	1	113	0	2.32	1	4.01
8	114.03	0	.	1	0	.	114	0	2.49	1	31.30

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	48.03	60.92	0.82	1.21	0.82	1.21	0		1	.
8	51.03	63.19	0.76	1.32	0.76	1.32	1	1	0	1.21
8	54.03	70.43	0.71	1.41	0.71	1.41	1	1	0	1.28
8	59.03	72.07	0.59	1.70	0.59	1.70	1	0	0	1.41
8	60.03	73.47	0.58	1.71	0.59	1.70	0		1	.
8	63.03	70.47	0.56	1.79	0.56	1.79	1	0	0	1.70
8	64.03	71.24	0.56	1.80	0.56	1.79	0		1	.
8	65.03	73.10	0.53	1.90	0.53	1.90	1	4	0	1.79
8	69.03	66.90	0.79	1.27	0.78	1.28	0		1	.
8	70.03	65.63	0.78	1.28	0.78	1.28	1	1	0	1.32
8	71.03	75.51	0.50	2.00	0.50	2.00	1	4	0	1.90
8	72.03	77.44	0.50	2.00	0.50	2.00	0		1	.
8	73.03	81.21	0.49	2.04	0.50	2.00	0		0	.
8	74.03	83.01	0.49	2.05	0.50	2.00	0		0	.
8	75.03	56.75	0.48	2.09	0.50	2.00	0		0	.
8	76.03	82.38	0.48	2.08	0.50	2.00	0		0	.
8	77.03	89.19	0.48	2.09	0.50	2.00	0		0	.
8	78.03	84.65	0.47	2.13	0.50	2.00	0		0	.
8	79.03	87.38	0.46	2.18	0.50	2.00	0		0	.
8	80.03	59.99	0.46	2.16	0.46	2.16	1	1	0	2.00
8	82.03	94.29	0.45	2.22	0.45	2.22	1	4	0	2.16
8	83.03	61.19	0.38	2.61	0.45	2.22	0		1	.
8	84.03	97.16	0.33	3.00	0.45	2.22	0		0	.
8	85.03	96.39	0.33	3.07	0.33	3.07	1	2	0	2.22
8	86.03	94.89	0.32	3.15	0.32	3.15	1	3	0	2.22
8	87.03	98.66	0.32	3.11	0.32	3.11	1	1	0	2.22
8	88.03	58.05	0.32	3.13	0.32	3.11	0		1	.
8	89.03	66.06	0.32	3.17	0.32	3.11	0		0	.
8	90.03	64.93	0.31	3.20	0.32	3.11	0		0	.
8	91.03	67.46	0.31	3.20	0.32	3.11	0		0	.
8	93.03	69.20	0.31	3.27	0.32	3.11	0		0	.
8	94.03	70.73	0.30	3.28	0.32	3.11	0		0	.
8	95.03	71.90	0.30	3.30	0.32	3.11	0		0	.
8	96.03	112.84	0.30	3.31	0.30	3.31	1	0	0	3.11
8	97.03	75.41	0.30	3.29	0.30	3.31	0		1	.
8	98.03	73.37	0.31	3.21	0.31	3.21	1	2	0	3.31
8	99.03	71.23	0.30	3.34	0.30	3.34	1	3	0	3.31
8	100.03	69.40	0.30	3.33	0.30	3.33	1	0	0	3.31
8	101.03	79.11	0.30	3.30	0.30	3.30	1	0	0	3.33
8	102.03	80.84	0.30	3.30	0.30	3.30	0		1	.
8	103.03	78.01	0.31	3.27	0.30	3.30	0		0	.
8	104.03	82.68	0.37	2.72	0.30	3.30	0		0	.
8	105.03	84.61	0.37	2.69	0.30	3.30	0		0	.
8	106.03	80.11	0.37	2.67	0.37	2.67	1	0	0	3.30
8	107.03	81.81	0.37	2.70	0.37	2.70	1	0	0	2.67
8	109.03	82.78	0.37	2.71	0.37	2.70	0		1	.
8	110.03	85.48	0.37	2.70	0.37	2.70	0		0	.
8	111.03	90.95	0.37	2.69	0.37	2.70	0		0	.
8	113.03	154.08	0.36	2.76	0.36	2.76	1	4	0	2.70
8	114.03	91.09	0.36	2.77	0.36	2.77	1	0	0	2.76

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	115.03	1	1	1	0	2	114	0	2.49	1	44.94
8	116.03	1	.	0	0	1	116	0	2.14	1	31.30
8	117.03	0	.	1	0	2	117	0	1.96	1	31.30
8	118.03	0	.	0	0	2	118	0	1.78	1	31.30
8	119.03	1	1	1	0	1	118	0	1.78	0	31.30
8	120.03	0	1	0	0	1	118	0	1.78	1	4.01
8	121.03	1	1	1	0	1	118	0	1.96	0	31.30
8	122.03	0	.	1	0	1	122	0	1.96	1	31.30
8	123.03	1		1	0	1	123	0	1.96	1	72.24
8	124.03	1	0	0	0	.	123	0	1.78	0	72.24
8	125.03	0	1	1	1	1	123	0	1.96	1	72.24
8	126.03	0	0	0	1	1	123	0	1.78	1	31.30
8	127.03	1	.	0	0	1	127	0	1.96	1	72.24
8	128.03	1	0	0	0	1	127	0	2.14	1	31.30
8	130.03	1	.	0	0	1	130	0	2.14	1	4.01
8	132.03	1	.	1	0	1	132	0	2.32	1	99.53
8	133.03	0	.	1	0	.	133	0	2.49	1	72.24
8	134.03	1	.	1	0	2	134	0	2.67	0	72.24
8	135.03	0	.	1	0	3	135	0	2.49	0	72.24
8	136.03	1	1	1	0	1	135	0	1.60	1	72.24
8	137.03	1	.	1	0	2	137	0	1.60	1	31.30
8	138.03	0	1	1	0	1	137	0	1.43	1	31.30
8	139.03	0	.	0	0	3	139	0	1.60	1	99.53
8	140.03	1	.	1	0	2	140	0	1.78	1	99.53
8	141.03	0	1	0	0	2	140	0	1.78	1	99.53
8	142.03	0	0	0	0	1	140	0	1.96	2	99.53
8	143.03	1	1	1	0	1	140	0	1.96	1	99.53
8	144.03	1	0	1	0	2	140	0	2.14	1	99.53
8	145.03	0	1	1	0	1	140	0	2.14	2	99.53
8	146.03	1	.	1	0	1	146	0	2.14	1	17.65
8	147.03	0	1	0	0	1	146	0	1.78	1	113.17
8	148.03	0	0	0	0	1	146	0	2.14	0	113.17
8	149.03	0	0	0	0	1	146	0	1.96	1	44.94
8	150.03	1	.	1	0	1	150	0	1.78	0	44.94
8	151.03	0	.	0	0	.	151	0	1.78	1	99.53
8	152.03	1	1	1	0	1	151	0	1.78	2	99.53
8	153.03	0	1	1	0	1	151	0	2.14	1	31.30
8	154.03	0	.	0	0	.	154	0	1.78	1	72.24
8	155.03	1	1	1	0	1	154	0	1.96	2	72.24
8	156.03	1	.	1	0	1	156	0	1.60	1	4.01
8	158.03	1	.	1	1	.	158	0	1.43	1	4.01
8	159.03	1	.	1	0	.	159	0	1.25	1	113.17
8	160.03	1	0	0	0	1	159	0	1.43	0	99.53
8	161.03	0	1	0	0	1	159	0	1.78	1	99.53
8	162.03	0	0	0	0	1	159	0	1.96	2	113.17
8	163.03	1	1	0	0	1	159	0	1.96	1	99.53
8	164.03	1	0	1	0	1	159	0	2.14	1	113.17
8	165.03	0	.	0	0	2	165	0	2.14	1	99.53
8	166.03	1	1	0	0	1	165	0	1.96	2	99.53
8	167.03	0	.	1	0	.	167	0	1.43	0	72.24

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	115.03	93.06	0.36	2.77	0.36	2.77	0		1	.
8	116.03	96.03	0.36	2.76	0.36	2.76	1	0	0	2.77
8	117.03	85.88	0.40	2.51	0.40	2.51	1	1	0	2.76
8	118.03	99.93	0.39	2.54	0.39	2.54	1	1	0	2.51
8	119.03	102.47	0.40	2.53	0.39	2.54	0		1	.
8	120.03	173.47	0.39	2.53	0.39	2.54	0		0	.
8	121.03	107.10	0.39	2.56	0.39	2.54	0		0	.
8	122.03	104.93	0.39	2.54	0.39	2.54	1	0	0	2.54
8	123.03	69.86	0.86	1.17	0.86	1.17	0		0	2.54
8	124.03	71.27	0.92	1.09	0.86	1.17	0		1	.
8	125.03	73.10	0.90	1.11	0.86	1.17	0		0	.
8	126.03	112.28	0.91	1.10	0.86	1.17	0		0	.
8	127.03	75.00	0.91	1.10	0.91	1.10	1	0	0	1.17
8	128.03	115.95	0.90	1.11	0.91	1.10	0		1	.
8	130.03	166.53	0.29	3.47	0.29	3.47	1	3	0	.
8	132.03	58.46	0.81	1.23	0.81	1.23	1	1	0	1.10
8	133.03	79.81	0.79	1.26	0.79	1.26	1	0	0	1.23
8	134.03	87.15	0.80	1.24	0.80	1.24	1	1	0	1.26
8	135.03	78.14	0.85	1.18	0.85	1.18	1	0	0	1.24
8	136.03	89.28	0.83	1.21	0.85	1.18	0		1	.
8	137.03	129.59	0.83	1.21	0.83	1.21	1	0	0	1.18
8	138.03	132.20	0.83	1.20	0.83	1.21	0		1	.
8	139.03	67.53	0.83	1.21	0.83	1.21	1	0	0	1.21
8	140.03	69.50	0.83	1.20	0.83	1.20	1	1	0	1.21
8	141.03	70.94	0.83	1.21	0.83	1.20	0		1	.
8	142.03	72.17	0.81	1.24	0.83	1.20	0		0	.
8	143.03	74.04	0.83	1.21	0.83	1.20	0		0	.
8	144.03	75.91	0.83	1.21	0.83	1.20	0		0	.
8	145.03	77.28	0.84	1.19	0.83	1.20	0		0	.
8	146.03	250.95	0.83	1.21	0.83	1.21	1	1	0	1.20
8	147.03	50.62	0.83	1.21	0.83	1.21	0		1	.
8	148.03	51.92	0.83	1.21	0.83	1.21	0		0	.
8	149.03	146.21	0.84	1.19	0.83	1.21	0		0	.
8	150.03	147.74	0.81	1.23	0.81	1.23	1	0	0	1.21
8	151.03	88.42	0.79	1.27	0.79	1.27	1	0	0	1.23
8	152.03	87.52	0.78	1.28	0.79	1.27	0		1	.
8	153.03	158.59	0.78	1.28	0.79	1.27	0		0	.
8	154.03	130.16	0.79	1.26	0.79	1.26	1	0	0	1.27
8	155.03	113.71	0.79	1.26	0.79	1.26	0		1	.
8	156.03	269.80	0.80	1.25	0.80	1.25	1	0	0	1.26
8	158.03	271.27	0.84	1.19	0.84	1.19	1	0	0	1.25
8	159.03	69.14	0.82	1.22	0.82	1.22	1	0	0	1.19
8	160.03	96.30	0.81	1.23	0.82	1.22	0		1	.
8	161.03	97.80	0.80	1.25	0.82	1.22	0		0	.
8	162.03	70.40	0.80	1.25	0.82	1.22	0		0	.
8	163.03	101.10	0.78	1.29	0.82	1.22	0		0	.
8	164.03	72.01	0.79	1.27	0.82	1.22	0		0	.
8	165.03	105.67	0.79	1.27	0.79	1.27	1	0	0	1.22
8	166.03	104.94	0.79	1.26	0.79	1.27	0		1	.
8	167.03	139.80	0.75	1.34	0.75	1.34	1	0	0	1.27

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	168.03	1	1	1	0	1	167	0	1.60	0	72.24
8	169.03	0	.	1	0	.	169	0	1.25	1	72.24
8	170.03	0	.	0	0	.	170	0	1.43	0	85.88
8	171.03	0	0	0	0	1	170	0	1.60	1	154.11
8	172.03	0	.	0	0	2	172	0	1.43	1	154.11
8	173.03	0	.	0	0	2	173	0	1.43	1	99.53
8	174.03	0	0	0	0	1	173	0	1.78	2	99.53
8	175.03	0	0	1	0	1	173	0	1.78	1	31.30
8	176.03	1	.	0	0	2	176	0	1.96	1	85.88
8	177.03	1	0	0	0	1	176	0	2.14	1	85.88
8	178.03	1	0	0	0	1	176	0	2.14	1	85.88
8	179.03	1	0	1	0	2	176	0	2.32	1	85.88
8	180.03	0	1	1	1	2	176	0	2.14	1	31.30
8	181.03	0	0	1	0	1	176	0	2.14	1	99.53
8	182.03	1	1	1	0	2	176	0	2.32	1	167.75
8	183.03	0	1	0	0	2	176	0	2.32	1	167.75
8	184.03	1	1	1	0	1	176	0	2.49	2	167.75
8	185.03	1	0	0	0	1	176	0	2.49	1	85.88
8	186.03	1	0	1	0	1	176	0	2.49	1	126.82
8	187.03	0	1	0	0	2	176	0	2.49	0	126.82
8	188.03	0	.	0	0	.	188	0	2.32	1	85.88
8	189.03	1	1	1	0	2	188	0	1.96	1	85.88
8	190.03	0	1	1	0	2	188	0	1.78	1	99.53
8	191.03	1	1	1	0	1	188	0	1.96	0	113.17
8	192.03	1	0	1	0	1	188	0	1.96	1	126.82
8	193.03	0	.	0	0	3	193	0	1.96	1	154.11
8	194.03	0	0	0	0	1	193	0	2.14	1	154.11
8	195.03	1	1	1	0	2	193	0	2.14	1	99.53
8	196.03	1	0	1	0	1	193	0	2.14	1	99.53
8	197.03	0	1	0	0	2	193	0	2.14	1	154.11
8	198.03	0	.	1	1	2	198	0	2.14	1	154.11
8	199.03	0	0	0	0	2	198	0	1.78	1	99.53
8	200.03	1	.	1	0	3	200	0	1.78	1	99.53
8	201.03	1	0	1	0	2	200	0	1.78	0	99.53
8	202.03	1	0	1	0	1	200	0	1.96	1	99.53
8	203.03	1	.	1	0	3	203	0	1.96	1	99.53
8	204.03	0	.	1	1	2	204	0	2.14	1	154.11
8	205.03	1	.	1	0	2	205	0	1.96	1	85.88
8	206.03	0	.	1	0	2	206	0	1.96	0	113.17
8	207.03	1	.	0	0	2	207	0	1.96	2	167.75
8	208.03	1	0	1	0	1	207	0	1.78	1	4.01
8	209.03	1	0	1	0	1	207	0	1.78	2	4.01
8	210.03	1	.	0	0	.	210	0	1.60	1	126.82
8	211.03	0	.	1	0	1	211	0	1.60	1	140.46
8	212.03	0	0	0	0	1	211	0	1.60	2	140.46
8	213.03	1	1	1	0	1	211	0	1.78	1	113.17
8	214.03	0	.	0	0	2	214	0	1.78	1	140.46
8	215.03	1	1	1	0	1	214	0	2.14	0	140.46
8	216.03	0	.	0	1	1	216	0	2.14	1	154.11
8	217.03	0	.	0	1	3	217	0	1.96	1	154.11

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	168.03	140.24	0.75	1.34	0.75	1.34	0		1	.
8	169.03	142.07	0.75	1.33	0.75	1.33	1	1	0	1.34
8	170.03	107.94	0.77	1.30	0.77	1.30	1	0	0	1.33
8	171.03	57.30	0.76	1.32	0.77	1.30	0		1	.
8	172.03	58.66	0.77	1.29	0.77	1.29	1	0	0	1.30
8	173.03	110.54	0.78	1.29	0.78	1.29	1	1	0	1.29
8	174.03	112.58	0.77	1.29	0.78	1.29	0		1	.
8	175.03	223.92	0.78	1.28	0.78	1.29	0		0	.
8	176.03	119.62	0.78	1.28	0.78	1.28	1	1	0	1.29
8	177.03	114.18	0.78	1.28	0.78	1.28	0		1	.
8	178.03	117.15	0.79	1.27	0.78	1.28	0		0	.
8	179.03	122.22	0.79	1.26	0.78	1.28	0		0	.
8	180.03	267.80	0.80	1.25	0.78	1.28	0		0	.
8	181.03	114.21	0.79	1.26	0.78	1.28	0		0	.
8	182.03	40.47	0.80	1.25	0.78	1.28	0		0	.
8	183.03	41.51	0.81	1.24	0.78	1.28	0		0	.
8	184.03	42.71	0.80	1.25	0.78	1.28	0		0	.
8	185.03	125.76	0.80	1.25	0.78	1.28	0		0	.
8	186.03	92.73	0.80	1.26	0.78	1.28	0		0	.
8	187.03	94.33	0.79	1.26	0.78	1.28	0		0	.
8	188.03	128.43	0.79	1.27	0.79	1.27	1	0	0	1.28
8	189.03	131.63	0.80	1.25	0.79	1.27	0		1	.
8	190.03	128.79	0.80	1.24	0.79	1.27	0		0	.
8	191.03	95.43	0.80	1.25	0.79	1.27	0		0	.
8	192.03	95.93	0.79	1.26	0.79	1.27	0		0	.
8	193.03	72.88	0.80	1.25	0.80	1.25	1	0	0	1.27
8	194.03	74.15	0.80	1.25	0.80	1.25	0		1	.
8	195.03	139.01	0.81	1.23	0.80	1.25	0		0	.
8	196.03	141.31	0.80	1.25	0.80	1.25	0		0	.
8	197.03	75.85	0.81	1.23	0.80	1.25	0		0	.
8	198.03	77.92	0.81	1.23	0.81	1.23	1	0	0	1.25
8	199.03	148.68	0.82	1.22	0.81	1.23	0		1	.
8	200.03	150.05	0.81	1.24	0.81	1.24	1	0	0	1.23
8	201.03	151.42	0.80	1.25	0.81	1.24	0		1	.
8	202.03	152.92	0.79	1.27	0.81	1.24	0		0	.
8	203.03	154.25	0.81	1.24	0.81	1.24	1	0	0	1.24
8	204.03	81.65	0.80	1.25	0.80	1.25	1	1	0	1.24
8	205.03	159.89	0.79	1.27	0.79	1.27	1	1	0	1.25
8	206.03	114.25	0.78	1.28	0.78	1.28	1	0	0	1.27
8	207.03	69.53	0.76	1.32	0.76	1.32	1	1	0	1.28
8	208.03	354.12	0.75	1.33	0.76	1.32	0		1	.
8	209.03	356.62	0.77	1.29	0.76	1.32	0		0	.
8	210.03	113.88	0.78	1.28	0.78	1.28	1	0	0	1.32
8	211.03	99.37	0.77	1.30	0.77	1.30	1	0	0	1.28
8	212.03	97.87	0.78	1.28	0.77	1.30	0		1	.
8	213.03	129.26	0.77	1.29	0.77	1.30	0		0	.
8	214.03	100.87	0.77	1.29	0.77	1.29	1	0	0	1.30
8	215.03	102.14	0.78	1.29	0.77	1.29	0		1	.
8	216.03	112.95	0.80	1.25	0.80	1.25	1	1	0	1.29
8	217.03	116.69	0.80	1.24	0.80	1.24	1	0	0	1.25

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	218.03	0	0	1	1	2	217	0	1.78	1	154.11
8	219.03	0	0	0	0	1	217	0	1.78	1	167.75
8	220.03	1	.	1	0	.	220	0	1.60	1	181.40
8	221.03	0	1	1	0	2	220	0	1.60	0	4.01
8	222.03	1	.	1	0	.	222	0	1.78	1	140.46
8	223.03	1	.	0	0	3	223	0	1.43	1	140.46
8	224.03	0	1	0	0	1	223	0	1.60	1	140.46
8	225.03	0	0	1	1	2	223	0	1.60	1	140.46
8	226.03	1	.	1	0	.	226	0	1.60	1	167.75
8	227.03	1	0	1	0	1	226	0	1.78	2	167.75
8	228.03	0	.	1	0	.	228	0	1.60	1	167.75
8	229.03	0	.	1	0	2	229	0	1.60	0	167.75
8	230.03	0	0	1	0	2	229	0	1.78	1	85.88
8	231.03	0	.	1	0	2	231	0	1.43	1	154.11
8	232.03	0	0	1	0	2	231	0	1.78	0	154.11
8	234.03	0	.	0	0	2	234	0	1.60	1	99.53
8	235.03	1	1	1	0	2	234	0	1.60	2	99.53
8	237.03	0	.	0	0	.	237	0	0.53	0	181.40
8	238.03	1	.	1	0	.	238	0	0.53	0	58.59
8	239.03	0	.	1	0	.	239	0	0.36	1	181.40
8	240.03	0	0	1	0	2	239	0	0.71	0	181.40
8	243.03	0	.	1	0	.	243	0	0.53	1	4.01
8	244.03	0	.	1	0	.	244	0	0.53	1	44.94
8	75.04	0	.	0	0	.	75	0	1.25	0	4.01
8	80.04	1	.	0	0	.	80	0	1.43	0	4.01
8	83.04	1	.	1	0	1	83	0	1.60	1	4.01
8	88.04	0	.	0	0	2	88	0	1.60	0	4.01
8	89.04	0	.	0	0	1	89	0	2.14	2	4.01
8	90.04	0	.	0	0	1	90	0	1.96	1	4.01
8	91.04	0	.	0	0	1	91	0	2.14	1	4.01
8	93.04	0	0	0	1	1	91	0	2.14	2	4.01
8	94.04	1	1	0	0	1	91	0	2.14	1	4.01
8	95.04	0	.	0	0	1	95	0	2.49	0	4.01
8	97.04	1	.	1	0	1	97	0	2.32	1	4.01
8	98.04	1	.	0	0	1	98	0	2.67	1	17.65
8	99.04	0	.	0	1	1	99	0	2.49	2	17.65
8	100.04	1	.	1	0	.	100	0	2.32	1	17.65
8	101.04	1	0	1	0	2	98	0	2.49	1	4.01
8	102.04	1	0	1	0	2	98	0	2.49	1	4.01
8	103.04	0	1	0	0	2	98	0	2.14	0	17.65
8	104.04	0	0	0	1	1	98	0	2.49	1	4.01
8	105.04	0	0	0	1	2	98	0	2.49	1	4.01
8	106.04	0	0	1	0	2	98	0	2.14	1	17.65
8	107.04	1	.	0	0	1	107	0	2.32	1	17.65
8	109.04	1	.	1	0	1	109	0	2.49	2	17.65
8	110.04	0	.	0	0	1	110	0	2.67	2	17.65
8	111.04	0	.	0	0	1	111	0	2.32	0	17.65
8	114.04	0	.	1	0	1	114	0	2.67	1	4.01
8	115.04	1	1	1	0	1	114	0	2.85	1	17.65
8	116.04	1	0	0	0	1	114	0	2.14	1	4.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	218.03	118.56	0.78	1.28	0.80	1.24	0		1	.
8	219.03	113.68	0.79	1.26	0.80	1.24	0		0	.
8	220.03	114.58	0.76	1.31	0.76	1.31	1	0	0	1.24
8	221.03	379.38	0.76	1.31	0.76	1.31	0		1	.
8	222.03	137.14	0.78	1.29	0.78	1.29	1	0	0	1.31
8	223.03	139.31	0.77	1.30	0.77	1.30	1	0	0	1.29
8	224.03	142.51	0.76	1.31	0.77	1.30	0		1	.
8	225.03	144.05	0.76	1.31	0.77	1.30	0		0	.
8	226.03	117.62	0.80	1.24	0.80	1.24	1	0	0	1.30
8	227.03	119.15	0.80	1.26	0.80	1.24	0		1	.
8	228.03	120.15	0.79	1.27	0.79	1.27	1	0	0	1.24
8	229.03	139.50	0.79	1.26	0.79	1.26	1	0	0	1.27
8	230.03	228.16	0.80	1.24	0.79	1.26	0		1	.
8	231.03	193.00	0.80	1.25	0.80	1.25	1	0	0	1.26
8	232.03	194.83	0.80	1.25	0.80	1.25	0		1	.
8	234.03	243.94	0.77	1.30	0.77	1.30	1	1	0	1.25
8	235.03	282.72	0.79	1.27	0.77	1.30	0		1	.
8	237.03	274.17	0.92	1.08	0.92	1.08	1	0	0	1.30
8	238.03	439.33	1.27	0.79	1.27	0.79	1	0	0	1.08
8	239.03	424.76	1.11	0.90	1.11	0.90	1	0	0	0.79
8	240.03	426.36	1.09	0.92	1.11	0.90	0		1	.
8	243.03	945.18	0.15	6.84	0.15	6.84	1	2	0	.
8	244.03	721.68	0.08	12.15	0.08	12.15	1	3	0	.
8	75.04	56.75	0.84	1.18	0.84	1.18	1	1	0	.
8	80.04	59.99	0.77	1.29	0.77	1.29	1	0	0	1.18
8	83.04	61.19	0.74	1.36	0.74	1.36	1	4	0	1.29
8	88.04	58.05	0.63	1.58	0.63	1.58	1	4	0	1.36
8	89.04	66.06	0.66	1.51	0.66	1.51	1	2	0	1.58
8	90.04	64.93	0.62	1.61	0.62	1.61	1	3	0	1.58
8	91.04	67.46	0.64	1.57	0.64	1.57	1	1	0	1.58
8	93.04	69.20	0.66	1.52	0.64	1.57	0		1	.
8	94.04	70.73	0.66	1.52	0.64	1.57	0		0	.
8	95.04	71.90	0.67	1.49	0.67	1.49	1	1	0	1.57
8	97.04	75.41	0.63	1.59	0.63	1.59	1	1	0	1.49
8	98.04	73.37	0.63	1.60	0.63	1.60	1	1	0	1.59
8	99.04	71.23	0.64	1.56	0.64	1.56	1	2	0	1.59
8	100.04	69.40	0.61	1.64	0.61	1.64	1	3	0	1.59
8	101.04	79.11	0.62	1.61	0.63	1.60	0		1	.
8	102.04	80.84	0.62	1.60	0.63	1.60	0		0	.
8	103.04	78.01	0.60	1.65	0.63	1.60	0		0	.
8	104.04	82.68	0.45	2.22	0.63	1.60	0		0	.
8	105.04	84.61	0.45	2.24	0.63	1.60	0		0	.
8	106.04	80.11	0.44	2.26	0.63	1.60	0		0	.
8	107.04	81.81	0.44	2.26	0.44	2.26	1	2	0	1.60
8	109.04	82.78	0.43	2.31	0.43	2.31	1	3	0	1.60
8	110.04	85.48	0.44	2.28	0.44	2.28	1	1	0	1.60
8	111.04	90.95	0.45	2.22	0.45	2.22	1	1	0	2.28
8	114.04	91.09	0.44	2.27	0.44	2.27	1	4	0	2.22
8	115.04	93.06	0.45	2.24	0.44	2.27	0		1	.
8	116.04	96.03	0.45	2.22	0.44	2.27	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	117.04	0	.	1	0	1	117	0	2.67	1	4.01
8	118.04	0	.	0	0	1	118	0	1.60	1	4.01
8	119.04	1	1	1	0	1	118	0	1.96	1	4.01
8	121.04	1	.	1	0	1	121	0	2.32	1	4.01
8	122.04	0	.	1	0	1	122	0	2.14	1	4.01
8	123.04	1	.	1	0	.	123	0	1.78	1	44.94
8	124.04	1	0	0	0	1	123	0	1.96	2	44.94
8	125.04	0	1	1	1	1	123	0	2.32	2	44.94
8	126.04	0	0	0	1	1	123	0	2.14	1	4.01
8	127.04	1	1	0	0	1	123	0	2.32	2	44.94
8	128.04	1	.	0	0	1	128	0	2.32	1	4.01
8	132.04	1	0	1	0	1	128	0	2.49	1	72.24
8	133.04	0	.	1	0	.	133	0	2.49	0	44.94
8	134.04	1	.	1	0	2	134	0	2.49	0	44.94
8	135.04	0	.	1	0	2	135	0	2.85	0	44.94
8	136.04	1	.	1	0	1	136	0	1.78	1	44.94
8	137.04	1	0	1	0	2	136	0	1.96	1	4.01
8	138.04	0	1	1	0	2	136	0	1.78	1	4.01
8	139.04	0	.	0	0	2	139	0	1.78	1	72.24
8	140.04	1	.	1	0	1	140	0	1.96	1	72.24
8	141.04	0	1	0	0	2	140	0	1.96	1	72.24
8	142.04	0	0	0	0	1	140	0	2.14	0	72.24
8	143.04	1	1	1	0	2	140	0	2.14	1	72.24
8	144.04	1	0	1	0	1	140	0	2.14	1	72.24
8	145.04	0	1	1	0	1	140	0	2.14	2	72.24
8	147.04	0	.	0	0	1	147	0	1.96	1	85.88
8	148.04	0	0	0	0	1	147	0	2.14	1	85.88
8	149.04	0	0	0	0	1	147	0	2.14	1	17.65
8	150.04	1	1	1	0	1	147	0	2.14	2	17.65
8	151.04	0	1	0	0	1	147	0	2.14	1	72.24
8	152.04	1	1	1	0	1	147	0	2.14	2	72.24
8	153.04	0	1	1	0	2	147	0	3.03	1	4.01
8	154.04	0	.	0	0	.	154	0	2.67	1	44.94
8	155.04	1	1	1	0	1	154	0	2.32	0	44.94
8	159.04	1	.	1	0	.	159	0	1.78	1	85.88
8	160.04	1	0	0	0	1	159	0	2.14	0	72.24
8	161.04	0	1	0	0	1	159	0	2.49	0	72.24
8	162.04	0	0	0	0	1	159	0	2.14	0	85.88
8	163.04	1	.	0	0	.	163	0	1.96	1	72.24
8	164.04	1	0	1	0	1	163	0	2.14	1	85.88
8	165.04	0	.	0	0	2	165	0	2.32	1	72.24
8	166.04	1	1	0	0	1	165	0	2.32	0	72.24
8	167.04	0	.	1	0	1	167	0	1.78	2	44.94
8	168.04	1	.	1	0	.	168	0	1.96	1	44.94
8	169.04	0	.	1	0	.	169	0	1.60	1	44.94
8	170.04	0	.	0	0	.	170	0	1.43	0	58.59
8	171.04	0	0	0	0	1	170	0	1.43	1	126.82
8	172.04	0	.	0	0	2	172	0	1.43	1	126.82
8	173.04	0	.	0	0	3	173	0	1.60	1	72.24
8	174.04	0	0	0	0	1	173	0	1.96	2	72.24

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	117.04	85.88	0.35	2.88	0.35	2.88	1	3	0	2.27
8	118.04	99.93	0.39	2.54	0.39	2.54	1	0	0	2.27
8	119.04	102.47	0.40	2.52	0.39	2.54	0		1	.
8	121.04	107.10	0.41	2.46	0.41	2.46	1	2	0	2.54
8	122.04	104.93	0.38	2.61	0.38	2.61	1	3	0	2.54
8	123.04	69.86	0.25	3.94	0.25	3.94	1	1	0	2.54
8	124.04	71.27	0.25	3.99	0.25	3.94	0		1	.
8	125.04	73.10	0.25	3.97	0.25	3.94	0		0	.
8	126.04	112.28	0.25	3.96	0.25	3.94	0		0	.
8	127.04	75.00	0.25	4.00	0.25	3.94	0		0	.
8	128.04	115.95	0.25	3.95	0.25	3.95	1	1	0	3.94
8	132.04	58.46	0.25	3.93	0.25	3.95	0		1	.
8	133.04	79.81	0.26	3.85	0.26	3.85	1	2	0	3.95
8	134.04	87.15	0.26	3.84	0.26	3.84	1	0	0	3.95
8	135.04	78.14	0.24	4.09	0.24	4.09	1	3	0	3.84
8	136.04	89.28	0.25	3.99	0.25	3.99	1	1	0	3.84
8	137.04	129.59	0.25	3.99	0.25	3.99	0		1	.
8	138.04	132.20	0.25	3.98	0.25	3.99	0		0	.
8	139.04	67.53	0.25	3.99	0.25	3.99	1	0	0	3.99
8	140.04	69.50	0.25	3.99	0.25	3.99	1	0	0	3.99
8	141.04	70.94	0.25	4.00	0.25	3.99	0		1	.
8	142.04	72.17	0.25	3.95	0.25	3.99	0		0	.
8	143.04	74.04	0.25	3.94	0.25	3.99	0		0	.
8	144.04	75.91	0.25	3.95	0.25	3.99	0		0	.
8	145.04	77.28	0.25	3.95	0.25	3.99	0		0	.
8	147.04	50.62	0.25	3.95	0.25	3.95	1	4	0	3.99
8	148.04	51.92	0.31	3.19	0.25	3.95	0		1	.
8	149.04	146.21	0.32	3.16	0.25	3.95	0		0	.
8	150.04	147.74	0.32	3.13	0.25	3.95	0		0	.
8	151.04	88.42	0.32	3.14	0.25	3.95	0		0	.
8	152.04	87.52	0.32	3.14	0.25	3.95	0		0	.
8	153.04	158.59	0.32	3.12	0.25	3.95	0		0	.
8	154.04	130.16	0.32	3.12	0.32	3.12	1	0	0	3.95
8	155.04	113.71	0.32	3.08	0.32	3.12	0		1	.
8	159.04	69.14	0.30	3.33	0.30	3.33	1	0	0	3.12
8	160.04	96.30	0.32	3.17	0.30	3.33	0		1	.
8	161.04	97.80	0.31	3.19	0.30	3.33	0		0	.
8	162.04	70.40	0.32	3.13	0.30	3.33	0		0	.
8	163.04	101.10	0.33	3.07	0.33	3.07	1	1	0	3.33
8	164.04	72.01	0.33	3.06	0.33	3.07	0		1	.
8	165.04	105.67	0.33	3.06	0.33	3.06	1	1	0	3.07
8	166.04	104.94	0.33	3.03	0.33	3.06	0		1	.
8	167.04	139.80	0.33	3.03	0.33	3.03	1	2	0	3.06
8	168.04	140.24	0.32	3.11	0.32	3.11	1	3	0	3.06
8	169.04	142.07	0.35	2.88	0.35	2.88	1	0	0	3.06
8	170.04	107.94	0.68	1.46	0.68	1.46	1	0	0	2.88
8	171.04	57.30	0.68	1.46	0.68	1.46	0		1	.
8	172.04	58.66	0.68	1.48	0.68	1.48	1	1	0	1.46
8	173.04	110.54	0.67	1.49	0.67	1.49	1	0	0	1.48
8	174.04	112.58	0.68	1.47	0.67	1.49	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	175.04	0	0	1	0	1	173	0	2.67	1	4.01
8	176.04	1	.	0	0	1	176	0	2.14	1	58.59
8	177.04	1	0	0	0	1	176	0	2.49	1	58.59
8	178.04	1	0	0	0	1	176	0	2.67	1	58.59
8	179.04	1	0	1	0	1	176	0	2.67	1	58.59
8	180.04	0	1	1	1	2	176	0	2.32	1	4.01
8	181.04	0	0	1	0	1	176	0	2.49	1	72.24
8	182.04	1	1	1	0	1	176	0	2.49	1	140.46
8	183.04	0	1	0	0	1	176	0	1.96	0	140.46
8	184.04	1	1	1	0	1	176	0	2.14	0	140.46
8	185.04	1	0	0	0	1	176	0	2.14	1	58.59
8	186.04	1	.	1	0	.	186	0	1.96	1	99.53
8	187.04	0	1	0	0	2	186	0	1.96	0	99.53
8	188.04	0	.	0	0	.	188	0	1.96	1	58.59
8	189.04	1	1	1	0	2	188	0	1.78	1	58.59
8	190.04	0	1	1	0	2	188	0	1.43	1	72.24
8	191.04	1	1	1	0	1	188	0	1.78	1	85.88
8	192.04	1	0	1	0	1	188	0	1.78	1	99.53
8	193.04	0	.	0	0	3	193	0	1.96	1	126.82
8	194.04	0	0	0	0	1	193	0	1.96	1	126.82
8	195.04	1	.	1	0	2	195	0	1.78	1	72.24
8	196.04	1	0	1	0	1	195	0	1.78	1	72.24
8	197.04	0	1	0	0	2	195	0	1.96	1	126.82
8	198.04	0	0	1	1	2	195	0	1.78	1	126.82
8	199.04	0	.	0	0	2	199	0	1.78	1	72.24
8	200.04	1	.	1	0	2	200	0	1.96	1	72.24
8	201.04	1	0	1	0	1	200	0	2.14	1	72.24
8	202.04	1	0	1	0	1	200	0	1.60	1	72.24
8	203.04	1	.	1	0	2	203	0	1.60	1	72.24
8	204.04	0	.	1	1	2	204	0	1.96	1	126.82
8	205.04	1	.	1	0	2	205	0	1.60	0	58.59
8	206.04	0	.	1	0	2	206	0	1.43	0	85.88
8	207.04	1	.	0	0	2	207	0	1.43	0	140.46
8	210.04	1	.	0	0	.	210	0	1.07	1	99.53
8	211.04	0	1	1	0	1	210	0	1.07	1	113.17
8	212.04	0	0	0	0	1	210	0	1.25	2	113.17
8	213.04	1	1	1	0	1	210	0	1.43	1	85.88
8	214.04	0	1	0	0	2	210	0	1.78	1	113.17
8	215.04	1	1	1	0	2	210	0	1.96	0	113.17
8	216.04	0	.	0	1	2	216	0	1.78	1	126.82
8	217.04	0	.	0	1	2	217	0	1.60	1	126.82
8	218.04	0	0	1	1	2	217	0	1.43	0	126.82
8	219.04	0	0	0	0	1	217	0	1.43	1	140.46
8	220.04	1	.	1	0	.	220	0	1.25	1	154.11
8	222.04	1	.	1	0	.	222	0	1.43	1	113.17
8	223.04	1	.	0	0	2	223	0	1.25	0	113.17
8	224.04	0	1	0	0	1	223	0	1.43	1	113.17
8	225.04	0	0	1	1	2	223	0	1.43	0	113.17
8	226.04	1	.	1	0	.	226	0	1.43	1	140.46
8	227.04	1	0	1	0	1	226	0	1.60	2	140.46

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	175.04	223.92	0.67	1.49	0.67	1.49	0		0	.
8	176.04	119.62	0.67	1.49	0.67	1.49	1	0	0	1.49
8	177.04	114.18	0.67	1.50	0.67	1.49	0		1	.
8	178.04	117.15	0.66	1.51	0.67	1.49	0		0	.
8	179.04	122.22	0.66	1.52	0.67	1.49	0		0	.
8	180.04	267.80	0.66	1.53	0.67	1.49	0		0	.
8	181.04	114.21	0.66	1.52	0.67	1.49	0		0	.
8	182.04	40.47	0.65	1.53	0.67	1.49	0		0	.
8	183.04	41.51	0.65	1.54	0.67	1.49	0		0	.
8	184.04	42.71	0.65	1.53	0.67	1.49	0		0	.
8	185.04	125.76	0.66	1.52	0.67	1.49	0		0	.
8	186.04	92.73	0.67	1.50	0.67	1.50	1	1	0	1.49
8	187.04	94.33	0.66	1.52	0.67	1.50	0		1	.
8	188.04	128.43	0.68	1.46	0.68	1.46	1	1	0	1.50
8	189.04	131.63	0.67	1.49	0.68	1.46	0		1	.
8	190.04	128.79	0.67	1.50	0.68	1.46	0		0	.
8	191.04	95.43	0.67	1.49	0.68	1.46	0		0	.
8	192.04	95.93	0.67	1.50	0.68	1.46	0		0	.
8	193.04	72.88	0.69	1.45	0.69	1.45	1	0	0	1.46
8	194.04	74.15	0.69	1.44	0.69	1.45	0		1	.
8	195.04	139.01	0.81	1.24	0.81	1.24	1	1	0	1.45
8	196.04	141.31	0.80	1.25	0.81	1.24	0		1	.
8	197.04	75.85	0.80	1.25	0.81	1.24	0		0	.
8	198.04	77.92	0.80	1.25	0.81	1.24	0		0	.
8	199.04	148.68	0.79	1.26	0.79	1.26	1	1	0	1.24
8	200.04	150.05	0.81	1.24	0.81	1.24	1	0	0	1.26
8	201.04	151.42	0.80	1.25	0.81	1.24	0		1	.
8	202.04	152.92	0.81	1.24	0.81	1.24	0		0	.
8	203.04	154.25	0.80	1.25	0.80	1.25	1	0	0	1.24
8	204.04	81.65	0.80	1.25	0.80	1.25	1	0	0	1.25
8	205.04	159.89	0.80	1.25	0.80	1.25	1	0	0	1.25
8	206.04	114.25	0.80	1.24	0.80	1.24	1	1	0	1.25
8	207.04	69.53	0.81	1.23	0.81	1.23	1	0	0	1.24
8	210.04	113.88	0.79	1.27	0.79	1.27	1	0	0	1.23
8	211.04	99.37	0.79	1.27	0.79	1.27	0		1	.
8	212.04	97.87	0.79	1.26	0.79	1.27	0		0	.
8	213.04	129.26	0.78	1.28	0.79	1.27	0		0	.
8	214.04	100.87	0.79	1.26	0.79	1.27	0		0	.
8	215.04	102.14	0.79	1.26	0.79	1.27	0		0	.
8	216.04	112.95	0.79	1.27	0.79	1.27	1	0	0	1.27
8	217.04	116.69	0.78	1.29	0.78	1.29	1	0	0	1.27
8	218.04	118.56	0.79	1.27	0.78	1.29	0		1	.
8	219.04	113.68	0.79	1.27	0.78	1.29	0		0	.
8	220.04	114.58	0.80	1.25	0.80	1.25	1	0	0	1.29
8	222.04	137.14	0.77	1.29	0.77	1.29	1	0	0	1.25
8	223.04	139.31	0.77	1.31	0.77	1.31	1	0	0	1.29
8	224.04	142.51	0.77	1.30	0.77	1.31	0		1	.
8	225.04	144.05	0.77	1.30	0.77	1.31	0		0	.
8	226.04	117.62	0.73	1.36	0.73	1.36	1	0	0	1.31
8	227.04	119.15	0.76	1.32	0.73	1.36	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	228.04	0	.	1	0	.	228	0	1.25	1	140.46
8	229.04	0	0	1	0	2	228	0	1.43	1	140.46
8	230.04	0	0	1	0	1	228	0	1.43	0	58.59
8	231.04	0	0	1	0	2	228	0	1.43	1	126.82
8	232.04	0	0	1	0	2	228	0	1.60	0	126.82
8	234.04	0	.	0	0	3	234	0	1.43	1	72.24
8	235.04	1	1	1	0	1	234	0	1.43	0	72.24
8	237.04	0	.	0	0	.	237	0	0.36	0	154.11
8	238.04	1	.	1	0	.	238	0	0.36	0	31.30
8	239.04	0	.	1	0	.	239	0	0.36	1	154.11
8	240.04	0	0	1	0	2	239	0	0.71	0	154.11
8	244.04	0	.	1	0	.	244	0	0.53	0	17.65
8	246.04	0	.	1	1	.	246	0	0.36	1	4.01
8	251.04	0	.	1	1	.	251	0	0.53	0	17.65
8	253.04	0	.	1	0	.	253	0	0.36	1	140.46
8	254.04	0	.	1	0	.	254	0	0.71	1	140.46
8	123.05	1	.	1	0	.	123	0	0.89	1	17.65
8	124.05	1	0	0	0	1	123	0	1.25	2	17.65
8	125.05	0	1	1	1	1	123	0	1.78	0	17.65
8	127.05	1	.	0	0	1	127	0	1.96	0	17.65
8	132.05	1	.	1	0	1	132	0	1.96	1	44.94
8	133.05	0	0	1	0	1	135	0	1.60	0	17.65
8	134.05	1	.	1	0	.	134	0	1.25	0	17.65
8	135.05	0	.	1	0	.	135	0	1.60	0	17.65
8	136.05	1	.	1	0	2	136	0	1.25	1	17.65
8	139.05	0	.	0	0	.	139	0	1.25	1	44.94
8	140.05	1	.	1	0	.	140	0	1.43	1	44.94
8	141.05	0	1	0	0	2	140	0	1.60	1	44.94
8	142.05	0	0	0	0	1	140	0	1.78	1	44.94
8	143.05	1	.	1	0	2	143	0	1.78	0	44.94
8	144.05	1	.	1	0	1	144	0	1.78	1	44.94
8	145.05	0	1	1	0	1	144	0	1.78	2	44.94
8	147.05	0	0	0	0	1	144	0	1.78	1	58.59
8	148.05	0	0	0	0	2	144	0	1.78	1	58.59
8	151.05	0	.	0	0	1	151	0	1.96	1	44.94
8	152.05	1	.	1	0	1	152	0	1.78	2	44.94
8	154.05	0	.	0	0	1	154	0	2.32	1	17.65
8	155.05	1	.	1	0	.	155	0	1.78	0	17.65
8	159.05	1	.	1	0	.	159	0	1.43	1	58.59
8	160.05	1	.	0	0	.	160	0	1.78	1	44.94
8	161.05	0	1	0	0	1	160	0	2.14	2	44.94
8	162.05	0	0	0	0	1	160	0	1.78	0	58.59
8	163.05	1	.	0	0	.	163	0	1.78	1	44.94
8	164.05	1	0	1	0	1	163	0	1.96	1	58.59
8	165.05	0	.	0	0	.	165	0	1.78	1	44.94
8	166.05	1	1	0	0	1	165	0	1.96	2	44.94
8	167.05	0	.	1	0	.	167	0	1.60	0	17.65
8	168.05	1	.	1	0	.	168	0	1.78	0	17.65
8	169.05	0	0	1	0	1	167	0	1.60	1	17.65
8	170.05	0	0	0	0	2	167	0	1.43	0	31.30

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	228.04	120.15	0.75	1.33	0.75	1.33	1	0	0	1.36
8	229.04	139.50	0.76	1.32	0.75	1.33	0		1	.
8	230.04	228.16	0.76	1.32	0.75	1.33	0		0	.
8	231.04	193.00	0.76	1.32	0.75	1.33	0		0	.
8	232.04	194.83	0.74	1.35	0.75	1.33	0		0	.
8	234.04	243.94	0.76	1.31	0.76	1.31	1	0	0	1.33
8	235.04	282.72	0.76	1.32	0.76	1.31	0		1	.
8	237.04	274.17	0.91	1.09	0.91	1.09	1	0	0	1.31
8	238.04	439.33	1.34	0.74	1.34	0.74	1	0	0	1.09
8	239.04	424.76	1.09	0.92	1.09	0.92	1	0	0	0.74
8	240.04	426.36	1.06	0.94	1.09	0.92	0		1	.
8	244.04	721.68	1.27	0.79	1.27	0.79	1	0	0	0.92
8	246.04	808.00	0.11	9.14	0.11	9.14	1	0	0	.
8	251.04	717.85	1.22	0.82	1.22	0.82	1	0	0	0.79
8	253.04	1087.65	1.71	0.58	1.71	0.58	1	0	0	0.82
8	254.04	1088.59	1.65	0.61	1.65	0.61	1	0	0	0.58
8	123.05	69.86	0.68	1.47	0.68	1.47	1	0	0	.
8	124.05	71.27	0.69	1.46	0.68	1.47	0		1	.
8	125.05	73.10	0.68	1.48	0.68	1.47	0		0	.
8	127.05	75.00	0.69	1.46	0.69	1.46	1	4	0	1.47
8	132.05	58.46	0.70	1.43	0.70	1.43	1	2	0	1.46
8	133.05	79.81	0.62	1.62	0.60	1.65	0		1	.
8	134.05	87.15	0.69	1.46	0.69	1.46	1	1	0	1.46
8	135.05	78.14	0.60	1.65	0.60	1.65	1	3	0	1.46
8	136.05	89.28	0.69	1.44	0.69	1.44	1	1	0	1.46
8	139.05	67.53	0.68	1.48	0.68	1.48	1	4	0	1.44
8	140.05	69.50	0.69	1.45	0.69	1.45	1	1	0	1.48
8	141.05	70.94	0.69	1.45	0.69	1.45	0		1	.
8	142.05	72.17	0.69	1.45	0.69	1.45	0		0	.
8	143.05	74.04	0.68	1.47	0.68	1.47	1	1	0	1.45
8	144.05	75.91	0.69	1.44	0.69	1.44	1	1	0	1.47
8	145.05	77.28	0.68	1.47	0.69	1.44	0		1	.
8	147.05	50.62	0.66	1.51	0.69	1.44	0		0	.
8	148.05	51.92	0.44	2.28	0.69	1.44	0		0	.
8	151.05	88.42	0.42	2.38	0.42	2.38	1	2	0	1.44
8	152.05	87.52	0.41	2.43	0.41	2.43	1	3	0	1.44
8	154.05	130.16	0.56	1.77	0.56	1.77	1	2	0	1.44
8	155.05	113.71	0.40	2.49	0.40	2.49	1	3	0	1.44
8	159.05	69.14	0.45	2.21	0.45	2.21	1	1	0	1.44
8	160.05	96.30	0.44	2.27	0.44	2.27	1	1	0	2.21
8	161.05	97.80	0.44	2.27	0.44	2.27	0		1	.
8	162.05	70.40	0.43	2.31	0.44	2.27	0		0	.
8	163.05	101.10	0.44	2.29	0.44	2.29	1	0	0	2.27
8	164.05	72.01	0.43	2.31	0.44	2.29	0		1	.
8	165.05	105.67	0.44	2.30	0.44	2.30	1	0	0	2.29
8	166.05	104.94	0.43	2.34	0.44	2.30	0		1	.
8	167.05	139.80	0.43	2.31	0.43	2.31	1	1	0	2.28
8	168.05	140.24	0.44	2.28	0.44	2.28	1	0	0	2.30
8	169.05	142.07	0.40	2.51	0.43	2.31	0		1	.
8	170.05	107.94	0.25	3.93	0.43	2.31	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	171.05	0	0	0	0	1	167	0	1.60	1	99.53
8	172.05	0	.	0	0	3	172	0	1.43	1	99.53
8	173.05	0	.	0	0	2	173	0	1.60	1	44.94
8	174.05	0	0	0	0	1	173	0	1.96	0	44.94
8	176.05	1	.	0	0	1	176	0	2.14	1	31.30
8	177.05	1	.	0	0	1	177	0	2.32	1	31.30
8	178.05	1	0	0	0	1	177	0	2.49	1	31.30
8	179.05	1	.	1	0	1	179	0	2.67	1	31.30
8	181.05	0	.	1	0	1	181	0	2.49	1	44.94
8	182.05	1	1	1	0	1	181	0	2.49	1	113.17
8	183.05	0	1	0	0	1	181	0	1.96	2	113.17
8	184.05	1	1	1	0	1	181	0	1.96	1	113.17
8	185.05	1	.	0	0	1	185	0	1.78	1	31.30
8	186.05	1	.	1	0	.	186	0	1.60	1	72.24
8	187.05	0	1	0	0	2	186	0	1.60	0	72.24
8	188.05	0	.	0	0	.	188	0	1.43	1	31.30
8	189.05	1	1	1	0	2	188	0	1.43	1	31.30
8	190.05	0	1	1	0	1	188	0	1.25	1	44.94
8	191.05	1	1	1	0	1	188	0	1.43	0	58.59
8	192.05	1	0	1	0	1	188	0	1.60	1	72.24
8	193.05	0	.	0	0	2	193	0	1.78	1	99.53
8	194.05	0	.	0	0	2	194	0	1.78	1	99.53
8	195.05	1	.	1	0	3	195	0	1.43	1	44.94
8	196.05	1	0	1	0	1	195	0	1.43	0	44.94
8	197.05	0	1	0	0	2	195	0	1.78	1	99.53
8	198.05	0	0	1	1	1	195	0	1.78	0	99.53
8	199.05	0	.	0	0	3	199	0	2.14	1	44.94
8	200.05	1	1	1	0	1	199	0	1.96	1	44.94
8	201.05	1	0	1	0	1	199	0	2.14	1	44.94
8	202.05	1	0	1	0	1	199	0	1.43	1	44.94
8	203.05	1	0	1	0	1	199	0	1.60	0	44.94
8	204.05	0	1	1	1	1	199	0	1.78	1	99.53
8	205.05	1	1	1	0	2	199	0	1.78	0	31.30
8	206.05	0	.	1	0	2	206	0	1.60	0	58.59
8	207.05	1	.	0	0	2	207	0	1.78	0	113.17
8	210.05	1	.	0	0	.	210	0	1.78	1	72.24
8	211.05	0	1	1	0	1	210	0	1.25	1	85.88
8	212.05	0	0	0	0	1	210	0	1.25	1	85.88
8	213.05	1	1	1	0	1	210	0	1.60	1	58.59
8	214.05	0	.	0	0	2	214	0	1.78	1	85.88
8	215.05	1	1	1	0	2	214	0	1.96	0	85.88
8	216.05	0	1	0	1	2	214	0	1.78	1	99.53
8	217.05	0	0	0	1	1	214	0	1.96	0	99.53
8	218.05	0	0	1	1	1	214	0	1.43	2	99.53
8	219.05	0	0	0	0	1	214	0	1.43	1	113.17
8	220.05	1	.	1	0	3	220	0	1.25	1	126.82
8	222.05	1	.	1	0	2	222	0	1.25	1	85.88
8	223.05	1	0	0	0	2	222	0	1.25	1	85.88
8	224.05	0	1	0	0	2	222	0	1.43	1	85.88
8	225.05	0	0	1	1	2	222	0	1.60	0	85.88

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	171.05	57.30	0.25	3.94	0.43	2.31	0		0	.
8	172.05	58.66	0.25	3.94	0.25	3.94	1	0	0	2.31
8	173.05	110.54	0.25	3.94	0.25	3.94	1	0	0	3.94
8	174.05	112.58	0.26	3.92	0.25	3.94	0		1	.
8	176.05	119.62	0.26	3.87	0.26	3.87	1	2	0	3.94
8	177.05	114.18	0.25	4.04	0.25	4.04	1	3	0	3.94
8	178.05	117.15	0.25	4.03	0.25	4.04	0		1	.
8	179.05	122.22	0.25	3.98	0.25	3.98	1	1	0	3.94
8	181.05	114.21	0.25	4.05	0.25	4.05	1	4	0	3.98
8	182.05	40.47	0.25	4.06	0.25	4.05	0		1	.
8	183.05	41.51	0.25	4.06	0.25	4.05	0		0	.
8	184.05	42.71	0.25	4.07	0.25	4.05	0		0	.
8	185.05	125.76	0.25	4.07	0.25	4.07	1	1	0	4.05
8	186.05	92.73	0.24	4.09	0.24	4.09	1	0	0	4.07
8	187.05	94.33	0.25	4.07	0.24	4.09	0		1	.
8	188.05	128.43	0.24	4.11	0.24	4.11	1	0	0	4.09
8	189.05	131.63	0.24	4.11	0.24	4.11	0		1	.
8	190.05	128.79	0.24	4.11	0.24	4.11	0		0	.
8	191.05	95.43	0.24	4.11	0.24	4.11	0		0	.
8	192.05	95.93	0.24	4.09	0.24	4.11	0		0	.
8	193.05	72.88	0.29	3.48	0.29	3.48	1	0	0	4.11
8	194.05	74.15	0.29	3.46	0.29	3.46	1	1	0	3.48
8	195.05	139.01	0.27	3.65	0.27	3.65	1	0	0	3.46
8	196.05	141.31	0.28	3.62	0.27	3.65	0		1	.
8	197.05	75.85	0.27	3.64	0.27	3.65	0		0	.
8	198.05	77.92	0.27	3.67	0.27	3.65	0		0	.
8	199.05	148.68	0.27	3.65	0.27	3.65	1	0	0	3.65
8	200.05	150.05	0.28	3.63	0.27	3.65	0		1	.
8	201.05	151.42	0.31	3.23	0.27	3.65	0		0	.
8	202.05	152.92	0.31	3.21	0.27	3.65	0		0	.
8	203.05	154.25	0.31	3.23	0.27	3.65	0		0	.
8	204.05	81.65	0.31	3.23	0.27	3.65	0		0	.
8	205.05	159.89	0.31	3.20	0.27	3.65	0		0	.
8	206.05	114.25	0.32	3.17	0.32	3.17	1	0	0	3.65
8	207.05	69.53	0.32	3.14	0.32	3.14	1	1	0	3.17
8	210.05	113.88	0.31	3.18	0.31	3.18	1	0	0	3.14
8	211.05	99.37	0.41	2.46	0.31	3.18	0		1	.
8	212.05	97.87	0.71	1.41	0.31	3.18	0		0	.
8	213.05	129.26	0.74	1.35	0.31	3.18	0		0	.
8	214.05	100.87	0.73	1.37	0.73	1.37	1	1	0	3.18
8	215.05	102.14	0.73	1.36	0.73	1.37	0		1	.
8	216.05	112.95	0.72	1.39	0.73	1.37	0		0	.
8	217.05	116.69	0.72	1.39	0.73	1.37	0		0	.
8	218.05	118.56	0.71	1.40	0.73	1.37	0		0	.
8	219.05	113.68	0.73	1.38	0.73	1.37	0		0	.
8	220.05	114.58	0.72	1.39	0.72	1.39	1	0	0	1.37
8	222.05	137.14	0.70	1.42	0.70	1.42	1	0	0	1.39
8	223.05	139.31	0.71	1.42	0.70	1.42	0		1	.
8	224.05	142.51	0.71	1.42	0.70	1.42	0		0	.
8	225.05	144.05	0.70	1.42	0.70	1.42	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	226.05	1	.	1	0	.	226	0	1.60	1	113.17
8	227.05	1	0	1	0	1	226	0	1.60	2	113.17
8	228.05	0	.	1	0	.	228	0	1.25	1	113.17
8	229.05	0	0	1	0	2	228	0	1.43	1	113.17
8	230.05	0	0	1	0	1	228	0	1.25	0	31.30
8	231.05	0	0	1	0	2	228	0	1.43	1	99.53
8	232.05	0	.	1	0	2	232	0	1.43	0	99.53
8	234.05	0	.	0	0	1	234	0	1.43	1	44.94
8	235.05	1	.	1	0	1	235	0	1.43	0	44.94
8	237.05	0	.	0	0	.	237	0	0.36	0	126.82
8	238.05	1	.	1	0	.	238	0	0.36	0	4.01
8	239.05	0	.	1	0	.	239	0	0.36	0	126.82
8	240.05	0	.	1	0	2	240	0	0.71	0	126.82
8	247.05	0	.	1	0	.	247	0	0.36	0	85.88
8	253.05	0	.	1	0	.	253	0	0.36	0	113.17
8	254.05	0	.	1	0	.	254	0	0.71	0	113.17
8	132.06	1	.	1	0	.	132	0	0.89	1	17.65
8	139.06	0	.	0	0	.	139	0	0.53	1	17.65
8	140.06	1	.	1	0	.	140	0	0.71	1	17.65
8	141.06	0	1	0	0	2	140	0	1.07	1	17.65
8	142.06	0	0	0	0	2	140	0	1.43	0	17.65
8	143.06	1	.	1	0	3	143	0	1.43	0	17.65
8	144.06	1	.	1	0	2	144	0	1.43	1	17.65
8	145.06	0	1	1	0	1	144	0	1.43	2	17.65
8	147.06	0	.	0	0	1	147	0	1.43	1	31.30
8	148.06	0	.	0	0	2	148	0	1.25	0	31.30
8	151.06	0	1	0	0	1	152	0	1.25	1	17.65
8	152.06	1	.	1	0	.	152	0	0.89	2	17.65
8	159.06	1	.	1	0	.	159	0	0.36	1	31.30
8	160.06	1	.	0	0	.	160	0	0.71	1	17.65
8	161.06	0	1	0	0	1	160	0	1.07	0	17.65
8	162.06	0	0	0	0	1	160	0	1.43	2	31.30
8	163.06	1	.	0	0	2	163	0	1.60	0	17.65
8	164.06	1	0	1	0	1	163	0	1.60	1	31.30
8	165.06	0	.	0	0	.	165	0	1.43	0	17.65
8	166.06	1	1	0	0	1	165	0	1.25	0	17.65
8	170.06	0	.	0	0	1	170	0	1.60	1	4.01
8	171.06	0	0	0	0	1	170	0	1.60	0	72.24
8	172.06	0	.	0	0	1	172	0	1.78	1	72.24
8	173.06	0	.	0	0	2	173	0	1.78	0	17.65
8	174.06	0	0	0	0	1	173	0	1.78	0	17.65
8	176.06	1	0	0	0	1	173	0	2.32	1	4.01
8	177.06	1	1	0	0	1	173	0	1.78	1	4.01
8	178.06	1	0	0	0	1	173	0	1.96	0	4.01
8	179.06	1	.	1	0	1	179	0	2.32	1	4.01
8	181.06	0	.	1	0	1	181	0	2.14	1	17.65
8	182.06	1	.	1	0	1	182	0	2.14	1	85.88
8	183.06	0	1	0	0	1	182	0	2.32	2	85.88
8	184.06	1	1	1	0	1	182	0	2.32	0	85.88
8	185.06	1	.	0	0	1	185	0	1.96	1	4.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	226.05	117.62	0.70	1.44	0.70	1.44	1	0	0	1.42
8	227.05	119.15	0.70	1.42	0.70	1.44	0		1	.
8	228.05	120.15	0.70	1.42	0.70	1.42	1	0	0	1.44
8	229.05	139.50	0.70	1.43	0.70	1.42	0		1	.
8	230.05	228.16	0.71	1.41	0.70	1.42	0		0	.
8	231.05	193.00	0.71	1.40	0.70	1.42	0		0	.
8	232.05	194.83	0.75	1.34	0.75	1.34	1	1	0	1.42
8	234.05	243.94	0.73	1.37	0.73	1.37	1	0	0	1.34
8	235.05	282.72	0.76	1.32	0.76	1.32	1	1	0	1.37
8	237.05	274.17	0.97	1.03	0.97	1.03	1	0	0	1.32
8	238.05	439.33	1.25	0.80	1.25	0.80	1	0	0	1.03
8	239.05	424.76	1.06	0.95	1.06	0.95	1	0	0	0.80
8	240.05	426.36	1.08	0.93	1.08	0.93	1	1	0	0.95
8	247.05	669.17	1.20	0.84	1.20	0.84	1	0	0	0.93
8	253.05	1087.65	1.51	0.66	1.51	0.66	1	0	0	0.84
8	254.05	1088.59	1.54	0.65	1.54	0.65	1	1	0	0.66
8	132.06	58.46	1.04	0.96	1.04	0.96	1	1	0	.
8	139.06	67.53	1.02	0.98	1.02	0.98	1	0	0	0.96
8	140.06	69.50	1.00	1.00	1.00	1.00	1	0	0	0.98
8	141.06	70.94	1.00	1.00	1.00	1.00	0		1	.
8	142.06	72.17	0.99	1.01	1.00	1.00	0		0	.
8	143.06	74.04	1.01	0.99	1.01	0.99	1	0	0	1.00
8	144.06	75.91	0.97	1.03	0.97	1.03	1	0	0	0.99
8	145.06	77.28	0.98	1.02	0.97	1.03	0		1	.
8	147.06	50.62	1.05	0.95	1.05	0.95	1	1	0	1.03
8	148.06	51.92	1.07	0.94	1.07	0.94	1	1	0	0.95
8	151.06	88.42	1.21	0.83	1.20	0.83	0		1	.
8	152.06	87.52	1.20	0.83	1.20	0.83	1	1	0	0.94
8	159.06	69.14	0.93	1.08	0.93	1.08	1	0	0	0.83
8	160.06	96.30	0.89	1.13	0.89	1.13	1	0	0	1.08
8	161.06	97.80	0.90	1.11	0.89	1.13	0		1	.
8	162.06	70.40	0.89	1.12	0.89	1.13	0		0	.
8	163.06	101.10	0.85	1.18	0.85	1.18	1	1	0	1.13
8	164.06	72.01	0.87	1.15	0.85	1.18	0		1	.
8	165.06	105.67	0.90	1.11	0.90	1.11	1	0	0	1.18
8	166.06	104.94	0.87	1.14	0.90	1.11	0		1	.
8	170.06	107.94	0.71	1.40	0.71	1.40	1	1	0	1.11
8	171.06	57.30	0.72	1.39	0.71	1.40	0		1	.
8	172.06	58.66	0.71	1.40	0.71	1.40	1	0	0	1.40
8	173.06	110.54	0.71	1.41	0.71	1.41	1	1	0	1.40
8	174.06	112.58	0.71	1.41	0.71	1.41	0		1	.
8	176.06	119.62	0.70	1.42	0.71	1.41	0		0	.
8	177.06	114.18	0.71	1.40	0.71	1.41	0		0	.
8	178.06	117.15	0.71	1.41	0.71	1.41	0		0	.
8	179.06	122.22	0.72	1.39	0.72	1.39	1	2	0	1.41
8	181.06	114.21	0.68	1.46	0.68	1.46	1	3	0	1.41
8	182.06	40.47	0.70	1.43	0.70	1.43	1	1	0	1.41
8	183.06	41.51	0.70	1.43	0.70	1.43	0		1	.
8	184.06	42.71	0.71	1.41	0.70	1.43	0		0	.
8	185.06	125.76	0.70	1.43	0.70	1.43	1	0	0	1.43

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	186.06	1	0	1	0	1	185	0	2.14	0	44.94
8	187.06	0	1	0	0	1	185	0	1.96	1	44.94
8	188.06	0	.	0	0	1	188	0	1.78	1	4.01
8	189.06	1	1	1	0	1	188	0	1.78	1	4.01
8	190.06	0	1	1	0	1	188	0	1.78	1	17.65
8	191.06	1	1	1	0	1	188	0	1.78	0	31.30
8	192.06	1	0	1	0	1	188	0	1.96	1	44.94
8	193.06	0	1	0	0	1	188	0	1.96	1	72.24
8	194.06	0	.	0	0	1	194	0	1.96	0	72.24
8	195.06	1	.	1	0	1	195	0	1.78	1	17.65
8	196.06	1	0	1	0	1	195	0	1.78	0	17.65
8	197.06	0	1	0	0	2	195	0	1.78	1	72.24
8	198.06	0	0	1	1	1	195	0	1.96	0	72.24
8	199.06	0	.	0	0	3	199	0	2.14	1	17.65
8	200.06	1	1	1	0	1	199	0	1.78	1	17.65
8	201.06	1	0	1	0	2	199	0	1.78	0	17.65
8	202.06	1	0	1	0	2	199	0	1.60	1	17.65
8	203.06	1	0	1	0	1	199	0	1.96	2	17.65
8	204.06	0	1	1	1	1	199	0	1.96	1	72.24
8	205.06	1	1	1	0	1	199	0	2.14	1	4.01
8	206.06	0	1	1	0	2	199	0	2.14	1	31.30
8	207.06	1	.	0	0	2	207	0	2.32	0	85.88
8	210.06	1	.	0	0	.	210	0	2.32	1	44.94
8	211.06	0	.	1	0	1	211	0	1.78	2	58.59
8	212.06	0	.	0	0	1	212	0	1.60	1	58.59
8	213.06	1	.	1	0	1	213	0	1.78	1	31.30
8	214.06	0	.	0	0	1	214	0	1.78	1	58.59
8	215.06	1	1	1	0	1	214	0	2.14	0	58.59
8	216.06	0	1	0	1	1	214	0	2.14	1	72.24
8	217.06	0	0	0	1	1	214	0	2.14	0	72.24
8	218.06	0	0	1	1	1	214	0	1.60	2	72.24
8	219.06	0	0	0	0	1	214	0	1.43	1	85.88
8	220.06	1	.	1	0	.	220	0	0.89	1	99.53
8	222.06	1	.	1	0	.	222	0	1.07	1	58.59
8	223.06	1	.	0	0	.	223	0	1.07	1	58.59
8	224.06	0	1	0	0	1	223	0	1.25	1	58.59
8	225.06	0	0	1	1	1	223	0	1.43	2	58.59
8	226.06	1	.	1	0	.	226	0	1.43	1	85.88
8	227.06	1	0	1	0	1	226	0	1.60	2	85.88
8	228.06	0	.	1	0	.	228	0	1.07	1	85.88
8	229.06	0	.	1	0	2	229	0	1.07	0	85.88
8	230.06	0	.	1	0	1	230	0	1.25	1	4.01
8	231.06	0	.	1	0	.	231	0	1.07	1	72.24
8	232.06	0	.	1	0	.	232	0	0.89	0	72.24
8	234.06	0	.	0	0	.	234	0	0.89	1	17.65
8	235.06	1	.	1	0	.	235	0	0.89	1	17.65
8	237.06	0	.	0	0	.	237	0	0.36	0	99.53
8	239.06	0	.	1	0	.	239	0	0.71	1	99.53
8	240.06	0	.	1	0	1	240	0	0.71	0	99.53
8	247.06	0	.	1	0	.	247	0	0.36	1	58.59

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	186.06	92.73	0.70	1.43	0.70	1.43	0		1	.
8	187.06	94.33	0.70	1.43	0.70	1.43	0		0	.
8	188.06	128.43	0.69	1.44	0.69	1.44	1	0	0	1.43
8	189.06	131.63	0.69	1.45	0.69	1.44	0		1	.
8	190.06	128.79	0.69	1.44	0.69	1.44	0		0	.
8	191.06	95.43	0.71	1.41	0.69	1.44	0		0	.
8	192.06	95.93	0.71	1.42	0.69	1.44	0		0	.
8	193.06	72.88	0.48	2.08	0.69	1.44	0		0	.
8	194.06	74.15	0.48	2.10	0.48	2.10	1	0	0	1.44
8	195.06	139.01	0.47	2.11	0.47	2.11	1	0	0	2.10
8	196.06	141.31	0.47	2.12	0.47	2.11	0		1	.
8	197.06	75.85	0.47	2.11	0.47	2.11	0		0	.
8	198.06	77.92	0.48	2.08	0.47	2.11	0		0	.
8	199.06	148.68	0.48	2.09	0.48	2.09	1	0	0	2.11
8	200.06	150.05	0.47	2.11	0.48	2.09	0		1	.
8	201.06	151.42	0.40	2.50	0.48	2.09	0		0	.
8	202.06	152.92	0.40	2.49	0.48	2.09	0		0	.
8	203.06	154.25	0.40	2.48	0.48	2.09	0		0	.
8	204.06	81.65	0.40	2.48	0.48	2.09	0		0	.
8	205.06	159.89	0.40	2.50	0.48	2.09	0		0	.
8	206.06	114.25	0.40	2.53	0.48	2.09	0		0	.
8	207.06	69.53	0.39	2.57	0.39	2.57	1	0	0	2.09
8	210.06	113.88	0.38	2.62	0.38	2.62	1	0	0	2.57
8	211.06	99.37	0.30	3.32	0.30	3.32	1	1	0	2.62
8	212.06	97.87	0.23	4.44	0.23	4.44	1	1	0	3.32
8	213.06	129.26	0.23	4.44	0.23	4.44	1	1	0	4.44
8	214.06	100.87	0.23	4.40	0.23	4.40	1	0	0	4.44
8	215.06	102.14	0.23	4.43	0.23	4.40	0		1	.
8	216.06	112.95	0.22	4.45	0.23	4.40	0		0	.
8	217.06	116.69	0.23	4.44	0.23	4.40	0		0	.
8	218.06	118.56	0.23	4.43	0.23	4.40	0		0	.
8	219.06	113.68	0.23	4.43	0.23	4.40	0		0	.
8	220.06	114.58	0.23	4.29	0.23	4.29	1	0	0	4.40
8	222.06	137.14	0.24	4.24	0.24	4.24	1	1	0	4.29
8	223.06	139.31	0.24	4.19	0.24	4.19	1	1	0	4.24
8	224.06	142.51	0.24	4.19	0.24	4.19	0		1	.
8	225.06	144.05	0.24	4.19	0.24	4.19	0		0	.
8	226.06	117.62	0.24	4.16	0.24	4.16	1	1	0	4.19
8	227.06	119.15	0.24	4.11	0.24	4.16	0		1	.
8	228.06	120.15	0.28	3.57	0.28	3.57	1	0	0	4.16
8	229.06	139.50	0.28	3.58	0.28	3.58	1	1	0	3.57
8	230.06	228.16	0.28	3.57	0.28	3.57	1	1	0	3.58
8	231.06	193.00	0.28	3.54	0.28	3.54	1	1	0	3.57
8	232.06	194.83	0.29	3.43	0.29	3.43	1	0	0	3.54
8	234.06	243.94	0.32	3.09	0.32	3.09	1	1	0	3.43
8	235.06	282.72	0.52	1.92	0.52	1.92	1	0	0	3.09
8	237.06	274.17	0.93	1.07	0.93	1.07	1	0	0	1.92
8	239.06	424.76	1.09	0.92	1.09	0.92	1	0	0	1.07
8	240.06	426.36	1.07	0.94	1.07	0.94	1	0	0	0.92
8	247.06	669.17	1.27	0.79	1.27	0.79	1	0	0	0.94

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	253.06	0	.	1	0	.	253	0	0.36	0	85.88
8	254.06	0	.	1	0	.	254	0	0.71	1	85.88
8	147.07	0	.	0	0	.	147	0	0.89	1	4.01
8	148.07	0	.	0	0	2	148	0	0.89	0	4.01
8	159.07	1	.	1	0	.	159	0	0.36	1	4.01
8	162.07	0	.	0	0	1	162	0	1.07	2	4.01
8	164.07	1	.	1	0	2	164	0	1.43	1	4.01
8	171.07	0	.	0	0	.	171	0	1.25	0	44.94
8	172.07	0	.	0	0	.	172	0	1.78	1	44.94
8	182.07	1	.	1	0	.	182	0	1.43	1	58.59
8	183.07	0	.	0	0	1	183	0	1.60	0	58.59
8	184.07	1	.	1	0	1	184	0	1.78	0	58.59
8	186.07	1	.	1	0	.	186	0	1.43	1	17.65
8	187.07	0	.	0	0	.	187	0	1.43	0	17.65
8	191.07	1	.	1	0	2	191	0	1.60	0	4.01
8	192.07	1	.	1	0	1	192	0	1.78	1	17.65
8	193.07	0	.	0	0	.	193	0	1.60	1	44.94
8	194.07	0	.	0	0	1	194	0	1.60	0	44.94
8	197.07	0	.	0	0	.	197	0	1.43	1	44.94
8	198.07	0	.	1	1	2	198	0	1.43	1	44.94
8	204.07	0	.	1	1	.	204	0	1.25	1	44.94
8	206.07	0	.	1	0	2	206	0	1.60	1	4.01
8	207.07	1	.	0	0	.	207	0	1.43	0	58.59
8	210.07	1	.	0	0	.	210	0	1.25	1	17.65
8	211.07	0	.	1	0	1	211	0	1.25	2	31.30
8	212.07	0	.	0	0	.	212	0	1.25	1	31.30
8	213.07	1	.	1	0	.	213	0	1.43	1	4.01
8	214.07	0	.	0	0	.	214	0	1.25	1	31.30
8	215.07	1	1	1	0	1	214	0	1.60	2	31.30
8	216.07	0	.	0	1	.	216	0	1.43	1	44.94
8	217.07	0	.	0	1	.	217	0	1.25	1	44.94
8	218.07	0	.	1	1	.	218	0	1.25	0	44.94
8	219.07	0	.	0	0	.	219	0	0.89	1	58.59
8	220.07	1	.	1	0	.	220	0	0.53	0	72.24
8	222.07	1	.	1	0	.	222	0	0.53	1	31.30
8	223.07	1	.	0	0	.	223	0	0.71	1	31.30
8	224.07	0	1	0	0	1	223	0	1.07	1	31.30
8	225.07	0	0	1	1	1	223	0	1.07	2	31.30
8	226.07	1	.	1	0	.	226	0	0.89	1	58.59
8	227.07	1	0	1	0	1	226	0	1.07	2	58.59
8	228.07	0	.	1	0	.	228	0	0.89	1	58.59
8	229.07	0	.	1	0	.	229	0	0.71	0	58.59
8	231.07	0	.	1	0	.	231	0	0.53	1	44.94
8	232.07	0	.	1	0	.	232	0	0.36	0	44.94
8	237.07	0	.	0	0	.	237	0	0.36	2	72.24
8	239.07	0	.	1	0	.	239	0	0.71	1	72.24
8	240.07	0	0	1	0	1	239	0	0.71	0	72.24
8	247.07	0	.	1	0	.	247	0	0.36	1	31.30
8	253.07	0	.	1	0	.	253	0	0.36	1	58.59
8	254.07	0	.	1	0	.	254	0	0.71	1	58.59

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	253.06	1087.65	1.66	0.60	1.66	0.60	1	0	0	0.79
8	254.06	1088.59	1.74	0.58	1.74	0.58	1	0	0	0.60
8	147.07	50.62	0.86	1.16	0.86	1.16	1	0	0	.
8	148.07	51.92	0.86	1.16	0.86	1.16	1	0	0	1.16
8	159.07	69.14	1.01	0.99	1.01	0.99	1	0	0	1.16
8	162.07	70.40	0.91	1.10	0.91	1.10	1	4	0	0.99
8	164.07	72.01	0.82	1.21	0.82	1.21	1	1	0	1.10
8	171.07	57.30	0.72	1.39	0.72	1.39	1	1	0	1.21
8	172.07	58.66	0.73	1.38	0.73	1.38	1	1	0	1.39
8	182.07	40.47	0.60	1.66	0.60	1.66	1	1	0	1.38
8	183.07	41.51	0.62	1.62	0.62	1.62	1	1	0	1.66
8	184.07	42.71	0.62	1.62	0.62	1.62	1	1	0	1.62
8	186.07	92.73	0.75	1.34	0.75	1.34	1	1	0	1.62
8	187.07	94.33	0.76	1.31	0.76	1.31	1	1	0	1.34
8	191.07	95.43	0.64	1.56	0.64	1.56	1	1	0	1.31
8	192.07	95.93	0.64	1.57	0.64	1.57	1	1	0	1.56
8	193.07	72.88	0.65	1.54	0.65	1.54	1	1	0	1.57
8	194.07	74.15	0.65	1.55	0.65	1.55	1	1	0	1.54
8	197.07	75.85	0.60	1.67	0.60	1.67	1	1	0	1.55
8	198.07	77.92	0.59	1.69	0.59	1.69	1	1	0	1.67
8	204.07	81.65	0.55	1.80	0.55	1.80	1	1	0	1.69
8	206.07	114.25	0.54	1.86	0.54	1.86	1	1	0	1.80
8	207.07	69.53	0.59	1.68	0.59	1.68	1	2	0	1.86
8	210.07	113.88	0.52	1.91	0.52	1.91	1	3	0	1.86
8	211.07	99.37	0.60	1.68	0.60	1.68	1	1	0	1.74
8	212.07	97.87	0.57	1.74	0.57	1.74	1	1	0	1.86
8	213.07	129.26	0.60	1.66	0.60	1.66	1	1	0	1.68
8	214.07	100.87	0.61	1.65	0.61	1.65	1	1	0	1.66
8	215.07	102.14	0.61	1.63	0.61	1.65	0		1	.
8	216.07	112.95	0.66	1.52	0.66	1.52	1	1	0	1.65
8	217.07	116.69	0.69	1.46	0.69	1.46	1	1	0	1.52
8	218.07	118.56	0.70	1.42	0.70	1.42	1	1	0	1.46
8	219.07	113.68	0.93	1.07	0.93	1.07	1	1	0	1.42
8	220.07	114.58	1.09	0.92	1.09	0.92	1	2	0	1.07
8	222.07	137.14	0.83	1.20	0.83	1.20	1	3	0	1.07
8	223.07	139.31	0.95	1.05	0.95	1.05	1	0	0	1.07
8	224.07	142.51	0.95	1.06	0.95	1.05	0		1	.
8	225.07	144.05	0.94	1.06	0.95	1.05	0		0	.
8	226.07	117.62	1.02	0.98	1.02	0.98	1	0	0	1.05
8	227.07	119.15	0.96	1.04	1.02	0.98	0		1	.
8	228.07	120.15	0.65	1.54	0.65	1.54	1	0	0	0.98
8	229.07	139.50	0.67	1.48	0.67	1.48	1	0	0	1.54
8	231.07	193.00	1.27	0.79	1.27	0.79	1	0	0	1.48
8	232.07	194.83	1.18	0.85	1.18	0.85	1	0	0	0.79
8	237.07	274.17	0.98	1.02	0.98	1.02	1	0	0	0.85
8	239.07	424.76	1.01	0.99	1.01	0.99	1	0	0	1.02
8	240.07	426.36	1.02	0.98	1.01	0.99	0		1	.
8	247.07	669.17	1.14	0.88	1.14	0.88	1	0	0	0.99
8	253.07	1087.65	0.64	1.57	0.64	1.57	1	0	0	0.88
8	254.07	1088.59	0.66	1.52	0.66	1.52	1	1	0	1.57

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	257.07	0	.	1	0	.	257	0	0.53	1	4.01
8	258.07	0	.	1	0	.	258	0	0.53	1	4.01
8	171.08	0	.	0	0	.	171	0	0.71	0	17.65
8	172.08	0	.	0	0	.	172	0	1.07	1	17.65
8	182.08	1	.	1	0	.	182	0	0.71	0	31.30
8	183.08	0	.	0	0	2	183	0	0.71	1	31.30
8	184.08	1	.	1	0	2	184	0	1.07	0	31.30
8	193.08	0	.	0	0	.	193	0	0.71	0	17.65
8	194.08	0	.	0	0	2	194	0	0.89	0	17.65
8	197.08	0	.	0	0	.	197	0	1.07	0	17.65
8	198.08	0	.	1	1	3	198	0	1.07	1	17.65
8	204.08	0	.	1	1	.	204	0	0.53	1	17.65
8	207.08	1	.	0	0	.	207	0	0.53	0	31.30
8	211.08	0	.	1	0	2	211	0	0.71	1	4.01
8	212.08	0	.	0	0	.	212	0	0.71	0	4.01
8	214.08	0	.	0	0	.	214	0	0.89	1	4.01
8	215.08	1	1	1	0	1	214	0	1.07	0	4.01
8	216.08	0	.	0	1	.	216	0	0.53	1	17.65
8	217.08	0	.	0	1	.	217	0	0.71	1	17.65
8	218.08	0	.	1	1	.	218	0	0.71	0	17.65
8	219.08	0	.	0	0	.	219	0	0.36	1	31.30
8	220.08	1	.	1	0	.	220	0	0.71	1	44.94
8	222.08	1	.	1	0	.	222	0	0.53	1	4.01
8	223.08	1	.	0	0	.	223	0	0.89	1	4.01
8	224.08	0	1	0	0	1	223	0	1.07	0	4.01
8	225.08	0	0	1	1	1	223	0	1.43	0	4.01
8	226.08	1	.	1	0	.	226	0	1.07	1	31.30
8	227.08	1	0	1	0	1	226	0	1.07	2	31.30
8	228.08	0	.	1	0	.	228	0	1.07	0	31.30
8	229.08	0	.	1	0	.	229	0	0.53	0	31.30
8	231.08	0	.	1	0	.	231	0	0.36	0	17.65
8	232.08	0	.	1	0	.	232	0	0.53	0	17.65
8	237.08	0	.	0	0	.	237	0	0.36	0	44.94
8	239.08	0	.	1	0	.	239	0	0.36	1	44.94
8	240.08	0	.	1	0	2	240	0	0.71	0	44.94
8	247.08	0	.	1	0	.	247	0	0.36	1	4.01
8	253.08	0	.	1	0	.	253	0	0.36	1	31.30
8	254.08	0	.	1	0	.	254	0	0.71	1	31.30
8	182.09	1	.	1	0	.	182	0	0.53	0	4.01
8	183.09	0	1	0	0	2	182	0	0.71	1	4.01
8	184.09	1	1	1	0	1	182	0	1.07	2	4.01
8	207.09	1	.	0	0	.	207	0	0.36	1	4.01
8	219.09	0	.	0	0	.	219	0	0.36	1	4.01
8	220.09	1	.	1	0	.	220	0	0.71	1	17.65
8	226.09	1	.	1	0	.	226	0	1.07	1	4.01
8	227.09	1	0	1	0	1	226	0	1.25	0	4.01
8	228.09	0	.	1	0	.	228	0	1.07	1	4.01
8	229.09	0	.	1	0	.	229	0	0.36	2	4.01
8	237.09	0	.	0	0	.	237	0	0.36	0	17.65
8	239.09	0	.	1	0	.	239	0	0.36	1	17.65

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	257.07	262.83	0.12	8.68	0.12	8.68	1	3	0	.
8	258.07	261.43	0.11	8.78	0.11	8.78	1	3	0	.
8	171.08	57.30	1.56	0.64	1.56	0.64	1	0	0	.
8	172.08	58.66	1.58	0.63	1.58	0.63	1	0	0	0.64
8	182.08	40.47	1.52	0.66	1.52	0.66	1	0	0	0.63
8	183.08	41.51	1.48	0.68	1.48	0.68	1	0	0	0.66
8	184.08	42.71	1.45	0.69	1.45	0.69	1	0	0	0.68
8	193.08	72.88	1.04	0.96	1.04	0.96	1	0	0	0.69
8	194.08	74.15	1.06	0.95	1.06	0.95	1	0	0	0.96
8	197.08	75.85	1.05	0.95	1.05	0.95	1	0	0	0.95
8	198.08	77.92	1.09	0.92	1.09	0.92	1	0	0	0.95
8	204.08	81.65	0.97	1.03	0.97	1.03	1	0	0	0.92
8	207.08	69.53	1.10	0.91	1.10	0.91	1	0	0	1.03
8	211.08	99.37	1.08	0.92	1.08	0.92	1	0	0	0.93
8	212.08	97.87	1.07	0.93	1.07	0.93	1	0	0	0.91
8	214.08	100.87	0.93	1.07	0.93	1.07	1	0	0	0.92
8	215.08	102.14	0.95	1.06	0.93	1.07	0		1	.
8	216.08	112.95	1.15	0.87	1.15	0.87	1	0	0	1.07
8	217.08	116.69	1.12	0.90	1.12	0.90	1	0	0	0.87
8	218.08	118.56	1.08	0.93	1.08	0.93	1	0	0	0.90
8	219.08	113.68	1.24	0.80	1.24	0.80	1	0	0	0.93
8	220.08	114.58	1.07	0.94	1.07	0.94	1	0	0	0.88
8	222.08	137.14	1.14	0.88	1.14	0.88	1	0	0	0.80
8	223.08	139.31	1.01	0.99	1.01	0.99	1	0	0	0.94
8	224.08	142.51	1.01	0.99	1.01	0.99	0		1	.
8	225.08	144.05	0.99	1.01	1.01	0.99	0		0	.
8	226.08	117.62	0.91	1.10	0.91	1.10	1	0	0	0.99
8	227.08	119.15	0.90	1.11	0.91	1.10	0		1	.
8	228.08	120.15	0.90	1.12	0.90	1.12	1	0	0	1.10
8	229.08	139.50	1.11	0.90	1.11	0.90	1	0	0	1.12
8	231.08	193.00	1.56	0.64	1.56	0.64	1	0	0	0.90
8	232.08	194.83	1.39	0.72	1.39	0.72	1	0	0	0.64
8	237.08	274.17	1.02	0.98	1.02	0.98	1	0	0	0.72
8	239.08	424.76	1.18	0.85	1.18	0.85	1	0	0	0.98
8	240.08	426.36	1.19	0.84	1.19	0.84	1	1	0	0.85
8	247.08	669.17	0.09	10.90	0.09	10.90	1	0	0	.
8	253.08	1087.65	1.78	0.56	1.78	0.56	1	0	0	0.84
8	254.08	1088.59	1.61	0.62	1.61	0.62	1	0	0	0.56
8	182.09	40.47	1.38	0.73	1.38	0.73	1	0	0	.
8	183.09	41.51	1.36	0.74	1.38	0.73	0		1	.
8	184.09	42.71	1.35	0.74	1.38	0.73	0		0	.
8	207.09	69.53	1.07	0.93	1.07	0.93	1	1	0	0.73
8	219.09	113.68	1.32	0.76	1.32	0.76	1	0	0	0.93
8	220.09	114.58	1.11	0.90	1.11	0.90	1	0	0	0.76
8	226.09	117.62	0.97	1.03	0.97	1.03	1	0	0	0.90
8	227.09	119.15	0.97	1.04	0.97	1.03	0		1	.
8	228.09	120.15	0.91	1.10	0.91	1.10	1	0	0	1.03
8	229.09	139.50	1.36	0.73	1.36	0.73	1	0	0	1.10
8	237.09	274.17	1.03	0.97	1.03	0.97	1	0	0	0.73
8	239.09	424.76	1.03	0.97	1.03	0.97	1	0	0	0.97

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
8	240.09	0	.	1	0	1	240	0	0.71	0	17.65
8	253.09	0	.	1	0	.	253	0	0.36	1	4.01
8	254.09	0	.	1	0	2	254	0	0.71	0	4.01
9	10	0	.	0	0	.	10	0	0.36	1	4.01
9	11	0	0	0	0	2	10	0	0.71	0	4.01
9	12	0	.	0	0	.	12	0	0.71	0	4.01
9	13	0	0	1	0	1	12	0	1.07	2	4.01
9	14	0	.	0	0	2	14	0	0.89	0	4.01
9	16	1	.	0	0	.	16	0	0.71	2	4.01
9	18	1	.	0	0	.	18	0	0.71	2	4.01
9	19	1	.	0	0	2	19	0	0.89	2	4.01
9	20	1	0	0	0	1	19	0	1.07	0	4.01
9	26	0	.	0	1	.	26	0	0.53	0	4.01
9	27	0	.	0	0	1	27	0	0.71	2	4.01
9	30	0	.	0	1	.	30	0	0.53	2	4.01
9	31	0	.	0	0	.	31	0	0.53	2	4.01
9	35	1	.	0	0	.	35	0	0.89	0	4.01
9	36	1	0	1	0	1	35	0	1.07	1	4.01
9	37	1	.	1	0	.	37	0	0.71	1	17.65
9	38	0	1	0	0	1	37	0	1.07	1	4.01
9	39	0	.	0	0	.	39	0	1.25	0	17.65
9	40	1	.	1	0	.	40	0	1.07	2	4.01
9	41	1	.	1	0	1	41	0	1.25	1	4.01
9	42	1	0	1	0	1	41	0	1.60	0	4.01
9	46	0	.	1	0	2	46	0	1.43	1	17.65
9	47	0	0	0	0	1	46	0	1.43	2	17.65
9	48	1	.	1	0	.	48	0	0.89	2	4.01
9	49	1	.	0	0	.	49	0	0.53	1	4.01
9	50	1	.	1	0	.	50	0	1.43	1	4.01
9	51	1	.	1	0	.	51	0	1.25	2	31.30
9	52	1	.	1	1	2	52	0	1.43	2	31.30
9	53	1	0	1	0	1	52	0	1.25	0	31.30
9	54	0	1	0	0	1	52	0	1.43	1	4.01
9	55	0	0	0	0	2	52	0	1.43	2	4.01
9	57	0	.	0	0	2	57	0	0.53	1	4.01
9	59	0	.	0	0	1	59	0	1.60	0	31.30
9	60	0	0	0	0	1	59	0	1.60	1	31.30
9	61	0	0	0	0	1	59	0	1.60	0	17.65
9	65	1	.	0	0	.	65	0	1.25	1	58.59
9	66	1	.	0	0	1	66	0	1.43	1	58.59
9	67	1	.	1	0	1	67	0	1.43	1	31.30
9	68	0	1	0	0	1	67	0	1.43	1	17.65
9	69	1	1	1	1	1	67	0	1.43	2	17.65
9	70	0	1	0	0	1	67	0	1.43	1	58.59
9	71	0	.	0	0	2	71	0	1.43	1	113.17
9	72	1	1	1	0	1	71	0	1.43	0	113.17
9	73	1	.	1	0	1	73	0	1.78	2	31.30
9	74	0	.	0	0	1	74	0	1.43	0	4.01
9	75	0	0	0	0	1	74	0	1.60	1	113.17
9	77	0	.	1	0	1	77	0	1.60	1	58.59

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
8	240.09	426.36	1.04	0.96	1.04	0.96	1	0	0	0.97
8	253.09	1087.65	1.73	0.58	1.73	0.58	1	0	0	0.96
8	254.09	1088.59	1.64	0.61	1.64	0.61	1	0	0	0.58
9	10	33.50	1.40	0.71	1.40	0.71	1	0	0	.
9	11	36.64	1.41	0.71	1.40	0.71	0		1	.
9	12	37.04	1.37	0.73	1.37	0.73	1	0	0	0.71
9	13	38.74	1.37	0.73	1.37	0.73	0		1	.
9	14	40.31	1.39	0.72	1.39	0.72	1	1	0	0.73
9	16	41.68	1.29	0.78	1.29	0.78	1	0	0	0.72
9	18	43.08	1.21	0.83	1.21	0.83	1	0	0	0.78
9	19	45.58	1.21	0.83	1.21	0.83	1	0	0	0.83
9	20	46.48	1.20	0.83	1.21	0.83	0		1	.
9	26	55.39	1.00	1.00	1.00	1.00	1	0	0	0.83
9	27	59.03	1.08	0.93	1.08	0.93	1	2	0	1.00
9	30	57.19	0.87	1.15	0.87	1.15	1	3	0	1.00
9	31	66.47	0.97	1.03	0.97	1.03	1	1	0	1.00
9	35	68.04	0.94	1.07	0.94	1.07	1	1	0	1.03
9	36	69.41	0.93	1.07	0.94	1.07	0		1	.
9	37	67.90	0.93	1.07	0.93	1.07	1	0	0	1.07
9	38	72.08	0.94	1.07	0.93	1.07	0		1	.
9	39	74.01	0.95	1.06	0.95	1.06	1	1	0	1.07
9	40	80.78	0.98	1.02	0.98	1.02	1	2	0	1.06
9	41	75.25	0.92	1.09	0.92	1.09	1	3	0	1.06
9	42	78.52	0.93	1.07	0.92	1.09	0		1	.
9	46	76.35	0.88	1.13	0.88	1.13	1	1	0	1.06
9	47	77.68	0.88	1.14	0.88	1.13	0		1	.
9	48	91.53	0.94	1.06	0.94	1.06	1	2	0	1.13
9	49	90.49	0.91	1.10	0.91	1.10	1	3	0	1.13
9	50	93.56	0.95	1.05	0.95	1.05	1	1	0	1.13
9	51	66.04	0.97	1.03	0.97	1.03	1	0	0	1.05
9	52	67.57	0.96	1.05	0.96	1.05	1	0	0	1.03
9	53	69.97	0.95	1.05	0.96	1.05	0		1	.
9	54	95.27	0.95	1.05	0.96	1.05	0		0	.
9	55	98.77	0.96	1.04	0.96	1.05	0		0	.
9	57	87.49	0.94	1.07	0.94	1.07	1	1	0	1.05
9	59	71.41	0.91	1.10	0.91	1.10	1	1	0	1.07
9	60	68.67	0.90	1.11	0.91	1.10	0		1	.
9	61	103.01	0.91	1.10	0.91	1.10	0		0	.
9	65	48.01	0.84	1.20	0.84	1.20	1	0	0	1.10
9	66	49.81	0.84	1.19	0.84	1.19	1	0	0	1.20
9	67	77.41	0.83	1.21	0.83	1.21	1	0	0	1.19
9	68	108.88	0.83	1.21	0.83	1.21	0		1	.
9	69	110.35	0.82	1.21	0.83	1.21	0		0	.
9	70	46.74	0.83	1.21	0.83	1.21	0		0	.
9	71	16.28	0.81	1.23	0.81	1.23	1	0	0	1.21
9	72	14.68	0.82	1.22	0.81	1.23	0		1	.
9	73	87.26	0.86	1.16	0.86	1.16	1	2	0	1.23
9	74	117.02	0.81	1.23	0.81	1.23	1	3	0	1.23
9	75	20.36	0.81	1.23	0.81	1.23	0		1	.
9	77	67.56	0.83	1.21	0.83	1.21	1	1	0	1.23

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	78	0	.	1	0	2	78	0	1.43	1	31.30
9	80	1	.	1	0	.	80	0	1.25	0	31.30
9	81	0	1	0	0	1	80	0	1.43	1	113.17
9	82	0	0	0	0	1	80	0	1.43	1	113.17
9	83	1	.	0	0	1	83	0	1.60	1	4.01
9	84	0	.	0	0	1	84	0	1.43	1	31.30
9	85	0	.	0	0	1	85	0	1.25	0	31.30
9	86	1	.	1	0	.	86	0	1.25	1	99.53
9	87	0	1	0	0	1	86	0	1.60	0	99.53
9	88	0	0	0	0	2	86	0	1.60	1	17.65
9	89	0	.	0	0	1	89	0	1.43	0	17.65
9	90	1	.	1	0	1	90	0	1.43	0	17.65
9	91	1	.	1	0	.	91	0	1.25	0	17.65
9	93	1	.	1	0	1	93	0	1.60	2	31.30
9	94	1	.	1	0	1	94	0	1.43	0	113.17
9	95	1	.	0	0	1	95	0	1.43	1	113.17
9	96	0	1	0	0	1	95	0	1.60	2	58.59
9	97	1	1	1	1	1	95	0	1.60	0	31.30
9	98	1	0	1	0	1	95	0	1.43	1	31.30
9	99	1	0	0	0	1	95	0	1.78	2	31.30
9	100	0	1	0	0	1	95	0	1.78	1	113.17
9	101	1	1	1	1	1	95	0	1.25	1	113.17
9	102	0	1	0	0	1	95	0	1.43	1	113.17
9	103	0	0	0	0	1	95	0	1.43	0	58.59
9	104	0	0	1	0	2	95	0	1.43	1	85.88
9	105	0	.	0	0	3	105	0	1.07	0	58.59
9	106	1	1	1	0	1	105	0	1.07	0	58.59
9	107	1	.	1	0	.	107	0	1.07	1	4.01
9	108	1	0	1	1	2	107	0	1.43	1	4.01
9	109	1	0	1	0	2	107	0	1.25	1	31.30
9	110	1	.	1	0	.	110	0	1.43	0	113.17
9	111	0	.	0	0	1	111	0	1.25	1	113.17
9	112	1	.	0	0	1	112	0	1.60	1	31.30
9	113	0	1	0	0	1	112	0	1.60	2	85.88
9	114	1	.	1	0	1	114	0	1.43	1	72.24
9	115	1	.	1	0	1	115	0	1.43	1	113.17
9	116	0	1	0	0	1	115	0	1.43	1	58.59
9	117	1	.	1	0	2	117	0	1.43	0	72.24
9	118	1	0	1	0	1	117	0	1.25	1	72.24
9	119	0	1	1	0	1	117	0	1.43	1	58.59
9	120	1	.	1	1	2	120	0	1.43	1	85.88
9	121	1	0	1	0	2	120	0	1.25	1	72.24
9	122	1	.	1	0	.	122	0	1.07	2	58.59
9	123	0	1	0	0	1	122	0	1.25	1	85.88
9	124	1	.	0	0	.	124	0	1.07	0	72.24
9	125	0	1	0	0	2	124	0	1.25	1	72.24
9	126	1	.	1	0	3	126	0	1.25	1	113.17
9	127	1	0	1	0	2	126	0	1.25	0	72.24
9	128	1	0	1	0	1	126	0	1.25	1	17.65
9	129	1	0	1	0	1	126	0	1.43	0	17.65

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	78	89.83	0.83	1.21	0.83	1.21	1	0	0	1.21
9	80	91.23	0.81	1.24	0.81	1.24	1	0	0	1.21
9	81	22.19	0.81	1.23	0.81	1.24	0		1	.
9	82	23.49	0.81	1.23	0.81	1.24	0		0	.
9	83	130.43	0.82	1.22	0.82	1.22	1	0	0	1.24
9	84	94.03	0.81	1.23	0.81	1.23	1	0	0	1.22
9	85	97.40	0.81	1.24	0.81	1.24	1	0	0	1.23
9	86	52.52	0.83	1.21	0.83	1.21	1	0	0	1.24
9	87	53.75	0.83	1.20	0.83	1.21	0		1	.
9	88	133.80	0.83	1.20	0.83	1.21	0		0	.
9	89	135.84	0.84	1.19	0.84	1.19	1	0	0	1.21
9	90	137.91	0.84	1.19	0.84	1.19	1	0	0	1.19
9	91	140.08	0.84	1.19	0.84	1.19	1	0	0	1.19
9	93	104.14	0.81	1.23	0.81	1.23	1	1	0	1.19
9	94	31.80	0.81	1.23	0.81	1.23	1	0	0	1.23
9	95	32.87	0.81	1.24	0.81	1.24	1	0	0	1.23
9	96	81.14	0.80	1.24	0.81	1.24	0		1	.
9	97	105.31	0.81	1.24	0.81	1.24	0		0	.
9	98	108.21	0.82	1.22	0.81	1.24	0		0	.
9	99	111.15	0.82	1.23	0.81	1.24	0		0	.
9	100	34.04	0.82	1.22	0.81	1.24	0		0	.
9	101	35.24	0.83	1.21	0.81	1.24	0		0	.
9	102	36.57	0.83	1.21	0.81	1.24	0		0	.
9	103	84.55	0.84	1.19	0.81	1.24	0		0	.
9	104	62.99	0.84	1.19	0.81	1.24	0		0	.
9	105	89.22	0.85	1.17	0.85	1.17	1	0	0	1.24
9	106	91.75	0.85	1.17	0.85	1.17	0		1	.
9	107	171.04	0.84	1.19	0.84	1.19	1	0	0	1.17
9	108	172.71	0.84	1.19	0.84	1.19	0		1	.
9	109	121.76	0.85	1.18	0.84	1.19	0		0	.
9	110	39.31	0.85	1.18	0.85	1.18	1	2	0	1.19
9	111	37.44	0.82	1.22	0.82	1.22	1	3	0	1.19
9	112	127.50	0.84	1.19	0.84	1.19	1	1	0	1.19
9	113	66.46	0.83	1.20	0.84	1.19	0		1	.
9	114	91.62	0.83	1.20	0.83	1.20	1	0	0	1.19
9	115	40.41	0.84	1.20	0.84	1.20	1	0	0	1.20
9	116	94.76	0.84	1.19	0.84	1.20	0		1	.
9	117	96.69	0.84	1.19	0.84	1.19	1	0	0	1.20
9	118	98.93	0.84	1.19	0.84	1.19	0		1	.
9	119	100.30	0.85	1.18	0.84	1.19	0		0	.
9	120	68.17	0.85	1.18	0.85	1.18	1	0	0	1.19
9	121	102.63	0.85	1.18	0.85	1.18	0		1	.
9	122	105.27	0.83	1.20	0.83	1.20	1	0	0	1.18
9	123	69.77	0.84	1.19	0.83	1.20	0		1	.
9	124	107.10	0.82	1.22	0.82	1.22	1	0	0	1.20
9	125	108.81	0.83	1.21	0.82	1.22	0		1	.
9	126	41.74	0.83	1.20	0.83	1.20	1	0	0	1.22
9	127	112.98	0.83	1.20	0.83	1.20	0		1	.
9	128	203.24	0.84	1.20	0.83	1.20	0		0	.
9	129	206.48	0.83	1.21	0.83	1.20	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	130	0	.	1	0	.	130	0	1.25	2	58.59
9	131	1	.	1	0	1	131	0	1.25	1	58.59
9	133	1	.	1	0	1	133	0	1.25	1	85.88
9	134	0	.	0	0	2	134	0	1.43	0	72.24
9	135	1	1	0	0	1	134	0	1.25	2	113.17
9	136	1	0	1	0	1	134	0	1.25	1	85.88
9	137	0	1	0	0	1	134	0	1.60	2	72.24
9	138	0	.	0	0	1	138	0	1.43	0	31.30
9	139	1	1	1	0	1	138	0	1.43	1	4.01
9	140	0	.	0	0	2	140	0	1.43	0	72.24
9	141	0	.	0	0	1	141	0	1.43	0	31.30
9	142	1	.	1	0	1	142	0	1.25	1	113.17
9	143	0	.	0	0	.	143	0	1.25	2	58.59
9	144	1	1	1	0	1	143	0	1.25	1	58.59
9	145	0	1	0	0	1	143	0	1.60	0	72.24
9	146	0	0	1	0	1	143	0	1.60	0	85.88
9	147	0	.	0	0	.	147	0	1.43	1	113.17
9	148	0	0	0	0	1	147	0	1.43	1	113.17
9	149	0	0	1	0	1	147	0	1.43	2	72.24
9	150	0	0	0	0	1	147	0	1.60	1	72.24
9	151	0	.	0	0	1	151	0	1.43	2	72.24
9	152	1	1	1	0	1	151	0	1.60	1	113.17
9	153	1	0	1	0	1	151	0	1.78	1	113.17
9	154	1	0	0	0	1	151	0	1.78	2	72.24
9	155	0	1	0	0	1	151	0	1.60	1	72.24
9	156	1	.	1	0	1	156	0	1.60	1	85.88
9	157	1	0	1	1	1	156	0	1.43	1	85.88
9	158	0	.	1	0	1	158	0	1.43	2	31.30
9	159	0	.	1	0	2	159	0	1.43	1	72.24
9	160	1	.	1	1	1	160	0	1.43	1	72.24
9	161	1	.	1	0	2	161	0	1.25	1	72.24
9	162	0	.	0	1	2	162	0	1.25	0	113.17
9	163	0	0	0	0	2	162	0	1.25	1	85.88
9	164	0	.	0	0	1	164	0	1.25	0	85.88
9	165	0	0	0	0	1	164	0	1.25	1	72.24
9	166	0	.	1	0	.	166	0	1.07	1	72.24
9	167	0	0	0	0	1	166	0	1.43	2	72.24
9	168	0	.	0	1	1	168	0	1.43	2	113.17
9	169	0	.	0	0	1	169	0	1.43	0	113.17
9	170	0	.	1	0	1	170	0	1.60	1	72.24
9	171	0	.	1	0	1	171	0	1.60	2	72.24
9	172	0	.	0	0	1	172	0	1.78	0	72.24
9	173	1	.	1	0	2	173	0	1.43	1	85.88
9	174	0	.	1	0	1	174	0	1.60	2	72.24
9	175	1	.	1	0	.	175	0	1.25	1	72.24
9	176	1	.	1	1	2	176	0	1.25	1	72.24
9	177	1	0	1	0	1	176	0	1.43	1	72.24
9	178	1	0	0	0	1	176	0	1.25	1	72.24
9	179	0	.	0	0	.	179	0	1.07	0	85.88
9	180	0	.	1	0	.	180	0	0.89	1	113.17

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	130	118.55	0.85	1.18	0.85	1.18	1	2	0	1.20
9	131	114.24	0.81	1.24	0.81	1.24	1	3	0	1.20
9	133	72.60	0.80	1.25	0.80	1.25	1	0	0	1.20
9	134	116.61	0.81	1.23	0.81	1.23	1	0	0	1.25
9	135	43.65	0.81	1.24	0.81	1.23	0		1	.
9	136	74.71	0.81	1.24	0.81	1.23	0		0	.
9	137	121.55	0.81	1.24	0.81	1.23	0		0	.
9	138	165.30	0.80	1.24	0.80	1.24	1	0	0	1.23
9	139	222.86	0.80	1.24	0.80	1.24	0		1	.
9	140	123.49	0.82	1.21	0.82	1.21	1	1	0	1.24
9	141	177.21	0.83	1.20	0.83	1.20	1	0	0	1.21
9	142	45.78	0.83	1.20	0.83	1.20	1	0	0	1.20
9	143	133.20	0.79	1.26	0.79	1.26	1	0	0	1.20
9	144	130.83	0.78	1.29	0.79	1.26	0		1	.
9	145	128.36	0.79	1.26	0.79	1.26	0		0	.
9	146	77.01	0.80	1.25	0.79	1.26	0		0	.
9	147	46.38	0.80	1.25	0.80	1.25	1	0	0	1.26
9	148	49.48	0.81	1.24	0.80	1.25	0		1	.
9	149	135.67	0.80	1.25	0.80	1.25	0		0	.
9	150	136.80	0.81	1.23	0.80	1.25	0		0	.
9	151	139.20	0.79	1.26	0.79	1.26	1	0	0	1.25
9	152	53.52	0.80	1.25	0.79	1.26	0		1	.
9	153	57.69	0.81	1.24	0.79	1.26	0		0	.
9	154	143.11	0.80	1.24	0.79	1.26	0		0	.
9	155	144.97	0.81	1.23	0.79	1.26	0		0	.
9	156	83.65	0.83	1.21	0.83	1.21	1	3	0	1.26
9	157	87.48	0.84	1.20	0.83	1.21	0		1	.
9	158	208.18	0.85	1.18	0.85	1.18	1	2	0	1.26
9	159	150.71	0.85	1.18	0.85	1.18	1	1	0	1.26
9	160	152.65	0.85	1.18	0.85	1.18	1	0	0	1.18
9	161	154.52	0.84	1.19	0.84	1.19	1	0	0	1.18
9	162	59.03	0.85	1.17	0.85	1.17	1	1	0	1.19
9	163	89.89	0.86	1.16	0.85	1.17	0		1	.
9	164	91.79	0.88	1.14	0.88	1.14	1	0	0	1.17
9	165	160.46	0.88	1.14	0.88	1.14	0		1	.
9	166	161.89	0.85	1.17	0.85	1.17	1	0	0	1.14
9	167	164.09	0.85	1.18	0.85	1.17	0		1	.
9	168	60.33	0.86	1.17	0.86	1.17	1	0	0	1.17
9	169	64.90	0.86	1.16	0.86	1.16	1	0	0	1.17
9	170	170.30	0.87	1.15	0.87	1.15	1	2	0	1.16
9	171	173.67	0.85	1.17	0.85	1.17	1	3	0	1.16
9	172	171.77	0.87	1.16	0.87	1.16	1	1	0	1.16
9	173	96.89	0.86	1.17	0.86	1.17	1	0	0	1.16
9	174	177.04	0.86	1.17	0.86	1.17	1	0	0	1.17
9	175	179.01	0.83	1.20	0.83	1.20	1	0	0	1.17
9	176	181.18	0.84	1.19	0.84	1.19	1	1	0	1.20
9	177	173.38	0.85	1.17	0.84	1.19	0		1	.
9	178	184.95	0.85	1.17	0.84	1.19	0		0	.
9	179	100.86	0.86	1.16	0.86	1.16	1	0	0	1.19
9	180	66.84	0.85	1.18	0.85	1.18	1	0	0	1.16

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	181	0	0	0	0	1	180	0	1.25	2	113.17
9	182	0	0	0	0	1	180	0	1.43	1	58.59
9	183	0	0	1	0	2	180	0	1.43	2	58.59
9	184	0	0	0	0	2	180	0	1.43	0	85.88
9	185	0	0	0	0	2	180	0	1.43	1	99.53
9	186	0	0	1	0	2	180	0	1.25	1	31.30
9	187	0	.	0	0	2	187	0	1.25	2	85.88
9	188	0	.	0	0	.	188	0	1.25	2	113.17
9	189	0	0	1	0	1	188	0	1.25	1	113.17
9	190	0	.	0	1	1	190	0	1.60	0	126.82
9	191	0	0	1	0	1	190	0	1.43	2	126.82
9	192	1	.	0	0	.	192	0	1.25	2	126.82
9	193	0	1	1	0	2	192	0	1.25	2	85.88
9	194	0	0	0	0	1	192	0	1.25	1	72.24
9	195	0	0	1	0	1	192	0	1.07	2	72.24
9	196	1	1	1	0	1	192	0	1.43	1	72.24
9	197	0	1	0	0	2	192	0	1.25	2	58.59
9	198	0	.	1	0	2	198	0	1.25	2	85.88
9	199	0	.	1	0	2	199	0	1.07	0	72.24
9	200	1	.	1	0	2	200	0	1.07	1	72.24
9	201	0	1	0	1	2	200	0	1.07	0	113.17
9	202	0	0	1	0	1	200	0	1.07	1	72.24
9	203	1	.	1	0	1	203	0	1.25	2	72.24
9	204	0	1	0	0	2	203	0	1.25	1	72.24
9	205	0	.	1	0	2	205	0	1.25	0	85.88
9	206	0	.	0	0	.	206	0	1.07	1	72.24
9	207	0	0	0	0	2	206	0	1.25	0	72.24
9	208	0	.	0	0	.	208	0	0.89	1	72.24
9	209	0	0	1	0	2	208	0	1.07	0	85.88
9	210	0	0	0	0	1	208	0	1.25	2	72.24
9	211	0	0	0	0	1	208	0	1.25	1	113.17
9	212	1	.	1	0	2	212	0	1.25	0	72.24
9	213	0	1	1	0	2	212	0	1.25	0	85.88
9	214	1	1	1	0	2	212	0	1.25	0	85.88
9	215	0	1	1	0	1	212	0	1.43	1	113.17
9	216	0	.	1	0	.	216	0	1.07	1	113.17
9	217	0	0	0	0	1	216	0	1.25	0	113.17
9	218	0	0	0	0	1	216	0	1.25	1	85.88
9	219	1	.	1	0	.	219	0	1.25	0	85.88
9	220	1	.	1	0	1	220	0	1.25	1	85.88
9	221	1	0	0	0	1	220	0	1.43	1	113.17
9	222	0	.	0	0	.	222	0	1.25	0	113.17
9	223	0	0	1	0	2	222	0	1.25	0	113.17
9	224	1	.	1	0	.	224	0	1.07	1	126.82
9	225	1	0	1	0	1	224	0	1.25	2	126.82
9	226	1	0	1	0	1	224	0	1.43	1	167.75
9	227	0	1	0	0	1	224	0	1.60	2	167.75
9	228	1	1	1	0	2	224	0	1.60	0	167.75
9	229	0	1	0	0	1	224	0	1.43	0	181.40
9	230	1	1	1	0	1	224	0	1.43	1	154.11

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	181	68.17	0.84	1.19	0.85	1.18	0		1	.
9	182	199.16	0.84	1.19	0.85	1.18	0		0	.
9	183	211.17	0.85	1.18	0.85	1.18	0		0	.
9	184	105.17	0.85	1.18	0.85	1.18	0		0	.
9	185	97.63	0.86	1.17	0.85	1.18	0		0	.
9	186	258.06	0.86	1.16	0.85	1.18	0		0	.
9	187	112.44	0.86	1.16	0.86	1.16	1	0	0	1.18
9	188	71.21	0.85	1.18	0.85	1.18	1	0	0	1.16
9	189	69.64	0.84	1.18	0.85	1.18	0		1	.
9	190	74.34	0.85	1.18	0.85	1.18	1	0	0	1.18
9	191	75.78	0.84	1.19	0.85	1.18	0		1	.
9	192	77.78	0.83	1.20	0.83	1.20	1	0	0	1.18
9	193	120.35	0.84	1.20	0.83	1.20	0		1	.
9	194	227.59	0.84	1.18	0.83	1.20	0		0	.
9	195	227.69	0.83	1.20	0.83	1.20	0		0	.
9	196	229.59	0.84	1.19	0.83	1.20	0		0	.
9	197	231.63	0.85	1.18	0.83	1.20	0		0	.
9	198	122.25	0.86	1.16	0.86	1.16	1	1	0	1.20
9	199	233.30	0.86	1.16	0.86	1.16	1	0	0	1.16
9	200	235.30	0.87	1.15	0.87	1.15	1	1	0	1.16
9	201	738.91	0.87	1.15	0.87	1.15	0		1	.
9	202	239.00	0.87	1.15	0.87	1.15	0		0	.
9	203	240.94	0.86	1.16	0.86	1.16	1	0	0	1.15
9	204	242.71	0.87	1.15	0.86	1.16	0		1	.
9	205	139.80	0.87	1.15	0.87	1.15	1	0	0	1.16
9	206	246.41	0.87	1.16	0.87	1.16	1	0	0	1.15
9	207	247.98	0.86	1.16	0.87	1.16	0		1	.
9	208	249.78	0.84	1.19	0.84	1.19	1	0	0	1.16
9	209	146.34	0.84	1.19	0.84	1.19	0		1	.
9	210	252.85	0.85	1.18	0.84	1.19	0		0	.
9	211	81.48	0.85	1.18	0.84	1.19	0		0	.
9	212	256.59	0.84	1.18	0.84	1.18	1	0	0	1.19
9	213	156.72	0.85	1.18	0.84	1.18	0		1	.
9	214	184.35	0.85	1.18	0.84	1.18	0		0	.
9	215	83.32	0.86	1.16	0.84	1.18	0		0	.
9	216	85.02	0.87	1.14	0.87	1.14	1	0	0	1.18
9	217	86.69	0.87	1.15	0.87	1.14	0		1	.
9	218	165.39	0.87	1.15	0.87	1.14	0		0	.
9	219	187.25	0.87	1.14	0.87	1.14	1	0	0	1.14
9	220	190.42	0.87	1.15	0.87	1.15	1	0	0	1.14
9	221	90.49	0.88	1.14	0.87	1.15	0		1	.
9	222	94.80	0.88	1.14	0.88	1.14	1	0	0	1.15
9	223	97.23	0.88	1.13	0.88	1.14	0		1	.
9	224	102.57	0.83	1.20	0.83	1.20	1	0	0	1.14
9	225	104.37	0.83	1.20	0.83	1.20	0		1	.
9	226	52.68	0.84	1.19	0.83	1.20	0		0	.
9	227	54.15	0.84	1.19	0.83	1.20	0		0	.
9	228	55.55	0.85	1.18	0.83	1.20	0		0	.
9	229	51.38	0.85	1.17	0.83	1.20	0		0	.
9	230	84.09	0.86	1.16	0.83	1.20	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	231	0	1	0	0	1	224	0	1.25	1	126.82
9	232	0	.	0	1	3	232	0	1.07	0	154.11
9	233	0	0	0	0	2	232	0	1.07	0	113.17
9	234	0	.	1	0	3	234	0	1.07	1	113.17
9	235	1	.	1	0	.	235	0	0.89	0	154.11
9	236	1	.	1	0	.	236	0	0.71	0	154.11
9	237	0	1	0	0	2	236	0	1.07	1	126.82
9	238	1	1	1	0	1	236	0	1.07	2	126.82
9	239	0	1	1	0	2	236	0	1.07	0	126.82
9	240	0	.	1	0	.	240	0	0.89	2	126.82
9	241	1	.	1	0	.	241	0	0.71	1	167.75
9	242	1	.	1	0	.	242	0	0.71	1	167.75
9	243	1	.	1	0	.	243	0	0.89	0	195.05
9	244	0	1	0	0	1	243	0	1.07	0	126.82
9	245	0	.	0	0	3	245	0	1.07	1	58.59
9	246	0	0	0	0	1	245	0	1.07	2	58.59
9	247	0	0	0	0	1	245	0	1.43	1	195.05
9	248	0	0	0	0	1	245	0	1.43	0	249.63
9	249	0	0	0	0	1	245	0	1.43	1	181.40
9	250	0	.	0	0	2	250	0	1.25	0	126.82
9	251	0	.	0	0	.	251	0	1.25	0	140.46
9	252	0	0	0	0	2	251	0	1.25	0	140.46
9	253	1	.	0	0	.	253	0	0.89	0	113.17
9	254	0	1	0	0	1	253	0	1.07	1	126.82
9	255	0	.	1	0	2	255	0	1.07	0	126.82
9	256	0	.	0	1	1	256	0	1.25	2	181.40
9	257	0	.	0	0	1	257	0	1.25	1	181.40
9	258	1	.	1	0	1	258	0	1.43	1	113.17
9	259	1	.	1	0	1	259	0	1.43	2	140.46
9	260	0	1	1	0	1	259	0	1.43	1	140.46
9	261	1	.	0	0	.	261	0	1.07	1	181.40
9	262	1	0	0	0	1	261	0	1.25	2	181.40
9	263	1	.	1	0	2	263	0	1.43	0	99.53
9	264	0	.	1	0	1	264	0	1.25	2	263.27
9	265	0	0	1	0	1	264	0	1.43	1	263.27
9	266	1	1	1	0	2	264	0	1.43	2	195.05
9	267	0	1	0	0	1	264	0	1.60	1	195.05
9	268	1	1	1	0	1	264	0	1.60	2	195.05
9	269	0	.	0	0	.	269	0	1.25	0	140.46
9	270	0	0	0	0	1	269	0	1.25	0	140.46
9	271	0	.	0	0	2	271	0	1.25	1	208.69
9	272	1	1	1	0	2	271	0	1.07	0	208.69
9	273	1	.	1	0	1	273	0	1.25	1	126.82
9	274	0	1	0	0	1	273	0	1.43	0	126.82
9	275	0	.	1	0	3	275	0	1.25	1	208.69
9	276	1	.	0	0	.	276	0	0.89	0	181.40
9	277	1	.	1	0	.	277	0	0.89	1	154.11
9	278	1	.	0	0	.	278	0	0.89	2	154.11
9	279	1	.	0	1	.	279	0	0.71	1	222.34
9	280	1	0	0	1	1	279	0	0.89	1	222.34

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	231	113.75	0.87	1.16	0.83	1.20	0		0	.
9	232	85.96	0.87	1.15	0.87	1.15	1	0	0	1.20
9	233	114.05	0.87	1.14	0.87	1.15	0		1	.
9	234	112.51	0.88	1.13	0.88	1.13	1	0	0	1.15
9	235	89.46	0.87	1.15	0.87	1.15	1	0	0	1.13
9	236	93.06	0.86	1.16	0.86	1.16	1	0	0	1.15
9	237	124.73	0.87	1.15	0.86	1.16	0		1	.
9	238	126.90	0.86	1.16	0.86	1.16	0		0	.
9	239	130.23	0.87	1.15	0.86	1.16	0		0	.
9	240	131.67	0.86	1.16	0.86	1.16	1	0	0	1.16
9	241	74.44	0.87	1.15	0.87	1.15	1	0	0	1.16
9	242	73.80	0.85	1.17	0.85	1.17	1	0	0	1.15
9	243	50.55	0.86	1.16	0.86	1.16	1	0	0	1.17
9	244	139.41	0.87	1.15	0.86	1.16	0		1	.
9	245	327.79	0.86	1.16	0.86	1.16	1	0	0	1.16
9	246	325.76	0.86	1.16	0.86	1.16	0		1	.
9	247	52.52	0.87	1.15	0.86	1.16	0		0	.
9	248	34.23	0.88	1.14	0.86	1.16	0		0	.
9	249	91.79	0.89	1.13	0.86	1.16	0		0	.
9	250	145.51	0.88	1.13	0.88	1.13	1	0	0	1.16
9	251	117.59	0.89	1.12	0.89	1.12	1	1	0	1.13
9	252	119.02	0.90	1.11	0.89	1.12	0		1	.
9	253	184.92	0.89	1.12	0.89	1.12	1	0	0	1.12
9	254	154.82	0.90	1.12	0.89	1.12	0		1	.
9	255	152.99	0.90	1.11	0.90	1.11	1	0	0	1.12
9	256	109.21	0.91	1.09	0.91	1.09	1	2	0	1.11
9	257	108.14	0.89	1.13	0.89	1.13	1	3	0	1.11
9	258	210.88	0.90	1.11	0.90	1.11	1	1	0	1.11
9	259	138.28	0.89	1.12	0.89	1.12	1	0	0	1.11
9	260	136.64	0.90	1.12	0.89	1.12	0		1	.
9	261	111.11	0.89	1.13	0.89	1.13	1	2	0	1.12
9	262	112.17	0.89	1.13	0.89	1.13	0		1	.
9	263	297.86	0.83	1.21	0.83	1.21	1	3	0	1.12
9	264	59.99	0.88	1.13	0.88	1.13	1	1	0	1.12
9	265	58.82	0.88	1.14	0.88	1.13	0		1	.
9	266	94.40	0.89	1.13	0.88	1.13	0		0	.
9	267	96.83	0.90	1.11	0.88	1.13	0		0	.
9	268	98.27	0.89	1.13	0.88	1.13	0		0	.
9	269	151.22	0.89	1.12	0.89	1.12	1	0	0	1.13
9	270	153.12	0.90	1.11	0.89	1.12	0		1	.
9	271	103.94	0.90	1.11	0.90	1.11	1	0	0	1.12
9	272	105.94	0.91	1.10	0.90	1.11	0		1	.
9	273	274.88	0.91	1.10	0.91	1.10	1	0	0	1.11
9	274	276.68	0.91	1.10	0.91	1.10	0		1	.
9	275	108.58	0.93	1.08	0.93	1.08	1	0	0	1.10
9	276	136.27	0.91	1.10	0.91	1.10	1	0	0	1.08
9	277	172.71	0.89	1.12	0.89	1.12	1	0	0	1.10
9	278	184.76	0.87	1.15	0.87	1.15	1	0	0	1.12
9	279	113.85	0.81	1.24	0.81	1.24	1	0	0	1.15
9	280	115.72	0.81	1.23	0.81	1.24	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	281	0	1	1	0	2	279	0	0.89	1	167.75
9	282	0	.	0	0	3	282	0	1.07	2	222.34
9	283	1	.	0	0	2	283	0	1.07	2	263.27
9	284	1	0	0	0	1	283	0	1.25	0	263.27
9	285	1	0	1	0	1	283	0	1.07	0	263.27
9	286	0	1	0	0	1	283	0	1.60	1	222.34
9	287	0	0	0	0	1	283	0	1.43	0	222.34
9	288	0	.	0	0	.	288	0	1.43	0	222.34
9	289	1	1	0	0	2	288	0	1.43	1	208.69
9	290	1	.	1	0	2	290	0	1.25	1	222.34
9	291	1	0	0	0	1	290	0	1.25	1	222.34
9	292	0	.	1	0	.	292	0	0.89	2	263.27
9	293	1	.	1	0	.	293	0	0.89	0	181.40
9	294	0	1	1	1	1	293	0	1.25	1	222.34
9	295	0	0	0	0	1	293	0	1.25	2	222.34
9	296	1	.	1	0	1	296	0	1.25	0	249.63
9	297	1	0	1	0	1	296	0	1.43	0	249.63
9	298	0	1	1	0	2	296	0	1.43	0	222.34
9	299	1	.	1	0	2	299	0	1.43	2	222.34
9	300	1	.	1	0	2	300	0	1.25	0	222.34
9	301	0	1	0	0	1	300	0	1.25	1	263.27
9	302	0	0	1	0	1	300	0	1.25	2	263.27
9	303	0	0	1	0	1	300	0	1.43	1	249.63
9	304	0	0	0	0	2	300	0	1.43	1	249.63
9	305	0	.	1	0	3	305	0	1.25	0	263.27
9	306	0	0	0	0	2	305	0	1.07	0	263.27
9	307	0	0	1	0	2	305	0	1.07	0	263.27
9	308	1	.	1	0	2	308	0	1.25	1	195.05
9	309	1	0	1	0	1	308	0	1.25	1	222.34
9	310	0	1	1	0	1	308	0	1.43	1	263.27
9	311	0	0	1	0	1	308	0	1.60	2	263.27
9	312	0	0	0	0	1	308	0	1.43	1	154.11
9	313	1	.	0	0	.	313	0	1.25	2	154.11
9	314	1	.	1	0	1	314	0	1.07	0	154.11
9	315	0	1	1	0	1	314	0	1.25	1	222.34
9	316	0	.	1	0	2	316	0	1.25	1	263.27
9	317	0	0	0	1	1	316	0	1.07	0	263.27
9	318	0	0	0	1	2	316	0	1.25	2	263.27
9	319	1	1	0	0	1	316	0	1.25	1	235.98
9	320	1	0	1	1	1	316	0	1.25	2	235.98
9	321	1	.	0	0	2	321	0	1.25	1	263.27
9	322	0	1	0	0	2	321	0	1.25	0	154.11
9	323	1	1	1	0	1	321	0	1.25	0	195.05
9	324	1	0	0	1	1	321	0	1.07	1	195.05
9	325	1	0	1	0	2	321	0	1.07	1	235.98
9	326	1	0	1	0	2	321	0	1.25	1	235.98
9	327	1	0	1	0	1	321	0	1.25	1	235.98
9	328	1	0	1	1	1	321	0	1.43	2	235.98
9	329	0	1	1	0	1	321	0	1.43	1	154.11
9	330	1	1	1	0	1	321	0	1.60	0	167.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	281	150.78	0.82	1.21	0.81	1.24	0		0	.
9	282	120.02	0.83	1.20	0.83	1.20	1	0	0	1.24
9	283	67.26	0.83	1.20	0.83	1.20	1	0	0	1.20
9	284	72.70	0.84	1.19	0.83	1.20	0		1	.
9	285	71.50	0.82	1.22	0.83	1.20	0		0	.
9	286	130.47	0.84	1.20	0.83	1.20	0		0	.
9	287	131.84	0.83	1.20	0.83	1.20	0		0	.
9	288	122.93	0.83	1.21	0.83	1.21	1	0	0	1.20
9	289	135.04	0.84	1.20	0.83	1.21	0		1	.
9	290	136.01	0.84	1.19	0.84	1.19	1	0	0	1.21
9	291	137.54	0.85	1.18	0.84	1.19	0		1	.
9	292	77.37	0.85	1.18	0.85	1.18	1	0	0	1.19
9	293	171.43	0.84	1.18	0.84	1.18	1	0	0	1.18
9	294	142.08	0.85	1.18	0.84	1.18	0		1	.
9	295	142.85	0.84	1.19	0.84	1.18	0		0	.
9	296	81.28	0.84	1.19	0.84	1.19	1	0	0	1.18
9	297	83.68	0.84	1.19	0.84	1.19	0		1	.
9	298	147.75	0.84	1.19	0.84	1.19	0		0	.
9	299	149.09	0.84	1.19	0.84	1.19	1	0	0	1.19
9	300	150.95	0.85	1.18	0.85	1.18	1	0	0	1.19
9	301	81.91	0.85	1.18	0.85	1.18	0		1	.
9	302	84.15	0.84	1.18	0.85	1.18	0		0	.
9	303	84.52	0.85	1.18	0.85	1.18	0		0	.
9	304	86.38	0.86	1.16	0.85	1.18	0		0	.
9	305	86.28	0.86	1.16	0.86	1.16	1	0	0	1.18
9	306	87.69	0.87	1.15	0.86	1.16	0		1	.
9	307	105.77	0.87	1.15	0.86	1.16	0		0	.
9	308	163.23	0.87	1.14	0.87	1.14	1	0	0	1.16
9	309	162.93	0.88	1.14	0.87	1.14	0		1	.
9	310	107.77	0.88	1.13	0.87	1.14	0		0	.
9	311	108.84	0.88	1.14	0.87	1.14	0		0	.
9	312	309.25	0.89	1.12	0.87	1.14	0		0	.
9	313	310.08	0.86	1.16	0.86	1.16	1	0	0	1.14
9	314	312.28	0.85	1.17	0.85	1.17	1	0	0	1.16
9	315	167.97	0.86	1.16	0.85	1.17	0		1	.
9	316	111.78	0.87	1.15	0.87	1.15	1	0	0	1.17
9	317	113.08	0.87	1.15	0.87	1.15	0		1	.
9	318	115.15	0.86	1.16	0.87	1.15	0		0	.
9	319	174.95	0.87	1.16	0.87	1.15	0		0	.
9	320	175.88	0.85	1.17	0.87	1.15	0		0	.
9	321	117.48	0.85	1.17	0.85	1.17	1	0	0	1.15
9	322	324.69	0.86	1.16	0.85	1.17	0		1	.
9	323	181.35	0.87	1.16	0.85	1.17	0		0	.
9	324	183.09	0.87	1.15	0.85	1.17	0		0	.
9	325	180.22	0.89	1.12	0.85	1.17	0		0	.
9	326	181.85	0.88	1.14	0.85	1.17	0		0	.
9	327	183.72	0.88	1.14	0.85	1.17	0		0	.
9	328	185.32	0.85	1.18	0.85	1.17	0		0	.
9	329	336.04	0.86	1.16	0.85	1.17	0		0	.
9	330	243.44	0.87	1.15	0.85	1.17	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	331	0	1	1	0	2	321	0	1.60	1	263.27
9	332	1	.	0	1	1	332	0	1.60	2	263.27
9	333	1	0	1	0	2	332	0	1.25	0	181.40
9	334	1	.	0	0	.	334	0	1.07	2	263.27
9	335	0	1	0	0	2	334	0	1.25	1	263.27
9	336	1	1	1	0	1	334	0	1.07	2	263.27
9	337	1	.	1	0	.	337	0	1.25	2	249.63
9	338	0	1	0	0	1	337	0	1.07	1	249.63
9	339	1	.	1	1	1	339	0	1.43	1	222.34
9	340	1	.	1	0	3	340	0	1.25	2	263.27
9	341	1	0	1	0	1	340	0	1.25	1	222.34
9	342	1	0	0	0	1	340	0	1.07	0	222.34
9	343	1	.	1	0	.	343	0	0.89	0	181.40
9	344	1	0	1	0	2	343	0	1.07	1	263.27
9	345	0	1	0	1	1	343	0	1.43	2	263.27
9	346	1	1	1	0	1	343	0	1.43	0	263.27
9	347	0	.	0	0	2	347	0	1.25	2	263.27
9	348	0	.	1	0	.	348	0	0.53	2	222.34
9	349	1	.	1	0	.	349	0	0.53	2	263.27
9	350	1	0	1	0	.	349	0	0.53	0	263.27
9	351	1	.	0	0	.	351	0	0.36	1	58.59
9	352	0	.	1	0	1	352	0	0.71	1	58.59
9	353	1	.	0	0	.	353	0	0.36	0	140.46
9	51.01	1	.	1	0	.	51	0	0.89	1	4.01
9	52.01	1	0	1	1	2	51	0	1.43	0	4.01
9	53.01	1	0	1	0	1	51	0	1.60	1	4.01
9	59.01	0	.	0	0	1	59	0	2.14	0	4.01
9	60.01	0	0	0	0	1	59	0	1.78	1	4.01
9	65.01	1	.	0	0	.	65	0	1.96	1	31.30
9	66.01	1	0	0	0	1	65	0	2.14	1	31.30
9	67.01	1	0	1	0	1	65	0	1.78	1	4.01
9	70.01	0	.	0	0	.	70	0	1.60	1	31.30
9	71.01	0	.	0	0	.	71	0	1.25	0	85.88
9	72.01	1	1	1	0	1	71	0	1.43	1	85.88
9	73.01	1	1	1	0	1	75	0	1.96	1	4.01
9	75.01	0	.	0	0	1	75	0	1.60	1	85.88
9	77.01	0	1	1	0	1	75	0	1.96	0	31.30
9	78.01	0	0	1	0	1	75	0	1.96	1	4.01
9	80.01	1	1	1	0	1	75	0	2.14	1	4.01
9	81.01	0	1	0	0	1	75	0	1.78	1	85.88
9	82.01	0	0	0	0	1	75	0	2.14	1	85.88
9	84.01	0	.	0	0	1	84	0	1.96	1	4.01
9	85.01	0	.	0	0	1	85	0	1.60	0	4.01
9	86.01	1	.	1	0	.	86	0	1.60	1	72.24
9	87.01	0	1	0	0	1	86	0	1.78	1	72.24
9	93.01	1	.	1	0	.	93	0	1.96	1	4.01
9	94.01	1	.	1	0	.	94	0	1.60	1	85.88
9	95.01	1	0	0	0	1	94	0	1.96	1	85.88
9	96.01	0	.	0	0	1	96	0	2.14	2	31.30
9	97.01	1	1	1	1	1	96	0	2.14	1	4.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	331	131.16	0.87	1.14	0.85	1.17	0		0	.
9	332	130.06	0.87	1.15	0.87	1.15	1	0	0	1.17
9	333	237.50	0.86	1.16	0.87	1.15	0		1	.
9	334	133.50	0.86	1.16	0.86	1.16	1	0	0	1.15
9	335	135.37	0.86	1.16	0.86	1.16	0		1	.
9	336	137.03	0.87	1.15	0.86	1.16	0		0	.
9	337	144.04	0.87	1.15	0.87	1.15	1	0	0	1.16
9	338	145.64	0.86	1.17	0.87	1.15	0		1	.
9	339	216.59	0.87	1.15	0.87	1.15	1	0	0	1.15
9	340	182.55	0.87	1.15	0.87	1.15	1	0	0	1.15
9	341	258.86	0.88	1.13	0.87	1.15	0		1	.
9	342	259.83	0.87	1.15	0.87	1.15	0		0	.
9	343	302.83	0.83	1.20	0.83	1.20	1	0	0	1.15
9	344	223.39	0.84	1.19	0.83	1.20	0		1	.
9	345	224.82	0.84	1.19	0.83	1.20	0		0	.
9	346	226.92	0.85	1.18	0.83	1.20	0		0	.
9	347	329.99	0.85	1.18	0.85	1.18	1	1	0	1.20
9	348	414.95	0.91	1.10	0.91	1.10	1	1	0	1.18
9	349	432.73	1.05	0.95	1.05	0.95	1	2	0	1.10
9	350	431.40	1.02	0.98	1.05	0.95	0		1	.
9	351	183.21	0.58	1.73	0.58	1.73	1	3	0	1.10
9	352	186.32	0.59	1.70	0.59	1.70	1	1	0	1.10
9	353	631.87	0.92	1.09	0.92	1.09	1	0	0	1.70
9	51.01	66.04	0.93	1.08	0.93	1.08	1	0	0	.
9	52.01	67.57	0.94	1.06	0.93	1.08	0		1	.
9	53.01	69.97	0.94	1.07	0.93	1.08	0		0	.
9	59.01	71.41	0.83	1.21	0.83	1.21	1	1	0	1.08
9	60.01	68.67	0.84	1.20	0.83	1.21	0		1	.
9	65.01	48.01	0.80	1.26	0.80	1.26	1	1	0	1.21
9	66.01	49.81	0.79	1.26	0.80	1.26	0		1	.
9	67.01	77.41	0.80	1.25	0.80	1.26	0		0	.
9	70.01	46.74	0.76	1.32	0.76	1.32	1	1	0	1.26
9	71.01	16.28	0.84	1.18	0.84	1.18	1	1	0	1.32
9	72.01	14.68	0.84	1.19	0.84	1.18	0		1	.
9	73.01	87.26	0.81	1.24	0.82	1.22	0		1	.
9	75.01	20.36	0.82	1.22	0.82	1.22	1	1	0	1.18
9	77.01	67.56	0.79	1.27	0.82	1.22	0		0	.
9	78.01	89.83	0.78	1.28	0.82	1.22	0		0	.
9	80.01	91.23	0.78	1.28	0.82	1.22	0		0	.
9	81.01	22.19	0.77	1.31	0.82	1.22	0		0	.
9	82.01	23.49	0.77	1.30	0.82	1.22	0		0	.
9	84.01	94.03	0.73	1.37	0.73	1.37	1	1	0	1.22
9	85.01	97.40	0.73	1.37	0.73	1.37	1	1	0	1.37
9	86.01	52.52	0.71	1.40	0.71	1.40	1	1	0	1.37
9	87.01	53.75	0.70	1.42	0.71	1.40	0		1	.
9	93.01	104.14	0.58	1.72	0.58	1.72	1	1	0	1.40
9	94.01	31.80	0.58	1.73	0.58	1.73	1	1	0	1.72
9	95.01	32.87	0.56	1.78	0.58	1.73	0		1	.
9	96.01	81.14	0.57	1.75	0.57	1.75	1	1	0	1.73
9	97.01	105.31	0.56	1.78	0.57	1.75	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	98.01	1	.	1	0	1	98	0	2.14	1	4.01
9	99.01	1	0	0	0	1	98	0	2.49	0	4.01
9	100.01	0	1	0	0	1	98	0	2.32	1	85.88
9	101.01	1	1	1	1	1	98	0	2.14	1	85.88
9	102.01	0	1	0	0	1	98	0	1.96	1	85.88
9	103.01	0	0	0	0	1	98	0	2.14	1	31.30
9	104.01	0	0	1	0	1	98	0	1.96	1	58.59
9	105.01	0	.	0	0	2	105	0	1.60	0	31.30
9	106.01	1	1	1	0	1	105	0	1.60	0	31.30
9	109.01	1	.	1	0	2	109	0	1.96	1	4.01
9	110.01	1	1	1	0	1	111	0	2.14	1	85.88
9	111.01	0	.	0	0	1	111	0	1.96	1	85.88
9	112.01	1	0	0	0	1	111	0	2.32	1	4.01
9	113.01	0	1	0	0	1	111	0	2.14	2	58.59
9	114.01	1	1	1	0	1	111	0	2.14	1	44.94
9	115.01	1	0	1	0	1	111	0	2.32	1	85.88
9	116.01	0	1	0	0	1	111	0	2.49	1	31.30
9	117.01	1	1	1	0	1	111	0	2.49	0	44.94
9	118.01	1	0	1	0	1	111	0	2.49	1	44.94
9	119.01	0	1	1	0	1	111	0	2.49	1	31.30
9	120.01	1	1	1	1	1	111	0	2.67	1	58.59
9	121.01	1	0	1	0	2	111	0	2.14	1	44.94
9	122.01	1	0	1	0	2	111	0	1.78	0	31.30
9	123.01	0	1	0	0	1	111	0	1.78	1	58.59
9	124.01	1	.	0	0	2	124	0	1.60	0	44.94
9	125.01	0	1	0	0	2	124	0	1.60	1	44.94
9	126.01	1	.	1	0	.	126	0	1.60	1	85.88
9	127.01	1	.	1	0	2	127	0	1.60	1	44.94
9	130.01	0	1	1	0	1	131	0	1.78	2	31.30
9	131.01	1	.	1	0	.	131	0	1.43	1	31.30
9	133.01	1	1	1	0	1	131	0	1.78	1	58.59
9	134.01	0	1	0	0	2	131	0	1.96	1	44.94
9	135.01	1	1	0	0	1	131	0	1.78	2	85.88
9	136.01	1	0	1	0	1	131	0	1.78	1	58.59
9	137.01	0	1	0	0	1	131	0	2.32	2	44.94
9	138.01	0	0	0	0	1	131	0	2.14	1	4.01
9	140.01	0	.	0	0	1	140	0	2.32	1	44.94
9	141.01	0	0	0	0	1	140	0	2.67	1	4.01
9	142.01	1	1	1	0	1	140	0	2.32	1	85.88
9	143.01	0	1	0	0	1	140	0	2.49	2	31.30
9	144.01	1	0	1	0	1	140	0	2.49	1	31.30
9	145.01	0	0	0	0	1	140	0	2.32	0	44.94
9	146.01	0	0	1	0	1	140	0	2.14	0	58.59
9	147.01	0	.	0	0	2	147	0	1.96	1	85.88
9	148.01	0	0	0	0	1	147	0	1.96	1	85.88
9	149.01	0	0	1	0	1	147	0	1.78	2	44.94
9	150.01	0	0	0	0	1	147	0	1.96	1	44.94
9	151.01	0	0	0	0	1	147	0	2.14	2	44.94
9	152.01	1	1	1	0	1	147	0	2.49	1	85.88
9	153.01	1	0	1	0	1	147	0	2.49	1	85.88

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	98.01	108.21	0.56	1.80	0.56	1.80	1	1	0	1.75
9	99.01	111.15	0.56	1.77	0.56	1.80	0		1	.
9	100.01	34.04	0.56	1.79	0.56	1.80	0		0	.
9	101.01	35.24	0.56	1.79	0.56	1.80	0		0	.
9	102.01	36.57	0.56	1.78	0.56	1.80	0		0	.
9	103.01	84.55	0.56	1.79	0.56	1.80	0		0	.
9	104.01	62.99	0.56	1.80	0.56	1.80	0		0	.
9	105.01	89.22	0.56	1.80	0.56	1.80	1	0	0	1.80
9	106.01	91.75	0.56	1.79	0.56	1.80	0		1	.
9	109.01	121.76	0.52	1.92	0.52	1.92	1	1	0	1.80
9	110.01	39.31	0.53	1.87	0.53	1.87	0		1	.
9	111.01	37.44	0.52	1.93	0.53	1.87	1	0	0	1.92
9	112.01	127.50	0.55	1.83	0.53	1.87	0		0	.
9	113.01	66.46	0.55	1.81	0.53	1.87	0		0	.
9	114.01	91.62	0.55	1.82	0.53	1.87	0		0	.
9	115.01	40.41	0.55	1.81	0.53	1.87	0		0	.
9	116.01	94.76	0.55	1.81	0.53	1.87	0		0	.
9	117.01	96.69	0.54	1.85	0.53	1.87	0		0	.
9	118.01	98.93	0.54	1.86	0.53	1.87	0		0	.
9	119.01	100.30	0.54	1.86	0.53	1.87	0		0	.
9	120.01	68.17	0.54	1.86	0.53	1.87	0		0	.
9	121.01	102.63	0.54	1.86	0.53	1.87	0		0	.
9	122.01	105.27	0.54	1.87	0.53	1.87	0		0	.
9	123.01	69.77	0.54	1.86	0.53	1.87	0		0	.
9	124.01	107.10	0.54	1.84	0.54	1.84	1	1	0	1.93
9	125.01	108.81	0.54	1.84	0.54	1.84	0		1	.
9	126.01	41.74	0.54	1.86	0.54	1.86	1	0	0	1.84
9	127.01	112.98	0.56	1.78	0.56	1.78	1	1	0	1.86
9	130.01	118.55	0.53	1.88	0.54	1.86	0		1	.
9	131.01	114.24	0.54	1.86	0.54	1.86	1	1	0	1.78
9	133.01	72.60	0.60	1.67	0.54	1.86	0		0	.
9	134.01	116.61	0.59	1.69	0.54	1.86	0		0	.
9	135.01	43.65	0.60	1.66	0.54	1.86	0		0	.
9	136.01	74.71	0.61	1.65	0.54	1.86	0		0	.
9	137.01	121.55	0.61	1.65	0.54	1.86	0		0	.
9	138.01	165.30	0.61	1.65	0.54	1.86	0		0	.
9	140.01	123.49	0.56	1.77	0.56	1.77	1	0	0	1.86
9	141.01	177.21	0.56	1.79	0.56	1.77	0		1	.
9	142.01	45.78	0.56	1.79	0.56	1.77	0		0	.
9	143.01	133.20	0.57	1.75	0.56	1.77	0		0	.
9	144.01	130.83	0.57	1.75	0.56	1.77	0		0	.
9	145.01	128.36	0.57	1.76	0.56	1.77	0		0	.
9	146.01	77.01	0.59	1.70	0.56	1.77	0		0	.
9	147.01	46.38	0.60	1.67	0.60	1.67	1	1	0	1.77
9	148.01	49.48	0.61	1.63	0.60	1.67	0		1	.
9	149.01	135.67	0.62	1.62	0.60	1.67	0		0	.
9	150.01	136.80	0.61	1.63	0.60	1.67	0		0	.
9	151.01	139.20	0.62	1.61	0.60	1.67	0		0	.
9	152.01	53.52	0.62	1.62	0.60	1.67	0		0	.
9	153.01	57.69	0.61	1.65	0.60	1.67	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	154.01	1	0	0	0	1	147	0	2.67	2	44.94
9	155.01	0	1	0	0	1	147	0	2.49	1	44.94
9	156.01	1	1	1	0	1	147	0	2.49	1	58.59
9	157.01	1	0	1	1	1	147	0	2.49	1	58.59
9	158.01	0	1	1	0	1	147	0	2.14	0	4.01
9	159.01	0	0	1	0	1	147	0	2.14	1	44.94
9	160.01	1	1	1	1	1	147	0	2.14	1	44.94
9	161.01	1	0	1	0	2	147	0	2.14	1	44.94
9	162.01	0	.	0	1	3	162	0	1.96	1	85.88
9	163.01	0	.	0	0	.	163	0	1.78	1	58.59
9	164.01	0	0	0	0	1	163	0	1.78	1	58.59
9	165.01	0	0	0	0	1	163	0	1.78	1	44.94
9	166.01	0	0	1	0	1	163	0	1.78	1	44.94
9	167.01	0	0	0	0	1	163	0	2.14	2	44.94
9	168.01	0	0	0	1	1	163	0	2.14	0	85.88
9	169.01	0	0	0	0	1	163	0	1.96	1	85.88
9	170.01	0	0	1	0	1	163	0	2.14	1	44.94
9	171.01	0	0	1	0	1	163	0	1.96	2	44.94
9	172.01	0	0	0	0	1	163	0	2.14	1	44.94
9	173.01	1	1	1	0	2	163	0	1.96	1	58.59
9	174.01	0	1	1	0	1	163	0	2.32	0	44.94
9	175.01	1	.	1	0	3	175	0	1.96	1	44.94
9	176.01	1	.	1	1	1	176	0	1.78	1	44.94
9	177.01	1	0	1	0	1	176	0	1.78	1	44.94
9	178.01	1	0	0	0	1	176	0	1.96	2	44.94
9	179.01	0	1	0	0	2	176	0	1.78	1	58.59
9	180.01	0	.	1	0	.	180	0	1.78	1	85.88
9	181.01	0	0	0	0	1	180	0	1.96	2	85.88
9	182.01	0	0	0	0	1	180	0	2.14	1	31.30
9	183.01	0	0	1	0	1	180	0	2.14	2	31.30
9	184.01	0	0	0	0	2	180	0	2.14	1	58.59
9	185.01	0	0	0	0	2	180	0	2.14	1	72.24
9	186.01	0	.	1	0	1	186	0	1.96	1	4.01
9	187.01	0	.	0	0	2	187	0	1.78	0	58.59
9	188.01	0	.	0	0	1	188	0	2.14	2	85.88
9	189.01	0	0	1	0	1	188	0	1.96	1	85.88
9	190.01	0	0	0	1	1	188	0	2.14	1	99.53
9	191.01	0	0	1	0	1	188	0	2.32	2	99.53
9	192.01	1	1	0	0	1	188	0	2.14	2	99.53
9	193.01	0	1	1	0	1	188	0	1.96	2	58.59
9	194.01	0	0	0	0	1	188	0	1.78	1	44.94
9	195.01	0	0	1	0	1	188	0	1.78	2	44.94
9	196.01	1	1	1	0	1	188	0	1.96	1	44.94
9	197.01	0	.	0	0	2	197	0	1.96	0	31.30
9	198.01	0	.	1	0	1	198	0	1.96	0	58.59
9	199.01	0	0	1	0	2	198	0	1.96	1	44.94
9	200.01	1	.	1	0	2	200	0	1.96	1	44.94
9	201.01	0	1	0	1	2	200	0	1.60	1	85.88
9	202.01	0	0	1	0	1	200	0	1.78	1	44.94
9	203.01	1	1	1	0	1	200	0	2.14	2	44.94

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	154.01	143.11	0.61	1.65	0.60	1.67	0		0	.
9	155.01	144.97	0.61	1.65	0.60	1.67	0		0	.
9	156.01	83.65	0.60	1.66	0.60	1.67	0		0	.
9	157.01	87.48	0.60	1.67	0.60	1.67	0		0	.
9	158.01	208.18	0.60	1.67	0.60	1.67	0		0	.
9	159.01	150.71	0.60	1.68	0.60	1.67	0		0	.
9	160.01	152.65	0.59	1.68	0.60	1.67	0		0	.
9	161.01	154.52	0.59	1.70	0.60	1.67	0		0	.
9	162.01	59.03	0.59	1.69	0.59	1.69	1	0	0	1.67
9	163.01	89.89	0.59	1.71	0.59	1.71	1	1	0	1.69
9	164.01	91.79	0.58	1.73	0.59	1.71	0		1	.
9	165.01	160.46	0.58	1.73	0.59	1.71	0		0	.
9	166.01	161.89	0.57	1.75	0.59	1.71	0		0	.
9	167.01	164.09	0.58	1.73	0.59	1.71	0		0	.
9	168.01	60.33	0.58	1.73	0.59	1.71	0		0	.
9	169.01	64.90	0.58	1.73	0.59	1.71	0		0	.
9	170.01	170.30	0.59	1.70	0.59	1.71	0		0	.
9	171.01	173.67	0.57	1.75	0.59	1.71	0		0	.
9	172.01	171.77	0.60	1.67	0.59	1.71	0		0	.
9	173.01	96.89	0.60	1.66	0.59	1.71	0		0	.
9	174.01	177.04	0.60	1.66	0.59	1.71	0		0	.
9	175.01	179.01	0.61	1.65	0.61	1.65	1	0	0	1.71
9	176.01	181.18	0.61	1.64	0.61	1.64	1	0	0	1.65
9	177.01	173.38	0.61	1.64	0.61	1.64	0		1	.
9	178.01	184.95	0.60	1.67	0.61	1.64	0		0	.
9	179.01	100.86	0.59	1.70	0.61	1.64	0		0	.
9	180.01	66.84	0.59	1.71	0.59	1.71	1	0	0	1.64
9	181.01	68.17	0.58	1.71	0.59	1.71	0		1	.
9	182.01	199.16	0.59	1.70	0.59	1.71	0		0	.
9	183.01	211.17	0.59	1.70	0.59	1.71	0		0	.
9	184.01	105.17	0.59	1.70	0.59	1.71	0		0	.
9	185.01	97.63	0.59	1.69	0.59	1.71	0		0	.
9	186.01	258.06	0.60	1.66	0.60	1.66	1	2	0	1.71
9	187.01	112.44	0.56	1.78	0.56	1.78	1	3	0	1.71
9	188.01	71.21	0.60	1.68	0.60	1.68	1	1	0	1.71
9	189.01	69.64	0.59	1.70	0.60	1.68	0		1	.
9	190.01	74.34	0.60	1.68	0.60	1.68	0		0	.
9	191.01	75.78	0.60	1.66	0.60	1.68	0		0	.
9	192.01	77.78	0.61	1.63	0.60	1.68	0		0	.
9	193.01	120.35	0.62	1.62	0.60	1.68	0		0	.
9	194.01	227.59	0.60	1.65	0.60	1.68	0		0	.
9	195.01	227.69	0.61	1.63	0.60	1.68	0		0	.
9	196.01	229.59	0.61	1.64	0.60	1.68	0		0	.
9	197.01	231.63	0.63	1.59	0.63	1.59	1	1	0	1.68
9	198.01	122.25	0.64	1.57	0.64	1.57	1	0	0	1.59
9	199.01	233.30	0.64	1.56	0.64	1.57	0		1	.
9	200.01	235.30	0.65	1.55	0.65	1.55	1	0	0	1.57
9	201.01	738.91	0.66	1.52	0.65	1.55	0		1	.
9	202.01	239.00	0.66	1.52	0.65	1.55	0		0	.
9	203.01	240.94	0.66	1.51	0.65	1.55	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	204.01	0	1	0	0	1	200	0	2.14	1	44.94
9	205.01	0	0	1	0	1	200	0	2.14	1	58.59
9	206.01	0	0	0	0	2	200	0	1.96	1	44.94
9	207.01	0	.	0	0	1	207	0	2.14	1	44.94
9	208.01	0	.	0	0	.	208	0	1.78	1	44.94
9	209.01	0	0	1	0	2	208	0	1.78	1	58.59
9	210.01	0	0	0	0	1	208	0	1.96	0	44.94
9	211.01	0	0	0	0	1	208	0	1.96	1	85.88
9	212.01	1	1	1	0	2	208	0	1.96	1	44.94
9	213.01	0	1	1	0	2	208	0	1.96	1	58.59
9	214.01	1	1	1	0	1	208	0	1.96	1	58.59
9	215.01	0	1	1	0	1	208	0	1.96	1	85.88
9	216.01	0	.	1	0	2	216	0	1.78	1	85.88
9	217.01	0	0	0	0	1	216	0	1.96	0	85.88
9	218.01	0	0	0	0	1	216	0	1.96	1	58.59
9	219.01	1	1	1	0	2	216	0	1.78	1	58.59
9	220.01	1	0	1	0	1	216	0	1.96	1	58.59
9	221.01	1	0	0	0	1	216	0	2.14	1	85.88
9	222.01	0	.	0	0	2	222	0	1.96	1	85.88
9	223.01	0	0	1	0	1	222	0	1.96	1	85.88
9	224.01	1	.	1	0	.	224	0	1.96	1	99.53
9	225.01	1	0	1	0	1	224	0	1.96	2	99.53
9	226.01	1	0	1	0	1	224	0	2.14	1	140.46
9	227.01	0	1	0	0	1	224	0	2.14	0	140.46
9	228.01	1	1	1	0	1	224	0	2.14	1	140.46
9	229.01	0	1	0	0	1	224	0	2.14	1	154.11
9	230.01	1	1	1	0	1	224	0	1.96	1	126.82
9	231.01	0	1	0	0	1	224	0	1.60	1	99.53
9	232.01	0	.	0	1	2	232	0	1.60	1	126.82
9	233.01	0	0	0	0	2	232	0	1.60	1	85.88
9	234.01	0	.	1	0	2	234	0	1.60	1	85.88
9	235.01	1	.	1	0	2	235	0	1.60	0	126.82
9	236.01	1	.	1	0	3	236	0	1.43	0	126.82
9	237.01	0	1	0	0	2	236	0	1.43	1	99.53
9	238.01	1	1	1	0	1	236	0	1.60	2	99.53
9	239.01	0	1	1	0	1	236	0	1.60	0	99.53
9	240.01	0	.	1	0	.	240	0	1.43	2	99.53
9	241.01	1	.	1	0	.	241	0	1.25	1	140.46
9	242.01	1	.	1	0	2	242	0	1.25	1	140.46
9	243.01	1	0	1	0	1	242	0	1.25	1	167.75
9	244.01	0	1	0	0	1	242	0	1.60	1	99.53
9	245.01	0	.	0	0	3	245	0	1.43	1	31.30
9	246.01	0	0	0	0	1	245	0	1.60	2	31.30
9	247.01	0	0	0	0	1	245	0	1.78	1	167.75
9	248.01	0	0	0	0	1	245	0	1.78	1	222.34
9	249.01	0	0	0	0	1	245	0	1.78	1	154.11
9	250.01	0	0	0	0	2	245	0	1.78	1	99.53
9	251.01	0	.	0	0	.	251	0	1.60	0	113.17
9	252.01	0	0	0	0	1	251	0	1.60	1	113.17
9	253.01	1	.	0	0	2	253	0	1.43	1	85.88

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	204.01	242.71	0.66	1.51	0.65	1.55	0		0	.
9	205.01	139.80	0.66	1.51	0.65	1.55	0		0	.
9	206.01	246.41	0.66	1.52	0.65	1.55	0		0	.
9	207.01	247.98	0.70	1.42	0.70	1.42	1	1	0	1.55
9	208.01	249.78	0.70	1.42	0.70	1.42	1	0	0	1.42
9	209.01	146.34	0.71	1.40	0.70	1.42	0		1	.
9	210.01	252.85	0.71	1.41	0.70	1.42	0		0	.
9	211.01	81.48	0.72	1.39	0.70	1.42	0		0	.
9	212.01	256.59	0.72	1.39	0.70	1.42	0		0	.
9	213.01	156.72	0.73	1.38	0.70	1.42	0		0	.
9	214.01	184.35	0.73	1.36	0.70	1.42	0		0	.
9	215.01	83.32	0.74	1.36	0.70	1.42	0		0	.
9	216.01	85.02	0.72	1.39	0.72	1.39	1	0	0	1.42
9	217.01	86.69	0.74	1.35	0.72	1.39	0		1	.
9	218.01	165.39	0.75	1.34	0.72	1.39	0		0	.
9	219.01	187.25	0.74	1.34	0.72	1.39	0		0	.
9	220.01	190.42	0.75	1.34	0.72	1.39	0		0	.
9	221.01	90.49	0.75	1.33	0.72	1.39	0		0	.
9	222.01	94.80	0.75	1.33	0.75	1.33	1	0	0	1.39
9	223.01	97.23	0.75	1.33	0.75	1.33	0		1	.
9	224.01	102.57	0.75	1.34	0.75	1.34	1	0	0	1.33
9	225.01	104.37	0.74	1.34	0.75	1.34	0		1	.
9	226.01	52.68	0.75	1.33	0.75	1.34	0		0	.
9	227.01	54.15	0.76	1.32	0.75	1.34	0		0	.
9	228.01	55.55	0.76	1.32	0.75	1.34	0		0	.
9	229.01	51.38	0.76	1.32	0.75	1.34	0		0	.
9	230.01	84.09	0.76	1.31	0.75	1.34	0		0	.
9	231.01	113.75	0.77	1.30	0.75	1.34	0		0	.
9	232.01	85.96	0.77	1.30	0.77	1.30	1	0	0	1.34
9	233.01	114.05	0.78	1.29	0.77	1.30	0		1	.
9	234.01	112.51	0.77	1.30	0.77	1.30	1	0	0	1.30
9	235.01	89.46	0.76	1.32	0.76	1.32	1	0	0	1.30
9	236.01	93.06	0.76	1.32	0.76	1.32	1	0	0	1.32
9	237.01	124.73	0.76	1.32	0.76	1.32	0		1	.
9	238.01	126.90	0.78	1.29	0.76	1.32	0		0	.
9	239.01	130.23	0.77	1.29	0.76	1.32	0		0	.
9	240.01	131.67	0.80	1.25	0.80	1.25	1	0	0	1.32
9	241.01	74.44	0.78	1.29	0.78	1.29	1	0	0	1.25
9	242.01	73.80	0.76	1.31	0.76	1.31	1	0	0	1.29
9	243.01	50.55	0.76	1.31	0.76	1.31	0		1	.
9	244.01	139.41	0.77	1.30	0.76	1.31	0		0	.
9	245.01	327.79	0.76	1.31	0.76	1.31	1	0	0	1.31
9	246.01	325.76	0.76	1.32	0.76	1.31	0		1	.
9	247.01	52.52	0.75	1.33	0.76	1.31	0		0	.
9	248.01	34.23	0.75	1.33	0.76	1.31	0		0	.
9	249.01	91.79	0.76	1.31	0.76	1.31	0		0	.
9	250.01	145.51	0.77	1.30	0.76	1.31	0		0	.
9	251.01	117.59	0.78	1.29	0.78	1.29	1	0	0	1.31
9	252.01	119.02	0.78	1.29	0.78	1.29	0		1	.
9	253.01	184.92	0.77	1.30	0.77	1.30	1	0	0	1.29

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	254.01	0	1	0	0	1	253	0	1.60	1	99.53
9	255.01	0	.	1	0	2	255	0	1.60	2	99.53
9	256.01	0	0	0	1	1	255	0	1.96	2	154.11
9	257.01	0	0	0	0	1	255	0	1.78	1	154.11
9	258.01	1	1	1	0	1	255	0	2.14	1	85.88
9	259.01	1	0	1	0	1	255	0	2.14	2	113.17
9	260.01	0	1	1	0	1	255	0	2.32	1	113.17
9	261.01	1	0	0	0	2	255	0	1.78	1	154.11
9	262.01	1	0	0	0	1	255	0	1.78	0	154.11
9	263.01	1	1	1	0	2	255	0	2.14	1	72.24
9	264.01	0	1	1	0	2	255	0	1.78	2	235.98
9	265.01	0	0	1	0	1	255	0	1.96	1	235.98
9	266.01	1	1	1	0	1	255	0	1.78	2	167.75
9	267.01	0	1	0	0	1	255	0	2.14	1	167.75
9	268.01	1	1	1	0	1	255	0	2.14	0	167.75
9	269.01	0	1	0	0	2	255	0	1.96	1	113.17
9	270.01	0	0	0	0	1	255	0	1.78	0	113.17
9	271.01	0	0	0	0	2	255	0	1.60	1	181.40
9	272.01	1	1	1	0	1	255	0	1.43	0	181.40
9	273.01	1	0	1	0	1	255	0	1.78	1	99.53
9	274.01	0	1	0	0	1	255	0	1.78	0	99.53
9	275.01	0	.	1	0	2	275	0	1.78	1	181.40
9	276.01	1	1	0	0	2	275	0	1.60	1	154.11
9	277.01	1	0	1	0	1	275	0	1.60	1	126.82
9	278.01	1	.	0	0	2	278	0	1.43	2	126.82
9	279.01	1	.	0	1	.	279	0	1.25	1	195.05
9	280.01	1	0	0	1	1	279	0	1.25	1	195.05
9	281.01	0	1	1	0	2	279	0	1.25	1	140.46
9	282.01	0	.	0	0	3	282	0	1.43	0	195.05
9	283.01	1	1	0	0	2	282	0	1.43	0	235.98
9	284.01	1	0	0	0	1	282	0	1.78	2	235.98
9	285.01	1	0	1	0	1	282	0	1.43	1	235.98
9	286.01	0	1	0	0	1	282	0	1.96	1	195.05
9	287.01	0	0	0	0	1	282	0	1.96	1	195.05
9	288.01	0	0	0	0	2	282	0	2.14	0	195.05
9	289.01	1	1	0	0	1	282	0	2.14	1	181.40
9	290.01	1	0	1	0	1	282	0	1.78	1	195.05
9	291.01	1	0	0	0	1	282	0	1.78	1	195.05
9	292.01	0	.	1	0	3	292	0	1.60	0	235.98
9	293.01	1	1	1	0	2	292	0	1.60	1	154.11
9	294.01	0	1	1	1	1	292	0	1.78	1	195.05
9	295.01	0	0	0	0	1	292	0	1.78	2	195.05
9	296.01	1	1	1	0	1	292	0	1.78	1	222.34
9	297.01	1	0	1	0	1	292	0	1.96	1	222.34
9	298.01	0	1	1	0	1	292	0	2.14	1	195.05
9	299.01	1	1	1	0	1	292	0	2.14	0	195.05
9	300.01	1	0	1	0	2	292	0	1.78	1	195.05
9	301.01	0	1	0	0	1	292	0	1.78	1	235.98
9	302.01	0	0	1	0	1	292	0	1.78	2	235.98
9	303.01	0	0	1	0	1	292	0	1.78	1	222.34

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	254.01	154.82	0.78	1.29	0.77	1.30	0		1	.
9	255.01	152.99	0.76	1.32	0.76	1.32	1	1	0	1.30
9	256.01	109.21	0.75	1.33	0.76	1.32	0		0	.
9	257.01	108.14	0.76	1.32	0.76	1.32	0		1	.
9	258.01	210.88	0.76	1.32	0.76	1.32	0		0	.
9	259.01	138.28	0.76	1.31	0.76	1.32	0		0	.
9	260.01	136.64	0.76	1.32	0.76	1.32	0		0	.
9	261.01	111.11	0.76	1.31	0.76	1.32	0		0	.
9	262.01	112.17	0.77	1.30	0.76	1.32	0		0	.
9	263.01	297.86	0.76	1.32	0.76	1.32	0		0	.
9	264.01	59.99	0.78	1.28	0.76	1.32	0		0	.
9	265.01	58.82	0.77	1.29	0.76	1.32	0		0	.
9	266.01	94.40	0.78	1.29	0.76	1.32	0		0	.
9	267.01	96.83	0.76	1.31	0.76	1.32	0		0	.
9	268.01	98.27	0.77	1.29	0.76	1.32	0		0	.
9	269.01	151.22	0.78	1.27	0.76	1.32	0		0	.
9	270.01	153.12	0.79	1.27	0.76	1.32	0		0	.
9	271.01	103.94	0.79	1.27	0.76	1.32	0		0	.
9	272.01	105.94	0.80	1.25	0.76	1.32	0		0	.
9	273.01	274.88	0.80	1.25	0.76	1.32	0		0	.
9	274.01	276.68	0.81	1.23	0.76	1.32	0		0	.
9	275.01	108.58	0.79	1.27	0.79	1.27	1	0	0	1.32
9	276.01	136.27	0.79	1.27	0.79	1.27	0		1	.
9	277.01	172.71	0.78	1.28	0.79	1.27	0		0	.
9	278.01	184.76	0.79	1.26	0.79	1.26	1	0	0	1.27
9	279.01	113.85	0.76	1.32	0.76	1.32	1	0	0	1.26
9	280.01	115.72	0.76	1.32	0.76	1.32	0		1	.
9	281.01	150.78	0.75	1.33	0.76	1.32	0		0	.
9	282.01	120.02	0.75	1.33	0.75	1.33	1	0	0	1.32
9	283.01	67.26	0.76	1.32	0.75	1.33	0		1	.
9	284.01	72.70	0.75	1.33	0.75	1.33	0		0	.
9	285.01	71.50	0.75	1.33	0.75	1.33	0		0	.
9	286.01	130.47	0.75	1.34	0.75	1.33	0		0	.
9	287.01	131.84	0.76	1.32	0.75	1.33	0		0	.
9	288.01	122.93	0.75	1.33	0.75	1.33	0		0	.
9	289.01	135.04	0.75	1.32	0.75	1.33	0		0	.
9	290.01	136.01	0.75	1.33	0.75	1.33	0		0	.
9	291.01	137.54	0.75	1.34	0.75	1.33	0		0	.
9	292.01	77.37	0.74	1.35	0.74	1.35	1	0	0	1.33
9	293.01	171.43	0.74	1.35	0.74	1.35	0		1	.
9	294.01	142.08	0.75	1.34	0.74	1.35	0		0	.
9	295.01	142.85	0.74	1.35	0.74	1.35	0		0	.
9	296.01	81.28	0.74	1.36	0.74	1.35	0		0	.
9	297.01	83.68	0.74	1.35	0.74	1.35	0		0	.
9	298.01	147.75	0.74	1.35	0.74	1.35	0		0	.
9	299.01	149.09	0.75	1.34	0.74	1.35	0		0	.
9	300.01	150.95	0.75	1.34	0.74	1.35	0		0	.
9	301.01	81.91	0.75	1.33	0.74	1.35	0		0	.
9	302.01	84.15	0.74	1.35	0.74	1.35	0		0	.
9	303.01	84.52	0.74	1.34	0.74	1.35	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	304.01	0	0	0	0	2	292	0	1.78	1	222.34
9	305.01	0	.	1	0	2	305	0	1.96	0	235.98
9	306.01	0	0	0	0	1	305	0	1.78	0	235.98
9	307.01	0	0	1	0	2	305	0	1.60	0	235.98
9	308.01	1	1	1	0	1	305	0	1.78	1	167.75
9	309.01	1	0	1	0	1	305	0	1.78	1	195.05
9	310.01	0	1	1	0	1	305	0	1.78	1	235.98
9	311.01	0	0	1	0	1	305	0	2.14	2	235.98
9	312.01	0	0	0	0	1	305	0	1.96	1	126.82
9	313.01	1	.	0	0	2	313	0	1.78	0	126.82
9	314.01	1	0	1	0	1	313	0	1.60	1	126.82
9	315.01	0	1	1	0	1	313	0	1.60	1	195.05
9	316.01	0	0	1	0	2	313	0	1.60	1	235.98
9	317.01	0	0	0	1	1	313	0	1.43	1	235.98
9	318.01	0	0	0	1	1	313	0	1.78	2	235.98
9	319.01	1	1	0	0	1	313	0	1.78	1	208.69
9	320.01	1	0	1	1	1	313	0	1.96	2	208.69
9	321.01	1	0	0	0	1	313	0	1.96	1	235.98
9	322.01	0	1	0	0	1	313	0	1.96	1	126.82
9	323.01	1	1	1	0	1	313	0	1.96	1	167.75
9	324.01	1	0	0	1	1	313	0	1.78	1	167.75
9	325.01	1	.	1	0	2	325	0	1.60	1	208.69
9	326.01	1	0	1	0	1	325	0	1.78	1	208.69
9	327.01	1	0	1	0	1	325	0	1.78	1	208.69
9	328.01	1	0	1	1	1	325	0	2.14	2	208.69
9	329.01	0	1	1	0	1	325	0	2.14	1	126.82
9	330.01	1	1	1	0	1	325	0	2.14	1	140.46
9	331.01	0	1	1	0	1	325	0	2.14	1	235.98
9	332.01	1	1	0	1	1	325	0	2.32	2	235.98
9	333.01	1	0	1	0	1	325	0	1.78	1	154.11
9	334.01	1	.	0	0	3	334	0	1.78	0	235.98
9	335.01	0	1	0	0	1	334	0	1.78	1	235.98
9	336.01	1	1	1	0	1	334	0	1.60	2	235.98
9	337.01	1	0	1	0	1	334	0	1.78	2	222.34
9	338.01	0	1	0	0	2	334	0	1.43	1	222.34
9	339.01	1	1	1	1	1	334	0	1.96	1	195.05
9	340.01	1	.	1	0	3	340	0	1.78	2	235.98
9	341.01	1	0	1	0	1	340	0	1.78	1	195.05
9	342.01	1	0	0	0	1	340	0	1.43	1	195.05
9	343.01	1	0	1	0	2	340	0	1.43	1	154.11
9	344.01	1	.	1	0	2	344	0	1.43	1	235.98
9	345.01	0	1	0	1	1	344	0	1.78	2	235.98
9	346.01	1	1	1	0	1	344	0	1.78	1	235.98
9	347.01	0	.	0	0	2	347	0	1.60	2	235.98
9	348.01	0	.	1	0	.	348	0	0.71	0	195.05
9	349.01	1	0	1	0	1	350	0	0.71	2	235.98
9	350.01	1	.	1	0	.	350	0	0.36	1	235.98
9	351.01	1	.	0	0	.	351	0	0.36	1	31.30
9	352.01	0	1	1	0	1	351	0	0.71	0	31.30
9	353.01	1	.	0	0	.	353	0	0.36	0	113.17

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	304.01	86.38	0.74	1.36	0.74	1.35	0		0	.
9	305.01	86.28	0.74	1.36	0.74	1.36	1	0	0	1.35
9	306.01	87.69	0.74	1.35	0.74	1.36	0		1	.
9	307.01	105.77	0.74	1.35	0.74	1.36	0		0	.
9	308.01	163.23	0.74	1.36	0.74	1.36	0		0	.
9	309.01	162.93	0.74	1.35	0.74	1.36	0		0	.
9	310.01	107.77	0.74	1.35	0.74	1.36	0		0	.
9	311.01	108.84	0.74	1.35	0.74	1.36	0		0	.
9	312.01	309.25	0.75	1.34	0.74	1.36	0		0	.
9	313.01	310.08	0.77	1.29	0.77	1.29	1	1	0	1.36
9	314.01	312.28	0.77	1.29	0.77	1.29	0		1	.
9	315.01	167.97	0.77	1.29	0.77	1.29	0		0	.
9	316.01	111.78	0.78	1.28	0.77	1.29	0		0	.
9	317.01	113.08	0.78	1.28	0.77	1.29	0		0	.
9	318.01	115.15	0.77	1.29	0.77	1.29	0		0	.
9	319.01	174.95	0.76	1.31	0.77	1.29	0		0	.
9	320.01	175.88	0.77	1.30	0.77	1.29	0		0	.
9	321.01	117.48	0.76	1.31	0.77	1.29	0		0	.
9	322.01	324.69	0.75	1.33	0.77	1.29	0		0	.
9	323.01	181.35	0.75	1.33	0.77	1.29	0		0	.
9	324.01	183.09	0.75	1.33	0.77	1.29	0		0	.
9	325.01	180.22	0.74	1.35	0.74	1.35	1	1	0	1.29
9	326.01	181.85	0.75	1.34	0.74	1.35	0		1	.
9	327.01	183.72	0.75	1.33	0.74	1.35	0		0	.
9	328.01	185.32	0.76	1.32	0.74	1.35	0		0	.
9	329.01	336.04	0.76	1.31	0.74	1.35	0		0	.
9	330.01	243.44	0.76	1.31	0.74	1.35	0		0	.
9	331.01	131.16	0.76	1.31	0.74	1.35	0		0	.
9	332.01	130.06	0.77	1.29	0.74	1.35	0		0	.
9	333.01	237.50	0.77	1.30	0.74	1.35	0		0	.
9	334.01	133.50	0.78	1.28	0.78	1.28	1	0	0	1.35
9	335.01	135.37	0.79	1.26	0.78	1.28	0		1	.
9	336.01	137.03	0.77	1.30	0.78	1.28	0		0	.
9	337.01	144.04	0.77	1.30	0.78	1.28	0		0	.
9	338.01	145.64	0.77	1.29	0.78	1.28	0		0	.
9	339.01	216.59	0.78	1.29	0.78	1.28	0		0	.
9	340.01	182.55	0.78	1.29	0.78	1.29	1	0	0	1.28
9	341.01	258.86	0.78	1.29	0.78	1.29	0		1	.
9	342.01	259.83	0.80	1.25	0.78	1.29	0		0	.
9	343.01	302.83	0.80	1.25	0.78	1.29	0		0	.
9	344.01	223.39	0.80	1.24	0.80	1.24	1	1	0	1.29
9	345.01	224.82	0.79	1.27	0.80	1.24	0		1	.
9	346.01	226.92	0.79	1.27	0.80	1.24	0		0	.
9	347.01	329.99	0.79	1.26	0.79	1.26	1	0	0	1.24
9	348.01	414.95	1.45	0.69	1.45	0.69	1	0	0	1.26
9	349.01	432.73	1.17	0.85	1.16	0.86	0		1	.
9	350.01	431.40	1.16	0.86	1.16	0.86	1	0	0	1.83
9	351.01	183.21	0.55	1.83	0.55	1.83	1	0	0	0.69
9	352.01	186.32	0.52	1.93	0.55	1.83	0		1	.
9	353.01	631.87	0.96	1.04	0.96	1.04	1	0	0	0.86

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	355.01	0	.	1	0	.	355	0	0.36	1	154.11
9	356.01	0	0	0	0	2	355	0	0.71	0	154.11
9	65.02	1	.	0	0	.	65	0	1.25	1	4.01
9	66.02	1	0	0	0	2	65	0	1.60	1	4.01
9	70.02	0	.	0	0	.	70	0	0.71	1	4.01
9	71.02	0	.	0	0	.	71	0	0.36	0	58.59
9	72.02	1	1	1	0	1	71	0	0.71	1	58.59
9	75.02	0	.	0	0	2	75	0	1.07	1	58.59
9	77.02	0	.	1	0	2	77	0	1.43	1	4.01
9	81.02	0	.	0	0	1	81	0	1.25	1	58.59
9	82.02	0	0	0	0	1	81	0	1.78	1	58.59
9	86.02	1	.	1	0	.	86	0	0.71	1	44.94
9	87.02	0	1	0	0	2	86	0	0.89	1	44.94
9	94.02	1	.	1	0	.	94	0	1.07	1	58.59
9	95.02	1	0	0	0	1	94	0	1.60	1	58.59
9	96.02	0	.	0	0	2	96	0	1.60	0	4.01
9	100.02	0	.	0	0	2	100	0	1.78	1	58.59
9	101.02	1	1	1	1	1	100	0	2.14	1	58.59
9	102.02	0	1	0	0	1	100	0	2.14	0	58.59
9	103.02	0	0	0	0	1	100	0	2.14	1	4.01
9	104.02	0	0	1	0	1	100	0	2.14	0	31.30
9	105.02	0	0	0	0	1	100	0	1.96	1	4.01
9	106.02	1	1	1	0	1	100	0	1.96	1	4.01
9	110.02	1	1	1	0	1	111	0	1.96	1	58.59
9	111.02	0	.	0	0	1	111	0	1.78	1	58.59
9	113.02	0	.	0	0	1	113	0	2.14	2	31.30
9	114.02	1	.	1	0	1	114	0	1.96	1	17.65
9	115.02	1	.	1	0	1	115	0	2.49	1	58.59
9	116.02	0	1	0	0	1	115	0	2.49	1	4.01
9	117.02	1	1	1	0	1	115	0	2.67	2	17.65
9	118.02	1	0	1	0	1	115	0	2.67	1	17.65
9	119.02	0	1	1	0	1	115	0	2.67	1	4.01
9	120.02	1	1	1	1	1	115	0	2.85	1	31.30
9	121.02	1	0	1	0	1	115	0	2.14	0	17.65
9	122.02	1	0	1	0	2	115	0	1.96	0	4.01
9	123.02	0	1	0	0	2	115	0	1.78	1	31.30
9	124.02	1	.	0	0	2	124	0	1.78	0	17.65
9	125.02	0	1	0	0	1	124	0	1.78	1	17.65
9	126.02	1	.	1	0	.	126	0	1.60	1	58.59
9	127.02	1	.	1	0	2	127	0	1.60	0	17.65
9	130.02	0	.	1	0	1	130	0	1.96	0	4.01
9	131.02	1	.	1	0	.	131	0	1.60	1	4.01
9	133.02	1	1	1	0	1	130	0	1.96	1	31.30
9	134.02	0	1	0	0	1	130	0	1.96	1	17.65
9	135.02	1	1	0	0	1	130	0	2.14	2	58.59
9	136.02	1	0	1	0	1	130	0	2.32	1	31.30
9	137.02	0	1	0	0	1	130	0	2.67	2	17.65
9	140.02	0	.	0	0	1	140	0	2.49	1	17.65
9	142.02	1	.	1	0	1	142	0	2.67	0	58.59
9	143.02	0	1	0	0	1	142	0	2.85	2	4.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	355.01	859.42	1.66	0.60	1.66	0.60	1	0	0	1.04
9	356.01	861.26	1.64	0.61	1.66	0.60	0		1	.
9	65.02	48.01	1.01	0.99	1.01	0.99	1	0	0	.
9	66.02	49.81	1.03	0.97	1.01	0.99	0		1	.
9	70.02	46.74	0.98	1.02	0.98	1.02	1	0	0	0.99
9	71.02	16.28	1.28	0.78	1.28	0.78	1	0	0	1.02
9	72.02	14.68	1.31	0.77	1.28	0.78	0		1	.
9	75.02	20.36	1.27	0.79	1.27	0.79	1	1	0	0.78
9	77.02	67.56	1.23	0.82	1.23	0.82	1	4	0	0.79
9	81.02	22.19	1.08	0.93	1.08	0.93	1	4	0	0.82
9	82.02	23.49	1.07	0.94	1.08	0.93	0		1	.
9	86.02	52.52	1.15	0.87	1.15	0.87	1	0	0	0.93
9	87.02	53.75	1.16	0.86	1.15	0.87	0		1	.
9	94.02	31.80	1.09	0.92	1.09	0.92	1	0	0	0.87
9	95.02	32.87	1.08	0.92	1.09	0.92	0		1	.
9	96.02	81.14	1.10	0.91	1.10	0.91	1	0	0	0.92
9	100.02	34.04	0.92	1.08	0.92	1.08	1	1	0	0.91
9	101.02	35.24	0.91	1.10	0.92	1.08	0		1	.
9	102.02	36.57	0.89	1.13	0.92	1.08	0		0	.
9	103.02	84.55	0.87	1.15	0.92	1.08	0		0	.
9	104.02	62.99	0.87	1.14	0.92	1.08	0		0	.
9	105.02	89.22	0.88	1.14	0.92	1.08	0		0	.
9	106.02	91.75	0.87	1.15	0.92	1.08	0		0	.
9	110.02	39.31	0.77	1.30	0.81	1.23	0		1	.
9	111.02	37.44	0.81	1.23	0.81	1.23	1	4	0	1.08
9	113.02	66.46	0.76	1.32	0.76	1.32	1	2	0	1.23
9	114.02	91.62	0.70	1.43	0.70	1.43	1	3	0	1.23
9	115.02	40.41	0.70	1.42	0.70	1.42	1	1	0	1.23
9	116.02	94.76	0.70	1.43	0.70	1.42	0		1	.
9	117.02	96.69	0.71	1.41	0.70	1.42	0		0	.
9	118.02	98.93	0.71	1.42	0.70	1.42	0		0	.
9	119.02	100.30	0.71	1.41	0.70	1.42	0		0	.
9	120.02	68.17	0.71	1.41	0.70	1.42	0		0	.
9	121.02	102.63	0.70	1.42	0.70	1.42	0		0	.
9	122.02	105.27	0.71	1.41	0.70	1.42	0		0	.
9	123.02	69.77	0.72	1.40	0.70	1.42	0		0	.
9	124.02	107.10	0.70	1.43	0.70	1.43	1	0	0	1.42
9	125.02	108.81	0.70	1.44	0.70	1.43	0		1	.
9	126.02	41.74	0.73	1.38	0.73	1.38	1	0	0	1.43
9	127.02	112.98	0.68	1.47	0.68	1.47	1	0	0	1.38
9	130.02	118.55	0.67	1.50	0.67	1.50	1	1	0	1.47
9	131.02	114.24	0.61	1.64	0.61	1.64	1	3	0	1.47
9	133.02	72.60	0.59	1.69	0.67	1.50	0		1	.
9	134.02	116.61	0.59	1.70	0.67	1.50	0		0	.
9	135.02	43.65	0.57	1.74	0.67	1.50	0		0	.
9	136.02	74.71	0.57	1.75	0.67	1.50	0		0	.
9	137.02	121.55	0.57	1.77	0.67	1.50	0		0	.
9	140.02	123.49	0.55	1.81	0.55	1.81	1	4	0	1.50
9	142.02	45.78	0.53	1.88	0.53	1.88	1	4	0	1.81
9	143.02	133.20	0.52	1.91	0.53	1.88	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	144.02	1	0	1	0	1	142	0	2.49	1	4.01
9	145.02	0	0	0	0	1	142	0	2.32	0	17.65
9	146.02	0	0	1	0	1	142	0	1.96	1	31.30
9	147.02	0	.	0	0	1	147	0	1.96	1	58.59
9	148.02	0	0	0	0	1	147	0	2.14	1	58.59
9	149.02	0	0	1	0	1	147	0	2.14	0	17.65
9	150.02	0	0	0	0	1	147	0	2.49	1	17.65
9	151.02	0	0	0	0	1	147	0	2.49	2	17.65
9	152.02	1	1	1	0	1	147	0	2.49	1	58.59
9	153.02	1	0	1	0	1	147	0	2.85	1	58.59
9	154.02	1	0	0	0	1	147	0	2.85	2	17.65
9	155.02	0	1	0	0	1	147	0	2.85	1	17.65
9	156.02	1	1	1	0	1	147	0	2.67	1	31.30
9	157.02	1	0	1	1	1	147	0	2.14	1	31.30
9	159.02	0	.	1	0	1	159	0	2.14	1	17.65
9	160.02	1	1	1	1	1	159	0	1.96	1	17.65
9	161.02	1	0	1	0	2	159	0	1.96	1	17.65
9	162.02	0	.	0	1	1	162	0	2.14	0	58.59
9	163.02	0	.	0	0	.	163	0	1.96	1	31.30
9	164.02	0	0	0	0	1	163	0	1.96	1	31.30
9	165.02	0	0	0	0	1	163	0	1.96	1	17.65
9	166.02	0	0	1	0	1	163	0	1.96	1	17.65
9	167.02	0	0	0	0	1	163	0	2.14	2	17.65
9	168.02	0	0	0	1	1	163	0	2.14	2	58.59
9	169.02	0	0	0	0	1	163	0	1.96	1	58.59
9	170.02	0	.	1	0	1	170	0	1.96	1	17.65
9	171.02	0	.	1	0	1	171	0	1.96	0	17.65
9	172.02	0	0	0	0	1	170	0	1.96	1	17.65
9	173.02	1	.	1	0	1	173	0	2.14	1	31.30
9	174.02	0	1	1	0	1	173	0	2.32	0	17.65
9	175.02	1	.	1	0	1	175	0	2.14	1	17.65
9	176.02	1	0	1	1	1	175	0	1.96	1	17.65
9	177.02	1	0	1	0	1	175	0	1.78	1	17.65
9	178.02	1	0	0	0	1	175	0	2.32	2	17.65
9	179.02	0	1	0	0	2	175	0	1.96	1	31.30
9	180.02	0	0	1	0	2	175	0	2.14	1	58.59
9	181.02	0	0	0	0	1	175	0	2.32	2	58.59
9	182.02	0	0	0	0	1	175	0	2.85	1	4.01
9	183.02	0	0	1	0	1	175	0	3.03	2	4.01
9	184.02	0	0	0	0	1	175	0	2.32	1	31.30
9	185.02	0	0	0	0	2	175	0	2.32	1	44.94
9	187.02	0	0	0	0	1	175	0	2.32	0	31.30
9	188.02	0	0	0	0	1	189	0	2.32	2	58.59
9	189.02	0	.	1	0	1	189	0	2.85	1	58.59
9	190.02	0	0	0	1	1	189	0	2.32	1	72.24
9	191.02	0	0	1	0	1	189	0	2.49	2	72.24
9	192.02	1	1	0	0	1	189	0	2.32	2	72.24
9	193.02	0	1	1	0	1	189	0	2.32	0	31.30
9	194.02	0	.	0	0	1	194	0	1.96	1	17.65
9	195.02	0	.	1	0	1	195	0	2.32	2	17.65

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	144.02	130.83	0.52	1.92	0.53	1.88	0		1	.
9	145.02	128.36	0.52	1.92	0.53	1.88	0		0	.
9	146.02	77.01	0.51	1.98	0.53	1.88	0		0	.
9	147.02	46.38	0.50	2.01	0.50	2.01	1	0	0	1.88
9	148.02	49.48	0.49	2.05	0.50	2.01	0		1	.
9	149.02	135.67	0.48	2.07	0.50	2.01	0		0	.
9	150.02	136.80	0.48	2.08	0.50	2.01	0		0	.
9	151.02	139.20	0.48	2.08	0.50	2.01	0		0	.
9	152.02	53.52	0.48	2.09	0.50	2.01	0		0	.
9	153.02	57.69	0.48	2.06	0.50	2.01	0		0	.
9	154.02	143.11	0.48	2.06	0.50	2.01	0		0	.
9	155.02	144.97	0.48	2.08	0.50	2.01	0		0	.
9	156.02	83.65	0.49	2.06	0.50	2.01	0		0	.
9	157.02	87.48	0.48	2.07	0.50	2.01	0		0	.
9	159.02	150.71	0.47	2.13	0.47	2.13	1	4	0	2.01
9	160.02	152.65	0.47	2.12	0.47	2.13	0		1	.
9	161.02	154.52	0.47	2.11	0.47	2.13	0		0	.
9	162.02	59.03	0.47	2.14	0.47	2.14	1	0	0	2.13
9	163.02	89.89	0.47	2.14	0.47	2.14	1	0	0	2.14
9	164.02	91.79	0.47	2.14	0.47	2.14	0		1	.
9	165.02	160.46	0.47	2.14	0.47	2.14	0		0	.
9	166.02	161.89	0.47	2.13	0.47	2.14	0		0	.
9	167.02	164.09	0.47	2.14	0.47	2.14	0		0	.
9	168.02	60.33	0.47	2.13	0.47	2.14	0		0	.
9	169.02	64.90	0.47	2.14	0.47	2.14	0		0	.
9	170.02	170.30	0.46	2.19	0.46	2.19	1	3	0	2.14
9	171.02	173.67	0.51	1.98	0.51	1.98	1	2	0	2.14
9	172.02	171.77	0.45	2.22	0.46	2.19	0		1	.
9	173.02	96.89	0.47	2.12	0.47	2.12	1	1	0	2.14
9	174.02	177.04	0.47	2.13	0.47	2.12	0		1	.
9	175.02	179.01	0.47	2.15	0.47	2.15	1	0	0	2.12
9	176.02	181.18	0.46	2.17	0.47	2.15	0		1	.
9	177.02	173.38	0.47	2.14	0.47	2.15	0		0	.
9	178.02	184.95	0.48	2.06	0.47	2.15	0		0	.
9	179.02	100.86	0.61	1.65	0.47	2.15	0		0	.
9	180.02	66.84	0.62	1.62	0.47	2.15	0		0	.
9	181.02	68.17	0.62	1.61	0.47	2.15	0		0	.
9	182.02	199.16	0.62	1.61	0.47	2.15	0		0	.
9	183.02	211.17	0.63	1.60	0.47	2.15	0		0	.
9	184.02	105.17	0.63	1.59	0.47	2.15	0		0	.
9	185.02	97.63	0.62	1.60	0.47	2.15	0		0	.
9	187.02	112.44	0.63	1.59	0.47	2.15	0		0	.
9	188.02	71.21	0.65	1.54	0.61	1.64	0		1	.
9	189.02	69.64	0.61	1.64	0.61	1.64	1	4	0	2.15
9	190.02	74.34	0.62	1.61	0.61	1.64	0		0	.
9	191.02	75.78	0.63	1.60	0.61	1.64	0		0	.
9	192.02	77.78	0.61	1.64	0.61	1.64	0		0	.
9	193.02	120.35	0.60	1.66	0.61	1.64	0		0	.
9	194.02	227.59	0.61	1.64	0.61	1.64	1	2	0	1.64
9	195.02	227.69	0.60	1.68	0.60	1.68	1	3	0	1.64

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	196.02	1	.	1	0	1	196	0	2.32	1	17.65
9	197.02	0	.	0	0	2	197	0	2.49	2	4.01
9	198.02	0	0	1	0	1	197	0	2.32	0	31.30
9	199.02	0	0	1	0	2	197	0	2.67	1	17.65
9	200.02	1	1	1	0	2	197	0	2.49	1	17.65
9	201.02	0	1	0	1	2	197	0	2.14	1	58.59
9	202.02	0	0	1	0	1	197	0	2.32	1	17.65
9	203.02	1	1	1	0	1	197	0	2.49	2	17.65
9	204.02	0	1	0	0	1	197	0	2.49	1	17.65
9	205.02	0	0	1	0	1	197	0	2.49	0	31.30
9	206.02	0	0	0	0	2	197	0	2.32	1	17.65
9	207.02	0	.	0	0	1	207	0	2.49	1	17.65
9	208.02	0	0	0	0	2	207	0	2.32	1	17.65
9	209.02	0	0	1	0	2	207	0	2.32	0	31.30
9	210.02	0	0	0	0	1	207	0	2.32	1	17.65
9	211.02	0	0	0	0	1	207	0	2.49	1	58.59
9	212.02	1	1	1	0	2	207	0	2.32	1	17.65
9	213.02	0	1	1	0	2	207	0	2.32	1	31.30
9	214.02	1	1	1	0	1	207	0	2.32	1	31.30
9	215.02	0	1	1	0	1	207	0	2.32	1	58.59
9	216.02	0	.	1	0	2	216	0	2.14	1	58.59
9	217.02	0	0	0	0	1	216	0	2.32	2	58.59
9	218.02	0	0	0	0	1	216	0	2.32	1	31.30
9	219.02	1	1	1	0	2	216	0	2.14	1	31.30
9	220.02	1	0	1	0	1	216	0	2.32	1	31.30
9	221.02	1	0	0	0	1	216	0	2.32	1	58.59
9	222.02	0	.	0	0	2	222	0	2.32	1	58.59
9	223.02	0	0	1	0	1	222	0	2.32	1	58.59
9	224.02	1	1	1	0	2	222	0	2.32	1	72.24
9	225.02	1	0	1	0	1	222	0	2.32	2	72.24
9	226.02	1	0	1	0	1	222	0	2.49	1	113.17
9	227.02	0	1	0	0	1	222	0	2.49	0	113.17
9	228.02	1	1	1	0	1	222	0	2.49	1	113.17
9	229.02	0	1	0	0	1	222	0	2.49	1	126.82
9	230.02	1	1	1	0	2	222	0	2.32	1	99.53
9	231.02	0	1	0	0	1	222	0	2.14	1	72.24
9	232.02	0	0	0	1	2	222	0	2.14	1	99.53
9	233.02	0	.	0	0	2	233	0	1.96	1	58.59
9	234.02	0	0	1	0	1	233	0	1.96	1	58.59
9	235.02	1	.	1	0	2	235	0	1.96	1	99.53
9	236.02	1	.	1	0	2	236	0	1.96	0	99.53
9	237.02	0	1	0	0	2	236	0	1.96	1	72.24
9	238.02	1	1	1	0	1	236	0	2.14	2	72.24
9	239.02	0	1	1	0	1	236	0	2.14	0	72.24
9	240.02	0	.	1	0	.	240	0	1.96	2	72.24
9	241.02	1	1	1	0	1	240	0	2.14	1	113.17
9	242.02	1	0	1	0	2	240	0	2.32	1	113.17
9	243.02	1	0	1	0	1	240	0	2.32	1	140.46
9	244.02	0	1	0	0	2	240	0	2.14	1	72.24
9	245.02	0	.	0	0	1	245	0	2.14	2	4.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	196.02	229.59	0.60	1.67	0.60	1.67	1	1	0	1.64
9	197.02	231.63	0.58	1.73	0.58	1.73	1	0	0	1.67
9	198.02	122.25	0.56	1.77	0.58	1.73	0		1	.
9	199.02	233.30	0.56	1.80	0.58	1.73	0		0	.
9	200.02	235.30	0.55	1.80	0.58	1.73	0		0	.
9	201.02	738.91	0.54	1.84	0.58	1.73	0		0	.
9	202.02	239.00	0.55	1.83	0.58	1.73	0		0	.
9	203.02	240.94	0.55	1.83	0.58	1.73	0		0	.
9	204.02	242.71	0.54	1.85	0.58	1.73	0		0	.
9	205.02	139.80	0.54	1.85	0.58	1.73	0		0	.
9	206.02	246.41	0.55	1.82	0.58	1.73	0		0	.
9	207.02	247.98	0.52	1.91	0.52	1.91	1	1	0	1.73
9	208.02	249.78	0.52	1.93	0.52	1.91	0		1	.
9	209.02	146.34	0.52	1.94	0.52	1.91	0		0	.
9	210.02	252.85	0.52	1.93	0.52	1.91	0		0	.
9	211.02	81.48	0.51	1.95	0.52	1.91	0		0	.
9	212.02	256.59	0.51	1.96	0.52	1.91	0		0	.
9	213.02	156.72	0.51	1.97	0.52	1.91	0		0	.
9	214.02	184.35	0.51	1.97	0.52	1.91	0		0	.
9	215.02	83.32	0.50	1.98	0.52	1.91	0		0	.
9	216.02	85.02	0.50	2.00	0.50	2.00	1	1	0	1.91
9	217.02	86.69	0.49	2.05	0.50	2.00	0		1	.
9	218.02	165.39	0.49	2.04	0.50	2.00	0		0	.
9	219.02	187.25	0.50	2.02	0.50	2.00	0		0	.
9	220.02	190.42	0.49	2.04	0.50	2.00	0		0	.
9	221.02	90.49	0.49	2.02	0.50	2.00	0		0	.
9	222.02	94.80	0.50	2.01	0.50	2.01	1	1	0	2.00
9	223.02	97.23	0.50	2.01	0.50	2.01	0		1	.
9	224.02	102.57	0.50	2.00	0.50	2.01	0		0	.
9	225.02	104.37	0.50	1.98	0.50	2.01	0		0	.
9	226.02	52.68	0.51	1.97	0.50	2.01	0		0	.
9	227.02	54.15	0.51	1.97	0.50	2.01	0		0	.
9	228.02	55.55	0.50	1.98	0.50	2.01	0		0	.
9	229.02	51.38	0.51	1.98	0.50	2.01	0		0	.
9	230.02	84.09	0.51	1.97	0.50	2.01	0		0	.
9	231.02	113.75	0.52	1.93	0.50	2.01	0		0	.
9	232.02	85.96	0.52	1.92	0.50	2.01	0		0	.
9	233.02	114.05	0.54	1.85	0.54	1.85	1	1	0	2.01
9	234.02	112.51	0.54	1.85	0.54	1.85	0		1	.
9	235.02	89.46	0.55	1.82	0.55	1.82	1	1	0	1.85
9	236.02	93.06	0.61	1.63	0.61	1.63	1	0	0	1.82
9	237.02	124.73	0.63	1.59	0.61	1.63	0		1	.
9	238.02	126.90	0.61	1.64	0.61	1.63	0		0	.
9	239.02	130.23	0.61	1.64	0.61	1.63	0		0	.
9	240.02	131.67	0.61	1.65	0.61	1.65	1	0	0	1.63
9	241.02	74.44	0.60	1.65	0.61	1.65	0		1	.
9	242.02	73.80	0.61	1.65	0.61	1.65	0		0	.
9	243.02	50.55	0.61	1.65	0.61	1.65	0		0	.
9	244.02	139.41	0.61	1.65	0.61	1.65	0		0	.
9	245.02	327.79	0.62	1.62	0.62	1.62	1	2	0	1.65

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	246.02	0	.	0	0	1	246	0	2.14	0	4.01
9	247.02	0	.	0	0	1	247	0	1.96	1	140.46
9	248.02	0	0	0	0	1	247	0	2.32	1	195.05
9	249.02	0	0	0	0	1	247	0	2.49	1	126.82
9	250.02	0	0	0	0	1	247	0	2.49	1	72.24
9	251.02	0	.	0	0	2	251	0	2.14	1	85.88
9	252.02	0	0	0	0	1	251	0	1.96	1	85.88
9	253.02	1	1	0	0	2	251	0	1.96	1	58.59
9	254.02	0	1	0	0	1	251	0	2.14	1	72.24
9	255.02	0	.	1	0	3	255	0	2.14	0	72.24
9	256.02	0	0	0	1	1	255	0	2.32	2	126.82
9	257.02	0	0	0	0	1	255	0	2.14	1	126.82
9	258.02	1	1	1	0	1	255	0	2.32	1	58.59
9	259.02	1	0	1	0	1	255	0	2.32	2	85.88
9	260.02	0	1	1	0	1	255	0	2.67	1	85.88
9	261.02	1	0	0	0	2	255	0	1.96	1	126.82
9	262.02	1	0	0	0	1	255	0	1.96	0	126.82
9	263.02	1	1	1	0	2	255	0	2.32	1	44.94
9	264.02	0	.	1	0	1	264	0	2.14	2	208.69
9	265.02	0	.	1	0	1	265	0	2.14	1	208.69
9	266.02	1	.	1	0	1	266	0	2.14	2	140.46
9	267.02	0	1	0	0	1	266	0	2.32	1	140.46
9	268.02	1	1	1	0	1	266	0	2.32	2	140.46
9	269.02	0	.	0	0	.	269	0	2.14	1	85.88
9	270.02	0	0	0	0	2	269	0	1.78	0	85.88
9	271.02	0	.	0	0	2	271	0	1.60	1	154.11
9	272.02	1	1	1	0	1	271	0	1.78	1	154.11
9	273.02	1	0	1	0	1	271	0	1.96	1	72.24
9	274.02	0	1	0	0	1	271	0	2.14	0	72.24
9	275.02	0	.	1	0	2	275	0	1.96	1	154.11
9	276.02	1	1	0	0	2	275	0	1.96	0	126.82
9	277.02	1	.	1	0	1	277	0	1.78	1	99.53
9	278.02	1	.	0	0	.	278	0	1.60	2	99.53
9	279.02	1	.	0	1	2	279	0	1.60	1	167.75
9	280.02	1	0	0	1	1	279	0	1.60	1	167.75
9	281.02	0	.	1	0	.	281	0	1.60	1	113.17
9	282.02	0	.	0	0	3	282	0	1.78	0	167.75
9	283.02	1	1	0	0	2	282	0	1.60	0	208.69
9	284.02	1	0	0	0	1	282	0	1.96	2	208.69
9	285.02	1	0	1	0	1	282	0	1.96	1	208.69
9	286.02	0	1	0	0	2	282	0	1.96	1	167.75
9	287.02	0	0	0	0	1	282	0	2.14	1	167.75
9	288.02	0	.	0	0	2	288	0	2.49	0	167.75
9	289.02	1	1	0	0	1	288	0	2.32	1	154.11
9	290.02	1	.	1	0	1	290	0	2.14	1	167.75
9	291.02	1	0	0	0	1	290	0	2.14	1	167.75
9	292.02	0	.	1	0	3	292	0	2.14	0	208.69
9	293.02	1	1	1	0	2	292	0	2.14	0	126.82
9	294.02	0	.	1	1	1	294	0	1.96	1	167.75
9	295.02	0	0	0	0	1	294	0	2.14	2	167.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	246.02	325.76	0.60	1.67	0.60	1.67	1	3	0	1.65
9	247.02	52.52	0.61	1.64	0.61	1.64	1	1	0	1.65
9	248.02	34.23	0.60	1.65	0.61	1.64	0		1	.
9	249.02	91.79	0.60	1.67	0.61	1.64	0		0	.
9	250.02	145.51	0.60	1.66	0.61	1.64	0		0	.
9	251.02	117.59	0.61	1.64	0.61	1.64	1	0	0	1.64
9	252.02	119.02	0.62	1.62	0.61	1.64	0		1	.
9	253.02	184.92	0.62	1.62	0.61	1.64	0		0	.
9	254.02	154.82	0.62	1.61	0.61	1.64	0		0	.
9	255.02	152.99	0.64	1.55	0.64	1.55	1	0	0	1.64
9	256.02	109.21	0.65	1.54	0.64	1.55	0		0	.
9	257.02	108.14	0.65	1.54	0.64	1.55	0		1	.
9	258.02	210.88	0.65	1.55	0.64	1.55	0		0	.
9	259.02	138.28	0.65	1.54	0.64	1.55	0		0	.
9	260.02	136.64	0.65	1.54	0.64	1.55	0		0	.
9	261.02	111.11	0.65	1.54	0.64	1.55	0		0	.
9	262.02	112.17	0.65	1.53	0.64	1.55	0		0	.
9	263.02	297.86	0.65	1.53	0.64	1.55	0		0	.
9	264.02	59.99	0.65	1.55	0.65	1.55	1	2	0	1.55
9	265.02	58.82	0.63	1.58	0.63	1.58	1	3	0	1.55
9	266.02	94.40	0.64	1.56	0.64	1.56	1	1	0	1.55
9	267.02	96.83	0.65	1.55	0.64	1.56	0		1	.
9	268.02	98.27	0.65	1.55	0.64	1.56	0		0	.
9	269.02	151.22	0.66	1.51	0.66	1.51	1	1	0	1.56
9	270.02	153.12	0.66	1.51	0.66	1.51	0		1	.
9	271.02	103.94	0.67	1.50	0.67	1.50	1	1	0	1.51
9	272.02	105.94	0.66	1.53	0.67	1.50	0		1	.
9	273.02	274.88	0.66	1.52	0.67	1.50	0		0	.
9	274.02	276.68	0.66	1.51	0.67	1.50	0		0	.
9	275.02	108.58	0.68	1.47	0.68	1.47	1	1	0	1.50
9	276.02	136.27	0.67	1.48	0.68	1.47	0		1	.
9	277.02	172.71	0.68	1.47	0.68	1.47	1	1	0	1.47
9	278.02	184.76	0.68	1.46	0.68	1.46	1	1	0	1.47
9	279.02	113.85	0.71	1.41	0.71	1.41	1	1	0	1.46
9	280.02	115.72	0.71	1.41	0.71	1.41	0		1	.
9	281.02	150.78	0.71	1.41	0.71	1.41	1	1	0	1.41
9	282.02	120.02	0.71	1.40	0.71	1.40	1	0	0	1.41
9	283.02	67.26	0.71	1.41	0.71	1.40	0		1	.
9	284.02	72.70	0.71	1.41	0.71	1.40	0		0	.
9	285.02	71.50	0.71	1.40	0.71	1.40	0		0	.
9	286.02	130.47	0.71	1.41	0.71	1.40	0		0	.
9	287.02	131.84	0.71	1.41	0.71	1.40	0		0	.
9	288.02	122.93	0.71	1.41	0.71	1.41	1	1	0	1.40
9	289.02	135.04	0.72	1.40	0.71	1.41	0		1	.
9	290.02	136.01	0.72	1.39	0.72	1.39	1	1	0	1.41
9	291.02	137.54	0.72	1.39	0.72	1.39	0		1	.
9	292.02	77.37	0.72	1.39	0.72	1.39	1	0	0	1.39
9	293.02	171.43	0.72	1.38	0.72	1.39	0		1	.
9	294.02	142.08	0.75	1.33	0.75	1.33	1	1	0	1.39
9	295.02	142.85	0.75	1.34	0.75	1.33	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	296.02	1	1	1	0	1	294	0	2.14	1	195.05
9	297.02	1	0	1	0	1	294	0	2.14	1	195.05
9	298.02	0	1	1	0	1	294	0	2.32	1	167.75
9	299.02	1	1	1	0	1	294	0	2.14	0	167.75
9	300.02	1	0	1	0	2	294	0	1.96	1	167.75
9	301.02	0	1	0	0	2	294	0	1.78	1	208.69
9	302.02	0	0	1	0	1	294	0	1.96	2	208.69
9	303.02	0	0	1	0	1	294	0	1.96	1	195.05
9	304.02	0	0	0	0	2	294	0	1.96	0	195.05
9	305.02	0	.	1	0	2	305	0	2.14	0	208.69
9	306.02	0	0	0	0	1	305	0	2.14	0	208.69
9	307.02	0	0	1	0	2	305	0	1.96	0	208.69
9	308.02	1	1	1	0	1	305	0	1.96	1	140.46
9	309.02	1	0	1	0	1	305	0	1.96	1	167.75
9	310.02	0	1	1	0	1	305	0	2.14	1	208.69
9	311.02	0	0	1	0	1	305	0	2.32	2	208.69
9	312.02	0	0	0	0	2	305	0	2.14	1	99.53
9	313.02	1	.	0	0	3	313	0	1.78	1	99.53
9	314.02	1	0	1	0	2	313	0	1.60	1	99.53
9	315.02	0	1	1	0	1	313	0	1.60	1	167.75
9	316.02	0	.	1	0	2	316	0	1.78	1	208.69
9	317.02	0	0	0	1	1	316	0	1.78	1	208.69
9	318.02	0	0	0	1	1	316	0	1.96	2	208.69
9	319.02	1	1	0	0	1	316	0	2.14	1	181.40
9	320.02	1	0	1	1	1	316	0	2.32	2	181.40
9	321.02	1	0	0	0	1	316	0	2.32	1	208.69
9	322.02	0	1	0	0	1	316	0	2.32	1	99.53
9	323.02	1	1	1	0	1	316	0	2.32	1	140.46
9	324.02	1	0	0	1	1	316	0	2.14	1	140.46
9	325.02	1	.	1	0	3	325	0	1.96	1	181.40
9	326.02	1	0	1	0	1	325	0	1.96	1	181.40
9	327.02	1	0	1	0	1	325	0	1.96	1	181.40
9	328.02	1	0	1	1	1	325	0	2.32	2	181.40
9	329.02	0	1	1	0	1	325	0	2.32	1	99.53
9	330.02	1	1	1	0	1	325	0	2.32	1	113.17
9	331.02	0	1	1	0	1	325	0	2.32	1	208.69
9	332.02	1	1	0	1	2	325	0	2.32	2	208.69
9	333.02	1	0	1	0	1	325	0	2.14	1	126.82
9	334.02	1	.	0	0	3	334	0	1.96	0	208.69
9	335.02	0	1	0	0	1	334	0	1.96	1	208.69
9	336.02	1	1	1	0	1	334	0	1.96	2	208.69
9	337.02	1	1	1	0	1	338	0	1.96	2	195.05
9	338.02	0	.	0	0	2	338	0	1.78	1	195.05
9	339.02	1	.	1	1	1	339	0	2.14	0	167.75
9	340.02	1	.	1	0	.	340	0	2.14	0	208.69
9	341.02	1	.	1	0	.	341	0	1.78	1	167.75
9	342.02	1	0	0	0	1	341	0	1.60	0	167.75
9	343.02	1	0	1	0	2	341	0	1.78	1	126.82
9	344.02	1	.	1	0	3	344	0	1.78	1	208.69
9	345.02	0	1	0	1	1	344	0	1.96	2	208.69

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	296.02	81.28	0.75	1.33	0.75	1.33	0		0	.
9	297.02	83.68	0.75	1.33	0.75	1.33	0		0	.
9	298.02	147.75	0.75	1.34	0.75	1.33	0		0	.
9	299.02	149.09	0.74	1.35	0.75	1.33	0		0	.
9	300.02	150.95	0.74	1.35	0.75	1.33	0		0	.
9	301.02	81.91	0.75	1.34	0.75	1.33	0		0	.
9	302.02	84.15	0.76	1.32	0.75	1.33	0		0	.
9	303.02	84.52	0.77	1.30	0.75	1.33	0		0	.
9	304.02	86.38	0.76	1.31	0.75	1.33	0		0	.
9	305.02	86.28	0.77	1.30	0.77	1.30	1	1	0	1.33
9	306.02	87.69	0.77	1.30	0.77	1.30	0		1	.
9	307.02	105.77	0.77	1.30	0.77	1.30	0		0	.
9	308.02	163.23	0.77	1.30	0.77	1.30	0		0	.
9	309.02	162.93	0.76	1.31	0.77	1.30	0		0	.
9	310.02	107.77	0.76	1.32	0.77	1.30	0		0	.
9	311.02	108.84	0.76	1.32	0.77	1.30	0		0	.
9	312.02	309.25	0.75	1.34	0.77	1.30	0		0	.
9	313.02	310.08	0.78	1.28	0.78	1.28	1	0	0	1.30
9	314.02	312.28	0.78	1.28	0.78	1.28	0		1	.
9	315.02	167.97	0.78	1.29	0.78	1.28	0		0	.
9	316.02	111.78	0.77	1.30	0.77	1.30	1	1	0	1.28
9	317.02	113.08	0.77	1.30	0.77	1.30	0		1	.
9	318.02	115.15	0.78	1.29	0.77	1.30	0		0	.
9	319.02	174.95	0.77	1.29	0.77	1.30	0		0	.
9	320.02	175.88	0.77	1.30	0.77	1.30	0		0	.
9	321.02	117.48	0.78	1.29	0.77	1.30	0		0	.
9	322.02	324.69	0.78	1.28	0.77	1.30	0		0	.
9	323.02	181.35	0.77	1.29	0.77	1.30	0		0	.
9	324.02	183.09	0.77	1.29	0.77	1.30	0		0	.
9	325.02	180.22	0.77	1.30	0.77	1.30	1	0	0	1.30
9	326.02	181.85	0.77	1.30	0.77	1.30	0		1	.
9	327.02	183.72	0.77	1.30	0.77	1.30	0		0	.
9	328.02	185.32	0.77	1.30	0.77	1.30	0		0	.
9	329.02	336.04	0.77	1.30	0.77	1.30	0		0	.
9	330.02	243.44	0.77	1.31	0.77	1.30	0		0	.
9	331.02	131.16	0.76	1.31	0.77	1.30	0		0	.
9	332.02	130.06	0.76	1.32	0.77	1.30	0		0	.
9	333.02	237.50	0.76	1.31	0.77	1.30	0		0	.
9	334.02	133.50	0.75	1.33	0.75	1.33	1	0	0	1.30
9	335.02	135.37	0.74	1.36	0.75	1.33	0		1	.
9	336.02	137.03	0.74	1.35	0.75	1.33	0		0	.
9	337.02	144.04	0.76	1.32	0.75	1.33	0		1	.
9	338.02	145.64	0.75	1.33	0.75	1.33	1	1	0	1.33
9	339.02	216.59	0.77	1.30	0.77	1.30	1	1	0	1.33
9	340.02	182.55	0.78	1.28	0.78	1.28	1	0	0	1.30
9	341.02	258.86	0.79	1.27	0.79	1.27	1	1	0	1.28
9	342.02	259.83	0.79	1.26	0.79	1.27	0		1	.
9	343.02	302.83	0.79	1.27	0.79	1.27	0		0	.
9	344.02	223.39	0.80	1.26	0.80	1.26	1	0	0	1.27
9	345.02	224.82	0.80	1.25	0.80	1.26	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	346.02	1	1	1	0	1	344	0	1.96	1	208.69
9	347.02	0	.	0	0	.	347	0	1.96	2	208.69
9	348.02	0	.	1	0	.	348	0	0.71	0	167.75
9	349.02	1	0	1	0	1	350	0	0.71	2	208.69
9	350.02	1	.	1	0	.	350	0	0.36	1	208.69
9	351.02	1	.	0	0	.	351	0	1.25	1	4.01
9	352.02	0	1	1	0	.	351	0	1.60	0	4.01
9	353.02	1	.	0	0	.	353	0	0.36	0	85.88
9	355.02	0	.	1	0	.	355	0	0.36	1	126.82
9	356.02	0	0	0	0	2	355	0	0.71	0	126.82
9	71.03	0	.	0	0	.	71	0	0.36	1	31.30
9	72.03	1	1	1	0	1	71	0	0.71	1	31.30
9	75.03	0	.	0	0	3	75	0	1.07	1	31.30
9	81.03	0	.	0	0	2	81	0	1.07	1	31.30
9	82.03	0	.	0	0	1	82	0	1.25	1	31.30
9	86.03	1	.	1	0	.	86	0	0.36	1	17.65
9	87.03	0	1	0	0	1	86	0	0.71	1	17.65
9	94.03	1	.	1	0	3	94	0	1.07	1	31.30
9	95.03	1	0	0	0	2	94	0	1.25	1	31.30
9	100.03	0	.	0	0	2	100	0	1.25	1	31.30
9	101.03	1	1	1	1	2	100	0	1.60	1	31.30
9	102.03	0	1	0	0	2	100	0	1.78	1	31.30
9	104.03	0	.	1	0	1	104	0	1.78	1	4.01
9	110.03	1	.	1	0	.	110	0	1.78	0	31.30
9	111.03	0	.	0	0	2	111	0	1.60	1	31.30
9	113.03	0	.	0	0	1	113	0	1.96	0	4.01
9	115.03	1	1	1	0	1	113	0	1.96	1	31.30
9	120.03	1	.	1	1	1	120	0	1.96	1	4.01
9	123.03	0	.	0	0	2	123	0	1.78	1	4.01
9	126.03	1	.	1	0	.	126	0	1.60	0	31.30
9	133.03	1	.	1	0	1	133	0	2.14	1	4.01
9	135.03	1	.	0	0	1	135	0	2.14	2	31.30
9	136.03	1	0	1	0	1	135	0	2.49	1	4.01
9	142.03	1	.	1	0	1	142	0	2.32	0	31.30
9	146.03	0	.	1	0	1	146	0	2.32	0	4.01
9	147.03	0	0	0	0	1	146	0	2.32	1	31.30
9	148.03	0	0	0	0	1	146	0	2.49	1	31.30
9	152.03	1	.	1	0	1	152	0	2.49	0	31.30
9	153.03	1	0	1	0	1	152	0	2.49	1	31.30
9	156.03	1	.	1	0	1	156	0	2.14	1	4.01
9	157.03	1	0	1	1	1	156	0	2.14	1	4.01
9	162.03	0	.	0	1	.	162	0	2.14	0	31.30
9	163.03	0	.	0	0	1	163	0	2.32	1	4.01
9	164.03	0	0	0	0	1	163	0	2.32	1	4.01
9	168.03	0	.	0	1	1	168	0	2.14	2	31.30
9	169.03	0	.	0	0	.	169	0	2.14	1	31.30
9	173.03	1	.	1	0	1	173	0	2.49	1	4.01
9	179.03	0	.	0	0	2	179	0	2.32	1	4.01
9	180.03	0	0	1	0	2	179	0	2.14	1	31.30
9	181.03	0	0	0	0	1	179	0	2.32	2	31.30

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	346.02	226.92	0.80	1.26	0.80	1.26	0		0	.
9	347.02	329.99	0.80	1.25	0.80	1.25	1	1	0	1.26
9	348.02	414.95	0.87	1.15	0.87	1.15	1	2	0	1.25
9	349.02	432.73	1.05	0.95	1.05	0.95	0		1	.
9	350.02	431.40	1.05	0.95	1.05	0.95	1	0	0	1.25
9	351.02	183.21	0.49	2.02	0.49	2.02	1	3	0	1.25
9	352.02	186.32	0.52	1.94	0.49	2.02	0		1	.
9	353.02	631.87	0.84	1.20	0.84	1.20	1	0	0	0.95
9	355.02	859.42	1.36	0.74	1.36	0.74	1	0	0	1.20
9	356.02	861.26	1.38	0.72	1.36	0.74	0		1	.
9	71.03	16.28	1.23	0.82	1.23	0.82	1	0	0	.
9	72.03	14.68	1.22	0.82	1.23	0.82	0		1	.
9	75.03	20.36	1.24	0.81	1.24	0.81	1	0	0	0.82
9	81.03	22.19	1.20	0.84	1.20	0.84	1	1	0	0.81
9	82.03	23.49	1.20	0.83	1.20	0.83	1	1	0	0.84
9	86.03	52.52	1.13	0.88	1.13	0.88	1	0	0	0.83
9	87.03	53.75	1.13	0.89	1.13	0.88	0		1	.
9	94.03	31.80	1.13	0.89	1.13	0.89	1	0	0	0.88
9	95.03	32.87	1.14	0.88	1.13	0.89	0		1	.
9	100.03	34.04	1.07	0.94	1.07	0.94	1	0	0	0.89
9	101.03	35.24	1.09	0.92	1.07	0.94	0		1	.
9	102.03	36.57	1.09	0.92	1.07	0.94	0		0	.
9	104.03	62.99	1.06	0.94	1.06	0.94	1	1	0	0.94
9	110.03	39.31	0.93	1.07	0.93	1.07	1	1	0	1.07
9	111.03	37.44	0.93	1.07	0.93	1.07	1	1	0	0.94
9	113.03	66.46	0.90	1.11	0.90	1.11	1	1	0	1.07
9	115.03	40.41	0.90	1.11	0.90	1.11	0		1	.
9	120.03	68.17	0.77	1.30	0.77	1.30	1	4	0	1.11
9	123.03	69.77	0.69	1.45	0.69	1.45	1	4	0	1.30
9	126.03	41.74	0.60	1.66	0.60	1.66	1	1	0	1.45
9	133.03	72.60	0.56	1.79	0.56	1.79	1	4	0	1.66
9	135.03	43.65	0.53	1.87	0.53	1.87	1	4	0	1.79
9	136.03	74.71	0.53	1.88	0.53	1.87	0		1	.
9	142.03	45.78	0.50	1.98	0.50	1.98	1	4	0	1.87
9	146.03	77.01	0.46	2.16	0.46	2.16	1	4	0	1.98
9	147.03	46.38	0.46	2.16	0.46	2.16	0		1	.
9	148.03	49.48	0.47	2.14	0.46	2.16	0		0	.
9	152.03	53.52	0.45	2.22	0.45	2.22	1	4	0	2.16
9	153.03	57.69	0.45	2.23	0.45	2.22	0		1	.
9	156.03	83.65	0.43	2.35	0.43	2.35	1	4	0	2.22
9	157.03	87.48	0.43	2.34	0.43	2.35	0		1	.
9	162.03	59.03	0.41	2.44	0.41	2.44	1	2	0	2.35
9	163.03	89.89	0.38	2.62	0.38	2.62	1	3	0	2.35
9	164.03	91.79	0.38	2.62	0.38	2.62	0		1	.
9	168.03	60.33	0.37	2.73	0.37	2.73	1	1	0	2.35
9	169.03	64.90	0.37	2.72	0.37	2.72	1	1	0	2.73
9	173.03	96.89	0.34	2.95	0.34	2.95	1	4	0	2.72
9	179.03	100.86	0.27	3.73	0.27	3.73	1	4	0	2.95
9	180.03	66.84	0.28	3.59	0.27	3.73	0		1	.
9	181.03	68.17	0.28	3.61	0.27	3.73	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	184.03	0	.	0	0	1	184	0	2.49	1	4.01
9	185.03	0	0	0	0	1	184	0	2.49	1	17.65
9	187.03	0	0	0	0	1	184	0	3.03	1	4.01
9	188.03	0	.	0	0	1	188	0	2.67	2	31.30
9	189.03	0	.	1	0	1	189	0	3.03	1	31.30
9	190.03	0	.	0	1	1	190	0	2.67	0	44.94
9	191.03	0	0	1	0	1	190	0	2.67	0	44.94
9	192.03	1	1	0	0	2	190	0	2.67	2	44.94
9	193.03	0	1	1	0	1	190	0	2.32	2	4.01
9	198.03	0	.	1	0	1	198	0	2.49	0	4.01
9	201.03	0	.	0	1	2	201	0	2.49	1	31.30
9	205.03	0	.	1	0	1	205	0	2.49	1	4.01
9	209.03	0	.	1	0	1	209	0	2.67	1	4.01
9	211.03	0	.	0	0	2	211	0	2.85	1	31.30
9	213.03	0	.	1	0	2	213	0	2.85	1	4.01
9	214.03	1	1	1	0	1	213	0	2.67	1	4.01
9	215.03	0	1	1	0	1	213	0	2.67	1	31.30
9	216.03	0	.	1	0	1	216	0	2.49	1	31.30
9	217.03	0	0	0	0	1	216	0	2.67	2	31.30
9	218.03	0	0	0	0	1	216	0	2.85	1	4.01
9	219.03	1	1	1	0	2	216	0	2.49	1	4.01
9	220.03	1	0	1	0	1	216	0	2.49	1	4.01
9	221.03	1	0	0	0	1	216	0	2.67	1	31.30
9	222.03	0	.	0	0	1	222	0	2.67	1	31.30
9	223.03	0	0	1	0	1	222	0	2.49	1	31.30
9	224.03	1	1	1	0	1	222	0	2.32	1	44.94
9	225.03	1	0	1	0	1	222	0	2.32	0	44.94
9	226.03	1	0	1	0	1	222	0	2.14	1	85.88
9	227.03	0	1	0	0	1	222	0	2.32	1	85.88
9	228.03	1	1	1	0	1	222	0	2.32	1	85.88
9	229.03	0	1	0	0	1	222	0	2.32	1	99.53
9	230.03	1	1	1	0	2	222	0	2.32	1	72.24
9	231.03	0	1	0	0	1	222	0	2.32	1	44.94
9	232.03	0	0	0	1	1	222	0	2.49	1	72.24
9	233.03	0	.	0	0	1	233	0	2.49	1	31.30
9	234.03	0	0	1	0	1	233	0	1.96	1	31.30
9	235.03	1	.	1	0	2	235	0	1.96	1	72.24
9	236.03	1	0	1	0	2	235	0	1.96	0	72.24
9	237.03	0	1	0	0	1	235	0	2.14	1	44.94
9	238.03	1	1	1	0	1	235	0	2.14	2	44.94
9	239.03	0	1	1	0	1	235	0	2.14	0	44.94
9	240.03	0	.	1	0	2	240	0	2.14	2	44.94
9	241.03	1	1	1	0	1	240	0	2.32	1	85.88
9	242.03	1	0	1	0	2	240	0	2.49	1	85.88
9	243.03	1	0	1	0	1	240	0	2.49	1	113.17
9	244.03	0	.	0	0	2	244	0	2.14	1	44.94
9	247.03	0	.	0	0	2	247	0	1.96	1	113.17
9	248.03	0	0	0	0	1	247	0	2.32	1	167.75
9	249.03	0	0	0	0	1	247	0	2.49	1	99.53
9	250.03	0	0	0	0	1	247	0	2.49	0	44.94

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	184.03	105.17	0.27	3.73	0.27	3.73	1	4	0	3.73
9	185.03	97.63	0.27	3.74	0.27	3.73	0		1	.
9	187.03	112.44	0.27	3.71	0.27	3.73	0		0	.
9	188.03	71.21	0.26	3.80	0.26	3.80	1	3	0	3.73
9	189.03	69.64	0.28	3.52	0.28	3.52	1	2	0	3.73
9	190.03	74.34	0.29	3.43	0.29	3.43	1	1	0	3.73
9	191.03	75.78	0.30	3.34	0.29	3.43	0		1	.
9	192.03	77.78	0.30	3.28	0.29	3.43	0		0	.
9	193.03	120.35	0.32	3.17	0.29	3.43	0		0	.
9	198.03	122.25	0.31	3.18	0.31	3.18	1	4	0	3.43
9	201.03	738.91	0.31	3.23	0.31	3.23	1	4	0	3.18
9	205.03	139.80	0.39	2.59	0.39	2.59	1	4	0	3.23
9	209.03	146.34	0.36	2.80	0.36	2.80	1	4	0	2.59
9	211.03	81.48	0.35	2.84	0.35	2.84	1	4	0	2.80
9	213.03	156.72	0.34	2.91	0.34	2.91	1	4	0	2.84
9	214.03	184.35	0.34	2.91	0.34	2.91	0		1	.
9	215.03	83.32	0.34	2.90	0.34	2.90	0		0	.
9	216.03	85.02	0.34	2.91	0.34	2.91	1	0	0	2.91
9	217.03	86.69	0.35	2.89	0.34	2.91	0		1	.
9	218.03	165.39	0.34	2.93	0.34	2.91	0		0	.
9	219.03	187.25	0.34	2.95	0.34	2.91	0		0	.
9	220.03	190.42	0.34	2.95	0.34	2.91	0		0	.
9	221.03	90.49	0.34	2.96	0.34	2.91	0		0	.
9	222.03	94.80	0.34	2.94	0.34	2.94	1	0	0	2.91
9	223.03	97.23	0.34	2.93	0.34	2.94	0		1	.
9	224.03	102.57	0.34	2.91	0.34	2.94	0		0	.
9	225.03	104.37	0.35	2.85	0.34	2.94	0		0	.
9	226.03	52.68	0.51	1.95	0.34	2.94	0		0	.
9	227.03	54.15	0.59	1.68	0.34	2.94	0		0	.
9	228.03	55.55	0.60	1.66	0.34	2.94	0		0	.
9	229.03	51.38	0.60	1.66	0.34	2.94	0		0	.
9	230.03	84.09	0.61	1.65	0.34	2.94	0		0	.
9	231.03	113.75	0.60	1.66	0.34	2.94	0		0	.
9	232.03	85.96	0.59	1.68	0.34	2.94	0		0	.
9	233.03	114.05	0.59	1.71	0.59	1.71	1	0	0	2.94
9	234.03	112.51	0.58	1.72	0.59	1.71	0		1	.
9	235.03	89.46	0.57	1.74	0.57	1.74	1	0	0	1.71
9	236.03	93.06	0.53	1.89	0.57	1.74	0		1	.
9	237.03	124.73	0.52	1.94	0.57	1.74	0		0	.
9	238.03	126.90	0.53	1.90	0.57	1.74	0		0	.
9	239.03	130.23	0.53	1.88	0.57	1.74	0		0	.
9	240.03	131.67	0.53	1.90	0.53	1.90	1	1	0	1.74
9	241.03	74.44	0.53	1.89	0.53	1.90	0		1	.
9	242.03	73.80	0.53	1.88	0.53	1.90	0		0	.
9	243.03	50.55	0.53	1.88	0.53	1.90	0		0	.
9	244.03	139.41	0.53	1.87	0.53	1.87	1	1	0	1.90
9	247.03	52.52	0.51	1.95	0.51	1.95	1	1	0	1.87
9	248.03	34.23	0.52	1.94	0.51	1.95	0		1	.
9	249.03	91.79	0.52	1.93	0.51	1.95	0		0	.
9	250.03	145.51	0.52	1.92	0.51	1.95	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	251.03	0	0	0	0	2	247	0	2.49	1	58.59
9	252.03	0	0	0	0	1	247	0	2.32	1	58.59
9	253.03	1	1	0	0	1	247	0	2.14	1	31.30
9	254.03	0	1	0	0	1	247	0	2.14	1	44.94
9	255.03	0	.	1	0	2	255	0	2.14	2	44.94
9	256.03	0	0	0	1	1	255	0	2.32	2	99.53
9	257.03	0	0	0	0	1	255	0	2.32	1	99.53
9	258.03	1	1	1	0	1	255	0	2.32	1	31.30
9	259.03	1	0	1	0	1	255	0	2.49	2	58.59
9	260.03	0	1	1	0	1	255	0	2.49	1	58.59
9	261.03	1	0	0	0	1	255	0	2.32	1	99.53
9	262.03	1	0	0	0	1	255	0	2.32	0	99.53
9	263.03	1	1	1	0	1	255	0	2.49	1	17.65
9	264.03	0	0	1	0	1	255	0	2.49	2	181.40
9	265.03	0	1	1	0	1	255	0	2.32	1	181.40
9	266.03	1	.	1	0	1	266	0	2.67	2	113.17
9	267.03	0	1	0	0	1	266	0	2.32	1	113.17
9	268.03	1	1	1	0	1	266	0	2.49	2	113.17
9	269.03	0	.	0	0	.	269	0	2.14	1	58.59
9	270.03	0	0	0	0	2	269	0	1.78	0	58.59
9	271.03	0	.	0	0	2	271	0	1.78	1	126.82
9	272.03	1	1	1	0	1	271	0	1.78	1	126.82
9	273.03	1	0	1	0	1	271	0	1.96	1	44.94
9	274.03	0	1	0	0	2	271	0	2.14	0	44.94
9	275.03	0	.	1	0	.	275	0	2.14	1	126.82
9	276.03	1	1	0	0	1	275	0	2.14	0	99.53
9	277.03	1	.	1	0	2	277	0	1.78	1	72.24
9	278.03	1	.	0	0	.	278	0	1.96	2	72.24
9	279.03	1	.	0	1	1	279	0	1.78	1	140.46
9	280.03	1	0	0	1	1	279	0	1.78	1	140.46
9	281.03	0	.	1	0	.	281	0	1.78	1	85.88
9	282.03	0	.	0	0	3	282	0	1.96	0	140.46
9	283.03	1	1	0	0	2	282	0	1.78	0	181.40
9	284.03	1	0	0	0	1	282	0	2.32	2	181.40
9	285.03	1	0	1	0	1	282	0	2.32	1	181.40
9	286.03	0	1	0	0	1	282	0	2.14	1	140.46
9	287.03	0	0	0	0	1	282	0	2.14	1	140.46
9	288.03	0	.	0	0	2	288	0	2.32	0	140.46
9	289.03	1	1	0	0	1	288	0	2.32	1	126.82
9	290.03	1	.	1	0	2	290	0	2.14	1	140.46
9	291.03	1	0	0	0	1	290	0	2.14	1	140.46
9	292.03	0	.	1	0	2	292	0	2.32	0	181.40
9	293.03	1	1	1	0	1	292	0	2.32	0	99.53
9	294.03	0	.	1	1	1	294	0	2.14	0	140.46
9	295.03	0	0	0	0	1	294	0	2.32	0	140.46
9	296.03	1	1	1	0	1	294	0	2.49	1	167.75
9	297.03	1	0	1	0	1	294	0	2.32	1	167.75
9	298.03	0	1	1	0	1	294	0	2.32	1	140.46
9	299.03	1	1	1	0	1	294	0	2.32	0	140.46
9	300.03	1	0	1	0	2	294	0	2.32	1	140.46

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	251.03	117.59	0.52	1.93	0.51	1.95	0		0	.
9	252.03	119.02	0.52	1.93	0.51	1.95	0		0	.
9	253.03	184.92	0.52	1.93	0.51	1.95	0		0	.
9	254.03	154.82	0.51	1.95	0.51	1.95	0		0	.
9	255.03	152.99	0.51	1.98	0.51	1.98	1	0	0	1.95
9	256.03	109.21	0.51	1.96	0.51	1.98	0		0	.
9	257.03	108.14	0.51	1.97	0.51	1.98	0		1	.
9	258.03	210.88	0.51	1.96	0.51	1.98	0		0	.
9	259.03	138.28	0.52	1.93	0.51	1.98	0		0	.
9	260.03	136.64	0.51	1.96	0.51	1.98	0		0	.
9	261.03	111.11	0.52	1.93	0.51	1.98	0		0	.
9	262.03	112.17	0.51	1.94	0.51	1.98	0		0	.
9	263.03	297.86	0.51	1.96	0.51	1.98	0		0	.
9	264.03	59.99	0.52	1.93	0.51	1.98	0		0	.
9	265.03	58.82	0.52	1.92	0.51	1.98	0		0	.
9	266.03	94.40	0.52	1.94	0.52	1.94	1	0	0	1.98
9	267.03	96.83	0.52	1.93	0.52	1.94	0		1	.
9	268.03	98.27	0.52	1.94	0.52	1.94	0		0	.
9	269.03	151.22	0.50	2.00	0.50	2.00	1	0	0	1.94
9	270.03	153.12	0.52	1.91	0.50	2.00	0		1	.
9	271.03	103.94	0.52	1.91	0.52	1.91	1	0	0	2.00
9	272.03	105.94	0.53	1.89	0.52	1.91	0		1	.
9	273.03	274.88	0.56	1.80	0.52	1.91	0		0	.
9	274.03	276.68	0.55	1.82	0.52	1.91	0		0	.
9	275.03	108.58	0.54	1.84	0.54	1.84	1	0	0	1.91
9	276.03	136.27	0.55	1.81	0.54	1.84	0		1	.
9	277.03	172.71	0.55	1.82	0.55	1.82	1	0	0	1.84
9	278.03	184.76	0.56	1.80	0.56	1.80	1	0	0	1.82
9	279.03	113.85	0.59	1.70	0.59	1.70	1	0	0	1.80
9	280.03	115.72	0.60	1.68	0.59	1.70	0		1	.
9	281.03	150.78	0.59	1.69	0.59	1.69	1	0	0	1.70
9	282.03	120.02	0.59	1.69	0.59	1.69	1	0	0	1.69
9	283.03	67.26	0.60	1.68	0.59	1.69	0		1	.
9	284.03	72.70	0.63	1.60	0.59	1.69	0		0	.
9	285.03	71.50	0.62	1.60	0.59	1.69	0		0	.
9	286.03	130.47	0.64	1.55	0.59	1.69	0		0	.
9	287.03	131.84	0.67	1.50	0.59	1.69	0		0	.
9	288.03	122.93	0.68	1.46	0.68	1.46	1	0	0	1.69
9	289.03	135.04	0.69	1.45	0.68	1.46	0		1	.
9	290.03	136.01	0.70	1.43	0.70	1.43	1	0	0	1.46
9	291.03	137.54	0.71	1.42	0.70	1.43	0		1	.
9	292.03	77.37	0.71	1.40	0.71	1.40	1	0	0	1.43
9	293.03	171.43	0.71	1.40	0.71	1.40	0		1	.
9	294.03	142.08	0.70	1.43	0.70	1.43	1	0	0	1.40
9	295.03	142.85	0.71	1.41	0.70	1.43	0		1	.
9	296.03	81.28	0.71	1.40	0.70	1.43	0		0	.
9	297.03	83.68	0.71	1.40	0.70	1.43	0		0	.
9	298.03	147.75	0.72	1.39	0.70	1.43	0		0	.
9	299.03	149.09	0.71	1.40	0.70	1.43	0		0	.
9	300.03	150.95	0.71	1.40	0.70	1.43	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	301.03	0	1	0	0	2	294	0	1.78	1	181.40
9	302.03	0	0	1	0	1	294	0	2.14	2	181.40
9	303.03	0	0	1	0	1	294	0	2.14	1	167.75
9	304.03	0	0	0	0	2	294	0	1.96	0	167.75
9	305.03	0	.	1	0	2	305	0	1.96	0	181.40
9	306.03	0	0	0	0	1	305	0	1.96	1	181.40
9	307.03	0	0	1	0	2	305	0	1.96	1	181.40
9	308.03	1	1	1	0	1	305	0	1.96	1	113.17
9	309.03	1	0	1	0	1	305	0	1.96	1	140.46
9	310.03	0	1	1	0	1	305	0	2.14	1	181.40
9	311.03	0	0	1	0	1	305	0	2.32	2	181.40
9	312.03	0	0	0	0	2	305	0	2.14	1	72.24
9	313.03	1	.	0	0	.	313	0	1.78	1	72.24
9	314.03	1	0	1	0	2	313	0	1.60	1	72.24
9	315.03	0	1	1	0	1	313	0	1.60	1	140.46
9	316.03	0	.	1	0	.	316	0	1.78	1	181.40
9	317.03	0	0	0	1	1	316	0	1.96	1	181.40
9	318.03	0	0	0	1	1	316	0	1.96	2	181.40
9	319.03	1	1	0	0	1	316	0	2.14	1	154.11
9	320.03	1	0	1	1	1	316	0	2.32	2	154.11
9	321.03	1	0	0	0	1	316	0	2.32	1	181.40
9	322.03	0	1	0	0	1	316	0	2.32	1	72.24
9	323.03	1	1	1	0	1	316	0	2.14	1	113.17
9	324.03	1	0	0	1	1	316	0	2.14	1	113.17
9	325.03	1	.	1	0	3	325	0	1.96	1	154.11
9	326.03	1	0	1	0	1	325	0	1.96	1	154.11
9	327.03	1	0	1	0	1	325	0	1.96	1	154.11
9	328.03	1	0	1	1	1	325	0	2.32	2	154.11
9	329.03	0	1	1	0	1	325	0	2.32	1	72.24
9	330.03	1	1	1	0	1	325	0	2.32	1	85.88
9	331.03	0	.	1	0	.	331	0	2.32	0	181.40
9	332.03	1	1	0	1	1	331	0	2.32	0	181.40
9	333.03	1	0	1	0	2	331	0	2.14	1	99.53
9	334.03	1	.	0	0	2	334	0	1.96	0	181.40
9	335.03	0	1	0	0	1	334	0	1.96	1	181.40
9	336.03	1	1	1	0	1	334	0	2.14	0	181.40
9	337.03	1	.	1	0	1	337	0	2.14	2	167.75
9	338.03	0	1	0	0	2	337	0	1.96	1	167.75
9	339.03	1	.	1	1	1	339	0	2.14	1	140.46
9	340.03	1	.	1	0	.	340	0	2.14	0	181.40
9	341.03	1	.	1	0	.	341	0	1.78	1	140.46
9	342.03	1	0	0	0	1	341	0	1.78	1	140.46
9	343.03	1	0	1	0	2	341	0	1.78	1	99.53
9	344.03	1	.	1	0	.	344	0	1.78	1	181.40
9	345.03	0	1	0	1	1	344	0	1.78	2	181.40
9	346.03	1	1	1	0	1	344	0	1.96	1	181.40
9	347.03	0	.	0	0	.	347	0	1.25	2	181.40
9	348.03	0	.	1	0	.	348	0	0.36	0	140.46
9	349.03	1	0	1	0	1	350	0	0.71	2	181.40
9	350.03	1	.	1	0	.	350	0	0.36	1	181.40

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	301.03	81.91	0.71	1.41	0.70	1.43	0		0	.
9	302.03	84.15	0.70	1.42	0.70	1.43	0		0	.
9	303.03	84.52	0.69	1.45	0.70	1.43	0		0	.
9	304.03	86.38	0.70	1.43	0.70	1.43	0		0	.
9	305.03	86.28	0.70	1.44	0.70	1.44	1	0	0	1.43
9	306.03	87.69	0.69	1.44	0.70	1.44	0		1	.
9	307.03	105.77	0.70	1.43	0.70	1.44	0		0	.
9	308.03	163.23	0.71	1.42	0.70	1.44	0		0	.
9	309.03	162.93	0.71	1.41	0.70	1.44	0		0	.
9	310.03	107.77	0.71	1.40	0.70	1.44	0		0	.
9	311.03	108.84	0.71	1.41	0.70	1.44	0		0	.
9	312.03	309.25	0.72	1.39	0.70	1.44	0		0	.
9	313.03	310.08	0.74	1.35	0.74	1.35	1	0	0	1.44
9	314.03	312.28	0.75	1.33	0.74	1.35	0		1	.
9	315.03	167.97	0.76	1.32	0.74	1.35	0		0	.
9	316.03	111.78	0.77	1.31	0.77	1.31	1	0	0	1.35
9	317.03	113.08	0.77	1.30	0.77	1.31	0		1	.
9	318.03	115.15	0.77	1.30	0.77	1.31	0		0	.
9	319.03	174.95	0.79	1.27	0.77	1.31	0		0	.
9	320.03	175.88	0.79	1.26	0.77	1.31	0		0	.
9	321.03	117.48	0.79	1.27	0.77	1.31	0		0	.
9	322.03	324.69	0.79	1.27	0.77	1.31	0		0	.
9	323.03	181.35	0.80	1.26	0.77	1.31	0		0	.
9	324.03	183.09	0.79	1.26	0.77	1.31	0		0	.
9	325.03	180.22	0.79	1.26	0.79	1.26	1	0	0	1.31
9	326.03	181.85	0.79	1.26	0.79	1.26	0		1	.
9	327.03	183.72	0.79	1.27	0.79	1.26	0		0	.
9	328.03	185.32	0.78	1.29	0.79	1.26	0		0	.
9	329.03	336.04	0.78	1.29	0.79	1.26	0		0	.
9	330.03	243.44	0.78	1.28	0.79	1.26	0		0	.
9	331.03	131.16	0.79	1.26	0.79	1.26	1	1	0	1.26
9	332.03	130.06	0.78	1.28	0.79	1.26	0		1	.
9	333.03	237.50	0.78	1.27	0.79	1.26	0		0	.
9	334.03	133.50	0.78	1.28	0.78	1.28	1	0	0	1.26
9	335.03	135.37	0.79	1.27	0.78	1.28	0		1	.
9	336.03	137.03	0.79	1.27	0.78	1.28	0		0	.
9	337.03	144.04	0.77	1.30	0.77	1.30	1	0	0	1.28
9	338.03	145.64	0.78	1.28	0.77	1.30	0		1	.
9	339.03	216.59	0.75	1.33	0.75	1.33	1	4	0	1.30
9	340.03	182.55	0.74	1.34	0.74	1.34	1	0	0	1.33
9	341.03	258.86	0.73	1.38	0.73	1.38	1	0	0	1.34
9	342.03	259.83	0.73	1.37	0.73	1.38	0		1	.
9	343.03	302.83	0.74	1.35	0.73	1.38	0		0	.
9	344.03	223.39	0.74	1.36	0.74	1.36	1	0	0	1.38
9	345.03	224.82	0.75	1.34	0.74	1.36	0		1	.
9	346.03	226.92	0.75	1.33	0.74	1.36	0		0	.
9	347.03	329.99	0.98	1.03	0.98	1.03	1	0	0	1.36
9	348.03	414.95	1.20	0.83	1.20	0.83	1	0	0	1.03
9	349.03	432.73	1.03	0.97	1.03	0.97	0		1	.
9	350.03	431.40	1.03	0.97	1.03	0.97	1	0	0	0.83

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	353.03	1	.	0	0	.	353	0	0.36	0	58.59
9	355.03	0	.	1	0	.	355	0	0.36	0	99.53
9	356.03	0	0	0	0	2	355	0	0.71	0	99.53
9	71.04	0	.	0	0	.	71	0	0.53	1	4.01
9	72.04	1	.	1	0	2	72	0	0.53	1	4.01
9	75.04	0	.	0	0	2	75	0	1.07	1	4.01
9	81.04	0	0	0	0	2	75	0	1.07	1	4.01
9	82.04	0	.	0	0	3	82	0	1.25	1	4.01
9	94.04	1	.	1	0	.	94	0	0.71	1	4.01
9	95.04	1	0	0	0	2	94	0	0.89	1	4.01
9	100.04	0	1	0	0	2	94	0	1.07	1	4.01
9	101.04	1	1	1	1	2	94	0	1.25	1	4.01
9	102.04	0	1	0	0	2	94	0	1.25	0	4.01
9	110.04	1	.	1	0	.	110	0	1.43	0	4.01
9	111.04	0	.	0	0	2	111	0	1.43	0	4.01
9	115.04	1	.	1	0	2	115	0	1.25	0	4.01
9	126.04	1	.	1	0	.	126	0	1.25	1	4.01
9	135.04	1	.	0	0	1	135	0	1.43	2	4.01
9	142.04	1	.	1	0	2	142	0	1.60	0	4.01
9	147.04	0	.	0	0	2	147	0	1.96	1	4.01
9	148.04	0	.	0	0	1	148	0	1.78	1	4.01
9	152.04	1	.	1	0	1	152	0	1.60	1	4.01
9	153.04	1	.	1	0	.	153	0	1.25	0	4.01
9	162.04	0	.	0	1	.	162	0	1.43	1	4.01
9	168.04	0	0	0	1	2	162	0	1.60	2	4.01
9	169.04	0	.	0	0	.	169	0	1.25	0	4.01
9	180.04	0	.	1	0	2	180	0	1.43	0	4.01
9	181.04	0	0	0	0	1	180	0	1.60	0	4.01
9	188.04	0	.	0	0	1	188	0	1.96	2	4.01
9	189.04	0	.	1	0	2	189	0	1.78	1	4.01
9	190.04	0	.	0	1	.	190	0	1.78	0	17.65
9	191.04	0	0	1	0	1	190	0	1.78	2	17.65
9	192.04	1	.	0	0	2	192	0	1.96	2	17.65
9	201.04	0	.	0	1	2	201	0	1.96	1	4.01
9	211.04	0	.	0	0	2	211	0	1.96	1	4.01
9	215.04	0	.	1	0	1	215	0	1.96	1	4.01
9	216.04	0	0	1	0	1	215	0	1.78	0	4.01
9	217.04	0	0	0	0	1	215	0	1.96	0	4.01
9	221.04	1	.	0	0	1	221	0	1.96	1	4.01
9	222.04	0	.	0	0	.	222	0	1.78	0	4.01
9	223.04	0	0	1	0	1	222	0	1.60	1	4.01
9	224.04	1	.	1	0	.	224	0	1.25	1	17.65
9	225.04	1	0	1	0	1	224	0	1.43	1	17.65
9	226.04	1	0	1	0	1	224	0	1.43	1	58.59
9	227.04	0	1	0	0	1	224	0	1.78	1	58.59
9	228.04	1	1	1	0	1	224	0	1.78	1	58.59
9	229.04	0	1	0	0	2	224	0	1.78	1	72.24
9	230.04	1	1	1	0	1	224	0	1.78	0	44.94
9	231.04	0	1	0	0	1	224	0	1.96	1	17.65
9	232.04	0	0	0	1	1	224	0	2.32	1	44.94

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	353.03	631.87	0.86	1.17	0.86	1.17	1	0	0	0.97
9	355.03	859.42	1.39	0.72	1.39	0.72	1	0	0	1.17
9	356.03	861.26	1.37	0.73	1.39	0.72	0		1	.
9	71.04	16.28	1.20	0.83	1.20	0.83	1	0	0	.
9	72.04	14.68	1.24	0.81	1.24	0.81	1	1	0	0.83
9	75.04	20.36	1.23	0.82	1.23	0.82	1	0	0	0.81
9	81.04	22.19	1.22	0.82	1.23	0.82	0		1	.
9	82.04	23.49	1.29	0.78	1.29	0.78	1	0	0	0.82
9	94.04	31.80	1.08	0.93	1.08	0.93	1	0	0	0.78
9	95.04	32.87	1.08	0.93	1.08	0.93	0		1	.
9	100.04	34.04	1.08	0.92	1.08	0.93	0		0	.
9	101.04	35.24	1.08	0.92	1.08	0.93	0		0	.
9	102.04	36.57	1.10	0.91	1.08	0.93	0		0	.
9	110.04	39.31	1.04	0.96	1.04	0.96	1	0	0	0.96
9	111.04	37.44	1.04	0.96	1.04	0.96	1	0	0	0.93
9	115.04	40.41	1.01	0.99	1.01	0.99	1	4	0	0.96
9	126.04	41.74	0.92	1.09	0.92	1.09	1	0	0	0.99
9	135.04	43.65	0.90	1.11	0.90	1.11	1	4	0	1.09
9	142.04	45.78	0.88	1.14	0.88	1.14	1	4	0	1.11
9	147.04	46.38	0.84	1.19	0.84	1.19	1	4	0	1.14
9	148.04	49.48	0.85	1.18	0.85	1.18	1	1	0	1.19
9	152.04	53.52	0.87	1.15	0.87	1.15	1	1	0	1.18
9	153.04	57.69	0.93	1.08	0.93	1.08	1	1	0	1.15
9	162.04	59.03	0.75	1.33	0.75	1.33	1	0	0	1.08
9	168.04	60.33	0.74	1.34	0.75	1.33	0		1	.
9	169.04	64.90	0.79	1.26	0.79	1.26	1	0	0	1.33
9	180.04	66.84	0.64	1.57	0.64	1.57	1	1	0	1.26
9	181.04	68.17	0.64	1.56	0.64	1.57	0		1	.
9	188.04	71.21	0.56	1.77	0.56	1.77	1	2	0	1.57
9	189.04	69.64	0.50	2.00	0.50	2.00	1	3	0	1.57
9	190.04	74.34	0.50	2.00	0.50	2.00	1	1	0	1.57
9	191.04	75.78	0.48	2.09	0.50	2.00	0		1	.
9	192.04	77.78	0.47	2.15	0.47	2.15	1	1	0	2.00
9	201.04	738.91	0.37	2.68	0.37	2.68	1	4	0	2.15
9	211.04	81.48	0.28	3.61	0.28	3.61	1	4	0	2.68
9	215.04	83.32	0.27	3.73	0.27	3.73	1	4	0	3.61
9	216.04	85.02	0.27	3.68	0.27	3.73	0		1	.
9	217.04	86.69	0.28	3.62	0.27	3.73	0		0	.
9	221.04	90.49	0.26	3.78	0.26	3.78	1	4	0	3.73
9	222.04	94.80	0.27	3.71	0.27	3.71	1	1	0	3.78
9	223.04	97.23	0.27	3.73	0.27	3.71	0		1	.
9	224.04	102.57	0.28	3.54	0.28	3.54	1	1	0	3.71
9	225.04	104.37	0.28	3.58	0.28	3.54	0		1	.
9	226.04	52.68	0.22	4.49	0.28	3.54	0		0	.
9	227.04	54.15	0.21	4.76	0.28	3.54	0		0	.
9	228.04	55.55	0.21	4.77	0.28	3.54	0		0	.
9	229.04	51.38	0.21	4.79	0.28	3.54	0		0	.
9	230.04	84.09	0.21	4.81	0.28	3.54	0		0	.
9	231.04	113.75	0.21	4.86	0.28	3.54	0		0	.
9	232.04	85.96	0.21	4.87	0.28	3.54	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	233.04	0	.	0	0	1	233	0	2.49	1	4.01
9	234.04	0	0	1	0	1	233	0	1.78	0	4.01
9	235.04	1	.	1	0	.	235	0	1.78	1	44.94
9	236.04	1	.	1	0	2	236	0	1.60	0	44.94
9	237.04	0	.	0	0	1	237	0	1.60	1	17.65
9	238.04	1	.	1	0	1	238	0	1.43	0	17.65
9	239.04	0	.	1	0	.	239	0	1.43	0	17.65
9	240.04	0	.	1	0	2	240	0	1.43	2	17.65
9	241.04	1	.	1	0	.	241	0	1.43	1	58.59
9	242.04	1	0	1	0	2	241	0	1.43	0	58.59
9	243.04	1	0	1	0	2	241	0	1.43	1	85.88
9	244.04	0	.	0	0	2	244	0	1.60	1	17.65
9	247.04	0	0	0	0	2	244	0	1.78	1	85.88
9	248.04	0	0	0	0	1	244	0	1.78	1	140.46
9	249.04	0	0	0	0	1	244	0	1.96	1	72.24
9	250.04	0	0	0	0	2	244	0	1.96	0	17.65
9	251.04	0	0	0	0	2	244	0	2.14	1	31.30
9	252.04	0	0	0	0	1	244	0	1.96	1	31.30
9	253.04	1	1	0	0	1	244	0	2.49	1	4.01
9	254.04	0	1	0	0	1	244	0	1.78	0	17.65
9	255.04	0	0	1	0	2	244	0	1.78	0	17.65
9	256.04	0	0	0	1	1	244	0	2.14	2	72.24
9	257.04	0	0	0	0	1	244	0	2.14	1	72.24
9	258.04	1	1	1	0	1	244	0	2.85	1	4.01
9	259.04	1	.	1	0	1	259	0	2.49	0	31.30
9	260.04	0	.	1	0	1	260	0	2.49	0	31.30
9	261.04	1	.	0	0	1	261	0	2.32	1	72.24
9	262.04	1	0	0	0	1	261	0	2.14	0	72.24
9	264.04	0	0	1	0	1	261	0	2.32	2	154.11
9	265.04	0	1	1	0	1	261	0	2.14	1	154.11
9	266.04	1	1	1	0	1	261	0	2.49	2	85.88
9	267.04	0	1	0	0	1	261	0	2.14	1	85.88
9	268.04	1	1	1	0	1	261	0	2.32	2	85.88
9	269.04	0	1	0	0	1	261	0	2.14	1	31.30
9	270.04	0	0	0	0	2	261	0	1.96	0	31.30
9	271.04	0	.	0	0	2	271	0	2.14	1	99.53
9	272.04	1	1	1	0	1	271	0	2.14	1	99.53
9	273.04	1	0	1	0	1	271	0	1.96	1	17.65
9	274.04	0	1	0	0	2	271	0	1.96	1	17.65
9	275.04	0	.	1	0	.	275	0	1.60	1	99.53
9	276.04	1	.	0	0	1	276	0	1.60	1	72.24
9	277.04	1	.	1	0	2	277	0	1.43	1	44.94
9	278.04	1	0	0	0	2	277	0	1.43	2	44.94
9	279.04	1	0	0	1	1	277	0	1.43	1	113.17
9	280.04	1	0	0	1	1	277	0	1.60	1	113.17
9	281.04	0	.	1	0	3	281	0	1.43	1	58.59
9	282.04	0	.	0	0	2	282	0	1.96	0	113.17
9	283.04	1	1	0	0	2	282	0	1.78	1	154.11
9	284.04	1	0	0	0	1	282	0	1.96	2	154.11
9	285.04	1	0	1	0	1	282	0	1.60	1	154.11

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	233.04	114.05	0.20	4.90	0.20	4.90	1	1	0	3.54
9	234.04	112.51	0.20	4.91	0.20	4.90	0		1	.
9	235.04	89.46	0.20	4.93	0.20	4.93	1	1	0	4.90
9	236.04	93.06	0.20	4.96	0.20	4.96	1	1	0	4.93
9	237.04	124.73	0.20	4.96	0.20	4.96	1	1	0	4.96
9	238.04	126.90	0.20	4.94	0.20	4.94	1	1	0	4.96
9	239.04	130.23	0.20	4.90	0.20	4.90	1	1	0	4.94
9	240.04	131.67	0.20	4.92	0.20	4.92	1	0	0	4.90
9	241.04	74.44	0.21	4.87	0.21	4.87	1	1	0	4.92
9	242.04	73.80	0.21	4.84	0.21	4.87	0		1	.
9	243.04	50.55	0.21	4.84	0.21	4.87	0		0	.
9	244.04	139.41	0.21	4.85	0.21	4.85	1	0	0	4.87
9	247.04	52.52	0.21	4.86	0.21	4.85	0		1	.
9	248.04	34.23	0.21	4.86	0.21	4.85	0		0	.
9	249.04	91.79	0.21	4.84	0.21	4.85	0		0	.
9	250.04	145.51	0.21	4.83	0.21	4.85	0		0	.
9	251.04	117.59	0.34	2.93	0.21	4.85	0		0	.
9	252.04	119.02	0.34	2.96	0.21	4.85	0		0	.
9	253.04	184.92	0.34	2.95	0.21	4.85	0		0	.
9	254.04	154.82	0.34	2.97	0.21	4.85	0		0	.
9	255.04	152.99	0.34	2.96	0.21	4.85	0		0	.
9	256.04	109.21	0.34	2.96	0.21	4.85	0		0	.
9	257.04	108.14	0.34	2.98	0.21	4.85	0		0	.
9	258.04	210.88	0.34	2.98	0.21	4.85	0		0	.
9	259.04	138.28	0.34	2.97	0.34	2.97	1	2	0	4.85
9	260.04	136.64	0.33	3.02	0.33	3.02	1	3	0	4.85
9	261.04	111.11	0.32	3.09	0.32	3.09	1	4	0	4.85
9	262.04	112.17	0.33	3.07	0.32	3.09	0		1	.
9	264.04	59.99	0.61	1.65	0.32	3.09	0		0	.
9	265.04	58.82	0.33	3.05	0.32	3.09	0		0	.
9	266.04	94.40	0.62	1.62	0.32	3.09	0		0	.
9	267.04	96.83	0.61	1.64	0.32	3.09	0		0	.
9	268.04	98.27	0.61	1.64	0.32	3.09	0		0	.
9	269.04	151.22	0.60	1.66	0.32	3.09	0		0	.
9	270.04	153.12	0.58	1.73	0.32	3.09	0		0	.
9	271.04	103.94	0.57	1.75	0.57	1.75	1	1	0	3.09
9	272.04	105.94	0.56	1.77	0.57	1.75	0		1	.
9	273.04	274.88	0.53	1.88	0.57	1.75	0		0	.
9	274.04	276.68	0.54	1.87	0.57	1.75	0		0	.
9	275.04	108.58	0.53	1.90	0.53	1.90	1	0	0	1.75
9	276.04	136.27	0.52	1.93	0.52	1.93	1	1	0	1.90
9	277.04	172.71	0.52	1.91	0.52	1.91	1	1	0	1.93
9	278.04	184.76	0.51	1.96	0.52	1.91	0		1	.
9	279.04	113.85	0.48	2.08	0.52	1.91	0		0	.
9	280.04	115.72	0.48	2.11	0.52	1.91	0		0	.
9	281.04	150.78	0.48	2.09	0.48	2.09	1	0	0	1.91
9	282.04	120.02	0.48	2.10	0.48	2.10	1	0	0	2.09
9	283.04	67.26	0.47	2.11	0.48	2.10	0		1	.
9	284.04	72.70	0.46	2.19	0.48	2.10	0		0	.
9	285.04	71.50	0.45	2.20	0.48	2.10	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	286.04	0	.	0	0	.	286	0	1.60	1	113.17
9	287.04	0	0	0	0	1	286	0	1.96	1	113.17
9	288.04	0	0	0	0	2	286	0	1.60	1	113.17
9	289.04	1	1	0	0	2	286	0	1.60	1	99.53
9	290.04	1	0	1	0	2	286	0	1.78	1	113.17
9	291.04	1	0	0	0	1	286	0	1.96	1	113.17
9	292.04	0	.	1	0	2	292	0	1.96	0	154.11
9	293.04	1	1	1	0	1	292	0	2.14	0	72.24
9	294.04	0	1	1	1	1	292	0	2.32	2	113.17
9	295.04	0	0	0	0	1	292	0	2.32	1	113.17
9	296.04	1	1	1	0	1	292	0	2.14	1	140.46
9	297.04	1	0	1	0	1	292	0	2.32	1	140.46
9	298.04	0	1	1	0	1	292	0	2.14	1	113.17
9	299.04	1	1	1	0	1	292	0	1.96	0	113.17
9	300.04	1	0	1	0	2	292	0	1.96	1	113.17
9	301.04	0	1	0	0	2	292	0	1.96	1	154.11
9	302.04	0	0	1	0	1	292	0	1.78	0	154.11
9	303.04	0	0	1	0	1	292	0	1.78	1	140.46
9	304.04	0	0	0	0	2	292	0	1.78	1	140.46
9	305.04	0	0	1	0	2	292	0	1.78	1	154.11
9	306.04	0	0	0	0	1	292	0	1.78	1	154.11
9	307.04	0	0	1	0	2	292	0	1.78	1	154.11
9	308.04	1	1	1	0	1	292	0	1.78	1	85.88
9	309.04	1	0	1	0	1	292	0	1.96	1	113.17
9	310.04	0	1	1	0	2	292	0	1.78	1	154.11
9	311.04	0	0	1	0	1	292	0	1.78	2	154.11
9	312.04	0	0	0	0	1	292	0	1.78	1	44.94
9	313.04	1	.	0	0	.	313	0	1.78	1	44.94
9	314.04	1	0	1	0	2	313	0	1.78	1	44.94
9	315.04	0	1	1	0	1	313	0	1.96	1	113.17
9	316.04	0	.	1	0	.	316	0	1.96	1	154.11
9	317.04	0	0	0	1	1	316	0	1.96	1	154.11
9	318.04	0	0	0	1	1	316	0	2.14	2	154.11
9	319.04	1	1	0	0	1	316	0	2.32	1	126.82
9	320.04	1	0	1	1	1	316	0	2.49	2	126.82
9	321.04	1	0	0	0	1	316	0	1.96	1	154.11
9	322.04	0	.	0	0	1	322	0	1.96	1	44.94
9	323.04	1	1	1	0	1	322	0	1.78	1	85.88
9	324.04	1	0	0	1	1	322	0	1.78	1	85.88
9	325.04	1	.	1	0	3	325	0	1.78	1	126.82
9	326.04	1	0	1	0	1	325	0	1.96	1	126.82
9	327.04	1	0	1	0	1	325	0	1.96	1	126.82
9	328.04	1	0	1	1	1	325	0	2.14	2	126.82
9	329.04	0	1	1	0	1	325	0	2.14	1	44.94
9	330.04	1	1	1	0	1	325	0	2.32	1	58.59
9	331.04	0	.	1	0	.	331	0	1.96	2	154.11
9	332.04	1	.	0	1	1	332	0	1.78	1	154.11
9	333.04	1	0	1	0	1	332	0	1.78	1	72.24
9	334.04	1	0	0	0	2	332	0	1.96	0	154.11
9	335.04	0	1	0	0	1	332	0	1.96	1	154.11

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	286.04	130.47	0.45	2.20	0.45	2.20	1	1	0	2.10
9	287.04	131.84	0.45	2.22	0.45	2.20	0		1	.
9	288.04	122.93	0.48	2.09	0.45	2.20	0		0	.
9	289.04	135.04	0.47	2.12	0.45	2.20	0		0	.
9	290.04	136.01	0.47	2.14	0.45	2.20	0		0	.
9	291.04	137.54	0.47	2.14	0.45	2.20	0		0	.
9	292.04	77.37	0.47	2.12	0.47	2.12	1	1	0	2.20
9	293.04	171.43	0.47	2.12	0.47	2.12	0		1	.
9	294.04	142.08	0.46	2.15	0.47	2.12	0		0	.
9	295.04	142.85	0.46	2.16	0.47	2.12	0		0	.
9	296.04	81.28	0.46	2.17	0.47	2.12	0		0	.
9	297.04	83.68	0.46	2.16	0.47	2.12	0		0	.
9	298.04	147.75	0.46	2.16	0.47	2.12	0		0	.
9	299.04	149.09	0.47	2.14	0.47	2.12	0		0	.
9	300.04	150.95	0.47	2.13	0.47	2.12	0		0	.
9	301.04	81.91	0.47	2.14	0.47	2.12	0		0	.
9	302.04	84.15	0.47	2.11	0.47	2.12	0		0	.
9	303.04	84.52	0.48	2.10	0.47	2.12	0		0	.
9	304.04	86.38	0.48	2.09	0.47	2.12	0		0	.
9	305.04	86.28	0.48	2.10	0.47	2.12	0		0	.
9	306.04	87.69	0.47	2.11	0.47	2.12	0		0	.
9	307.04	105.77	0.48	2.09	0.47	2.12	0		0	.
9	308.04	163.23	0.48	2.06	0.47	2.12	0		0	.
9	309.04	162.93	0.49	2.04	0.47	2.12	0		0	.
9	310.04	107.77	0.49	2.03	0.47	2.12	0		0	.
9	311.04	108.84	0.50	2.01	0.47	2.12	0		0	.
9	312.04	309.25	0.49	2.02	0.47	2.12	0		0	.
9	313.04	310.08	0.57	1.75	0.57	1.75	1	0	0	2.12
9	314.04	312.28	0.57	1.75	0.57	1.75	0		1	.
9	315.04	167.97	0.57	1.74	0.57	1.75	0		0	.
9	316.04	111.78	0.58	1.73	0.58	1.73	1	0	0	1.75
9	317.04	113.08	0.58	1.72	0.58	1.73	0		1	.
9	318.04	115.15	0.58	1.73	0.58	1.73	0		0	.
9	319.04	174.95	0.57	1.75	0.58	1.73	0		0	.
9	320.04	175.88	0.57	1.75	0.58	1.73	0		0	.
9	321.04	117.48	0.57	1.76	0.58	1.73	0		0	.
9	322.04	324.69	0.57	1.75	0.57	1.75	1	1	0	1.73
9	323.04	181.35	0.58	1.73	0.57	1.75	0		1	.
9	324.04	183.09	0.58	1.72	0.57	1.75	0		0	.
9	325.04	180.22	0.59	1.70	0.59	1.70	1	0	0	1.75
9	326.04	181.85	0.59	1.71	0.59	1.70	0		1	.
9	327.04	183.72	0.59	1.70	0.59	1.70	0		0	.
9	328.04	185.32	0.60	1.67	0.59	1.70	0		0	.
9	329.04	336.04	0.60	1.66	0.59	1.70	0		0	.
9	330.04	243.44	0.61	1.64	0.59	1.70	0		0	.
9	331.04	131.16	0.62	1.62	0.62	1.62	1	0	0	1.70
9	332.04	130.06	0.61	1.64	0.61	1.64	1	1	0	1.62
9	333.04	237.50	0.62	1.62	0.61	1.64	0		1	.
9	334.04	133.50	0.69	1.46	0.61	1.64	0		0	.
9	335.04	135.37	0.70	1.43	0.61	1.64	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	336.04	1	1	1	0	1	332	0	1.96	2	154.11
9	337.04	1	0	1	0	1	332	0	2.14	2	140.46
9	338.04	0	1	0	0	2	332	0	1.78	1	140.46
9	339.04	1	1	1	1	1	332	0	1.96	1	113.17
9	340.04	1	.	1	0	.	340	0	1.78	0	154.11
9	341.04	1	0	1	0	1	340	0	1.60	1	113.17
9	342.04	1	0	0	0	1	340	0	1.43	1	113.17
9	343.04	1	0	1	0	2	340	0	1.43	1	72.24
9	344.04	1	.	1	0	.	344	0	1.60	1	154.11
9	345.04	0	1	0	1	1	344	0	1.07	2	154.11
9	346.04	1	1	1	0	1	344	0	1.07	1	154.11
9	347.04	0	.	0	0	.	347	0	0.53	2	154.11
9	348.04	0	.	1	0	.	348	0	0.36	0	113.17
9	349.04	1	0	1	0	1	350	0	0.53	2	154.11
9	350.04	1	.	1	0	.	350	0	0.36	1	154.11
9	353.04	1	.	0	0	.	353	0	0.53	0	31.30
9	355.04	0	.	1	0	.	355	0	0.36	0	72.24
9	356.04	0	.	0	0	2	356	0	0.71	0	72.24
9	226.05	1	.	1	0	.	226	0	0.71	1	31.30
9	227.05	0	1	0	0	2	226	0	1.07	0	31.30
9	228.05	1	1	1	0	1	226	0	1.25	1	31.30
9	229.05	0	1	0	0	2	226	0	1.43	1	44.94
9	230.05	1	1	1	0	1	226	0	1.43	1	17.65
9	232.05	0	.	0	1	2	232	0	1.60	0	17.65
9	235.05	1	.	1	0	.	235	0	1.43	1	17.65
9	236.05	1	.	1	0	.	236	0	1.07	2	17.65
9	241.05	1	.	1	0	.	241	0	0.71	1	31.30
9	242.05	1	.	1	0	.	242	0	0.89	1	31.30
9	243.05	1	0	1	0	2	242	0	0.89	1	58.59
9	247.05	0	.	0	0	2	247	0	1.43	1	58.59
9	248.05	0	.	0	0	2	248	0	1.60	1	113.17
9	249.05	0	.	0	0	1	249	0	1.78	1	44.94
9	251.05	0	.	0	0	2	251	0	1.43	1	4.01
9	252.05	0	0	0	0	1	251	0	1.25	1	4.01
9	256.05	0	0	0	1	1	257	0	1.43	1	44.94
9	257.05	0	.	0	0	.	257	0	1.25	1	44.94
9	259.05	1	.	1	0	.	259	0	1.60	1	4.01
9	260.05	0	.	1	0	1	260	0	1.78	2	4.01
9	261.05	1	.	0	0	.	261	0	1.60	1	44.94
9	262.05	1	0	0	0	1	261	0	1.43	1	44.94
9	264.05	0	0	1	0	1	261	0	1.78	2	126.82
9	265.05	0	1	1	0	1	261	0	1.43	1	126.82
9	266.05	1	1	1	0	1	261	0	1.78	2	58.59
9	267.05	0	1	0	0	1	261	0	1.96	1	58.59
9	268.05	1	1	1	0	2	261	0	1.78	0	58.59
9	269.05	0	1	0	0	2	261	0	1.60	1	4.01
9	270.05	0	0	0	0	1	261	0	1.78	0	4.01
9	271.05	0	.	0	0	.	271	0	1.96	1	72.24
9	272.05	1	1	1	0	1	271	0	2.32	1	72.24
9	275.05	0	.	1	0	.	275	0	1.60	1	72.24

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	336.04	137.03	0.71	1.41	0.61	1.64	0		0	.
9	337.04	144.04	0.71	1.41	0.61	1.64	0		0	.
9	338.04	145.64	0.71	1.41	0.61	1.64	0		0	.
9	339.04	216.59	0.71	1.41	0.61	1.64	0		0	.
9	340.04	182.55	0.72	1.39	0.72	1.39	1	0	0	1.64
9	341.04	258.86	0.72	1.38	0.72	1.39	0		1	.
9	342.04	259.83	0.73	1.37	0.72	1.39	0		0	.
9	343.04	302.83	0.73	1.37	0.72	1.39	0		0	.
9	344.04	223.39	0.72	1.39	0.72	1.39	1	0	0	1.39
9	345.04	224.82	0.71	1.41	0.72	1.39	0		1	.
9	346.04	226.92	0.71	1.41	0.72	1.39	0		0	.
9	347.04	329.99	1.07	0.93	1.07	0.93	1	0	0	1.39
9	348.04	414.95	1.26	0.79	1.26	0.79	1	0	0	0.93
9	349.04	432.73	1.08	0.93	1.08	0.93	0		1	.
9	350.04	431.40	1.08	0.93	1.08	0.93	1	0	0	0.79
9	353.04	631.87	0.91	1.10	0.91	1.10	1	0	0	0.93
9	355.04	859.42	1.38	0.73	1.38	0.73	1	0	0	1.10
9	356.04	861.26	1.36	0.73	1.36	0.73	1	0	0	0.73
9	226.05	52.68	0.95	1.05	0.95	1.05	1	1	0	.
9	227.05	54.15	0.95	1.05	0.95	1.05	0		1	.
9	228.05	55.55	0.94	1.06	0.95	1.05	0		0	.
9	229.05	51.38	0.95	1.05	0.95	1.05	0		0	.
9	230.05	84.09	0.95	1.05	0.95	1.05	0		0	.
9	232.05	85.96	0.92	1.09	0.92	1.09	1	4	0	1.05
9	235.05	89.46	0.87	1.15	0.87	1.15	1	0	0	1.09
9	236.05	93.06	0.91	1.10	0.91	1.10	1	0	0	1.15
9	241.05	74.44	0.83	1.20	0.83	1.20	1	0	0	1.10
9	242.05	73.80	0.84	1.19	0.84	1.19	1	1	0	1.20
9	243.05	50.55	0.84	1.19	0.84	1.19	0		1	.
9	247.05	52.52	0.77	1.29	0.77	1.29	1	4	0	1.19
9	248.05	34.23	0.77	1.30	0.77	1.30	1	1	0	1.29
9	249.05	91.79	0.75	1.33	0.75	1.33	1	1	0	1.30
9	251.05	117.59	0.30	3.32	0.30	3.32	1	1	0	1.33
9	252.05	119.02	0.30	3.31	0.30	3.32	0		1	.
9	256.05	109.21	0.33	3.05	0.33	3.06	0		1	.
9	257.05	108.14	0.33	3.06	0.33	3.06	1	1	0	3.32
9	259.05	138.28	0.33	3.02	0.33	3.02	1	3	0	3.06
9	260.05	136.64	0.34	2.95	0.34	2.95	1	2	0	3.06
9	261.05	111.11	0.34	2.95	0.34	2.95	1	1	0	3.06
9	262.05	112.17	0.34	2.97	0.34	2.95	0		1	.
9	264.05	59.99	0.23	4.38	0.34	2.95	0		0	.
9	265.05	58.82	0.33	3.00	0.34	2.95	0		0	.
9	266.05	94.40	0.23	4.42	0.34	2.95	0		0	.
9	267.05	96.83	0.23	4.41	0.34	2.95	0		0	.
9	268.05	98.27	0.23	4.38	0.34	2.95	0		0	.
9	269.05	151.22	0.23	4.39	0.34	2.95	0		0	.
9	270.05	153.12	0.23	4.39	0.34	2.95	0		0	.
9	271.05	103.94	0.23	4.38	0.23	4.38	1	0	0	2.95
9	272.05	105.94	0.23	4.37	0.23	4.38	0		1	.
9	275.05	108.58	0.22	4.48	0.22	4.48	1	0	0	4.38

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	276.05	1	.	0	0	.	276	0	1.25	0	44.94
9	277.05	1	.	1	0	.	277	0	0.89	1	17.65
9	278.05	1	.	0	0	2	278	0	1.07	2	17.65
9	279.05	1	.	0	1	.	279	0	0.71	1	85.88
9	280.05	1	0	0	1	2	279	0	0.89	1	85.88
9	281.05	0	.	1	0	1	281	0	1.25	1	31.30
9	282.05	0	.	0	0	2	282	0	1.43	0	85.88
9	283.05	1	.	0	0	2	283	0	1.25	1	126.82
9	284.05	1	.	0	0	1	284	0	1.60	2	126.82
9	285.05	1	.	1	0	1	285	0	1.43	1	126.82
9	286.05	0	.	0	0	.	286	0	1.78	1	85.88
9	287.05	0	0	0	0	1	286	0	1.78	1	85.88
9	288.05	0	0	0	0	2	286	0	1.60	1	85.88
9	289.05	1	1	0	0	2	286	0	1.96	1	72.24
9	290.05	1	0	1	0	2	286	0	1.60	1	85.88
9	291.05	1	0	0	0	1	286	0	1.78	1	85.88
9	292.05	0	.	1	0	2	292	0	1.96	1	126.82
9	293.05	1	1	1	0	1	292	0	2.14	0	44.94
9	294.05	0	.	1	1	2	294	0	1.60	2	85.88
9	295.05	0	0	0	0	1	294	0	1.96	1	85.88
9	296.05	1	1	1	0	1	294	0	1.96	1	113.17
9	297.05	1	0	1	0	1	294	0	2.14	1	113.17
9	298.05	0	1	1	0	2	294	0	2.14	1	85.88
9	299.05	1	1	1	0	1	294	0	2.14	0	85.88
9	300.05	1	.	1	0	2	300	0	1.78	1	85.88
9	301.05	0	1	0	0	1	300	0	2.14	1	126.82
9	302.05	0	0	1	0	1	300	0	1.96	0	126.82
9	303.05	0	0	1	0	2	300	0	1.96	1	113.17
9	304.05	0	0	0	0	2	300	0	1.96	0	113.17
9	305.05	0	0	1	0	2	300	0	1.96	1	126.82
9	306.05	0	0	0	0	1	300	0	1.96	1	126.82
9	307.05	0	0	1	0	1	300	0	2.14	0	126.82
9	308.05	1	1	1	0	1	300	0	1.78	1	58.59
9	309.05	1	0	1	0	1	300	0	1.78	1	85.88
9	310.05	0	1	1	0	2	300	0	1.78	0	126.82
9	311.05	0	0	1	0	1	300	0	1.78	2	126.82
9	312.05	0	.	0	0	1	312	0	1.60	1	17.65
9	313.05	1	1	0	0	1	312	0	1.96	1	17.65
9	314.05	1	0	1	0	2	312	0	1.78	1	17.65
9	315.05	0	1	1	0	1	312	0	1.78	1	85.88
9	316.05	0	.	1	0	2	316	0	1.96	1	126.82
9	317.05	0	0	0	1	1	316	0	1.96	1	126.82
9	318.05	0	0	0	1	1	316	0	1.96	2	126.82
9	319.05	1	1	0	0	1	316	0	2.14	1	99.53
9	320.05	1	0	1	1	1	316	0	2.14	2	99.53
9	321.05	1	0	0	0	1	316	0	2.32	1	126.82
9	322.05	0	.	0	0	2	322	0	2.49	1	17.65
9	323.05	1	1	1	0	1	322	0	2.14	1	58.59
9	324.05	1	0	0	1	1	322	0	1.96	1	58.59
9	325.05	1	.	1	0	.	325	0	1.60	1	99.53

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	276.05	136.27	0.23	4.40	0.23	4.40	1	0	0	4.48
9	277.05	172.71	0.24	4.10	0.24	4.10	1	0	0	4.40
9	278.05	184.76	0.27	3.65	0.27	3.65	1	2	0	4.10
9	279.05	113.85	0.25	3.93	0.25	3.93	1	3	0	4.10
9	280.05	115.72	0.25	3.92	0.25	3.93	0		1	.
9	281.05	150.78	0.26	3.87	0.26	3.87	1	0	0	4.10
9	282.05	120.02	0.26	3.79	0.26	3.79	1	2	0	3.87
9	283.05	67.26	0.25	3.96	0.25	3.96	1	3	0	3.87
9	284.05	72.70	0.26	3.85	0.26	3.85	1	3	0	3.87
9	285.05	71.50	0.26	3.81	0.26	3.81	1	2	0	3.87
9	286.05	130.47	0.27	3.65	0.27	3.65	1	0	0	3.87
9	287.05	131.84	0.28	3.58	0.27	3.65	0		1	.
9	288.05	122.93	0.33	3.06	0.27	3.65	0		0	.
9	289.05	135.04	0.33	3.00	0.27	3.65	0		0	.
9	290.05	136.01	0.34	2.98	0.27	3.65	0		0	.
9	291.05	137.54	0.33	2.99	0.27	3.65	0		0	.
9	292.05	77.37	0.33	3.01	0.33	3.01	1	0	0	3.65
9	293.05	171.43	0.33	3.00	0.33	3.01	0		1	.
9	294.05	142.08	0.33	3.00	0.33	3.00	1	1	0	3.01
9	295.05	142.85	0.34	2.98	0.33	3.00	0		1	.
9	296.05	81.28	0.34	2.96	0.33	3.00	0		0	.
9	297.05	83.68	0.34	2.95	0.33	3.00	0		0	.
9	298.05	147.75	0.34	2.93	0.33	3.00	0		0	.
9	299.05	149.09	0.34	2.93	0.33	3.00	0		0	.
9	300.05	150.95	0.35	2.90	0.35	2.90	1	1	0	3.00
9	301.05	81.91	0.36	2.81	0.35	2.90	0		1	.
9	302.05	84.15	0.61	1.63	0.35	2.90	0		0	.
9	303.05	84.52	0.61	1.63	0.35	2.90	0		0	.
9	304.05	86.38	0.61	1.63	0.35	2.90	0		0	.
9	305.05	86.28	0.61	1.64	0.35	2.90	0		0	.
9	306.05	87.69	0.61	1.64	0.35	2.90	0		0	.
9	307.05	105.77	0.61	1.65	0.35	2.90	0		0	.
9	308.05	163.23	0.59	1.69	0.35	2.90	0		0	.
9	309.05	162.93	0.59	1.71	0.35	2.90	0		0	.
9	310.05	107.77	0.58	1.72	0.35	2.90	0		0	.
9	311.05	108.84	0.59	1.71	0.35	2.90	0		0	.
9	312.05	309.25	0.60	1.68	0.60	1.68	1	1	0	2.90
9	313.05	310.08	0.49	2.06	0.60	1.68	0		1	.
9	314.05	312.28	0.48	2.06	0.60	1.68	0		0	.
9	315.05	167.97	0.48	2.09	0.60	1.68	0		0	.
9	316.05	111.78	0.47	2.12	0.47	2.12	1	1	0	1.68
9	317.05	113.08	0.47	2.13	0.47	2.12	0		1	.
9	318.05	115.15	0.47	2.14	0.47	2.12	0		0	.
9	319.05	174.95	0.47	2.14	0.47	2.12	0		0	.
9	320.05	175.88	0.47	2.14	0.47	2.12	0		0	.
9	321.05	117.48	0.47	2.14	0.47	2.12	0		0	.
9	322.05	324.69	0.47	2.15	0.47	2.15	1	0	0	2.12
9	323.05	181.35	0.46	2.17	0.47	2.15	0		1	.
9	324.05	183.09	0.46	2.18	0.47	2.15	0		0	.
9	325.05	180.22	0.47	2.14	0.47	2.14	1	0	0	2.15

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	326.05	1	0	1	0	1	325	0	1.78	0	99.53
9	327.05	1	0	1	0	1	325	0	1.78	1	99.53
9	328.05	1	0	1	1	1	325	0	1.78	2	99.53
9	329.05	0	1	1	0	1	325	0	1.78	0	17.65
9	330.05	1	1	1	0	1	325	0	2.14	1	31.30
9	331.05	0	.	1	0	1	331	0	2.14	0	126.82
9	332.05	1	.	0	1	3	332	0	2.32	0	126.82
9	333.05	1	.	1	0	1	333	0	2.32	1	44.94
9	334.05	1	0	0	0	2	333	0	2.32	0	126.82
9	335.05	0	.	0	0	2	335	0	1.78	1	126.82
9	336.05	1	1	1	0	1	335	0	1.78	2	126.82
9	337.05	1	.	1	0	1	337	0	1.78	2	113.17
9	338.05	0	.	0	0	2	338	0	1.78	1	113.17
9	339.05	1	1	1	1	1	338	0	1.96	1	85.88
9	340.05	1	.	1	0	3	340	0	1.78	0	126.82
9	341.05	1	0	1	0	1	340	0	1.96	1	85.88
9	342.05	1	0	0	0	1	340	0	1.96	1	85.88
9	343.05	1	.	1	0	2	343	0	1.78	1	44.94
9	344.05	1	.	1	0	2	344	0	1.60	1	126.82
9	345.05	0	1	0	1	1	344	0	1.60	2	126.82
9	346.05	1	1	1	0	1	344	0	1.60	1	126.82
9	347.05	0	.	0	0	.	347	0	1.07	2	126.82
9	348.05	0	.	1	0	.	348	0	1.07	0	85.88
9	349.05	1	0	1	0	1	350	0	0.53	2	126.82
9	350.05	1	.	1	0	.	350	0	0.36	1	126.82
9	353.05	1	.	0	0	.	353	0	0.53	1	4.01
9	355.05	0	.	1	0	.	355	0	0.36	1	44.94
9	356.05	0	.	0	0	2	356	0	0.53	0	44.94
9	226.06	1	.	1	0	.	226	0	0.53	1	4.01
9	227.06	0	.	0	0	2	227	0	0.89	2	4.01
9	228.06	1	1	1	0	1	227	0	1.25	1	4.01
9	229.06	0	.	0	0	.	229	0	0.89	1	17.65
9	241.06	1	.	1	0	.	241	0	0.53	1	4.01
9	242.06	1	.	1	0	.	242	0	0.53	1	4.01
9	243.06	1	.	1	0	.	243	0	0.89	1	31.30
9	247.06	0	.	0	0	2	247	0	1.07	1	31.30
9	248.06	0	.	0	0	2	248	0	1.25	1	85.88
9	249.06	0	.	0	0	.	249	0	0.89	1	17.65
9	256.06	0	0	0	1	2	257	0	0.71	0	17.65
9	257.06	0	.	0	0	.	257	0	0.36	0	17.65
9	261.06	1	.	0	0	.	261	0	1.07	1	17.65
9	262.06	1	0	0	0	1	261	0	1.25	0	17.65
9	264.06	0	0	1	0	1	261	0	1.43	2	99.53
9	265.06	0	1	1	0	1	261	0	1.25	1	99.53
9	266.06	1	.	1	0	2	266	0	1.60	2	31.30
9	267.06	0	1	0	0	1	266	0	1.60	1	31.30
9	268.06	1	.	1	0	2	268	0	1.43	0	31.30
9	271.06	0	.	0	0	.	271	0	0.89	1	44.94
9	272.06	1	.	1	0	2	272	0	1.25	1	44.94
9	275.06	0	.	1	0	.	275	0	1.07	1	44.94

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	326.05	181.85	0.47	2.13	0.47	2.14	0		1	.
9	327.05	183.72	0.51	1.96	0.47	2.14	0		0	.
9	328.05	185.32	0.51	1.97	0.47	2.14	0		0	.
9	329.05	336.04	0.51	1.96	0.47	2.14	0		0	.
9	330.05	243.44	0.51	1.98	0.47	2.14	0		0	.
9	331.05	131.16	0.51	1.96	0.51	1.96	1	2	0	2.14
9	332.05	130.06	0.49	2.04	0.49	2.04	1	3	0	2.14
9	333.05	237.50	0.50	2.00	0.50	2.00	1	1	0	2.14
9	334.05	133.50	0.47	2.14	0.50	2.00	0		1	.
9	335.05	135.37	0.46	2.16	0.46	2.16	1	1	0	2.00
9	336.05	137.03	0.46	2.15	0.46	2.16	0		1	.
9	337.05	144.04	0.46	2.15	0.46	2.15	1	1	0	2.16
9	338.05	145.64	0.46	2.16	0.46	2.16	1	1	0	2.15
9	339.05	216.59	0.46	2.16	0.46	2.16	0		1	.
9	340.05	182.55	0.46	2.20	0.46	2.20	1	0	0	2.16
9	341.05	258.86	0.45	2.20	0.46	2.20	0		1	.
9	342.05	259.83	0.45	2.22	0.46	2.20	0		0	.
9	343.05	302.83	0.45	2.22	0.45	2.22	1	1	0	2.20
9	344.05	223.39	0.45	2.23	0.45	2.23	1	0	0	2.22
9	345.05	224.82	0.45	2.22	0.45	2.23	0		1	.
9	346.05	226.92	0.45	2.22	0.45	2.23	0		0	.
9	347.05	329.99	1.03	0.97	1.03	0.97	1	0	0	2.23
9	348.05	414.95	1.15	0.87	1.15	0.87	1	0	0	0.97
9	349.05	432.73	1.12	0.90	1.10	0.91	0		1	.
9	350.05	431.40	1.10	0.91	1.10	0.91	1	0	0	0.87
9	353.05	631.87	0.95	1.05	0.95	1.05	1	0	0	0.91
9	355.05	859.42	1.40	0.71	1.40	0.71	1	0	0	1.05
9	356.05	861.26	1.42	0.71	1.42	0.71	1	0	0	0.71
9	226.06	52.68	1.01	0.99	1.01	0.99	1	0	0	.
9	227.06	54.15	1.02	0.98	1.02	0.98	1	1	0	0.99
9	228.06	55.55	1.03	0.97	1.02	0.98	0		1	.
9	229.06	51.38	1.03	0.97	1.03	0.97	1	0	0	0.98
9	241.06	74.44	0.93	1.07	0.93	1.07	1	0	0	0.97
9	242.06	73.80	0.93	1.08	0.93	1.08	1	0	0	1.07
9	243.06	50.55	0.94	1.06	0.94	1.06	1	1	0	1.08
9	247.06	52.52	0.96	1.04	0.96	1.04	1	1	0	1.06
9	248.06	34.23	0.96	1.04	0.96	1.04	1	0	0	1.04
9	249.06	91.79	1.17	0.86	1.17	0.86	1	0	0	1.04
9	256.06	109.21	1.16	0.86	1.15	0.87	0		1	.
9	257.06	108.14	1.15	0.87	1.15	0.87	1	0	0	0.86
9	261.06	111.11	0.94	1.06	0.94	1.06	1	0	0	0.87
9	262.06	112.17	0.93	1.08	0.94	1.06	0		1	.
9	264.06	59.99	0.93	1.08	0.94	1.06	0		0	.
9	265.06	58.82	0.92	1.09	0.94	1.06	0		0	.
9	266.06	94.40	0.92	1.08	0.92	1.08	1	1	0	1.06
9	267.06	96.83	0.93	1.07	0.92	1.08	0		1	.
9	268.06	98.27	0.94	1.07	0.94	1.07	1	1	0	1.08
9	271.06	103.94	0.95	1.05	0.95	1.05	1	0	0	1.07
9	272.06	105.94	0.96	1.04	0.96	1.04	1	1	0	1.05
9	275.06	108.58	0.99	1.01	0.99	1.01	1	0	0	1.04

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	276.06	1	.	0	0	.	276	0	0.53	0	17.65
9	279.06	1	.	0	1	.	279	0	0.36	1	58.59
9	280.06	1	0	0	1	2	279	0	0.71	1	58.59
9	281.06	0	.	1	0	1	281	0	1.43	1	4.01
9	282.06	0	.	0	0	2	282	0	1.60	0	58.59
9	283.06	1	.	0	0	2	283	0	1.25	1	99.53
9	284.06	1	1	0	0	1	282	0	1.78	2	99.53
9	285.06	1	0	1	0	2	282	0	1.43	1	99.53
9	286.06	0	1	0	0	1	282	0	1.78	0	58.59
9	287.06	0	0	0	0	1	282	0	1.96	1	58.59
9	288.06	0	.	0	0	2	288	0	1.78	1	58.59
9	289.06	1	1	0	0	1	288	0	1.78	1	44.94
9	290.06	1	.	1	0	.	290	0	1.43	1	58.59
9	291.06	1	0	0	0	1	290	0	1.60	1	58.59
9	292.06	0	.	1	0	2	292	0	1.78	1	99.53
9	293.06	1	1	1	0	1	292	0	1.96	1	17.65
9	294.06	0	.	1	1	2	294	0	1.25	2	58.59
9	295.06	0	0	0	0	1	294	0	1.60	1	58.59
9	296.06	1	1	1	0	2	294	0	1.60	1	85.88
9	297.06	1	0	1	0	1	294	0	1.78	0	85.88
9	298.06	0	1	1	0	2	294	0	1.96	1	58.59
9	299.06	1	1	1	0	1	294	0	1.78	0	58.59
9	300.06	1	.	1	0	3	300	0	1.60	1	58.59
9	301.06	0	1	0	0	1	300	0	1.78	1	99.53
9	302.06	0	0	1	0	2	300	0	1.78	0	99.53
9	303.06	0	0	1	0	1	300	0	1.96	1	85.88
9	304.06	0	0	0	0	1	300	0	1.96	0	85.88
9	305.06	0	0	1	0	2	300	0	1.96	1	99.53
9	306.06	0	0	0	0	1	300	0	1.96	1	99.53
9	307.06	0	0	1	0	1	300	0	2.14	0	99.53
9	308.06	1	1	1	0	1	300	0	1.78	1	31.30
9	309.06	1	0	1	0	1	300	0	1.78	1	58.59
9	310.06	0	1	1	0	1	300	0	1.78	1	99.53
9	311.06	0	0	1	0	2	300	0	1.96	2	99.53
9	315.06	0	.	1	0	1	315	0	1.78	1	58.59
9	316.06	0	.	1	0	2	316	0	1.78	1	99.53
9	317.06	0	0	0	1	1	316	0	1.78	1	99.53
9	318.06	0	0	0	1	1	316	0	1.96	2	99.53
9	319.06	1	1	0	0	1	316	0	2.14	1	72.24
9	320.06	1	0	1	1	1	316	0	2.14	2	72.24
9	321.06	1	0	0	0	1	316	0	2.14	1	99.53
9	323.06	1	.	1	0	1	323	0	2.14	1	31.30
9	324.06	1	0	0	1	1	323	0	1.96	1	31.30
9	325.06	1	.	1	0	.	325	0	1.43	1	72.24
9	326.06	1	0	1	0	1	325	0	1.60	1	72.24
9	327.06	1	0	1	0	1	325	0	1.78	1	72.24
9	328.06	1	0	1	1	1	325	0	1.78	2	72.24
9	330.06	1	.	1	0	1	330	0	2.49	1	4.01
9	331.06	0	1	1	0	1	332	0	2.32	1	99.53
9	332.06	1	.	0	1	2	332	0	1.96	2	99.53

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	276.06	136.27	1.04	0.96	1.04	0.96	1	0	0	1.01
9	279.06	113.85	0.77	1.30	0.77	1.30	1	0	0	0.96
9	280.06	115.72	0.77	1.31	0.77	1.30	0		1	.
9	281.06	150.78	0.72	1.39	0.72	1.39	1	4	0	1.30
9	282.06	120.02	0.70	1.42	0.70	1.42	1	0	0	1.39
9	283.06	67.26	0.72	1.39	0.72	1.39	1	0	0	1.39
9	284.06	72.70	0.70	1.43	0.70	1.42	0		0	.
9	285.06	71.50	0.68	1.48	0.70	1.42	0		1	.
9	286.06	130.47	0.60	1.67	0.70	1.42	0		0	.
9	287.06	131.84	0.56	1.79	0.70	1.42	0		0	.
9	288.06	122.93	0.40	2.47	0.40	2.47	1	1	0	1.42
9	289.06	135.04	0.40	2.53	0.40	2.47	0		1	.
9	290.06	136.01	0.40	2.49	0.40	2.49	1	1	0	2.47
9	291.06	137.54	0.40	2.50	0.40	2.49	0		1	.
9	292.06	77.37	0.40	2.50	0.40	2.50	1	1	0	2.49
9	293.06	171.43	0.40	2.51	0.40	2.50	0		1	.
9	294.06	142.08	0.40	2.51	0.40	2.51	1	0	0	2.50
9	295.06	142.85	0.39	2.54	0.40	2.51	0		1	.
9	296.06	81.28	0.39	2.55	0.40	2.51	0		0	.
9	297.06	83.68	0.39	2.57	0.40	2.51	0		0	.
9	298.06	147.75	0.39	2.60	0.40	2.51	0		0	.
9	299.06	149.09	0.38	2.60	0.40	2.51	0		0	.
9	300.06	150.95	0.38	2.65	0.38	2.65	1	0	0	2.51
9	301.06	81.91	0.37	2.73	0.38	2.65	0		1	.
9	302.06	84.15	0.25	3.92	0.38	2.65	0		0	.
9	303.06	84.52	0.25	3.94	0.38	2.65	0		0	.
9	304.06	86.38	0.25	3.95	0.38	2.65	0		0	.
9	305.06	86.28	0.26	3.92	0.38	2.65	0		0	.
9	306.06	87.69	0.26	3.90	0.38	2.65	0		0	.
9	307.06	105.77	0.26	3.91	0.38	2.65	0		0	.
9	308.06	163.23	0.26	3.91	0.38	2.65	0		0	.
9	309.06	162.93	0.26	3.91	0.38	2.65	0		0	.
9	310.06	107.77	0.26	3.91	0.38	2.65	0		0	.
9	311.06	108.84	0.26	3.91	0.38	2.65	0		0	.
9	315.06	167.97	0.24	4.16	0.24	4.16	1	1	0	2.65
9	316.06	111.78	0.24	4.17	0.24	4.17	1	0	0	4.16
9	317.06	113.08	0.24	4.16	0.24	4.17	0		1	.
9	318.06	115.15	0.24	4.16	0.24	4.17	0		0	.
9	319.06	174.95	0.24	4.14	0.24	4.17	0		0	.
9	320.06	175.88	0.24	4.16	0.24	4.17	0		0	.
9	321.06	117.48	0.24	4.16	0.24	4.17	0		0	.
9	323.06	181.35	0.24	4.21	0.24	4.21	1	1	0	4.17
9	324.06	183.09	0.24	4.18	0.24	4.21	0		1	.
9	325.06	180.22	0.34	2.97	0.34	2.97	1	0	0	4.21
9	326.06	181.85	0.34	2.96	0.34	2.97	0		1	.
9	327.06	183.72	0.32	3.13	0.34	2.97	0		0	.
9	328.06	185.32	0.32	3.10	0.34	2.97	0		0	.
9	330.06	243.44	0.31	3.21	0.31	3.21	1	4	0	2.97
9	331.06	131.16	0.31	3.20	0.31	3.19	0		1	.
9	332.06	130.06	0.31	3.19	0.31	3.19	1	0	0	3.21

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	333.06	1	1	1	0	1	332	0	2.32	0	17.65
9	334.06	1	0	0	0	1	332	0	2.49	0	99.53
9	335.06	0	.	0	0	2	335	0	1.78	1	99.53
9	336.06	1	1	1	0	1	335	0	1.78	2	99.53
9	337.06	1	.	1	0	1	337	0	1.78	2	85.88
9	338.06	0	.	0	0	3	338	0	1.43	1	85.88
9	339.06	1	1	1	1	1	338	0	1.96	1	58.59
9	340.06	1	.	1	0	3	340	0	1.96	0	99.53
9	341.06	1	.	1	0	1	341	0	1.43	1	58.59
9	342.06	1	0	0	0	1	341	0	1.78	1	58.59
9	343.06	1	.	1	0	.	343	0	1.60	1	17.65
9	344.06	1	.	1	0	.	344	0	1.78	1	99.53
9	345.06	0	.	0	1	1	345	0	1.96	2	99.53
9	346.06	1	.	1	0	2	346	0	1.43	0	99.53
9	347.06	0	.	0	0	.	347	0	0.36	2	99.53
9	348.06	0	.	1	0	.	348	0	0.36	0	58.59
9	349.06	1	0	1	0	1	350	0	0.71	2	99.53
9	350.06	1	.	1	0	.	350	0	0.36	1	99.53
9	355.06	0	.	1	0	.	355	0	0.36	1	17.65
9	356.06	0	.	0	0	.	356	0	0.71	0	17.65
9	363.06	1	.	1	0	.	363	0	0.36	1	85.88
9	243.07	1	.	1	0	.	243	0	0.71	1	4.01
9	247.07	0	.	0	0	2	247	0	0.89	1	4.01
9	248.07	0	.	0	0	.	248	0	0.71	0	58.59
9	264.07	0	0	1	0	1	265	0	1.25	2	72.24
9	265.07	0	.	1	0	.	265	0	0.89	1	72.24
9	266.07	1	.	1	0	2	266	0	1.25	2	4.01
9	267.07	0	.	0	0	1	267	0	1.25	1	4.01
9	268.07	1	.	1	0	2	268	0	1.25	0	4.01
9	271.07	0	.	0	0	.	271	0	0.36	1	17.65
9	272.07	1	.	1	0	.	272	0	0.71	1	17.65
9	275.07	0	.	1	0	.	275	0	0.71	1	17.65
9	279.07	1	.	0	1	.	279	0	0.36	1	31.30
9	280.07	1	0	0	1	2	279	0	0.71	1	31.30
9	282.07	0	.	0	0	2	282	0	1.43	0	31.30
9	283.07	1	.	0	0	2	283	0	1.07	0	72.24
9	284.07	1	0	0	0	1	285	0	1.43	2	72.24
9	285.07	1	.	1	0	2	285	0	1.07	1	72.24
9	286.07	0	.	0	0	.	286	0	1.43	0	31.30
9	287.07	0	0	0	0	1	286	0	1.25	1	31.30
9	288.07	0	.	0	0	.	288	0	1.43	1	31.30
9	289.07	1	.	0	0	.	289	0	1.07	0	17.65
9	290.07	1	.	1	0	.	290	0	1.07	1	31.30
9	291.07	1	0	0	0	1	290	0	1.07	1	31.30
9	292.07	0	.	1	0	3	292	0	1.07	1	72.24
9	294.07	0	.	1	1	2	294	0	1.07	2	31.30
9	295.07	0	0	0	0	1	294	0	1.43	1	31.30
9	296.07	1	1	1	0	2	294	0	1.43	1	58.59
9	297.07	1	0	1	0	1	294	0	1.60	0	58.59
9	298.07	0	1	1	0	1	294	0	1.78	1	31.30

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	333.06	237.50	0.32	3.17	0.31	3.19	0		0	.
9	334.06	133.50	0.32	3.16	0.31	3.19	0		0	.
9	335.06	135.37	0.32	3.09	0.32	3.09	1	0	0	3.19
9	336.06	137.03	0.33	3.07	0.32	3.09	0		1	.
9	337.06	144.04	0.32	3.09	0.32	3.09	1	1	0	3.09
9	338.06	145.64	0.32	3.09	0.32	3.09	1	0	0	3.09
9	339.06	216.59	0.33	3.06	0.32	3.09	0		1	.
9	340.06	182.55	0.62	1.62	0.62	1.62	1	0	0	3.09
9	341.06	258.86	0.63	1.60	0.63	1.60	1	1	0	1.62
9	342.06	259.83	0.63	1.59	0.63	1.60	0		1	.
9	343.06	302.83	0.64	1.57	0.64	1.57	1	0	0	1.60
9	344.06	223.39	0.64	1.57	0.64	1.57	1	1	0	1.57
9	345.06	224.82	0.66	1.52	0.66	1.52	1	1	0	1.57
9	346.06	226.92	0.65	1.54	0.65	1.54	1	0	0	1.52
9	347.06	329.99	1.03	0.97	1.03	0.97	1	0	0	1.54
9	348.06	414.95	1.10	0.91	1.10	0.91	1	0	0	0.97
9	349.06	432.73	1.10	0.91	1.11	0.90	0		1	.
9	350.06	431.40	1.11	0.90	1.11	0.90	1	0	0	0.91
9	355.06	859.42	1.49	0.67	1.49	0.67	1	0	0	0.90
9	356.06	861.26	1.51	0.66	1.51	0.66	1	1	0	0.67
9	363.06	1096.56	1.37	0.73	1.37	0.73	1	0	0	0.66
9	243.07	50.55	0.91	1.10	0.91	1.10	1	0	0	.
9	247.07	52.52	0.91	1.10	0.91	1.10	1	0	0	1.10
9	248.07	34.23	1.27	0.79	1.27	0.79	1	1	0	1.10
9	264.07	59.99	1.23	0.81	1.23	0.81	0		1	.
9	265.07	58.82	1.23	0.81	1.23	0.81	1	1	0	0.79
9	266.07	94.40	1.22	0.82	1.22	0.82	1	0	0	0.81
9	267.07	96.83	1.21	0.83	1.21	0.83	1	1	0	0.82
9	268.07	98.27	1.21	0.82	1.21	0.82	1	0	0	0.83
9	271.07	103.94	1.18	0.85	1.18	0.85	1	0	0	0.82
9	272.07	105.94	1.19	0.84	1.19	0.84	1	0	0	0.85
9	275.07	108.58	1.19	0.84	1.19	0.84	1	0	0	0.84
9	279.07	113.85	0.85	1.18	0.85	1.18	1	0	0	0.84
9	280.07	115.72	0.85	1.17	0.85	1.18	0		1	.
9	282.07	120.02	0.82	1.22	0.82	1.22	1	1	0	1.23
9	283.07	67.26	0.81	1.23	0.81	1.23	1	1	0	1.18
9	284.07	72.70	0.92	1.09	0.91	1.10	0		1	.
9	285.07	71.50	0.91	1.10	0.91	1.10	1	1	0	1.22
9	286.07	130.47	0.97	1.03	0.97	1.03	1	1	0	1.10
9	287.07	131.84	0.98	1.02	0.97	1.03	0		1	.
9	288.07	122.93	0.72	1.39	0.72	1.39	1	3	0	1.03
9	289.07	135.04	0.94	1.07	0.94	1.07	1	1	0	1.03
9	290.07	136.01	0.91	1.10	0.91	1.10	1	0	0	1.07
9	291.07	137.54	0.91	1.10	0.91	1.10	0		1	.
9	292.07	77.37	0.92	1.08	0.92	1.08	1	0	0	1.10
9	294.07	142.08	0.88	1.14	0.88	1.14	1	4	0	1.08
9	295.07	142.85	0.87	1.15	0.88	1.14	0		1	.
9	296.07	81.28	0.87	1.15	0.88	1.14	0		0	.
9	297.07	83.68	0.87	1.15	0.88	1.14	0		0	.
9	298.07	147.75	0.87	1.14	0.88	1.14	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	299.07	1	1	1	0	1	294	0	1.43	0	31.30
9	300.07	1	.	1	0	2	300	0	1.43	0	31.30
9	301.07	0	1	0	0	1	300	0	1.43	1	72.24
9	302.07	0	0	1	0	2	300	0	1.43	2	72.24
9	303.07	0	0	1	0	1	300	0	1.60	1	58.59
9	304.07	0	.	0	0	1	304	0	1.60	0	58.59
9	305.07	0	0	1	0	2	304	0	1.78	1	72.24
9	306.07	0	0	0	0	1	304	0	1.78	1	72.24
9	307.07	0	0	1	0	1	304	0	1.78	0	72.24
9	308.07	1	1	1	0	2	304	0	1.96	1	4.01
9	309.07	1	0	1	0	1	304	0	1.78	1	31.30
9	310.07	0	1	1	0	1	304	0	1.96	1	72.24
9	311.07	0	0	1	0	2	304	0	2.14	0	72.24
9	315.07	0	.	1	0	2	315	0	1.96	1	31.30
9	316.07	0	.	1	0	2	316	0	1.78	1	72.24
9	317.07	0	0	0	1	1	316	0	1.78	1	72.24
9	318.07	0	0	0	1	1	316	0	1.78	2	72.24
9	319.07	1	1	0	0	1	316	0	1.78	1	44.94
9	320.07	1	0	1	1	1	316	0	1.96	2	44.94
9	321.07	1	0	0	0	1	316	0	1.96	1	72.24
9	323.07	1	0	1	0	1	316	0	1.96	1	4.01
9	324.07	1	.	0	1	2	324	0	1.78	1	4.01
9	325.07	1	.	1	0	3	325	0	1.43	1	44.94
9	326.07	1	0	1	0	1	325	0	1.60	1	44.94
9	327.07	1	0	1	0	2	325	0	1.96	1	44.94
9	328.07	1	0	1	1	1	325	0	1.96	0	44.94
9	331.07	0	1	1	0	1	332	0	2.32	1	72.24
9	332.07	1	.	0	1	2	332	0	1.96	2	72.24
9	334.07	1	.	0	0	1	334	0	1.96	0	72.24
9	335.07	0	.	0	0	.	335	0	1.60	1	72.24
9	336.07	1	1	1	0	2	335	0	1.60	2	72.24
9	337.07	1	.	1	0	.	337	0	1.25	2	58.59
9	338.07	0	1	0	0	1	337	0	1.25	1	58.59
9	339.07	1	.	1	1	.	339	0	1.25	1	31.30
9	340.07	1	.	1	0	.	340	0	1.25	0	72.24
9	341.07	1	.	1	0	.	341	0	0.71	1	31.30
9	342.07	1	0	0	0	1	341	0	1.07	1	31.30
9	344.07	1	.	1	0	.	344	0	1.07	1	72.24
9	345.07	0	.	0	1	1	345	0	1.43	2	72.24
9	346.07	1	.	1	0	2	346	0	1.07	0	72.24
9	347.07	0	.	0	0	.	347	0	0.36	2	72.24
9	348.07	0	.	1	0	.	348	0	0.36	0	31.30
9	349.07	1	0	1	0	1	350	0	0.71	2	72.24
9	350.07	1	.	1	0	.	350	0	0.36	1	72.24
9	363.07	1	.	1	0	.	363	0	0.36	0	58.59
9	248.1	0	.	0	0	.	248	0	0.36	0	4.01
9	264.1	0	0	1	0	2	265	0	0.89	2	17.65
9	265.1	0	.	1	0	.	265	0	0.36	1	17.65
9	283.1	1	.	0	0	.	283	0	0.71	0	17.65
9	284.1	1	0	0	0	1	285	0	0.89	2	17.65

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	299.07	149.09	0.87	1.15	0.88	1.14	0		0	.
9	300.07	150.95	0.87	1.15	0.87	1.15	1	0	0	1.14
9	301.07	81.91	0.88	1.14	0.87	1.15	0		1	.
9	302.07	84.15	0.88	1.13	0.87	1.15	0		0	.
9	303.07	84.52	0.89	1.13	0.87	1.15	0		0	.
9	304.07	86.38	0.88	1.14	0.88	1.14	1	1	0	1.15
9	305.07	86.28	0.86	1.16	0.88	1.14	0		1	.
9	306.07	87.69	0.84	1.18	0.88	1.14	0		0	.
9	307.07	105.77	0.83	1.21	0.88	1.14	0		0	.
9	308.07	163.23	0.82	1.21	0.88	1.14	0		0	.
9	309.07	162.93	0.82	1.22	0.88	1.14	0		0	.
9	310.07	107.77	0.82	1.22	0.88	1.14	0		0	.
9	311.07	108.84	0.82	1.23	0.88	1.14	0		0	.
9	315.07	167.97	0.82	1.22	0.82	1.22	1	1	0	1.14
9	316.07	111.78	0.82	1.21	0.82	1.21	1	1	0	1.22
9	317.07	113.08	0.82	1.21	0.82	1.21	0		1	.
9	318.07	115.15	0.83	1.20	0.82	1.21	0		0	.
9	319.07	174.95	0.83	1.21	0.82	1.21	0		0	.
9	320.07	175.88	0.84	1.19	0.82	1.21	0		0	.
9	321.07	117.48	0.85	1.17	0.82	1.21	0		0	.
9	323.07	181.35	0.83	1.20	0.82	1.21	0		0	.
9	324.07	183.09	2.02	0.50	2.02	0.50	1	2	0	1.21
9	325.07	180.22	0.40	2.49	0.40	2.49	1	3	0	1.21
9	326.07	181.85	0.40	2.49	0.40	2.49	0		1	.
9	327.07	183.72	0.40	2.51	0.40	2.49	0		0	.
9	328.07	185.32	0.40	2.52	0.40	2.49	0		0	.
9	331.07	131.16	0.39	2.56	0.39	2.56	0		1	.
9	332.07	130.06	0.39	2.56	0.39	2.56	1	4	0	1.21
9	334.07	133.50	0.38	2.65	0.38	2.65	1	4	0	2.56
9	335.07	135.37	0.37	2.70	0.37	2.70	1	1	0	2.65
9	336.07	137.03	0.37	2.73	0.37	2.70	0		1	.
9	337.07	144.04	0.40	2.49	0.40	2.49	1	1	0	2.70
9	338.07	145.64	0.40	2.48	0.40	2.49	0		1	.
9	339.07	216.59	0.45	2.24	0.45	2.24	1	1	0	2.49
9	340.07	182.55	0.30	3.32	0.30	3.32	1	0	0	2.24
9	341.07	258.86	0.43	2.33	0.43	2.33	1	0	0	3.32
9	342.07	259.83	0.43	2.35	0.43	2.33	0		1	.
9	344.07	223.39	0.60	1.68	0.60	1.68	1	0	0	2.33
9	345.07	224.82	0.59	1.71	0.59	1.71	1	0	0	1.68
9	346.07	226.92	0.59	1.69	0.59	1.69	1	0	0	1.71
9	347.07	329.99	1.07	0.93	1.07	0.93	1	0	0	1.69
9	348.07	414.95	1.03	0.97	1.03	0.97	1	0	0	0.93
9	349.07	432.73	1.16	0.86	1.16	0.86	0		1	.
9	350.07	431.40	1.16	0.86	1.16	0.86	1	0	0	0.97
9	363.07	1096.56	0.36	2.74	0.36	2.74	1	0	0	.
9	248.1	34.23	1.77	0.57	1.77	0.57	1	0	0	.
9	264.1	59.99	1.58	0.63	1.57	0.64	0		1	.
9	265.1	58.82	1.57	0.64	1.57	0.64	1	0	0	0.57
9	283.1	67.26	1.05	0.95	1.05	0.95	1	0	0	0.64
9	284.1	72.70	1.01	0.99	1.00	1.00	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
9	285.1	1	.	1	0	.	285	0	0.53	1	17.65
9	292.1	0	.	1	0	.	292	0	0.71	0	17.65
9	296.1	1	.	1	0	.	296	0	1.07	1	4.01
9	297.1	1	0	1	0	1	296	0	1.25	1	4.01
9	301.1	0	.	0	0	.	301	0	1.25	1	17.65
9	302.1	0	0	1	0	2	301	0	1.43	0	17.65
9	303.1	0	0	1	0	1	301	0	1.60	1	4.01
9	304.1	0	0	0	0	2	301	0	1.78	0	4.01
9	305.1	0	.	1	0	2	305	0	1.78	1	17.65
9	306.1	0	0	0	0	2	305	0	1.96	1	17.65
9	307.1	0	.	1	0	.	307	0	1.07	1	17.65
9	310.1	0	.	1	0	.	310	0	1.43	1	17.65
9	311.1	0	0	1	0	2	310	0	1.60	1	17.65
9	316.1	0	.	1	0	.	316	0	1.25	1	17.65
9	317.1	0	0	0	1	2	316	0	1.25	0	17.65
9	318.1	0	.	0	1	2	318	0	1.25	0	17.65
9	321.1	1	.	0	0	.	321	0	1.25	1	17.65
9	331.1	0	1	1	0	1	332	0	1.43	1	17.65
9	332.1	1	.	0	1	.	332	0	1.25	2	17.65
9	334.1	1	.	0	0	2	334	0	1.43	0	17.65
9	335.1	0	.	0	0	.	335	0	1.25	1	17.65
9	336.1	1	1	1	0	2	335	0	1.25	1	17.65
9	337.1	1	.	1	0	.	337	0	0.53	2	4.01
9	338.1	0	1	0	0	1	337	0	0.89	1	4.01
9	340.1	1	.	1	0	.	340	0	0.36	2	17.65
9	344.1	1	.	1	0	.	344	0	0.36	1	17.65
9	345.1	0	1	0	1	1	344	0	0.71	2	17.65
9	346.1	1	.	1	0	2	346	0	1.07	1	17.65
9	347.1	0	.	0	0	.	347	0	0.36	2	17.65
9	349.1	1	0	1	0	1	350	0	0.71	2	17.65
9	350.1	1	.	1	0	.	350	0	0.36	1	17.65
9	363.1	1	.	1	0	.	363	0	0.36	0	4.01
10	2	0	.	1	0	.	2	0	0.28	1	65.55
10	3	0	.	0	1	1	3	0	0.56	2	19.75
10	8	0	.	0	0	.	8	0	0.28	1	4.49
10	9	1	1	1	0	2	8	0	0.70	1	4.49
10	10	0	1	0	0	2	8	0	0.98	1	4.49
10	14	0	.	0	0	.	14	0	0.56	1	19.75
10	15	0	0	1	0	2	14	0	1.12	1	4.49
10	16	1	1	0	0	2	14	0	0.84	1	19.75
10	17	1	0	0	0	1	14	0	1.12	1	19.75
10	19	1	.	0	0	1	19	1	1.40	2	4.49
10	21	0	.	0	0	1	21	1	1.54	0	4.49
10	23	0	.	0	0	1	23	1	2.11	0	4.49
10	25	0	.	1	0	1	25	1	1.54	2	50.28
10	26	0	0	0	0	1	25	1	1.40	2	50.28
10	28	0	.	1	0	1	28	1	1.83	2	50.28
10	30	0	.	1	0	1	30	1	1.54	0	50.28
10	31	1	.	1	0	1	31	1	1.97	1	4.49
10	32	0	.	1	0	1	32	1	1.68	2	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
9	285.1	71.50	1.00	1.00	1.00	1.00	1	0	0	0.95
9	292.1	77.37	0.86	1.16	0.86	1.16	1	0	0	1.00
9	296.1	81.28	0.84	1.19	0.84	1.19	1	0	0	1.16
9	297.1	83.68	0.83	1.20	0.84	1.19	0		1	.
9	301.1	81.91	0.77	1.29	0.77	1.29	1	1	0	1.19
9	302.1	84.15	0.78	1.29	0.77	1.29	0		1	.
9	303.1	84.52	0.77	1.30	0.77	1.29	0		0	.
9	304.1	86.38	0.77	1.29	0.77	1.29	0		0	.
9	305.1	86.28	0.77	1.29	0.77	1.29	1	1	0	1.29
9	306.1	87.69	0.78	1.29	0.77	1.29	0		1	.
9	307.1	105.77	0.94	1.07	0.94	1.07	1	0	0	1.29
9	310.1	107.77	0.91	1.10	0.91	1.10	1	0	0	1.07
9	311.1	108.84	0.90	1.11	0.91	1.10	0		1	.
9	316.1	111.78	0.89	1.12	0.89	1.12	1	0	0	1.10
9	317.1	113.08	0.89	1.12	0.89	1.12	0		1	.
9	318.1	115.15	0.90	1.11	0.90	1.11	1	1	0	1.12
9	321.1	117.48	0.87	1.15	0.87	1.15	1	0	0	1.11
9	331.1	131.16	0.89	1.12	0.89	1.12	0		1	.
9	332.1	130.06	0.89	1.12	0.89	1.12	1	1	0	1.15
9	334.1	133.50	0.89	1.12	0.89	1.12	1	0	0	1.12
9	335.1	135.37	0.89	1.12	0.89	1.12	1	0	0	1.12
9	336.1	137.03	0.91	1.10	0.89	1.12	0		1	.
9	337.1	144.04	0.87	1.15	0.87	1.15	1	0	0	1.12
9	338.1	145.64	0.87	1.15	0.87	1.15	0		1	.
9	340.1	182.55	1.18	0.85	1.18	0.85	1	2	0	1.15
9	344.1	223.39	0.94	1.07	0.94	1.07	1	0	0	1.15
9	345.1	224.82	0.94	1.06	0.94	1.07	0		1	.
9	346.1	226.92	0.94	1.07	0.94	1.07	1	1	0	1.07
9	347.1	329.99	1.11	0.90	1.11	0.90	1	0	0	1.07
9	349.1	432.73	1.16	0.86	1.15	0.87	0		1	.
9	350.1	431.40	1.15	0.87	1.15	0.87	1	0	0	0.90
9	363.1	1096.56	1.30	0.77	1.30	0.77	1	0	0	0.87
10	2	11.15	1.19	0.84	1.19	0.84	1	0	0	.
10	3	50.92	1.24	0.80	1.24	0.80	1	1	0	0.84
10	8	57.76	1.12	0.89	1.12	0.89	1	0	0	0.80
10	9	58.70	1.11	0.90	1.12	0.89	0		1	.
10	10	59.80	1.11	0.90	1.12	0.89	0		0	.
10	14	57.99	0.97	1.03	0.97	1.03	1	1	0	0.89
10	15	61.60	0.98	1.02	0.97	1.03	0		1	.
10	16	59.50	0.97	1.03	0.97	1.03	0		0	.
10	17	60.76	0.96	1.04	0.97	1.03	0		0	.
10	19	64.63	0.89	1.13	0.89	1.13	1	4	0	1.03
10	21	63.57	0.86	1.17	0.86	1.17	1	4	0	1.13
10	23	66.84	0.86	1.17	0.86	1.17	1	4	0	1.17
10	25	40.14	0.83	1.21	0.83	1.21	1	4	0	1.17
10	26	41.81	0.83	1.21	0.83	1.21	0		1	.
10	28	44.15	0.85	1.18	0.85	1.18	1	2	0	1.21
10	30	43.01	0.82	1.22	0.82	1.22	1	4	0	1.21
10	31	68.64	0.77	1.29	0.77	1.29	1	3	0	1.22
10	32	67.80	0.83	1.21	0.83	1.21	1	2	0	1.22

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	34	0	.	1	0	1	34	1	1.68	0	4.49
10	36	1	.	1	0	1	36	0	1.68	2	19.75
10	37	0	1	0	0	1	36	0	1.68	0	4.49
10	38	1	.	0	0	1	38	0	1.26	1	4.49
10	40	1	.	1	0	1	40	0	1.40	0	19.75
10	41	0	1	1	0	1	40	0	1.54	2	19.75
10	42	0	0	0	0	1	40	0	1.68	1	19.75
10	46	0	.	0	0	1	46	0	1.54	2	50.28
10	48	0	0	1	0	1	49	0	1.40	2	19.75
10	49	0	.	0	0	1	49	0	1.40	1	19.75
10	50	0	0	0	0	1	49	0	1.54	2	50.28
10	52	0	.	1	0	1	52	0	1.54	2	50.28
10	53	1	.	1	0	1	53	0	1.54	1	19.75
10	54	0	.	0	0	1	54	0	1.68	0	50.28
10	55	1	1	1	0	1	52	0	1.54	0	19.75
10	57	1	.	1	0	1	57	1	1.12	2	35.02
10	60	0	1	0	0	1	57	1	1.68	2	50.28
10	61	1	.	0	0	1	61	1	1.40	0	19.75
10	62	1	.	1	0	1	62	1	1.40	1	19.75
10	63	0	.	0	0	1	63	1	1.68	2	35.02
10	64	0	0	0	0	1	63	1	1.97	2	19.75
10	65	0	0	1	0	1	63	1	1.68	2	19.75
10	68	1	.	1	0	1	68	1	1.40	1	4.49
10	69	1	0	1	0	1	68	1	1.40	1	35.02
10	70	1	.	0	0	1	70	1	1.97	2	35.02
10	72	1	.	1	0	1	72	1	2.25	2	35.02
10	74	0	.	1	0	1	74	1	1.12	1	4.49
10	77	0	.	0	0	1	77	1	2.53	2	50.28
10	78	1	.	0	0	.	78	1	1.68	1	4.49
10	79	0	.	1	0	1	79	1	1.97	0	4.49
10	81	0	.	0	0	1	81	1	2.39	2	50.28
10	83	1	.	0	0	1	83	1	1.97	1	19.75
10	84	1	0	1	0	1	83	1	1.97	1	19.75
10	85	1	.	1	0	.	85	1	2.11	2	4.49
10	87	0	1	1	0	1	85	1	2.39	2	35.02
10	89	0	0	0	0	1	85	1	2.53	2	50.28
10	90	1	.	0	0	1	90	1	2.39	1	19.75
10	91	0	.	0	0	1	91	1	2.11	0	19.75
10	93	1	.	0	0	1	93	1	2.25	0	4.49
10	94	1	.	0	0	1	94	1	2.53	1	4.49
10	96	0	1	0	0	1	93	1	2.39	0	19.75
10	99	0	0	0	0	1	93	1	2.39	0	19.75
10	100	1	.	0	0	1	100	1	2.39	1	19.75
10	101	0	.	0	1	1	101	1	2.67	1	4.49
10	102	1	.	1	0	1	102	1	2.39	2	65.55
10	103	1	0	1	0	1	102	1	2.53	2	50.28
10	104	1	.	0	0	1	104	1	2.11	0	35.02
10	105	1	.	1	0	1	105	1	2.53	0	35.02
10	106	0	.	1	0	1	106	1	2.67	0	4.49
10	108	1	.	1	1	1	108	1	2.25	1	35.02

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	34	69.77	0.77	1.29	0.77	1.29	1	2	0	1.22
10	36	71.04	0.79	1.27	0.79	1.27	1	2	0	1.22
10	37	74.68	0.77	1.30	0.79	1.27	0		1	.
10	38	73.51	0.73	1.36	0.73	1.36	1	3	0	1.22
10	40	73.91	0.75	1.33	0.75	1.33	1	4	0	1.22
10	41	74.64	0.75	1.33	0.75	1.33	0		1	.
10	42	75.75	0.76	1.31	0.75	1.33	0		0	.
10	46	51.42	0.70	1.44	0.70	1.44	1	4	0	1.33
10	48	78.82	0.66	1.50	0.66	1.52	0		1	.
10	49	78.35	0.66	1.52	0.66	1.52	1	4	0	1.44
10	50	53.62	0.67	1.50	0.66	1.52	0		0	.
10	52	56.12	0.66	1.50	0.66	1.50	1	1	0	1.56
10	53	79.95	0.64	1.56	0.64	1.56	1	4	0	1.52
10	54	54.86	0.62	1.60	0.62	1.60	1	3	0	1.50
10	55	83.82	0.66	1.52	0.66	1.50	0		1	.
10	57	56.09	0.63	1.59	0.63	1.59	1	1	0	1.50
10	60	57.49	0.63	1.58	0.63	1.59	0		1	.
10	61	86.46	0.60	1.66	0.60	1.66	1	3	0	1.59
10	62	87.62	0.61	1.63	0.61	1.63	1	1	0	1.59
10	63	57.23	0.63	1.60	0.63	1.60	1	1	0	1.63
10	64	91.23	0.64	1.57	0.63	1.60	0		1	.
10	65	90.76	0.64	1.57	0.63	1.60	0		0	.
10	68	90.56	0.56	1.79	0.56	1.79	1	3	0	1.60
10	69	58.93	0.57	1.77	0.56	1.79	0		1	.
10	70	61.36	0.58	1.72	0.58	1.72	1	3	0	1.60
10	72	60.30	0.60	1.66	0.60	1.66	1	2	0	1.60
10	74	87.06	0.53	1.88	0.53	1.88	1	3	0	1.60
10	77	60.43	0.55	1.82	0.55	1.82	1	2	0	1.60
10	78	92.06	0.51	1.96	0.51	1.96	1	3	0	1.60
10	79	94.83	0.54	1.86	0.54	1.86	1	2	0	1.60
10	81	61.96	0.61	1.64	0.61	1.64	1	2	0	1.60
10	83	92.10	0.49	2.06	0.49	2.06	1	3	0	1.60
10	84	93.40	0.52	1.92	0.49	2.06	0		1	.
10	85	97.10	0.55	1.81	0.55	1.81	1	2	0	1.60
10	87	63.13	0.56	1.78	0.55	1.81	0		1	.
10	89	63.23	0.57	1.76	0.55	1.81	0		0	.
10	90	95.17	0.47	2.13	0.47	2.13	1	3	0	1.60
10	91	96.67	0.49	2.03	0.49	2.03	1	2	0	1.60
10	93	102.44	0.49	2.04	0.49	2.04	1	3	0	1.60
10	94	100.57	0.58	1.73	0.58	1.73	1	2	0	1.60
10	96	105.44	0.51	1.97	0.49	2.04	0		1	.
10	99	102.87	0.52	1.94	0.49	2.04	0		0	.
10	100	99.67	0.42	2.35	0.42	2.35	1	3	0	1.60
10	101	112.02	0.53	1.89	0.53	1.89	1	2	0	1.60
10	102	39.71	0.51	1.96	0.51	1.96	1	3	0	1.60
10	103	67.17	0.52	1.91	0.51	1.96	0		1	.
10	104	62.40	0.43	2.35	0.43	2.35	1	3	0	1.60
10	105	66.17	0.54	1.84	0.54	1.84	1	2	0	1.60
10	106	114.48	0.49	2.04	0.49	2.04	1	3	0	1.60
10	108	64.47	0.50	2.01	0.50	2.01	1	4	0	1.60

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	109	1	.	1	0	1	109	1	2.53	2	50.28
10	110	1	0	0	0	1	109	1	2.39	2	19.75
10	111	1	0	0	0	1	109	1	2.39	2	19.75
10	113	0	.	1	0	1	113	1	2.25	1	4.49
10	114	1	.	1	0	1	114	1	2.25	2	35.02
10	115	0	.	0	1	1	115	1	2.53	2	19.75
10	117	0	.	1	0	1	117	1	2.81	0	35.02
10	118	1	.	1	0	.	118	1	1.97	0	4.49
10	120	0	.	0	0	1	118	1	2.11	2	19.75
10	121	0	.	0	0	1	121	1	2.11	1	4.49
10	122	1	.	1	0	1	122	1	2.11	0	4.49
10	123	1	.	1	0	1	123	1	2.11	1	4.49
10	124	1	.	1	0	1	124	1	1.97	1	19.75
10	125	1	.	1	0	1	125	1	2.25	1	4.49
10	126	1	.	0	0	1	126	1	1.97	2	35.02
10	127	0	.	1	1	1	125	1	1.83	1	19.75
10	128	0	.	1	0	1	128	1	2.11	0	19.75
10	129	1	.	0	0	1	129	1	2.53	1	4.49
10	130	0	.	0	0	1	130	1	2.39	2	35.02
10	131	0	0	0	0	1	130	1	2.39	0	19.75
10	132	0	1	0	0	1	129	1	2.25	1	4.49
10	133	0	0	1	0	1	129	1	2.53	1	4.49
10	134	0	.	1	0	1	134	0	2.53	1	50.28
10	135	0	0	1	1	1	134	0	2.39	2	50.28
10	136	0	0	1	0	1	134	0	2.67	1	4.49
10	137	1	.	1	0	1	137	0	2.53	2	50.28
10	138	0	.	0	0	1	138	0	2.39	1	19.75
10	139	1	.	1	0	1	139	0	2.67	2	50.28
10	140	0	1	1	0	1	139	0	2.67	1	19.75
10	141	0	.	0	1	1	141	1	2.67	1	19.75
10	142	1	.	1	0	1	142	1	2.53	2	50.28
10	143	0	0	0	0	1	141	1	2.67	1	4.49
10	144	1	0	1	0	1	142	1	2.39	2	4.49
10	145	1	1	0	0	1	141	1	2.39	1	4.49
10	146	0	1	0	0	1	142	1	2.25	2	50.28
10	147	1	0	1	0	1	141	1	2.53	1	4.49
10	148	0	.	0	0	1	148	1	2.67	0	19.75
10	149	0	.	1	0	1	149	1	2.53	1	35.02
10	150	0	.	1	0	1	150	1	2.39	1	4.49
10	151	1	.	1	0	1	151	1	2.53	2	4.49
10	152	0	.	1	0	1	152	1	2.39	1	35.02
10	153	0	.	1	0	1	153	1	2.53	2	35.02
10	154	1	.	1	1	.	154	1	2.11	1	4.49
10	155	1	.	1	0	1	155	0	2.39	2	35.02
10	156	1	0	0	0	1	155	0	2.25	0	19.75
10	157	1	.	1	1	1	157	0	2.11	1	4.49
10	158	1	0	0	1	1	157	0	2.25	1	4.49
10	159	1	.	1	0	1	159	0	2.11	1	4.49
10	160	0	.	0	0	1	160	0	2.53	2	35.02
10	161	0	.	1	1	1	161	0	2.25	0	35.02

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	109	68.60	0.51	1.96	0.51	1.96	1	2	0	2.01
10	110	118.42	0.54	1.84	0.51	1.96	0		1	.
10	111	120.66	0.55	1.83	0.51	1.96	0		0	.
10	113	124.76	0.47	2.12	0.47	2.12	1	3	0	2.01
10	114	69.34	0.54	1.86	0.54	1.86	1	2	0	2.01
10	115	110.21	0.47	2.14	0.47	2.14	1	3	0	2.01
10	117	67.30	0.46	2.17	0.46	2.17	1	3	0	2.01
10	118	138.68	0.52	1.93	0.52	1.93	1	2	0	2.01
10	120	133.44	0.52	1.93	0.52	1.93	1	0	1	.
10	121	129.67	0.45	2.24	0.45	2.24	1	3	0	2.01
10	122	135.57	0.47	2.14	0.47	2.14	1	2	0	2.01
10	123	131.50	0.45	2.23	0.45	2.23	1	3	0	2.01
10	124	130.40	0.48	2.09	0.48	2.09	1	2	0	2.01
10	125	140.51	0.49	2.04	0.49	2.04	1	3	0	2.01
10	126	70.71	0.51	1.95	0.51	1.95	1	2	0	2.01
10	127	136.11	0.49	2.06	0.49	2.04	1	0	1	.
10	128	137.87	0.52	1.92	0.52	1.92	1	2	0	2.01
10	129	141.98	0.50	1.99	0.50	1.99	1	3	0	2.01
10	130	72.14	0.53	1.89	0.53	1.89	1	2	0	2.01
10	131	139.64	0.54	1.86	0.53	1.89	0		1	.
10	132	145.68	0.50	1.99	0.50	1.99	0		1	.
10	133	148.75	0.52	1.94	0.50	1.99	0		0	.
10	134	70.67	0.52	1.91	0.52	1.91	1	1	0	2.01
10	135	71.41	0.52	1.91	0.52	1.91	0		1	.
10	136	157.39	0.53	1.88	0.52	1.91	0		0	.
10	137	73.58	0.53	1.89	0.53	1.89	1	3	0	1.91
10	138	145.75	0.56	1.78	0.56	1.78	1	2	0	1.91
10	139	75.11	0.56	1.77	0.56	1.77	1	1	0	1.91
10	140	147.65	0.57	1.74	0.56	1.77	0		1	.
10	141	150.55	0.58	1.71	0.58	1.71	1	2	0	1.77
10	142	77.65	0.56	1.78	0.56	1.78	1	3	0	1.77
10	143	157.93	0.60	1.66	0.58	1.71	0		1	.
10	144	165.74	0.60	1.67	0.56	1.78	0		1	.
10	145	167.94	0.61	1.64	0.58	1.71	0		0	.
10	146	79.38	0.61	1.65	0.56	1.78	0		0	.
10	147	172.74	0.63	1.59	0.58	1.71	0		0	.
10	148	159.46	0.64	1.56	0.64	1.56	1	1	0	1.77
10	149	74.34	0.64	1.56	0.64	1.56	1	1	0	1.56
10	150	176.95	0.66	1.51	0.66	1.51	1	2	0	1.56
10	151	177.55	0.63	1.58	0.63	1.58	1	3	0	1.56
10	152	76.51	0.66	1.52	0.66	1.52	1	1	0	1.56
10	153	80.48	0.70	1.42	0.70	1.42	1	2	0	1.52
10	154	185.92	0.63	1.58	0.63	1.58	1	3	0	1.52
10	155	78.51	0.67	1.50	0.67	1.50	1	1	0	1.52
10	156	170.84	0.67	1.49	0.67	1.50	0		1	.
10	157	189.03	0.60	1.67	0.60	1.67	1	3	0	1.50
10	158	193.00	0.61	1.64	0.60	1.67	0		1	.
10	159	196.10	0.63	1.59	0.63	1.59	1	2	0	1.50
10	160	82.22	0.59	1.69	0.59	1.69	1	3	0	1.50
10	161	82.75	0.62	1.61	0.62	1.61	1	1	0	1.50

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	162	0	1	1	0	1	161	0	2.53	0	19.75
10	163	1	1	0	0	1	161	0	2.53	1	19.75
10	164	0	0	0	0	1	161	0	2.25	2	19.75
10	165	0	0	1	0	1	161	0	2.39	0	19.75
10	166	1	0	1	0	1	161	0	2.11	2	4.49
10	167	1	1	1	0	1	161	0	2.25	1	4.49
10	168	1	0	1	0	1	161	0	2.25	1	4.49
10	169	0	1	0	0	1	161	0	2.25	0	35.02
10	170	0	0	0	0	1	161	0	1.97	1	4.49
10	171	0	.	0	0	1	171	1	1.97	1	4.49
10	172	1	.	1	0	2	172	1	1.83	2	19.75
10	173	1	1	0	0	1	171	1	1.83	1	19.75
10	174	0	1	0	0	1	172	1	2.25	2	50.28
10	175	0	1	0	0	1	171	1	2.25	1	50.28
10	176	0	0	1	0	1	171	1	2.25	1	35.02
10	177	0	0	0	0	1	172	1	2.39	2	19.75
10	178	1	1	1	0	1	171	1	2.11	1	19.75
10	179	0	0	0	0	1	172	1	2.25	2	19.75
10	180	1	0	1	1	1	171	1	1.83	1	19.75
10	181	1	1	0	1	1	172	1	1.83	2	65.55
10	182	1	0	1	0	1	171	1	1.83	1	19.75
10	183	1	0	1	0	1	172	1	1.83	2	65.55
10	184	1	0	0	0	1	171	1	2.11	1	19.75
10	185	1	0	0	0	1	171	1	2.11	1	50.28
10	186	1	0	1	0	1	172	1	1.97	2	35.02
10	187	1	.	1	1	1	187	0	1.83	1	50.28
10	188	1	0	0	0	1	187	0	1.68	2	19.75
10	189	1	0	1	0	1	187	0	1.68	1	19.75
10	190	1	0	1	0	1	187	0	1.83	2	19.75
10	191	0	1	1	0	1	187	0	1.97	1	19.75
10	192	1	1	0	1	1	187	0	1.97	2	50.28
10	193	0	1	0	0	1	187	0	1.97	1	19.75
10	194	0	0	1	0	1	187	0	1.83	1	65.55
10	195	0	.	0	0	.	195	0	1.54	2	35.02
10	196	0	.	1	0	1	196	0	1.68	1	35.02
10	197	0	0	1	0	1	195	0	1.68	0	65.55
10	198	0	0	1	1	1	195	0	1.83	1	19.75
10	199	0	0	0	0	1	195	0	1.68	1	35.02
10	200	0	0	0	0	1	195	0	1.68	2	35.02
10	201	0	0	1	0	1	195	0	1.83	1	35.02
10	202	0	0	0	0	1	195	0	1.83	0	19.75
10	203	0	0	1	0	1	195	0	1.97	1	19.75
10	204	0	0	1	0	1	195	0	2.11	2	19.75
10	205	0	0	0	0	1	195	0	2.11	1	35.02
10	206	0	.	1	0	1	206	1	1.83	2	35.02
10	207	1	.	1	0	1	207	1	1.83	1	35.02
10	208	0	0	0	0	1	206	1	1.97	2	19.75
10	209	1	0	1	0	1	207	1	1.97	1	19.75
10	210	0	.	1	0	1	210	0	1.83	1	50.28
10	211	0	0	0	0	1	210	0	1.68	1	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	162	183.32	0.62	1.60	0.62	1.61	0		0	.
10	163	175.75	0.61	1.64	0.62	1.61	0		1	.
10	164	191.46	0.63	1.59	0.62	1.61	0		0	.
10	165	198.54	0.66	1.52	0.62	1.61	0		0	.
10	166	204.14	0.68	1.47	0.62	1.61	0		0	.
10	167	200.64	0.63	1.58	0.62	1.61	0		0	.
10	168	203.21	0.66	1.51	0.62	1.61	0		0	.
10	169	84.39	0.69	1.45	0.62	1.61	0		0	.
10	170	207.34	0.69	1.44	0.62	1.61	0		0	.
10	171	209.71	0.71	1.41	0.71	1.41	1	2	0	1.61
10	172	206.74	0.66	1.51	0.66	1.51	1	3	0	1.61
10	173	207.08	0.70	1.43	0.71	1.41	0		1	.
10	174	81.35	0.70	1.43	0.66	1.51	0		1	.
10	175	81.02	0.71	1.42	0.71	1.41	0		0	.
10	176	85.45	0.71	1.40	0.71	1.41	0		0	.
10	177	215.22	0.70	1.43	0.66	1.51	0		0	.
10	178	214.52	0.71	1.41	0.71	1.41	0		0	.
10	179	216.65	0.69	1.46	0.66	1.51	0		0	.
10	180	223.66	0.69	1.44	0.71	1.41	0		0	.
10	181	50.52	0.66	1.52	0.66	1.51	0		0	.
10	182	225.83	0.69	1.44	0.71	1.41	0		0	.
10	183	52.32	0.67	1.50	0.66	1.51	0		0	.
10	184	227.50	0.69	1.46	0.71	1.41	0		0	.
10	185	84.19	0.70	1.43	0.71	1.41	0		0	.
10	186	87.29	0.66	1.51	0.66	1.51	0		0	.
10	187	86.55	0.70	1.42	0.70	1.42	1	1	0	1.61
10	188	233.20	0.68	1.48	0.70	1.42	0		1	.
10	189	233.54	0.70	1.43	0.70	1.42	0		0	.
10	190	234.57	0.70	1.44	0.70	1.42	0		0	.
10	191	235.74	0.71	1.40	0.70	1.42	0		0	.
10	192	88.39	0.72	1.39	0.70	1.42	0		0	.
10	193	237.31	0.73	1.38	0.70	1.42	0		0	.
10	194	54.02	0.74	1.35	0.70	1.42	0		0	.
10	195	91.46	0.72	1.38	0.72	1.38	1	0	0	1.40
10	196	89.12	0.72	1.40	0.72	1.40	1	1	0	1.42
10	197	55.99	0.71	1.40	0.72	1.38	0		1	.
10	198	245.18	0.73	1.37	0.72	1.38	0		0	.
10	199	95.30	0.74	1.34	0.72	1.38	0		0	.
10	200	99.23	0.74	1.35	0.72	1.38	0		0	.
10	201	97.83	0.74	1.35	0.72	1.38	0		0	.
10	202	250.39	0.73	1.37	0.72	1.38	0		0	.
10	203	250.55	0.73	1.38	0.72	1.38	0		0	.
10	204	251.96	0.73	1.38	0.72	1.38	0		0	.
10	205	101.04	0.73	1.36	0.72	1.38	0		0	.
10	206	107.64	0.74	1.36	0.74	1.36	1	3	0	1.38
10	207	102.54	0.75	1.34	0.75	1.34	1	2	0	1.38
10	208	260.90	0.73	1.37	0.74	1.36	0		1	.
10	209	258.30	0.75	1.33	0.75	1.34	0		1	.
10	210	92.03	0.75	1.33	0.75	1.33	1	1	0	1.38
10	211	262.07	0.73	1.37	0.75	1.33	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	212	0	0	0	0	1	210	0	1.40	1	19.75
10	213	0	.	1	1	1	213	0	1.40	2	19.75
10	214	0	.	1	0	.	214	0	1.40	1	50.28
10	215	0	.	1	0	1	215	0	1.54	0	19.75
10	216	1	1	1	0	1	215	0	1.54	1	19.75
10	217	0	1	1	0	2	215	0	1.40	1	65.55
10	218	1	.	0	0	.	218	0	1.26	1	35.02
10	219	1	0	0	0	2	218	0	1.26	1	65.55
10	220	1	.	0	1	2	220	0	1.12	1	19.75
10	221	1	0	0	0	1	220	0	0.98	1	65.55
10	222	1	0	0	0	1	220	0	0.98	1	19.75
10	223	0	.	0	0	2	223	0	1.12	1	50.28
10	224	0	0	1	0	1	223	0	1.12	1	50.28
10	225	0	0	1	0	1	223	0	1.12	1	35.02
10	226	1	.	1	0	.	226	0	1.12	1	80.81
10	227	0	1	0	0	2	226	0	1.26	1	35.02
10	228	1	1	0	0	1	226	0	1.26	1	65.55
10	229	0	1	1	0	2	226	0	1.26	1	35.02
10	230	0	0	1	0	1	226	0	1.54	2	35.02
10	231	0	.	1	1	2	231	0	1.54	1	80.81
10	232	1	.	1	1	1	232	0	1.26	1	50.28
10	233	0	.	1	0	1	233	0	1.26	1	35.02
10	234	0	.	0	0	1	234	0	1.40	2	35.02
10	235	0	.	1	0	1	235	0	1.54	1	35.02
10	236	0	0	0	0	1	235	0	1.54	0	35.02
10	237	0	0	1	0	1	235	0	1.54	1	65.55
10	238	0	0	1	0	1	235	0	1.54	2	35.02
10	239	1	1	1	0	1	235	0	1.40	1	35.02
10	240	1	0	1	0	1	235	0	1.68	2	35.02
10	241	0	1	1	0	1	235	0	1.54	1	65.55
10	242	0	0	0	0	1	235	0	1.68	1	19.75
10	243	0	0	0	1	1	235	0	1.83	0	19.75
10	244	1	1	1	0	1	235	0	1.83	1	65.55
10	245	0	1	1	0	1	235	0	1.68	0	35.02
10	246	1	1	1	0	1	235	0	1.54	1	50.28
10	247	0	1	0	0	1	235	0	1.54	2	35.02
10	248	1	.	1	0	1	248	0	1.40	1	50.28
10	249	1	.	1	0	1	249	0	1.40	2	35.02
10	250	1	.	1	0	1	250	0	1.54	1	65.55
10	251	0	.	0	0	1	251	0	1.54	0	65.55
10	252	1	1	1	0	1	251	0	1.68	1	35.02
10	253	1	0	1	1	1	251	0	1.40	1	50.28
10	254	1	0	0	0	1	251	0	1.54	2	35.02
10	255	1	0	1	0	1	251	0	1.54	1	35.02
10	256	0	1	1	0	1	251	0	1.40	1	50.28
10	257	0	.	0	0	1	257	0	1.54	2	65.55
10	258	1	1	1	0	1	257	0	1.68	1	80.81
10	259	0	1	1	0	1	257	0	1.68	1	80.81
10	260	1	.	1	0	2	260	0	1.54	0	80.81
10	261	1	.	1	0	2	261	0	1.40	1	50.28

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	212	263.53	0.77	1.31	0.75	1.33	0		0	.
10	213	267.67	0.76	1.31	0.76	1.31	1	2	0	1.33
10	214	94.00	0.72	1.38	0.72	1.38	1	3	0	1.33
10	215	267.77	0.71	1.40	0.71	1.40	1	1	0	1.33
10	216	269.31	0.72	1.39	0.71	1.40	0		1	.
10	217	59.06	0.72	1.39	0.71	1.40	0		0	.
10	218	104.41	0.72	1.39	0.72	1.39	1	0	0	1.40
10	219	57.59	0.72	1.39	0.72	1.39	0		1	.
10	220	278.48	0.74	1.36	0.74	1.36	1	1	0	1.39
10	221	59.63	0.75	1.34	0.74	1.36	0		1	.
10	222	282.22	0.75	1.33	0.74	1.36	0		0	.
10	223	101.54	0.77	1.31	0.77	1.31	1	1	0	1.36
10	224	100.30	0.77	1.29	0.77	1.31	0		1	.
10	225	116.18	0.76	1.31	0.77	1.31	0		0	.
10	226	58.93	0.74	1.34	0.74	1.34	1	0	0	1.31
10	227	120.09	0.74	1.34	0.74	1.34	0		1	.
10	228	63.27	0.74	1.34	0.74	1.34	0		0	.
10	229	136.50	0.75	1.33	0.74	1.34	0		0	.
10	230	176.61	0.76	1.31	0.74	1.34	0		0	.
10	231	62.10	0.77	1.30	0.77	1.30	1	0	0	1.34
10	232	111.81	0.78	1.28	0.78	1.28	1	0	0	1.30
10	233	207.64	0.79	1.27	0.79	1.27	1	2	0	1.28
10	234	182.75	0.76	1.31	0.76	1.31	1	3	0	1.28
10	235	239.64	0.79	1.27	0.79	1.27	1	1	0	1.28
10	236	242.68	0.78	1.29	0.79	1.27	0		1	.
10	237	66.17	0.78	1.28	0.79	1.27	0		0	.
10	238	257.33	0.75	1.33	0.79	1.27	0		0	.
10	239	248.08	0.76	1.32	0.79	1.27	0		0	.
10	240	251.82	0.75	1.34	0.79	1.27	0		0	.
10	241	64.27	0.74	1.35	0.79	1.27	0		0	.
10	242	310.48	0.74	1.35	0.79	1.27	0		0	.
10	243	312.25	0.76	1.32	0.79	1.27	0		0	.
10	244	67.50	0.77	1.30	0.79	1.27	0		0	.
10	245	266.43	0.74	1.35	0.79	1.27	0		0	.
10	246	200.44	0.77	1.31	0.79	1.27	0		0	.
10	247	269.04	0.75	1.34	0.79	1.27	0		0	.
10	248	216.22	0.74	1.36	0.74	1.36	1	0	0	1.27
10	249	273.64	0.77	1.30	0.77	1.30	1	2	0	1.36
10	250	72.04	0.74	1.35	0.74	1.35	1	3	0	1.36
10	251	69.47	0.75	1.34	0.75	1.34	1	1	0	1.36
10	252	276.81	0.76	1.31	0.75	1.34	0		1	.
10	253	250.82	0.77	1.29	0.75	1.34	0		0	.
10	254	284.39	0.77	1.30	0.75	1.34	0		0	.
10	255	279.35	0.77	1.30	0.75	1.34	0		0	.
10	256	267.67	0.77	1.29	0.75	1.34	0		0	.
10	257	70.41	0.78	1.29	0.78	1.29	1	0	0	1.34
10	258	69.97	0.78	1.28	0.78	1.29	0		1	.
10	259	69.81	0.78	1.27	0.78	1.29	0		0	.
10	260	71.64	0.79	1.27	0.79	1.27	1	0	0	1.29
10	261	287.09	0.80	1.25	0.80	1.25	1	0	0	1.27

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	262	0	.	1	0	2	262	0	1.26	1	50.28
10	263	0	.	0	0	2	263	0	1.26	1	65.55
10	264	0	.	1	0	3	264	0	1.12	1	80.81
10	265	0	.	0	0	.	265	0	0.84	1	50.28
10	266	1	.	0	0	.	266	0	0.84	1	65.55
10	267	0	1	1	0	1	266	0	1.12	1	50.28
10	268	0	0	0	0	2	266	0	1.12	1	65.55
10	269	0	0	1	0	2	266	0	1.12	1	80.81
10	270	0	0	1	0	2	266	0	1.12	1	80.81
10	271	1	.	1	0	1	271	0	1.26	2	65.55
10	273	0	.	1	1	.	273	0	1.12	0	96.08
10	274	1	1	1	0	2	273	0	1.12	1	65.55
10	275	1	.	1	0	.	275	0	0.98	1	80.81
10	276	1	0	1	0	1	275	0	1.12	1	96.08
10	277	1	.	1	0	1	277	0	1.12	0	65.55
10	278	0	1	0	0	2	277	0	1.12	0	50.28
10	279	1	.	1	0	1	279	0	0.98	1	50.28
10	280	0	.	1	0	1	280	0	1.12	1	65.55
10	281	0	0	0	0	1	282	0	1.40	2	50.28
10	282	0	.	1	0	.	282	0	1.12	1	50.28
10	283	0	0	0	0	1	282	0	1.54	1	80.81
10	284	1	.	1	0	1	284	0	1.12	1	65.55
10	285	1	0	1	0	1	286	0	1.26	2	80.81
10	286	1	.	1	0	1	286	0	1.26	1	80.81
10	287	1	0	1	0	1	286	0	1.40	1	80.81
10	288	0	1	0	0	2	286	0	1.40	1	65.55
10	289	0	.	1	0	3	289	0	1.12	1	50.28
10	290	1	1	1	0	2	289	0	1.26	1	50.28
10	291	1	0	1	0	2	289	0	1.26	0	50.28
10	292	0	.	1	0	2	292	0	1.12	1	65.55
10	293	1	.	1	0	1	293	0	0.98	1	65.55
10	294	0	.	1	0	.	294	1	0.98	1	50.28
10	295	1	.	1	0	1	295	1	1.26	2	50.28
10	296	0	0	0	0	1	294	1	1.40	1	96.08
10	297	1	0	1	0	1	295	1	1.54	2	96.08
10	298	0	.	1	0	1	298	0	1.54	2	50.28
10	299	0	0	0	0	1	298	0	1.40	1	96.08
10	300	0	0	0	0	1	298	0	1.54	0	96.08
10	301	1	1	1	1	2	298	0	1.54	1	80.81
10	302	0	1	1	0	2	298	0	1.40	1	80.81
10	303	0	.	1	0	.	303	0	0.98	1	50.28
10	304	0	.	1	0	3	304	0	1.12	1	80.81
10	305	0	.	0	1	.	305	0	0.84	1	50.28
10	306	0	0	0	0	2	305	0	1.12	1	96.08
10	307	1	1	0	0	2	305	0	1.12	1	96.08
10	308	1	0	1	0	2	305	0	1.12	1	96.08
10	309	0	1	1	0	1	305	0	1.12	1	96.08
10	310	0	0	0	0	2	305	0	1.12	1	50.28
10	311	0	.	0	0	1	311	0	1.26	1	96.08
10	312	0	.	1	1	.	312	0	0.98	1	80.81

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	262	290.16	0.82	1.22	0.82	1.22	1	0	0	1.25
10	263	73.18	0.83	1.20	0.83	1.20	1	0	0	1.22
10	264	73.44	0.86	1.17	0.86	1.17	1	0	0	1.20
10	265	299.07	0.85	1.18	0.85	1.18	1	0	0	1.17
10	266	76.71	0.82	1.21	0.82	1.21	1	0	0	1.18
10	267	302.74	0.85	1.18	0.82	1.21	0		1	.
10	268	78.85	0.86	1.16	0.82	1.21	0		0	.
10	269	77.01	0.86	1.16	0.82	1.21	0		0	.
10	270	75.51	0.87	1.15	0.82	1.21	0		0	.
10	271	94.30	1.10	0.91	1.10	0.91	1	2	0	1.21
10	273	48.22	0.78	1.29	0.78	1.29	1	0	0	1.21
10	274	80.68	0.79	1.27	0.78	1.29	0		1	.
10	275	85.29	0.77	1.30	0.77	1.30	1	0	0	1.29
10	276	51.75	0.78	1.28	0.77	1.30	0		1	.
10	277	87.99	0.79	1.27	0.79	1.27	1	1	0	1.30
10	278	316.18	0.79	1.26	0.79	1.27	0		1	.
10	279	317.55	0.79	1.26	0.79	1.26	1	0	0	1.27
10	280	82.72	0.79	1.27	0.79	1.27	1	0	0	1.26
10	281	322.12	0.78	1.28	0.77	1.30	0		1	.
10	282	321.36	0.77	1.30	0.77	1.30	1	0	0	1.27
10	283	87.82	0.79	1.26	0.77	1.30	0		0	.
10	284	84.45	0.78	1.28	0.78	1.28	1	0	0	1.30
10	285	87.09	0.79	1.27	0.78	1.29	0		1	.
10	286	86.02	0.78	1.29	0.78	1.29	1	0	0	1.28
10	287	81.98	0.77	1.29	0.78	1.29	0		0	.
10	288	86.39	0.78	1.28	0.78	1.29	0		0	.
10	289	330.10	0.78	1.28	0.78	1.28	1	0	0	1.29
10	290	329.20	0.80	1.25	0.78	1.28	0		1	.
10	291	330.70	0.80	1.25	0.78	1.28	0		0	.
10	292	90.23	0.81	1.23	0.81	1.23	1	1	0	1.28
10	293	92.39	0.81	1.23	0.81	1.23	1	0	0	1.23
10	294	336.44	0.78	1.29	0.78	1.29	1	2	0	1.23
10	295	336.67	0.74	1.34	0.74	1.34	1	3	0	1.23
10	296	63.67	0.77	1.29	0.78	1.29	0		1	.
10	297	62.43	0.75	1.34	0.74	1.34	0		1	.
10	298	343.11	0.76	1.32	0.76	1.32	1	1	0	1.23
10	299	58.66	0.76	1.32	0.76	1.32	0		1	.
10	300	57.59	0.78	1.28	0.76	1.32	0		0	.
10	301	94.16	0.80	1.26	0.76	1.32	0		0	.
10	302	95.63	0.81	1.24	0.76	1.32	0		0	.
10	303	348.62	0.82	1.22	0.82	1.22	1	0	0	1.32
10	304	98.10	0.83	1.20	0.83	1.20	1	0	0	1.22
10	305	351.72	0.81	1.23	0.81	1.23	1	0	0	1.20
10	306	67.80	0.82	1.22	0.81	1.23	0		1	.
10	307	68.57	0.83	1.21	0.81	1.23	0		0	.
10	308	70.47	0.83	1.20	0.81	1.23	0		0	.
10	309	69.84	0.83	1.20	0.81	1.23	0		0	.
10	310	357.09	0.85	1.18	0.81	1.23	0		0	.
10	311	71.24	0.85	1.17	0.85	1.17	1	0	0	1.23
10	312	102.17	0.83	1.20	0.83	1.20	1	0	0	1.17

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	313	0	.	1	0	.	313	0	0.98	1	80.81
10	314	1	1	1	0	1	313	0	1.12	1	80.81
10	315	1	.	1	0	.	315	0	0.98	1	65.55
10	316	0	1	1	0	2	315	0	1.12	0	65.55
10	317	1	.	1	0	.	317	0	0.98	1	65.55
10	318	0	1	1	0	1	317	0	1.12	2	80.81
10	319	1	1	1	0	1	317	0	1.40	1	80.81
10	320	1	0	1	0	1	317	0	1.54	2	96.08
10	321	1	.	0	0	1	321	0	1.54	1	80.81
10	322	0	.	1	0	1	322	0	1.54	2	96.08
10	323	0	0	0	0	1	322	0	1.54	2	80.81
10	324	0	0	1	0	1	322	0	1.68	1	80.81
10	325	1	1	1	0	1	322	0	1.83	1	80.81
10	326	0	1	0	0	1	322	0	1.54	2	80.81
10	327	0	0	0	0	1	322	0	1.68	1	35.02
10	328	0	0	1	0	1	322	0	1.68	1	65.55
10	331	1	.	1	0	1	331	0	1.68	1	65.55
10	332	0	.	1	0	2	332	0	1.68	1	65.55
10	333	1	.	1	0	.	333	0	1.26	1	96.08
10	334	0	1	1	0	2	333	0	1.26	1	80.81
10	335	0	0	0	0	2	333	0	1.12	0	65.55
10	336	1	.	1	0	.	336	0	0.98	0	65.55
10	337	1	0	1	0	1	336	0	1.26	0	65.55
10	338	0	1	1	0	1	336	0	1.40	1	65.55
10	339	1	1	0	0	1	336	0	1.26	1	96.08
10	340	0	1	1	0	1	336	0	1.26	0	96.08
10	341	0	0	1	0	1	336	0	1.54	1	96.08
10	342	1	.	1	1	.	342	0	1.26	2	96.08
10	343	0	1	0	0	1	342	0	1.40	1	65.55
10	344	1	1	1	0	2	342	0	1.26	1	80.81
10	345	1	.	1	0	.	345	0	1.12	1	80.81
10	346	0	.	1	0	.	346	0	1.12	2	96.08
10	347	0	0	0	0	1	346	0	1.12	0	80.81
10	348	1	1	1	0	1	346	0	1.40	2	96.08
10	349	0	1	1	0	1	346	0	1.54	0	80.81
10	350	1	0	1	0	1	346	0	1.40	1	80.81
10	351	1	1	1	0	1	346	0	1.68	2	80.81
10	352	1	0	1	0	1	346	0	1.68	1	80.81
10	353	1	0	1	1	1	346	0	1.68	1	80.81
10	354	1	0	1	0	1	346	0	1.68	2	96.08
10	355	1	0	1	0	1	346	0	1.68	1	80.81
10	356	0	1	1	0	1	346	0	1.68	2	96.08
10	357	0	0	1	0	1	346	0	1.97	1	96.08
10	358	1	1	1	0	1	346	0	1.83	2	96.08
10	359	1	0	1	0	1	346	0	1.68	1	80.81
10	360	0	1	0	0	1	346	0	1.97	2	96.08
10	361	1	1	1	1	1	346	0	1.97	1	80.81
10	362	0	1	1	0	1	346	0	1.83	1	80.81
10	363	1	1	0	0	1	346	0	1.97	2	80.81
10	364	0	1	0	0	1	346	0	1.83	1	80.81

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	313	107.08	0.81	1.24	0.81	1.24	1	0	0	1.20
10	314	105.07	0.82	1.22	0.81	1.24	0		1	.
10	315	112.11	0.80	1.25	0.80	1.25	1	0	0	1.24
10	316	114.28	0.80	1.25	0.80	1.25	0		1	.
10	317	123.79	0.79	1.27	0.79	1.27	1	0	0	1.25
10	318	110.48	0.75	1.33	0.79	1.27	0		1	.
10	319	110.21	0.77	1.29	0.79	1.27	0		0	.
10	320	74.28	0.75	1.33	0.79	1.27	0		0	.
10	321	113.25	0.57	1.75	0.57	1.75	1	3	0	1.34
10	322	76.01	0.76	1.32	0.76	1.32	1	1	0	1.27
10	323	317.05	0.76	1.32	0.76	1.32	0		0	.
10	324	116.39	0.74	1.34	0.76	1.32	0		1	.
10	325	119.02	0.76	1.32	0.76	1.32	0		0	.
10	326	319.76	0.77	1.30	0.76	1.32	0		0	.
10	327	310.78	0.74	1.34	0.76	1.32	0		0	.
10	328	315.38	0.78	1.29	0.76	1.32	0		0	.
10	331	317.85	0.75	1.34	0.75	1.34	1	4	0	1.32
10	332	319.12	0.75	1.34	0.75	1.34	1	4	0	1.34
10	333	72.61	0.73	1.37	0.73	1.37	1	0	0	1.34
10	334	314.78	0.74	1.35	0.73	1.37	0		1	.
10	335	330.57	0.74	1.35	0.73	1.37	0		0	.
10	336	327.33	0.71	1.40	0.71	1.40	1	0	0	1.37
10	337	323.29	0.71	1.41	0.71	1.40	0		1	.
10	338	337.74	0.72	1.38	0.71	1.40	0		0	.
10	339	76.41	0.72	1.38	0.71	1.40	0		0	.
10	340	78.08	0.72	1.38	0.71	1.40	0		0	.
10	341	79.88	0.73	1.37	0.71	1.40	0		0	.
10	342	81.98	0.71	1.41	0.71	1.41	1	0	0	1.40
10	343	345.45	0.72	1.40	0.71	1.41	0		1	.
10	344	327.40	0.72	1.40	0.71	1.41	0		0	.
10	345	330.07	0.70	1.42	0.70	1.42	1	0	0	1.41
10	346	84.72	0.64	1.56	0.64	1.56	1	0	0	1.42
10	347	334.70	0.66	1.51	0.64	1.56	0		1	.
10	348	83.09	0.67	1.50	0.64	1.56	0		0	.
10	349	350.95	0.69	1.45	0.64	1.56	0		0	.
10	350	332.57	0.66	1.51	0.64	1.56	0		0	.
10	351	353.06	0.69	1.46	0.64	1.56	0		0	.
10	352	353.59	0.70	1.43	0.64	1.56	0		0	.
10	353	355.66	0.71	1.41	0.64	1.56	0		0	.
10	354	88.39	0.69	1.45	0.64	1.56	0		0	.
10	355	357.73	0.72	1.38	0.64	1.56	0		0	.
10	356	86.69	0.72	1.39	0.64	1.56	0		0	.
10	357	90.19	0.72	1.39	0.64	1.56	0		0	.
10	358	92.13	0.72	1.40	0.64	1.56	0		0	.
10	359	362.50	0.72	1.38	0.64	1.56	0		0	.
10	360	96.93	0.73	1.36	0.64	1.56	0		0	.
10	361	364.20	0.71	1.40	0.64	1.56	0		0	.
10	362	366.40	0.72	1.38	0.64	1.56	0		0	.
10	363	366.74	0.72	1.38	0.64	1.56	0		0	.
10	364	369.71	0.73	1.37	0.64	1.56	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	365	1	1	1	0	2	346	0	1.68	1	111.35
10	366	0	.	1	1	1	366	0	1.54	0	80.81
10	367	0	.	1	1	1	367	0	1.68	1	80.81
10	368	1	0	1	0	2	369	0	1.54	2	80.81
10	369	1	.	1	0	1	369	0	1.54	1	80.81
10	370	1	0	1	0	1	369	0	1.68	2	80.81
10	371	1	0	0	0	1	369	0	1.83	1	80.81
10	372	0	1	1	0	1	369	0	1.68	1	80.81
10	373	0	.	1	0	1	373	0	1.68	2	80.81
10	374	0	0	0	0	1	373	0	1.54	1	80.81
10	375	1	.	1	0	.	375	0	1.54	1	80.81
10	376	1	0	0	0	1	375	0	1.68	0	80.81
10	377	1	.	1	0	1	377	0	1.97	1	80.81
10	378	0	.	0	0	1	378	0	1.83	2	80.81
10	379	0	0	0	0	1	378	0	1.40	1	111.35
10	380	0	.	0	0	1	380	0	1.12	2	80.81
10	381	0	0	1	0	1	380	0	1.26	1	96.08
10	382	1	.	1	0	2	382	0	1.26	1	111.35
10	383	0	1	0	0	1	382	0	1.12	1	111.35
10	384	1	1	1	0	1	382	0	1.12	0	111.35
10	385	0	1	0	0	1	382	0	1.26	1	96.08
10	386	0	0	0	0	1	382	0	1.12	1	111.35
10	387	0	.	1	0	2	387	0	0.98	1	80.81
10	388	1	1	0	1	1	387	0	1.12	0	111.35
10	389	1	.	1	0	.	389	0	0.98	1	111.35
10	390	1	.	1	0	.	390	0	0.84	0	96.08
10	391	0	1	1	0	2	390	0	0.98	1	111.35
10	392	1	1	1	0	2	390	0	0.98	1	111.35
10	393	1	0	1	1	2	390	0	0.98	1	96.08
10	394	1	0	1	0	2	390	0	0.98	1	96.08
10	395	1	.	1	1	.	395	0	0.98	1	96.08
10	396	1	0	1	0	1	395	0	1.12	1	96.08
10	397	1	0	1	0	1	395	0	1.12	1	96.08
10	398	0	1	0	0	1	395	0	1.12	1	111.35
10	399	0	.	1	0	2	399	0	1.12	1	111.35
10	400	0	0	1	0	1	399	0	1.12	0	111.35
10	401	0	0	0	0	1	399	0	1.12	0	111.35
10	402	0	.	0	0	.	402	0	0.98	1	111.35
10	403	1	1	0	0	1	402	0	1.12	1	111.35
10	404	0	1	1	0	1	402	0	1.12	1	111.35
10	405	0	0	1	0	2	402	0	1.12	1	96.08
10	406	1	1	0	0	1	402	0	1.12	1	96.08
10	407	1	0	1	0	1	402	0	1.26	1	96.08
10	408	0	.	1	0	.	408	0	1.12	1	111.35
10	409	1	.	0	0	.	409	0	0.98	0	111.35
10	410	0	.	1	0	.	410	0	0.98	1	111.35
10	411	1	1	1	0	1	410	0	1.26	2	111.35
10	412	0	1	1	0	1	410	0	1.40	1	111.35
10	413	0	.	1	0	1	413	0	1.12	1	111.35
10	414	1	.	1	1	.	414	0	0.98	1	111.35

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	365	85.59	0.74	1.34	0.64	1.56	0		0	.
10	366	374.71	0.71	1.40	0.71	1.40	1	3	0	1.56
10	367	375.98	0.77	1.29	0.77	1.29	1	2	0	1.56
10	368	378.38	0.75	1.33	0.76	1.32	0		1	.
10	369	377.78	0.76	1.32	0.76	1.32	1	0	0	1.56
10	370	380.48	0.75	1.33	0.76	1.32	0		0	.
10	371	380.42	0.76	1.32	0.76	1.32	0		0	.
10	372	382.62	0.76	1.31	0.76	1.32	0		0	.
10	373	385.32	0.77	1.30	0.77	1.30	1	0	0	1.32
10	374	384.42	0.76	1.31	0.77	1.30	0		1	.
10	375	386.69	0.72	1.40	0.72	1.40	1	3	0	1.30
10	376	388.59	0.74	1.34	0.72	1.40	0		1	.
10	377	389.39	0.76	1.32	0.76	1.32	1	2	0	1.30
10	378	392.23	0.76	1.31	0.76	1.31	1	1	0	1.30
10	379	88.12	0.77	1.29	0.76	1.31	0		1	.
10	380	396.50	0.76	1.31	0.76	1.31	1	1	0	1.31
10	381	93.80	0.77	1.30	0.76	1.31	0		1	.
10	382	87.02	0.76	1.31	0.76	1.31	1	0	0	1.31
10	383	88.99	0.77	1.29	0.76	1.31	0		1	.
10	384	92.90	0.77	1.29	0.76	1.31	0		0	.
10	385	102.47	0.78	1.28	0.76	1.31	0		0	.
10	386	95.67	0.78	1.28	0.76	1.31	0		0	.
10	387	408.84	0.78	1.29	0.78	1.29	1	0	0	1.31
10	388	91.03	0.78	1.28	0.78	1.29	0		0	.
10	389	101.60	0.76	1.32	0.76	1.32	1	0	0	1.29
10	390	106.14	0.72	1.39	0.72	1.39	1	0	0	1.32
10	391	109.58	0.73	1.37	0.72	1.39	0		1	.
10	392	106.74	0.71	1.40	0.72	1.39	0		0	.
10	393	109.78	0.72	1.38	0.72	1.39	0		0	.
10	394	112.38	0.72	1.39	0.72	1.39	0		0	.
10	395	116.65	0.69	1.44	0.69	1.44	1	0	0	1.39
10	396	118.35	0.69	1.45	0.69	1.44	0		1	.
10	397	121.16	0.69	1.44	0.69	1.44	0		0	.
10	398	112.11	0.70	1.43	0.69	1.44	0		0	.
10	399	114.62	0.72	1.40	0.72	1.40	1	1	0	1.44
10	400	115.49	0.71	1.40	0.72	1.40	0		1	.
10	401	116.72	0.73	1.38	0.72	1.40	0		0	.
10	402	118.55	0.72	1.39	0.72	1.39	1	0	0	1.40
10	403	118.35	0.73	1.37	0.72	1.39	0		1	.
10	404	121.46	0.73	1.36	0.72	1.39	0		0	.
10	405	342.58	0.76	1.32	0.72	1.39	0		0	.
10	406	342.78	0.77	1.30	0.72	1.39	0		0	.
10	407	308.14	0.78	1.29	0.72	1.39	0		0	.
10	408	126.73	0.77	1.30	0.77	1.30	1	0	0	1.39
10	409	152.72	0.77	1.30	0.77	1.30	1	0	0	1.30
10	410	152.63	0.72	1.38	0.72	1.38	1	0	0	1.30
10	411	158.46	0.72	1.39	0.72	1.38	0		1	.
10	412	347.22	0.73	1.37	0.72	1.38	0		0	.
10	413	350.65	0.73	1.37	0.73	1.37	1	0	0	1.38
10	414	396.47	0.71	1.41	0.71	1.41	1	0	0	1.37

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	415	1	0	1	0	2	414	0	1.12	1	111.35
10	416	1	0	1	0	1	414	0	1.12	1	111.35
10	417	1	0	1	0	2	414	0	0.98	1	111.35
10	418	0	1	1	0	2	414	0	0.98	1	111.35
10	419	0	.	0	0	2	419	0	0.84	1	111.35
10	420	1	.	0	0	1	420	0	0.98	1	50.28
10	421	0	1	1	0	2	420	0	0.98	1	50.28
10	422	1	.	1	1	3	422	0	0.98	1	111.35
10	423	1	.	1	0	1	423	0	1.12	1	111.35
10	424	1	0	0	0	1	423	0	1.12	1	111.35
10	425	1	.	0	0	2	425	0	0.98	1	80.81
10	426	1	0	0	0	1	425	0	1.12	1	111.35
10	427	0	.	1	0	2	427	0	1.12	2	80.81
10	428	0	.	0	0	2	428	0	0.98	0	65.55
10	429	1	.	1	0	2	429	0	1.26	0	111.35
10	430	0	.	0	0	.	430	0	0.28	0	65.55
10	431	0	0	1	0	2	430	0	0.56	0	65.55
10	432	0	.	1	0	.	432	0	0.28	0	80.81
10	2.01	0	.	1	0	.	2	0	0.28	0	35.02
10	25.01	0	.	1	0	.	25	0	1.26	1	19.75
10	26.01	0	.	0	0	1	26	0	1.26	0	19.75
10	28.01	0	.	1	0	1	28	0	1.68	0	19.75
10	30.01	0	.	1	0	1	30	0	1.54	1	19.75
10	46.01	0	.	0	0	.	46	0	1.12	0	19.75
10	50.01	0	.	0	0	.	50	0	1.40	0	19.75
10	52.01	0	.	1	0	1	52	0	1.68	2	19.75
10	54.01	0	.	0	0	1	54	0	1.26	1	19.75
10	57.01	1	.	1	0	2	57	0	1.26	0	4.49
10	60.01	0	.	0	0	1	60	0	1.83	2	19.75
10	63.01	0	.	0	0	1	63	0	1.68	0	4.49
10	69.01	1	.	1	0	1	69	0	1.68	1	4.49
10	70.01	1	.	0	0	1	70	0	2.25	2	4.49
10	72.01	1	.	1	0	1	72	0	2.25	0	4.49
10	77.01	0	.	0	0	.	77	0	2.67	2	19.75
10	81.01	0	.	0	0	1	81	0	2.53	2	19.75
10	87.01	0	.	1	0	1	87	1	2.81	0	4.49
10	89.01	0	.	0	0	1	89	1	2.95	2	19.75
10	102.01	1	1	1	0	1	89	1	2.95	2	35.02
10	103.01	1	0	1	0	1	89	1	3.09	2	19.75
10	104.01	1	.	0	0	1	104	1	2.53	1	4.49
10	105.01	1	0	1	0	1	108	1	2.95	1	4.49
10	108.01	1	.	1	1	1	108	1	2.67	1	4.49
10	109.01	1	.	1	0	1	109	1	2.95	2	19.75
10	114.01	1	.	1	0	1	114	1	2.67	1	4.49
10	117.01	0	.	1	0	1	117	1	3.23	1	4.49
10	126.01	1	.	0	0	1	126	0	2.81	0	4.49
10	130.01	0	.	0	0	1	130	0	2.95	0	4.49
10	134.01	0	.	1	0	1	134	0	2.95	1	19.75
10	135.01	0	0	1	1	1	134	0	2.95	2	19.75
10	137.01	1	.	1	0	1	137	0	3.09	2	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	415	400.67	0.70	1.43	0.71	1.41	0		1	.
10	416	403.17	0.71	1.40	0.71	1.41	0		0	.
10	417	405.31	0.72	1.38	0.71	1.41	0		0	.
10	418	407.01	0.74	1.35	0.71	1.41	0		0	.
10	419	409.51	0.74	1.36	0.74	1.36	1	0	0	1.41
10	420	519.15	0.74	1.36	0.74	1.36	1	1	0	1.36
10	421	520.59	0.75	1.33	0.74	1.36	0		1	.
10	422	411.08	0.76	1.31	0.76	1.31	1	0	0	1.36
10	423	412.95	0.76	1.31	0.76	1.31	1	0	0	1.31
10	424	414.22	0.76	1.31	0.76	1.31	0		1	.
10	425	473.48	0.80	1.25	0.80	1.25	1	0	0	1.31
10	426	415.82	0.81	1.23	0.80	1.25	0		1	.
10	427	477.05	0.85	1.18	0.85	1.18	1	2	0	1.25
10	428	385.65	0.77	1.30	0.77	1.30	1	3	0	1.25
10	429	416.89	0.83	1.21	0.83	1.21	1	0	0	1.25
10	430	728.23	1.06	0.95	1.06	0.95	1	0	0	1.21
10	431	729.30	1.04	0.96	1.06	0.95	0		1	.
10	432	774.08	1.19	0.84	1.19	0.84	1	0	0	0.95
10	2.01	11.15	1.41	0.71	1.41	0.71	1	0	0	.
10	25.01	40.14	1.01	0.99	1.01	0.99	1	1	0	0.71
10	26.01	41.81	0.99	1.01	0.99	1.01	1	1	0	0.99
10	28.01	44.15	1.01	0.99	1.01	0.99	1	1	0	1.02
10	30.01	43.01	0.98	1.02	0.98	1.02	1	1	0	1.01
10	46.01	51.42	0.98	1.02	0.98	1.02	1	1	0	0.99
10	50.01	53.62	0.96	1.04	0.96	1.04	1	1	0	1.02
10	52.01	56.12	0.99	1.01	0.99	1.01	1	2	0	1.05
10	54.01	54.86	0.95	1.05	0.95	1.05	1	4	0	1.04
10	57.01	56.09	0.90	1.11	0.90	1.11	1	3	0	1.05
10	60.01	57.49	0.86	1.16	0.86	1.16	1	2	0	1.05
10	63.01	57.23	0.81	1.24	0.81	1.24	1	3	0	1.05
10	69.01	58.93	0.80	1.25	0.80	1.25	1	4	0	1.05
10	70.01	61.36	0.79	1.27	0.79	1.27	1	2	0	1.25
10	72.01	60.30	0.75	1.34	0.75	1.34	1	3	0	1.25
10	77.01	60.43	0.75	1.34	0.75	1.34	1	1	0	1.25
10	81.01	61.96	0.62	1.61	0.62	1.61	1	2	0	1.34
10	87.01	63.13	0.56	1.79	0.56	1.79	1	2	0	1.34
10	89.01	63.23	0.56	1.80	0.56	1.80	1	2	0	1.34
10	102.01	39.71	0.51	1.97	0.56	1.80	0		1	.
10	103.01	67.17	0.50	2.01	0.56	1.80	0		0	.
10	104.01	62.40	0.54	1.84	0.54	1.84	1	3	0	1.34
10	105.01	66.17	0.46	2.20	0.45	2.25	0		1	.
10	108.01	64.47	0.45	2.25	0.45	2.25	1	3	0	1.34
10	109.01	68.60	0.47	2.12	0.47	2.12	1	2	0	1.34
10	114.01	69.34	0.40	2.49	0.40	2.49	1	3	0	1.34
10	117.01	67.30	0.43	2.31	0.43	2.31	1	3	0	1.34
10	126.01	70.71	0.35	2.86	0.35	2.86	1	3	0	1.34
10	130.01	72.14	0.33	3.00	0.33	3.00	1	3	0	1.34
10	134.01	70.67	0.32	3.08	0.32	3.08	1	1	0	1.34
10	135.01	71.41	0.32	3.10	0.32	3.08	0		1	.
10	137.01	73.58	0.32	3.17	0.32	3.17	1	4	0	3.08

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	139.01	1	.	1	0	1	139	1	3.23	2	19.75
10	142.01	1	0	1	0	.	139	1	2.95	2	19.75
10	146.01	0	.	0	0	1	146	0	2.81	2	19.75
10	149.01	0	.	1	0	1	149	0	3.09	1	4.49
10	152.01	0	.	1	0	1	152	0	2.95	1	4.49
10	153.01	0	.	1	0	1	153	0	3.09	0	4.49
10	155.01	1	.	1	0	1	155	0	2.95	0	4.49
10	160.01	0	.	0	0	1	160	0	3.23	0	4.49
10	161.01	0	.	1	1	1	161	0	3.09	2	4.49
10	169.01	0	.	0	0	1	169	0	3.09	1	4.49
10	174.01	0	0	0	0	1	175	0	2.95	2	19.75
10	175.01	0	.	0	0	1	175	0	2.67	1	19.75
10	176.01	0	0	1	0	1	175	0	3.09	0	4.49
10	181.01	1	.	0	1	1	181	0	2.67	2	35.02
10	183.01	1	.	1	0	1	183	0	2.81	2	35.02
10	185.01	1	.	0	0	1	185	0	2.67	1	19.75
10	186.01	1	.	1	0	1	186	0	2.81	0	4.49
10	187.01	1	0	1	1	1	185	0	2.81	0	19.75
10	192.01	1	.	0	1	1	192	0	2.95	2	19.75
10	194.01	0	.	1	0	1	194	1	2.95	0	35.02
10	195.01	0	.	0	0	.	195	1	2.67	0	4.49
10	196.01	0	.	1	0	1	196	1	2.81	1	4.49
10	197.01	0	.	1	0	1	197	1	2.81	2	35.02
10	199.01	0	.	0	0	1	199	1	2.81	1	4.49
10	200.01	0	.	0	0	1	200	1	2.95	0	4.49
10	201.01	0	0	1	0	1	199	1	2.95	1	4.49
10	205.01	0	.	0	0	1	205	0	3.23	1	4.49
10	206.01	0	.	1	0	1	206	0	2.95	0	4.49
10	207.01	1	.	1	0	1	207	0	2.95	1	4.49
10	210.01	0	.	1	0	1	210	0	2.81	0	19.75
10	214.01	0	.	1	0	1	214	0	2.67	1	19.75
10	217.01	0	.	1	0	1	217	0	2.67	0	35.02
10	218.01	1	.	0	0	.	218	0	2.67	1	4.49
10	219.01	1	0	0	0	1	218	0	2.67	1	35.02
10	221.01	1	.	0	0	1	221	0	2.39	1	35.02
10	223.01	0	.	0	0	1	223	0	2.67	1	19.75
10	224.01	0	.	1	0	1	224	0	2.39	0	19.75
10	225.01	0	.	1	0	1	225	0	2.53	1	4.49
10	226.01	1	1	1	0	1	225	0	2.81	1	50.28
10	227.01	0	1	0	0	1	225	0	2.67	1	4.49
10	228.01	1	1	0	0	1	225	0	2.67	1	35.02
10	229.01	0	1	1	0	1	225	0	2.39	1	4.49
10	230.01	0	0	1	0	1	225	0	2.39	0	4.49
10	231.01	0	0	1	1	1	225	0	2.81	1	50.28
10	232.01	1	.	1	1	1	232	0	2.53	1	19.75
10	233.01	0	.	1	0	1	233	0	2.25	1	4.49
10	234.01	0	.	0	0	1	234	0	2.53	0	4.49
10	235.01	0	0	1	0	1	233	0	2.25	1	4.49
10	236.01	0	.	0	0	1	236	1	2.39	2	4.49
10	237.01	0	.	1	0	1	237	1	2.81	0	35.02

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	139.01	75.11	0.31	3.27	0.31	3.27	1	2	0	3.17
10	142.01	77.65	0.30	3.30	0.31	3.27	0		1	.
10	146.01	79.38	0.28	3.52	0.28	3.52	1	2	0	3.17
10	149.01	74.34	0.26	3.91	0.26	3.91	1	3	0	3.17
10	152.01	76.51	0.25	4.02	0.25	4.02	1	3	0	3.17
10	153.01	80.48	0.25	4.06	0.25	4.06	1	3	0	3.17
10	155.01	78.51	0.24	4.20	0.24	4.20	1	3	0	3.17
10	160.01	82.22	0.24	4.15	0.24	4.15	1	4	0	3.17
10	161.01	82.75	0.24	4.22	0.24	4.22	1	4	0	4.15
10	169.01	84.39	0.22	4.63	0.22	4.63	1	4	0	4.22
10	174.01	81.35	0.21	4.83	0.21	4.84	0		1	.
10	175.01	81.02	0.21	4.84	0.21	4.84	1	0	0	4.63
10	176.01	85.45	0.21	4.83	0.21	4.84	0		0	.
10	181.01	50.52	0.20	4.93	0.20	4.93	1	4	0	4.84
10	183.01	52.32	0.20	4.93	0.20	4.93	1	2	0	4.93
10	185.01	84.19	0.20	5.02	0.20	5.02	1	1	0	4.93
10	186.01	87.29	0.20	5.04	0.20	5.04	1	3	0	4.93
10	187.01	86.55	0.20	5.03	0.20	5.02	0		1	.
10	192.01	88.39	0.19	5.20	0.19	5.20	1	2	0	5.02
10	194.01	54.02	0.19	5.26	0.19	5.26	1	2	0	5.02
10	195.01	91.46	0.18	5.41	0.18	5.41	1	3	0	5.02
10	196.01	89.12	0.18	5.44	0.18	5.44	1	3	0	5.02
10	197.01	55.99	0.19	5.30	0.19	5.30	1	2	0	5.02
10	199.01	95.30	0.18	5.50	0.18	5.50	1	3	0	5.02
10	200.01	99.23	0.19	5.39	0.19	5.39	1	2	0	5.02
10	201.01	97.83	0.18	5.48	0.18	5.50	0		1	.
10	205.01	101.04	0.18	5.50	0.18	5.50	1	1	0	5.02
10	206.01	107.64	0.20	4.90	0.20	4.90	1	2	0	5.50
10	207.01	102.54	0.18	5.48	0.18	5.48	1	3	0	5.50
10	210.01	92.03	0.17	5.72	0.17	5.72	1	3	0	5.50
10	214.01	94.00	0.17	5.75	0.17	5.75	1	2	0	5.50
10	217.01	59.06	0.17	6.05	0.17	6.05	1	3	0	5.50
10	218.01	104.41	0.17	5.86	0.17	5.86	1	0	0	5.50
10	219.01	57.59	0.17	5.78	0.17	5.86	0		1	.
10	221.01	59.63	0.17	5.87	0.17	5.87	1	4	0	5.86
10	223.01	101.54	0.17	5.75	0.17	5.75	1	2	0	5.87
10	224.01	100.30	0.17	6.03	0.17	6.03	1	3	0	5.87
10	225.01	116.18	0.22	4.51	0.22	4.51	1	1	0	5.87
10	226.01	58.93	0.23	4.34	0.22	4.51	0		1	.
10	227.01	120.09	0.26	3.78	0.22	4.51	0		0	.
10	228.01	63.27	0.27	3.65	0.22	4.51	0		0	.
10	229.01	136.50	0.29	3.44	0.22	4.51	0		0	.
10	230.01	176.61	0.30	3.35	0.22	4.51	0		0	.
10	231.01	62.10	0.40	2.52	0.22	4.51	0		0	.
10	232.01	111.81	0.43	2.33	0.43	2.33	1	2	0	4.51
10	233.01	207.64	0.44	2.29	0.44	2.29	1	1	0	4.51
10	234.01	182.75	0.39	2.55	0.39	2.55	1	3	0	4.51
10	235.01	239.64	0.45	2.23	0.44	2.29	0		1	.
10	236.01	242.68	0.53	1.88	0.53	1.88	1	2	0	2.29
10	237.01	66.17	0.47	2.14	0.47	2.14	1	3	0	2.29

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	238.01	0	0	1	0	1	236	1	2.81	0	4.49
10	239.01	1	1	1	0	1	237	1	2.25	0	4.49
10	240.01	1	1	1	0	1	236	1	2.67	0	4.49
10	241.01	0	1	1	0	1	237	1	2.95	1	35.02
10	244.01	1	.	1	0	1	244	1	2.81	1	35.02
10	245.01	0	1	1	0	1	236	1	2.39	0	4.49
10	246.01	1	.	1	0	1	246	0	2.53	1	19.75
10	247.01	0	1	0	0	1	246	0	2.53	2	4.49
10	248.01	1	1	1	0	1	246	0	2.39	1	19.75
10	249.01	1	.	1	0	1	249	0	2.53	0	4.49
10	250.01	1	.	1	0	1	250	0	2.53	0	35.02
10	251.01	0	1	0	0	1	249	0	2.53	0	35.02
10	252.01	1	1	1	0	1	249	0	2.81	1	4.49
10	253.01	1	.	1	1	1	253	0	2.25	1	19.75
10	254.01	1	.	0	0	2	254	0	2.67	0	4.49
10	255.01	1	.	1	0	1	255	0	2.53	1	4.49
10	256.01	0	.	1	0	1	256	0	2.39	1	19.75
10	257.01	0	0	0	0	1	256	0	2.53	2	35.02
10	258.01	1	1	1	0	1	256	0	2.81	1	50.28
10	259.01	0	1	1	0	1	256	0	2.81	1	50.28
10	260.01	1	1	1	0	1	256	0	2.81	1	50.28
10	261.01	1	0	1	0	2	256	0	2.25	1	19.75
10	262.01	0	1	1	0	1	256	0	2.11	1	19.75
10	263.01	0	0	0	0	2	256	0	1.83	1	35.02
10	264.01	0	.	1	0	3	264	0	1.54	1	50.28
10	265.01	0	0	0	0	2	264	0	1.40	1	19.75
10	266.01	1	1	0	0	1	264	0	1.40	1	35.02
10	267.01	0	1	1	0	2	264	0	1.54	1	19.75
10	268.01	0	0	0	0	1	264	0	1.54	1	35.02
10	269.01	0	0	1	0	2	264	0	1.54	1	50.28
10	270.01	0	0	1	0	1	264	0	1.68	1	50.28
10	271.01	1	.	1	0	1	271	0	2.53	2	35.02
10	273.01	0	0	1	1	1	264	0	1.68	1	65.55
10	274.01	1	1	1	0	2	264	0	1.68	1	35.02
10	275.01	1	.	1	0	.	275	0	1.83	1	50.28
10	276.01	1	.	1	0	1	276	0	1.83	1	65.55
10	277.01	1	.	1	0	1	277	0	1.83	0	35.02
10	278.01	0	1	0	0	1	277	0	1.83	1	19.75
10	279.01	1	1	1	0	1	277	0	1.83	1	19.75
10	280.01	0	1	1	0	1	277	0	1.83	1	35.02
10	281.01	0	.	0	0	1	281	0	2.25	0	19.75
10	282.01	0	.	1	0	2	282	0	1.97	1	19.75
10	283.01	0	.	0	0	1	283	0	2.11	1	50.28
10	284.01	1	1	1	0	1	283	0	1.97	1	35.02
10	285.01	1	.	1	0	1	285	0	2.25	2	50.28
10	286.01	1	0	1	0	1	283	0	2.11	0	50.28
10	287.01	1	.	1	0	1	287	0	2.11	1	50.28
10	288.01	0	1	0	0	1	287	0	2.25	1	35.02
10	289.01	0	.	1	0	1	289	0	2.39	0	19.75
10	290.01	1	.	1	0	1	290	0	2.25	1	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	238.01	257.33	0.63	1.58	0.53	1.88	0		1	.
10	239.01	248.08	0.52	1.93	0.47	2.14	0		1	.
10	240.01	251.82	0.55	1.82	0.53	1.88	0		0	.
10	241.01	64.27	0.52	1.91	0.47	2.14	0		0	.
10	244.01	67.50	0.52	1.93	0.52	1.93	1	3	0	2.29
10	245.01	266.43	0.58	1.74	0.53	1.88	0		0	.
10	246.01	200.44	0.61	1.65	0.61	1.65	1	1	0	2.29
10	247.01	269.04	0.60	1.67	0.61	1.65	0		1	.
10	248.01	216.22	0.61	1.64	0.61	1.65	0		0	.
10	249.01	273.64	0.61	1.63	0.61	1.63	1	3	0	1.65
10	250.01	72.04	0.65	1.53	0.65	1.53	1	2	0	1.65
10	251.01	69.47	0.61	1.63	0.61	1.63	0		1	.
10	252.01	276.81	0.61	1.65	0.61	1.63	0		0	.
10	253.01	250.82	0.60	1.65	0.60	1.65	1	1	0	1.65
10	254.01	284.39	0.65	1.53	0.65	1.53	1	2	0	1.65
10	255.01	279.35	0.62	1.61	0.62	1.61	1	3	0	1.65
10	256.01	267.67	0.64	1.56	0.64	1.56	1	1	0	1.65
10	257.01	70.41	0.62	1.60	0.64	1.56	0		1	.
10	258.01	69.97	0.63	1.58	0.64	1.56	0		0	.
10	259.01	69.81	0.63	1.58	0.64	1.56	0		0	.
10	260.01	71.64	0.64	1.56	0.64	1.56	0		0	.
10	261.01	287.09	0.65	1.54	0.64	1.56	0		0	.
10	262.01	290.16	0.64	1.55	0.64	1.56	0		0	.
10	263.01	73.18	0.64	1.56	0.64	1.56	0		0	.
10	264.01	73.44	0.64	1.56	0.64	1.56	1	0	0	1.56
10	265.01	299.07	0.64	1.57	0.64	1.56	0		1	.
10	266.01	76.71	0.63	1.58	0.64	1.56	0		0	.
10	267.01	302.74	0.63	1.59	0.64	1.56	0		0	.
10	268.01	78.85	0.63	1.59	0.64	1.56	0		0	.
10	269.01	77.01	0.64	1.57	0.64	1.56	0		0	.
10	270.01	75.51	0.62	1.60	0.64	1.56	0		0	.
10	271.01	94.30	0.95	1.06	0.95	1.06	1	2	0	1.63
10	273.01	48.22	0.62	1.61	0.64	1.56	0		0	.
10	274.01	80.68	0.62	1.61	0.64	1.56	0		0	.
10	275.01	85.29	0.61	1.63	0.61	1.63	1	0	0	1.56
10	276.01	51.75	0.61	1.63	0.61	1.63	1	1	0	1.63
10	277.01	87.99	0.61	1.64	0.61	1.64	1	3	0	1.63
10	278.01	316.18	0.61	1.64	0.61	1.64	0		1	.
10	279.01	317.55	0.61	1.65	0.61	1.64	0		0	.
10	280.01	82.72	0.61	1.64	0.61	1.64	0		0	.
10	281.01	322.12	0.51	1.95	0.51	1.95	1	3	0	1.65
10	282.01	321.36	0.60	1.65	0.60	1.65	1	1	0	1.63
10	283.01	87.82	0.61	1.65	0.61	1.65	1	1	0	1.65
10	284.01	84.45	0.61	1.65	0.61	1.65	0		1	.
10	285.01	87.09	0.63	1.58	0.63	1.58	1	2	0	1.65
10	286.01	86.02	0.60	1.67	0.61	1.65	0		0	.
10	287.01	81.98	0.59	1.70	0.59	1.70	1	3	0	1.65
10	288.01	86.39	0.58	1.71	0.59	1.70	0		1	.
10	289.01	330.10	0.59	1.69	0.59	1.69	1	0	0	1.65
10	290.01	329.20	0.59	1.70	0.59	1.70	1	1	0	1.69

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	291.01	1	0	1	0	1	290	0	2.39	1	19.75
10	292.01	0	.	1	0	2	292	0	2.25	1	35.02
10	293.01	1	1	1	0	1	292	0	2.39	0	35.02
10	294.01	0	.	1	0	.	294	0	2.25	1	19.75
10	295.01	1	1	1	0	1	294	0	2.53	2	19.75
10	296.01	0	1	0	0	1	294	0	2.39	1	65.55
10	297.01	1	0	1	0	1	294	0	2.53	2	65.55
10	298.01	0	.	1	0	1	298	0	2.39	2	19.75
10	299.01	0	.	0	0	1	299	0	2.39	1	65.55
10	300.01	0	.	0	0	1	300	0	2.39	1	65.55
10	301.01	1	1	1	1	1	300	0	2.39	1	50.28
10	302.01	0	1	1	0	1	300	0	2.53	1	50.28
10	303.01	0	.	1	0	.	303	0	2.11	1	19.75
10	304.01	0	.	1	0	1	304	0	2.11	1	50.28
10	305.01	0	0	0	1	1	304	0	1.83	1	19.75
10	306.01	0	0	0	0	1	304	0	2.11	1	65.55
10	307.01	1	1	0	0	1	304	0	2.11	1	65.55
10	308.01	1	0	1	0	1	304	0	2.25	1	65.55
10	309.01	0	1	1	0	1	304	0	2.25	1	65.55
10	310.01	0	0	0	0	2	304	0	2.39	1	19.75
10	311.01	0	0	0	0	1	304	0	2.53	1	65.55
10	312.01	0	.	1	1	.	312	0	2.39	1	50.28
10	313.01	0	0	1	0	2	312	0	2.11	1	50.28
10	314.01	1	1	1	0	1	312	0	2.11	1	50.28
10	315.01	1	.	1	0	1	315	0	2.11	1	35.02
10	316.01	0	.	1	0	1	316	0	2.11	1	35.02
10	317.01	1	.	1	0	2	317	0	1.97	1	35.02
10	318.01	0	.	1	0	1	318	0	2.11	2	50.28
10	319.01	1	.	1	0	1	319	0	2.25	1	50.28
10	320.01	1	0	1	0	1	319	0	2.53	2	65.55
10	321.01	1	0	0	0	1	319	0	2.25	0	50.28
10	322.01	0	1	1	0	1	319	0	2.67	2	65.55
10	323.01	0	0	0	0	1	319	0	2.67	2	50.28
10	324.01	0	0	1	0	1	319	0	2.53	1	50.28
10	325.01	1	.	1	0	1	325	0	2.81	1	50.28
10	326.01	0	.	0	0	1	326	0	2.39	2	50.28
10	327.01	0	.	0	0	1	327	0	2.11	1	4.49
10	328.01	0	.	1	0	1	328	0	2.67	1	35.02
10	331.01	1	1	1	0	1	328	0	2.67	1	35.02
10	332.01	0	.	1	0	1	332	0	2.67	1	35.02
10	333.01	1	1	1	0	1	332	0	2.39	1	65.55
10	334.01	0	1	1	0	1	332	0	2.39	1	50.28
10	335.01	0	0	0	0	1	332	0	2.11	0	35.02
10	336.01	1	.	1	0	1	336	0	2.11	0	35.02
10	337.01	1	0	1	0	1	336	0	2.25	1	35.02
10	338.01	0	1	1	0	1	336	0	2.25	1	35.02
10	339.01	1	.	0	0	1	339	0	2.11	1	65.55
10	340.01	0	.	1	0	1	340	0	2.11	2	65.55
10	341.01	0	.	1	0	1	341	0	2.39	1	65.55
10	342.01	1	1	1	1	1	341	0	2.39	2	65.55

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	291.01	330.70	0.59	1.70	0.59	1.70	0		1	.
10	292.01	90.23	0.59	1.69	0.59	1.69	1	0	0	1.70
10	293.01	92.39	0.59	1.71	0.59	1.69	0		1	.
10	294.01	336.44	0.59	1.70	0.59	1.70	1	0	0	1.69
10	295.01	336.67	0.58	1.72	0.59	1.70	0		1	.
10	296.01	63.67	0.59	1.69	0.59	1.70	0		0	.
10	297.01	62.43	0.58	1.72	0.59	1.70	0		0	.
10	298.01	343.11	0.62	1.62	0.62	1.62	1	2	0	1.70
10	299.01	58.66	0.58	1.72	0.58	1.72	1	3	0	1.70
10	300.01	57.59	0.61	1.65	0.61	1.65	1	1	0	1.70
10	301.01	94.16	0.61	1.63	0.61	1.65	0		1	.
10	302.01	95.63	0.60	1.65	0.61	1.65	0		0	.
10	303.01	348.62	0.61	1.65	0.61	1.65	1	0	0	1.65
10	304.01	98.10	0.61	1.65	0.61	1.65	1	0	0	1.65
10	305.01	351.72	0.61	1.63	0.61	1.65	0		1	.
10	306.01	67.80	0.62	1.62	0.61	1.65	0		0	.
10	307.01	68.57	0.62	1.61	0.61	1.65	0		0	.
10	308.01	70.47	0.62	1.61	0.61	1.65	0		0	.
10	309.01	69.84	0.63	1.60	0.61	1.65	0		0	.
10	310.01	357.09	0.62	1.60	0.61	1.65	0		0	.
10	311.01	71.24	0.63	1.60	0.61	1.65	0		0	.
10	312.01	102.17	0.62	1.61	0.62	1.61	1	0	0	1.65
10	313.01	107.08	0.62	1.60	0.62	1.61	0		1	.
10	314.01	105.07	0.62	1.60	0.62	1.61	0		0	.
10	315.01	112.11	0.62	1.62	0.62	1.62	1	0	0	1.61
10	316.01	114.28	0.62	1.61	0.62	1.61	1	1	0	1.62
10	317.01	123.79	0.64	1.56	0.64	1.56	1	2	0	1.61
10	318.01	110.48	0.61	1.63	0.61	1.63	1	3	0	1.61
10	319.01	110.21	0.62	1.62	0.62	1.62	1	1	0	1.61
10	320.01	74.28	0.62	1.60	0.62	1.62	0		1	.
10	321.01	113.25	0.62	1.62	0.62	1.62	0		0	.
10	322.01	76.01	0.63	1.60	0.62	1.62	0		0	.
10	323.01	317.05	0.63	1.58	0.62	1.62	0		0	.
10	324.01	116.39	0.61	1.64	0.62	1.62	0		0	.
10	325.01	119.02	0.51	1.96	0.51	1.96	1	3	0	1.62
10	326.01	319.76	0.67	1.50	0.67	1.50	1	2	0	1.65
10	327.01	310.78	0.61	1.65	0.61	1.65	1	1	0	1.62
10	328.01	315.38	0.60	1.68	0.60	1.68	1	3	0	1.65
10	331.01	317.85	0.60	1.66	0.60	1.68	0		1	.
10	332.01	319.12	0.60	1.65	0.60	1.65	1	1	0	1.65
10	333.01	72.61	0.61	1.64	0.60	1.65	0		1	.
10	334.01	314.78	0.61	1.65	0.60	1.65	0		0	.
10	335.01	330.57	0.60	1.65	0.60	1.65	0		0	.
10	336.01	327.33	0.61	1.64	0.61	1.64	1	0	0	1.65
10	337.01	323.29	0.60	1.67	0.61	1.64	0		1	.
10	338.01	337.74	0.61	1.64	0.61	1.64	0		0	.
10	339.01	76.41	0.61	1.64	0.61	1.64	1	2	0	1.64
10	340.01	78.08	0.59	1.70	0.59	1.70	1	3	0	1.64
10	341.01	79.88	0.61	1.64	0.61	1.64	1	1	0	1.64
10	342.01	81.98	0.60	1.66	0.61	1.64	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	343.01	0	1	0	0	1	341	0	2.39	1	35.02
10	344.01	1	.	1	0	1	344	0	2.25	1	50.28
10	345.01	1	.	1	0	1	345	0	2.25	1	50.28
10	346.01	0	.	1	0	1	346	0	2.25	2	65.55
10	347.01	0	.	0	0	1	347	0	1.97	2	50.28
10	348.01	1	1	1	0	1	347	0	2.11	2	65.55
10	349.01	0	.	1	0	1	349	0	2.11	1	50.28
10	350.01	1	.	1	0	1	350	0	1.83	1	50.28
10	351.01	1	1	1	0	1	349	0	2.25	2	50.28
10	352.01	1	0	1	0	1	349	0	2.25	1	50.28
10	353.01	1	0	1	1	1	349	0	2.53	1	50.28
10	354.01	1	0	1	0	1	349	0	2.25	2	65.55
10	355.01	1	0	1	0	1	349	0	2.67	1	50.28
10	356.01	0	.	1	0	2	356	0	2.53	2	65.55
10	357.01	0	0	1	0	1	356	0	2.81	1	65.55
10	358.01	1	1	1	0	1	356	0	2.81	2	65.55
10	359.01	1	0	1	0	1	356	0	2.53	1	50.28
10	360.01	0	1	0	0	1	356	0	2.95	2	65.55
10	361.01	1	0	1	1	1	356	0	2.81	1	50.28
10	362.01	0	0	1	0	1	356	0	2.67	1	50.28
10	363.01	1	1	0	0	1	356	0	2.95	2	50.28
10	364.01	0	1	0	0	1	356	0	2.81	1	50.28
10	365.01	1	1	1	0	2	356	0	2.81	1	80.81
10	366.01	0	1	1	1	1	356	0	2.53	1	50.28
10	367.01	0	0	1	1	1	356	0	2.53	1	50.28
10	368.01	1	1	1	0	1	356	0	2.39	2	50.28
10	369.01	1	0	1	0	1	356	0	2.25	1	50.28
10	370.01	1	0	1	0	1	356	0	2.67	2	50.28
10	371.01	1	0	0	0	1	356	0	2.53	1	50.28
10	372.01	0	1	1	0	1	356	0	2.53	1	50.28
10	373.01	0	0	1	0	1	356	0	2.81	2	50.28
10	374.01	0	0	0	0	2	356	0	2.53	1	50.28
10	375.01	1	1	1	0	1	356	0	2.81	1	50.28
10	376.01	1	0	0	0	1	356	0	2.81	2	50.28
10	377.01	1	0	1	0	1	356	0	2.95	1	50.28
10	378.01	0	1	0	0	2	356	0	2.25	2	50.28
10	379.01	0	0	0	0	1	356	0	2.11	1	80.81
10	380.01	0	.	0	0	2	380	0	1.68	1	50.28
10	381.01	0	0	1	0	1	380	0	1.83	1	65.55
10	382.01	1	.	1	0	.	382	0	1.68	1	80.81
10	383.01	0	1	0	0	2	382	0	1.54	1	80.81
10	384.01	1	1	1	0	1	382	0	1.54	0	80.81
10	385.01	0	1	0	0	1	382	0	1.83	1	65.55
10	386.01	0	0	0	0	1	382	0	1.83	1	80.81
10	387.01	0	0	1	0	2	382	0	1.68	1	50.28
10	388.01	1	1	0	1	1	382	0	1.83	0	80.81
10	389.01	1	.	1	0	.	389	0	1.68	1	80.81
10	390.01	1	0	1	0	2	389	0	1.40	0	65.55
10	391.01	0	1	1	0	1	389	0	1.40	1	80.81
10	392.01	1	1	1	0	1	389	0	1.54	1	80.81

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	343.01	345.45	0.60	1.66	0.61	1.64	0		0	.
10	344.01	327.40	0.61	1.63	0.61	1.63	1	2	0	1.64
10	345.01	330.07	0.62	1.61	0.62	1.61	1	2	0	1.64
10	346.01	84.72	0.58	1.73	0.58	1.73	1	3	0	1.64
10	347.01	334.70	0.62	1.62	0.62	1.62	1	1	0	1.64
10	348.01	83.09	0.62	1.61	0.62	1.62	0		1	.
10	349.01	350.95	0.60	1.66	0.60	1.66	1	1	0	1.62
10	350.01	332.57	0.59	1.71	0.59	1.71	1	3	0	1.62
10	351.01	353.06	0.60	1.67	0.60	1.66	0		1	.
10	352.01	353.59	0.59	1.69	0.60	1.66	0		0	.
10	353.01	355.66	0.59	1.68	0.60	1.66	0		0	.
10	354.01	88.39	0.58	1.71	0.60	1.66	0		0	.
10	355.01	357.73	0.59	1.70	0.60	1.66	0		0	.
10	356.01	86.69	0.59	1.69	0.59	1.69	1	1	0	1.66
10	357.01	90.19	0.60	1.68	0.59	1.69	0		1	.
10	358.01	92.13	0.58	1.71	0.59	1.69	0		0	.
10	359.01	362.50	0.59	1.70	0.59	1.69	0		0	.
10	360.01	96.93	0.59	1.69	0.59	1.69	0		0	.
10	361.01	364.20	0.59	1.70	0.59	1.69	0		0	.
10	362.01	366.40	0.59	1.70	0.59	1.69	0		0	.
10	363.01	366.74	0.58	1.72	0.59	1.69	0		0	.
10	364.01	369.71	0.58	1.72	0.59	1.69	0		0	.
10	365.01	85.59	0.59	1.70	0.59	1.69	0		0	.
10	366.01	374.71	0.59	1.70	0.59	1.69	0		0	.
10	367.01	375.98	0.58	1.72	0.59	1.69	0		0	.
10	368.01	378.38	0.57	1.75	0.59	1.69	0		0	.
10	369.01	377.78	0.58	1.73	0.59	1.69	0		0	.
10	370.01	380.48	0.57	1.76	0.59	1.69	0		0	.
10	371.01	380.42	0.57	1.76	0.59	1.69	0		0	.
10	372.01	382.62	0.57	1.75	0.59	1.69	0		0	.
10	373.01	385.32	0.56	1.78	0.59	1.69	0		0	.
10	374.01	384.42	0.57	1.76	0.59	1.69	0		0	.
10	375.01	386.69	0.56	1.78	0.59	1.69	0		0	.
10	376.01	388.59	0.56	1.79	0.59	1.69	0		0	.
10	377.01	389.39	0.56	1.79	0.59	1.69	0		0	.
10	378.01	392.23	0.56	1.79	0.59	1.69	0		0	.
10	379.01	88.12	0.55	1.80	0.59	1.69	0		0	.
10	380.01	396.50	0.59	1.71	0.59	1.71	1	0	0	1.69
10	381.01	93.80	0.59	1.70	0.59	1.71	0		1	.
10	382.01	87.02	0.59	1.70	0.59	1.70	1	1	0	1.71
10	383.01	88.99	0.59	1.69	0.59	1.70	0		1	.
10	384.01	92.90	0.60	1.67	0.59	1.70	0		0	.
10	385.01	102.47	0.60	1.67	0.59	1.70	0		0	.
10	386.01	95.67	0.60	1.66	0.59	1.70	0		0	.
10	387.01	408.84	0.60	1.66	0.59	1.70	0		0	.
10	388.01	91.03	0.60	1.66	0.59	1.70	0		0	.
10	389.01	101.60	0.60	1.65	0.60	1.65	1	1	0	1.70
10	390.01	106.14	0.60	1.67	0.60	1.65	0		1	.
10	391.01	109.58	0.60	1.68	0.60	1.65	0		0	.
10	392.01	106.74	0.60	1.66	0.60	1.65	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	393.01	1	0	1	1	1	389	0	1.40	1	65.55
10	394.01	1	0	1	0	1	389	0	1.54	1	65.55
10	395.01	1	0	1	1	2	389	0	1.68	1	65.55
10	396.01	1	.	1	0	2	396	0	1.68	1	65.55
10	397.01	1	0	1	0	1	396	0	1.68	0	65.55
10	398.01	0	1	0	0	1	396	0	1.68	1	80.81
10	399.01	0	.	1	0	2	399	0	1.68	1	80.81
10	400.01	0	0	1	0	1	399	0	1.68	1	80.81
10	401.01	0	0	0	0	1	399	0	1.83	1	80.81
10	402.01	0	0	0	0	1	399	0	1.83	1	80.81
10	403.01	1	1	0	0	1	399	0	1.83	1	80.81
10	404.01	0	1	1	0	1	399	0	1.83	1	80.81
10	405.01	0	0	1	0	2	399	0	1.83	1	65.55
10	406.01	1	1	0	0	1	399	0	1.83	1	65.55
10	407.01	1	0	1	0	2	399	0	1.97	1	65.55
10	408.01	0	1	1	0	2	399	0	1.97	1	80.81
10	409.01	1	.	0	0	2	409	0	1.83	1	80.81
10	410.01	0	.	1	0	2	410	0	1.83	1	80.81
10	411.01	1	1	1	0	1	410	0	1.97	0	80.81
10	412.01	0	1	1	0	1	410	0	1.97	1	80.81
10	413.01	0	0	1	0	1	410	0	1.68	1	80.81
10	414.01	1	1	1	1	2	410	0	1.68	1	80.81
10	415.01	1	0	1	0	2	410	0	1.68	1	80.81
10	416.01	1	0	1	0	1	410	0	1.68	1	80.81
10	417.01	1	0	1	0	1	410	0	1.54	1	80.81
10	418.01	0	1	1	0	2	410	0	1.54	1	80.81
10	419.01	0	.	0	0	2	419	0	1.40	1	80.81
10	420.01	1	.	0	0	2	420	0	1.54	1	19.75
10	421.01	0	1	1	0	2	420	0	1.54	1	19.75
10	422.01	1	.	1	1	3	422	0	1.68	1	80.81
10	423.01	1	0	1	0	1	422	0	1.83	1	80.81
10	424.01	1	0	0	0	1	422	0	1.83	1	80.81
10	425.01	1	.	0	0	2	425	0	1.68	1	50.28
10	426.01	1	0	0	0	1	425	0	1.83	1	80.81
10	427.01	0	0	1	0	2	425	0	1.97	0	50.28
10	428.01	0	1	0	0	1	425	0	1.83	0	35.02
10	429.01	1	1	1	0	1	425	0	1.97	1	80.81
10	430.01	0	.	0	0	.	430	0	0.28	0	35.02
10	431.01	0	.	1	0	2	431	0	0.56	0	35.02
10	432.01	0	.	1	0	.	432	0	0.28	0	50.28
10	2.02	0	.	1	0	.	2	0	0.28	1	4.49
10	102.02	1	.	1	0	.	102	0	0.98	0	4.49
10	181.02	1	.	0	1	.	181	1	1.26	0	4.49
10	183.02	1	0	1	0	1	181	1	1.68	0	4.49
10	194.02	0	.	1	0	1	194	0	1.97	0	4.49
10	197.02	0	.	1	0	1	197	0	1.97	0	4.49
10	217.02	0	.	1	0	1	217	0	2.25	2	4.49
10	219.02	1	.	0	0	1	219	0	2.11	1	4.49
10	221.02	1	.	0	0	1	221	0	2.39	1	4.49
10	226.02	1	.	1	0	.	226	0	2.25	1	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	393.01	109.78	0.60	1.66	0.60	1.65	0		0	.
10	394.01	112.38	0.60	1.67	0.60	1.65	0		0	.
10	395.01	116.65	0.60	1.66	0.60	1.65	0		0	.
10	396.01	118.35	0.60	1.67	0.60	1.67	1	1	0	1.65
10	397.01	121.16	0.61	1.65	0.60	1.67	0		1	.
10	398.01	112.11	0.61	1.65	0.60	1.67	0		0	.
10	399.01	114.62	0.60	1.66	0.60	1.66	1	0	0	1.67
10	400.01	115.49	0.61	1.63	0.60	1.66	0		1	.
10	401.01	116.72	0.61	1.64	0.60	1.66	0		0	.
10	402.01	118.55	0.61	1.64	0.60	1.66	0		0	.
10	403.01	118.35	0.61	1.63	0.60	1.66	0		0	.
10	404.01	121.46	0.61	1.64	0.60	1.66	0		0	.
10	405.01	342.58	0.61	1.65	0.60	1.66	0		0	.
10	406.01	342.78	0.60	1.65	0.60	1.66	0		0	.
10	407.01	308.14	0.61	1.65	0.60	1.66	0		0	.
10	408.01	126.73	0.61	1.64	0.60	1.66	0		0	.
10	409.01	152.72	0.61	1.64	0.61	1.64	1	0	0	1.66
10	410.01	152.63	0.60	1.66	0.60	1.66	1	0	0	1.64
10	411.01	158.46	0.61	1.63	0.60	1.66	0		1	.
10	412.01	347.22	0.62	1.63	0.60	1.66	0		0	.
10	413.01	350.65	0.62	1.62	0.60	1.66	0		0	.
10	414.01	396.47	0.62	1.63	0.60	1.66	0		0	.
10	415.01	400.67	0.62	1.61	0.60	1.66	0		0	.
10	416.01	403.17	0.63	1.60	0.60	1.66	0		0	.
10	417.01	405.31	0.65	1.54	0.60	1.66	0		0	.
10	418.01	407.01	0.65	1.55	0.60	1.66	0		0	.
10	419.01	409.51	0.65	1.54	0.65	1.54	1	1	0	1.66
10	420.01	519.15	0.66	1.52	0.66	1.52	1	0	0	1.54
10	421.01	520.59	0.66	1.52	0.66	1.52	0		1	.
10	422.01	411.08	0.65	1.54	0.65	1.54	1	0	0	1.52
10	423.01	412.95	0.65	1.55	0.65	1.54	0		1	.
10	424.01	414.22	0.65	1.55	0.65	1.54	0		0	.
10	425.01	473.48	0.62	1.62	0.62	1.62	1	1	0	1.54
10	426.01	415.82	0.62	1.62	0.62	1.62	0		1	.
10	427.01	477.05	0.61	1.63	0.62	1.62	0		0	.
10	428.01	385.65	0.62	1.62	0.62	1.62	0		0	.
10	429.01	416.89	0.61	1.64	0.62	1.62	0		0	.
10	430.01	728.23	1.24	0.80	1.24	0.80	1	0	0	1.62
10	431.01	729.30	1.31	0.76	1.31	0.76	1	1	0	0.80
10	432.01	774.08	1.21	0.82	1.21	0.82	1	0	0	0.76
10	2.02	11.15	1.46	0.68	1.46	0.68	1	0	0	.
10	102.02	39.71	1.00	1.00	1.00	1.00	1	1	0	0.68
10	181.02	50.52	0.75	1.34	0.75	1.34	1	1	0	1.00
10	183.02	52.32	0.73	1.37	0.75	1.34	0		1	.
10	194.02	54.02	0.66	1.52	0.66	1.52	1	4	0	1.34
10	197.02	55.99	0.65	1.55	0.65	1.55	1	1	0	1.52
10	217.02	59.06	0.62	1.62	0.62	1.62	1	2	0	1.55
10	219.02	57.59	0.48	2.08	0.48	2.08	1	3	0	1.55
10	221.02	59.63	0.48	2.10	0.48	2.10	1	1	0	1.55
10	226.02	58.93	0.26	3.87	0.26	3.87	1	1	0	2.10

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	228.02	1	.	0	0	1	228	0	2.25	1	4.49
10	231.02	0	.	1	1	.	231	0	2.25	0	19.75
10	237.02	0	.	1	0	1	237	0	2.11	2	4.49
10	241.02	0	.	1	0	1	241	0	2.25	1	4.49
10	244.02	1	.	1	0	1	244	0	2.11	1	4.49
10	250.02	1	.	1	0	1	250	0	2.25	2	4.49
10	251.02	0	.	0	0	1	251	0	1.97	1	4.49
10	257.02	0	.	0	0	1	257	0	2.11	0	4.49
10	258.02	1	.	1	0	1	258	0	2.25	0	19.75
10	259.02	0	1	1	0	.	258	0	2.25	1	19.75
10	260.02	1	1	1	0	1	258	0	2.39	0	19.75
10	263.02	0	.	0	0	1	263	0	1.83	1	4.49
10	264.02	0	.	1	0	2	264	0	1.83	0	19.75
10	266.02	1	.	0	0	1	266	0	1.68	1	4.49
10	268.02	0	.	0	0	1	268	0	1.54	1	4.49
10	269.02	0	0	1	0	1	268	0	1.83	0	19.75
10	270.02	0	.	1	0	1	270	0	1.68	0	19.75
10	271.02	1	.	1	0	1	271	0	3.09	2	4.49
10	273.02	0	.	1	1	1	273	0	1.83	0	35.02
10	274.02	1	1	1	0	1	273	0	1.83	1	4.49
10	275.02	1	.	1	0	.	275	0	1.97	0	19.75
10	276.02	1	.	1	0	1	276	0	1.83	0	35.02
10	277.02	1	.	1	0	1	277	0	2.25	0	4.49
10	280.02	0	.	1	0	1	280	0	2.11	1	4.49
10	283.02	0	.	0	0	1	283	0	2.11	2	19.75
10	284.02	1	.	1	0	1	284	0	1.97	1	4.49
10	285.02	1	.	1	0	1	285	0	2.39	2	19.75
10	286.02	1	.	1	0	1	286	0	2.25	0	19.75
10	287.02	1	.	1	0	1	287	0	1.97	0	19.75
10	288.02	0	1	0	0	1	287	0	2.25	1	4.49
10	292.02	0	.	1	0	1	292	0	2.67	1	4.49
10	293.02	1	.	1	0	1	293	0	2.95	0	4.49
10	296.02	0	.	0	0	1	296	0	2.67	0	35.02
10	297.02	1	.	1	0	1	297	0	2.67	2	35.02
10	299.02	0	.	0	0	1	299	0	2.81	1	35.02
10	300.02	0	.	0	0	1	300	0	2.39	1	35.02
10	301.02	1	.	1	1	1	301	0	2.67	1	19.75
10	302.02	0	.	1	0	1	302	0	2.81	0	19.75
10	304.02	0	.	1	0	1	304	0	2.53	0	19.75
10	306.02	0	.	0	0	1	306	0	2.39	2	35.02
10	307.02	1	1	0	0	1	306	0	2.53	1	35.02
10	308.02	1	0	1	0	1	306	0	2.81	0	35.02
10	309.02	0	1	1	0	1	306	0	2.67	0	35.02
10	311.02	0	.	0	0	1	311	0	3.09	0	35.02
10	312.02	0	0	1	1	1	311	0	2.81	1	19.75
10	313.02	0	0	1	0	1	311	0	2.95	0	19.75
10	314.02	1	1	1	0	1	311	0	2.95	1	19.75
10	315.02	1	0	1	0	1	311	0	2.67	0	4.49
10	316.02	0	.	1	0	1	316	1	2.67	1	4.49
10	317.02	1	1	1	0	1	316	1	2.53	1	4.49

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	228.02	63.27	0.22	4.61	0.22	4.61	1	4	0	3.87
10	231.02	62.10	0.17	5.86	0.17	5.86	1	1	0	4.61
10	237.02	66.17	0.16	6.42	0.16	6.42	1	2	0	5.86
10	241.02	64.27	0.15	6.79	0.15	6.79	1	3	0	5.86
10	244.02	67.50	0.15	6.88	0.15	6.88	1	4	0	5.86
10	250.02	72.04	0.14	7.38	0.14	7.38	1	4	0	7.37
10	251.02	69.47	0.14	7.37	0.14	7.37	1	4	0	6.88
10	257.02	70.41	0.13	7.65	0.13	7.65	1	4	0	7.38
10	258.02	69.97	0.13	7.62	0.13	7.62	1	1	0	7.65
10	259.02	69.81	0.13	7.67	0.13	7.62	0		1	.
10	260.02	71.64	0.13	7.69	0.13	7.62	0		0	.
10	263.02	73.18	0.13	7.86	0.13	7.86	1	4	0	7.62
10	264.02	73.44	0.13	7.91	0.13	7.91	1	0	0	7.86
10	266.02	76.71	0.13	7.97	0.13	7.97	1	4	0	7.91
10	268.02	78.85	0.12	8.04	0.12	8.04	1	2	0	7.97
10	269.02	77.01	0.12	8.05	0.12	8.04	0		1	.
10	270.02	75.51	0.12	8.14	0.12	8.14	1	3	0	7.97
10	271.02	94.30	0.12	8.42	0.12	8.42	1	2	0	8.47
10	273.02	48.22	0.12	8.07	0.12	8.07	1	1	0	7.97
10	274.02	80.68	0.12	8.13	0.12	8.07	0		1	.
10	275.02	85.29	0.13	7.97	0.13	7.97	1	2	0	8.07
10	276.02	51.75	0.12	8.18	0.12	8.18	1	3	0	8.07
10	277.02	87.99	0.12	8.07	0.12	8.07	1	2	0	8.07
10	280.02	82.72	0.12	8.41	0.12	8.41	1	3	0	8.07
10	283.02	87.82	0.12	8.23	0.12	8.23	1	2	0	8.07
10	284.02	84.45	0.12	8.53	0.12	8.53	1	3	0	8.07
10	285.02	87.09	0.12	8.47	0.12	8.47	1	1	0	8.07
10	286.02	86.02	0.12	8.38	0.12	8.38	1	2	0	8.07
10	287.02	81.98	0.12	8.56	0.12	8.56	1	3	0	8.07
10	288.02	86.39	0.12	8.58	0.12	8.56	0		1	.
10	292.02	90.23	0.12	8.66	0.12	8.66	1	3	0	8.47
10	293.02	92.39	0.11	8.73	0.11	8.73	1	3	0	8.47
10	296.02	63.67	0.12	8.52	0.12	8.52	1	3	0	8.47
10	297.02	62.43	0.12	8.41	0.12	8.41	1	2	0	8.47
10	299.02	58.66	0.11	8.76	0.11	8.76	1	3	0	8.47
10	300.02	57.59	0.11	8.89	0.11	8.89	1	3	0	8.47
10	301.02	94.16	0.11	8.72	0.11	8.72	1	1	0	8.47
10	302.02	95.63	0.11	8.71	0.11	8.71	1	1	0	8.72
10	304.02	98.10	0.11	8.79	0.11	8.79	1	4	0	8.71
10	306.02	67.80	0.11	8.94	0.11	8.94	1	4	0	8.79
10	307.02	68.57	0.11	8.90	0.11	8.94	0		1	.
10	308.02	70.47	0.11	8.92	0.11	8.94	0		0	.
10	309.02	69.84	0.11	8.96	0.11	8.94	0		0	.
10	311.02	71.24	0.11	8.95	0.11	8.95	1	4	0	8.94
10	312.02	102.17	0.11	8.94	0.11	8.95	0		1	.
10	313.02	107.08	0.31	3.26	0.11	8.95	0		0	.
10	314.02	105.07	0.39	2.59	0.11	8.95	0		0	.
10	315.02	112.11	0.40	2.52	0.11	8.95	0		0	.
10	316.02	114.28	0.40	2.50	0.40	2.50	1	3	0	8.95
10	317.02	123.79	0.40	2.49	0.40	2.50	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	318.02	0	.	1	0	1	318	1	2.81	2	19.75
10	319.02	1	0	1	0	1	316	1	2.67	1	19.75
10	320.02	1	1	1	0	1	318	1	3.09	2	35.02
10	321.02	1	.	0	0	1	321	1	2.81	2	19.75
10	322.02	0	.	1	0	1	322	1	2.81	2	35.02
10	323.02	0	0	0	0	1	322	1	2.81	2	19.75
10	324.02	0	.	1	0	1	324	1	2.81	1	19.75
10	325.02	1	.	1	0	1	325	0	2.95	1	19.75
10	326.02	0	0	0	0	1	322	1	2.53	2	19.75
10	328.02	0	.	1	0	1	328	1	2.95	1	4.49
10	331.02	1	1	1	0	1	328	1	2.81	1	4.49
10	332.02	0	1	1	0	1	328	1	2.81	1	4.49
10	333.02	1	1	1	0	1	328	1	2.95	1	35.02
10	334.02	0	1	1	0	1	328	1	2.67	1	19.75
10	335.02	0	0	0	0	1	322	1	3.09	2	4.49
10	336.02	1	0	1	0	1	328	1	2.67	1	4.49
10	337.02	1	1	1	0	1	328	1	2.53	1	4.49
10	338.02	0	1	1	0	1	328	1	3.37	1	4.49
10	339.02	1	1	0	0	1	328	1	2.39	1	35.02
10	340.02	0	0	1	0	1	322	1	2.39	2	35.02
10	341.02	0	.	1	0	1	341	0	2.67	1	35.02
10	342.02	1	1	1	1	1	341	0	2.95	2	35.02
10	343.02	0	1	0	0	1	341	0	2.67	1	4.49
10	344.02	1	.	1	0	1	344	0	2.81	1	19.75
10	345.02	1	0	1	0	1	344	0	2.95	1	19.75
10	346.02	0	.	1	0	1	346	0	2.67	2	35.02
10	347.02	0	1	0	0	1	350	0	3.09	0	19.75
10	348.02	1	1	1	0	1	350	0	2.53	0	35.02
10	349.02	0	1	1	0	1	350	0	2.39	1	19.75
10	350.02	1	.	1	0	1	350	0	2.95	1	19.75
10	351.02	1	1	1	0	1	350	0	2.39	2	19.75
10	352.02	1	0	1	0	1	350	0	2.67	1	19.75
10	353.02	1	0	1	1	1	350	0	2.53	1	19.75
10	354.02	1	0	1	0	1	350	0	2.53	2	35.02
10	355.02	1	0	1	0	1	350	0	2.81	1	19.75
10	356.02	0	.	1	0	2	356	0	2.39	2	35.02
10	357.02	0	0	1	0	1	356	0	2.67	1	35.02
10	358.02	1	1	1	0	1	356	0	2.67	2	35.02
10	359.02	1	0	1	0	1	356	0	2.67	1	19.75
10	360.02	0	.	0	0	1	360	1	2.81	2	35.02
10	361.02	1	.	1	1	1	361	1	2.95	1	19.75
10	362.02	0	1	1	0	1	361	1	2.81	1	19.75
10	363.02	1	1	0	0	1	360	1	2.95	2	19.75
10	364.02	0	.	0	0	1	364	0	2.81	1	19.75
10	365.02	1	.	1	0	.	365	0	2.67	0	50.28
10	366.02	0	1	1	1	1	365	0	2.39	1	19.75
10	367.02	0	0	1	1	1	365	0	2.25	0	19.75
10	368.02	1	1	1	0	1	365	0	2.25	2	19.75
10	369.02	1	0	1	0	1	365	0	2.11	1	19.75
10	370.02	1	0	1	0	1	365	0	2.67	2	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	318.02	110.48	0.42	2.41	0.42	2.41	1	2	0	8.95
10	319.02	110.21	0.41	2.42	0.40	2.50	0		0	.
10	320.02	74.28	0.44	2.29	0.42	2.41	0		1	.
10	321.02	113.25	0.41	2.43	0.41	2.43	1	3	0	8.95
10	322.02	76.01	0.50	2.00	0.50	2.00	1	2	0	8.95
10	323.02	317.05	0.57	1.76	0.50	2.00	0		1	.
10	324.02	116.39	0.40	2.47	0.40	2.47	1	3	0	8.95
10	325.02	119.02	0.46	2.18	0.46	2.18	1	2	0	8.95
10	326.02	319.76	0.54	1.86	0.50	2.00	0		0	.
10	328.02	315.38	0.40	2.49	0.40	2.49	1	3	0	8.95
10	331.02	317.85	0.40	2.51	0.40	2.49	0		1	.
10	332.02	319.12	0.40	2.49	0.40	2.49	0		0	.
10	333.02	72.61	0.40	2.48	0.40	2.49	0		0	.
10	334.02	314.78	0.46	2.17	0.40	2.49	0		0	.
10	335.02	330.57	0.50	2.00	0.50	2.00	0		0	.
10	336.02	327.33	0.48	2.09	0.40	2.49	0		0	.
10	337.02	323.29	0.46	2.19	0.40	2.49	0		0	.
10	338.02	337.74	0.48	2.09	0.40	2.49	0		0	.
10	339.02	76.41	0.48	2.08	0.40	2.49	0		0	.
10	340.02	78.08	0.49	2.04	0.50	2.00	0		0	.
10	341.02	79.88	0.49	2.05	0.49	2.05	1	1	0	8.95
10	342.02	81.98	0.49	2.03	0.49	2.05	0		1	.
10	343.02	345.45	0.50	1.98	0.49	2.05	0		0	.
10	344.02	327.40	0.49	2.05	0.49	2.05	1	3	0	2.05
10	345.02	330.07	0.48	2.08	0.49	2.05	0		1	.
10	346.02	84.72	0.51	1.95	0.51	1.95	1	2	0	2.05
10	347.02	334.70	0.48	2.08	0.48	2.08	0		1	.
10	348.02	83.09	0.49	2.05	0.48	2.08	0		0	.
10	349.02	350.95	0.49	2.03	0.48	2.08	0		0	.
10	350.02	332.57	0.48	2.08	0.48	2.08	1	1	0	2.05
10	351.02	353.06	0.50	2.01	0.48	2.08	0		0	.
10	352.02	353.59	0.50	1.98	0.48	2.08	0		0	.
10	353.02	355.66	0.50	1.99	0.48	2.08	0		0	.
10	354.02	88.39	0.51	1.96	0.48	2.08	0		0	.
10	355.02	357.73	0.50	1.99	0.48	2.08	0		0	.
10	356.02	86.69	0.51	1.97	0.51	1.97	1	0	0	2.08
10	357.02	90.19	0.51	1.98	0.51	1.97	0		1	.
10	358.02	92.13	0.51	1.97	0.51	1.97	0		0	.
10	359.02	362.50	0.51	1.95	0.51	1.97	0		0	.
10	360.02	96.93	0.50	1.99	0.50	1.99	1	3	0	1.97
10	361.02	364.20	0.51	1.95	0.51	1.95	1	2	0	1.97
10	362.02	366.40	0.54	1.86	0.51	1.95	0		1	.
10	363.02	366.74	0.51	1.96	0.50	1.99	0		1	.
10	364.02	369.71	0.54	1.86	0.54	1.86	1	1	0	1.97
10	365.02	85.59	0.53	1.87	0.53	1.87	1	1	0	1.86
10	366.02	374.71	0.54	1.86	0.53	1.87	0		1	.
10	367.02	375.98	0.52	1.91	0.53	1.87	0		0	.
10	368.02	378.38	0.54	1.86	0.53	1.87	0		0	.
10	369.02	377.78	0.53	1.88	0.53	1.87	0		0	.
10	370.02	380.48	0.55	1.82	0.53	1.87	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	371.02	1	0	0	0	1	365	0	2.39	1	19.75
10	372.02	0	1	1	0	1	365	0	2.53	1	19.75
10	373.02	0	0	1	0	1	365	0	2.81	2	19.75
10	374.02	0	0	0	0	1	365	0	2.53	1	19.75
10	375.02	1	1	1	0	1	365	0	2.95	1	19.75
10	376.02	1	0	0	0	1	365	0	2.81	2	19.75
10	377.02	1	0	1	0	1	365	0	2.95	1	19.75
10	378.02	0	1	0	0	2	365	0	2.11	2	19.75
10	379.02	0	0	0	0	1	365	0	2.11	1	50.28
10	380.02	0	.	0	0	2	380	0	1.83	1	19.75
10	381.02	0	0	1	0	1	380	0	1.83	1	35.02
10	382.02	1	.	1	0	.	382	0	1.68	1	50.28
10	383.02	0	1	0	0	1	382	0	1.68	1	50.28
10	384.02	1	1	1	0	1	382	0	1.68	1	50.28
10	385.02	0	1	0	0	1	382	0	1.83	1	35.02
10	386.02	0	0	0	0	1	382	0	2.11	0	50.28
10	387.02	0	0	1	0	1	382	0	1.97	0	19.75
10	388.02	1	1	0	1	1	382	0	2.25	1	50.28
10	389.02	1	.	1	0	.	389	0	1.97	1	50.28
10	390.02	1	0	1	0	2	389	0	1.68	0	35.02
10	391.02	0	1	1	0	1	389	0	1.68	1	50.28
10	392.02	1	1	1	0	1	389	0	1.83	1	50.28
10	393.02	1	0	1	1	1	389	0	1.54	1	35.02
10	394.02	1	0	1	0	1	389	0	1.83	1	35.02
10	395.02	1	0	1	1	1	389	0	1.83	1	35.02
10	396.02	1	.	1	0	1	396	0	1.83	1	35.02
10	397.02	1	0	1	0	1	396	0	1.83	1	35.02
10	398.02	0	1	0	0	1	396	0	1.83	1	50.28
10	399.02	0	0	1	0	2	396	0	1.83	1	50.28
10	400.02	0	0	1	0	1	396	0	1.83	0	50.28
10	401.02	0	0	0	0	1	396	0	1.97	1	50.28
10	402.02	0	0	0	0	1	396	0	1.97	1	50.28
10	403.02	1	1	0	0	1	396	0	1.97	1	50.28
10	404.02	0	1	1	0	1	396	0	1.97	1	50.28
10	405.02	0	0	1	0	2	396	0	1.97	1	35.02
10	406.02	1	1	0	0	1	396	0	1.97	1	35.02
10	407.02	1	0	1	0	2	396	0	1.97	1	35.02
10	408.02	0	1	1	0	2	396	0	1.97	1	50.28
10	409.02	1	.	0	0	2	409	0	1.97	1	50.28
10	410.02	0	.	1	0	2	410	0	1.97	1	50.28
10	411.02	1	1	1	0	1	410	0	1.83	1	50.28
10	412.02	0	1	1	0	1	410	0	1.83	1	50.28
10	413.02	0	0	1	0	1	410	0	1.68	1	50.28
10	414.02	1	.	1	1	2	414	0	1.68	1	50.28
10	415.02	1	0	1	0	2	414	0	1.68	1	50.28
10	416.02	1	0	1	0	1	414	0	1.68	1	50.28
10	417.02	1	0	1	0	1	414	0	1.54	1	50.28
10	418.02	0	1	1	0	2	414	0	1.68	1	50.28
10	419.02	0	.	0	0	2	419	0	1.54	1	50.28
10	422.02	1	.	1	1	3	422	0	1.68	1	50.28

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	371.02	380.42	0.55	1.82	0.53	1.87	0		0	.
10	372.02	382.62	0.55	1.82	0.53	1.87	0		0	.
10	373.02	385.32	0.55	1.80	0.53	1.87	0		0	.
10	374.02	384.42	0.55	1.82	0.53	1.87	0		0	.
10	375.02	386.69	0.55	1.81	0.53	1.87	0		0	.
10	376.02	388.59	0.55	1.81	0.53	1.87	0		0	.
10	377.02	389.39	0.57	1.75	0.53	1.87	0		0	.
10	378.02	392.23	0.55	1.82	0.53	1.87	0		0	.
10	379.02	88.12	0.56	1.78	0.53	1.87	0		0	.
10	380.02	396.50	0.56	1.78	0.56	1.78	1	1	0	1.87
10	381.02	93.80	0.56	1.79	0.56	1.78	0		1	.
10	382.02	87.02	0.56	1.78	0.56	1.78	1	0	0	1.78
10	383.02	88.99	0.56	1.78	0.56	1.78	0		1	.
10	384.02	92.90	0.56	1.79	0.56	1.78	0		0	.
10	385.02	102.47	0.55	1.81	0.56	1.78	0		0	.
10	386.02	95.67	0.55	1.80	0.56	1.78	0		0	.
10	387.02	408.84	0.55	1.81	0.56	1.78	0		0	.
10	388.02	91.03	0.54	1.85	0.56	1.78	0		0	.
10	389.02	101.60	0.55	1.83	0.55	1.83	1	0	0	1.78
10	390.02	106.14	0.55	1.81	0.55	1.83	0		1	.
10	391.02	109.58	0.55	1.80	0.55	1.83	0		0	.
10	392.02	106.74	0.55	1.82	0.55	1.83	0		0	.
10	393.02	109.78	0.55	1.83	0.55	1.83	0		0	.
10	394.02	112.38	0.55	1.82	0.55	1.83	0		0	.
10	395.02	116.65	0.55	1.83	0.55	1.83	0		0	.
10	396.02	118.35	0.55	1.81	0.55	1.81	1	0	0	1.83
10	397.02	121.16	0.55	1.82	0.55	1.81	0		1	.
10	398.02	112.11	0.55	1.82	0.55	1.81	0		0	.
10	399.02	114.62	0.55	1.83	0.55	1.81	0		0	.
10	400.02	115.49	0.55	1.83	0.55	1.81	0		0	.
10	401.02	116.72	0.55	1.82	0.55	1.81	0		0	.
10	402.02	118.55	0.55	1.83	0.55	1.81	0		0	.
10	403.02	118.35	0.55	1.83	0.55	1.81	0		0	.
10	404.02	121.46	0.55	1.82	0.55	1.81	0		0	.
10	405.02	342.58	0.55	1.83	0.55	1.81	0		0	.
10	406.02	342.78	0.54	1.86	0.55	1.81	0		0	.
10	407.02	308.14	0.54	1.85	0.55	1.81	0		0	.
10	408.02	126.73	0.54	1.86	0.55	1.81	0		0	.
10	409.02	152.72	0.54	1.86	0.54	1.86	1	1	0	1.81
10	410.02	152.63	0.54	1.84	0.54	1.84	1	1	0	1.86
10	411.02	158.46	0.54	1.84	0.54	1.84	0		1	.
10	412.02	347.22	0.54	1.84	0.54	1.84	0		0	.
10	413.02	350.65	0.54	1.85	0.54	1.84	0		0	.
10	414.02	396.47	0.55	1.82	0.55	1.82	1	1	0	1.84
10	415.02	400.67	0.54	1.85	0.55	1.82	0		1	.
10	416.02	403.17	0.54	1.86	0.55	1.82	0		0	.
10	417.02	405.31	0.52	1.92	0.55	1.82	0		0	.
10	418.02	407.01	0.52	1.92	0.55	1.82	0		0	.
10	419.02	409.51	0.52	1.91	0.52	1.91	1	0	0	1.82
10	422.02	411.08	0.49	2.03	0.49	2.03	1	0	0	1.91

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	423.02	1	0	1	0	1	422	0	1.83	1	50.28
10	424.02	1	0	0	0	1	422	0	1.83	1	50.28
10	425.02	1	.	0	0	3	425	0	1.68	1	19.75
10	426.02	1	0	0	0	2	425	0	1.83	1	50.28
10	427.02	0	0	1	0	2	425	0	1.83	1	19.75
10	428.02	0	1	0	0	1	425	0	2.39	1	4.49
10	429.02	1	1	1	0	1	425	0	1.83	1	50.28
10	430.02	0	.	0	0	.	430	0	0.28	2	4.49
10	431.02	0	.	1	0	2	431	0	0.56	1	4.49
10	432.02	0	.	1	0	.	432	0	0.28	0	19.75
10	273.03	0	.	1	1	.	273	0	1.12	1	4.49
10	276.03	1	.	1	0	.	276	0	0.98	0	4.49
10	296.03	0	.	0	0	1	296	0	1.54	2	4.49
10	297.03	1	.	1	0	.	297	0	1.40	0	4.49
10	299.03	0	0	0	0	1	300	0	1.68	0	4.49
10	300.03	0	.	0	0	.	300	0	1.26	1	4.49
10	306.03	0	.	0	0	.	306	0	1.26	0	4.49
10	307.03	1	.	0	0	1	307	0	1.54	1	4.49
10	308.03	1	.	1	0	1	308	0	1.83	2	4.49
10	309.03	0	.	1	0	1	309	0	1.68	1	4.49
10	311.03	0	.	0	0	1	311	0	2.11	0	4.49
10	320.03	1	.	1	0	1	320	0	2.11	0	4.49
10	322.03	0	.	1	0	1	322	0	1.68	2	4.49
10	333.03	1	.	1	0	1	333	0	2.11	1	4.49
10	339.03	1	.	0	0	1	339	0	1.83	1	4.49
10	340.03	0	1	1	0	1	339	0	1.83	2	4.49
10	341.03	0	0	1	0	1	339	0	1.83	1	4.49
10	342.03	1	1	1	1	1	339	0	2.11	0	4.49
10	346.03	0	.	1	0	1	346	0	1.83	2	4.49
10	348.03	1	.	1	0	1	348	0	1.83	1	4.49
10	354.03	1	.	1	0	1	354	0	2.39	0	4.49
10	356.03	0	.	1	0	2	356	0	1.68	0	4.49
10	357.03	0	.	1	0	1	357	0	2.25	1	4.49
10	358.03	1	1	1	0	1	357	0	2.39	2	4.49
10	360.03	0	.	0	0	1	360	0	2.67	0	4.49
10	365.03	1	.	1	0	.	365	0	1.83	1	19.75
10	379.03	0	.	0	0	1	379	0	1.97	1	19.75
10	381.03	0	.	1	0	1	381	0	2.25	1	4.49
10	382.03	1	.	1	0	1	382	0	1.68	1	19.75
10	383.03	0	1	0	0	1	382	0	2.11	1	19.75
10	384.03	1	.	1	0	1	384	0	2.25	0	19.75
10	385.03	0	.	0	0	1	385	0	2.11	1	4.49
10	386.03	0	.	0	0	1	386	0	2.39	0	19.75
10	388.03	1	.	0	1	1	388	0	2.39	1	19.75
10	389.03	1	.	1	0	1	389	0	2.25	0	19.75
10	390.03	1	.	1	0	1	390	0	1.97	1	4.49
10	391.03	0	.	1	0	1	391	0	1.68	0	19.75
10	392.03	1	.	1	0	1	392	0	1.97	0	19.75
10	393.03	1	.	1	1	1	393	0	1.68	1	4.49
10	394.03	1	0	1	0	2	393	0	1.83	1	4.49

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	423.02	412.95	0.50	2.01	0.49	2.03	0		1	.
10	424.02	414.22	0.50	2.00	0.49	2.03	0		0	.
10	425.02	473.48	0.51	1.98	0.51	1.98	1	0	0	2.03
10	426.02	415.82	0.51	1.98	0.51	1.98	0		1	.
10	427.02	477.05	0.49	2.04	0.51	1.98	0		0	.
10	428.02	385.65	0.52	1.92	0.51	1.98	0		0	.
10	429.02	416.89	0.50	2.00	0.51	1.98	0		0	.
10	430.02	728.23	1.45	0.69	1.45	0.69	1	2	0	1.98
10	431.02	729.30	1.45	0.69	1.45	0.69	1	3	0	1.98
10	432.02	774.08	0.14	6.99	0.14	6.99	1	0	0	.
10	273.03	48.22	0.81	1.23	0.81	1.23	1	1	0	.
10	276.03	51.75	0.84	1.19	0.84	1.19	1	1	0	1.23
10	296.03	63.67	0.72	1.39	0.72	1.39	1	2	0	1.39
10	297.03	62.43	0.67	1.49	0.67	1.49	1	3	0	1.39
10	299.03	58.66	0.74	1.35	0.72	1.39	0		0	.
10	300.03	57.59	0.72	1.39	0.72	1.39	1	1	0	1.19
10	306.03	67.80	0.70	1.42	0.70	1.42	1	1	0	1.39
10	307.03	68.57	0.68	1.47	0.68	1.47	1	4	0	1.42
10	308.03	70.47	0.71	1.41	0.71	1.41	1	2	0	1.47
10	309.03	69.84	0.67	1.48	0.67	1.48	1	3	0	1.47
10	311.03	71.24	0.66	1.52	0.66	1.52	1	1	0	1.47
10	320.03	74.28	0.12	8.50	0.12	8.50	1	2	0	1.52
10	322.03	76.01	0.11	8.82	0.11	8.82	1	1	0	1.52
10	333.03	72.61	0.11	8.82	0.11	8.82	1	3	0	1.52
10	339.03	76.41	0.11	9.34	0.11	9.34	1	4	0	8.82
10	340.03	78.08	0.11	9.31	0.11	9.34	0		1	.
10	341.03	79.88	0.11	9.32	0.11	9.34	0		0	.
10	342.03	81.98	0.11	9.29	0.11	9.34	0		0	.
10	346.03	84.72	0.11	9.39	0.11	9.39	1	1	0	9.34
10	348.03	83.09	0.11	9.51	0.11	9.51	1	4	0	9.39
10	354.03	88.39	0.10	9.61	0.10	9.61	1	2	0	9.51
10	356.03	86.69	0.10	9.83	0.10	9.83	1	3	0	9.51
10	357.03	90.19	0.10	9.70	0.10	9.70	1	1	0	9.51
10	358.03	92.13	0.10	9.70	0.10	9.70	0		1	.
10	360.03	96.93	0.11	9.52	0.11	9.52	1	2	0	9.70
10	365.03	85.59	0.10	10.03	0.10	10.03	1	3	0	9.70
10	379.03	88.12	0.09	10.60	0.09	10.60	1	1	0	9.70
10	381.03	93.80	0.09	10.72	0.09	10.72	1	1	0	10.60
10	382.03	87.02	0.09	10.69	0.09	10.69	1	1	0	10.72
10	383.03	88.99	0.09	10.72	0.09	10.69	0		1	.
10	384.03	92.90	0.09	10.65	0.09	10.65	1	2	0	10.69
10	385.03	102.47	0.09	10.72	0.09	10.72	1	3	0	10.69
10	386.03	95.67	0.09	10.70	0.09	10.70	1	1	0	10.69
10	388.03	91.03	0.09	10.89	0.09	10.89	1	3	0	10.70
10	389.03	101.60	0.09	10.77	0.09	10.77	1	2	0	10.70
10	390.03	106.14	0.09	10.91	0.09	10.91	1	3	0	10.70
10	391.03	109.58	0.09	10.80	0.09	10.80	1	2	0	10.70
10	392.03	106.74	0.09	10.91	0.09	10.91	1	3	0	10.70
10	393.03	109.78	0.09	10.80	0.09	10.80	1	1	0	10.70
10	394.03	112.38	0.10	10.13	0.09	10.80	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
10	395.03	1	0	1	1	1	393	0	1.97	1	4.49
10	396.03	1	0	1	0	1	393	0	2.25	1	4.49
10	397.03	1	0	1	0	1	393	0	2.39	1	4.49
10	398.03	0	1	0	0	1	393	0	1.83	1	19.75
10	399.03	0	.	1	0	.	399	0	1.83	1	19.75
10	400.03	0	0	1	0	1	399	0	1.97	0	19.75
10	401.03	0	0	0	0	1	399	0	2.11	1	19.75
10	402.03	0	0	0	0	1	399	0	2.39	1	19.75
10	403.03	1	1	0	0	1	399	0	2.25	1	19.75
10	404.03	0	1	1	0	1	399	0	2.53	1	19.75
10	405.03	0	0	1	0	1	399	0	2.25	1	4.49
10	406.03	1	1	0	0	1	399	0	2.39	1	4.49
10	407.03	1	0	1	0	1	399	0	2.53	1	4.49
10	408.03	0	1	1	0	1	399	0	2.67	1	19.75
10	409.03	1	.	0	0	1	409	0	2.39	1	19.75
10	410.03	0	.	1	0	1	410	0	2.25	1	19.75
10	411.03	1	1	1	0	1	410	0	2.39	1	19.75
10	412.03	0	1	1	0	1	410	0	2.39	1	19.75
10	413.03	0	0	1	0	1	410	0	2.53	1	19.75
10	414.03	1	.	1	1	1	414	0	2.25	1	19.75
10	415.03	1	0	1	0	1	414	0	1.97	1	19.75
10	416.03	1	0	1	0	1	414	0	1.83	1	19.75
10	417.03	1	0	1	0	2	414	0	1.68	1	19.75
10	418.03	0	1	1	0	2	414	0	1.83	1	19.75
10	419.03	0	.	0	0	2	419	0	1.68	1	19.75
10	422.03	1	.	1	1	1	422	0	1.68	1	19.75
10	423.03	1	0	1	0	1	422	0	1.68	1	19.75
10	424.03	1	0	0	0	1	422	0	1.68	1	19.75
10	426.03	1	.	0	0	2	426	0	1.68	1	19.75
10	429.03	1	.	1	0	1	429	0	1.83	1	19.75
11	1	1	.	1	0	.	1	0	0.28	1	4.49
11	2	1	.	1	0	.	2	0	0.42	1	4.49
11	3	1	.	1	0	.	3	0	0.56	1	4.49
11	4	0	1	1	0	2	3	0	0.70	0	4.49
11	5	0	.	1	0	.	5	0	0.42	1	19.75
11	6	0	.	1	0	2	6	0	0.56	1	19.75
11	7	1	.	1	0	.	7	0	0.56	2	4.49
11	8	1	0	0	0	1	7	0	0.70	1	4.49
11	9	0	1	1	1	1	7	0	0.84	1	4.49
11	10	0	0	1	0	1	7	0	0.70	1	4.49
11	11	0	0	1	0	2	7	0	0.70	1	4.49
11	13	0	.	1	0	2	13	0	0.70	0	4.49
11	16	1	.	1	0	.	16	0	0.84	1	35.02
11	17	0	.	0	0	.	17	0	0.42	0	19.75
11	18	0	.	0	0	.	18	0	0.42	0	19.75
11	19	0	.	1	0	.	19	0	0.70	2	19.75
11	21	1	1	1	0	1	19	0	1.12	0	4.49
11	22	1	.	1	0	1	22	1	0.70	1	4.49
11	23	0	.	0	0	1	23	1	1.12	2	4.49
11	24	1	0	1	0	1	22	1	0.98	1	4.49

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
10	395.03	116.65	0.10	10.10	0.09	10.80	0		0	.
10	396.03	118.35	0.10	10.03	0.09	10.80	0		0	.
10	397.03	121.16	0.10	10.07	0.09	10.80	0		0	.
10	398.03	112.11	0.11	9.32	0.09	10.80	0		0	.
10	399.03	114.62	0.28	3.59	0.28	3.59	1	1	0	10.80
10	400.03	115.49	0.28	3.55	0.28	3.59	0		1	.
10	401.03	116.72	0.28	3.53	0.28	3.59	0		0	.
10	402.03	118.55	0.47	2.13	0.28	3.59	0		0	.
10	403.03	118.35	0.54	1.84	0.28	3.59	0		0	.
10	404.03	121.46	0.55	1.83	0.28	3.59	0		0	.
10	405.03	342.58	0.55	1.83	0.28	3.59	0		0	.
10	406.03	342.78	0.55	1.81	0.28	3.59	0		0	.
10	407.03	308.14	0.55	1.83	0.28	3.59	0		0	.
10	408.03	126.73	0.55	1.83	0.28	3.59	0		0	.
10	409.03	152.72	0.54	1.84	0.54	1.84	1	0	0	3.59
10	410.03	152.63	0.54	1.84	0.54	1.84	1	0	0	1.84
10	411.03	158.46	0.54	1.85	0.54	1.84	0		1	.
10	412.03	347.22	0.54	1.86	0.54	1.84	0		0	.
10	413.03	350.65	0.54	1.86	0.54	1.84	0		0	.
10	414.03	396.47	0.53	1.89	0.53	1.89	1	0	0	1.84
10	415.03	400.67	0.53	1.89	0.53	1.89	0		1	.
10	416.03	403.17	0.52	1.91	0.53	1.89	0		0	.
10	417.03	405.31	0.52	1.91	0.53	1.89	0		0	.
10	418.03	407.01	0.52	1.93	0.53	1.89	0		0	.
10	419.03	409.51	0.52	1.92	0.52	1.92	1	1	0	1.89
10	422.03	411.08	0.52	1.91	0.52	1.91	1	0	0	1.92
10	423.03	412.95	0.53	1.90	0.52	1.91	0		1	.
10	424.03	414.22	0.53	1.89	0.52	1.91	0		0	.
10	426.03	415.82	0.51	1.96	0.51	1.96	1	4	0	1.91
10	429.03	416.89	0.49	2.05	0.49	2.05	1	4	0	1.96
11	1	45.74	1.27	0.79	1.27	0.79	1	0	0	.
11	2	46.61	1.25	0.80	1.25	0.80	1	0	0	0.79
11	3	47.61	1.14	0.88	1.14	0.88	1	0	0	0.80
11	4	49.01	1.18	0.85	1.14	0.88	0		1	.
11	5	56.08	1.43	0.70	1.43	0.70	1	1	0	0.88
11	6	57.72	1.45	0.69	1.45	0.69	1	1	0	0.70
11	7	59.32	1.14	0.87	1.14	0.87	1	0	0	0.69
11	8	61.16	1.18	0.85	1.14	0.87	0		1	.
11	9	63.02	1.20	0.83	1.14	0.87	0		0	.
11	10	64.16	1.21	0.83	1.14	0.87	0		0	.
11	11	65.66	1.21	0.83	1.14	0.87	0		0	.
11	13	66.76	1.04	0.96	1.04	0.96	1	0	0	0.87
11	16	47.22	1.04	0.96	1.04	0.96	1	1	0	0.96
11	17	72.50	1.19	0.84	1.19	0.84	1	1	0	0.96
11	18	74.70	1.15	0.87	1.15	0.87	1	0	0	0.84
11	19	75.94	1.07	0.93	1.07	0.93	1	0	0	0.87
11	21	77.81	1.07	0.93	1.07	0.93	0		1	.
11	22	75.47	0.93	1.07	0.93	1.07	1	3	0	0.93
11	23	78.81	1.00	1.00	1.00	1.00	1	2	0	0.93
11	24	76.67	0.93	1.08	0.93	1.07	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	25	1	.	1	0	2	25	0	1.26	1	19.75
11	26	1	0	1	0	1	25	0	1.12	1	19.75
11	27	0	1	0	0	1	25	0	1.12	0	35.02
11	28	0	.	1	0	.	28	0	0.84	1	35.02
11	29	1	.	1	0	1	29	0	0.70	1	50.28
11	30	0	1	0	0	1	29	0	0.84	1	35.02
11	31	0	.	0	0	2	31	0	0.70	1	19.75
11	32	1	.	0	0	.	32	0	0.84	2	50.28
11	33	1	0	1	0	1	32	0	1.12	1	50.28
11	34	0	.	0	0	.	34	0	0.98	1	4.49
11	35	1	.	1	0	.	35	0	0.84	0	19.75
11	36	1	.	1	0	1	36	0	1.26	1	19.75
11	37	0	1	1	0	1	36	0	1.54	2	50.28
11	38	0	.	1	0	2	38	1	1.40	2	50.28
11	40	0	.	0	0	1	40	1	1.83	2	50.28
11	42	0	.	1	0	1	42	1	1.54	0	4.49
11	43	0	.	1	0	1	43	1	1.54	1	4.49
11	46	0	.	0	0	1	46	1	1.54	1	35.02
11	47	1	.	1	0	1	47	1	1.97	0	19.75
11	48	1	.	1	0	1	48	1	1.83	1	19.75
11	49	1	.	1	1	1	49	1	1.83	0	19.75
11	50	0	.	0	0	1	50	1	1.54	2	35.02
11	51	0	0	1	0	1	50	1	1.83	2	35.02
11	55	0	.	1	0	1	55	1	1.40	2	35.02
11	56	1	.	1	0	1	56	1	1.68	1	4.49
11	58	0	.	0	0	1	58	1	1.68	1	19.75
11	59	1	0	1	0	1	55	1	1.68	2	50.28
11	60	0	0	1	0	1	58	1	1.83	1	19.75
11	61	1	0	1	0	1	55	1	1.40	2	50.28
11	62	0	0	0	0	1	58	1	1.68	1	19.75
11	63	0	0	1	0	1	58	1	1.54	1	65.55
11	64	0	.	0	0	2	64	0	1.12	1	19.75
11	65	1	1	0	0	1	64	0	1.12	0	35.02
11	66	1	0	0	0	1	64	0	1.12	1	19.75
11	67	1	0	1	0	1	64	0	1.26	2	4.49
11	68	1	.	0	0	1	68	0	1.26	2	35.02
11	69	1	.	1	0	1	69	0	1.54	1	4.49
11	70	1	.	0	0	1	70	0	1.83	1	4.49
11	71	1	0	1	0	1	70	0	1.40	1	19.75
11	72	1	0	1	1	1	70	0	1.12	1	19.75
11	73	1	0	1	0	1	70	0	1.40	1	35.02
11	74	0	1	0	0	1	70	0	1.68	2	35.02
11	75	1	.	0	0	1	75	0	1.68	2	35.02
11	76	0	0	1	0	1	77	0	1.68	2	35.02
11	77	0	.	0	0	1	77	0	1.68	1	19.75
11	78	1	.	1	0	1	78	0	1.83	1	65.55
11	79	1	0	0	0	1	78	0	1.54	2	19.75
11	80	0	1	0	0	1	78	0	1.54	1	19.75
11	81	0	0	0	0	1	78	0	1.68	2	19.75
11	82	1	1	1	0	1	78	0	1.54	1	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	25	78.27	1.00	1.00	1.00	1.00	1	1	0	0.93
11	26	79.71	0.98	1.02	1.00	1.00	0		1	.
11	27	56.06	1.00	1.00	1.00	1.00	0		0	.
11	28	57.16	1.06	0.94	1.06	0.94	1	0	0	1.00
11	29	56.03	1.07	0.94	1.07	0.94	1	0	0	0.94
11	30	58.06	1.07	0.93	1.07	0.94	0		1	.
11	31	88.45	1.09	0.92	1.09	0.92	1	0	0	0.94
11	32	58.40	1.01	0.99	1.01	0.99	1	0	0	0.92
11	33	58.26	1.00	1.00	1.01	0.99	0		1	.
11	34	93.19	0.98	1.03	0.98	1.03	1	0	0	0.99
11	35	91.99	0.94	1.07	0.94	1.07	1	0	0	1.03
11	36	93.22	0.97	1.03	0.97	1.03	1	1	0	1.07
11	37	61.10	0.95	1.06	0.97	1.03	0		1	.
11	38	60.36	0.98	1.03	0.98	1.03	1	2	0	1.03
11	40	63.27	0.96	1.04	0.96	1.04	1	2	0	1.03
11	42	96.19	0.85	1.17	0.85	1.17	1	3	0	1.03
11	43	94.42	0.79	1.27	0.79	1.27	1	3	0	1.03
11	46	59.36	0.79	1.27	0.79	1.27	1	3	0	1.03
11	47	98.03	0.81	1.23	0.81	1.23	1	2	0	1.03
11	48	96.92	0.79	1.26	0.79	1.26	1	3	0	1.03
11	49	100.23	0.82	1.22	0.82	1.22	1	1	0	1.03
11	50	62.50	0.81	1.24	0.81	1.24	1	2	0	1.22
11	51	64.67	0.81	1.23	0.81	1.24	0		1	.
11	55	65.40	0.78	1.28	0.78	1.28	1	2	0	1.22
11	56	102.66	0.67	1.49	0.67	1.49	1	3	0	1.22
11	58	100.06	0.66	1.50	0.66	1.50	1	1	0	1.22
11	59	64.94	0.74	1.35	0.78	1.28	0		1	.
11	60	103.10	0.67	1.50	0.66	1.50	0		1	.
11	61	66.77	0.73	1.37	0.78	1.28	0		0	.
11	62	104.63	0.66	1.52	0.66	1.50	0		0	.
11	63	38.64	0.68	1.46	0.66	1.50	0		0	.
11	64	111.71	0.71	1.41	0.71	1.41	1	1	0	1.50
11	65	67.97	0.71	1.42	0.71	1.41	0		1	.
11	66	113.68	0.70	1.43	0.71	1.41	0		0	.
11	67	114.98	0.70	1.43	0.71	1.41	0		0	.
11	68	74.25	0.71	1.41	0.71	1.41	1	2	0	1.41
11	69	117.05	0.68	1.47	0.68	1.47	1	3	0	1.41
11	70	119.48	0.69	1.45	0.69	1.45	1	1	0	1.41
11	71	115.24	0.70	1.43	0.69	1.45	0		1	.
11	72	116.48	0.70	1.43	0.69	1.45	0		0	.
11	73	70.31	0.70	1.43	0.69	1.45	0		0	.
11	74	72.01	0.69	1.45	0.69	1.45	0		0	.
11	75	75.88	0.69	1.45	0.69	1.45	1	0	0	1.45
11	76	78.28	0.68	1.47	0.68	1.46	0		1	.
11	77	122.12	0.68	1.46	0.68	1.46	1	1	0	1.45
11	78	41.74	0.68	1.47	0.68	1.47	1	0	0	1.46
11	79	124.92	0.67	1.50	0.68	1.47	0		1	.
11	80	126.62	0.69	1.45	0.68	1.47	0		0	.
11	81	128.69	0.67	1.49	0.68	1.47	0		0	.
11	82	129.49	0.69	1.44	0.68	1.47	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	83	0	1	1	0	2	78	0	1.40	1	50.28
11	84	0	0	1	0	1	78	0	1.54	2	50.28
11	85	0	.	1	0	2	85	0	1.12	2	50.28
11	86	0	1	1	0	1	85	0	1.54	2	50.28
11	87	1	1	1	0	1	85	0	1.26	1	50.28
11	88	0	.	1	0	1	88	0	1.54	0	19.75
11	89	0	.	1	0	1	89	1	1.83	2	65.55
11	90	0	0	1	0	1	89	1	1.97	2	65.55
11	91	0	.	1	0	1	91	1	1.54	1	19.75
11	92	0	0	0	0	1	91	1	1.68	1	19.75
11	93	1	1	1	0	1	89	1	2.39	2	4.49
11	94	1	1	1	0	1	91	1	2.11	1	4.49
11	95	0	1	1	0	1	96	0	2.25	2	65.55
11	96	1	.	1	0	1	96	0	2.39	1	4.49
11	97	0	0	0	0	1	96	0	1.83	1	19.75
11	98	1	1	0	0	1	96	0	2.11	1	19.75
11	99	0	1	0	0	1	96	0	2.11	1	35.02
11	100	0	0	0	0	1	96	0	1.83	2	65.55
11	101	0	0	0	0	1	96	0	1.83	1	19.75
11	102	1	1	1	0	1	96	0	1.83	2	50.28
11	103	0	.	0	0	1	103	0	1.40	2	35.02
11	104	0	.	0	0	1	104	0	1.68	2	35.02
11	105	0	.	0	0	1	105	0	1.83	1	35.02
11	106	1	1	1	0	1	104	0	1.68	1	19.75
11	107	1	0	1	0	1	104	0	1.68	1	19.75
11	108	0	1	0	0	1	104	0	1.54	0	50.28
11	109	0	0	0	0	1	104	0	1.68	2	50.28
11	110	0	0	1	0	1	104	0	1.40	1	19.75
11	111	0	0	1	0	1	104	0	1.54	1	19.75
11	112	1	1	1	0	1	104	0	1.68	0	50.28
11	113	0	1	0	0	1	104	0	1.68	1	35.02
11	114	0	0	1	0	1	104	0	1.68	2	50.28
11	115	0	0	1	0	1	104	0	1.54	0	19.75
11	116	0	0	1	0	1	104	0	1.54	1	19.75
11	117	0	.	1	0	1	117	0	1.54	1	19.75
11	118	1	.	1	0	2	118	0	1.54	1	4.49
11	119	0	.	0	1	2	119	0	1.40	0	35.02
11	120	0	.	0	0	1	120	0	1.54	1	35.02
11	121	0	0	0	0	2	120	0	1.40	1	65.55
11	122	0	0	0	0	1	120	0	1.68	0	65.55
11	123	0	0	0	0	1	120	0	1.40	0	65.55
11	124	0	0	0	0	1	120	0	1.54	1	19.75
11	125	0	0	0	0	1	120	0	1.26	0	35.02
11	126	1	.	1	0	1	126	0	1.40	0	80.81
11	127	0	.	0	0	1	127	0	1.40	1	35.02
11	128	1	.	1	0	1	128	0	1.54	1	19.75
11	129	1	.	1	0	1	129	0	1.54	1	50.28
11	130	1	.	1	0	1	130	0	1.40	0	50.28
11	131	1	.	1	0	1	131	0	1.54	1	19.75
11	132	1	.	1	0	.	132	0	1.26	0	50.28

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	83	75.18	0.74	1.35	0.68	1.47	0		0	.
11	84	75.65	0.73	1.37	0.68	1.47	0		0	.
11	85	77.35	0.76	1.32	0.76	1.32	1	0	0	1.47
11	86	79.25	0.78	1.28	0.76	1.32	0		0	.
11	87	77.95	0.73	1.36	0.76	1.32	0		0	.
11	88	137.97	0.79	1.27	0.79	1.27	1	1	0	1.32
11	89	48.48	0.80	1.25	0.80	1.25	1	2	0	1.27
11	90	45.91	0.81	1.24	0.80	1.25	0		1	.
11	91	136.86	0.71	1.41	0.71	1.41	1	3	0	1.27
11	92	139.00	0.70	1.43	0.71	1.41	0		1	.
11	93	145.84	0.77	1.31	0.80	1.25	0		0	.
11	94	142.47	0.75	1.32	0.71	1.41	0		0	.
11	95	50.58	0.75	1.34	0.76	1.31	0		1	.
11	96	148.54	0.76	1.31	0.76	1.31	1	1	0	1.27
11	97	140.70	0.77	1.31	0.76	1.31	0		0	.
11	98	142.74	0.77	1.30	0.76	1.31	0		0	.
11	99	81.95	0.76	1.31	0.76	1.31	0		0	.
11	100	53.45	0.75	1.33	0.76	1.31	0		0	.
11	101	152.35	0.76	1.31	0.76	1.31	0		0	.
11	102	83.15	0.75	1.33	0.76	1.31	0		0	.
11	103	89.09	0.76	1.32	0.76	1.32	1	2	0	1.31
11	104	91.56	0.75	1.33	0.75	1.33	1	1	0	1.31
11	105	86.22	0.72	1.39	0.72	1.39	1	3	0	1.31
11	106	158.39	0.75	1.34	0.75	1.33	0		1	.
11	107	159.99	0.75	1.34	0.75	1.33	0		0	.
11	108	88.99	0.74	1.35	0.75	1.33	0		0	.
11	109	92.03	0.74	1.35	0.75	1.33	0		0	.
11	110	164.46	0.72	1.39	0.75	1.33	0		0	.
11	111	165.96	0.73	1.37	0.75	1.33	0		0	.
11	112	86.39	0.71	1.41	0.75	1.33	0		0	.
11	113	94.60	0.72	1.40	0.75	1.33	0		0	.
11	114	94.17	0.71	1.41	0.75	1.33	0		0	.
11	115	172.20	0.70	1.42	0.75	1.33	0		0	.
11	116	170.73	0.69	1.45	0.75	1.33	0		0	.
11	117	173.50	0.71	1.41	0.71	1.41	1	2	0	1.33
11	118	178.54	0.68	1.48	0.68	1.48	1	3	0	1.33
11	119	99.30	0.70	1.43	0.70	1.43	1	1	0	1.33
11	120	96.40	0.69	1.45	0.69	1.45	1	0	0	1.43
11	121	55.15	0.70	1.44	0.69	1.45	0		1	.
11	122	56.29	0.68	1.48	0.69	1.45	0		0	.
11	123	56.95	0.69	1.45	0.69	1.45	0		0	.
11	124	180.68	0.67	1.49	0.69	1.45	0		0	.
11	125	104.64	0.67	1.48	0.69	1.45	0		0	.
11	126	54.35	0.68	1.47	0.68	1.47	1	2	0	1.45
11	127	106.64	0.66	1.52	0.66	1.52	1	3	0	1.45
11	128	186.21	0.67	1.49	0.67	1.49	1	1	0	1.45
11	129	101.24	0.67	1.48	0.67	1.48	1	2	0	1.49
11	130	102.61	0.65	1.55	0.65	1.55	1	3	0	1.49
11	131	190.45	0.66	1.51	0.66	1.51	1	1	0	1.49
11	132	103.51	0.62	1.62	0.62	1.62	1	0	0	1.51

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	133	0	0	0	0	1	132	0	1.68	0	19.75
11	134	0	0	1	0	1	132	0	1.54	1	19.75
11	135	0	0	1	0	1	136	0	1.26	2	35.02
11	136	0	.	0	0	.	136	0	1.12	1	35.02
11	137	0	0	1	0	1	136	0	1.40	1	19.75
11	138	0	.	0	0	2	138	0	0.98	1	19.75
11	139	1	1	1	0	1	138	0	1.26	2	35.02
11	140	0	1	1	0	1	138	0	1.40	1	19.75
11	141	0	0	1	0	1	138	0	1.54	2	19.75
11	142	0	0	0	0	1	138	0	1.54	1	65.55
11	143	1	1	1	0	1	138	0	1.40	2	19.75
11	144	1	.	1	0	.	144	0	1.40	1	65.55
11	145	0	.	1	0	1	145	0	1.12	0	80.81
11	146	0	.	0	0	1	146	0	0.84	1	19.75
11	147	1	1	1	1	1	146	0	1.12	2	19.75
11	148	1	0	1	0	1	146	0	1.12	1	19.75
11	149	0	.	0	0	1	149	0	1.40	2	35.02
11	150	0	.	0	0	1	150	0	1.26	1	35.02
11	151	0	0	1	1	1	150	0	1.40	2	50.28
11	152	0	.	1	0	.	152	0	1.12	1	19.75
11	154	1	.	1	0	1	154	0	1.26	2	35.02
11	155	0	1	1	0	.	154	0	1.26	1	35.02
11	156	1	1	1	0	1	154	0	1.54	0	35.02
11	157	1	0	0	0	2	154	0	1.40	0	65.55
11	158	0	1	1	0	1	154	0	1.40	2	19.75
11	159	0	0	1	0	1	154	0	1.40	1	19.75
11	160	0	0	0	1	1	154	0	1.54	1	50.28
11	161	0	0	0	0	1	154	0	1.54	2	35.02
11	162	0	0	0	0	1	154	0	1.83	1	35.02
11	163	1	1	1	0	2	154	0	1.54	2	65.55
11	164	1	0	1	0	1	154	0	1.54	1	35.02
11	165	0	1	0	0	2	154	0	1.54	1	19.75
11	166	1	1	1	0	1	154	0	1.40	1	19.75
11	167	1	.	0	0	.	167	0	1.26	0	19.75
11	168	0	.	0	0	2	168	0	1.40	1	65.55
11	169	1	.	1	0	1	169	0	1.40	0	65.55
11	170	0	.	0	0	1	170	0	1.68	0	50.28
11	171	0	0	1	0	2	170	0	1.40	1	19.75
11	172	1	.	0	0	.	172	0	1.68	1	19.75
11	173	0	.	1	1	.	173	0	1.40	1	19.75
11	174	0	.	1	0	1	174	0	1.54	0	19.75
11	175	0	.	0	0	2	175	0	1.54	1	35.02
11	176	1	1	0	0	1	175	0	1.68	0	65.55
11	177	1	.	1	0	1	177	0	1.54	0	35.02
11	178	0	.	0	0	1	178	0	1.54	1	35.02
11	179	1	.	1	0	1	179	0	1.68	1	35.02
11	180	0	.	0	0	1	180	0	1.68	0	50.28
11	181	0	0	0	0	2	180	0	1.54	1	50.28
11	182	0	.	1	0	1	182	0	1.68	2	35.02
11	183	0	0	0	0	1	182	0	1.83	1	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	133	193.76	0.65	1.54	0.62	1.62	0		0	.
11	134	192.19	0.62	1.61	0.62	1.62	0		1	.
11	135	108.85	0.60	1.68	0.60	1.68	0		1	.
11	136	102.34	0.60	1.68	0.60	1.68	1	0	0	1.62
11	137	198.66	0.61	1.64	0.60	1.68	0		0	.
11	138	200.70	0.60	1.66	0.60	1.66	1	0	0	1.68
11	139	114.99	0.60	1.68	0.60	1.66	0		1	.
11	140	202.30	0.60	1.65	0.60	1.66	0		0	.
11	141	203.23	0.60	1.66	0.60	1.66	0		0	.
11	142	58.72	0.61	1.63	0.60	1.66	0		0	.
11	143	205.67	0.62	1.62	0.60	1.66	0		0	.
11	144	60.56	0.63	1.59	0.63	1.59	1	1	0	1.66
11	145	55.85	0.64	1.57	0.64	1.57	1	0	0	1.59
11	146	212.27	0.63	1.58	0.63	1.58	1	0	0	1.57
11	147	212.91	0.63	1.60	0.63	1.58	0		1	.
11	148	214.48	0.65	1.55	0.63	1.58	0		0	.
11	149	118.26	0.64	1.56	0.64	1.56	1	1	0	1.58
11	150	115.75	0.66	1.53	0.66	1.53	1	1	0	1.56
11	151	112.45	0.66	1.53	0.66	1.53	0		1	.
11	152	220.68	0.65	1.54	0.65	1.54	1	0	0	1.53
11	154	122.49	0.64	1.57	0.64	1.57	1	1	0	1.54
11	155	121.46	0.64	1.57	0.64	1.57	0		1	.
11	156	123.86	0.64	1.55	0.64	1.57	0		0	.
11	157	61.63	0.64	1.57	0.64	1.57	0		0	.
11	158	227.79	0.62	1.60	0.64	1.57	0		0	.
11	159	227.02	0.62	1.60	0.64	1.57	0		0	.
11	160	116.05	0.64	1.57	0.64	1.57	0		0	.
11	161	131.90	0.64	1.57	0.64	1.57	0		0	.
11	162	134.34	0.65	1.55	0.64	1.57	0		0	.
11	163	66.96	0.65	1.54	0.64	1.57	0		0	.
11	164	139.41	0.65	1.54	0.64	1.57	0		0	.
11	165	235.36	0.65	1.55	0.64	1.57	0		0	.
11	166	236.46	0.66	1.51	0.64	1.57	0		0	.
11	167	238.97	0.65	1.53	0.65	1.53	1	0	0	1.57
11	168	63.33	0.69	1.45	0.69	1.45	1	2	0	1.53
11	169	63.06	0.66	1.51	0.66	1.51	1	3	0	1.53
11	170	127.87	0.70	1.44	0.70	1.44	1	2	0	1.53
11	171	243.27	0.69	1.45	0.70	1.44	0		1	.
11	172	245.54	0.68	1.47	0.68	1.47	1	0	0	1.53
11	173	249.14	0.68	1.48	0.68	1.48	1	0	0	1.47
11	174	256.65	0.79	1.27	0.79	1.27	1	2	0	1.48
11	175	144.01	0.67	1.49	0.67	1.49	1	3	0	1.48
11	176	65.26	0.65	1.55	0.67	1.49	0		1	.
11	177	167.97	0.69	1.46	0.69	1.46	1	2	0	1.48
11	178	148.52	0.65	1.55	0.65	1.55	1	3	0	1.48
11	179	170.71	0.66	1.51	0.66	1.51	1	1	0	1.48
11	180	144.48	0.69	1.45	0.69	1.45	1	1	0	1.51
11	181	142.01	0.69	1.46	0.69	1.45	0		1	.
11	182	176.01	0.68	1.47	0.68	1.47	1	0	0	1.45
11	183	261.99	0.68	1.47	0.68	1.47	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	184	1	1	1	0	.	185	0	1.68	2	65.55
11	185	0	.	0	0	1	185	0	1.68	1	65.55
11	186	0	0	1	0	1	185	0	1.83	1	19.75
11	187	1	1	1	0	2	185	0	1.54	1	65.55
11	188	0	0	1	0	1	185	0	1.68	0	80.81
11	189	1	.	1	0	1	189	0	1.26	0	35.02
11	190	0	1	0	0	1	189	0	1.54	1	35.02
11	191	0	0	1	0	1	189	0	1.54	0	35.02
11	192	0	.	1	0	2	192	0	1.26	1	50.28
11	193	0	0	1	0	1	192	0	1.54	0	50.28
11	194	1	1	1	0	1	192	0	1.68	0	80.81
11	195	1	0	1	1	1	192	0	1.68	1	35.02
11	196	1	0	1	0	1	192	0	1.83	2	35.02
11	197	1	0	1	0	1	192	0	1.68	1	80.81
11	198	1	.	1	0	.	198	0	1.68	1	19.75
11	199	1	0	1	0	1	198	0	1.68	1	50.28
11	200	0	1	0	0	1	198	0	1.83	1	50.28
11	201	1	1	1	0	1	198	0	1.83	1	19.75
11	202	1	.	1	0	1	202	0	1.68	2	35.02
11	203	0	1	0	0	1	202	0	1.68	1	35.02
11	204	1	1	1	0	1	202	0	1.97	2	35.02
11	205	1	0	1	0	1	202	0	1.97	1	35.02
11	206	1	.	1	0	1	206	0	1.68	1	96.08
11	207	0	.	0	0	1	207	0	1.83	2	35.02
11	208	1	.	1	0	1	208	0	1.97	1	50.28
11	209	1	.	1	0	1	209	0	1.83	2	35.02
11	210	1	.	1	0	1	210	0	1.83	1	50.28
11	211	0	1	1	0	1	210	0	1.97	2	35.02
11	212	1	.	1	0	1	212	0	2.11	1	50.28
11	213	1	.	1	1	2	213	0	1.68	1	96.08
11	214	0	1	1	0	1	213	0	1.68	1	35.02
11	215	0	0	0	0	1	213	0	1.54	1	35.02
11	216	0	0	0	0	2	213	0	1.54	1	65.55
11	217	0	.	0	0	2	217	0	1.26	1	65.55
11	218	1	.	0	0	.	218	0	1.26	1	50.28
11	219	0	.	1	1	2	219	0	1.26	1	65.55
11	220	0	0	0	0	2	219	0	1.40	1	50.28
11	221	0	.	0	0	.	221	0	0.98	1	96.08
11	222	1	1	0	0	1	221	0	1.12	1	96.08
11	223	0	1	0	0	2	221	0	1.12	1	50.28
11	224	0	0	1	1	2	221	0	1.12	1	50.28
11	225	0	.	1	0	3	225	0	1.12	1	65.55
11	226	0	.	1	0	2	226	0	1.12	1	65.55
11	227	1	.	0	0	.	227	0	1.12	1	65.55
11	228	0	1	1	0	2	227	0	1.26	1	50.28
11	229	1	.	1	0	.	229	0	1.12	1	50.28
11	230	0	1	0	0	1	229	0	1.26	1	50.28
11	231	1	.	1	1	2	231	0	1.12	1	50.28
11	232	1	.	1	1	.	232	0	0.70	1	50.28
11	233	0	1	0	0	1	232	0	0.84	1	80.81

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	184	69.87	0.66	1.51	0.66	1.53	0		1	.
11	185	68.53	0.66	1.53	0.66	1.53	1	0	0	1.47
11	186	267.00	0.67	1.50	0.66	1.53	0		0	.
11	187	71.84	0.69	1.46	0.66	1.53	0		0	.
11	188	69.03	0.67	1.50	0.66	1.53	0		0	.
11	189	180.85	0.68	1.46	0.68	1.46	1	0	0	1.53
11	190	178.48	0.67	1.49	0.68	1.46	0		1	.
11	191	187.09	0.71	1.41	0.68	1.46	0		0	.
11	192	180.35	0.72	1.39	0.72	1.39	1	0	0	1.46
11	193	180.95	0.70	1.42	0.72	1.39	0		1	.
11	194	71.54	0.71	1.40	0.72	1.39	0		0	.
11	195	191.66	0.75	1.34	0.72	1.39	0		0	.
11	196	199.57	0.74	1.35	0.72	1.39	0		0	.
11	197	74.51	0.73	1.38	0.72	1.39	0		0	.
11	198	282.74	0.71	1.41	0.71	1.41	1	0	0	1.39
11	199	186.66	0.71	1.40	0.71	1.41	0		1	.
11	200	188.69	0.73	1.37	0.71	1.41	0		0	.
11	201	287.55	0.74	1.36	0.71	1.41	0		0	.
11	202	217.15	0.72	1.38	0.72	1.38	1	0	0	1.41
11	203	205.74	0.73	1.38	0.72	1.38	0		1	.
11	204	226.03	0.72	1.39	0.72	1.38	0		0	.
11	205	226.53	0.72	1.40	0.72	1.38	0		0	.
11	206	55.38	0.74	1.36	0.74	1.36	1	2	0	1.38
11	207	232.80	0.70	1.43	0.70	1.43	1	3	0	1.38
11	208	192.46	0.72	1.39	0.72	1.39	1	1	0	1.38
11	209	241.28	0.77	1.30	0.77	1.30	1	2	0	1.39
11	210	196.57	0.71	1.41	0.71	1.41	1	3	0	1.39
11	211	243.58	0.69	1.45	0.71	1.41	0		1	.
11	212	210.75	0.73	1.38	0.73	1.38	1	1	0	1.39
11	213	58.79	0.72	1.39	0.72	1.39	1	0	0	1.38
11	214	247.08	0.74	1.36	0.72	1.39	0		1	.
11	215	251.62	0.75	1.34	0.72	1.39	0		0	.
11	216	74.74	0.75	1.33	0.72	1.39	0		0	.
11	217	73.17	0.75	1.34	0.75	1.34	1	0	0	1.39
11	218	238.68	0.72	1.38	0.72	1.38	1	0	0	1.34
11	219	77.34	0.73	1.37	0.73	1.37	1	1	0	1.38
11	220	251.86	0.73	1.36	0.73	1.37	0		1	.
11	221	50.25	0.76	1.32	0.76	1.32	1	0	0	1.37
11	222	57.29	0.77	1.31	0.76	1.32	0		1	.
11	223	263.13	0.78	1.29	0.76	1.32	0		0	.
11	224	264.54	0.78	1.28	0.76	1.32	0		0	.
11	225	78.81	0.79	1.26	0.79	1.26	1	0	0	1.32
11	226	81.98	0.79	1.26	0.79	1.26	1	0	0	1.26
11	227	83.28	0.77	1.29	0.77	1.29	1	0	0	1.26
11	228	272.14	0.79	1.27	0.77	1.29	0		1	.
11	229	274.15	0.76	1.31	0.76	1.31	1	0	0	1.29
11	230	275.95	0.77	1.29	0.76	1.31	0		1	.
11	231	277.55	0.78	1.29	0.78	1.29	1	1	0	1.31
11	232	280.82	0.78	1.28	0.78	1.28	1	0	0	1.29
11	233	81.71	0.79	1.26	0.78	1.28	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	234	1	.	1	0	2	234	0	0.84	1	65.55
11	235	1	0	1	0	1	234	0	0.98	1	65.55
11	236	0	1	0	0	2	234	0	1.12	1	50.28
11	237	1	1	1	0	2	234	0	1.26	1	50.28
11	238	1	0	1	1	1	234	0	1.26	1	50.28
11	239	0	1	1	0	1	234	0	1.40	1	50.28
11	240	1	.	0	0	.	240	0	1.40	1	50.28
11	241	1	0	0	0	1	240	0	1.40	2	50.28
11	242	0	1	1	1	1	240	0	1.40	1	80.81
11	243	0	0	1	0	1	240	0	1.40	2	80.81
11	244	0	0	1	0	1	240	0	1.40	1	80.81
11	245	0	0	0	0	1	240	0	1.40	1	65.55
11	246	0	.	1	0	1	246	0	1.40	2	50.28
11	247	0	0	0	0	1	246	0	1.40	1	50.28
11	248	1	1	0	0	1	246	0	1.40	1	96.08
11	249	1	0	0	0	2	246	0	1.26	1	50.28
11	250	1	0	1	0	1	246	0	1.26	0	50.28
11	251	1	.	1	0	1	251	0	1.26	1	96.08
11	252	0	.	1	0	2	252	0	1.12	1	65.55
11	253	0	.	1	0	1	253	0	1.12	2	50.28
11	254	1	.	1	0	.	254	0	0.84	0	50.28
11	255	1	0	1	0	1	254	0	0.98	1	80.81
11	256	0	1	0	1	1	254	0	1.12	1	80.81
11	257	0	.	1	0	2	257	0	1.12	1	65.55
11	258	0	.	0	0	.	258	0	0.98	1	65.55
11	259	0	.	0	0	2	259	0	0.98	1	50.28
11	260	1	.	1	0	.	260	0	0.84	1	50.28
11	261	0	1	1	0	1	260	0	0.98	1	50.28
11	263	1	.	1	0	.	263	0	0.70	1	50.28
11	264	1	0	1	0	1	263	0	0.98	1	50.28
11	265	0	1	1	0	2	263	0	0.98	1	65.55
11	266	1	.	0	0	2	266	0	0.84	1	50.28
11	267	0	1	1	0	2	266	0	0.98	1	80.81
11	268	0	0	0	0	1	266	0	1.12	2	80.81
11	269	0	0	1	0	1	266	0	1.26	1	50.28
11	270	0	0	0	0	2	266	0	1.26	1	80.81
11	271	0	0	1	0	2	266	0	1.26	1	50.28
11	272	1	.	1	0	2	272	0	1.12	1	65.55
11	273	1	.	1	0	3	273	0	0.98	1	111.35
11	274	1	.	1	0	3	274	0	0.98	1	50.28
11	275	1	.	1	0	3	275	0	0.98	1	50.28
11	276	0	1	0	0	1	275	0	1.12	1	50.28
11	277	0	0	0	0	2	275	0	0.98	1	50.28
11	278	0	.	0	0	3	278	0	0.98	1	80.81
11	279	0	.	1	0	1	279	0	1.26	2	65.55
11	280	1	.	0	0	1	280	0	1.12	1	65.55
11	281	0	1	0	0	2	280	0	1.26	1	65.55
11	282	1	.	1	0	2	282	0	1.26	1	65.55
11	283	1	.	1	0	2	283	0	1.26	1	80.81
11	284	1	0	0	0	1	283	0	1.40	1	80.81

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	234	85.05	0.80	1.26	0.80	1.26	1	0	0	1.28
11	235	86.02	0.81	1.23	0.80	1.26	0		1	.
11	236	289.19	0.81	1.23	0.80	1.26	0		0	.
11	237	290.53	0.81	1.24	0.80	1.26	0		0	.
11	238	291.96	0.82	1.23	0.80	1.26	0		0	.
11	239	293.70	0.82	1.21	0.80	1.26	0		0	.
11	240	295.97	0.83	1.21	0.83	1.21	1	0	0	1.26
11	241	295.33	0.79	1.26	0.83	1.21	0		1	.
11	242	84.35	0.82	1.23	0.83	1.21	0		0	.
11	243	85.42	0.79	1.27	0.83	1.21	0		0	.
11	244	86.02	0.80	1.25	0.83	1.21	0		0	.
11	245	88.29	0.82	1.23	0.83	1.21	0		0	.
11	246	308.81	0.79	1.26	0.79	1.26	1	0	0	1.21
11	247	308.41	0.78	1.28	0.79	1.26	0		1	.
11	248	60.39	0.79	1.27	0.79	1.26	0		0	.
11	249	312.78	0.79	1.27	0.79	1.26	0		0	.
11	250	311.05	0.79	1.26	0.79	1.26	0		0	.
11	251	61.79	0.78	1.29	0.78	1.29	1	0	0	1.26
11	252	90.79	0.79	1.26	0.79	1.26	1	1	0	1.29
11	253	321.13	0.82	1.22	0.82	1.22	1	1	0	1.26
11	254	318.89	0.78	1.28	0.78	1.28	1	0	0	1.22
11	255	88.19	0.80	1.25	0.78	1.28	0		1	.
11	256	88.89	0.80	1.25	0.78	1.28	0		0	.
11	257	94.06	0.83	1.21	0.83	1.21	1	0	0	1.28
11	258	95.73	0.83	1.20	0.83	1.20	1	1	0	1.21
11	259	329.83	0.83	1.20	0.83	1.20	1	0	0	1.20
11	260	332.00	0.80	1.24	0.80	1.24	1	0	0	1.20
11	261	335.51	0.83	1.20	0.80	1.24	0		1	.
11	263	338.44	0.79	1.27	0.79	1.27	1	0	0	1.24
11	264	339.81	0.80	1.26	0.79	1.27	0		1	.
11	265	100.03	0.80	1.25	0.79	1.27	0		0	.
11	266	343.51	0.80	1.26	0.80	1.26	1	0	0	1.27
11	267	95.09	0.80	1.25	0.80	1.26	0		1	.
11	268	94.03	0.78	1.28	0.80	1.26	0		0	.
11	269	353.29	0.79	1.26	0.80	1.26	0		0	.
11	270	99.30	0.79	1.26	0.80	1.26	0		0	.
11	271	361.70	0.80	1.25	0.80	1.26	0		0	.
11	272	102.63	0.80	1.25	0.80	1.25	1	0	0	1.26
11	273	63.86	0.79	1.26	0.79	1.26	1	0	0	1.25
11	274	367.74	0.81	1.24	0.81	1.24	1	0	0	1.26
11	275	369.24	0.78	1.28	0.78	1.28	1	0	0	1.24
11	276	370.81	0.78	1.28	0.78	1.28	0		1	.
11	277	372.68	0.78	1.29	0.78	1.28	0		0	.
11	278	105.47	0.78	1.28	0.78	1.28	1	0	0	1.28
11	279	400.33	1.09	0.91	1.09	0.91	1	2	0	1.28
11	280	110.78	0.77	1.29	0.77	1.29	1	0	0	1.28
11	281	121.25	0.77	1.29	0.77	1.29	0		1	.
11	282	130.19	0.78	1.28	0.78	1.28	1	0	0	1.29
11	283	107.94	0.76	1.32	0.76	1.32	1	3	0	1.28
11	284	109.01	0.76	1.32	0.76	1.32	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	285	1	.	1	0	.	285	0	0.98	1	96.08
11	286	0	1	1	0	1	285	0	1.12	1	65.55
11	287	0	0	0	0	1	285	0	1.12	1	80.81
11	288	0	0	0	0	1	285	0	1.12	1	96.08
11	289	1	1	1	0	1	285	0	1.12	1	96.08
11	290	1	0	1	0	1	285	0	1.26	1	96.08
11	291	1	.	1	0	3	291	0	1.26	1	80.81
11	292	1	.	1	0	.	292	0	0.98	1	80.81
11	293	1	0	0	0	1	292	0	1.26	1	96.08
11	294	1	0	0	0	1	292	0	1.26	1	96.08
11	295	1	.	1	0	.	295	0	0.98	1	80.81
11	296	0	.	0	0	2	296	0	0.98	1	96.08
11	297	1	1	0	0	1	296	0	1.12	1	96.08
11	298	1	.	1	0	3	298	0	1.12	1	96.08
11	299	0	1	1	0	1	298	0	1.12	1	80.81
11	300	1	1	1	0	2	298	0	1.26	1	65.55
11	301	1	0	1	0	1	298	0	1.26	1	65.55
11	302	1	0	1	0	1	298	0	1.26	1	65.55
11	303	0	.	0	0	2	303	0	1.26	1	80.81
11	304	1	1	1	0	2	303	0	1.26	1	80.81
11	305	1	0	1	0	1	303	0	1.26	1	65.55
11	306	1	.	1	0	3	306	0	1.12	1	65.55
11	307	0	.	0	0	2	307	0	1.12	1	80.81
11	308	1	.	1	0	.	308	0	0.98	1	65.55
11	309	1	0	1	0	1	308	0	1.12	1	65.55
11	310	1	.	1	0	.	310	0	0.98	1	96.08
11	311	0	1	1	0	1	310	0	1.12	0	96.08
11	312	0	0	1	0	2	310	0	1.26	1	65.55
11	313	1	.	1	0	.	313	0	1.12	1	65.55
11	314	0	1	0	0	2	313	0	1.12	1	96.08
11	315	1	1	1	0	1	313	0	1.26	1	80.81
11	316	0	1	0	0	1	313	0	1.26	1	80.81
11	317	1	.	1	0	.	317	0	1.12	0	111.35
11	318	1	0	1	0	1	317	0	1.26	1	111.35
11	319	1	.	0	1	.	319	0	1.12	1	111.35
11	320	1	.	1	0	2	320	0	1.26	1	80.81
11	321	1	.	1	0	.	321	0	1.26	1	80.81
11	322	0	1	1	0	1	321	0	1.40	1	65.55
11	323	0	0	1	0	2	321	0	1.40	1	80.81
11	324	1	.	0	0	3	324	0	1.12	1	96.08
11	325	1	0	1	0	1	324	0	1.26	1	96.08
11	326	1	.	1	0	.	326	0	1.26	1	96.08
11	327	0	1	1	0	1	326	0	1.40	2	96.08
11	328	1	1	1	0	1	326	0	1.40	1	80.81
11	329	1	0	0	0	1	326	0	1.40	1	80.81
11	330	1	.	1	1	.	330	0	1.26	1	80.81
11	331	1	0	1	0	1	330	0	1.54	1	80.81
11	332	0	.	1	0	.	332	0	1.26	1	96.08
11	333	0	0	0	0	1	332	0	1.54	1	96.08
11	334	0	0	0	0	2	332	0	1.40	1	96.08

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	285	72.33	0.74	1.35	0.74	1.35	1	0	0	1.28
11	286	131.10	0.76	1.32	0.74	1.35	0		1	.
11	287	126.06	0.76	1.32	0.74	1.35	0		0	.
11	288	73.57	0.77	1.30	0.74	1.35	0		0	.
11	289	74.54	0.78	1.29	0.74	1.35	0		0	.
11	290	75.74	0.78	1.28	0.74	1.35	0		0	.
11	291	160.16	0.79	1.27	0.79	1.27	1	0	0	1.35
11	292	294.63	0.76	1.31	0.76	1.31	1	0	0	1.27
11	293	77.97	0.77	1.30	0.76	1.31	0		1	.
11	294	77.07	0.78	1.28	0.76	1.31	0		0	.
11	295	298.93	0.77	1.30	0.77	1.30	1	0	0	1.31
11	296	79.94	0.77	1.30	0.77	1.30	1	0	0	1.30
11	297	78.94	0.78	1.29	0.77	1.30	0		1	.
11	298	81.04	0.76	1.31	0.76	1.31	1	0	0	1.30
11	299	305.17	0.76	1.32	0.76	1.31	0		1	.
11	300	322.29	0.75	1.34	0.76	1.31	0		0	.
11	301	327.59	0.70	1.43	0.76	1.31	0		0	.
11	302	328.66	0.70	1.43	0.76	1.31	0		0	.
11	303	310.11	0.70	1.42	0.70	1.42	1	1	0	1.31
11	304	308.17	0.70	1.43	0.70	1.42	0		1	.
11	305	333.33	0.71	1.41	0.70	1.42	0		0	.
11	306	345.48	0.69	1.45	0.69	1.45	1	0	0	1.42
11	307	312.28	0.70	1.42	0.70	1.42	1	1	0	1.45
11	308	346.81	0.68	1.47	0.68	1.47	1	0	0	1.42
11	309	349.35	0.68	1.46	0.68	1.47	0		1	.
11	310	83.78	0.65	1.55	0.65	1.55	1	0	0	1.47
11	311	85.51	0.66	1.52	0.65	1.55	0		1	.
11	312	354.39	0.66	1.51	0.65	1.55	0		0	.
11	313	358.69	0.65	1.55	0.65	1.55	1	0	0	1.55
11	314	87.22	0.65	1.54	0.65	1.55	0		1	.
11	315	353.08	0.65	1.54	0.65	1.55	0		0	.
11	316	355.02	0.66	1.51	0.65	1.55	0		0	.
11	317	89.25	0.65	1.54	0.65	1.54	1	0	0	1.55
11	318	86.15	0.66	1.53	0.65	1.54	0		1	.
11	319	87.72	0.64	1.57	0.64	1.57	1	0	0	1.54
11	320	363.23	0.65	1.54	0.65	1.54	1	0	0	1.57
11	321	362.53	0.62	1.61	0.62	1.61	1	0	0	1.54
11	322	396.69	0.64	1.57	0.62	1.61	0		1	.
11	323	366.50	0.64	1.56	0.62	1.61	0		0	.
11	324	89.18	0.63	1.58	0.63	1.58	1	0	0	1.61
11	325	90.59	0.64	1.56	0.63	1.58	0		1	.
11	326	93.49	0.63	1.59	0.63	1.59	1	0	0	1.58
11	327	95.92	0.62	1.60	0.63	1.59	0		1	.
11	328	381.41	0.63	1.58	0.63	1.59	0		0	.
11	329	384.52	0.64	1.56	0.63	1.59	0		0	.
11	330	409.37	0.62	1.61	0.62	1.61	1	0	0	1.59
11	331	412.51	0.63	1.59	0.62	1.61	0		1	.
11	332	104.17	0.61	1.63	0.61	1.63	1	0	0	1.61
11	333	97.06	0.62	1.61	0.61	1.63	0		1	.
11	334	98.06	0.63	1.59	0.61	1.63	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	335	0	0	0	0	2	332	0	1.40	1	80.81
11	336	0	0	0	0	1	332	0	1.40	1	80.81
11	337	0	.	1	0	.	337	0	1.26	1	96.08
11	338	0	.	1	0	.	338	0	0.98	1	111.35
11	339	0	.	1	0	1	339	0	0.98	0	80.81
11	340	0	0	1	0	1	339	0	1.12	1	80.81
11	341	0	.	0	0	1	341	0	0.98	1	80.81
11	342	1	.	1	0	2	342	0	0.98	1	96.08
11	343	0	1	0	0	1	342	0	1.26	1	80.81
11	344	0	.	1	0	.	344	0	1.12	1	111.35
11	345	1	.	1	0	2	345	0	1.26	1	111.35
11	346	1	.	1	0	1	346	0	1.40	1	96.08
11	347	0	.	1	0	.	347	0	1.54	1	111.35
11	348	0	.	1	0	.	348	0	0.98	1	111.35
11	349	1	.	1	0	.	349	0	0.84	1	111.35
11	350	1	.	1	0	3	350	0	0.84	1	111.35
11	351	1	.	0	0	.	351	0	0.98	1	111.35
11	352	1	0	1	0	1	351	0	1.12	1	96.08
11	353	1	0	1	1	1	351	0	0.98	1	50.28
11	354	0	1	0	0	2	351	0	1.12	1	50.28
11	356	0	.	1	0	.	356	0	0.28	0	96.08
11	357	0	0	1	0	1	356	0	0.56	0	96.08
11	358	1	.	1	1	.	358	0	0.28	1	96.08
11	359	0	1	1	0	1	358	0	0.56	1	96.08
11	360	0	.	1	0	.	360	0	0.28	1	80.81
11	361	0	.	1	0	.	361	0	0.28	2	96.08
11	16.01	1	.	1	0	.	16	0	0.70	1	4.49
11	27.01	0	.	0	0	.	27	0	1.12	0	4.49
11	28.01	0	.	1	0	.	28	0	0.98	1	4.49
11	29.01	1	.	1	0	.	29	0	0.56	0	19.75
11	30.01	0	.	0	0	1	30	0	1.12	1	4.49
11	32.01	1	.	0	0	1	32	0	1.40	2	19.75
11	33.01	1	0	1	0	1	32	0	1.54	1	19.75
11	37.01	0	.	1	0	1	37	0	2.11	2	19.75
11	38.01	0	.	1	0	2	38	0	1.97	0	19.75
11	40.01	0	.	0	0	1	40	0	2.39	2	19.75
11	46.01	0	.	0	0	1	46	0	1.97	1	4.49
11	50.01	0	.	0	0	1	50	0	2.11	0	4.49
11	51.01	0	0	1	0	1	50	0	2.25	2	4.49
11	55.01	0	.	1	0	1	55	0	2.11	0	4.49
11	59.01	1	1	1	0	1	55	0	2.25	2	19.75
11	61.01	1	.	1	0	1	61	0	2.11	2	19.75
11	63.01	0	.	1	0	1	63	0	2.11	0	35.02
11	65.01	1	.	0	0	1	65	0	1.83	0	4.49
11	68.01	1	.	0	0	1	68	0	1.97	2	4.49
11	73.01	1	.	1	0	1	73	0	2.25	1	4.49
11	74.01	0	1	0	0	1	73	0	2.25	0	4.49
11	75.01	1	.	0	0	1	75	0	2.53	0	4.49
11	76.01	0	.	1	0	1	76	0	2.67	0	4.49
11	78.01	1	.	1	0	1	78	0	2.39	1	35.02

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	335	422.32	0.63	1.58	0.61	1.63	0		0	.
11	336	424.16	0.64	1.55	0.61	1.63	0		0	.
11	337	100.33	0.64	1.56	0.64	1.56	1	0	0	1.63
11	338	197.09	0.64	1.55	0.64	1.55	1	0	0	1.56
11	339	429.83	0.83	1.20	0.83	1.20	1	0	0	1.55
11	340	430.80	0.88	1.13	0.83	1.20	0		1	.
11	341	432.50	0.89	1.13	0.89	1.13	1	0	0	1.20
11	342	103.03	0.88	1.14	0.88	1.14	1	0	0	1.13
11	343	436.10	0.89	1.13	0.88	1.14	0		1	.
11	344	173.84	0.90	1.11	0.90	1.11	1	0	0	1.14
11	345	173.34	0.90	1.11	0.90	1.11	1	0	0	1.11
11	346	206.50	0.93	1.07	0.93	1.07	1	0	0	1.11
11	347	92.65	0.91	1.10	0.91	1.10	1	0	0	1.07
11	348	110.01	0.78	1.29	0.78	1.29	1	0	0	1.10
11	349	110.67	0.77	1.30	0.77	1.30	1	0	0	1.29
11	350	208.40	0.75	1.33	0.75	1.33	1	0	0	1.30
11	351	242.04	0.72	1.38	0.72	1.38	1	0	0	1.33
11	352	350.88	0.74	1.35	0.72	1.38	0		1	.
11	353	503.71	0.75	1.33	0.72	1.38	0		0	.
11	354	505.74	0.77	1.31	0.72	1.38	0		0	.
11	356	491.85	0.81	1.23	0.81	1.23	1	0	0	1.38
11	357	493.09	0.80	1.26	0.81	1.23	0		1	.
11	358	189.32	0.95	1.05	0.95	1.05	1	0	0	1.23
11	359	351.81	0.99	1.01	0.95	1.05	0		1	.
11	360	583.55	0.59	1.70	0.59	1.70	1	0	0	1.05
11	361	727.76	0.53	1.88	0.53	1.88	1	0	0	1.70
11	16.01	47.22	1.29	0.78	1.29	0.78	1	0	0	.
11	27.01	56.06	0.99	1.01	0.99	1.01	1	1	0	0.78
11	28.01	57.16	0.95	1.05	0.95	1.05	1	0	0	1.01
11	29.01	56.03	0.95	1.05	0.95	1.05	1	2	0	1.05
11	30.01	58.06	0.91	1.10	0.91	1.10	1	3	0	1.05
11	32.01	58.40	0.88	1.13	0.88	1.13	1	1	0	1.05
11	33.01	58.26	0.89	1.13	0.88	1.13	0		1	.
11	37.01	61.10	0.83	1.21	0.83	1.21	1	2	0	1.13
11	38.01	60.36	0.78	1.28	0.78	1.28	1	4	0	1.13
11	40.01	63.27	0.78	1.28	0.78	1.28	1	1	0	1.28
11	46.01	59.36	0.74	1.35	0.74	1.35	1	3	0	1.28
11	50.01	62.50	0.72	1.39	0.72	1.39	1	4	0	1.28
11	51.01	64.67	0.72	1.38	0.72	1.39	0		1	.
11	55.01	65.40	0.69	1.46	0.69	1.46	1	4	0	1.39
11	59.01	64.94	0.68	1.47	0.69	1.46	0		1	.
11	61.01	66.77	0.69	1.46	0.69	1.46	1	3	0	1.46
11	63.01	38.64	0.75	1.34	0.75	1.34	1	2	0	1.46
11	65.01	67.97	0.64	1.55	0.64	1.55	1	4	0	1.46
11	68.01	74.25	0.67	1.49	0.67	1.49	1	2	0	1.55
11	73.01	70.31	0.56	1.80	0.56	1.80	1	0	0	1.55
11	74.01	72.01	0.57	1.74	0.56	1.80	0		1	.
11	75.01	75.88	0.59	1.69	0.59	1.69	1	2	0	1.80
11	76.01	78.28	0.59	1.71	0.59	1.71	1	4	0	1.80
11	78.01	41.74	0.53	1.87	0.53	1.87	1	3	0	1.71

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	83.01	0	.	1	0	.	83	0	2.11	1	19.75
11	84.01	0	0	1	0	1	83	0	2.39	2	19.75
11	85.01	0	1	1	0	1	87	0	1.97	0	19.75
11	86.01	0	1	1	0	1	87	0	2.39	0	19.75
11	87.01	1	.	1	0	1	87	0	2.11	0	19.75
11	89.01	0	.	1	0	1	89	1	2.81	2	35.02
11	90.01	0	0	1	0	1	89	1	2.95	2	35.02
11	95.01	0	0	1	0	1	89	1	3.23	2	35.02
11	99.01	0	.	0	0	1	99	1	3.51	1	4.49
11	100.01	0	0	0	0	1	89	1	2.95	2	35.02
11	102.01	1	.	1	0	1	102	1	2.95	0	19.75
11	103.01	0	.	0	0	1	103	1	2.95	0	4.49
11	104.01	0	0	0	0	1	103	1	2.81	0	4.49
11	105.01	0	.	0	0	1	105	1	2.95	1	4.49
11	108.01	0	0	0	0	1	103	1	2.95	2	19.75
11	109.01	0	0	0	0	1	103	1	2.81	2	19.75
11	112.01	1	.	1	0	1	112	1	2.81	0	19.75
11	113.01	0	.	0	0	1	113	1	2.67	1	4.49
11	114.01	0	.	1	0	1	114	1	2.53	2	19.75
11	119.01	0	.	0	1	1	119	1	2.53	0	4.49
11	120.01	0	.	0	0	1	120	1	2.67	1	4.49
11	121.01	0	.	0	0	1	121	0	2.67	1	35.02
11	122.01	0	0	0	0	1	121	0	2.67	2	35.02
11	123.01	0	.	0	0	1	123	0	2.67	2	35.02
11	125.01	0	.	0	0	1	125	0	2.81	0	4.49
11	126.01	1	.	1	0	1	126	0	2.53	2	50.28
11	127.01	0	.	0	0	1	127	0	2.95	1	4.49
11	129.01	1	.	1	0	1	129	0	2.81	1	19.75
11	130.01	1	.	1	0	1	130	0	2.67	2	19.75
11	132.01	1	.	1	0	1	132	0	2.81	2	19.75
11	135.01	0	.	1	0	1	135	0	2.81	0	4.49
11	136.01	0	.	0	0	.	136	0	2.53	1	4.49
11	139.01	1	.	1	0	1	139	0	2.39	2	4.49
11	142.01	0	.	0	0	1	142	0	2.81	1	35.02
11	144.01	1	.	1	0	.	144	0	2.81	1	35.02
11	145.01	0	1	1	0	1	144	0	2.81	2	50.28
11	149.01	0	.	0	0	1	149	0	2.53	2	4.49
11	150.01	0	0	0	0	1	149	0	2.39	1	4.49
11	151.01	0	0	1	1	1	149	0	2.81	2	19.75
11	154.01	1	1	1	0	1	155	0	2.67	2	4.49
11	155.01	0	.	1	0	.	155	0	2.39	1	4.49
11	156.01	1	0	1	0	1	155	0	2.95	1	4.49
11	157.01	1	0	0	0	1	155	0	2.39	2	35.02
11	160.01	0	.	0	1	1	160	0	2.67	0	19.75
11	161.01	0	.	0	0	1	161	0	2.81	2	4.49
11	162.01	0	.	0	0	1	162	0	3.09	1	4.49
11	163.01	1	.	1	0	1	163	0	2.53	2	35.02
11	164.01	1	.	1	0	1	164	0	2.81	1	4.49
11	168.01	0	.	0	0	1	168	0	2.81	1	35.02
11	169.01	1	.	1	0	1	169	0	2.81	2	35.02

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	83.01	75.18	0.50	1.99	0.50	1.99	1	1	0	1.71
11	84.01	75.65	0.50	2.00	0.50	1.99	0		1	.
11	85.01	77.35	0.50	1.99	0.50	2.00	0		1	.
11	86.01	79.25	0.49	2.03	0.50	2.00	0		0	.
11	87.01	77.95	0.50	2.00	0.50	2.00	1	1	0	1.99
11	89.01	48.48	0.47	2.13	0.47	2.13	1	2	0	2.00
11	90.01	45.91	0.47	2.12	0.47	2.13	0		1	.
11	95.01	50.58	0.47	2.14	0.47	2.13	0		0	.
11	99.01	81.95	0.40	2.47	0.40	2.47	1	1	0	2.00
11	100.01	53.45	0.43	2.32	0.47	2.13	0		0	.
11	102.01	83.15	0.40	2.47	0.40	2.47	1	3	0	2.47
11	103.01	89.09	0.40	2.48	0.40	2.48	1	2	0	2.47
11	104.01	91.56	0.40	2.48	0.40	2.48	0		1	.
11	105.01	86.22	0.39	2.58	0.39	2.58	1	3	0	2.47
11	108.01	88.99	0.40	2.49	0.40	2.48	0		0	.
11	109.01	92.03	0.41	2.44	0.40	2.48	0		0	.
11	112.01	86.39	0.38	2.62	0.38	2.62	1	2	0	2.47
11	113.01	94.60	0.36	2.75	0.36	2.75	1	3	0	2.47
11	114.01	94.17	0.39	2.55	0.39	2.55	1	2	0	2.47
11	119.01	99.30	0.37	2.72	0.37	2.72	1	2	0	2.47
11	120.01	96.40	0.35	2.86	0.35	2.86	1	3	0	2.47
11	121.01	55.15	0.36	2.75	0.36	2.75	1	1	0	2.47
11	122.01	56.29	0.36	2.75	0.36	2.75	0		1	.
11	123.01	56.95	0.36	2.74	0.36	2.74	1	1	0	2.75
11	125.01	104.64	0.37	2.73	0.37	2.73	1	1	0	2.74
11	126.01	54.35	0.36	2.81	0.36	2.81	1	3	0	2.73
11	127.01	106.64	0.38	2.66	0.38	2.66	1	2	0	2.73
11	129.01	101.24	0.35	2.84	0.35	2.84	1	3	0	2.73
11	130.01	102.61	0.36	2.80	0.36	2.80	1	2	0	2.73
11	132.01	103.51	0.36	2.79	0.36	2.79	1	4	0	2.73
11	135.01	108.85	0.35	2.87	0.35	2.87	1	1	0	2.79
11	136.01	102.34	0.31	3.23	0.31	3.23	1	3	0	2.79
11	139.01	114.99	0.34	2.94	0.34	2.94	1	4	0	2.87
11	142.01	58.72	0.33	2.99	0.33	2.99	1	4	0	2.94
11	144.01	60.56	0.33	3.04	0.33	3.04	1	0	0	2.99
11	145.01	55.85	0.32	3.08	0.33	3.04	0		1	.
11	149.01	118.26	0.32	3.17	0.32	3.17	1	1	0	3.04
11	150.01	115.75	0.31	3.19	0.32	3.17	0		1	.
11	151.01	112.45	0.32	3.15	0.32	3.17	0		0	.
11	154.01	122.49	0.31	3.19	0.31	3.26	0		1	.
11	155.01	121.46	0.31	3.26	0.31	3.26	1	0	0	3.17
11	156.01	123.86	0.31	3.24	0.31	3.26	0		0	.
11	157.01	61.63	0.31	3.22	0.31	3.26	0		0	.
11	160.01	116.05	0.30	3.29	0.30	3.29	1	4	0	3.26
11	161.01	131.90	0.34	2.90	0.34	2.90	1	2	0	3.29
11	162.01	134.34	0.33	3.00	0.33	3.00	1	3	0	3.29
11	163.01	66.96	0.40	2.48	0.40	2.48	1	2	0	3.29
11	164.01	139.41	0.39	2.55	0.39	2.55	1	3	0	3.29
11	168.01	63.33	0.33	2.99	0.33	2.99	1	3	0	3.29
11	169.01	63.06	0.34	2.91	0.34	2.91	1	2	0	3.29

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	170.01	0	.	0	0	1	170	1	3.23	2	19.75
11	175.01	0	.	0	0	1	175	1	2.67	1	4.49
11	176.01	1	1	0	0	1	170	1	2.81	2	35.02
11	177.01	1	0	1	0	1	170	1	2.81	2	4.49
11	178.01	0	0	0	0	1	175	1	3.09	1	4.49
11	179.01	1	.	1	0	1	179	0	2.95	1	4.49
11	180.01	0	.	0	0	1	180	0	2.81	2	19.75
11	181.01	0	.	0	0	1	181	0	2.67	1	19.75
11	182.01	0	.	1	0	1	182	0	2.95	0	4.49
11	184.01	1	1	1	0	1	185	0	3.23	2	35.02
11	185.01	0	.	0	0	1	185	0	2.95	1	35.02
11	187.01	1	.	1	0	1	187	0	2.67	1	35.02
11	188.01	0	1	1	0	1	187	0	2.81	2	50.28
11	189.01	1	0	1	0	1	187	0	2.39	2	4.49
11	190.01	0	1	0	0	1	187	0	2.53	1	4.49
11	191.01	0	0	1	0	1	187	0	2.53	1	4.49
11	192.01	0	0	1	0	1	187	0	2.25	1	19.75
11	193.01	0	0	1	0	1	187	0	2.67	2	19.75
11	194.01	1	1	1	0	1	187	0	2.67	2	50.28
11	195.01	1	0	1	1	1	187	0	3.09	1	4.49
11	196.01	1	0	1	0	1	187	0	3.37	2	4.49
11	197.01	1	0	1	0	1	187	0	2.67	1	50.28
11	199.01	1	.	1	0	1	199	0	2.53	1	19.75
11	200.01	0	1	0	0	1	199	0	2.95	1	19.75
11	202.01	1	.	1	0	1	202	0	2.95	2	4.49
11	203.01	0	1	0	0	1	202	0	2.95	1	4.49
11	204.01	1	1	1	0	1	202	0	2.81	2	4.49
11	205.01	1	0	1	0	1	202	0	3.09	1	4.49
11	206.01	1	.	1	0	1	206	0	2.95	1	65.55
11	207.01	0	.	0	0	1	207	0	2.95	0	4.49
11	208.01	1	0	1	0	1	206	0	3.51	1	19.75
11	209.01	1	.	1	0	2	209	0	2.53	0	4.49
11	210.01	1	.	1	0	1	210	0	3.23	1	19.75
11	211.01	0	.	1	0	1	211	0	2.81	0	4.49
11	212.01	1	0	1	0	1	209	0	3.23	1	19.75
11	213.01	1	.	1	1	1	213	0	3.23	1	65.55
11	214.01	0	1	1	0	1	213	0	2.53	1	4.49
11	215.01	0	0	0	0	1	213	0	2.25	0	4.49
11	216.01	0	0	0	0	1	213	0	2.67	0	35.02
11	217.01	0	0	0	0	1	213	0	2.67	1	35.02
11	218.01	1	.	0	0	1	218	0	2.25	1	19.75
11	219.01	0	.	1	1	1	219	0	2.25	1	35.02
11	220.01	0	0	0	0	1	219	0	2.25	1	19.75
11	221.01	0	.	0	0	.	221	0	1.83	1	65.55
11	222.01	1	1	0	0	1	221	0	1.68	0	65.55
11	223.01	0	1	0	0	2	221	0	1.54	1	19.75
11	224.01	0	0	1	1	1	221	0	1.68	1	19.75
11	225.01	0	.	1	0	2	225	0	1.68	1	35.02
11	226.01	0	0	1	0	2	225	0	1.83	1	35.02
11	227.01	1	.	0	0	3	227	0	1.83	1	35.02

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	170.01	127.87	0.35	2.83	0.35	2.83	1	2	0	3.29
11	175.01	144.01	0.32	3.14	0.32	3.14	1	3	0	3.29
11	176.01	65.26	0.33	2.99	0.35	2.83	0		1	.
11	177.01	167.97	0.33	3.07	0.35	2.83	0		0	.
11	178.01	148.52	0.32	3.08	0.32	3.14	0		1	.
11	179.01	170.71	0.33	3.06	0.33	3.06	1	1	0	3.29
11	180.01	144.48	0.32	3.08	0.32	3.08	1	2	0	3.06
11	181.01	142.01	0.32	3.15	0.32	3.15	1	3	0	3.06
11	182.01	176.01	0.32	3.14	0.32	3.14	1	1	0	3.06
11	184.01	69.87	0.32	3.12	0.32	3.11	0		0	.
11	185.01	68.53	0.32	3.11	0.32	3.11	1	4	0	3.14
11	187.01	71.84	0.33	2.99	0.33	2.99	1	3	0	3.11
11	188.01	69.03	0.34	2.95	0.33	2.99	0		1	.
11	189.01	180.85	0.35	2.86	0.33	2.99	0		0	.
11	190.01	178.48	0.35	2.84	0.33	2.99	0		0	.
11	191.01	187.09	0.35	2.83	0.33	2.99	0		0	.
11	192.01	180.35	0.37	2.71	0.33	2.99	0		0	.
11	193.01	180.95	0.37	2.74	0.33	2.99	0		0	.
11	194.01	71.54	0.40	2.47	0.33	2.99	0		0	.
11	195.01	191.66	0.39	2.54	0.33	2.99	0		0	.
11	196.01	199.57	0.40	2.51	0.33	2.99	0		0	.
11	197.01	74.51	0.40	2.49	0.33	2.99	0		0	.
11	199.01	186.66	0.40	2.52	0.40	2.52	1	1	0	3.11
11	200.01	188.69	0.40	2.50	0.40	2.52	0		1	.
11	202.01	217.15	0.41	2.45	0.41	2.45	1	1	0	2.52
11	203.01	205.74	0.41	2.47	0.41	2.45	0		1	.
11	204.01	226.03	0.41	2.45	0.41	2.45	0		0	.
11	205.01	226.53	0.41	2.45	0.41	2.45	0		0	.
11	206.01	55.38	0.41	2.45	0.41	2.45	1	3	0	2.45
11	207.01	232.80	0.45	2.23	0.45	2.23	1	2	0	2.45
11	208.01	192.46	0.41	2.45	0.41	2.45	0		1	.
11	209.01	241.28	0.44	2.29	0.44	2.29	1	3	0	2.31
11	210.01	196.57	0.43	2.31	0.43	2.31	1	1	0	2.45
11	211.01	243.58	0.48	2.07	0.48	2.07	1	2	0	2.31
11	212.01	210.75	0.45	2.24	0.44	2.29	0		1	.
11	213.01	58.79	0.46	2.15	0.46	2.15	1	1	0	2.31
11	214.01	247.08	0.46	2.16	0.46	2.15	0		1	.
11	215.01	251.62	0.46	2.16	0.46	2.15	0		0	.
11	216.01	74.74	0.46	2.15	0.46	2.15	0		0	.
11	217.01	73.17	0.47	2.13	0.46	2.15	0		0	.
11	218.01	238.68	0.47	2.12	0.47	2.12	1	0	0	2.15
11	219.01	77.34	0.47	2.14	0.47	2.14	1	0	0	2.12
11	220.01	251.86	0.47	2.13	0.47	2.14	0		1	.
11	221.01	50.25	0.46	2.16	0.46	2.16	1	0	0	2.14
11	222.01	57.29	0.46	2.15	0.46	2.16	0		1	.
11	223.01	263.13	0.47	2.14	0.46	2.16	0		0	.
11	224.01	264.54	0.47	2.12	0.46	2.16	0		0	.
11	225.01	78.81	0.48	2.09	0.48	2.09	1	0	0	2.16
11	226.01	81.98	0.49	2.06	0.48	2.09	0		1	.
11	227.01	83.28	0.49	2.05	0.49	2.05	1	0	0	2.09

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	228.01	0	1	1	0	2	227	0	1.83	1	19.75
11	229.01	1	.	1	0	.	229	0	1.83	1	19.75
11	230.01	0	1	0	0	1	229	0	1.83	1	19.75
11	231.01	1	.	1	1	1	231	0	1.68	1	19.75
11	232.01	1	.	1	1	.	232	0	1.40	1	19.75
11	233.01	0	1	0	0	1	232	0	1.40	1	50.28
11	234.01	1	.	1	0	2	234	0	1.40	1	35.02
11	235.01	1	0	1	0	2	234	0	1.54	1	35.02
11	236.01	0	1	0	0	2	234	0	1.68	1	19.75
11	237.01	1	1	1	0	1	234	0	1.83	1	19.75
11	238.01	1	0	1	1	1	234	0	1.83	1	19.75
11	239.01	0	1	1	0	2	234	0	2.11	1	19.75
11	240.01	1	0	0	0	.	241	0	2.25	1	19.75
11	241.01	1	.	0	0	1	241	0	2.11	2	19.75
11	242.01	0	1	1	1	1	241	0	2.11	1	50.28
11	243.01	0	0	1	0	1	241	0	2.11	2	50.28
11	244.01	0	0	1	0	1	241	0	2.25	1	50.28
11	245.01	0	0	0	0	1	241	0	2.11	1	35.02
11	246.01	0	0	1	0	1	241	0	2.11	2	19.75
11	247.01	0	0	0	0	2	241	0	1.83	1	19.75
11	248.01	1	1	0	0	1	241	0	1.97	0	65.55
11	249.01	1	0	0	0	1	241	0	1.83	1	19.75
11	250.01	1	0	1	0	1	241	0	1.97	0	19.75
11	251.01	1	0	1	0	1	241	0	1.97	1	65.55
11	252.01	0	.	1	0	3	252	0	1.68	1	35.02
11	253.01	0	.	1	0	1	253	0	1.40	0	19.75
11	254.01	1	.	1	0	.	254	0	1.26	1	19.75
11	255.01	1	.	1	0	1	255	0	1.26	1	50.28
11	256.01	0	.	0	1	1	256	0	1.54	1	50.28
11	257.01	0	0	1	0	2	256	0	1.54	1	35.02
11	258.01	0	.	0	0	.	258	0	1.40	1	35.02
11	259.01	0	.	0	0	2	259	0	1.68	1	19.75
11	260.01	1	.	1	0	2	260	0	1.68	1	19.75
11	261.01	0	.	1	0	2	261	0	1.40	1	19.75
11	263.01	1	.	1	0	2	263	0	1.26	1	19.75
11	264.01	1	0	1	0	1	263	0	1.40	1	19.75
11	265.01	0	.	1	0	2	265	0	1.54	1	35.02
11	266.01	1	1	0	0	2	265	0	1.68	1	19.75
11	267.01	0	1	1	0	2	265	0	1.68	1	50.28
11	268.01	0	0	0	0	1	265	0	1.83	0	50.28
11	269.01	0	0	1	0	1	265	0	1.97	1	19.75
11	270.01	0	0	0	0	1	265	0	1.68	1	50.28
11	271.01	0	0	1	0	2	265	0	1.68	1	19.75
11	272.01	1	1	1	0	2	265	0	1.68	1	35.02
11	273.01	1	.	1	0	3	273	0	1.40	1	80.81
11	274.01	1	.	1	0	2	274	0	1.40	1	19.75
11	275.01	1	.	1	0	2	275	0	1.40	1	19.75
11	276.01	0	.	0	0	1	276	0	1.40	1	19.75
11	277.01	0	.	0	0	2	277	0	1.54	1	19.75
11	278.01	0	.	0	0	3	278	0	1.40	1	50.28

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	228.01	272.14	0.49	2.05	0.49	2.05	0		1	.
11	229.01	274.15	0.49	2.05	0.49	2.05	1	0	0	2.05
11	230.01	275.95	0.49	2.03	0.49	2.05	0		1	.
11	231.01	277.55	0.49	2.03	0.49	2.03	1	0	0	2.05
11	232.01	280.82	0.46	2.17	0.46	2.17	1	0	0	2.03
11	233.01	81.71	0.46	2.16	0.46	2.17	0		1	.
11	234.01	85.05	0.47	2.14	0.47	2.14	1	1	0	2.17
11	235.01	86.02	0.47	2.14	0.47	2.14	0		1	.
11	236.01	289.19	0.47	2.12	0.47	2.14	0		0	.
11	237.01	290.53	0.47	2.11	0.47	2.14	0		0	.
11	238.01	291.96	0.47	2.11	0.47	2.14	0		0	.
11	239.01	293.70	0.48	2.09	0.47	2.14	0		0	.
11	240.01	295.97	0.48	2.10	0.47	2.13	0		1	.
11	241.01	295.33	0.47	2.13	0.47	2.13	1	1	0	2.14
11	242.01	84.35	0.48	2.10	0.47	2.13	0		0	.
11	243.01	85.42	0.48	2.06	0.47	2.13	0		0	.
11	244.01	86.02	0.48	2.09	0.47	2.13	0		0	.
11	245.01	88.29	0.48	2.08	0.47	2.13	0		0	.
11	246.01	308.81	0.48	2.07	0.47	2.13	0		0	.
11	247.01	308.41	0.48	2.08	0.47	2.13	0		0	.
11	248.01	60.39	0.48	2.08	0.47	2.13	0		0	.
11	249.01	312.78	0.50	2.00	0.47	2.13	0		0	.
11	250.01	311.05	0.47	2.11	0.47	2.13	0		0	.
11	251.01	61.79	0.50	2.00	0.47	2.13	0		0	.
11	252.01	90.79	0.50	2.00	0.50	2.00	1	0	0	2.13
11	253.01	321.13	0.53	1.90	0.53	1.90	1	2	0	2.00
11	254.01	318.89	0.50	2.00	0.50	2.00	1	3	0	2.00
11	255.01	88.19	0.52	1.93	0.52	1.93	1	1	0	2.00
11	256.01	88.89	0.53	1.90	0.53	1.90	1	1	0	1.93
11	257.01	94.06	0.53	1.88	0.53	1.90	0		1	.
11	258.01	95.73	0.58	1.73	0.58	1.73	1	0	0	1.90
11	259.01	329.83	0.59	1.71	0.59	1.71	1	1	0	1.73
11	260.01	332.00	0.60	1.67	0.60	1.67	1	0	0	1.71
11	261.01	335.51	0.63	1.58	0.63	1.58	1	1	0	1.67
11	263.01	338.44	0.64	1.57	0.64	1.57	1	0	0	1.58
11	264.01	339.81	0.63	1.58	0.64	1.57	0		1	.
11	265.01	100.03	0.63	1.58	0.63	1.58	1	1	0	1.57
11	266.01	343.51	0.63	1.60	0.63	1.58	0		1	.
11	267.01	95.09	0.63	1.58	0.63	1.58	0		0	.
11	268.01	94.03	0.64	1.56	0.63	1.58	0		0	.
11	269.01	353.29	0.64	1.55	0.63	1.58	0		0	.
11	270.01	99.30	0.64	1.56	0.63	1.58	0		0	.
11	271.01	361.70	0.64	1.56	0.63	1.58	0		0	.
11	272.01	102.63	0.64	1.55	0.63	1.58	0		0	.
11	273.01	63.86	0.64	1.55	0.64	1.55	1	0	0	1.58
11	274.01	367.74	0.63	1.59	0.63	1.59	1	0	0	1.55
11	275.01	369.24	0.63	1.58	0.63	1.58	1	0	0	1.59
11	276.01	370.81	0.64	1.56	0.64	1.56	1	1	0	1.58
11	277.01	372.68	0.64	1.56	0.64	1.56	1	1	0	1.56
11	278.01	105.47	0.64	1.56	0.64	1.56	1	0	0	1.56

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	279.01	0	.	1	0	1	279	0	1.83	2	35.02
11	280.01	1	1	0	0	1	278	0	1.40	1	35.02
11	281.01	0	1	0	0	2	278	0	1.40	1	35.02
11	282.01	1	1	1	0	2	278	0	1.40	1	35.02
11	283.01	1	0	1	0	2	278	0	1.54	1	50.28
11	284.01	1	0	0	0	1	278	0	1.68	1	50.28
11	285.01	1	.	1	0	.	285	0	1.54	1	65.55
11	286.01	0	1	1	0	1	285	0	1.54	1	35.02
11	287.01	0	0	0	0	1	285	0	1.54	1	50.28
11	288.01	0	0	0	0	1	285	0	1.54	1	65.55
11	289.01	1	1	1	0	1	285	0	1.54	1	65.55
11	290.01	1	0	1	0	1	285	0	1.68	1	65.55
11	291.01	1	.	1	0	2	291	0	1.83	1	50.28
11	292.01	1	.	1	0	.	292	0	1.54	1	50.28
11	293.01	1	0	0	0	1	292	0	1.68	1	65.55
11	294.01	1	0	0	0	1	292	0	1.68	1	65.55
11	295.01	1	.	1	0	.	295	0	1.54	1	50.28
11	296.01	0	.	0	0	2	296	0	1.54	1	65.55
11	297.01	1	1	0	0	2	296	0	1.54	1	65.55
11	298.01	1	.	1	0	3	298	0	1.54	1	65.55
11	299.01	0	1	1	0	1	298	0	1.54	1	50.28
11	300.01	1	1	1	0	1	298	0	1.68	1	35.02
11	301.01	1	0	1	0	1	298	0	1.83	1	35.02
11	302.01	1	0	1	0	1	298	0	1.83	1	35.02
11	303.01	0	.	0	0	2	303	0	1.83	1	50.28
11	304.01	1	1	1	0	1	303	0	1.83	1	50.28
11	305.01	1	.	1	0	1	305	0	1.83	1	35.02
11	306.01	1	.	1	0	1	306	0	1.83	1	35.02
11	307.01	0	.	0	0	3	307	0	1.68	1	50.28
11	308.01	1	1	1	0	2	307	0	1.68	1	35.02
11	309.01	1	0	1	0	1	307	0	1.83	1	35.02
11	310.01	1	.	1	0	3	310	0	1.68	1	65.55
11	311.01	0	1	1	0	1	310	0	1.54	1	65.55
11	312.01	0	0	1	0	2	310	0	1.68	1	35.02
11	313.01	1	.	1	0	2	313	0	1.68	1	35.02
11	314.01	0	1	0	0	2	313	0	1.54	1	65.55
11	315.01	1	1	1	0	2	313	0	1.68	1	50.28
11	316.01	0	1	0	0	1	313	0	1.68	1	50.28
11	317.01	1	1	1	0	1	313	0	1.68	0	80.81
11	318.01	1	0	1	0	1	313	0	1.68	1	80.81
11	319.01	1	.	0	1	2	319	0	1.83	1	80.81
11	320.01	1	.	1	0	2	320	0	1.68	1	50.28
11	321.01	1	.	1	0	1	321	0	1.97	0	50.28
11	322.01	0	1	1	0	1	321	0	1.83	1	35.02
11	323.01	0	0	1	0	2	321	0	1.83	1	50.28
11	324.01	1	.	0	0	.	324	0	1.68	1	65.55
11	325.01	1	0	1	0	1	324	0	1.83	1	65.55
11	326.01	1	.	1	0	2	326	0	1.68	1	65.55
11	327.01	0	1	1	0	1	326	0	1.68	0	65.55
11	328.01	1	1	1	0	1	326	0	1.68	1	50.28

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	279.01	400.33	1.36	0.74	1.36	0.74	1	2	0	1.55
11	280.01	110.78	0.65	1.54	0.64	1.56	0		1	.
11	281.01	121.25	0.65	1.54	0.64	1.56	0		0	.
11	282.01	130.19	0.65	1.55	0.64	1.56	0		0	.
11	283.01	107.94	0.65	1.55	0.64	1.56	0		0	.
11	284.01	109.01	0.65	1.53	0.64	1.56	0		0	.
11	285.01	72.33	0.64	1.55	0.64	1.55	1	0	0	1.56
11	286.01	131.10	0.64	1.56	0.64	1.55	0		1	.
11	287.01	126.06	0.64	1.56	0.64	1.55	0		0	.
11	288.01	73.57	0.64	1.56	0.64	1.55	0		0	.
11	289.01	74.54	0.63	1.58	0.64	1.55	0		0	.
11	290.01	75.74	0.63	1.58	0.64	1.55	0		0	.
11	291.01	160.16	0.64	1.56	0.64	1.56	1	3	0	1.55
11	292.01	294.63	0.63	1.58	0.63	1.58	1	0	0	1.55
11	293.01	77.97	0.63	1.58	0.63	1.58	0		1	.
11	294.01	77.07	0.63	1.59	0.63	1.58	0		0	.
11	295.01	298.93	0.63	1.60	0.63	1.60	1	0	0	1.58
11	296.01	79.94	0.63	1.58	0.63	1.58	1	1	0	1.60
11	297.01	78.94	0.63	1.57	0.63	1.58	0		1	.
11	298.01	81.04	0.64	1.56	0.64	1.56	1	0	0	1.58
11	299.01	305.17	0.64	1.56	0.64	1.56	0		1	.
11	300.01	322.29	0.64	1.55	0.64	1.56	0		0	.
11	301.01	327.59	0.64	1.55	0.64	1.56	0		0	.
11	302.01	328.66	0.64	1.55	0.64	1.56	0		0	.
11	303.01	310.11	0.64	1.56	0.64	1.56	1	0	0	1.56
11	304.01	308.17	0.64	1.56	0.64	1.56	0		1	.
11	305.01	333.33	0.64	1.56	0.64	1.56	1	1	0	1.56
11	306.01	345.48	0.65	1.54	0.65	1.54	1	0	0	1.56
11	307.01	312.28	0.65	1.54	0.65	1.54	1	0	0	1.54
11	308.01	346.81	0.66	1.52	0.65	1.54	0		1	.
11	309.01	349.35	0.66	1.52	0.65	1.54	0		0	.
11	310.01	83.78	0.65	1.54	0.65	1.54	1	0	0	1.54
11	311.01	85.51	0.64	1.56	0.65	1.54	0		1	.
11	312.01	354.39	0.64	1.56	0.65	1.54	0		0	.
11	313.01	358.69	0.64	1.56	0.64	1.56	1	1	0	1.54
11	314.01	87.22	0.64	1.57	0.64	1.56	0		1	.
11	315.01	353.08	0.64	1.56	0.64	1.56	0		0	.
11	316.01	355.02	0.63	1.58	0.64	1.56	0		0	.
11	317.01	89.25	0.63	1.59	0.64	1.56	0		0	.
11	318.01	86.15	0.63	1.58	0.64	1.56	0		0	.
11	319.01	87.72	0.66	1.51	0.66	1.51	1	2	0	1.56
11	320.01	363.23	0.61	1.63	0.61	1.63	1	3	0	1.56
11	321.01	362.53	0.62	1.62	0.62	1.62	1	1	0	1.56
11	322.01	396.69	0.61	1.65	0.62	1.62	0		1	.
11	323.01	366.50	0.61	1.63	0.62	1.62	0		0	.
11	324.01	89.18	0.61	1.64	0.61	1.64	1	0	0	1.62
11	325.01	90.59	0.61	1.64	0.61	1.64	0		1	.
11	326.01	93.49	0.60	1.66	0.60	1.66	1	0	0	1.64
11	327.01	95.92	0.62	1.61	0.60	1.66	0		1	.
11	328.01	381.41	0.62	1.62	0.60	1.66	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	329.01	1	0	0	0	1	326	0	1.83	1	50.28
11	330.01	1	.	1	1	2	330	0	1.83	1	50.28
11	331.01	1	0	1	0	1	330	0	1.97	1	50.28
11	332.01	0	1	1	0	2	330	0	1.83	1	65.55
11	333.01	0	0	0	0	1	330	0	1.97	1	65.55
11	334.01	0	0	0	0	2	330	0	1.83	1	65.55
11	335.01	0	.	0	0	2	335	0	1.83	1	50.28
11	336.01	0	0	0	0	1	335	0	1.83	1	50.28
11	337.01	0	.	1	0	2	337	0	1.83	1	65.55
11	338.01	0	.	1	0	.	338	0	1.26	1	80.81
11	339.01	0	0	1	0	1	338	0	1.26	1	50.28
11	340.01	0	0	1	0	2	338	0	1.26	1	50.28
11	341.01	0	0	0	0	1	338	0	1.26	1	50.28
11	342.01	1	1	1	0	2	338	0	1.40	1	65.55
11	343.01	0	1	0	0	1	338	0	1.54	1	50.28
11	344.01	0	.	1	0	.	344	0	1.54	1	80.81
11	345.01	1	1	1	0	2	344	0	1.83	1	80.81
11	346.01	1	0	1	0	1	344	0	1.83	1	65.55
11	347.01	0	1	1	0	1	344	0	2.11	1	80.81
11	348.01	0	.	1	0	.	348	0	1.40	1	80.81
11	349.01	1	1	1	0	2	348	0	1.12	1	80.81
11	350.01	1	.	1	0	3	350	0	1.12	1	80.81
11	351.01	1	0	0	0	1	350	0	1.26	1	80.81
11	352.01	1	0	1	0	1	350	0	1.26	1	65.55
11	353.01	1	0	1	1	1	350	0	1.26	1	19.75
11	354.01	0	.	0	0	2	354	0	1.54	1	19.75
11	356.01	0	.	1	0	.	356	0	0.28	0	65.55
11	357.01	0	0	1	0	1	356	0	0.56	0	65.55
11	358.01	1	.	1	1	.	358	0	0.28	1	65.55
11	359.01	0	1	1	0	2	358	0	0.56	0	65.55
11	360.01	0	.	1	0	.	360	0	0.28	0	50.28
11	361.01	0	.	1	0	.	361	0	0.28	0	65.55
11	63.02	0	.	1	0	.	63	0	1.12	1	4.49
11	78.02	1	.	1	0	2	78	0	1.26	2	4.49
11	89.02	0	.	1	0	1	89	0	1.83	2	4.49
11	90.02	0	.	1	0	.	90	0	1.54	1	4.49
11	95.02	0	.	1	0	.	95	0	1.97	0	4.49
11	100.02	0	.	0	0	1	100	0	1.83	0	4.49
11	121.02	0	.	0	0	1	121	0	2.11	1	4.49
11	122.02	0	0	0	0	1	121	0	1.97	0	4.49
11	123.02	0	.	0	0	1	123	0	2.39	0	4.49
11	126.02	1	.	1	0	.	126	0	1.83	1	19.75
11	142.02	0	.	0	0	1	142	0	2.53	1	4.49
11	144.02	1	1	1	0	1	142	0	2.53	1	4.49
11	145.02	0	.	1	0	1	145	0	2.53	2	19.75
11	157.02	1	.	0	0	1	157	0	2.11	0	4.49
11	163.02	1	.	1	0	1	163	0	2.11	0	4.49
11	168.02	0	.	0	0	1	168	0	2.53	1	4.49
11	169.02	1	.	1	0	1	169	0	2.53	2	4.49
11	176.02	1	.	0	0	1	176	0	2.25	1	4.49

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	329.01	384.52	0.61	1.64	0.60	1.66	0		0	.
11	330.01	409.37	0.61	1.63	0.61	1.63	1	1	0	1.66
11	331.01	412.51	0.61	1.64	0.61	1.63	0		1	.
11	332.01	104.17	0.61	1.64	0.61	1.63	0		0	.
11	333.01	97.06	0.61	1.64	0.61	1.63	0		0	.
11	334.01	98.06	0.61	1.65	0.61	1.63	0		0	.
11	335.01	422.32	0.61	1.64	0.61	1.64	1	1	0	1.63
11	336.01	424.16	0.60	1.66	0.61	1.64	0		1	.
11	337.01	100.33	0.60	1.68	0.60	1.68	1	1	0	1.64
11	338.01	197.09	0.60	1.68	0.60	1.68	1	0	0	1.68
11	339.01	429.83	0.49	2.05	0.60	1.68	0		1	.
11	340.01	430.80	0.48	2.08	0.60	1.68	0		0	.
11	341.01	432.50	0.48	2.10	0.60	1.68	0		0	.
11	342.01	103.03	0.48	2.09	0.60	1.68	0		0	.
11	343.01	436.10	0.49	2.06	0.60	1.68	0		0	.
11	344.01	173.84	0.48	2.07	0.48	2.07	1	0	0	1.68
11	345.01	173.34	0.48	2.08	0.48	2.07	0		1	.
11	346.01	206.50	0.47	2.11	0.48	2.07	0		0	.
11	347.01	92.65	0.47	2.14	0.48	2.07	0		0	.
11	348.01	110.01	0.47	2.13	0.47	2.13	1	0	0	2.07
11	349.01	110.67	0.46	2.15	0.47	2.13	0		1	.
11	350.01	208.40	0.47	2.11	0.47	2.11	1	0	0	2.13
11	351.01	242.04	0.47	2.11	0.47	2.11	0		1	.
11	352.01	350.88	0.47	2.12	0.47	2.11	0		0	.
11	353.01	503.71	0.47	2.12	0.47	2.11	0		0	.
11	354.01	505.74	0.47	2.12	0.47	2.12	1	1	0	2.11
11	356.01	491.85	0.77	1.29	0.77	1.29	1	0	0	2.12
11	357.01	493.09	0.78	1.27	0.77	1.29	0		1	.
11	358.01	189.32	0.96	1.04	0.96	1.04	1	0	0	1.29
11	359.01	351.81	0.92	1.09	0.96	1.04	0		1	.
11	360.01	583.55	0.64	1.57	0.64	1.57	1	0	0	1.04
11	361.01	727.76	1.42	0.71	1.42	0.71	1	0	0	1.57
11	63.02	38.64	0.85	1.18	0.85	1.18	1	1	0	.
11	78.02	41.74	0.81	1.23	0.81	1.23	1	4	0	1.18
11	89.02	48.48	0.73	1.37	0.73	1.37	1	2	0	1.23
11	90.02	45.91	0.67	1.49	0.67	1.49	1	3	0	1.23
11	95.02	50.58	0.70	1.42	0.70	1.42	1	1	0	1.23
11	100.02	53.45	0.72	1.39	0.72	1.39	1	1	0	1.42
11	121.02	55.15	0.56	1.78	0.56	1.78	1	1	0	1.39
11	122.02	56.29	0.57	1.76	0.56	1.78	0		1	.
11	123.02	56.95	0.58	1.73	0.58	1.73	1	2	0	1.78
11	126.02	54.35	0.54	1.87	0.54	1.87	1	3	0	1.78
11	142.02	58.72	0.45	2.20	0.45	2.20	1	1	0	1.78
11	144.02	60.56	0.44	2.26	0.45	2.20	0		1	.
11	145.02	55.85	0.41	2.41	0.41	2.41	1	3	0	2.20
11	157.02	61.63	0.39	2.59	0.39	2.59	1	4	0	2.20
11	163.02	66.96	0.29	3.48	0.29	3.48	1	2	0	2.59
11	168.02	63.33	0.29	3.41	0.29	3.41	1	2	0	2.59
11	169.02	63.06	0.28	3.51	0.28	3.51	1	3	0	2.59
11	176.02	65.26	0.27	3.72	0.27	3.72	1	3	0	2.59

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	184.02	1	1	1	0	1	185	0	2.53	2	4.49
11	185.02	0	.	0	0	1	185	0	2.25	1	4.49
11	187.02	1	.	1	0	1	187	0	2.39	1	4.49
11	188.02	0	.	1	0	.	188	0	2.25	2	19.75
11	194.02	1	.	1	0	1	194	0	2.11	0	19.75
11	197.02	1	.	1	0	2	197	0	2.25	0	19.75
11	206.02	1	.	1	0	.	206	0	2.53	0	35.02
11	213.02	1	.	1	1	1	213	0	2.81	0	35.02
11	216.02	0	.	0	0	1	216	0	2.53	1	4.49
11	217.02	0	.	0	0	1	217	0	2.53	1	4.49
11	219.02	0	.	1	1	1	219	0	2.25	1	4.49
11	221.02	0	.	0	0	1	221	0	2.11	1	35.02
11	222.02	1	1	0	0	1	221	0	2.11	0	35.02
11	225.02	0	.	1	0	1	225	0	1.97	1	4.49
11	226.02	0	.	1	0	1	226	0	2.11	1	4.49
11	227.02	1	.	0	0	2	227	0	2.11	1	4.49
11	233.02	0	.	0	0	1	233	0	1.97	0	19.75
11	234.02	1	.	1	0	2	234	0	2.11	1	4.49
11	235.02	1	0	1	0	1	234	0	2.39	1	4.49
11	242.02	0	.	1	1	1	242	0	2.25	1	19.75
11	243.02	0	0	1	0	1	242	0	2.39	2	19.75
11	244.02	0	.	1	0	1	244	0	2.67	1	19.75
11	245.02	0	.	0	0	1	245	0	2.39	1	4.49
11	248.02	1	.	0	0	1	248	0	2.25	2	35.02
11	251.02	1	.	1	0	1	251	0	2.39	0	35.02
11	252.02	0	.	1	0	2	252	0	2.39	1	4.49
11	255.02	1	.	1	0	1	255	0	1.83	1	19.75
11	256.02	0	.	0	1	1	256	0	2.25	0	19.75
11	257.02	0	.	1	0	1	257	0	2.25	1	4.49
11	258.02	0	.	0	0	1	258	0	2.25	1	4.49
11	265.02	0	.	1	0	1	265	0	2.39	1	4.49
11	267.02	0	.	1	0	1	267	0	2.53	0	19.75
11	268.02	0	.	0	0	1	268	0	2.39	1	19.75
11	270.02	0	.	0	0	1	270	0	2.11	1	19.75
11	272.02	1	.	1	0	2	272	0	2.25	1	4.49
11	273.02	1	0	1	0	1	272	0	1.97	1	50.28
11	278.02	0	.	0	0	2	278	0	2.11	1	19.75
11	279.02	0	.	1	0	1	279	0	2.67	2	4.49
11	280.02	1	1	0	0	1	278	0	2.39	1	4.49
11	281.02	0	1	0	0	1	278	0	2.25	1	4.49
11	282.02	1	1	1	0	1	278	0	1.97	1	4.49
11	283.02	1	0	1	0	1	278	0	2.39	1	19.75
11	284.02	1	0	0	0	1	278	0	2.53	1	19.75
11	285.02	1	.	1	0	1	285	0	2.67	0	35.02
11	286.02	0	1	1	0	1	285	0	2.39	1	4.49
11	287.02	0	0	0	0	1	285	0	2.25	0	19.75
11	288.02	0	0	0	0	1	285	0	2.39	1	35.02
11	289.02	1	1	1	0	1	285	0	2.39	0	35.02
11	290.02	1	0	1	0	1	285	0	2.53	0	35.02
11	291.02	1	0	1	0	1	285	0	2.81	1	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	184.02	69.87	0.26	3.90	0.26	3.92	0		1	.
11	185.02	68.53	0.26	3.92	0.26	3.92	1	4	0	2.59
11	187.02	71.84	0.24	4.12	0.24	4.12	1	1	0	3.92
11	188.02	69.03	0.24	4.13	0.24	4.13	1	1	0	4.12
11	194.02	71.54	0.20	4.95	0.20	4.95	1	1	0	4.13
11	197.02	74.51	0.20	5.03	0.20	5.03	1	1	0	4.95
11	206.02	55.38	0.18	5.46	0.18	5.46	1	1	0	5.03
11	213.02	58.79	0.17	5.89	0.17	5.89	1	1	0	5.46
11	216.02	74.74	0.16	6.26	0.16	6.26	1	2	0	5.89
11	217.02	73.17	0.16	6.39	0.16	6.39	1	3	0	5.89
11	219.02	77.34	0.16	6.39	0.16	6.39	1	2	0	5.89
11	221.02	50.25	0.15	6.50	0.15	6.50	1	4	0	5.89
11	222.02	57.29	0.15	6.54	0.15	6.50	0		1	.
11	225.02	78.81	0.15	6.74	0.15	6.74	1	1	0	6.50
11	226.02	81.98	0.15	6.76	0.15	6.76	1	1	0	6.74
11	227.02	83.28	0.15	6.78	0.15	6.78	1	1	0	6.76
11	233.02	81.71	0.14	7.23	0.14	7.23	1	3	0	6.78
11	234.02	85.05	0.14	7.26	0.14	7.26	1	0	0	6.78
11	235.02	86.02	0.14	7.28	0.14	7.26	0		1	.
11	242.02	84.35	0.13	7.61	0.13	7.61	1	1	0	7.26
11	243.02	85.42	0.13	7.61	0.13	7.61	0		1	.
11	244.02	86.02	0.13	7.58	0.13	7.58	1	2	0	7.61
11	245.02	88.29	0.13	7.69	0.13	7.69	1	3	0	7.61
11	248.02	60.39	0.13	7.45	0.13	7.45	1	2	0	7.61
11	251.02	61.79	0.14	7.28	0.14	7.28	1	2	0	7.61
11	252.02	90.79	0.13	7.97	0.13	7.97	1	3	0	7.61
11	255.02	88.19	0.12	8.15	0.12	8.15	1	3	0	7.61
11	256.02	88.89	0.12	8.21	0.12	8.21	1	4	0	7.61
11	257.02	94.06	0.12	8.01	0.12	8.01	1	1	0	8.21
11	258.02	95.73	0.13	7.95	0.13	7.95	1	0	0	8.01
11	265.02	100.03	0.12	8.43	0.12	8.43	1	0	0	7.95
11	267.02	95.09	0.12	8.41	0.12	8.41	1	2	0	8.43
11	268.02	94.03	0.12	8.47	0.12	8.47	1	3	0	8.43
11	270.02	99.30	0.12	8.46	0.12	8.46	1	4	0	8.43
11	272.02	102.63	0.12	8.49	0.12	8.49	1	4	0	8.46
11	273.02	63.86	0.12	8.47	0.12	8.49	0		1	.
11	278.02	105.47	0.30	3.39	0.30	3.39	1	0	0	8.49
11	279.02	400.33	1.45	0.69	1.45	0.69	1	2	0	2.46
11	280.02	110.78	0.29	3.39	0.30	3.39	0		1	.
11	281.02	121.25	0.29	3.40	0.30	3.39	0		0	.
11	282.02	130.19	0.30	3.39	0.30	3.39	0		0	.
11	283.02	107.94	0.30	3.39	0.30	3.39	0		0	.
11	284.02	109.01	0.30	3.36	0.30	3.39	0		0	.
11	285.02	72.33	0.29	3.40	0.29	3.40	1	0	0	3.39
11	286.02	131.10	0.29	3.44	0.29	3.40	0		1	.
11	287.02	126.06	0.29	3.45	0.29	3.40	0		0	.
11	288.02	73.57	0.29	3.43	0.29	3.40	0		0	.
11	289.02	74.54	0.29	3.48	0.29	3.40	0		0	.
11	290.02	75.74	0.29	3.42	0.29	3.40	0		0	.
11	291.02	160.16	0.30	3.35	0.29	3.40	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	292.02	1	.	1	0	1	292	0	2.11	1	19.75
11	293.02	1	0	0	0	2	292	0	1.83	1	35.02
11	294.02	1	0	0	0	1	292	0	1.97	0	35.02
11	295.02	1	.	1	0	1	295	0	1.97	1	19.75
11	296.02	0	.	0	0	2	296	0	1.83	0	35.02
11	297.02	1	1	0	0	1	296	0	1.97	1	35.02
11	298.02	1	.	1	0	2	298	0	1.97	0	35.02
11	299.02	0	.	1	0	1	299	0	2.11	1	19.75
11	300.02	1	.	1	0	1	300	0	2.53	0	4.49
11	301.02	1	0	1	0	1	300	0	2.67	1	4.49
11	302.02	1	0	1	0	1	300	0	2.81	1	4.49
11	303.02	0	1	0	0	1	300	0	2.39	0	19.75
11	304.02	1	.	1	0	1	304	0	2.25	1	19.75
11	305.02	1	.	1	0	1	305	0	2.95	1	4.49
11	306.02	1	.	1	0	1	306	0	2.67	1	4.49
11	307.02	0	.	0	0	1	307	0	2.53	0	19.75
11	308.02	1	.	1	0	1	308	0	2.53	1	4.49
11	309.02	1	.	1	0	1	309	0	2.67	1	4.49
11	310.02	1	.	1	0	2	310	0	2.53	0	35.02
11	311.02	0	.	1	0	1	311	0	2.53	0	35.02
11	312.02	0	0	1	0	1	311	0	2.11	1	4.49
11	313.02	1	.	1	0	2	313	0	2.25	1	4.49
11	314.02	0	1	0	0	1	313	0	2.25	1	35.02
11	315.02	1	1	1	0	1	313	0	1.97	1	19.75
11	316.02	0	1	0	0	1	313	0	2.25	1	19.75
11	317.02	1	1	1	0	1	313	0	2.39	1	50.28
11	318.02	1	0	1	0	2	313	0	2.11	1	50.28
11	319.02	1	.	0	1	1	319	0	2.67	1	50.28
11	320.02	1	.	1	0	1	320	0	2.53	1	19.75
11	321.02	1	.	1	0	1	321	0	2.53	1	19.75
11	322.02	0	.	1	0	1	322	0	2.67	1	4.49
11	323.02	0	0	1	0	1	322	0	2.25	1	19.75
11	324.02	1	.	0	0	.	324	0	2.25	1	35.02
11	325.02	1	0	1	0	1	324	0	2.39	1	35.02
11	326.02	1	0	1	0	2	324	0	2.11	1	35.02
11	327.02	0	1	1	0	1	324	0	2.25	1	35.02
11	328.02	1	1	1	0	2	324	0	2.39	1	19.75
11	329.02	1	0	0	0	1	324	0	2.67	1	19.75
11	330.02	1	.	1	1	1	330	0	1.97	1	19.75
11	331.02	1	0	1	0	1	330	0	1.97	1	19.75
11	332.02	0	1	1	0	1	330	0	1.83	1	35.02
11	333.02	0	0	0	0	2	330	0	1.83	1	35.02
11	334.02	0	0	0	0	2	330	0	1.83	1	35.02
11	335.02	0	.	0	0	.	335	0	1.68	1	19.75
11	336.02	0	0	0	0	2	335	0	1.68	1	19.75
11	337.02	0	.	1	0	3	337	0	1.68	1	35.02
11	338.02	0	.	1	0	.	338	0	1.40	1	50.28
11	339.02	0	0	1	0	1	338	0	1.40	1	19.75
11	340.02	0	0	1	0	1	338	0	1.40	1	19.75
11	341.02	0	0	0	0	1	338	0	1.40	1	19.75

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	292.02	294.63	0.32	3.09	0.32	3.09	1	0	0	3.40
11	293.02	77.97	0.34	2.93	0.32	3.09	0		1	.
11	294.02	77.07	0.34	2.93	0.32	3.09	0		0	.
11	295.02	298.93	0.42	2.35	0.42	2.35	1	0	0	3.09
11	296.02	79.94	0.42	2.38	0.42	2.38	1	0	0	2.35
11	297.02	78.94	0.41	2.41	0.42	2.38	0		1	.
11	298.02	81.04	0.42	2.39	0.42	2.39	1	2	0	2.38
11	299.02	305.17	0.41	2.45	0.41	2.45	1	3	0	2.38
11	300.02	322.29	0.41	2.42	0.41	2.42	1	1	0	2.38
11	301.02	327.59	0.41	2.46	0.41	2.42	0		1	.
11	302.02	328.66	0.41	2.46	0.41	2.42	0		0	.
11	303.02	310.11	0.40	2.50	0.41	2.42	0		0	.
11	304.02	308.17	0.41	2.46	0.41	2.46	1	1	0	2.42
11	305.02	333.33	0.39	2.58	0.39	2.58	1	3	0	2.46
11	306.02	345.48	0.40	2.48	0.40	2.48	1	2	0	2.46
11	307.02	312.28	0.39	2.57	0.39	2.57	1	3	0	2.46
11	308.02	346.81	0.40	2.50	0.40	2.50	1	1	0	2.46
11	309.02	349.35	0.42	2.41	0.42	2.41	1	2	0	2.50
11	310.02	83.78	0.38	2.60	0.38	2.60	1	3	0	2.50
11	311.02	85.51	0.40	2.47	0.40	2.47	1	1	0	2.50
11	312.02	354.39	0.40	2.51	0.40	2.47	0		1	.
11	313.02	358.69	0.40	2.48	0.40	2.48	1	0	0	2.47
11	314.02	87.22	0.40	2.48	0.40	2.48	0		1	.
11	315.02	353.08	0.41	2.44	0.40	2.48	0		0	.
11	316.02	355.02	0.57	1.76	0.40	2.48	0		0	.
11	317.02	89.25	0.60	1.68	0.40	2.48	0		0	.
11	318.02	86.15	0.60	1.67	0.40	2.48	0		0	.
11	319.02	87.72	0.58	1.74	0.58	1.74	1	3	0	2.48
11	320.02	363.23	0.60	1.66	0.60	1.66	1	2	0	2.48
11	321.02	362.53	0.61	1.64	0.61	1.64	1	1	0	2.48
11	322.02	396.69	0.63	1.58	0.63	1.58	1	1	0	1.64
11	323.02	366.50	0.64	1.56	0.63	1.58	0		1	.
11	324.02	89.18	0.64	1.55	0.64	1.55	1	0	0	1.58
11	325.02	90.59	0.65	1.54	0.64	1.55	0		1	.
11	326.02	93.49	0.65	1.53	0.64	1.55	0		0	.
11	327.02	95.92	0.66	1.52	0.64	1.55	0		0	.
11	328.02	381.41	0.66	1.52	0.64	1.55	0		0	.
11	329.02	384.52	0.66	1.51	0.64	1.55	0		0	.
11	330.02	409.37	0.66	1.52	0.66	1.52	1	0	0	1.55
11	331.02	412.51	0.67	1.50	0.66	1.52	0		1	.
11	332.02	104.17	0.67	1.50	0.66	1.52	0		0	.
11	333.02	97.06	0.68	1.48	0.66	1.52	0		0	.
11	334.02	98.06	0.68	1.48	0.66	1.52	0		0	.
11	335.02	422.32	0.68	1.46	0.68	1.46	1	0	0	1.52
11	336.02	424.16	0.69	1.44	0.68	1.46	0		1	.
11	337.02	100.33	0.70	1.43	0.70	1.43	1	0	0	1.46
11	338.02	197.09	0.69	1.46	0.69	1.46	1	0	0	1.43
11	339.02	429.83	0.69	1.45	0.69	1.46	0		1	.
11	340.02	430.80	0.68	1.48	0.69	1.46	0		0	.
11	341.02	432.50	0.68	1.47	0.69	1.46	0		0	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	342.02	1	1	1	0	2	338	0	1.54	1	35.02
11	343.02	0	1	0	0	2	338	0	1.68	1	19.75
11	344.02	0	.	1	0	.	344	0	1.68	1	50.28
11	345.02	1	1	1	0	2	344	0	1.83	1	50.28
11	346.02	1	0	1	0	1	344	0	1.40	1	35.02
11	347.02	0	1	1	0	2	344	0	1.54	1	50.28
11	348.02	0	.	1	0	.	348	0	1.40	0	50.28
11	349.02	1	1	1	0	2	348	0	1.12	1	50.28
11	350.02	1	.	1	0	2	350	0	1.26	1	50.28
11	351.02	1	0	0	0	2	350	0	1.26	1	50.28
11	352.02	1	0	1	0	2	350	0	1.26	1	35.02
11	356.02	0	.	1	0	.	356	0	0.28	0	65.55
11	357.02	0	0	1	0	1	356	0	0.56	0	35.02
11	358.02	1	.	1	1	.	358	0	0.42	1	35.02
11	359.02	0	.	1	0	.	359	0	0.42	1	35.02
11	360.02	0	.	1	0	.	360	0	0.28	0	19.75
11	361.02	0	.	1	0	.	361	0	0.28	2	35.02
11	362.02	0	.	1	0	.	362	0	0.42	1	4.49
11	369.02	0	.	0	0	.	369	0	0.28	1	4.49
11	370.02	0	.	1	0	.	370	0	0.56	0	4.49
11	371.02	0	.	1	0	.	371	0	0.56	1	4.49
11	206.03	1	.	1	0	.	206	0	0.98	2	4.49
11	213.03	1	.	1	1	3	213	0	1.26	0	4.49
11	221.03	0	.	0	0	.	221	0	1.12	1	4.49
11	222.03	1	.	0	0	1	222	0	1.40	0	4.49
11	248.03	1	.	0	0	.	248	0	1.54	1	4.49
11	251.03	1	.	1	0	1	251	0	1.68	2	4.49
11	273.03	1	.	1	0	.	273	0	1.68	1	19.75
11	285.03	1	.	1	0	.	285	0	1.97	0	4.49
11	288.03	0	.	0	0	1	288	0	1.83	1	4.49
11	289.03	1	1	1	0	1	288	0	1.97	2	4.49
11	290.03	1	0	1	0	1	288	0	2.25	0	4.49
11	293.03	1	.	0	0	1	293	0	1.54	0	4.49
11	294.03	1	.	0	0	1	294	0	1.68	2	4.49
11	296.03	0	.	0	0	1	296	0	1.54	2	4.49
11	297.03	1	.	0	0	1	297	0	1.68	1	4.49
11	298.03	1	.	1	0	1	298	0	1.68	0	4.49
11	310.03	1	.	1	0	.	310	0	1.97	1	4.49
11	311.03	0	.	1	0	1	311	0	2.11	0	4.49
11	314.03	0	.	0	0	1	314	0	1.97	1	4.49
11	317.03	1	.	1	0	1	317	0	2.53	2	19.75
11	318.03	1	.	1	0	.	318	0	1.68	0	19.75
11	319.03	1	0	0	1	1	318	0	2.39	0	19.75
11	324.03	1	.	0	0	1	324	0	2.25	1	4.49
11	325.03	1	.	1	0	1	325	0	2.39	1	4.49
11	326.03	1	.	1	0	2	326	0	2.25	0	4.49
11	327.03	0	.	1	0	1	327	0	2.25	0	4.49
11	332.03	0	.	1	0	1	332	0	1.40	1	4.49
11	333.03	0	.	0	0	1	333	0	1.54	1	4.49
11	334.03	0	0	0	0	1	333	0	1.68	0	4.49

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	342.02	103.03	0.68	1.48	0.69	1.46	0		0	.
11	343.02	436.10	0.66	1.51	0.69	1.46	0		0	.
11	344.02	173.84	0.67	1.50	0.67	1.50	1	0	0	1.46
11	345.02	173.34	0.67	1.50	0.67	1.50	0		1	.
11	346.02	206.50	0.68	1.46	0.67	1.50	0		0	.
11	347.02	92.65	0.70	1.42	0.67	1.50	0		0	.
11	348.02	110.01	0.71	1.40	0.71	1.40	1	0	0	1.50
11	349.02	110.67	0.68	1.47	0.71	1.40	0		1	.
11	350.02	208.40	0.69	1.44	0.69	1.44	1	0	0	1.40
11	351.02	242.04	0.69	1.44	0.69	1.44	0		1	.
11	352.02	350.88	0.69	1.45	0.69	1.44	0		0	.
11	356.02	491.85	0.77	1.29	0.77	1.29	1	0	0	1.44
11	357.02	493.09	1.08	0.92	0.77	1.29	0		1	.
11	358.02	189.32	0.85	1.17	0.85	1.17	1	2	0	1.29
11	359.02	351.81	0.79	1.27	0.79	1.27	1	3	0	1.29
11	360.02	583.55	0.44	2.29	0.44	2.29	1	3	0	1.29
11	361.02	727.76	1.57	0.64	1.57	0.64	1	0	0	1.29
11	362.02	1133.40	0.71	1.40	0.71	1.40	1	0	0	1.87
11	369.02	1107.00	0.60	1.67	0.60	1.67	1	0	0	0.64
11	370.02	1110.54	0.59	1.69	0.59	1.69	1	0	0	1.67
11	371.02	1112.68	0.53	1.87	0.53	1.87	1	0	0	1.69
11	206.03	55.38	1.16	0.86	1.16	0.86	1	2	0	.
11	213.03	58.79	1.13	0.88	1.13	0.88	1	0	0	0.89
11	221.03	50.25	0.90	1.11	0.90	1.11	1	3	0	.
11	222.03	57.29	1.12	0.89	1.12	0.89	1	1	0	.
11	248.03	60.39	0.69	1.44	0.69	1.44	1	1	0	0.88
11	251.03	61.79	0.55	1.83	0.55	1.83	1	4	0	1.44
11	273.03	63.86	0.46	2.19	0.46	2.19	1	1	0	1.83
11	285.03	72.33	0.13	7.67	0.13	7.67	1	1	0	2.19
11	288.03	73.57	0.13	7.74	0.13	7.74	1	4	0	7.67
11	289.03	74.54	0.13	7.72	0.13	7.74	0		1	.
11	290.03	75.74	0.13	7.79	0.13	7.74	0		0	.
11	293.03	77.97	0.12	8.41	0.12	8.41	1	2	0	7.74
11	294.03	77.07	0.12	8.48	0.12	8.48	1	3	0	7.74
11	296.03	79.94	0.11	9.04	0.11	9.04	1	2	0	7.74
11	297.03	78.94	0.11	9.11	0.11	9.11	1	3	0	7.74
11	298.03	81.04	0.11	9.10	0.11	9.10	1	4	0	7.74
11	310.03	83.78	0.11	9.46	0.11	9.46	1	1	0	9.10
11	311.03	85.51	0.10	9.58	0.10	9.58	1	4	0	9.46
11	314.03	87.22	0.10	9.70	0.10	9.70	1	0	0	9.58
11	317.03	89.25	0.10	10.52	0.10	10.52	1	2	0	9.70
11	318.03	86.15	0.09	10.70	0.09	10.70	1	3	0	9.70
11	319.03	87.72	0.09	10.72	0.09	10.70	0		1	.
11	324.03	89.18	0.09	11.09	0.09	11.09	1	4	0	9.70
11	325.03	90.59	0.09	11.10	0.09	11.10	1	1	0	11.09
11	326.03	93.49	0.09	11.08	0.09	11.08	1	1	0	11.10
11	327.03	95.92	0.09	11.08	0.09	11.08	1	2	0	11.08
11	332.03	104.17	0.09	11.10	0.09	11.10	1	2	0	11.08
11	333.03	97.06	0.09	11.37	0.09	11.37	1	3	0	11.08
11	334.03	98.06	0.09	11.41	0.09	11.37	0		1	.

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
11	337.03	0	.	1	0	3	337	0	1.54	1	4.49
11	338.03	0	.	1	0	.	338	0	0.98	1	19.75
11	342.03	1	.	1	0	2	342	0	1.40	1	4.49
11	344.03	0	.	1	0	.	344	0	1.26	1	19.75
11	345.03	1	.	1	0	.	345	0	1.12	0	19.75
11	346.03	1	.	1	0	.	346	0	0.84	0	4.49
11	347.03	0	.	1	0	2	347	0	1.54	0	19.75
11	348.03	0	.	1	0	.	348	0	0.84	0	19.75
11	349.03	1	1	1	0	1	348	0	0.84	0	19.75
11	350.03	1	.	1	0	.	350	0	0.98	1	19.75
11	351.03	1	.	0	0	.	351	0	0.84	1	19.75
11	352.03	1	.	1	0	.	352	0	0.84	1	4.49
11	356.03	0	.	1	0	.	356	0	0.28	2	4.49
11	357.03	0	0	1	0	2	356	0	0.56	2	4.49
11	358.03	1	.	1	1	.	358	0	0.42	1	4.49
11	359.03	0	.	1	0	.	359	0	0.42	1	4.49
11	361.03	0	.	1	0	.	361	0	0.28	2	4.49
12	2		0	1		.	2	0	0.37	0	10.42
12	5		0	1		.	5	0	0.37	1	19.01
12	6		1	1		.	6	0	0.56	0	1.83
12	7		1	1		.	7	0	0.37	1	19.01
12	8		1	1		2	7	0	0.75	1	19.01
12	9		0	0		2	9	0	0.93	1	1.83
12	10		1	1		.	10	0	0.93	1	19.01
12	11		1	1		.	11	0	0.75	0	1.83
12	12		0	0		1	11	0	1.12	2	1.83
12	13		1	1		1	13	0	1.12	1	1.83
12	14		1	1		1	14	0	1.31	0	1.83
12	17		1	1		1	17	0	1.68	2	1.83
12	18		1	1		1	18	0	1.86	1	1.83
12	23		0	0		.	23	0	0.75	2	27.60
12	25		1	1		1	25	0	1.68	0	19.01
12	27		1	1		1	27	0	1.68	2	44.79
12	29		1	1		1	29	0	1.86	1	1.83
12	32		1	1		.	32	0	1.86	1	19.01
12	33		1	1		1	32	0	1.86	1	19.01
12	34		0	1		2	32	0	1.68	0	27.60
12	35		1	1		.	35	0	0.37	1	27.60
12	36		0	0		2	35	0	0.75	0	27.60
12	37		0	0		1	37	0	1.31	1	70.56
12	38		0	0		1	37	0	1.12	1	70.56
12	39		1	1		2	39	0	1.12	2	36.19
12	41		0	0		.	41	0	0.37	1	27.60
12	42		1	1		2	42	0	0.75	1	27.60
12	43		0	1		2	42	0	0.93	2	27.60
12	44		1	1		1	42	0	0.93	1	1.83
12	45		0	1		1	42	0	1.31	1	1.83
12	46		0	1		2	46	0	1.31	2	19.01
12	47		1	1		2	46	0	1.31	2	44.79
12	48		0	0		2	46	0	1.31	2	44.79

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
11	337.03	100.33	0.09	11.55	0.09	11.55	1	0	0	11.08
11	338.03	197.09	0.12	8.24	0.12	8.24	1	2	0	11.55
11	342.03	103.03	0.08	11.86	0.08	11.86	1	3	0	11.55
11	344.03	173.84	0.11	9.35	0.11	9.35	1	2	0	11.55
11	345.03	173.34	0.11	9.44	0.11	9.44	1	3	0	11.55
11	346.03	206.50	0.12	8.57	0.12	8.57	1	2	0	11.55
11	347.03	92.65	0.08	12.50	0.08	12.50	1	3	0	11.55
11	348.03	110.01	0.08	12.02	0.08	12.02	1	0	0	11.55
11	349.03	110.67	0.08	11.95	0.08	12.02	0		1	.
11	350.03	208.40	0.12	8.09	0.12	8.09	1	1	0	12.02
11	351.03	242.04	0.16	6.14	0.16	6.14	1	1	0	8.09
11	352.03	350.88	0.25	3.97	0.25	3.97	1	1	0	6.14
11	356.03	491.85	1.29	0.78	1.29	0.78	1	0	0	3.97
11	357.03	493.09	1.28	0.78	1.29	0.78	0		1	.
11	358.03	189.32	0.07	14.50	0.07	14.50	1	3	0	.
11	359.03	351.81	0.11	8.82	0.11	8.82	1	3	0	.
11	361.03	727.76	1.63	0.61	1.63	0.61	1	0	0	0.78
12	2	60.70	0.92	1.09	0.92	1.09	1	0		.
12	5	51.48	0.79	1.26	0.79	1.26	1	0		1.09
12	6	81.12	0.76	1.32	0.76	1.32	1	0		1.26
12	7	65.00	0.83	1.20	0.83	1.20	1	0		1.32
12	8	67.20	0.83	1.20	0.83	1.20	0			
12	9	91.69	0.84	1.18	0.84	1.18	1	0		1.20
12	10	68.27	0.75	1.34	0.75	1.34	1	0		1.18
12	11	95.56	0.61	1.64	0.61	1.64	1	0		1.34
12	12	96.43	0.62	1.60	0.61	1.64	0			
12	13	98.10	0.64	1.57	0.64	1.57	1	1		1.64
12	14	99.37	0.64	1.57	0.64	1.57	1	0		1.57
12	17	101.10	0.58	1.71	0.58	1.71	1	2		1.57
12	18	102.17	0.45	2.22	0.45	2.22	1	2		1.57
12	23	65.10	0.45	2.20	0.45	2.20	1	3		1.57
12	25	68.77	0.44	2.26	0.44	2.26	1	1		1.57
12	27	48.65	0.43	2.33	0.43	2.33	1	4		2.26
12	29	101.20	0.43	2.34	0.43	2.34	1	1		2.33
12	32	73.51	0.40	2.47	0.40	2.47	1	0		2.34
12	33	78.64	0.41	2.43	0.40	2.47	0			
12	34	86.99	0.42	2.37	0.40	2.47	0			
12	35	96.96	0.49	2.04	0.49	2.04	1	1		2.47
12	36	98.56	0.50	2.01	0.49	2.04	0			
12	37	41.97	0.51	1.94	0.51	1.94	1	1		2.04
12	38	46.14	0.52	1.94	0.51	1.94	0			
12	39	81.95	0.52	1.92	0.52	1.92	1	1		1.94
12	41	106.77	0.58	1.72	0.58	1.72	1	0		1.92
12	42	108.67	0.61	1.65	0.61	1.65	1	1		1.72
12	43	110.74	0.63	1.58	0.61	1.65	0			
12	44	142.61	0.57	1.75	0.61	1.65	0			
12	45	143.44	0.58	1.72	0.61	1.65	0			
12	46	112.05	0.58	1.72	0.58	1.72	1	0		1.65
12	47	83.99	0.57	1.76	0.58	1.72	0			
12	48	86.22	0.58	1.73	0.58	1.72	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	49		1	1		2	46	0	1.12	0	44.79
12	50		1	1		2	50	0	1.12	1	19.01
12	51		1	1		2	51	0	0.93	1	19.01
12	52		1	1		2	52	0	0.93	1	19.01
12	53		0	0		2	52	0	1.12	0	27.60
12	54		1	1		2	52	0	0.93	2	27.60
12	55		1	1		2	55	0	1.12	0	1.83
12	56		0	0		1	55	0	1.31	2	27.60
12	57		1	1		1	57	0	1.68	0	1.83
12	58		1	1		1	58	0	1.49	1	1.83
12	59		1	1		1	59	0	1.86	2	1.83
12	60		0	0		.	60	0	1.31	2	36.19
12	61		0	1		1	61	0	1.68	1	1.83
12	62		1	1		1	62	0	1.49	1	1.83
12	63		1	1		1	63	0	1.68	0	1.83
12	64		0	1		1	64	0	1.68	2	36.19
12	66		1	1		.	66	0	1.49	1	1.83
12	67		1	1		2	67	0	1.49	0	36.19
12	68		0	0		1	66	0	1.49	2	79.15
12	69		0	1		.	69	0	1.31	1	61.97
12	70		1	1		1	70	0	1.49	1	19.01
12	71		1	0		2	71	0	1.49	1	36.19
12	72		1	0		2	71	0	1.49	2	36.19
12	73		1	1		2	73	0	1.49	2	36.19
12	74		1	1		1	73	0	1.49	0	36.19
12	75		1	1		1	73	0	1.49	2	36.19
12	76		1	1		.	76	0	1.31	1	1.83
12	77		1	1		2	76	0	1.49	2	70.56
12	78		0	1		1	76	0	1.31	0	1.83
12	79		1	1		2	79	0	1.49	2	61.97
12	80		1	1		1	79	0	1.68	1	19.01
12	81		1	1		1	79	0	1.68	2	19.01
12	82		0	1		1	79	0	1.49	1	36.19
12	83		0	0		1	79	0	1.86	2	1.83
12	84		1	1		.	84	0	1.49	1	87.74
12	85		0	0		2	85	0	1.68	2	87.74
12	86		0	1		2	85	0	1.31	0	36.19
12	87		0	1		2	85	0	1.12	2	36.19
12	88		0	1		.	88	0	1.12	0	87.74
12	89		1	1		2	88	0	1.12	1	61.97
12	90		1	1		2	90	0	1.31	2	61.97
12	91		1	1		1	90	0	1.49	1	61.97
12	92		1	1		2	90	0	1.31	2	19.01
12	93		1	1		2	93	0	1.49	0	19.01
12	94		0	0		2	94	0	1.49	0	27.60
12	95		0	0		2	94	0	1.31	1	61.97
12	96		1	1		2	94	0	1.12	2	61.97
12	97		1	1		.	97	0	1.31	0	79.15
12	98		1	1		2	98	0	1.12	1	10.42
12	99		0	0		1	98	0	1.49	2	10.42

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	49	88.19	0.59	1.71	0.58	1.72	0			
12	50	121.09	0.57	1.76	0.57	1.76	1	0		1.72
12	51	122.09	0.57	1.75	0.57	1.75	1	0		1.76
12	52	123.66	0.57	1.75	0.57	1.75	1	0		1.75
12	53	121.12	0.58	1.73	0.57	1.75	0			
12	54	122.82	0.57	1.74	0.57	1.75	0			
12	55	160.16	0.57	1.74	0.57	1.74	1	0		1.75
12	56	124.36	0.60	1.67	0.57	1.74	0			
12	57	163.97	0.60	1.65	0.60	1.65	1	0		1.74
12	58	165.07	0.61	1.65	0.61	1.65	1	0		1.65
12	59	166.60	0.60	1.67	0.60	1.67	1	1		1.65
12	60	101.64	0.60	1.67	0.60	1.67	1	3		1.67
12	61	170.64	0.61	1.64	0.61	1.64	1	2		1.67
12	62	161.76	0.44	2.27	0.44	2.27	1	3		1.67
12	63	172.57	0.61	1.64	0.61	1.64	1	2		1.67
12	64	103.14	0.63	1.58	0.63	1.58	1	3		1.67
12	66	176.21	0.58	1.71	0.58	1.71	1	2		1.67
12	67	105.44	0.59	1.69	0.59	1.69	1	3		1.67
12	68	67.70	0.60	1.66	0.58	1.71	0			
12	69	77.81	0.57	1.75	0.57	1.75	1	3		1.67
12	70	139.41	0.59	1.70	0.59	1.70	1	1		1.67
12	71	106.78	0.59	1.69	0.59	1.69	1	1		1.70
12	72	107.54	0.58	1.71	0.59	1.69	0			
12	73	109.85	0.58	1.71	0.58	1.71	1	0		1.69
12	74	111.58	0.59	1.71	0.58	1.71	0			
12	75	113.85	0.60	1.66	0.58	1.71	0			
12	76	194.36	0.60	1.68	0.60	1.68	1	0		1.71
12	77	75.64	0.60	1.68	0.60	1.68	0			
12	78	197.13	0.59	1.69	0.60	1.68	0			
12	79	94.33	0.58	1.72	0.58	1.72	1	0		1.68
12	80	152.35	0.59	1.71	0.58	1.72	0			
12	81	152.75	0.58	1.74	0.58	1.72	0			
12	82	115.75	0.57	1.74	0.58	1.72	0			
12	83	203.87	0.59	1.70	0.58	1.72	0			
12	84	54.82	0.54	1.85	0.54	1.85	1	0		1.72
12	85	55.96	0.55	1.82	0.55	1.82	1	0		1.85
12	86	130.10	0.57	1.76	0.55	1.82	0			
12	87	132.00	0.59	1.71	0.55	1.82	0			
12	88	61.83	0.58	1.73	0.58	1.73	1	0		1.82
12	89	113.55	0.58	1.74	0.58	1.73	0			
12	90	115.71	0.57	1.76	0.57	1.76	1	1		1.73
12	91	117.65	0.57	1.74	0.57	1.76	0			
12	92	170.20	0.58	1.71	0.57	1.76	0			
12	93	170.57	0.60	1.67	0.60	1.67	1	1		1.76
12	94	170.07	0.61	1.63	0.61	1.63	1	1		1.67
12	95	119.69	0.63	1.59	0.61	1.63	0			
12	96	121.65	0.63	1.58	0.61	1.63	0			
12	97	91.49	0.60	1.67	0.60	1.67	1	0		1.63
12	98	233.57	0.55	1.81	0.55	1.81	1	1		1.67
12	99	234.10	0.60	1.67	0.55	1.81	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	100		0	1		1	98	0	1.49	2	10.42
12	101		1	1		1	98	0	1.86	1	10.42
12	102		1	1		1	98	0	1.49	2	10.42
12	103		0	0		2	98	0	1.49	2	61.97
12	104		1	1		2	104	0	1.49	2	44.79
12	105		1	1		.	105	0	1.31	2	44.79
12	106		1	1		2	106	0	1.12	1	19.01
12	107		1	1		.	107	0	1.31	1	1.83
12	108		1	1		.	108	0	1.12	0	70.56
12	109		1	1		1	109	0	1.31	0	70.56
12	110		1	1		1	109	0	1.31	1	44.79
12	111		1	1		2	111	0	1.31	0	44.79
12	112		1	1		.	112	0	1.31	2	10.42
12	113		0	1		1	112	0	1.68	2	44.79
12	114		1	1		1	114	0	1.49	1	79.15
12	115		1	1		1	114	0	1.86	2	79.15
12	116		0	1		2	114	0	1.49	2	19.01
12	117		1	1		2	117	0	1.49	2	27.60
12	118		0	0		1	117	0	1.68	2	27.60
12	119		1	1		1	117	0	1.49	1	44.79
12	120		0	0		2	117	0	1.31	2	79.15
12	121		0	0		1	117	0	1.68	1	79.15
12	122		0	1		1	117	0	1.68	2	53.38
12	123		0	0		1	123	0	1.49	2	44.79
12	124		1	1		.	124	0	1.31	2	44.79
12	125		1	1		.	125	0	0.56	2	36.19
12	126		1	1		1	125	0	0.75	0	36.19
12	127		0	0		2	127	0	0.75	1	27.60
12	128		1	1		1	127	0	1.12	0	36.19
12	129		0	1		2	127	0	1.31	2	27.60
12	130		1	1		.	130	0	1.12	0	53.38
12	131		0	0		2	130	0	1.31	2	53.38
12	132		0	0		2	130	0	1.49	0	70.56
12	133		0	0		1	130	0	1.68	2	70.56
12	134		1	1		.	134	0	1.49	1	44.79
12	135		1	1		2	134	0	1.49	1	53.38
12	136		0	1		2	136	0	1.49	2	19.01
12	137		1	1		1	136	0	1.31	2	70.56
12	138		0	0		1	136	0	1.68	0	79.15
12	139		1	1		1	139	0	1.49	1	70.56
12	140		0	0		1	139	0	1.68	0	70.56
12	141		1	1		1	139	0	1.68	2	70.56
12	142		1	1		1	142	0	1.86	2	70.56
12	143		1	1		1	142	0	1.86	1	70.56
12	144		1	1		1	142	0	1.86	0	70.56
12	145		0	0		1	142	0	1.86	0	70.56
12	146		1	1		2	142	0	1.49	2	70.56
12	147		1	1		2	147	0	1.31	0	70.56
12	148		1	1		1	148	0	1.68	2	61.97
12	149		1	0		1	149	0	1.49	0	61.97

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	100	235.84	0.60	1.67	0.55	1.81	0			
12	101	237.31	0.61	1.64	0.55	1.81	0			
12	102	239.07	0.62	1.61	0.55	1.81	0			
12	103	125.62	0.65	1.55	0.55	1.81	0			
12	104	154.19	0.66	1.50	0.66	1.50	1	1		1.81
12	105	155.83	0.66	1.52	0.66	1.52	1	0		1.50
12	106	189.99	0.67	1.49	0.67	1.49	1	1		1.52
12	107	250.25	0.68	1.46	0.68	1.46	1	2		1.49
12	108	92.72	0.70	1.43	0.70	1.43	1	3		1.49
12	109	94.02	0.71	1.41	0.71	1.41	1	1		1.49
12	110	161.97	0.69	1.44	0.71	1.41	0			
12	111	163.80	0.70	1.43	0.70	1.43	1	0		1.41
12	112	258.86	0.68	1.47	0.68	1.47	1	0		1.43
12	113	165.50	0.69	1.44	0.68	1.47	0			
12	114	93.62	0.67	1.49	0.67	1.49	1	0		1.47
12	115	95.43	0.66	1.51	0.67	1.49	0			
12	116	213.48	0.69	1.45	0.67	1.49	0			
12	117	212.98	0.68	1.48	0.68	1.48	1	0		1.49
12	118	214.61	0.70	1.44	0.68	1.48	0			
12	119	169.74	0.69	1.45	0.68	1.48	0			
12	120	97.63	0.70	1.43	0.68	1.48	0			
12	121	99.10	0.68	1.48	0.68	1.48	0			
12	122	134.90	0.70	1.44	0.68	1.48	0			
12	123	174.11	0.68	1.46	0.68	1.46	1	0		1.48
12	124	177.05	0.64	1.56	0.64	1.56	1	0		1.46
12	125	173.14	0.42	2.41	0.42	2.41	1	0		1.56
12	126	176.78	0.43	2.33	0.42	2.41	0			
12	127	243.58	0.43	2.34	0.43	2.34	1	0		2.41
12	128	178.41	0.44	2.29	0.43	2.34	0			
12	129	248.45	0.45	2.21	0.43	2.34	0			
12	130	138.74	0.30	3.33	0.30	3.33	1	0		2.34
12	131	136.64	0.45	2.21	0.30	3.33	0			
12	132	95.59	0.46	2.20	0.30	3.33	0			
12	133	97.33	0.45	2.21	0.30	3.33	0			
12	134	186.89	0.43	2.31	0.43	2.31	1	0		3.33
12	135	143.31	0.44	2.25	0.43	2.31	0			
12	136	261.76	0.46	2.20	0.46	2.20	1	1		2.31
12	137	102.07	0.48	2.10	0.46	2.20	0			
12	138	101.57	0.45	2.24	0.46	2.20	0			
12	139	99.46	0.45	2.22	0.45	2.22	1	0		2.20
12	140	104.50	0.46	2.20	0.45	2.22	0			
12	141	123.32	0.45	2.25	0.45	2.22	0			
12	142	119.62	0.45	2.24	0.45	2.24	1	0		2.22
12	143	105.67	0.44	2.29	0.45	2.24	0			
12	144	108.14	0.45	2.20	0.45	2.24	0			
12	145	110.81	0.47	2.11	0.45	2.24	0			
12	146	123.19	0.47	2.11	0.45	2.24	0			
12	147	124.52	0.48	2.07	0.48	2.07	1	1		2.24
12	148	168.47	0.50	2.02	0.50	2.02	1	2		2.07
12	149	162.83	0.53	1.89	0.53	1.89	1	3		2.07

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	150		1	1		2	150	0	1.31	1	61.97
12	151		0	0		1	151	0	1.68	0	1.83
12	152		1	1		2	152	0	1.68	1	61.97
12	153		1	1		1	152	0	1.86	2	61.97
12	154		1	1		2	152	0	1.68	2	19.01
12	155		1	1		2	152	0	1.68	2	61.97
12	156		1	0		1	152	0	1.86	1	36.19
12	157		1	1		1	152	0	1.86	1	61.97
12	158		1	1		.	158	0	1.49	0	36.19
12	159		1	1		1	158	0	1.49	2	36.19
12	160		1	1		2	160	0	1.31	0	87.74
12	161		1	1		2	160	0	1.49	2	87.74
12	162		1	1		1	160	0	1.68	1	61.97
12	163		1	1		1	160	0	1.86	1	27.60
12	164		1	1		1	160	0	1.68	2	27.60
12	165		0	1		2	160	0	1.49	2	44.79
12	166		0	1		.	166	0	1.31	2	44.79
12	167		1	1		1	166	0	1.31	2	44.79
12	168		1	1		1	168	1	1.49	2	44.79
12	169		1	1		1	169	1	1.31	1	44.79
12	170		1	1		1	168	1	1.49	2	61.97
12	171		1	1		1	169	1	1.49	1	61.97
12	172		1	1		.	172	0	1.49	2	87.74
12	173		1	1		2	173	0	1.49	2	87.74
12	174		0	0		1	173	0	1.49	1	61.97
12	175		0	0		2	173	0	1.31	2	70.56
12	176		1	1		2	176	0	1.12	2	70.56
12	177		1	1		2	177	0	1.12	1	87.74
12	178		1	1		.	178	0	1.12	2	61.97
12	179		0	1		1	178	0	1.31	0	53.38
12	180		1	1		2	180	0	1.12	1	19.01
12	181		1	1		1	180	0	1.49	0	61.97
12	182		1	1		1	180	0	1.49	1	61.97
12	183		0	1		1	180	0	1.31	0	87.74
12	184		0	1		2	180	0	1.31	1	53.38
12	185		0	0		1	180	0	1.49	2	53.38
12	186		0	1		1	180	0	1.68	0	27.60
12	187		0	1		.	187	0	1.31	1	27.60
12	188		1	1		1	187	0	1.31	2	70.56
12	189		1	1		1	189	0	1.49	0	27.60
12	190		0	1		1	189	0	1.49	2	79.15
12	191		0	0		1	189	0	1.86	1	79.15
12	192		0	1		1	189	0	1.49	2	79.15
12	193		0	1		2	189	0	1.49	1	70.56
12	194		1	1		1	189	0	1.49	2	70.56
12	195		0	0		1	195	0	1.49	1	53.38
12	196		0	0		1	195	0	1.68	0	53.38
12	197		1	1		2	197	0	1.31	1	70.56
12	198		0	1		2	197	0	1.31	2	53.38
12	199		0	0		1	199	0	1.49	2	53.38

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	150	164.86	0.49	2.03	0.49	2.03	1	3		2.07
12	151	335.64	0.53	1.89	0.53	1.89	1	1		2.07
12	152	166.83	0.54	1.84	0.54	1.84	1	1		1.89
12	153	170.54	0.56	1.79	0.54	1.84	0			
12	154	288.02	0.55	1.81	0.54	1.84	0			
12	155	172.10	0.56	1.79	0.54	1.84	0			
12	156	234.87	0.60	1.67	0.54	1.84	0			
12	157	173.74	0.64	1.56	0.54	1.84	0			
12	158	247.98	0.63	1.60	0.63	1.60	1	0		1.84
12	159	250.49	0.63	1.59	0.63	1.60	0			
12	160	91.72	0.61	1.64	0.61	1.64	1	0		1.60
12	161	97.90	0.62	1.62	0.61	1.64	0			
12	162	178.34	0.63	1.58	0.61	1.64	0			
12	163	311.58	0.65	1.53	0.61	1.64	0			
12	164	313.25	0.66	1.51	0.61	1.64	0			
12	165	257.79	0.70	1.44	0.61	1.64	0			
12	166	262.37	0.65	1.53	0.65	1.53	1	0		1.64
12	167	264.23	0.67	1.49	0.65	1.53	0			
12	168	266.37	0.69	1.46	0.69	1.46	1	2		1.53
12	169	268.84	0.67	1.49	0.67	1.49	1	3		1.53
12	170	182.51	0.67	1.48	0.69	1.46	0			
12	171	181.78	0.65	1.54	0.67	1.49	0			
12	172	96.00	0.61	1.65	0.61	1.65	1	0		1.53
12	173	98.83	0.60	1.68	0.60	1.68	1	0		1.65
12	174	189.09	0.60	1.67	0.60	1.68	0			
12	175	130.93	0.61	1.63	0.60	1.68	0			
12	176	145.74	0.60	1.66	0.60	1.66	1	0		1.68
12	177	109.38	0.60	1.66	0.60	1.66	1	0		1.66
12	178	192.46	0.59	1.71	0.59	1.71	1	0		1.66
12	179	193.19	0.60	1.68	0.59	1.71	0			
12	180	343.78	0.59	1.68	0.59	1.68	1	0		1.71
12	181	195.36	0.56	1.80	0.59	1.68	0			
12	182	197.20	0.59	1.71	0.59	1.68	0			
12	183	110.38	0.60	1.67	0.59	1.68	0			
12	184	206.81	0.60	1.66	0.59	1.68	0			
12	185	214.55	0.61	1.63	0.59	1.68	0			
12	186	355.35	0.63	1.60	0.59	1.68	0			
12	187	357.86	0.60	1.68	0.60	1.68	1	0		1.68
12	188	146.18	0.59	1.68	0.60	1.68	0			
12	189	361.43	0.58	1.71	0.58	1.71	1	0		1.68
12	190	148.14	0.61	1.65	0.58	1.71	0			
12	191	146.71	0.60	1.68	0.58	1.71	0			
12	192	149.91	0.61	1.63	0.58	1.71	0			
12	193	150.08	0.61	1.63	0.58	1.71	0			
12	194	151.78	0.61	1.63	0.58	1.71	0			
12	195	220.22	0.61	1.63	0.61	1.63	1	0		1.71
12	196	232.16	0.62	1.60	0.61	1.63	0			
12	197	162.06	0.61	1.65	0.61	1.63	1	0		1.63
12	198	252.32	0.62	1.61	0.61	1.63	0			
12	199	250.15	0.61	1.63	0.61	1.63	1	0		1.65

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	200		1	1		1	199	0	1.31	0	70.56
12	201		1	0		.	201	0	1.31	1	53.38
12	202		1	1		1	201	0	1.31	2	53.38
12	203		1	1		1	201	0	1.49	0	10.42
12	204		1	1		2	204	0	1.31	2	79.15
12	205		0	0		2	204	0	1.12	0	79.15
12	206		1	1		2	204	0	1.31	1	79.15
12	207		1	1		2	204	0	1.31	2	79.15
12	208		1	1		1	204	0	1.12	1	79.15
12	209		1	1		1	209	0	1.49	2	61.97
12	210		1	0		1	209	0	1.31	1	61.97
12	211		0	0		1	209	0	1.68	2	61.97
12	212		1	1		2	209	0	1.31	1	53.38
12	213		0	1		2	213	0	1.31	2	27.60
12	214		1	1		.	214	0	0.93	1	79.15
12	215		1	1		1	214	0	1.31	2	79.15
12	216		1	1		1	214	0	1.12	2	87.74
12	217		0	0		1	214	0	1.31	1	79.15
12	218		1	1		1	214	0	1.31	1	87.74
12	219		1	1		2	214	0	1.31	0	87.74
12	220		0	0		2	214	0	1.31	2	44.79
12	221		0	1		2	214	0	1.31	2	44.79
12	222		0	1		1	214	0	1.31	1	19.01
12	223		0	0		2	214	0	1.12	1	87.74
12	224		1	1		2	214	0	1.12	0	44.79
12	225		0	0		1	214	0	1.31	2	87.74
12	226		0	0		.	226	0	1.12	1	44.79
12	227		1	1		2	226	0	1.12	2	79.15
12	228		0	0		2	226	0	1.12	0	44.79
12	229		1	1		2	229	0	1.12	1	44.79
12	230		0	0		2	230	0	1.12	0	79.15
12	231		0	0		1	230	0	1.31	0	79.15
12	232		1	1		.	232	0	1.31	2	44.79
12	233		1	0		2	233	0	1.31	1	61.97
12	234		1	1		.	234	0	1.12	1	61.97
12	235		1	1		1	235	0	1.31	2	44.79
12	236		1	1		1	236	0	1.12	0	61.97
12	237		0	0		1	237	0	1.49	1	79.15
12	238		0	0		1	237	0	1.49	2	79.15
12	239		1	1		2	237	0	1.49	1	44.79
12	240		0	0		1	237	0	1.68	2	44.79
12	241		1	1		1	237	0	1.86	0	44.79
12	242		1	1		.	242	0	1.49	0	96.33
12	243		0	0		2	242	0	1.49	1	61.97
12	244		0	1		1	242	0	1.49	2	79.15
12	245		0	1		1	242	0	1.49	0	79.15
12	246		0	0		1	242	0	1.49	2	79.15
12	247		0	0		1	242	0	1.68	1	79.15
12	248		0	0		2	242	0	1.49	0	79.15
12	249		1	1		1	242	0	1.49	2	87.74

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	200	163.53	0.61	1.65	0.61	1.63	0			
12	201	268.77	0.60	1.67	0.60	1.67	1	0		1.63
12	202	274.44	0.59	1.70	0.60	1.67	0			
12	203	432.53	0.59	1.71	0.60	1.67	0			
12	204	163.16	0.60	1.68	0.60	1.68	1	1		1.67
12	205	166.90	0.61	1.64	0.60	1.68	0			
12	206	170.83	0.62	1.62	0.60	1.68	0			
12	207	169.40	0.62	1.61	0.60	1.68	0			
12	208	172.77	0.62	1.62	0.60	1.68	0			
12	209	291.52	0.64	1.55	0.64	1.55	1	1		1.68
12	210	293.46	0.63	1.58	0.64	1.55	0			
12	211	295.89	0.65	1.54	0.64	1.55	0			
12	212	290.19	0.66	1.52	0.64	1.55	0			
12	213	406.87	0.69	1.46	0.69	1.46	1	1		1.55
12	214	184.98	0.69	1.45	0.69	1.45	1	0		1.46
12	215	182.18	0.69	1.44	0.69	1.45	0			
12	216	155.89	0.69	1.44	0.69	1.45	0			
12	217	190.29	0.70	1.42	0.69	1.45	0			
12	218	161.83	0.71	1.41	0.69	1.45	0			
12	219	163.40	0.72	1.39	0.69	1.45	0			
12	220	363.30	0.72	1.38	0.69	1.45	0			
12	221	361.26	0.71	1.42	0.69	1.45	0			
12	222	424.32	0.73	1.37	0.69	1.45	0			
12	223	164.26	0.75	1.33	0.69	1.45	0			
12	224	368.07	0.76	1.31	0.69	1.45	0			
12	225	165.03	0.77	1.29	0.69	1.45	0			
12	226	373.24	0.76	1.32	0.76	1.32	1	0		1.45
12	227	199.70	0.77	1.30	0.76	1.32	0			
12	228	379.82	0.77	1.29	0.76	1.32	0			
12	229	382.09	0.76	1.31	0.76	1.31	1	0		1.32
12	230	207.24	0.74	1.36	0.74	1.36	1	0		1.31
12	231	202.37	0.70	1.42	0.74	1.36	0			
12	232	388.26	0.66	1.52	0.66	1.52	1	0		1.36
12	233	318.08	0.66	1.52	0.66	1.52	1	0		1.52
12	234	322.12	0.66	1.52	0.66	1.52	1	0		1.52
12	235	399.44	0.66	1.52	0.66	1.52	1	2		1.52
12	236	320.65	0.65	1.53	0.65	1.53	1	3		1.52
12	237	206.04	0.67	1.49	0.67	1.49	1	1		1.52
12	238	204.13	0.65	1.53	0.67	1.49	0			
12	239	398.53	0.67	1.48	0.67	1.49	0			
12	240	400.74	0.67	1.48	0.67	1.49	0			
12	241	404.64	0.68	1.47	0.67	1.49	0			
12	242	171.50	0.68	1.47	0.68	1.47	1	0		1.49
12	243	331.90	0.70	1.42	0.68	1.47	0			
12	244	216.68	0.71	1.42	0.68	1.47	0			
12	245	218.58	0.72	1.38	0.68	1.47	0			
12	246	220.52	0.73	1.37	0.68	1.47	0			
12	247	214.38	0.72	1.39	0.68	1.47	0			
12	248	222.32	0.70	1.42	0.68	1.47	0			
12	249	195.40	0.70	1.43	0.68	1.47	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	250		0	0		1	242	0	1.86	1	87.74
12	251		0	1		2	242	0	1.49	2	79.15
12	252		1	1		.	252	0	1.49	1	70.56
12	253		1	1		1	252	0	1.49	2	70.56
12	254		1	1		1	252	0	1.31	1	79.15
12	255		0	0		2	252	0	1.31	2	79.15
12	256		0	1		2	252	0	1.12	2	79.15
12	257		0	0		2	252	0	1.31	1	79.15
12	258		0	1		1	252	0	1.12	2	79.15
12	259		0	0		1	252	0	1.31	0	79.15
12	260		0	1		1	252	0	1.31	2	87.74
12	261		1	1		2	252	0	1.12	1	87.74
12	262		1	1		2	252	0	1.31	0	96.33
12	263		0	0		2	263	0	1.31	2	79.15
12	264		0	1		2	263	0	1.12	2	79.15
12	265		1	1		.	265	0	1.12	0	36.19
12	266		1	1		.	266	0	0.93	2	79.15
12	267		1	1		1	266	0	1.31	1	96.33
12	268		0	1		2	268	0	1.31	2	61.97
12	269		1	0		1	269	0	1.12	2	79.15
12	270		1	1		.	270	0	1.12	0	87.74
12	271		1	1		1	270	0	1.12	2	87.74
12	272		0	0		1	270	0	0.93	2	79.15
12	273		1	1		1	270	0	0.93	1	79.15
12	274		0	1		1	270	0	1.31	2	79.15
12	275		0	0		1	270	0	1.31	0	79.15
12	276		0	0		2	270	0	1.12	2	79.15
12	277		1	1		.	277	0	0.93	2	53.38
12	278		0	0		2	277	0	1.12	2	79.15
12	280		0	1		.	280	0	0.37	0	79.15
12	281		0	1		.	281	0	0.93	0	53.38
12	282		1	1		.	282	0	0.75	1	53.38
12	283		0	0		2	283	0	1.12	1	27.60
12	284		0	0		2	283	0	1.31	0	27.60
12	285		0	0		.	285	0	1.31	1	87.74
12	286		0	0		.	286	0	0.75	2	27.60
12	287		0	1		.	287	0	0.37	0	53.38
12	288		0	1		.	288	0	0.56	2	53.38
12	289		0	0		2	289	0	1.31	2	79.15
12	290		0	0		.	290	0	0.37	0	27.60
12	291		0	1		1	290	0	0.75	1	27.60
12	292		0	0		1	290	0	0.93	2	27.60
12	293		0	0		1	293	0	0.93	2	27.60
12	294		0	0		.	294	0	0.56	0	96.33
12	5.1		0	1		.	5	0	0.37	1	1.83
12	7.1		1	1		.	7	0	0.37	1	1.83
12	8.1		1	1		2	8	0	1.12	0	1.83
12	10.1		1	1		.	10	0	1.68	1	1.83
12	23.1		0	0		.	23	0	0.93	0	10.42
12	25.1		1	1		1	25	0	2.24	1	1.83

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	250	196.70	0.70	1.42	0.68	1.47	0			
12	251	227.56	0.71	1.40	0.68	1.47	0			
12	252	228.59	0.64	1.56	0.64	1.56	1	0		1.47
12	253	229.99	0.64	1.56	0.64	1.56	0			
12	254	229.69	0.64	1.56	0.64	1.56	0			
12	255	266.33	0.65	1.54	0.64	1.56	0			
12	256	276.71	0.65	1.53	0.64	1.56	0			
12	257	259.16	0.68	1.47	0.64	1.56	0			
12	258	301.36	0.68	1.47	0.64	1.56	0			
12	259	304.03	0.70	1.43	0.64	1.56	0			
12	260	209.14	0.72	1.39	0.64	1.56	0			
12	261	216.52	0.71	1.41	0.64	1.56	0			
12	262	223.02	0.70	1.42	0.64	1.56	0			
12	263	317.71	0.71	1.41	0.71	1.41	1	1		1.56
12	264	321.32	0.71	1.40	0.71	1.41	0			
12	265	457.03	0.69	1.45	0.69	1.45	1	0		1.41
12	266	326.62	0.65	1.53	0.65	1.53	1	0		1.45
12	267	227.23	0.65	1.54	0.65	1.53	0			
12	268	406.41	0.66	1.51	0.66	1.51	1	1		1.53
12	269	331.43	0.67	1.50	0.67	1.50	1	0		1.51
12	270	237.24	0.60	1.66	0.60	1.66	1	0		1.50
12	271	233.60	0.61	1.65	0.60	1.66	0			
12	272	345.78	0.62	1.61	0.60	1.66	0			
12	273	341.54	0.63	1.59	0.60	1.66	0			
12	274	344.24	0.65	1.54	0.60	1.66	0			
12	275	346.94	0.66	1.50	0.60	1.66	0			
12	276	426.76	0.68	1.47	0.60	1.66	0			
12	277	442.54	0.72	1.38	0.72	1.38	1	1		1.66
12	278	445.84	0.75	1.33	0.72	1.38	0			
12	280	551.95	0.78	1.28	0.78	1.28	1	0		1.38
12	281	583.95	0.92	1.08	0.92	1.08	1	2		1.28
12	282	582.78	0.61	1.65	0.61	1.65	1	3		1.28
12	283	671.60	0.66	1.50	0.66	1.50	1	2		1.28
12	284	673.44	0.67	1.49	0.66	1.50	0			
12	285	608.31	0.68	1.47	0.68	1.47	1	1		1.28
12	286	691.22	0.97	1.03	0.97	1.03	1	0		1.47
12	287	445.14	0.28	3.62	0.28	3.62	1	3		1.03
12	288	431.53	0.28	3.55	0.28	3.55	1	3		1.03
12	289	576.61	0.32	3.16	0.32	3.16	1	3		1.03
12	290	879.85	0.94	1.06	0.94	1.06	1	0		1.03
12	291	881.18	0.95	1.05	0.94	1.06	0			
12	292	882.72	0.96	1.04	0.94	1.06	0			
12	293	884.32	1.00	1.00	1.00	1.00	1	1		1.06
12	294	830.40	1.10	0.91	1.10	0.91	1	1		1.00
12	5.1	51.48	0.73	1.36	0.73	1.36	1	0		.
12	7.1	65.00	0.79	1.27	0.79	1.27	1	0		1.36
12	8.1	67.20	0.79	1.27	0.79	1.27	1	2		1.27
12	10.1	68.27	0.73	1.38	0.73	1.38	1	2		1.27
12	23.1	65.10	0.51	1.97	0.51	1.97	1	3		1.27
12	25.1	68.77	0.51	1.97	0.51	1.97	1	2		1.27

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	27.1		1	1		1	27	0	1.68	2	27.60
12	32.1		1	1		2	32	0	2.61	0	1.83
12	33.1		1	1		1	32	0	2.05	1	1.83
12	34.1		0	1		.	34	0	1.49	1	10.42
12	35.1		1	1		.	35	0	0.37	1	10.42
12	36.1		0	0		2	35	0	0.75	0	10.42
12	37.1		0	0		1	35	0	1.68	1	53.38
12	38.1		0	0		1	35	0	1.49	2	53.38
12	39.1		1	1		.	39	0	1.68	2	19.01
12	41.1		0	0		.	41	0	1.12	1	10.42
12	42.1		1	1		2	42	0	1.12	1	10.42
12	43.1		0	1		2	42	0	1.31	2	10.42
12	46.1		0	1		1	46	0	1.86	2	1.83
12	47.1		1	1		2	46	0	2.05	0	27.60
12	48.1		0	0		2	48	0	1.86	2	27.60
12	49.1		1	1		2	48	0	1.86	0	27.60
12	50.1		1	1		2	48	0	1.68	0	1.83
12	51.1		1	1		2	51	0	1.68	1	1.83
12	52.1		1	1		2	52	0	1.86	1	1.83
12	53.1		0	0		.	53	0	1.68	1	10.42
12	54.1		1	1		2	54	0	1.86	1	10.42
12	56.1		0	0		2	56	0	2.24	2	10.42
12	60.1		0	0		.	60	0	2.24	2	19.01
12	64.1		0	1		1	64	0	2.24	1	19.01
12	67.1		1	1		2	67	0	2.24	0	19.01
12	68.1		0	0		1	68	0	2.05	1	61.97
12	69.1		0	1		1	69	0	1.86	1	44.79
12	70.1		1	1		1	70	0	2.05	1	1.83
12	71.1		1	0		.	71	0	2.24	0	19.01
12	72.1		1	0		2	71	0	2.42	2	19.01
12	73.1		1	1		2	73	0	2.24	2	19.01
12	74.1		1	1		1	73	0	2.24	1	19.01
12	75.1		1	1		2	73	0	1.86	2	19.01
12	77.1		1	1		2	77	0	1.86	0	53.38
12	79.1		1	1		2	79	0	2.05	0	44.79
12	80.1		1	1		1	79	0	2.05	1	1.83
12	81.1		1	1		1	79	0	2.24	2	1.83
12	82.1		0	1		1	82	0	2.42	1	19.01
12	84.1		1	1		2	84	0	2.42	1	70.56
12	85.1		0	0		2	85	0	2.24	2	70.56
12	86.1		0	1		2	86	0	2.05	1	19.01
12	87.1		0	1		2	87	0	1.86	1	19.01
12	88.1		0	1		2	88	0	1.86	1	70.56
12	89.1		1	1		2	89	0	1.86	0	44.79
12	90.1		1	1		2	90	0	1.86	0	44.79
12	91.1		1	1		2	90	0	2.05	2	44.79
12	92.1		1	1		2	92	0	2.42	2	1.83
12	93.1		1	1		1	93	0	2.42	1	1.83
12	94.1		0	0		1	94	0	2.24	1	10.42
12	95.1		0	0		1	95	0	2.61	0	44.79

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	27.1	48.65	0.51	1.97	0.51	1.97	1	3		1.27
12	32.1	73.51	0.50	1.98	0.50	1.98	1	4		1.27
12	33.1	78.64	0.50	2.01	0.50	1.98	0			
12	34.1	86.99	0.58	1.71	0.58	1.71	1	1		1.98
12	35.1	96.96	0.69	1.45	0.69	1.45	1	0		1.71
12	36.1	98.56	0.68	1.48	0.69	1.45	0			
12	37.1	41.97	0.73	1.37	0.69	1.45	0			
12	38.1	46.14	0.73	1.38	0.69	1.45	0			
12	39.1	81.95	0.72	1.40	0.72	1.40	1	0		1.45
12	41.1	106.77	0.59	1.70	0.59	1.70	1	0		1.40
12	42.1	108.67	0.59	1.70	0.59	1.70	1	0		1.70
12	43.1	110.74	0.57	1.75	0.59	1.70	0			
12	46.1	112.05	0.56	1.78	0.56	1.78	1	4		1.70
12	47.1	83.99	0.56	1.78	0.56	1.78	0			
12	48.1	86.22	0.57	1.76	0.57	1.76	1	1		1.78
12	49.1	88.19	0.57	1.77	0.57	1.76	0			
12	50.1	121.09	0.57	1.76	0.57	1.76	0			
12	51.1	122.09	0.57	1.76	0.57	1.76	1	2		1.76
12	52.1	123.66	0.57	1.76	0.57	1.76	1	2		1.76
12	53.1	121.12	0.57	1.75	0.57	1.75	1	3		1.76
12	54.1	122.82	0.58	1.73	0.58	1.73	1	3		1.76
12	56.1	124.36	0.52	1.93	0.52	1.93	1	1		1.76
12	60.1	101.64	0.46	2.18	0.46	2.18	1	0		1.93
12	64.1	103.14	0.40	2.49	0.40	2.49	1	4		2.18
12	67.1	105.44	0.38	2.61	0.38	2.61	1	4		2.49
12	68.1	67.70	0.40	2.51	0.40	2.51	1	4		2.68
12	69.1	77.81	0.37	2.68	0.37	2.68	1	4		2.61
12	70.1	139.41	0.38	2.63	0.38	2.63	1	1		2.51
12	71.1	106.78	0.37	2.67	0.37	2.67	1	0		2.63
12	72.1	107.54	0.37	2.68	0.37	2.67	0			
12	73.1	109.85	0.38	2.66	0.38	2.66	1	1		2.67
12	74.1	111.58	0.37	2.67	0.38	2.66	0			
12	75.1	113.85	0.37	2.68	0.38	2.66	0			
12	77.1	75.64	0.36	2.81	0.36	2.81	1	4		2.66
12	79.1	94.33	0.35	2.88	0.35	2.88	1	1		2.81
12	80.1	152.35	0.81	1.24	0.35	2.88	0			
12	81.1	152.75	0.35	2.87	0.35	2.88	0			
12	82.1	115.75	0.35	2.89	0.35	2.89	1	1		2.88
12	84.1	54.82	0.33	3.00	0.33	3.00	1	1		2.89
12	85.1	55.96	0.33	3.01	0.33	3.01	1	1		3.00
12	86.1	130.10	0.33	3.03	0.33	3.03	1	1		3.01
12	87.1	132.00	0.33	3.05	0.33	3.05	1	1		3.03
12	88.1	61.83	0.33	3.05	0.33	3.05	1	1		3.05
12	89.1	113.55	0.33	3.05	0.33	3.05	1	1		3.05
12	90.1	115.71	0.33	3.01	0.33	3.01	1	0		3.05
12	91.1	117.65	0.33	3.00	0.33	3.01	0			
12	92.1	170.20	0.33	2.99	0.33	2.99	1	1		3.01
12	93.1	170.57	0.33	3.02	0.33	3.02	1	0		2.99
12	94.1	170.07	0.33	3.02	0.33	3.02	1	3		3.02
12	95.1	119.69	0.33	3.03	0.33	3.03	1	1		3.02

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	96.1		1	1		2	95	0	2.24	2	44.79
12	97.1		1	1		2	95	0	2.42	1	61.97
12	103.1		0	0		2	103	0	2.24	1	44.79
12	104.1		1	1		1	104	0	2.24	0	27.60
12	105.1		1	1		2	105	0	2.24	2	27.60
12	106.1		1	1		2	106	0	2.24	1	1.83
12	108.1		1	1		.	108	0	2.24	1	53.38
12	109.1		1	1		1	109	0	2.61	0	53.38
12	110.1		1	1		1	109	0	2.42	1	27.60
12	111.1		1	1		2	109	0	2.05	1	27.60
12	113.1		0	1		1	113	0	2.24	2	27.60
12	114.1		1	1		1	113	0	2.24	1	61.97
12	115.1		1	1		1	113	0	2.61	2	61.97
12	116.1		0	1		2	116	0	2.42	1	1.83
12	117.1		1	1		.	116	0	2.24	2	10.42
12	118.1		0	0		1	116	0	2.61	2	10.42
12	119.1		1	1		1	116	0	2.80	1	27.60
12	120.1		0	0		2	120	0	2.42	2	61.97
12	121.1		0	0		1	120	0	2.80	1	61.97
12	122.1		0	1		1	120	0	2.61	1	36.19
12	123.1		0	0		1	120	0	2.61	0	27.60
12	124.1		1	1		.	124	0	2.61	2	27.60
12	125.1		1	1		.	125	0	1.12	0	19.01
12	126.1		1	1		1	125	0	1.12	1	19.01
12	127.1		0	0		2	125	0	1.31	1	10.42
12	128.1		1	1		1	125	0	1.49	0	19.01
12	129.1		0	1		2	129	0	1.86	0	10.42
12	130.1		1	1		2	130	0	1.86	1	36.19
12	131.1		0	0		2	130	0	1.86	2	36.19
12	132.1		0	0		2	130	0	2.24	1	53.38
12	133.1		0	0		1	130	0	2.24	2	53.38
12	134.1		1	1		1	130	0	2.24	1	27.60
12	135.1		1	1		1	130	0	2.42	0	36.19
12	136.1		0	1		2	136	0	2.42	0	1.83
12	137.1		1	1		1	136	0	2.61	2	53.38
12	138.1		0	0		1	136	0	2.24	2	61.97
12	139.1		1	1		1	136	0	2.61	1	53.38
12	140.1		0	0		1	136	0	2.61	1	53.38
12	141.1		1	1		1	141	1	2.80	2	53.38
12	142.1		1	1		1	141	1	2.98	0	53.38
12	143.1		1	1		1	143	1	2.61	1	53.38
12	144.1		1	1		1	143	1	2.98	1	53.38
12	145.1		0	0		2	143	1	2.98	1	53.38
12	146.1		1	1		2	146	0	2.61	0	53.38
12	147.1		1	1		.	147	0	2.42	0	53.38
12	148.1		1	1		2	148	0	2.61	1	44.79
12	149.1		1	0		2	149	0	2.42	1	44.79
12	150.1		1	1		1	150	0	2.24	0	44.79
12	152.1		1	1		2	152	0	2.42	1	44.79
12	153.1		1	1		1	152	0	2.98	0	44.79

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	96.1	121.65	0.43	2.31	0.33	3.03	0			
12	97.1	91.49	0.42	2.35	0.33	3.03	0			
12	103.1	125.62	0.36	2.80	0.36	2.80	1	1		3.03
12	104.1	154.19	0.35	2.82	0.35	2.82	1	0		2.80
12	105.1	155.83	0.35	2.84	0.35	2.84	1	0		2.82
12	106.1	189.99	0.35	2.87	0.35	2.87	1	2		2.84
12	108.1	92.72	0.33	3.05	0.33	3.05	1	3		2.84
12	109.1	94.02	0.33	3.07	0.33	3.07	1	1		2.84
12	110.1	161.97	0.33	3.04	0.33	3.07	0			
12	111.1	163.80	0.36	2.80	0.33	3.07	0			
12	113.1	165.50	0.34	2.91	0.34	2.91	1	4		3.07
12	114.1	93.62	0.35	2.88	0.34	2.91	0			
12	115.1	95.43	0.35	2.88	0.34	2.91	0			
12	116.1	213.48	0.36	2.80	0.36	2.80	1	1		2.91
12	117.1	212.98	0.39	2.56	0.36	2.80	0			
12	118.1	214.61	0.39	2.54	0.36	2.80	0			
12	119.1	169.74	0.39	2.55	0.36	2.80	0			
12	120.1	97.63	0.39	2.54	0.39	2.54	1	1		2.80
12	121.1	99.10	0.39	2.56	0.39	2.54	0			
12	122.1	134.90	0.40	2.53	0.39	2.54	0			
12	123.1	174.11	0.41	2.46	0.39	2.54	0			
12	124.1	177.05	0.40	2.48	0.40	2.48	1	0		2.54
12	125.1	173.14	0.37	2.69	0.37	2.69	1	0		2.48
12	126.1	176.78	0.37	2.74	0.37	2.69	0			
12	127.1	243.58	0.37	2.71	0.37	2.69	0			
12	128.1	178.41	0.37	2.73	0.37	2.69	0			
12	129.1	248.45	0.37	2.74	0.37	2.74	1	1		2.69
12	130.1	138.74	0.36	2.74	0.36	2.74	1	0		2.74
12	131.1	136.64	0.37	2.74	0.36	2.74	0			
12	132.1	95.59	0.36	2.76	0.36	2.74	0			
12	133.1	97.33	0.36	2.75	0.36	2.74	0			
12	134.1	186.89	0.36	2.77	0.36	2.74	0			
12	135.1	143.31	0.36	2.74	0.36	2.74	0			
12	136.1	261.76	0.36	2.75	0.36	2.75	1	0		2.74
12	137.1	102.07	0.37	2.73	0.36	2.75	0			
12	138.1	101.57	0.36	2.76	0.36	2.75	0			
12	139.1	99.46	0.36	2.77	0.36	2.75	0			
12	140.1	104.50	0.36	2.75	0.36	2.75	0			
12	141.1	123.32	0.40	2.52	0.40	2.52	1	2		2.75
12	142.1	119.62	0.41	2.44	0.40	2.52	0			
12	143.1	105.67	0.36	2.81	0.36	2.81	1	3		2.75
12	144.1	108.14	0.35	2.86	0.36	2.81	0			
12	145.1	110.81	0.35	2.82	0.36	2.81	0			
12	146.1	123.19	0.37	2.71	0.37	2.71	1	1		2.75
12	147.1	124.52	0.36	2.74	0.36	2.74	1	0		2.71
12	148.1	168.47	0.38	2.62	0.38	2.62	1	1		2.74
12	149.1	162.83	0.34	2.98	0.34	2.98	1	3		2.74
12	150.1	164.86	0.36	2.81	0.36	2.81	1	2		2.74
12	152.1	166.83	0.35	2.84	0.35	2.84	1	0		2.62
12	153.1	170.54	0.36	2.81	0.35	2.84	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	154.1		1	1		2	152	0	2.80	1	1.83
12	155.1		1	1		2	152	0	2.98	2	44.79
12	156.1		1	0		2	152	0	2.98	1	19.01
12	157.1		1	1		1	152	0	2.80	1	44.79
12	158.1		1	1		2	152	0	2.61	2	19.01
12	159.1		1	1		1	152	0	2.42	2	19.01
12	160.1		1	1		2	160	0	2.05	1	70.56
12	161.1		1	1		1	160	0	2.05	2	70.56
12	162.1		1	1		1	160	0	2.24	1	44.79
12	163.1		1	1		1	160	0	2.42	1	10.42
12	164.1		1	1		2	160	0	2.42	2	10.42
12	165.1		0	1		2	160	0	2.24	0	27.60
12	166.1		0	1		2	166	0	2.05	0	27.60
12	167.1		1	1		1	166	0	1.86	2	27.60
12	168.1		1	1		1	166	0	2.24	2	27.60
12	169.1		1	1		1	166	0	1.86	1	27.60
12	170.1		1	1		1	171	0	2.42	2	44.79
12	171.1		1	1		2	171	0	2.24	1	44.79
12	172.1		1	1		1	171	0	2.61	2	70.56
12	173.1		1	1		2	171	0	2.42	2	70.56
12	174.1		0	0		1	171	0	2.61	1	44.79
12	175.1		0	0		2	171	0	2.24	2	53.38
12	176.1		1	1		1	176	0	2.05	2	53.38
12	177.1		1	1		2	177	0	1.86	1	70.56
12	178.1		1	1		1	178	0	2.05	0	44.79
12	179.1		0	1		1	178	0	2.05	1	36.19
12	180.1		1	1		2	180	0	2.24	1	1.83
12	181.1		1	1		1	181	0	2.24	0	44.79
12	182.1		1	1		1	182	0	2.61	1	44.79
12	183.1		0	1		1	182	0	2.61	1	70.56
12	184.1		0	1		1	182	0	2.61	1	36.19
12	185.1		0	0		1	182	0	2.42	2	36.19
12	186.1		0	1		1	182	0	2.42	1	10.42
12	187.1		0	1		1	182	0	2.42	1	10.42
12	188.1		1	1		1	182	0	2.61	2	53.38
12	189.1		1	1		1	182	0	2.61	1	10.42
12	190.1		0	1		2	182	0	2.42	2	61.97
12	191.1		0	0		1	182	0	2.80	1	61.97
12	192.1		0	1		1	182	0	2.61	2	61.97
12	193.1		0	1		1	182	0	2.61	1	53.38
12	194.1		1	1		1	182	0	2.80	2	53.38
12	195.1		0	0		1	182	0	2.61	1	36.19
12	196.1		0	0		1	182	0	2.42	2	36.19
12	197.1		1	1		1	182	0	2.24	1	53.38
12	198.1		0	1		2	198	0	2.24	0	36.19
12	199.1		0	0		1	198	0	2.42	2	36.19
12	200.1		1	1		1	198	0	2.24	0	53.38
12	201.1		1	0		2	201	0	2.24	1	36.19
12	202.1		1	1		1	201	0	2.24	2	36.19
12	204.1		1	1		2	204	0	2.24	2	61.97

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	154.1	288.02	0.36	2.81	0.35	2.84	0			
12	155.1	172.10	0.35	2.83	0.35	2.84	0			
12	156.1	234.87	0.34	2.91	0.35	2.84	0			
12	157.1	173.74	0.34	2.95	0.35	2.84	0			
12	158.1	247.98	0.35	2.89	0.35	2.84	0			
12	159.1	250.49	0.35	2.89	0.35	2.84	0			
12	160.1	91.72	0.35	2.89	0.35	2.89	1	1		2.84
12	161.1	97.90	0.34	2.91	0.35	2.89	0			
12	162.1	178.34	0.35	2.88	0.35	2.89	0			
12	163.1	311.58	0.35	2.89	0.35	2.89	0			
12	164.1	313.25	0.34	2.92	0.35	2.89	0			
12	165.1	257.79	0.34	2.91	0.35	2.89	0			
12	166.1	262.37	0.34	2.92	0.34	2.92	1	1		2.89
12	167.1	264.23	0.34	2.93	0.34	2.92	0			
12	168.1	266.37	0.34	2.91	0.34	2.92	0			
12	169.1	268.84	0.35	2.89	0.34	2.92	0			
12	170.1	182.51	0.35	2.88	0.35	2.84	0			
12	171.1	181.78	0.35	2.84	0.35	2.84	1	1		2.92
12	172.1	96.00	0.35	2.82	0.35	2.84	0			
12	173.1	98.83	0.36	2.80	0.35	2.84	0			
12	174.1	189.09	0.36	2.80	0.35	2.84	0			
12	175.1	130.93	0.37	2.72	0.35	2.84	0			
12	176.1	145.74	0.39	2.57	0.39	2.57	1	2		2.84
12	177.1	109.38	0.36	2.79	0.60	1.66	1	3		2.84
12	178.1	192.46	0.37	2.70	0.37	2.70	1	1		2.84
12	179.1	193.19	0.37	2.67	0.37	2.70	0			
12	180.1	343.78	0.35	2.82	0.35	2.82	1	2		2.70
12	181.1	195.36	0.40	2.48	0.40	2.48	1	3		2.70
12	182.1	197.20	0.39	2.56	0.39	2.56	1	1		2.70
12	183.1	110.38	0.39	2.56	0.39	2.56	0			
12	184.1	206.81	0.39	2.59	0.39	2.56	0			
12	185.1	214.55	0.38	2.60	0.39	2.56	0			
12	186.1	355.35	0.39	2.59	0.39	2.56	0			
12	187.1	357.86	0.39	2.57	0.39	2.56	0			
12	188.1	146.18	0.39	2.58	0.39	2.56	0			
12	189.1	361.43	0.39	2.59	0.39	2.56	0			
12	190.1	148.14	0.38	2.61	0.39	2.56	0			
12	191.1	146.71	0.39	2.58	0.39	2.56	0			
12	192.1	149.91	0.38	2.61	0.39	2.56	0			
12	193.1	150.08	0.39	2.58	0.39	2.56	0			
12	194.1	151.78	0.39	2.55	0.39	2.56	0			
12	195.1	220.22	0.39	2.57	0.39	2.56	0			
12	196.1	232.16	0.40	2.53	0.39	2.56	0			
12	197.1	162.06	0.40	2.51	0.39	2.56	0			
12	198.1	252.32	0.40	2.47	0.40	2.47	1	1		2.56
12	199.1	250.15	0.41	2.46	0.40	2.47	0			
12	200.1	163.53	0.41	2.41	0.40	2.47	0			
12	201.1	268.77	0.41	2.44	0.41	2.44	1	0		2.47
12	202.1	274.44	0.41	2.46	0.41	2.44	0			
12	204.1	163.16	0.41	2.46	0.41	2.46	1	0		2.44

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	205.1		0	0		1	204	0	2.05	1	61.97
12	206.1		1	1		1	204	0	1.86	1	61.97
12	207.1		1	1		.	207	0	1.68	2	61.97
12	208.1		1	1		1	207	0	1.86	1	61.97
12	209.1		1	1		1	210	0	2.24	2	44.79
12	210.1		1	0		1	210	0	1.86	1	44.79
12	211.1		0	0		1	210	0	2.61	2	44.79
12	212.1		1	1		2	210	0	2.24	1	36.19
12	213.1		0	1		.	213	0	2.24	2	10.42
12	214.1		1	1		.	214	0	1.86	1	61.97
12	215.1		1	1		1	214	0	1.86	2	61.97
12	216.1		1	1		1	214	0	1.86	1	70.56
12	217.1		0	0		2	214	0	2.05	1	61.97
12	218.1		1	1		1	214	0	2.24	1	70.56
12	219.1		1	1		2	214	0	2.42	1	70.56
12	220.1		0	0		2	214	0	2.42	2	27.60
12	221.1		0	1		2	221	0	2.42	2	27.60
12	222.1		0	1		1	221	0	2.24	1	1.83
12	223.1		0	0		2	221	0	2.24	1	70.56
12	224.1		1	1		1	221	0	2.42	1	27.60
12	225.1		0	0		1	221	0	2.42	1	70.56
12	226.1		0	0		2	226	0	2.42	1	27.60
12	227.1		1	1		2	226	0	2.42	2	61.97
12	228.1		0	0		1	226	0	2.42	1	27.60
12	229.1		1	1		1	226	0	2.42	1	27.60
12	230.1		0	0		1	230	0	2.61	2	61.97
12	231.1		0	0		1	231	0	2.61	1	61.97
12	232.1		1	1		2	232	0	2.61	2	27.60
12	233.1		1	0		1	232	0	2.24	1	44.79
12	234.1		1	1		.	234	0	1.86	2	44.79
12	235.1		1	1		1	234	0	1.86	2	27.60
12	236.1		1	1		1	234	0	2.05	1	44.79
12	237.1		0	0		1	234	0	2.05	1	61.97
12	238.1		0	0		1	234	0	2.24	2	61.97
12	239.1		1	1		1	234	0	2.61	1	27.60
12	240.1		0	0		1	234	0	2.61	2	27.60
12	241.1		1	1		1	234	0	2.98	1	27.60
12	242.1		1	1		.	242	0	2.42	0	79.15
12	243.1		0	0		2	242	0	2.24	1	44.79
12	244.1		0	1		2	242	0	1.86	1	61.97
12	245.1		0	1		2	242	0	1.86	1	61.97
12	246.1		0	0		1	242	0	1.86	2	61.97
12	247.1		0	0		1	242	0	2.24	1	61.97
12	248.1		0	0		1	242	0	2.42	1	61.97
12	249.1		1	1		1	242	0	2.42	2	70.56
12	250.1		0	0		1	242	0	2.61	1	70.56
12	251.1		0	1		2	251	0	2.42	2	61.97
12	252.1		1	1		.	252	0	2.05	1	53.38
12	253.1		1	1		1	252	0	2.05	2	53.38
12	254.1		1	1		1	252	0	1.86	1	61.97

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	205.1	166.90	0.42	2.40	0.41	2.46	0			
12	206.1	170.83	0.42	2.41	0.41	2.46	0			
12	207.1	169.40	0.42	2.39	0.42	2.39	1	1		2.46
12	208.1	172.77	0.42	2.38	0.42	2.39	0			
12	209.1	291.52	0.41	2.41	0.41	2.42	0			
12	210.1	293.46	0.41	2.42	0.41	2.42	1	0		2.39
12	211.1	295.89	0.42	2.39	0.41	2.42	0			
12	212.1	290.19	0.42	2.40	0.41	2.42	0			
12	213.1	406.87	0.43	2.35	0.43	2.35	1	0		2.42
12	214.1	184.98	0.43	2.35	0.43	2.35	1	0		2.35
12	215.1	182.18	0.43	2.33	0.43	2.35	0			
12	216.1	155.89	0.45	2.24	0.43	2.35	0			
12	217.1	190.29	0.47	2.14	0.43	2.35	0			
12	218.1	161.83	0.47	2.11	0.43	2.35	0			
12	219.1	163.40	0.49	2.06	0.43	2.35	0			
12	220.1	363.30	0.49	2.05	0.43	2.35	0			
12	221.1	361.26	0.49	2.05	0.49	2.05	1	1		2.35
12	222.1	424.32	0.49	2.04	0.49	2.05	0			
12	223.1	164.26	0.49	2.04	0.49	2.05	0			
12	224.1	368.07	0.49	2.04	0.49	2.05	0			
12	225.1	165.03	0.49	2.02	0.49	2.05	0			
12	226.1	373.24	0.49	2.06	0.49	2.06	1	0		2.05
12	227.1	199.70	0.48	2.10	0.49	2.06	0			
12	228.1	379.82	0.47	2.13	0.49	2.06	0			
12	229.1	382.09	0.47	2.13	0.49	2.06	0			
12	230.1	207.24	0.49	2.06	0.49	2.06	1	2		2.06
12	231.1	202.37	0.47	2.14	0.47	2.14	1	3		2.06
12	232.1	388.26	0.48	2.09	0.48	2.09	1	0		2.06
12	233.1	318.08	0.48	2.10	0.48	2.09	0			
12	234.1	322.12	0.48	2.09	0.48	2.09	1	0		2.09
12	235.1	399.44	0.49	2.03	0.48	2.09	0			
12	236.1	320.65	0.47	2.13	0.48	2.09	0			
12	237.1	206.04	0.48	2.10	0.48	2.09	0			
12	238.1	204.13	0.48	2.09	0.48	2.09	0			
12	239.1	398.53	0.47	2.11	0.48	2.09	0			
12	240.1	400.74	0.46	2.15	0.48	2.09	0			
12	241.1	404.64	0.47	2.15	0.48	2.09	0			
12	242.1	171.50	0.46	2.16	0.46	2.16	1	0		2.09
12	243.1	331.90	0.46	2.17	0.46	2.16	0			
12	244.1	216.68	0.47	2.14	0.46	2.16	0			
12	245.1	218.58	0.47	2.15	0.46	2.16	0			
12	246.1	220.52	0.47	2.14	0.46	2.16	0			
12	247.1	214.38	0.47	2.15	0.46	2.16	0			
12	248.1	222.32	0.47	2.14	0.46	2.16	0			
12	249.1	195.40	0.47	2.13	0.46	2.16	0			
12	250.1	196.70	0.47	2.13	0.46	2.16	0			
12	251.1	227.56	0.47	2.12	0.47	2.12	1	1		2.16
12	252.1	228.59	0.49	2.06	0.49	2.06	1	1		2.12
12	253.1	229.99	0.49	2.05	0.49	2.06	0			
12	254.1	229.69	0.49	2.05	0.49	2.06	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	255.1		0	0		2	252	0	1.68	2	61.97
12	256.1		0	1		2	252	0	1.86	2	61.97
12	257.1		0	0		2	252	0	1.86	1	61.97
12	258.1		0	1		1	252	0	1.86	2	61.97
12	259.1		0	0		2	259	0	1.86	0	61.97
12	260.1		0	1		2	259	0	1.86	0	70.56
12	261.1		1	1		1	259	0	1.86	1	70.56
12	262.1		1	1		2	259	0	2.24	2	79.15
12	263.1		0	0		.	263	0	1.86	0	61.97
12	264.1		0	1		2	263	0	1.86	0	61.97
12	265.1		1	1		.	265	0	1.86	0	19.01
12	266.1		1	1		.	266	0	1.49	2	61.97
12	267.1		1	1		1	266	0	1.68	1	79.15
12	268.1		0	1		1	268	0	1.68	2	44.79
12	269.1		1	0		1	268	0	1.68	1	61.97
12	270.1		1	1		.	270	0	1.86	0	70.56
12	271.1		1	1		1	270	0	1.49	2	70.56
12	272.1		0	0		1	270	0	1.49	2	61.97
12	273.1		1	1		1	270	0	1.49	1	61.97
12	274.1		0	1		2	274	0	1.86	1	61.97
12	275.1		0	0		2	274	0	1.86	1	61.97
12	276.1		0	0		2	276	0	1.86	1	61.97
12	277.1		1	1		.	277	0	1.49	2	36.19
12	278.1		0	0		2	277	0	1.68	1	61.97
12	280.1		0	1		.	280	0	0.37	2	61.97
12	281.1		0	1		1	282	0	1.12	1	36.19
12	282.1		1	1		.	282	0	0.75	1	36.19
12	283.1		0	0		.	283	0	1.12	1	10.42
12	284.1		0	0		2	283	0	1.49	0	10.42
12	285.1		0	0		.	285	0	1.49	1	70.56
12	286.1		0	0		.	286	0	0.75	0	10.42
12	287.1		0	1		.	287	0	0.37	1	36.19
12	288.1		0	1		.	288	0	0.75	2	36.19
12	289.1		0	0		2	282	0	1.49	0	61.97
12	290.1		0	0		.	290	0	0.37	2	10.42
12	291.1		0	1		2	290	0	0.75	1	10.42
12	292.1		0	0		2	292	0	1.12	2	10.42
12	293.1		0	0		2	293	0	1.31	2	10.42
12	294.1		0	0		.	294	0	0.56	2	79.15
12	300.1		1	1		1	35	0	1.12	1	36.19
12	301.1		0	1		2	35	0	1.49	2	44.79
12	27.2		1	1		.	27	0	0.75	1	10.42
12	28.2		0	1		.	28	0	1.68	2	19.01
12	37.2		0	0		1	301	0	1.68	1	36.19
12	38.2		0	0		2	301	0	1.86	1	36.19
12	39.2		1	1		.	39	0	1.86	2	1.83
12	47.2		1	1		.	47	0	1.68	0	10.42
12	48.2		0	0		.	48	0	1.49	2	10.42
12	49.2		1	1		2	49	0	1.49	1	10.42
12	60.2		0	0		.	60	0	1.31	1	1.83

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	255.1	266.33	0.49	2.04	0.49	2.06	0			
12	256.1	276.71	0.49	2.05	0.49	2.06	0			
12	257.1	259.16	0.49	2.02	0.49	2.06	0			
12	258.1	301.36	0.48	2.08	0.49	2.06	0			
12	259.1	304.03	0.49	2.06	0.49	2.06	1	1		2.06
12	260.1	209.14	0.49	2.05	0.49	2.06	0			
12	261.1	216.52	0.49	2.05	0.49	2.06	0			
12	262.1	223.02	0.49	2.05	0.49	2.06	0			
12	263.1	317.71	0.49	2.04	0.49	2.04	1	0		2.06
12	264.1	321.32	0.49	2.05	0.49	2.04	0			
12	265.1	457.03	0.49	2.03	0.49	2.03	1	0		2.04
12	266.1	326.62	0.52	1.92	0.52	1.92	1	0		2.03
12	267.1	227.23	0.52	1.92	0.52	1.92	0			
12	268.1	406.41	0.52	1.93	0.52	1.93	1	0		1.92
12	269.1	331.43	0.52	1.92	0.52	1.93	0			
12	270.1	237.24	0.52	1.92	0.52	1.92	1	0		1.93
12	271.1	233.60	0.52	1.91	0.52	1.92	0			
12	272.1	345.78	0.53	1.89	0.52	1.92	0			
12	273.1	341.54	0.53	1.88	0.52	1.92	0			
12	274.1	344.24	0.54	1.87	0.54	1.87	1	1		1.92
12	275.1	346.94	0.53	1.88	0.54	1.87	0			
12	276.1	426.76	0.53	1.88	0.53	1.88	1	1		1.87
12	277.1	442.54	0.53	1.89	0.53	1.89	1	0		1.88
12	278.1	445.84	0.53	1.89	0.53	1.89	0			
12	280.1	551.95	1.02	0.98	1.02	0.98	1	2		1.89
12	281.1	583.95	0.50	2.00	0.50	2.01	0			
12	282.1	582.78	0.50	2.01	0.50	2.01	1	0		5.31
12	283.1	671.60	0.83	1.21	0.83	1.21	1	1		2.01
12	284.1	673.44	0.81	1.23	0.83	1.21	0			
12	285.1	608.31	0.87	1.16	0.87	1.16	1	0		1.21
12	286.1	691.22	0.91	1.09	0.91	1.09	1	0		1.16
12	287.1	445.14	0.21	4.86	0.21	4.86	1	0		1.89
12	288.1	431.53	0.19	5.31	0.19	5.31	1	0		4.86
12	289.1	576.61	0.33	3.07	0.50	2.01	0			
12	290.1	879.85	0.98	1.02	0.98	1.02	1	0		1.09
12	291.1	881.18	0.95	1.05	0.98	1.02	0			
12	292.1	882.72	0.99	1.01	0.99	1.01	1	1		1.02
12	293.1	884.32	1.00	1.00	1.00	1.00	1	0		1.01
12	294.1	830.40	1.09	0.91	1.09	0.91	1	0		1.00
12	300.1	53.15	0.77	1.30	0.69	1.45	0			
12	301.1	58.16	0.74	1.35	0.69	1.45	0			
12	27.2	48.65	0.72	1.39	0.72	1.39	1	1		.
12	28.2	38.10	0.75	1.34	0.75	1.34	1	1		1.39
12	37.2	41.97	0.75	1.33	0.76	1.32	0			
12	38.2	46.14	0.75	1.34	0.76	1.32	0			
12	39.2	81.95	0.75	1.33	0.75	1.33	1	0		1.32
12	47.2	83.99	0.57	1.74	0.57	1.74	1	1		1.33
12	48.2	86.22	0.57	1.77	0.57	1.77	1	0		1.74
12	49.2	88.19	0.57	1.77	0.57	1.77	1	1		1.77
12	60.2	101.64	0.58	1.73	0.58	1.73	1	0		1.77

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	64.2		0	1		2	60	0	1.31	1	1.83
12	67.2		1	1		2	67	0	1.68	0	1.83
12	68.2		0	0		2	68	0	1.68	0	44.79
12	69.2		0	1		.	69	0	1.31	1	27.60
12	71.2		1	0		1	71	0	1.86	1	1.83
12	72.2		1	0		2	72	0	2.24	2	1.83
12	73.2		1	1		2	73	0	1.86	1	1.83
12	74.2		1	1		1	73	0	1.86	1	1.83
12	75.2		1	1		2	75	0	1.86	0	1.83
12	77.2		1	1		.	75	0	1.68	1	36.19
12	79.2		1	1		2	79	0	1.86	0	27.60
12	82.2		0	1		1	82	0	2.42	1	1.83
12	84.2		1	1		.	84	0	1.31	1	53.38
12	85.2		0	0		.	85	0	1.31	2	53.38
12	86.2		0	1		.	86	0	1.68	1	1.83
12	87.2		0	1		.	87	0	1.49	1	1.83
12	88.2		0	1		.	88	0	1.49	1	53.38
12	89.2		1	1		2	89	0	1.49	0	27.60
12	90.2		1	1		.	90	0	1.49	2	27.60
12	91.2		1	1		2	90	0	1.49	2	27.60
12	95.2		0	0		1	95	0	2.24	1	27.60
12	96.2		1	1		2	96	0	2.05	2	27.60
12	97.2		1	1		.	97	0	1.49	2	44.79
12	103.2		0	0		.	103	0	1.49	1	27.60
12	104.2		1	1		1	103	0	1.68	1	10.42
12	105.2		1	1		2	103	0	1.68	2	10.42
12	108.2		1	1		.	108	0	1.86	1	36.19
12	109.2		1	1		1	109	0	2.05	0	36.19
12	110.2		1	1		1	110	0	1.86	1	10.42
12	111.2		1	1		2	111	0	1.68	1	10.42
12	113.2		0	1		2	111	0	1.68	0	10.42
12	114.2		1	1		2	114	0	1.68	1	44.79
12	115.2		1	1		1	114	0	1.86	2	44.79
12	119.2		1	1		1	119	0	2.42	1	10.42
12	120.2		0	0		1	120	0	2.24	2	44.79
12	121.2		0	0		1	120	0	2.61	1	44.79
12	122.2		0	1		1	120	0	2.24	1	19.01
12	123.2		0	0		1	123	0	2.42	1	10.42
12	124.2		1	1		.	124	0	2.80	2	10.42
12	125.2		1	1		.	125	0	1.86	1	1.83
12	126.2		1	1		1	126	0	1.86	2	1.83
12	128.2		1	1		1	128	0	1.86	2	1.83
12	130.2		1	1		2	130	0	2.24	0	19.01
12	131.2		0	0		2	130	0	2.24	0	19.01
12	132.2		0	0		2	130	0	2.42	1	36.19
12	133.2		0	0		1	130	0	2.42	2	36.19
12	134.2		1	1		1	130	0	2.61	1	10.42
12	135.2		1	1		1	130	0	2.98	1	19.01
12	137.2		1	1		1	130	0	3.36	0	36.19
12	138.2		0	0		2	138	0	2.42	2	44.79

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	64.2	103.14	0.58	1.73	0.58	1.73	0			
12	67.2	105.44	0.58	1.71	0.58	1.71	1	1		1.73
12	68.2	67.70	0.58	1.73	0.58	1.73	1	1		1.73
12	69.2	77.81	0.58	1.73	0.58	1.73	1	1		1.71
12	71.2	106.78	0.56	1.79	0.56	1.79	1	0		1.73
12	72.2	107.54	0.56	1.78	0.56	1.78	1	4		1.79
12	73.2	109.85	0.55	1.80	0.55	1.80	1	0		1.78
12	74.2	111.58	0.55	1.82	0.55	1.80	0			
12	75.2	113.85	0.55	1.80	0.55	1.80	1	1		1.80
12	77.2	75.64	0.55	1.81	0.55	1.80	0			
12	79.2	94.33	0.55	1.83	0.55	1.83	1	0		1.80
12	82.2	115.75	0.51	1.96	0.51	1.96	1	0		1.83
12	84.2	54.82	0.57	1.77	0.57	1.77	1	0		1.96
12	85.2	55.96	0.57	1.74	0.57	1.74	1	0		1.77
12	86.2	130.10	0.58	1.73	0.58	1.73	1	0		1.74
12	87.2	132.00	0.58	1.72	0.58	1.72	1	0		1.73
12	88.2	61.83	0.57	1.75	0.57	1.75	1	0		1.72
12	89.2	113.55	0.59	1.70	0.59	1.70	1	0		1.75
12	90.2	115.71	0.60	1.66	0.60	1.66	1	1		1.70
12	91.2	117.65	0.60	1.68	0.60	1.66	0			
12	95.2	119.69	0.51	1.97	0.51	1.97	1	4		1.66
12	96.2	121.65	0.38	2.65	0.38	2.65	1	1		1.97
12	97.2	91.49	0.43	2.34	0.43	2.34	1	1		2.65
12	103.2	125.62	0.43	2.35	0.43	2.35	1	0		2.34
12	104.2	154.19	0.43	2.32	0.43	2.35	0			
12	105.2	155.83	0.43	2.33	0.43	2.35	0			
12	108.2	92.72	0.43	2.33	0.43	2.33	1	0		2.35
12	109.2	94.02	0.43	2.33	0.43	2.33	1	1		2.33
12	110.2	161.97	0.42	2.36	0.42	2.36	1	1		2.33
12	111.2	163.80	0.39	2.60	0.39	2.60	1	1		2.36
12	113.2	165.50	0.39	2.58	0.39	2.60	0			
12	114.2	93.62	0.38	2.61	0.38	2.61	1	4		2.60
12	115.2	95.43	0.39	2.58	0.38	2.61	0			
12	119.2	169.74	0.31	3.24	0.31	3.24	1	1		2.61
12	120.2	97.63	0.31	3.27	0.31	3.27	1	0		3.24
12	121.2	99.10	0.31	3.23	0.31	3.27	0			
12	122.2	134.90	0.31	3.27	0.31	3.27	0			
12	123.2	174.11	0.30	3.31	0.30	3.31	1	2		3.27
12	124.2	177.05	0.30	3.30	0.30	3.30	1	2		3.27
12	125.2	173.14	0.30	3.38	0.30	3.38	1	3		3.27
12	126.2	176.78	0.30	3.35	0.30	3.38	1	3		3.27
12	128.2	178.41	0.29	3.49	0.29	3.49	1	1		3.27
12	130.2	138.74	0.28	3.60	0.28	3.60	1	1		3.38
12	131.2	136.64	0.27	3.73	0.28	3.60	0			
12	132.2	95.59	0.27	3.69	0.28	3.60	0			
12	133.2	97.33	0.27	3.68	0.28	3.60	0			
12	134.2	186.89	0.27	3.65	0.28	3.60	0			
12	135.2	143.31	0.27	3.67	0.28	3.60	0			
12	137.2	102.07	0.27	3.75	0.28	3.60	0			
12	138.2	101.57	0.28	3.58	0.28	3.58	1	2		3.60

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	139.2		1	1		1	139	0	3.17	1	36.19
12	140.2		0	0		1	140	0	2.98	1	36.19
12	141.2		1	1		2	145	0	2.98	1	36.19
12	142.2		1	1		1	145	0	2.98	1	36.19
12	143.2		1	1		2	140	0	2.80	1	36.19
12	144.2		1	1		2	140	0	2.98	2	36.19
12	145.2		0	0		2	145	0	2.98	1	36.19
12	146.2		1	1		.	146	0	2.61	2	36.19
12	147.2		1	1		.	147	0	2.80	1	36.19
12	148.2		1	1		2	148	0	2.80	0	27.60
12	149.2		1	0		2	149	0	2.80	1	27.60
12	150.2		1	1		1	149	0	2.80	0	27.60
12	152.2		1	1		2	148	0	2.61	1	27.60
12	153.2		1	1		1	153	0	2.98	1	27.60
12	155.2		1	1		1	153	0	2.98	2	27.60
12	156.2		1	0		1	153	0	2.98	1	1.83
12	157.2		1	1		1	153	0	2.98	1	27.60
12	158.2		1	1		2	158	0	2.61	1	1.83
12	159.2		1	1		1	158	0	2.42	0	1.83
12	160.2		1	1		1	160	0	2.61	1	53.38
12	161.2		1	1		1	160	0	2.42	2	53.38
12	162.2		1	1		1	162	0	2.24	1	27.60
12	165.2		0	1		1	165	0	2.05	1	10.42
12	166.2		0	1		.	166	0	1.86	0	10.42
12	167.2		1	1		1	166	0	2.05	1	10.42
12	168.2		1	1		2	166	0	2.42	2	10.42
12	169.2		1	1		1	166	0	2.05	1	10.42
12	170.2		1	1		1	171	0	2.42	2	27.60
12	171.2		1	1		1	171	0	2.24	1	27.60
12	172.2		1	1		1	171	0	2.61	0	53.38
12	173.2		1	1		1	171	0	2.61	2	53.38
12	174.2		0	0		1	171	0	2.80	1	27.60
12	175.2		0	0		2	175	0	2.42	2	36.19
12	176.2		1	1		1	176	0	2.24	2	36.19
12	177.2		1	1		2	175	0	2.05	1	53.38
12	178.2		1	1		1	178	0	2.24	1	27.60
12	179.2		0	1		1	178	0	2.24	1	19.01
12	181.2		1	1		2	178	0	2.24	1	27.60
12	182.2		1	1		2	182	0	2.61	1	27.60
12	183.2		0	1		1	183	0	2.61	1	53.38
12	184.2		0	1		1	184	0	2.61	1	19.01
12	185.2		0	0		1	184	0	2.61	2	19.01
12	188.2		1	1		1	188	0	2.80	0	36.19
12	190.2		0	1		1	190	0	2.61	2	44.79
12	191.2		0	0		1	190	0	2.61	1	44.79
12	192.2		0	1		1	190	0	2.61	0	44.79
12	193.2		0	1		1	190	0	2.61	0	36.19
12	194.2		1	1		1	190	0	2.98	0	36.19
12	195.2		0	0		1	190	0	2.61	1	19.01
12	196.2		0	0		1	190	0	2.42	0	19.01

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	139.2	99.46	0.26	3.84	0.26	3.84	1	3		3.60
12	140.2	104.50	0.27	3.65	0.27	3.65	1	1		3.60
12	141.2	123.32	0.29	3.42	0.27	3.66	0			
12	142.2	119.62	0.29	3.50	0.27	3.66	0			
12	143.2	105.67	0.28	3.61	0.27	3.65	0			
12	144.2	108.14	0.28	3.59	0.27	3.65	0			
12	145.2	110.81	0.27	3.66	0.27	3.66	1	1		3.65
12	146.2	123.19	0.30	3.35	0.30	3.35	1	0		3.66
12	147.2	124.52	0.30	3.32	0.30	3.32	1	0		3.35
12	148.2	168.47	0.36	2.76	0.36	2.76	1	0		2.95
12	149.2	162.83	0.34	2.95	0.34	2.95	1	0		3.32
12	150.2	164.86	0.35	2.84	0.34	2.95	0			
12	152.2	166.83	0.35	2.88	0.36	2.76	0			
12	153.2	170.54	0.34	2.91	0.34	2.91	1	4		2.76
12	155.2	172.10	0.33	2.99	0.34	2.91	0			
12	156.2	234.87	0.33	3.01	0.34	2.91	0			
12	157.2	173.74	0.33	3.00	0.34	2.91	0			
12	158.2	247.98	0.33	3.06	0.33	3.06	1	2		2.91
12	159.2	250.49	0.33	3.00	0.33	3.06	0			
12	160.2	91.72	0.36	2.75	0.36	2.75	1	3		2.91
12	161.2	97.90	0.37	2.72	0.36	2.75	0			
12	162.2	178.34	0.37	2.73	0.37	2.73	1	1		2.91
12	165.2	257.79	0.35	2.85	0.35	2.85	1	4		2.73
12	166.2	262.37	0.36	2.79	0.36	2.79	1	0		2.85
12	167.2	264.23	0.36	2.80	0.36	2.79	0			
12	168.2	266.37	0.35	2.87	0.36	2.79	0			
12	169.2	268.84	0.35	2.87	0.36	2.79	0			
12	170.2	182.51	0.35	2.85	0.35	2.87	0			
12	171.2	181.78	0.35	2.87	0.35	2.87	1	0		2.79
12	172.2	96.00	0.35	2.89	0.35	2.87	0			
12	173.2	98.83	0.34	2.91	0.35	2.87	0			
12	174.2	189.09	0.34	2.92	0.35	2.87	0			
12	175.2	130.93	0.36	2.79	0.36	2.79	1	1		2.87
12	176.2	145.74	0.39	2.55	0.39	2.55	1	2		2.79
12	177.2	109.38	0.35	2.84	0.36	2.79	0			
12	178.2	192.46	0.34	2.90	0.34	2.90	1	1		2.79
12	179.2	193.19	0.34	2.93	0.34	2.90	0			
12	181.2	195.36	0.32	3.12	0.34	2.90	0			
12	182.2	197.20	0.33	3.06	0.33	3.06	1	1		2.90
12	183.2	110.38	0.33	3.05	0.33	3.05	1	1		3.06
12	184.2	206.81	0.34	2.98	0.34	2.98	1	1		3.05
12	185.2	214.55	0.33	3.06	0.34	2.98	0			
12	188.2	146.18	0.31	3.20	0.31	3.20	1	4		2.98
12	190.2	148.14	0.32	3.16	0.32	3.16	1	4		3.20
12	191.2	146.71	0.31	3.21	0.32	3.16	0			
12	192.2	149.91	0.31	3.19	0.32	3.16	0			
12	193.2	150.08	0.31	3.24	0.32	3.16	0			
12	194.2	151.78	0.31	3.19	0.32	3.16	0			
12	195.2	220.22	0.32	3.17	0.32	3.16	0			
12	196.2	232.16	0.32	3.16	0.32	3.16	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	197.2		1	1		1	190	0	2.61	1	36.19
12	198.2		0	1		2	198	0	2.42	0	19.01
12	199.2		0	0		1	198	0	2.42	2	19.01
12	200.2		1	1		1	198	0	2.42	2	36.19
12	201.2		1	0		2	198	0	2.42	1	19.01
12	202.2		1	1		1	198	0	2.42	2	19.01
12	204.2		1	1		.	204	0	2.24	0	44.79
12	205.2		0	0		1	204	0	1.86	0	44.79
12	206.2		1	1		1	204	0	1.86	0	44.79
12	207.2		1	1		.	207	0	1.86	2	44.79
12	208.2		1	1		1	207	0	2.05	1	44.79
12	209.2		1	1		1	207	0	2.42	0	27.60
12	210.2		1	0		1	207	0	2.42	1	27.60
12	211.2		0	0		1	207	0	2.98	0	27.60
12	212.2		1	1		2	207	0	2.80	1	19.01
12	214.2		1	1		1	214	0	2.80	1	44.79
12	215.2		1	1		1	215	0	2.61	2	44.79
12	216.2		1	1		2	216	0	2.42	1	53.38
12	217.2		0	0		2	216	0	2.61	1	44.79
12	218.2		1	1		1	216	0	2.42	1	53.38
12	219.2		1	1		2	216	0	2.61	1	53.38
12	220.2		0	0		2	216	0	2.61	2	10.42
12	221.2		0	1		2	221	0	2.61	0	10.42
12	223.2		0	0		2	221	0	2.61	1	53.38
12	224.2		1	1		1	224	0	2.98	1	10.42
12	225.2		0	0		2	224	0	3.17	2	53.38
12	226.2		0	0		2	224	0	3.17	1	10.42
12	227.2		1	1		1	224	0	3.17	2	44.79
12	228.2		0	0		1	224	0	2.98	1	10.42
12	229.2		1	1		1	224	0	2.80	1	10.42
12	230.2		0	0		1	230	0	3.17	2	44.79
12	231.2		0	0		1	231	0	2.98	1	44.79
12	232.2		1	1		2	232	0	2.98	2	10.42
12	233.2		1	0		1	232	0	2.24	0	27.60
12	234.2		1	1		2	234	0	2.05	2	27.60
12	235.2		1	1		1	235	0	2.24	2	10.42
12	236.2		1	1		1	234	0	2.24	1	27.60
12	237.2		0	0		1	237	0	2.24	0	44.79
12	238.2		0	0		1	237	0	2.61	2	44.79
12	239.2		1	1		1	239	0	2.42	1	10.42
12	240.2		0	0		1	240	0	2.61	0	10.42
12	241.2		1	1		1	241	0	2.98	1	10.42
12	242.2		1	1		2	242	0	2.61	0	61.97
12	243.2		0	0		2	242	0	2.24	1	27.60
12	244.2		0	1		2	242	0	2.05	1	44.79
12	245.2		0	1		2	242	0	1.86	1	44.79
12	246.2		0	0		1	246	1	1.86	2	44.79
12	247.2		0	0		1	247	1	2.05	1	44.79
12	248.2		0	0		1	247	1	2.42	1	44.79
12	249.2		1	1		1	246	1	2.61	2	53.38

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	197.2	162.06	0.32	3.14	0.32	3.16	0			
12	198.2	252.32	0.31	3.18	0.31	3.18	1	0		3.16
12	199.2	250.15	0.31	3.19	0.31	3.18	0			
12	200.2	163.53	0.31	3.19	0.31	3.18	0			
12	201.2	268.77	0.32	3.09	0.31	3.18	0			
12	202.2	274.44	0.36	2.81	0.31	3.18	0			
12	204.2	163.16	0.35	2.84	0.35	2.84	1	1		3.18
12	205.2	166.90	0.34	2.92	0.35	2.84	0			
12	206.2	170.83	0.34	2.91	0.35	2.84	0			
12	207.2	169.40	0.34	2.91	0.34	2.91	1	0		2.84
12	208.2	172.77	0.34	2.94	0.34	2.91	0			
12	209.2	291.52	0.34	2.93	0.34	2.91	0			
12	210.2	293.46	0.35	2.85	0.34	2.91	0			
12	211.2	295.89	0.34	2.93	0.34	2.91	0			
12	212.2	290.19	0.34	2.95	0.34	2.91	0			
12	214.2	184.98	0.33	3.06	0.33	3.06	1	2		2.91
12	215.2	182.18	0.31	3.20	0.31	3.20	1	3		2.91
12	216.2	155.89	0.35	2.87	0.35	2.87	1	1		2.91
12	217.2	190.29	0.35	2.87	0.35	2.87	0			
12	218.2	161.83	0.34	2.90	0.35	2.87	0			
12	219.2	163.40	0.34	2.92	0.35	2.87	0			
12	220.2	363.30	0.34	2.91	0.35	2.87	0			
12	221.2	361.26	0.34	2.91	0.34	2.91	1	0		2.87
12	223.2	164.26	0.34	2.98	0.34	2.91	0			
12	224.2	368.07	0.34	2.94	0.34	2.94	1	4		2.91
12	225.2	165.03	0.34	2.92	0.34	2.94	0			
12	226.2	373.24	0.35	2.89	0.34	2.94	0			
12	227.2	199.70	0.35	2.86	0.34	2.94	0			
12	228.2	379.82	0.35	2.85	0.34	2.94	0			
12	229.2	382.09	0.35	2.84	0.34	2.94	0			
12	230.2	207.24	0.35	2.89	0.35	2.89	1	3		2.94
12	231.2	202.37	0.37	2.73	0.37	2.73	1	2		2.94
12	232.2	388.26	0.36	2.78	0.36	2.78	1	1		2.94
12	233.2	318.08	0.36	2.77	0.36	2.78	0			
12	234.2	322.12	0.36	2.76	0.36	2.76	1	0		2.78
12	235.2	399.44	0.37	2.73	0.37	2.73	1	2		2.76
12	236.2	320.65	0.36	2.75	0.36	2.76	0			
12	237.2	206.04	0.38	2.65	0.38	2.65	1	2		2.76
12	238.2	204.13	0.39	2.58	0.38	2.65	0			
12	239.2	398.53	0.35	2.87	0.35	2.87	1	3		2.76
12	240.2	400.74	0.36	2.76	0.36	2.76	1	3		2.76
12	241.2	404.64	0.38	2.64	0.38	2.64	1	1		2.76
12	242.2	171.50	0.39	2.58	0.39	2.58	1	0		2.64
12	243.2	331.90	0.40	2.52	0.39	2.58	0			
12	244.2	216.68	0.40	2.47	0.39	2.58	0			
12	245.2	218.58	0.40	2.47	0.39	2.58	0			
12	246.2	220.52	0.41	2.47	0.41	2.47	1	2		2.58
12	247.2	214.38	0.41	2.46	0.41	2.46	1	3		2.58
12	248.2	222.32	0.41	2.45	0.41	2.46	0			
12	249.2	195.40	0.41	2.44	0.41	2.47	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	250.2		0	0		1	247	1	2.42	1	53.38
12	251.2		0	1		2	251	0	2.61	0	44.79
12	252.2		1	1		.	252	0	1.68	1	36.19
12	253.2		1	1		1	252	0	1.86	2	36.19
12	254.2		1	1		1	252	0	1.68	1	44.79
12	255.2		0	0		2	252	0	1.68	2	44.79
12	256.2		0	1		2	252	0	1.86	0	44.79
12	257.2		0	0		2	257	0	1.86	1	44.79
12	258.2		0	1		1	257	0	1.86	0	44.79
12	259.2		0	0		1	259	0	1.86	0	44.79
12	260.2		0	1		1	259	0	1.86	0	53.38
12	261.2		1	1		1	259	0	2.05	1	53.38
12	262.2		1	1		2	259	0	2.24	2	61.97
12	263.2		0	0		.	263	0	2.05	0	44.79
12	264.2		0	1		2	263	0	2.05	1	44.79
12	265.2		1	1		2	265	0	2.24	1	1.83
12	266.2		1	1		.	266	0	1.86	2	44.79
12	267.2		1	1		1	266	0	1.86	1	61.97
12	268.2		0	1		1	268	0	2.05	2	27.60
12	269.2		1	0		1	268	0	1.86	1	44.79
12	270.2		1	1		.	270	0	2.05	2	53.38
12	271.2		1	1		1	270	0	1.86	2	53.38
12	272.2		0	0		1	272	0	1.49	2	44.79
12	273.2		1	1		.	273	0	1.49	1	44.79
12	274.2		0	1		1	274	0	1.86	1	44.79
12	275.2		0	0		2	274	0	1.86	1	44.79
12	276.2		0	0		2	276	0	2.05	0	44.79
12	277.2		1	1		.	277	0	1.86	0	19.01
12	278.2		0	0		2	278	0	1.86	1	44.79
12	280.2		0	1		.	280	0	0.37	1	44.79
12	281.2		0	1		2	282	0	0.75	0	19.01
12	282.2		1	1		.	282	0	0.37	1	19.01
12	285.2		0	0		.	285	0	0.56	0	53.38
12	287.2		0	1		.	287	0	1.31	0	19.01
12	288.2		0	1		.	288	0	0.56	2	19.01
12	289.2		0	0		2	282	0	1.12	0	44.79
12	294.2		0	0		.	294	0	0.37	2	61.97
12	300.2		1	1		2	300	0	0.93	0	19.01
12	301.2		0	1		2	301	0	1.49	1	27.60
12	310.2		1	1		.	310	0	0.56	1	1.83
12	28.3		0	1		.	28	0	0.56	2	1.83
12	37.3		0	0		2	301	0	1.68	1	19.01
12	38.3		0	0		2	301	0	1.86	1	19.01
12	68.3		0	0		.	68	0	0.93	0	27.60
12	69.3		0	1		.	69	0	0.93	1	10.42
12	77.3		1	1		.	77	0	1.12	1	19.01
12	79.3		1	1		2	79	0	1.49	1	10.42
12	84.3		1	1		.	84	0	0.37	1	36.19
12	85.3		0	0		.	85	0	0.75	0	36.19
12	88.3		0	1		.	88	0	0.93	0	36.19

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	250.2	196.70	0.41	2.42	0.41	2.46	0			
12	251.2	227.56	0.41	2.43	0.41	2.43	1	0		2.58
12	252.2	228.59	0.40	2.47	0.40	2.47	1	0		2.43
12	253.2	229.99	0.40	2.49	0.40	2.47	0			
12	254.2	229.69	0.40	2.48	0.40	2.47	0			
12	255.2	266.33	0.40	2.47	0.40	2.47	0			
12	256.2	276.71	0.41	2.46	0.40	2.47	0			
12	257.2	259.16	0.41	2.47	0.41	2.47	1	1		2.47
12	258.2	301.36	0.42	2.40	0.41	2.47	0			
12	259.2	304.03	0.42	2.40	0.42	2.40	1	0		2.47
12	260.2	209.14	0.42	2.37	0.42	2.40	0			
12	261.2	216.52	0.45	2.22	0.42	2.40	0			
12	262.2	223.02	0.47	2.15	0.42	2.40	0			
12	263.2	317.71	0.48	2.08	0.48	2.08	1	0		2.40
12	264.2	321.32	0.48	2.06	0.48	2.08	0			
12	265.2	457.03	0.48	2.08	0.48	2.08	1	2		2.08
12	266.2	326.62	0.46	2.17	0.46	2.17	1	3		2.08
12	267.2	227.23	0.46	2.16	0.46	2.17	0			
12	268.2	406.41	0.48	2.10	0.48	2.10	1	1		2.08
12	269.2	331.43	0.46	2.15	0.48	2.10	0			
12	270.2	237.24	0.47	2.14	0.47	2.14	1	0		2.10
12	271.2	233.60	0.47	2.11	0.47	2.14	0			
12	272.2	345.78	0.52	1.93	0.52	1.93	1	2		2.14
12	273.2	341.54	0.47	2.13	0.47	2.13	1	3		2.14
12	274.2	344.24	0.47	2.12	0.47	2.12	1	0		2.14
12	275.2	346.94	0.48	2.10	0.47	2.12	0			
12	276.2	426.76	0.47	2.11	0.47	2.11	1	0		2.12
12	277.2	442.54	0.50	2.00	0.50	2.00	1	0		2.11
12	278.2	445.84	0.54	1.84	0.54	1.84	1	2		2.00
12	280.2	551.95	0.72	1.39	0.72	1.39	1	0		2.00
12	281.2	583.95	0.59	1.69	0.59	1.68	0			
12	282.2	582.78	0.59	1.68	0.59	1.68	1	0		1.39
12	285.2	608.31	1.00	1.00	1.00	1.00	1	0		1.68
12	287.2	445.14	0.17	5.72	0.17	5.72	1	3		2.00
12	288.2	431.53	0.24	4.24	0.24	4.24	1	3		2.00
12	289.2	576.61	0.60	1.68	0.59	1.68	0			
12	294.2	830.40	1.28	0.78	1.28	0.78	1	0		1.00
12	300.2	53.15	0.78	1.28	0.78	1.28	1	1		1.34
12	301.2	58.16	0.76	1.32	0.76	1.32	1	1		1.28
12	310.2	518.45	0.62	1.61	0.62	1.61	1	2		2.00
12	28.3	38.10	1.32	0.75	1.32	0.75	1	0		.
12	37.3	41.97	0.90	1.11	0.91	1.10	0			
12	38.3	46.14	0.91	1.10	0.91	1.10	0			
12	68.3	67.70	0.76	1.32	0.76	1.32	1	0		1.57
12	69.3	77.81	0.64	1.57	0.64	1.57	1	0		0.95
12	77.3	75.64	0.70	1.43	0.70	1.43	1	0		1.32
12	79.3	94.33	0.69	1.45	0.69	1.45	1	1		1.43
12	84.3	54.82	0.85	1.18	0.85	1.18	1	0		1.26
12	85.3	55.96	0.97	1.03	0.97	1.03	1	0		1.18
12	88.3	61.83	0.87	1.15	0.87	1.15	1	0		1.03

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	89.3		1	1		2	88	0	1.12	0	10.42
12	90.3		1	1		.	90	0	1.12	1	10.42
12	91.3		1	1		2	90	0	1.31	1	10.42
12	95.3		0	0		2	90	0	1.49	1	10.42
12	96.3		1	1		.	96	0	1.49	0	10.42
12	97.3		1	1		.	97	0	0.93	2	27.60
12	103.3		0	0		2	103	0	0.93	1	10.42
12	108.3		1	1		.	108	0	1.12	1	19.01
12	109.3		1	1		2	109	0	1.12	0	19.01
12	114.3		1	1		2	114	0	1.31	1	27.60
12	115.3		1	1		1	114	0	1.49	2	27.60
12	120.3		0	0		1	120	0	2.05	2	27.60
12	121.3		0	0		1	120	0	2.42	2	27.60
12	122.3		0	1		1	120	0	1.86	1	1.83
12	130.3		1	1		2	131	0	2.98	1	1.83
12	131.3		0	0		2	131	0	2.80	1	1.83
12	132.3		0	0		1	131	0	2.80	1	19.01
12	133.3		0	0		1	131	0	2.98	2	19.01
12	135.3		1	1		2	135	0	3.36	1	1.83
12	137.3		1	1		1	139	0	3.36	1	19.01
12	138.3		0	0		2	138	0	2.80	2	27.60
12	139.3		1	1		1	139	0	3.36	1	19.01
12	140.3		0	0		1	138	0	3.17	1	19.01
12	141.3		1	1		2	141	0	2.80	1	19.01
12	142.3		1	1		1	141	0	2.80	0	19.01
12	143.3		1	1		1	138	0	2.98	1	19.01
12	144.3		1	1		2	138	0	2.98	2	19.01
12	145.3		0	0		2	145	0	2.80	1	19.01
12	146.3		1	1		2	146	0	2.61	2	19.01
12	147.3		1	1		.	147	0	2.61	0	19.01
12	148.3		1	1		2	148	0	2.42	1	10.42
12	149.3		1	0		2	147	0	2.42	1	10.42
12	150.3		1	1		2	147	0	2.42	1	10.42
12	152.3		1	1		2	152	0	2.42	1	10.42
12	153.3		1	1		1	153	0	2.42	1	10.42
12	155.3		1	1		1	153	0	2.42	0	10.42
12	157.3		1	1		1	153	0	2.80	0	10.42
12	160.3		1	1		1	160	0	2.80	1	36.19
12	161.3		1	1		1	160	0	2.61	2	36.19
12	162.3		1	1		1	162	0	2.61	0	10.42
12	170.3		1	1		1	171	0	2.61	2	10.42
12	171.3		1	1		1	171	0	2.24	1	10.42
12	172.3		1	1		1	171	0	2.61	0	36.19
12	173.3		1	1		1	171	0	2.61	2	36.19
12	174.3		0	0		1	171	0	2.61	1	10.42
12	175.3		0	0		2	175	0	2.42	2	19.01
12	176.3		1	1		2	183	0	2.61	0	19.01
12	177.3		1	1		1	177	0	2.42	0	36.19
12	178.3		1	1		1	178	0	2.24	1	10.42
12	179.3		0	1		1	178	0	2.24	1	1.83

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	89.3	113.55	0.88	1.14	0.87	1.15	0			
12	90.3	115.71	0.87	1.14	0.87	1.14	1	0		1.15
12	91.3	117.65	0.86	1.16	0.87	1.14	0			
12	95.3	119.69	0.86	1.16	0.87	1.14	0			
12	96.3	121.65	0.84	1.19	0.84	1.19	1	0		1.14
12	97.3	91.49	0.70	1.42	0.70	1.42	1	0		1.19
12	103.3	125.62	0.70	1.44	0.70	1.44	1	0		1.42
12	108.3	92.72	0.65	1.54	0.65	1.54	1	0		1.44
12	109.3	94.02	0.66	1.51	0.66	1.51	1	0		1.54
12	114.3	93.62	0.56	1.78	0.56	1.78	1	1		1.51
12	115.3	95.43	0.55	1.81	0.56	1.78	0			
12	120.3	97.63	0.53	1.88	0.53	1.88	1	4		1.78
12	121.3	99.10	0.53	1.87	0.53	1.88	0			
12	122.3	134.90	0.50	1.99	0.53	1.88	0			
12	130.3	138.74	0.38	2.62	0.37	2.70	0			
12	131.3	136.64	0.37	2.70	0.37	2.70	1	1		1.88
12	132.3	95.59	0.39	2.59	0.37	2.70	0			
12	133.3	97.33	0.37	2.70	0.37	2.70	0			
12	135.3	143.31	0.36	2.80	0.36	2.80	1	2		2.70
12	137.3	102.07	0.35	2.89	0.35	2.85	0			
12	138.3	101.57	0.34	2.91	0.34	2.91	1	1		2.70
12	139.3	99.46	0.35	2.85	0.35	2.85	1	3		2.70
12	140.3	104.50	0.34	2.97	0.34	2.91	0			
12	141.3	123.32	0.32	3.16	0.32	3.16	1	0		3.12
12	142.3	119.62	0.31	3.21	0.32	3.16	0			
12	143.3	105.67	0.33	3.05	0.34	2.91	0			
12	144.3	108.14	0.32	3.10	0.34	2.91	0			
12	145.3	110.81	0.32	3.12	0.32	3.12	1	0		2.91
12	146.3	123.19	0.29	3.41	0.29	3.41	1	0		3.16
12	147.3	124.52	0.29	3.42	0.29	3.42	1	0		3.41
12	148.3	168.47	0.26	3.81	0.26	3.81	1	2		3.42
12	149.3	162.83	0.27	3.77	0.29	3.42	0			
12	150.3	164.86	0.26	3.82	0.29	3.42	0			
12	152.3	166.83	0.26	3.77	0.26	3.77	1	3		3.42
12	153.3	170.54	0.27	3.77	0.27	3.77	1	1		3.42
12	155.3	172.10	0.26	3.78	0.27	3.77	0			
12	157.3	173.74	0.26	3.88	0.27	3.77	0			
12	160.3	91.72	0.23	4.42	0.23	4.42	1	4		3.77
12	161.3	97.90	0.23	4.43	0.23	4.42	0			
12	162.3	178.34	0.22	4.47	0.22	4.47	1	4		4.42
12	170.3	182.51	0.20	5.01	0.20	5.05	0			
12	171.3	181.78	0.20	5.05	0.20	5.05	1	4		4.47
12	172.3	96.00	0.20	5.00	0.20	5.05	0			
12	173.3	98.83	0.20	4.98	0.20	5.05	0			
12	174.3	189.09	0.20	4.99	0.20	5.05	0			
12	175.3	130.93	0.19	5.22	0.19	5.22	1	3		5.05
12	176.3	145.74	0.23	4.26	0.22	4.60	0			
12	177.3	109.38	0.20	4.97	0.20	4.97	1	2		5.05
12	178.3	192.46	0.19	5.35	0.19	5.35	1	3		5.05
12	179.3	193.19	0.19	5.14	0.19	5.35	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	181.3		1	1		1	181	0	2.42	1	10.42
12	182.3		1	1		1	181	0	2.61	1	10.42
12	183.3		0	1		2	183	0	2.61	2	36.19
12	184.3		0	1		1	184	0	2.98	1	1.83
12	185.3		0	0		1	185	0	3.17	2	1.83
12	188.3		1	1		2	188	0	2.80	1	19.01
12	190.3		0	1		1	190	0	3.17	0	27.60
12	191.3		0	0		1	188	0	2.80	0	27.60
12	192.3		0	1		1	192	0	3.17	0	27.60
12	193.3		0	1		1	193	0	2.80	2	19.01
12	194.3		1	1		1	184	0	2.98	0	19.01
12	195.3		0	0		1	184	0	3.36	1	1.83
12	196.3		0	0		1	184	0	2.61	1	1.83
12	197.3		1	1		2	197	0	2.98	1	19.01
12	198.3		0	1		1	198	0	2.80	2	1.83
12	199.3		0	0		1	198	0	2.61	0	1.83
12	200.3		1	1		1	200	0	2.61	2	19.01
12	201.3		1	0		2	201	0	2.61	1	1.83
12	202.3		1	1		1	201	0	2.80	1	1.83
12	204.3		1	1		.	204	0	2.61	0	27.60
12	205.3		0	0		1	204	0	2.05	1	27.60
12	206.3		1	1		2	206	0	2.05	1	27.60
12	207.3		1	1		1	206	0	2.24	2	27.60
12	208.3		1	1		1	206	0	2.42	1	27.60
12	209.3		1	1		1	209	0	2.61	1	10.42
12	210.3		1	0		1	209	0	2.80	2	10.42
12	211.3		0	0		1	209	0	2.98	0	10.42
12	212.3		1	1		1	212	0	2.98	1	1.83
12	214.3		1	1		1	215	0	2.98	1	27.60
12	215.3		1	1		2	215	0	3.17	0	27.60
12	216.3		1	1		1	215	0	2.80	1	36.19
12	217.3		0	0		2	215	0	2.61	1	27.60
12	218.3		1	1		1	215	0	2.61	0	36.19
12	219.3		1	1		2	215	0	2.42	1	36.19
12	223.3		0	0		2	223	0	2.42	1	36.19
12	225.3		0	0		1	225	0	2.98	2	36.19
12	227.3		1	1		1	227	0	2.98	2	27.60
12	230.3		0	0		1	230	0	2.80	0	27.60
12	231.3		0	0		1	230	0	2.80	2	27.60
12	233.3		1	0		1	233	0	2.42	1	10.42
12	234.3		1	1		1	234	0	2.42	2	10.42
12	236.3		1	1		2	234	0	2.42	0	10.42
12	237.3		0	0		1	237	0	2.61	2	27.60
12	238.3		0	0		1	237	0	2.80	1	27.60
12	242.3		1	1		1	242	0	2.80	0	44.79
12	243.3		0	0		1	242	0	2.61	1	10.42
12	244.3		0	1		1	242	0	2.61	0	27.60
12	245.3		0	1		1	245	0	2.24	0	27.60
12	246.3		0	0		1	246	0	2.42	2	27.60
12	247.3		0	0		1	246	0	2.42	1	27.60

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	181.3	195.36	0.21	4.69	0.21	4.69	1	2		5.05
12	182.3	197.20	0.22	4.58	0.21	4.69	0			
12	183.3	110.38	0.22	4.60	0.22	4.60	1	1		5.05
12	184.3	206.81	0.22	4.46	0.22	4.46	1	2		4.60
12	185.3	214.55	0.23	4.39	0.23	4.39	1	2		4.60
12	188.3	146.18	0.23	4.36	0.23	4.36	1	3		4.60
12	190.3	148.14	0.23	4.38	0.23	4.38	1	3		4.60
12	191.3	146.71	0.23	4.41	0.23	4.36	0			
12	192.3	149.91	0.23	4.33	0.23	4.33	1	1		4.60
12	193.3	150.08	0.25	3.97	0.25	3.97	1	2		4.33
12	194.3	151.78	0.23	4.34	0.22	4.46	0			
12	195.3	220.22	0.22	4.45	0.22	4.46	0			
12	196.3	232.16	0.26	3.83	0.22	4.46	0			
12	197.3	162.06	0.37	2.69	0.37	2.69	1	1		4.33
12	198.3	252.32	0.38	2.61	0.38	2.61	1	2		2.69
12	199.3	250.15	0.38	2.67	0.38	2.61	0			
12	200.3	163.53	0.38	2.66	0.38	2.66	1	3		2.69
12	201.3	268.77	0.36	2.78	0.36	2.78	1	2		2.69
12	202.3	274.44	0.33	3.01	0.36	2.78	0			
12	204.3	163.16	0.33	3.00	0.33	3.00	1	3		2.69
12	205.3	166.90	0.33	2.99	0.33	3.00	0			
12	206.3	170.83	0.34	2.90	0.34	2.90	1	1		2.69
12	207.3	169.40	0.34	2.91	0.34	2.90	0			
12	208.3	172.77	0.35	2.90	0.34	2.90	0			
12	209.3	291.52	0.35	2.89	0.35	2.89	1	1		2.90
12	210.3	293.46	0.33	3.00	0.35	2.89	0			
12	211.3	295.89	0.34	2.91	0.35	2.89	0			
12	212.3	290.19	0.34	2.92	0.34	2.92	1	3		2.89
12	214.3	184.98	0.35	2.85	0.34	2.93	0			
12	215.3	182.18	0.34	2.93	0.34	2.93	1	1		2.89
12	216.3	155.89	0.31	3.18	0.34	2.93	0			
12	217.3	190.29	0.31	3.28	0.34	2.93	0			
12	218.3	161.83	0.31	3.27	0.34	2.93	0			
12	219.3	163.40	0.30	3.29	0.34	2.93	0			
12	223.3	164.26	0.29	3.50	0.29	3.50	1	4		2.93
12	225.3	165.03	0.28	3.60	0.28	3.60	1	4		3.50
12	227.3	199.70	0.27	3.73	0.27	3.73	1	4		3.60
12	230.3	207.24	0.26	3.91	0.26	3.91	1	4		3.73
12	231.3	202.37	0.25	3.96	0.26	3.91	0			
12	233.3	318.08	0.25	4.06	0.25	4.06	1	4		3.91
12	234.3	322.12	0.24	4.08	0.24	4.08	1	1		4.06
12	236.3	320.65	0.24	4.11	0.24	4.08	0			
12	237.3	206.04	0.24	4.22	0.24	4.22	1	4		4.08
12	238.3	204.13	0.23	4.30	0.24	4.22	0			
12	242.3	171.50	0.22	4.47	0.22	4.47	1	4		4.22
12	243.3	331.90	0.23	4.43	0.22	4.47	0			
12	244.3	216.68	0.21	4.70	0.22	4.47	0			
12	245.3	218.58	0.25	4.00	0.25	4.00	1	2		4.47
12	246.3	220.52	0.22	4.61	0.22	4.61	1	3		4.47
12	247.3	214.38	0.22	4.59	0.22	4.61	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	248.3		0	0		1	248	0	2.61	1	27.60
12	249.3		1	1		1	248	0	2.98	2	36.19
12	250.3		0	0		1	248	0	2.61	1	36.19
12	251.3		0	1		2	251	0	2.80	2	27.60
12	252.3		1	1		2	251	0	2.24	1	19.01
12	253.3		1	1		1	251	0	2.24	2	19.01
12	254.3		1	1		1	251	0	2.42	1	27.60
12	255.3		0	0		1	251	0	2.61	2	27.60
12	256.3		0	1		2	256	0	1.86	0	27.60
12	257.3		0	0		.	257	0	2.05	1	27.60
12	258.3		0	1		1	257	0	2.24	2	27.60
12	259.3		0	0		1	257	0	2.42	1	27.60
12	260.3		0	1		1	257	0	2.05	0	36.19
12	261.3		1	1		1	257	0	2.24	1	36.19
12	262.3		1	1		2	257	0	2.24	2	44.79
12	263.3		0	0		.	263	0	2.24	0	27.60
12	264.3		0	1		2	264	0	2.42	1	27.60
12	266.3		1	1		.	266	0	2.61	2	27.60
12	267.3		1	1		1	267	0	2.42	1	44.79
12	268.3		0	1		1	268	0	2.80	0	10.42
12	269.3		1	0		2	268	0	2.42	1	27.60
12	270.3		1	1		.	270	0	2.42	2	36.19
12	271.3		1	1		1	270	0	2.42	2	36.19
12	272.3		0	0		.	273	0	2.05	2	27.60
12	273.3		1	1		.	273	0	2.05	1	27.60
12	274.3		0	1		.	274	0	2.05	1	27.60
12	275.3		0	0		1	274	0	2.05	1	27.60
12	276.3		0	0		.	276	0	1.49	2	27.60
12	277.3		1	1		.	277	0	1.68	1	1.83
12	278.3		0	0		.	278	0	1.12	0	27.60
12	280.3		0	1		.	280	0	0.37	0	27.60
12	281.3		0	1		1	282	0	0.75	0	1.83
12	282.3		1	1		.	282	0	0.37	1	1.83
12	285.3		0	0		.	285	0	0.37	1	36.19
12	287.3		0	1		.	287	0	1.68	0	1.83
12	288.3		0	1		.	288	0	0.93	2	1.83
12	289.3		0	0		.	289	0	0.75	0	27.60
12	294.3		0	0		.	294	0	0.37	2	44.79
12	295.3		0	0		.	295	0	0.37	0	27.60
12	300.3		1	1		.	300	0	0.75	1	1.83
12	301.3		0	1		2	301	0	1.49	1	10.42
12	302.3		0	0		.	302	0	0.37	2	10.42
12	303.3		1	0		.	303	0	1.12	0	10.42
12	304.3		1	0		2	303	0	1.31	1	10.42
12	305.3		0	1		.	305	0	0.56	1	10.42
12	306.3		1	0		2	306	0	1.86	1	1.83
12	307.3		1	1		2	306	0	1.86	1	1.83
12	309.3		1	1		1	309	0	2.98	2	1.83
12	37.4		0	0		.	37	0	0.93	1	1.83
12	38.4		0	0		2	38	0	1.12	1	1.83

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	248.3	222.32	0.25	4.07	0.25	4.07	1	1		4.47
12	249.3	195.40	0.28	3.58	0.25	4.07	0			
12	250.3	196.70	0.27	3.73	0.25	4.07	0			
12	251.3	227.56	0.28	3.58	0.28	3.58	1	1		4.07
12	252.3	228.59	0.34	2.98	0.28	3.58	0			
12	253.3	229.99	0.34	2.98	0.28	3.58	0			
12	254.3	229.69	0.33	2.99	0.28	3.58	0			
12	255.3	266.33	0.33	3.01	0.28	3.58	0			
12	256.3	276.71	0.34	2.97	0.34	2.97	1	1		3.58
12	257.3	259.16	0.34	2.90	0.34	2.90	1	0		2.97
12	258.3	301.36	0.38	2.63	0.34	2.90	0			
12	259.3	304.03	0.39	2.59	0.34	2.90	0			
12	260.3	209.14	0.38	2.63	0.34	2.90	0			
12	261.3	216.52	0.36	2.77	0.34	2.90	0			
12	262.3	223.02	0.35	2.83	0.34	2.90	0			
12	263.3	317.71	0.35	2.87	0.35	2.87	1	0		2.90
12	264.3	321.32	0.36	2.81	0.36	2.81	1	0		2.87
12	266.3	326.62	0.35	2.87	0.35	2.87	1	2		2.81
12	267.3	227.23	0.34	2.96	0.35	2.87	1	3		2.81
12	268.3	406.41	0.34	2.98	0.34	2.98	1	4		2.81
12	269.3	331.43	0.34	2.94	0.34	2.98	0			
12	270.3	237.24	0.34	2.93	0.34	2.93	1	0		2.98
12	271.3	233.60	0.34	2.94	0.34	2.93	0			
12	272.3	345.78	0.33	3.04	0.33	3.00	0			
12	273.3	341.54	0.33	3.00	0.33	3.00	1	0		2.93
12	274.3	344.24	0.33	3.00	0.33	3.00	1	1		3.00
12	275.3	346.94	0.33	3.00	0.33	3.00	0			
12	276.3	426.76	0.43	2.31	0.43	2.31	1	1		3.00
12	277.3	442.54	0.41	2.43	0.41	2.43	1	0		2.31
12	278.3	445.84	0.50	2.01	0.50	2.01	1	1		2.48
12	280.3	551.95	0.93	1.08	0.93	1.08	1	0		2.01
12	281.3	583.95	0.47	2.13	0.48	2.10	0			
12	282.3	582.78	0.48	2.10	0.48	2.10	1	0		1.08
12	285.3	608.31	1.02	0.98	1.02	0.98	1	0		1.97
12	287.3	445.14	0.40	2.48	0.40	2.48	1	0		2.43
12	288.3	431.53	0.20	5.04	0.20	5.04	1	3		2.01
12	289.3	576.61	0.51	1.97	0.51	1.97	1	1		2.10
12	294.3	830.40	1.30	0.77	1.30	0.77	1	0		0.98
12	295.3	1013.44	1.21	0.83	1.21	0.83	1	0		0.77
12	300.3	53.15	0.77	1.29	0.77	1.29	1	1		1.06
12	301.3	58.16	0.91	1.10	0.91	1.10	1	0		1.06
12	302.3	52.58	0.95	1.06	0.95	1.06	1	0		0.75
12	303.3	55.25	0.94	1.06	0.94	1.06	1	0		1.29
12	304.3	56.66	0.94	1.06	0.94	1.06	0			
12	305.3	75.24	1.05	0.95	1.05	0.95	1	0		1.10
12	306.3	94.53	0.80	1.26	0.80	1.26	1	4		1.45
12	307.3	95.83	0.79	1.26	0.80	1.26	0			
12	309.3	197.63	0.26	3.90	0.26	3.90	1	2		5.05
12	37.4	41.97	1.10	0.91	1.10	0.91	1	1		.
12	38.4	46.14	1.12	0.89	1.12	0.89	1	1		0.91

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	68.4		0	0		.	68	0	0.37	0	10.42
12	77.4		1	1		.	77	0	0.37	0	1.83
12	84.4		1	1		.	84	0	0.37	1	19.01
12	85.4		0	0		.	85	0	0.75	2	19.01
12	88.4		0	1		.	88	0	0.93	2	19.01
12	97.4		1	1		.	97	0	1.12	0	10.42
12	108.4		1	1		.	108	0	0.93	1	1.83
12	109.4		1	1		2	109	0	1.31	1	1.83
12	114.4		1	1		2	109	0	1.12	1	10.42
12	115.4		1	1		1	109	0	1.68	2	10.42
12	120.4		0	0		2	120	0	2.61	2	10.42
12	121.4		0	0		1	120	0	2.80	2	10.42
12	132.4		0	0		1	132	0	2.61	1	1.83
12	133.4		0	0		1	133	0	2.98	0	1.83
12	137.4		1	1		1	139	0	3.36	1	1.83
12	138.4		0	0		1	138	0	3.17	2	10.42
12	139.4		1	1		1	139	0	3.36	1	1.83
12	140.4		0	0		1	138	0	3.36	1	1.83
12	141.4		1	1		.	141	0	2.24	0	1.83
12	142.4		1	1		1	142	0	1.68	0	1.83
12	143.4		1	1		1	138	0	3.17	1	1.83
12	144.4		1	1		2	138	0	2.98	2	1.83
12	145.4		0	0		.	145	0	2.42	0	1.83
12	146.4		1	1		.	146	0	2.05	2	1.83
12	147.4		1	1		2	147	0	2.24	2	1.83
12	160.4		1	1		.	160	0	1.68	0	19.01
12	161.4		1	1		2	160	0	1.86	2	19.01
12	172.4		1	1		1	172	0	2.24	0	19.01
12	173.4		1	1		.	173	0	1.86	0	19.01
12	175.4		0	0		2	175	0	2.05	2	1.83
12	176.4		1	1		.	176	0	1.68	1	1.83
12	177.4		1	1		.	177	0	2.05	2	19.01
12	183.4		0	1		2	183	0	2.24	1	19.01
12	188.4		1	1		1	176	0	1.86	1	1.83
12	190.4		0	1		1	190	0	2.61	2	10.42
12	191.4		0	0		.	191	0	2.24	1	10.42
12	192.4		0	1		1	192	0	2.80	2	10.42
12	193.4		0	1		2	193	0	2.61	0	1.83
12	194.4		1	1		1	194	0	2.61	0	1.83
12	197.4		1	1		.	197	0	2.05	1	1.83
12	200.4		1	1		1	200	0	2.05	2	1.83
12	204.4		1	1		.	204	0	2.24	2	10.42
12	205.4		0	0		.	205	0	2.05	1	10.42
12	206.4		1	1		1	206	0	2.24	1	10.42
12	207.4		1	1		1	206	0	2.05	2	10.42
12	208.4		1	1		1	206	0	2.61	1	10.42
12	214.4		1	1		1	215	0	2.61	2	10.42
12	215.4		1	1		2	215	0	2.80	1	10.42
12	216.4		1	1		1	215	0	2.61	1	19.01
12	217.4		0	0		2	215	0	2.42	0	10.42

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	68.4	67.70	1.02	0.98	1.02	0.98	1	0		0.89
12	77.4	75.64	1.04	0.96	1.04	0.96	1	0		0.98
12	84.4	54.82	0.83	1.21	0.83	1.21	1	0		0.96
12	85.4	55.96	0.75	1.33	0.75	1.33	1	0		1.21
12	88.4	61.83	0.71	1.41	0.71	1.41	1	0		1.33
12	97.4	91.49	0.57	1.75	0.57	1.75	1	0		1.41
12	108.4	92.72	0.49	2.02	0.49	2.02	1	0		1.75
12	109.4	94.02	0.49	2.04	0.49	2.04	1	1		2.02
12	114.4	93.62	0.49	2.05	0.49	2.04	0			
12	115.4	95.43	0.49	2.02	0.49	2.04	0			
12	120.4	97.63	0.51	1.98	0.51	1.98	1	2		2.04
12	121.4	99.10	0.51	1.95	0.51	1.98	0			
12	132.4	95.59	0.41	2.46	0.41	2.46	1	3		2.04
12	133.4	97.33	0.44	2.30	0.44	2.30	1	3		2.04
12	137.4	102.07	0.41	2.44	0.41	2.44	0			
12	138.4	101.57	0.42	2.40	0.42	2.40	1	4		2.44
12	139.4	99.46	0.41	2.44	0.41	2.44	1	1		2.04
12	140.4	104.50	0.42	2.40	0.42	2.40	0			
12	141.4	123.32	0.47	2.14	0.47	2.14	1	2		2.20
12	142.4	119.62	0.46	2.16	0.46	2.16	1	3		2.20
12	143.4	105.67	0.42	2.40	0.42	2.40	0			
12	144.4	108.14	0.42	2.38	0.42	2.40	0			
12	145.4	110.81	0.45	2.20	0.45	2.20	1	1		2.40
12	146.4	123.19	0.47	2.11	0.47	2.11	1	3		2.20
12	147.4	124.52	0.47	2.15	0.47	2.15	1	2		2.20
12	160.4	91.72	0.33	3.00	0.33	3.00	1	3		2.20
12	161.4	97.90	0.33	3.02	0.33	3.00	0			
12	172.4	96.00	0.30	3.28	0.30	3.28	1	1		2.20
12	173.4	98.83	0.30	3.30	0.30	3.30	1	1		3.28
12	175.4	130.93	0.30	3.35	0.30	3.35	1	4		3.30
12	176.4	145.74	0.24	4.19	0.24	4.19	1	1		4.45
12	177.4	109.38	0.28	3.61	0.28	3.61	1	1		3.35
12	183.4	110.38	0.22	4.45	0.22	4.45	1	1		3.61
12	188.4	146.18	0.22	4.47	0.24	4.19	0			
12	190.4	148.14	0.23	4.44	0.23	4.44	1	4		4.47
12	191.4	146.71	0.22	4.47	0.22	4.47	1	1		4.19
12	192.4	149.91	0.22	4.51	0.22	4.51	1	1		4.44
12	193.4	150.08	0.22	4.64	0.22	4.64	1	3		4.51
12	194.4	151.78	0.23	4.38	0.23	4.38	1	2		4.51
12	197.4	162.06	0.18	5.56	0.18	5.56	1	1		4.51
12	200.4	163.53	0.17	5.75	0.17	5.75	1	1		5.56
12	204.4	163.16	0.17	5.92	0.17	5.92	1	4		5.75
12	205.4	166.90	0.17	5.91	0.17	5.92	1	1		5.92
12	206.4	170.83	0.17	5.98	0.17	5.98	1	1		5.91
12	207.4	169.40	0.17	5.89	0.17	5.98	0			
12	208.4	172.77	0.17	6.05	0.17	5.98	0			
12	214.4	184.98	0.16	6.32	0.16	6.24	0			
12	215.4	182.18	0.16	6.24	0.16	6.24	1	1		5.98
12	216.4	155.89	0.16	6.34	0.16	6.24	0			
12	217.4	190.29	0.16	6.36	0.16	6.24	0			

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	218.4		1	1		1	215	0	2.61	1	19.01
12	219.4		1	1		2	215	0	2.42	1	19.01
12	223.4		0	0		2	215	0	2.42	1	19.01
12	225.4		0	0		1	215	0	2.61	2	19.01
12	227.4		1	1		1	215	0	2.42	1	10.42
12	230.4		0	0		1	230	0	2.42	1	10.42
12	231.4		0	0		1	231	0	2.24	0	10.42
12	237.4		0	0		1	238	0	2.24	2	10.42
12	238.4		0	0		1	238	0	2.24	0	10.42
12	242.4		1	1		1	242	0	2.42	0	27.60
12	244.4		0	1		1	244	0	2.42	0	10.42
12	245.4		0	1		1	245	0	2.24	0	10.42
12	246.4		0	0		1	246	0	2.42	2	10.42
12	247.4		0	0		1	247	0	2.42	1	10.42
12	248.4		0	0		1	248	0	2.42	1	10.42
12	249.4		1	1		1	248	0	2.80	0	19.01
12	250.4		0	0		1	248	0	2.80	0	19.01
12	251.4		0	1		2	251	0	2.98	2	10.42
12	252.4		1	1		2	251	0	3.17	1	1.83
12	253.4		1	1		1	253	1	3.54	2	1.83
12	254.4		1	1		1	254	1	3.54	1	10.42
12	255.4		0	0		1	253	1	3.17	2	10.42
12	256.4		0	1		2	253	1	2.24	2	10.42
12	257.4		0	0		2	254	1	2.61	1	10.42
12	258.4		0	1		2	258	0	2.80	0	10.42
12	259.4		0	0		1	258	0	2.98	2	10.42
12	260.4		0	1		1	258	0	2.24	1	19.01
12	261.4		1	1		2	258	0	2.24	1	19.01
12	262.4		1	1		1	262	0	2.42	2	27.60
12	263.4		0	0		.	263	0	2.24	1	10.42
12	264.4		0	1		2	263	0	2.61	1	10.42
12	266.4		1	1		1	263	0	2.80	0	10.42
12	267.4		1	1		1	263	0	2.61	2	27.60
12	269.4		1	0		2	269	0	2.61	1	10.42
12	270.4		1	1		.	270	0	2.61	2	19.01
12	271.4		1	1		1	270	0	2.42	0	19.01
12	272.4		0	0		.	272	0	2.05	2	10.42
12	273.4		1	1		.	273	0	2.05	1	10.42
12	274.4		0	1		.	274	0	1.86	1	10.42
12	275.4		0	0		1	275	0	2.05	0	10.42
12	276.4		0	0		.	276	0	0.56	0	10.42
12	278.4		0	0		.	278	0	0.37	2	10.42
12	280.4		0	1		.	280	0	0.37	2	10.42
12	285.4		0	0		.	285	0	0.37	0	19.01
12	289.4		0	0		.	289	0	0.37	2	10.42
12	294.4		0	0		.	294	0	0.37	2	27.60
12	295.4		0	0		.	295	0	0.37	1	10.42
12	84.5		1	1		.	84	0	0.37	1	1.83
12	85.5		0	0		2	84	0	0.75	2	1.83
12	88.5		0	1		.	88	0	0.75	0	1.83

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	218.4	161.83	0.16	6.37	0.16	6.24	0			
12	219.4	163.40	0.16	6.36	0.16	6.24	0			
12	223.4	164.26	0.16	6.37	0.16	6.24	0			
12	225.4	165.03	0.16	6.42	0.16	6.24	0			
12	227.4	199.70	0.16	6.33	0.16	6.24	0			
12	230.4	207.24	0.16	6.07	0.16	6.07	1	2		6.24
12	231.4	202.37	0.16	6.36	0.16	6.36	1	1		6.24
12	237.4	206.04	0.15	6.61	0.15	6.71	0			
12	238.4	204.13	0.15	6.71	0.15	6.71	1	1		6.36
12	242.4	171.50	0.15	6.58	0.15	6.58	1	1		6.71
12	244.4	216.68	0.21	4.77	0.21	4.77	1	2		6.58
12	245.4	218.58	0.19	5.31	0.19	5.31	1	3		4.96
12	246.4	220.52	0.21	4.82	0.21	4.82	1	2		6.58
12	247.4	214.38	0.20	4.96	0.20	4.96	1	3		4.82
12	248.4	222.32	0.19	5.29	0.19	5.29	1	1		5.31
12	249.4	195.40	0.19	5.38	0.19	5.29	0			
12	250.4	196.70	0.19	5.31	0.19	5.29	0			
12	251.4	227.56	0.27	3.77	0.27	3.77	1	0		5.29
12	252.4	228.59	0.23	4.35	0.27	3.77	0			
12	253.4	229.99	0.23	4.36	0.23	4.36	1	2		3.77
12	254.4	229.69	0.23	4.33	0.23	4.33	1	3		3.77
12	255.4	266.33	0.24	4.16	0.23	4.36	0			
12	256.4	276.71	0.24	4.11	0.23	4.36	0			
12	257.4	259.16	0.24	4.19	0.23	4.33	0			
12	258.4	301.36	0.23	4.41	0.23	4.41	1	1		3.77
12	259.4	304.03	0.22	4.45	0.23	4.41	0			
12	260.4	209.14	0.23	4.26	0.23	4.41	0			
12	261.4	216.52	0.24	4.23	0.23	4.41	0			
12	262.4	223.02	0.24	4.19	0.24	4.19	1	1		4.41
12	263.4	317.71	0.23	4.26	0.23	4.26	1	0		4.19
12	264.4	321.32	0.23	4.33	0.23	4.26	0			
12	266.4	326.62	0.23	4.36	0.23	4.26	0			
12	267.4	227.23	0.23	4.38	0.23	4.26	0			
12	269.4	331.43	0.22	4.45	0.22	4.45	1	4		4.26
12	270.4	237.24	0.22	4.49	0.22	4.49	1	0		4.45
12	271.4	233.60	0.22	4.50	0.22	4.49	0			
12	272.4	345.78	0.23	4.35	0.23	4.35	1	2		4.49
12	273.4	341.54	0.22	4.45	0.22	4.45	1	3		4.49
12	274.4	344.24	0.23	4.44	0.23	4.44	1	3		4.49
12	275.4	346.94	0.23	4.43	0.23	4.44	1	1		4.49
12	276.4	426.76	0.92	1.09	0.92	1.09	1	0		4.43
12	278.4	445.84	1.17	0.85	1.17	0.85	1	0		1.09
12	280.4	551.95	0.88	1.14	0.88	1.14	1	0		0.85
12	285.4	608.31	1.13	0.89	1.13	0.89	1	0		0.83
12	289.4	576.61	1.20	0.83	1.20	0.83	1	0		1.14
12	294.4	830.40	1.26	0.79	1.26	0.79	1	0		0.89
12	295.4	1013.44	1.21	0.83	1.21	0.83	1	0		0.79
12	84.5	54.82	0.66	1.52	0.66	1.52	1	0		.
12	85.5	55.96	0.63	1.59	0.66	1.52	0			
12	88.5	61.83	0.70	1.43	0.70	1.43	1	0		1.52

St	ID	Gen	Follow Gen	Carry	Large	Trds	Grp	Flow Type	Den	Lane	Dist
12	160.5		1	1		.	160	0	0.75	1	1.83
12	161.5		1	1		2	161	0	1.31	2	1.83
12	172.5		1	1		.	172	0	1.31	0	1.83
12	173.5		1	1		.	173	0	1.49	1	1.83
12	177.5		1	1		.	177	0	0.93	1	1.83
12	183.5		0	1		2	183	0	1.12	2	1.83
12	216.5		1	1		.	216	0	1.49	1	1.83
12	218.5		1	1		.	218	0	1.49	1	1.83
12	219.5		1	1		2	219	0	1.68	1	1.83
12	223.5		0	0		.	223	0	1.86	1	1.83
12	225.5		0	0		1	223	0	2.05	1	1.83
12	242.5		1	1		.	242	0	1.31	0	10.42
12	249.5		1	1		.	249	0	1.49	1	1.83
12	250.5		0	0		1	249	0	1.86	2	1.83
12	260.5		0	1		.	260	0	1.31	1	1.83
12	261.5		1	1		.	261	0	1.31	0	1.83
12	262.5		1	1		.	262	0	1.49	2	10.42
12	267.5		1	1		.	267	0	1.49	2	10.42
12	270.5		1	1		.	270	0	1.68	2	1.83
12	271.5		1	1		1	270	0	1.31	2	1.83
12	285.5		0	0		.	285	0	0.37	1	1.83
12	294.5		0	0		.	294	0	0.37	0	10.42
12	298.5		0	1		.	298	0	1.49	1	1.83
12	299.5		0	1		1	299	0	1.86	2	1.83

St	ID	Pre-Obs	Speed	Norm Time	1st Per Speed	1st Per Time	1st Per	1st Per Type	1st Follow	Prev Grp Time
12	160.5	91.72	0.56	1.80	0.56	1.80	1	0		1.43
12	161.5	97.90	0.61	1.64	0.56	1.80	1	2		1.80
12	172.5	96.00	0.54	1.85	0.54	1.85	1	3		1.80
12	173.5	98.83	0.58	1.71	0.58	1.71	1	0		1.80
12	177.5	109.38	0.67	1.48	0.67	1.48	1	0		1.71
12	183.5	110.38	0.67	1.49	0.67	1.49	1	0		1.48
12	216.5	155.89	0.46	2.16	0.46	2.16	1	1		1.49
12	218.5	161.83	0.50	2.00	0.50	2.00	1	1		2.16
12	219.5	163.40	0.50	2.02	0.50	2.02	1	1		2.00
12	223.5	164.26	0.49	2.05	0.49	2.05	1	0		2.02
12	225.5	165.03	0.48	2.07	0.49	2.05	0			
12	242.5	171.50	0.45	2.22	0.45	2.22	1	1		2.05
12	249.5	195.40	0.26	3.84	0.26	3.84	1	1		3.46
12	250.5	196.70	0.27	3.76	0.26	3.84	0			
12	260.5	209.14	0.15	6.46	0.15	6.46	1	1		3.84
12	261.5	216.52	0.16	6.15	0.16	6.15	1	1		6.46
12	262.5	223.02	0.17	5.95	0.17	5.95	1	1		6.15
12	267.5	227.23	0.17	5.90	0.17	5.90	1	1		5.95
12	270.5	237.24	0.18	5.44	0.18	5.44	1	0		5.90
12	271.5	233.60	0.18	5.45	0.18	5.44	0			
12	285.5	608.31	1.06	0.95	1.06	0.95	1	0		5.44
12	294.5	830.40	1.13	0.89	1.13	0.89	1	0		0.95
12	298.5	177.31	0.52	1.92	0.52	1.92	1	1		2.22
12	299.5	181.45	0.29	3.46	0.29	3.46	1	1		1.92

Appendix C: Statistical Tests

For the variables from Building 6, the mean effective normalized descent times (s/m) are provided for the entire population and for the leaders and followers. The standard deviation (s/m) is provided below each mean. The p-value for a t-test comparing the means between all occupants for the number of treads and for all variables for the first persons in flow units is also provided for all categorical variables. For the travel distance, the paired t-test compares the first and second observation for each person.

Gender	Male	Female
All	1.68	1.73
Standard Deviation	0.33	0.30
Follower	1.77	1.76
Standard Deviation	0.30	0.30
First Persons in Flow Unit	1.50	1.70
Standard Deviation	0.32	0.31
p-value	$1.87*10^{-6}$*	

*Significant based on 95% confidence level

Encumbrance	Not Carrying	Carrying
All	1.69	1.72
Standard Deviation	0.32	0.31
Follower	1.76	1.77
Standard Deviation	0.31	0.28
First Persons in Flow Unit	1.60	1.65
Standard Deviation	0.31	0.34
p-value	0.23	

*Significant based on 95% confidence level

Body Size	Not Large	Large
All	1.70	1.82
Standard Deviation	0.31	0.48
Follower	1.76	1.71
Standard Deviation	0.30	0.23
First Persons in Flow Unit	1.61	1.89
Standard Deviation	0.31	0.58
p-value	0.18	

*Significant based on 95% confidence level

Exit Lane	Inner	Middle	Outer
All	1.68	1.74	1.72
Standard Deviation	0.34	0.30	0.29
Follower	1.75	1.79	1.76
Standard Deviation	0.32	0.28	0.29
First Persons in Flow Unit	1.61	1.66	1.62
Standard Deviation	0.35	0.32	0.27
p-value to Inner		0.37	0.83
p-value to Middle	0.37		0.51
p-value to Outer	0.83	0.51	

*Significant based on 95% confidence level

Open Treads	< 2	2	3	> 3
All	1.80	1.71	1.66	1.57
Standard Deviation	0.32	0.28	0.33	0.31
p-value to < 2		0.003*	$4.3*10^{-105}$*	$1.2*10^{-9}$*
p-value to 2	0.003*		0.24	$3.3*10^{-5}$*
p-value to 3	$4.3*10^{-105}$*	0.24		0.05*
p-value to > 3	$1.2*10^{-9}$*	$3.3*10^{-5}$*	0.05*	
Follower	1.82	1.72	1.65	
Standard Deviation	0.32	0.27	0.29	
First Persons in Flow Unit	1.71	1.68	1.67	1.57
Standard Deviation	0.34	0.31	0.36	0.31
p-value to < 2		0.71	0.65	0.08
p-value to 2	0.71		0.91	0.04*
p-value to 3	0.65	0.91		0.08
p-value to > 3	0.08	0.04*	0.08	

*Significant based on 95% confidence level

Travel Distance	First Observation	Second Observation
Mean	1.46	1.51
Standard Deviation	0.21	0.20
p-value	0.02*	

*Significant based on 95% confidence level

Next, a series of χ^2 test were conducted for the relationships between variables. Subsequent tests compared the actual and expected results when the data was first sorted by the first persons in flow units and followers.

	All	1st Person	Follower	Female	Male	Item	No Item	Large	Not Large
1st Person	248			159	89	112	136	10	238
Follower	347			162	185	152	195	6	341
Total	595			321	274	264	331	16	579
Expected				133.8	114.2	110.0	138.0	6.7	241.3
Values				187.2	159.8	154.0	193.0	9.3	337.7
Chi-statistic				8.1	9.5	0.1	0.0	2.9	0.1
p-value				0.004*	0.002 *	0.806	0.827	0.091	0.779
Female	321	159	162			197	124	10	311
Male	274	89	185			67	207	6	268
Total	595	248	347			264	331	16	579
Expected		133.8	187.2			142.4	178.6	8.6	312.4
Values		114.2	159.8			121.6	152.4	7.4	266.6
Chi-Statistic		10.3	7.4			45.4	36.2	0.5	0.0
p-value		0.001*	0.007*			$1.6*10^{-11}$*	$1.8*10^{-9}$*	0.493	0.909
Items	264	112	152	197	67			5	259
No Items	331	136	195	124	207			11	320
Total	595	248	347	321	274			16	579
Expected		110.0	154.0	142.4	121.6			7.1	256.9
Values		138.0	193.0	178.6	152.4			8.9	322.1
Chi-Statistic		0.1	0.0	37.6	44.0			1.1	0.0
p-value		0.802	0.832	$8.7*10^{-10}$*	$3.2*10^{-11}$*			0.291	0.861
Large	16	10	6	10	6	5	11		
Not Large	579	238	341	311	268	259	320		
Total	595	248	347	321	274	264	331		
Expected		6.7	9.3	8.6	7.4	7.1	8.9		
Values		241.3	337.7	312.4	266.6	256.9	322.1		
Chi-Statistic		1.7	1.2	0.2	0.3	0.6	0.5		
p-value		0.191	0.269	0.637	0.609	0.424	0.476		

*Significant based on 95% confidence level

	All	1st Person	Follower	Female	Male	Item	No Item	Large	Not Large
Treads<2	178	24	154	93	85	65	113	3	175
Treads2	217	50	167	99	118	110	107	5	212
Treads3	80	54	26	52	28	30	50	4	76
Treads>3	120	120	0	77	43	59	61	4	116
Total	595	248	347	321	274	264	331	16	579
Expected		74.2	103.8	96.0	82.0	79.0	99.0	4.8	173.2
Values		90.4	126.6	117.1	99.9	96.3	120.7	5.8	211.2
		33.3	46.7	43.2	36.8	35.5	44.5	2.2	77.8
		50.0	70.0	64.7	55.3	53.2	66.8	3.2	116.8
Chi-Statistic		162.8	116.3	7.0	8.2	5.9	4.7	2.6	0.1
p-value		$4.7*10^{-37}$*	$4.8*10^{-25}$*	0.071	0.042*	0.116	0.195	0.464	0.995
Inner	269	135	134	162	107	135	134	10	259
Middle	131	51	80	78	53	62	69	3	128
Outer	195	62	133	81	114	67	128	3	192
Total	595	248	347	321	274	264	331	16	579
Expected		112.1	156.9	145.1	123.9	119.4	149.6	7.2	261.8
Values		54.6	76.4	70.7	60.3	58.1	72.9	3.5	127.5
		81.3	113.7	105.2	89.8	86.5	108.5	5.2	189.8
Chi-Statistic		9.5	6.8	8.3	9.7	6.7	5.4	2.1	0.1
p-value		0.009*	0.034*	0.016*	0.008*	0.035*	0.069	0.351	0.971

*Significant based on 95% confidence level

	All	Treads <2	Treads2	Treads3	Treads >3	Inner	Middle	Outer
1st Person	24	50	54	120	135	51	62	24
Follower	154	167	26	0	134	80	133	154
Total	178	217	80	120	269	131	195	178
Expected		74.2	90.4	33.3	50.0	112.1	54.6	81.3
Values		103.8	126.6	46.7	70.0	156.9	76.4	113.7
Chi-Statistic		58.2	31.0	21.9	167.9	8.0	0.4	7.8
p-value		2.3* 10^{-14}*	2.6* 10^{-8}*	2.8* 10^{-6}*	2.1* 10^{-38}*	0.005*	0.523	0.005 *
Female	321	93	99	52	77	162	78	81
Male	274	85	118	28	43	107	53	114
Total	595	178	217	80	120	269	131	195
Expected		96.0	117.1	43.2	64.7	145.1	70.7	105.2
Values		82.0	99.9	36.8	55.3	123.9	60.3	89.8
Chi-Statistic		0.2	6.1	3.9	5.0	4.3	1.6	12.1
p-value		0.649	0.014*	0.047*	0.025*	0.039*	0.199	5.1* 10^{-4}*
Items	264	65	110	30	59	135	62	67
No Items	331	113	107	50	61	134	69	128
Total	595	178	217	80	120	269	131	195
Expected		79.0	96.3	35.5	53.2	119.4	58.1	86.5
Values		99.0	120.7	44.5	66.8	149.6	72.9	108.5
Chi-Statistic		4.4	3.5	1.5	1.1	3.7	0.5	7.9
p-value		0.035*	0.061	0.216	0.290	0.055	0.496	0.005 *
Large	16	3	5	4	4	10	3	3
Not Large	579	175	212	76	116	259	128	192
Total	595	178	217	80	120	269	131	195
Expected		4.8	5.8	2.2	3.2	7.2	3.5	5.2
Values		173.2	211.2	77.8	116.8	261.8	127.5	189.8
Chi-Statistic		0.7	0.1	1.6	0.2	1.1	0.1	1.0
p-value	321	0.408	0.726	0.201	0.663	0.297	0.778	0.321

*Significant based on 95% confidence level

	All	Treads <2	Treads2	Treads3	Treads >3	Inner	Middle	Outer
Treads<2	178					68	32	78
Treads2	217					90	56	71
Treads3	80					41	23	16
Treads>3	120					70	20	30
Total	595					269	131	195
Expected						80.5	39.2	58.3
Values						98.1	47.8	71.1
						36.2	17.6	26.2
						54.3	26.4	39.3
Chi-Statistic						7.8	5.9	12.8
p-value						0.050*	0.114	0.005 *
Inner	269	68	90	41	70			
Middle	131	32	56	23	20			
Outer	195	78	71	16	30			
Total	595	178	217	80	120			
Expected		80.5	98.1	36.2	54.3			
Values		39.2	47.8	17.6	26.4			
		58.3	71.1	26.2	39.3			
Chi-Statistic		9.9	2.1	6.3	8.3			
p-value		0.007*	0.353	0.043*	0.015*			

*Significant based on 95% confidence level

First Persons	All	Female	Male	Item	No Item	Large	Not Large
Female	159			95	64	6	153
Male	89			17	72	4	85
Total	248			112	136	10	238
Expected				71.8	87.2	6.4	152.6
Values				40.2	48.8	3.6	85.4
Chi-Statistic				20.9	17.2	0.1	0.0
p-value				$4.9*10^{-6}$*	$3.4*10^{-5}$*	0.786	0.956
Items	112	95	17			2	110
No Items	136	64	72			8	128
Total	248	159	89			10	238
Expected		71.8	40.2			4.5	107.5
Values		87.2	48.8			5.5	130.5
Chi-Statistic		13.7	24.4			2.6	0.1
p-value		$2.2*10^{-4}$*	$7.8*10^{-7}$*			0.110	0.743
Large	10	6	4	2	8		
Not Large	238	153	85	110	128		
Total	248	159	89	112	136		
Expected		6.4	3.6	4.5	5.5		
Values		152.6	85.4	107.5	130.5		
Chi-Statistic		0.0	0.0	1.5	1.2		
p-value		0.868	0.825	0.227	0.273		
Treads<2	24			17	7	10	14
Treads2	50			28	22	27	23
Treads3	54			37	17	16	38
Treads>3	120			77	43	59	61
Total	248			159	89	112	136
Expected				15.4	8.6	10.8	13.2
Values				32.1	17.9	22.6	27.4
				34.6	19.4	24.4	29.6
				76.9	43.1	54.2	65.8
Chi-Statistic				0.8	1.5	4.2	3.5
p-value				0.838	0.680	0.237	0.322
Inner	135			93	42	69	66
Middle	51			34	17	20	31
Outer	62			32	30	23	39
Total	248			159	89	112	136
Expected				86.6	48.4	61.0	74.0
Values				32.7	18.3	23.0	28.0
				39.8	22.3	28.0	34.0
Chi-Statistic				2.0	3.7	2.4	1.9
p-value				0.360	0.161	0.309	0.380

*Significant based on 95% confidence level

First Persons	All	Treads <2	Treads2	Treads3	Treads >3	Inner	Middle	Outer
Female	159	17	28	37	77	93	34	32
Male	89	7	22	17	43	42	17	30
Total	248	24	50	54	120	135	51	62
Expected		15.4	32.1	34.6	76.9	86.6	32.7	39.8
Values		8.6	17.9	19.4	43.1	48.4	18.3	22.3
Chi-Statistic		0.5	1.4	0.5	0.0	1.3	0.1	4.2
p-value		0.492	0.232	0.500	0.990	0.247	0.704	0.040 *
Items	112	10	27	16	59	69	20	23
No Items	136	14	23	38	61	66	31	39
Total	248	24	50	54	120	135	51	62
Expected		10.8	22.6	24.4	54.2	61.0	23.0	28.0
Values		13.2	27.4	29.6	65.8	74.0	28.0	34.0
Chi-Statistic		0.1	1.6	5.3	0.8	1.9	0.7	1.6
p-value		0.731	0.209	0.022*	0.378	0.165	0.394	0.202
Large	10	1	1	4	4	7	1	2
Not Large	238	23	49	50	116	128	50	60
Total	248	24	50	54	120	135	51	62
Expected		1.0	2.0	2.2	4.8	5.4	2.1	2.5
Values		23.0	48.0	51.8	115.2	129.6	48.9	59.5
Chi-Statistic		0.0	0.5	1.6	0.2	0.5	0.6	0.1
p-value		0.973	0.465	0.207	0.697	0.496	0.452	0.747
Treads<2	24					10	7	7
Treads2	50					28	8	14
Treads3	54					27	16	11
Treads>3	120					70	20	30
Total	248					135	51	62
Expected						13.1	4.9	6.0
Values						27.2	10.3	12.5
						29.4	11.1	13.5
						65.3	24.7	30.0
Chi-Statistic						1.3	4.4	0.8
p-value						0.736	0.220	0.847
Inner	135	10	28	27	70			
Middle	51	7	8	16	20			
Outer	62	7	14	11	30			
Total	248	24	50	54	120			
Expected		13.1	27.2	29.4	65.3			
Values		4.9	10.3	11.1	24.7			
		6.0	12.5	13.5	30.0			
Chi-Statistic		1.7	0.7	2.8	1.2			
p-value		0.417	0.702	0.245	0.543			

*Significant based on 95% confidence level

Followers	All	Female	Male	Item	No Item	Large	Not Large
Female	162			102	60	4	158
Male	185			50	135	2	183
Total	347			152	195	6	341
Expected				71.0	91.0	2.8	159.2
Values				81.0	104.0	3.2	181.8
Chi-Statistic				25.5	19.8	1.0	0.0
p-value				$4.5*10^{-7}$*	$8.4*10^{-6}$*	0.327	0.896
Items	152	102	50			3	149
No Items	195	60	135			3	192
Total	347	162	185			6	341
Expected		71.0	81.0			2.6	149.4
Values		91.0	104.0			3.4	191.6
Chi-Statistic		24.2	21.2			0.1	0.0
p-value		$8.9*10^{-7}$*	$4.2*10^{-6}$*			0.760	0.968
Large	6	4	2	3	3		
Not Large	341	158	183	149	192		
Total	347	162	185	152	195		
Expected		2.8	3.2	2.6	3.4		
Values		159.2	181.8	149.4	191.6		
Chi-Statistic		0.5	0.5	0.1	0.0		
p-value		0.470	0.499	0.817	0.838		
Treads<2	154	76	78	55	99	2	152
Treads2	167	71	96	83	84	4	163
Treads3	26	15	11	14	12	0	26
Total	347	162	185	152	195	6	341
Expected		71.9	82.1	67.5	86.5	2.7	151.3
Values		78.0	89.0	73.2	93.8	2.9	164.1
		12.1	13.9	11.4	14.6	0.4	25.6
Chi-Statistic		1.5	1.3	4.2	3.3	1.0	0.0
p-value		0.465	0.511	0.121	0.193	0.594	0.991
Inner	134	69	65	66	68	3	131
Middle	80	44	36	42	38	2	78
Outer	133	49	84	44	89	1	132
Total	347	162	185	152	195	6	341
Expected		62.6	71.4	58.7	75.3	2.3	131.7
Values		37.3	42.7	35.0	45.0	1.4	78.6
		62.1	70.9	58.3	74.7	2.3	130.7
Chi-Statistic		4.6	4.0	5.8	4.5	1.2	0.0
p-value		0.100	0.133	0.056	0.105	0.546	0.989

*Significant based on 95% confidence level

Followers	All	Treads<2	Treads2	Treads3	Inner	Middle	Outer
Female	162	76	71	15	69	44	49
Male	185	78	96	11	65	36	84
Total	347	154	167	26	134	80	133
Expected		71.9	78.0	12.1	62.6	37.3	62.1
Values		82.1	89.0	13.9	71.4	42.7	70.9
Chi-Statistic		0.4	1.2	1.3	1.2	2.2	5.2
p-value		0.507	0.280	0.261	0.265	0.136	0.023*
Items	152	55	83	14	66	42	44
No Items	195	99	84	12	68	38	89
Total	347	154	167	26	134	80	133
Expected		67.5	73.2	11.4	58.7	35.0	58.3
Values		86.5	93.8	14.6	75.3	45.0	74.7
Chi-Statistic		4.1	2.4	1.1	1.6	2.5	6.2
p-value		0.043*	0.125	0.302	0.204	0.117	0.013*
Large	6	2	4	0	3	2	1
Not Large	341	152	163	26	131	78	132
Total	347	154	167	26	134	80	133
Expected		2.7	2.9	0.4	2.3	1.4	2.3
Values		151.3	164.1	25.6	131.7	78.6	130.7
Chi-Statistic		0.2	0.4	0.5	0.2	0.3	0.7
p-value		0.682	0.509	0.499	0.651	0.597	0.387
Treads<2	154				58	25	71
Treads2	167				62	48	57
Treads3	26				14	7	5
Total	347				134	80	133
Expected					59.5	35.5	59.0
Values					64.5	38.5	64.0
					10.0	6.0	10.0
Chi-Statistic					1.7	5.6	5.7
p-value					0.429	0.060	0.059
Inner	134	58	62	14			
Middle	80	25	48	7			
Outer	133	71	57	5			
Total	347	154	167	26			
Expected		59.5	64.5	10.0			
Values		35.5	38.5	6.0			
		59.0	64.0	10.0			
Chi-Statistic		5.6	3.2	4.2			
p-value		0.062	0.201	0.122			

*Significant based on 95% confidence level

Next, the travel distance (m) and pre-observation time were compared for the different levels of the categorical variables using t-tests.

Variable	Trav. Dist. Mean	Trav. Dist. St. Dev.	Trav. Dist. p-value	Pre-Obs. Mean	Pre-Obs. St. Dev.	Pre-Obs. p-value
1st Person	130.3	99.2	0.90	195.0	99.0	0.50
Follower	131.2	84.2	0.90	200.5	98.9	0.50
Treads<2	122.3	79.0	0.11	208.1	103.0	0.12
Treads2	138.5	96.6	0.13	194.9	89.2	0.52
Treads3	131.8	92.1	0.92	187.5	108.0	0.34
Treads>3	129.0	94.7	0.81	196.8	102.9	0.86
Female	132.3	90.8	0.68	192.9	91.4	0.16
Male	129.2	90.6	0.68	204.5	106.8	0.16
Carry	134.9	93.7	0.33	202.3	92.6	0.36
Not Carry	127.6	88.2	0.33	194.9	103.7	0.36
Large	184.5	115.0	0.08	167.3	63.8	0.07
Not Large	129.3	89.6	0.08	199.1	99.6	0.07
Inner	130.9	90.2	0.99	198.8	95.3	0.90
Middle	133.8	91.4	0.67	199.3	100.2	0.88
Outer	128.7	91..2	0.70	196.7	103.3	0.79

*Significant based on 95% confidence level

The last piece of analysis for Building 6 involved calculating the R^2 value. The sum of the squares of the difference between the actual and predicted values was 20.3. The sum of the square of the difference between the actual and average values was 59.5. In the table, the predicted value is in s/m.

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
0	4.1	1.24	0.18	0.00	0	108.1	1.41	0.21	0.03
0	5.1	1.53	0.08	0.01	0	109.1	1.60	0.16	0.08
0	6.1	1.48	0.11	0.01	0	110.1	1.38	0.17	0.01
0	8.1	1.64	0.10	0.06	0	18.2	1.54	0.13	0.04
0	9.1	1.61	0.08	0.04	0	19.2	1.59	0.17	0.09
0	10.1	1.64	0.07	0.04	0	20.2	1.39	0.18	0.01
0	13.1	1.23	0.04	0.08	0	21.2	1.47	0.18	0.03
0	16.1	1.28	0.69	0.17	0	24.2	1.62	0.03	0.01
0	17.1	1.29	0.26	0.01	0	26.2	1.72	0.02	0.02
0	18.1	1.51	0.01	0.01	0	33.2	1.60	0.02	0.00
0	24.1	1.42	0.00	0.09	0	41.2	1.60	0.04	0.01
0	30.1	1.67	0.01	0.01	0	42.2	1.70	0.02	0.02
0	31.1	1.57	0.02	0.07	0	43.2	1.60	0.02	0.00
0	33.1	1.57	0.00	0.04	0	46.2	1.71	0.02	0.02
0	37.1	1.64	0.01	0.02	0	47.2	1.72	0.00	0.00
0	39.1	1.66	0.00	0.00	0	53.2	1.71	0.03	0.03
0	40.1	1.77	0.00	0.00	0	58.2	1.41	0.00	0.06
0	41.1	1.59	0.06	0.02	0	59.2	1.63	0.03	0.01
0	42.1	1.63	0.00	0.00	0	72.2	1.48	0.01	0.02
0	43.1	1.66	0.00	0.00	0	73.2	1.47	0.04	0.00
0	46.1	1.63	0.00	0.00	0	76.2	1.79	0.01	0.04
0	48.1	1.77	0.01	0.03	0	77.2	1.77	0.03	0.06
0	52.1	1.56	0.00	0.01	0	81.2	1.44	0.03	0.01
0	53.1	1.69	0.01	0.01	0	82.2	1.74	0.02	0.04
0	54.1	1.79	0.08	0.13	0	84.2	1.70	0.01	0.01
0	58.1	1.44	0.01	0.15	0	94.2	1.64	0.02	0.03
0	59.1	1.66	0.00	0.00	0	95.2	1.55	0.02	0.00
0	60.1	1.57	0.02	0.00	0	105.2	1.29	0.33	0.02
0	61.1	1.57	0.02	0.00	0	108.2	1.30	0.38	0.04
0	72.1	1.50	0.01	0.02	0	110.2	1.43	0.38	0.12
0	73.1	1.49	0.00	0.02	0	80.4	1.43	0.00	0.09
0	74.1	1.81	0.12	0.20	0	81.4	1.48	0.00	0.05
0	76.1	1.82	0.00	0.03	0	82.4	1.71	0.03	0.03
0	77.1	1.77	0.00	0.00	0	84.4	1.67	0.00	0.01
0	81.1	1.47	0.01	0.02	0	87.4	1.56	0.39	0.22
0	82.1	1.73	0.01	0.02	0	88.4	1.75	0.29	0.34
0	84.1	1.72	0.02	0.02	0	94.4	1.56	0.04	0.00
0	86.1	1.59	0.08	0.02	0	98.4	2.07	0.00	0.14
0	88.1	2.00	0.05	0.26	1	5.1	1.51	0.27	0.10
0	92.1	1.73	0.04	0.05	1	6.1	1.51	0.05	0.00
0	93.1	1.78	0.03	0.01	1	7.1	1.56	0.01	0.00
0	94.1	1.67	0.22	0.19	1	8.1	1.61	0.02	0.00
0	95.1	1.58	0.02	0.00	1	20.1	1.58	0.01	0.00
0	96.1	2.14	1.07	0.36	1	22.1	1.59	0.00	0.01
0	98.1	2.12	1.43	0.61	1	30.1	1.72	0.06	0.07
0	99.1	1.41	0.19	0.02	1	33.1	1.53	0.05	0.00
0	101.1	1.54	0.21	0.09	1	34.1	1.69	0.06	0.06
0	102.1	1.68	0.18	0.16	1	35.1	1.64	0.02	0.01
0	104.1	1.36	0.14	0.00	1	36.1	1.38	0.06	0.01
0	105.1	1.32	0.21	0.00	1	38.1	1.64	0.10	0.14

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
1	39.1	1.63	0.08	0.12	2	116.1	1.68	0.02	0.03
1	40.1	1.64	0.11	0.07	2	117.1	1.65	0.02	0.03
1	41.1	1.55	0.12	0.04	2	129.1	1.38	0.14	0.00
1	43.1	1.59	0.16	0.08	2	130.1	1.37	0.07	0.01
1	44.1	1.72	0.06	0.06	2	136.1	1.54	0.01	0.00
1	51.1	1.73	0.07	0.08	2	150.1	1.68	0.06	0.05
1	52.1	1.57	0.02	0.00	2	160.1	1.58	0.00	0.02
1	53.1	1.58	0.07	0.16	2	161.1	1.59	0.00	0.00
1	56.1	1.48	0.27	0.55	2	162.1	1.68	0.00	0.00
1	57.1	1.64	0.21	0.28	2	165.1	1.81	0.00	0.01
1	59.1	1.81	0.24	0.15	2	166.1	1.58	0.00	0.01
1	60.1	1.82	0.25	0.15	2	167.1	1.67	0.00	0.00
1	69.1	1.76	0.29	0.23	2	172.1	1.43	0.09	0.33
1	78.1	1.81	0.31	0.21	2	174.1	1.46	0.03	0.17
1	85.1	1.79	0.21	0.15	2	176.1	1.72	0.04	0.03
1	117.1	2.13	0.15	0.00	2	179.1	1.46	0.11	0.34
1	122.1	2.07	0.07	0.01	2	180.1	1.63	0.08	0.13
1	124.1	1.99	0.43	0.14	2	181.1	1.62	0.15	0.22
1	125.1	1.93	0.11	0.01	2	183.1	1.63	0.08	0.12
1	132.1	1.91	0.22	0.07	2	208.1	1.83	0.01	0.05
1	135.1	1.60	0.65	0.49	2	209.1	1.73	0.03	0.02
1	136.1	1.67	1.91	2.01	2	210.1	1.70	0.03	0.03
1	138.1	1.68	0.08	0.07	2	211.1	1.63	0.03	0.07
1	139.1	1.78	0.07	0.12	2	80.2	1.73	0.00	0.01
1	140.1	1.74	0.14	0.16	2	84.2	1.51	0.01	0.01
1	141.1	1.83	0.15	0.25	2	96.2	1.63	0.08	0.04
1	142.1	1.55	0.23	0.11	2	115.2	1.59	0.07	0.02
1	143.1	1.65	0.22	0.17	2	116.2	1.68	0.05	0.04
1	145.1	1.64	0.23	0.17	2	117.2	1.59	0.02	0.00
1	148.1	1.69	0.20	0.18	2	150.2	1.73	0.07	0.09
1	122.3	1.58	0.09	0.03	2	179.2	1.35	0.03	0.04
1	138.3	1.64	0.12	0.08	2	180.2	1.58	0.02	0.00
1	139.3	1.70	0.10	0.10	2	183.2	1.60	0.01	0.00
1	140.3	1.69	0.15	0.14	2	190.2	1.55	0.18	0.07
1	141.3	1.71	0.12	0.13	2	191.2	1.40	0.56	0.20
1	142.3	1.47	0.11	0.01	2	208.2	1.67	0.39	0.35
1	145.3	1.51	0.13	0.03	2	209.2	1.73	0.06	0.07
1	146.3	1.58	0.10	0.04	2	210.2	1.70	0.06	0.06
1	148.3	1.55	0.27	0.14	2	211.2	1.44	0.31	0.09
1	138.4	1.62	0.11	0.06	2	84.3	1.59	0.05	0.01
1	140.4	1.67	0.19	0.16	2	96.3	1.61	0.05	0.02
1	142.4	1.45	0.12	0.01	2	115.3	1.57	0.04	0.00
1	145.4	1.49	0.14	0.03	2	117.3	1.57	0.03	0.00
1	147.4	1.63	0.25	0.18	2	179.3	1.43	0.01	0.02
1	148.4	1.53	0.35	0.17	2	180.3	1.56	0.02	0.00
2	48.1	1.75	0.00	0.01	2	183.3	1.58	0.02	0.00
2	58.1	1.58	0.01	0.00	2	191.3	1.38	0.72	0.27
2	65.1	1.75	0.00	0.01	2	211.3	1.42	0.27	0.06
2	96.1	1.74	0.01	0.01	2	211.4	1.38	0.38	0.09
2	115.1	1.65	0.01	0.02	4	29.1	1.48	0.00	0.08

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
4	32.1	1.56	0.00	0.01	0	20.1	1.61	0.01	0.00
4	33.1	1.64	0.03	0.05	0	21.1	1.61	0.01	0.00
4	66.1	1.50	0.01	0.02	0	22.1	1.61	0.01	0.00
4	67.1	1.64	0.00	0.00	0	25.1	1.73	0.00	0.00
4	72.1	1.59	0.00	0.00	0	26.1	1.73	0.00	0.00
4	73.1	1.47	0.00	0.04	0	27.1	1.73	0.00	0.00
4	74.1	1.55	0.01	0.00	0	28.1	1.73	0.00	0.00
4	76.1	1.52	0.01	0.01	0	29.1	1.73	0.00	0.00
4	81.1	1.64	0.01	0.00	0	32.1	1.83	0.01	0.00
4	86.1	1.63	0.00	0.00	0	34.1	1.76	0.00	0.00
4	87.1	1.73	0.15	0.13	0	35.1	1.76	0.00	0.00
4	89.1	1.84	0.14	0.06	0	36.1	1.76	0.00	0.00
4	90.1	1.82	0.12	0.05	0	38.1	1.78	0.01	0.00
4	92.1	1.79	0.12	0.07	0	44.1	1.67	0.00	0.00
4	93.1	1.88	0.14	0.04	0	45.1	1.67	0.00	0.00
4	94.1	1.66	0.15	0.19	0	47.1	1.61	0.01	0.00
4	95.1	1.82	0.19	0.10	0	49.1	1.61	0.01	0.00
4	100.1	1.82	0.07	0.02	0	50.1	1.61	0.01	0.00
4	101.1	1.78	0.09	0.05	0	51.1	1.61	0.01	0.00
4	103.1	1.75	0.14	0.11	0	55.1	1.43	0.05	0.00
4	113.1	1.74	0.24	0.20	0	56.1	1.43	0.06	0.00
4	114.1	1.60	0.32	0.46	0	57.1	1.43	0.06	0.00
4	132.1	1.33	0.06	0.38	0	62.1	1.57	0.02	0.00
4	135.1	1.35	0.24	0.71	0	63.1	1.57	0.02	0.00
4	142.1	1.49	0.00	0.03	0	64.1	1.57	0.02	0.00
4	143.1	1.54	0.03	0.12	0	65.1	1.57	0.01	0.00
4	145.1	1.67	0.05	0.06	0	66.1	1.57	0.01	0.00
4	155.1	1.74	0.04	0.03	0	67.1	1.57	0.01	0.00
4	156.1	1.64	0.01	0.02	0	68.1	1.57	0.01	0.00
4	157.1	1.68	0.00	0.01	0	69.1	1.57	0.01	0.00
4	173.1	1.68	0.00	0.00	0	70.1	1.57	0.01	0.00
4	188.1	1.65	0.11	0.15	0	71.1	1.57	0.01	0.00
4	205.1	1.86	0.08	0.02	0	75.1	1.66	0.00	0.00
4	206.1	1.91	0.07	0.00	0	78.1	1.61	0.01	0.00
4	212.1	1.81	0.05	0.02	0	79.1	1.61	0.01	0.00
4	216.1	2.08	0.49	0.11	0	80.1	1.61	0.01	0.00
4	70.2	1.43	0.11	0.00	0	83.1	1.57	0.02	0.00
4	74.2	1.49	0.03	0.00	0	85.1	1.57	0.02	0.00
4	75.2	1.44	0.01	0.02	0	87.1	1.43	0.08	0.00
4	76.2	1.46	0.03	0.01	0	89.1	1.49	0.04	0.00
4	103.2	1.69	0.00	0.00	0	90.1	1.49	0.05	0.00
4	113.2	1.65	0.00	0.00	0	91.1	1.49	0.04	0.00
4	193.2	1.74	0.01	0.00	0	97.1	2.90	1.28	0.00
4	216.2	2.08	0.00	0.13	0	100.1	1.27	0.18	0.00
4	100.3	1.77	0.01	0.03	0	103.1	1.28	0.14	0.00
4	103.3	1.67	0.00	0.00	0	106.1	1.25	0.20	0.00
4	113.3	1.63	0.00	0.01	0	107.1	1.25	0.20	0.00
4	216.3	2.06	0.02	0.24	0	22.2	1.29	0.18	0.00
0	7.1	1.37	0.13	0.00	0	25.2	1.52	0.04	0.00
0	19.1	1.61	0.01	0.00	0	27.2	1.52	0.04	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
0	28.2	1.52	0.03	0.00	0	83.4	1.75	0.02	0.01
0	29.2	1.57	0.01	0.00	0	85.4	1.75	0.00	0.00
0	34.2	1.58	0.01	0.00	0	89.4	1.17	0.31	0.00
0	35.2	1.58	0.01	0.00	0	90.4	1.17	0.31	0.00
0	36.2	1.58	0.01	0.00	0	91.4	1.17	0.31	0.00
0	44.2	1.56	0.02	0.00	0	93.4	1.70	0.00	0.00
0	45.2	1.56	0.03	0.00	0	95.4	1.51	0.04	0.00
0	48.2	1.69	0.00	0.00	0	96.4	1.70	0.00	0.00
0	49.2	1.69	0.00	0.00	0	97.4	1.70	0.00	0.00
0	50.2	1.69	0.00	0.00	1	9.1	1.58	0.01	0.00
0	51.2	1.69	0.00	0.00	1	10.1	1.58	0.01	0.00
0	52.2	1.69	0.00	0.00	1	11.1	1.58	0.01	0.00
0	54.2	1.54	0.03	0.00	1	12.1	1.58	0.02	0.00
0	55.2	1.54	0.03	0.00	1	13.1	1.58	0.01	0.00
0	56.2	1.54	0.03	0.00	1	14.1	1.58	0.01	0.00
0	57.2	1.54	0.03	0.00	1	15.1	1.58	0.01	0.00
0	60.2	1.54	0.03	0.00	1	16.1	1.58	0.01	0.00
0	61.2	1.54	0.02	0.00	1	17.1	1.58	0.01	0.00
0	62.2	1.54	0.03	0.00	1	18.1	1.58	0.01	0.00
0	63.2	1.54	0.03	0.00	1	19.1	1.58	0.00	0.00
0	64.2	1.54	0.02	0.00	1	23.1	1.71	0.00	0.00
0	65.2	1.54	0.03	0.00	1	24.1	1.71	0.00	0.00
0	66.2	1.54	0.03	0.00	1	25.1	1.71	0.00	0.00
0	67.2	1.54	0.03	0.00	1	31.1	1.46	0.06	0.00
0	68.2	1.54	0.04	0.00	1	32.1	1.46	0.06	0.00
0	69.2	1.54	0.04	0.00	1	37.1	1.45	0.06	0.00
0	70.2	1.54	0.04	0.00	1	42.1	1.30	0.15	0.00
0	71.2	1.54	0.04	0.00	1	45.1	1.47	0.05	0.00
0	75.2	1.61	0.01	0.00	1	46.1	1.47	0.06	0.00
0	78.2	1.52	0.03	0.00	1	47.1	1.47	0.05	0.00
0	79.2	1.52	0.03	0.00	1	48.1	1.47	0.05	0.00
0	80.2	1.52	0.03	0.00	1	49.1	1.47	0.05	0.00
0	83.2	1.59	0.01	0.00	1	50.1	1.47	0.06	0.00
0	85.2	1.59	0.01	0.00	1	54.1	2.16	0.20	0.00
0	86.2	1.59	0.01	0.00	1	55.1	2.16	0.20	0.00
0	87.2	1.59	0.01	0.00	1	58.1	2.23	0.27	0.00
0	88.2	1.59	0.01	0.00	1	61.1	2.20	0.24	0.00
0	89.2	1.59	0.01	0.00	1	62.1	2.20	0.23	0.00
0	90.2	1.59	0.01	0.00	1	63.1	2.20	0.25	0.00
0	91.2	1.59	0.01	0.00	1	70.1	2.24	0.30	0.00
0	92.2	1.59	0.00	0.00	1	71.1	2.24	0.30	0.00
0	93.2	1.59	0.01	0.00	1	72.1	2.24	0.28	0.00
0	96.2	1.59	0.01	0.00	1	73.1	2.24	0.33	0.00
0	97.2	1.59	0.01	0.00	1	74.1	2.24	0.32	0.00
0	98.2	1.59	0.01	0.00	1	75.1	2.24	0.32	0.00
0	106.2	1.13	0.34	0.00	1	76.1	2.24	0.34	0.00
0	107.2	1.13	0.31	0.00	1	77.1	2.24	0.37	0.01
0	109.2	1.13	0.33	0.00	1	79.1	2.26	0.33	0.00
0	78.4	1.70	0.00	0.00	1	80.1	2.26	0.32	0.00
0	79.4	1.70	0.00	0.00	1	81.1	2.26	0.33	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
1	82.1	2.26	0.32	0.00	1	147.1	1.26	0.18	0.00
1	83.1	2.26	0.33	0.00	1	123.3	1.41	0.08	0.00
1	84.1	2.26	0.31	0.00	1	143.3	1.35	0.13	0.00
1	86.1	2.17	0.23	0.00	1	144.3	1.35	0.13	0.00
1	87.1	2.23	0.27	0.00	1	147.3	1.18	0.26	0.00
1	88.1	2.17	0.24	0.00	1	139.4	1.37	0.11	0.00
1	89.1	2.17	0.23	0.00	1	141.4	1.27	0.20	0.00
1	90.1	2.17	0.25	0.00	1	143.4	1.33	0.13	0.00
1	91.1	2.17	0.25	0.00	1	144.4	1.33	0.14	0.00
1	92.1	2.17	0.25	0.00	1	146.4	1.34	0.13	0.00
1	93.1	2.17	0.25	0.00	2	49.1	1.67	0.00	0.00
1	94.1	2.17	0.26	0.00	2	83.1	1.90	0.05	0.00
1	95.1	2.17	0.23	0.00	2	84.1	1.90	0.05	0.00
1	96.1	2.17	0.23	0.00	2	97.1	1.81	0.01	0.00
1	97.1	2.17	0.24	0.00	2	98.1	1.81	0.01	0.00
1	98.1	2.17	0.23	0.00	2	99.1	1.81	0.01	0.00
1	99.1	2.17	0.24	0.00	2	128.1	1.33	0.13	0.00
1	100.1	2.17	0.23	0.00	2	131.1	1.44	0.07	0.00
1	101.1	2.17	0.24	0.00	2	137.1	1.60	0.01	0.00
1	102.1	2.17	0.24	0.00	2	138.1	1.60	0.01	0.00
1	103.1	2.17	0.24	0.00	2	139.1	1.60	0.01	0.00
1	104.1	2.17	0.24	0.00	2	140.1	1.60	0.01	0.00
1	105.1	2.17	0.24	0.00	2	141.1	1.60	0.01	0.00
1	106.1	2.17	0.12	0.01	2	163.1	1.71	0.00	0.00
1	107.1	2.17	0.23	0.00	2	164.1	1.71	0.00	0.00
1	108.1	2.17	0.22	0.00	2	168.1	1.66	0.00	0.00
1	109.1	2.17	0.16	0.00	2	169.1	1.66	0.00	0.00
1	110.1	2.17	0.16	0.00	2	170.1	1.66	0.00	0.00
1	111.1	2.17	0.16	0.00	2	171.1	2.01	0.05	0.01
1	112.1	2.17	0.17	0.00	2	175.1	1.87	0.02	0.00
1	113.1	2.17	0.17	0.00	2	177.1	1.90	0.04	0.00
1	114.1	2.17	0.15	0.01	2	178.1	1.90	0.05	0.00
1	115.1	2.17	0.18	0.00	2	182.1	1.98	0.08	0.00
1	116.1	2.17	0.23	0.00	2	184.1	1.98	0.08	0.00
1	118.1	2.17	0.37	0.02	2	185.1	1.98	0.09	0.00
1	119.1	2.17	0.36	0.02	2	186.1	1.98	0.10	0.00
1	120.1	2.17	0.28	0.00	2	187.1	1.98	0.09	0.00
1	121.1	2.17	0.34	0.01	2	190.1	1.98	0.09	0.00
1	123.1	1.98	0.07	0.00	2	191.1	1.98	0.10	0.00
1	126.1	2.36	0.35	0.00	2	77.2	1.63	0.00	0.00
1	127.1	2.17	0.24	0.00	2	78.2	1.63	0.00	0.01
1	128.1	2.36	0.46	0.00	2	79.2	1.63	0.00	0.01
1	129.1	2.17	0.22	0.00	2	83.2	1.60	0.01	0.00
1	130.1	2.36	0.37	0.00	2	97.2	1.42	0.08	0.00
1	131.1	2.17	0.21	0.00	2	98.2	1.42	0.08	0.00
1	133.1	2.17	0.19	0.00	2	99.2	1.42	0.08	0.00
1	134.1	2.17	0.25	0.00	2	182.2	1.62	0.01	0.00
1	137.1	2.17	0.25	0.00	2	83.3	1.48	0.03	0.00
1	144.1	1.23	0.22	0.00	2	97.3	1.47	0.06	0.00
1	146.1	1.23	0.22	0.00	2	98.3	1.47	0.07	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
2	99.3	1.47	0.06	0.00	4	199.1	2.04	0.19	0.01
2	116.3	1.53	0.03	0.00	4	200.1	2.04	0.18	0.01
2	182.3	1.56	0.02	0.00	4	201.1	2.04	0.19	0.01
4	30.1	1.64	0.00	0.00	4	202.1	2.04	0.19	0.01
4	31.1	1.64	0.00	0.00	4	203.1	2.04	0.17	0.01
4	34.1	1.64	0.00	0.00	4	207.1	1.97	0.07	0.00
4	35.1	1.64	0.01	0.00	4	213.1	1.93	0.06	0.00
4	36.1	1.64	0.00	0.00	4	214.1	1.93	0.06	0.00
4	37.1	1.64	0.00	0.00	4	215.1	2.20	0.26	0.00
4	38.1	1.64	0.00	0.00	4	217.1	2.27	0.34	0.00
4	39.1	1.64	0.00	0.00	4	72.2	1.54	0.03	0.00
4	40.1	1.64	0.01	0.00	4	100.2	1.70	0.00	0.00
4	41.1	1.64	0.00	0.00	4	101.2	1.70	0.00	0.00
4	42.1	1.64	0.00	0.00	4	102.2	1.70	0.00	0.00
4	43.1	1.64	0.00	0.00	4	104.2	1.70	0.00	0.00
4	44.1	1.64	0.01	0.00	4	105.2	1.70	0.00	0.00
4	68.1	1.63	0.00	0.00	4	106.2	1.71	0.00	0.00
4	69.1	1.63	0.00	0.00	4	107.2	1.71	0.00	0.00
4	70.1	1.63	0.01	0.00	4	108.2	1.71	0.00	0.00
4	71.1	1.63	0.01	0.00	4	109.2	1.71	0.00	0.00
4	75.1	1.62	0.01	0.00	4	110.2	1.71	0.00	0.00
4	82.1	1.58	0.02	0.00	4	111.2	1.71	0.00	0.00
4	91.1	2.05	0.19	0.01	4	112.2	1.71	0.00	0.00
4	102.1	2.08	0.11	0.00	4	114.2	1.64	0.00	0.00
4	104.1	2.08	0.10	0.00	4	192.2	1.78	0.00	0.00
4	105.1	2.08	0.11	0.00	4	194.2	1.78	0.00	0.00
4	106.1	2.08	0.11	0.00	4	195.2	1.78	0.00	0.00
4	107.1	2.08	0.11	0.00	4	196.2	1.78	0.00	0.00
4	108.1	2.08	0.11	0.00	4	197.2	1.78	0.01	0.00
4	109.1	2.08	0.11	0.00	4	215.2	1.64	0.00	0.00
4	110.1	2.08	0.11	0.00	4	217.2	1.64	0.00	0.00
4	111.1	2.08	0.11	0.00	4	101.3	1.66	0.00	0.00
4	112.1	2.08	0.11	0.00	4	102.3	1.61	0.01	0.00
4	144.1	1.92	0.04	0.00	4	104.3	1.61	0.01	0.00
4	146.1	1.92	0.04	0.00	4	105.3	1.61	0.01	0.00
4	147.1	1.92	0.05	0.00	4	106.3	1.57	0.02	0.00
4	148.1	1.92	0.05	0.00	4	107.3	1.57	0.02	0.00
4	149.1	1.92	0.05	0.00	4	108.3	1.57	0.02	0.00
4	151.1	1.92	0.05	0.00	4	109.3	1.57	0.02	0.00
4	152.1	1.92	0.05	0.00	4	110.3	1.57	0.02	0.00
4	153.1	1.92	0.05	0.00	4	111.3	1.57	0.01	0.00
4	154.1	1.92	0.05	0.00	4	112.3	1.57	0.01	0.00
4	189.1	2.04	0.12	0.00	4	114.3	1.71	0.00	0.00
4	192.1	2.04	0.12	0.00	4	215.3	1.71	0.00	0.00
4	193.1	2.04	0.12	0.00	4	217.3	1.71	0.00	0.00
4	194.1	2.04	0.13	0.00					
4	195.1	2.04	0.14	0.00					
4	196.1	2.04	0.16	0.00					
4	197.1	2.04	0.16	0.00					
4	198.1	2.04	0.17	0.01					

The next set of χ^2 tests and t-tests are for the different first person types in the heavy density buildings.

	All	Female	Male	Items	No Items	Large	Not Large
1st Person	4963	2691	2272	3343	1620	291	4672
Follower	6909	3842	3067	4612	2297	418	6491
Total	11872	6533	5339	7955	3917	709	11163
Expected		2731.1	2231.9	3325.5	1637.5	296.4	4666.6
Value		3801.9	3107.1	4629.5	2279.5	412.6	6496.4
Chi-Statistic		1.0	1.2	0.2	0.3	0.2	0.0
p-value		0.315	0.266	0.691	0.571	0.681	0.918
Pass	826	469	357	600	226	52	774
Other	4137	2222	1915	2743	1394	239	3898
Total	4963	2691	2272	3343	1620	291	4672
Expected		447.9	378.1	556.4	269.6	48.4	777.6
Value		2243.1	1893.9	2786.6	1350.4	242.6	3894.4
Chi-Statistic		1.2	1.4	4.1	8.5	0.3	0.0
p-value		0.274	0.234	0.043*	0.004*	0.574	0.889
Passed	988	601	387	693	295	39	949
Other	3975	2090	1885	2650	1325	252	3723
Total	4963	2691	2272	3343	1620	291	4672
Expected		535.7	452.3	665.5	322.5	57.9	930.1
Value		2155.3	1819.7	2677.5	1297.5	233.1	3741.9
Chi-Statistic		9.9	11.8	1.4	2.9	7.7	0.5
p-value		0.002*	6.0*10-4*	0.234	0.087	0.005*	0.488
Merge	278	136	142	165	113	22	256
Other	4685	2555	2130	3178	1507	269	4416
Total	4963	2691	2272	3343	1620	291	4672
Expected		150.7	127.3	187.3	90.7	16.3	261.7
Value		2540.3	2144.7	3155.7	1529.3	274.7	4410.3
Chi-Statistic		1.5	1.8	2.8	5.8	2.1	0.1
p-value		0.217	0.179	0.094	0.016*	0.146	0.717
Congestion	1299	688	611	867	432	74	1225
Other	3664	2003	1661	2476	1188	217	3447
Total	4963	2691	2272	3343	1620	291	4672
Expected		704.3	594.7	875.0	424.0	76.2	1222.8
Value		1986.7	1677.3	2468.0	1196.0	214.8	3449.2
Chi-Statistic		0.5	0.6	0.1	0.2	0.1	0.0
p-value		0.474	0.436	0.753	0.652	0.773	0.943
Free	1572	797	775	1018	554	104	1468
Other	3391	1894	1497	2325	1066	187	3204
Total	4963	2691	2272	3343	1620	291	4672
Expected		852.4	719.6	1058.9	513.1	92.2	1479.8
Value		1838.6	1552.4	2284.1	1106.9	198.8	3192.2
Chi-Statistic		5.3	6.2	2.3	4.8	2.2	0.1
p-value		0.022*	0.013*	0.129	0.029*	0.136	0.710

*Significant based on 95% confidence level

	All	Treads <2	Treads 2	Treads >2	Lane Flow	Unified Flow	Inner	Middle	Outer
1st Person	4963	2738	934	1291	939	4024	1330	893	2740
Follower	6909	5877	1021	11	1737	5172	2334	608	3967
Total	11872	8615	1955	1302	2676	9196	3664	1501	6707
Expected		3601	817	544	1119	3844	1532	627	2804
Value		5014	1138	758	1557	5352	2132	874	3903
Chi-Stat.		355.7	28.6	1760.3	49.6	14.4	45.6	193.1	2.5
p-value		2.4* 10^{-79}*	8.7* 10^{-8}*	0.000*	1.9* 10^{-12}*	1.5* 10^{-4}*	1.4* 10^{-11}*	6.8* 10^{-44}*	0.114
Pass	826	739	44	43	382	444	453	166	207
Other	4137	1999	890	1248	557	3580	877	727	2533
Total	4963	2738	934	1291	939	4024	1330	893	2740
Expected		456	155	215	156	670	221	149	456
Value		2282	779	1076	783	3354	1109	744	2284
Chi-Stat.		211.3	95.9	164.9	391.1	91.3	290.8	2.4	163.1
p-value		7.1* 10^{-48}*	1.2* 10^{-22}*	9.5* 10^{-38}*	4.7* 10^{-87}*	1.3* 10^{-21}*	3.3* 10^{-65}*	0.118	2.3* 10^{-37}*
Passed	988	798	104	86	439	549	215	136	637
Other	3975	1940	830	1205	500	3475	1115	757	2103
Total	4963	2738	934	1291	939	4024	1330	893	2740
Expected		545	186	257	187	801	265	178	545
Value		2193	748	1034	752	3223	1065	715	2195
Chi-Stat.		146.6	45.1	142.1	424.4	99.0	11.7	12.3	19.2
p-value		9.8* 10^{-34}*	1.9* 10^{-11}*	9.4* 10^{-33}*	2.7* 10^{-94}*	2.5* 10^{-23}*	6.3* 10^{-4}*	4.6* 10^{-4}*	1.2* 10^{-5}*
Merge	278	223	53	2	36	242	76	62	140
Other	4685	2515	881	1289	903	3782	1254	831	2600
Total	4963	2738	934	1291	939	4024	1330	893	2740
Expected		153	52	72	53	225	74	50	153
Value		2585	882	1219	886	3799	1256	843	2587
Chi-Stat.		33.5	0.0	72.4	5.5	1.3	0.0	3.0	1.3
p-value		7.2* 10^{-9}*	0.923	1.7* 10^{-17}*	0.018*	0.255	0.858	0.081	0.263
Congestion	1299	750	409	140	72	1227	327	221	751
Other	3664	1988	525	1151	867	2797	1003	672	1989
Total	4963	2738	934	1291	939	4024	1330	893	2740
Expected		717	244	338	246	1053	348	234	717
Value		2021	690	953	693	2971	982	659	2023
Chi-Stat.		2.1	150.0	157.0	166.4	38.8	1.7	0.9	2.2
p-value		0.147	1.7* 10^{-34}*	5.1* 10^{-36}*	4.5* 10^{-38}*	4.6* 10^{-10}*	0.188	0.332	0.141
Free	1572	228	324	1020	10	1562	259	308	1005
Other	3391	2510	610	271	929	2462	1071	585	1735
Total	4963	2738	934	1291	939	4024	1330	893	2740
Expected		867	296	409	297	1275	421	283	868
Value		1871	638	882	642	2749	909	610	1872
Chi-Stat.		689.6	3.9	1336.5	406.5	94.9	91.5	3.3	31.7
p-value		5.4* 10^{-152}*	0.048*	1.3* 10^{-292}*	2.1* 10^{-90}*	2.0* 10^{-22}*	1.1* 10^{-21}*	0.070	1.8* 10^{-8}*

*Significant based on 95% confidence level

	Trav. Dist.	Pre-Obs.		Trav. Dist.	Pre-Obs.		Trav. Dist.	Pre-Obs.
1st Per. Mean	66.72	190.70	Passed Mean	58.94	176.76	Cong. Mean	65.47	162.27
1st Per. St Dev	59.57	186.94	Passed St Dev	54.98	118.31	Cong. St Dev	58.04	125.95
Follow Mean	90.12	174.17	Other Mean	68.65	194.17	Other Mean	67.17	200.78
Follow St Dev	63.11	119.55	Other St Dev	60.51	200.25	Other St Dev	60.10	203.30
p-value	$1.9*10^{-92}$*	$4.4*10^{-8}$*	p-value	$1.2*10^{-6}$*	$4.2*10^{-4}$*	p-value	0.369	$2.6*10^{-15}$*
Pass Mean	67.65	166.63	Allow Mean	29.56	133.70	Free Mean	78.73	245.69
Pass St Dev	58.62	113.59	Allow St Dev	33.87	110.76	Free St Dev	63.96	273.58
Other Mean	66.53	195.51	Other Mean	68.93	194.09	Other Mean	61.15	165.21
Other St Dev	59.76	198.03	Other St Dev	60.04	189.98	Other St Dev	56.58	120.07
p-value	0.618	$9.4*10^{-9}$*	p-value	$3.0*10^{-52}$*	$9.7*10^{-16}$*	p-value	$2.1*10^{-20}$*	$4.1*10^{-28}$*

*Significant based on 95% confidence level

The last piece of analysis for Buildings 4, 5, and 8 involved calculating the R^2 value. The sum of the squares of the difference between the actual and predicted values was 1581.6. The sum of the square of the difference between the actual and average values was 15899.7. In the table, the predicted value is in s/m.

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	39.01	1.07	0.42	0.33	6	110.01	2.28	0.00	0.00
6	41.01	1.64	0.47	0.00	6	111.01	2.28	0.00	0.00
6	44.01	1.62	0.32	0.01	6	112.01	2.65	0.03	0.04
6	45.01	1.72	0.27	0.00	6	113.01	2.28	0.00	0.00
6	46.01	1.69	0.57	0.03	6	114.01	2.46	0.01	0.00
6	47.01	1.53	0.53	0.00	6	115.01	2.46	0.03	0.00
6	48.01	1.53	0.42	0.01	6	116.01	2.28	0.00	0.00
6	51.01	2.08	0.00	0.02	6	117.01	2.46	0.05	0.00
6	55.01	1.54	1.61	0.27	6	118.01	2.46	0.06	0.01
6	56.01	1.07	1.25	0.01	6	119.01	2.46	0.06	0.01
6	58.01	1.16	0.90	0.03	6	120.01	2.28	0.02	0.02
6	62.01	1.37	0.10	0.37	6	121.01	2.46	0.08	0.01
6	63.01	1.98	0.05	0.01	6	122.01	2.46	0.10	0.02
6	64.01	1.94	0.12	0.00	6	123.01	2.28	0.02	0.02
6	65.01	2.10	0.14	0.04	6	124.01	2.46	0.11	0.03
6	66.01	1.91	0.13	0.00	6	125.01	2.28	0.03	0.04
6	67.01	2.43	0.00	0.01	6	126.01	2.46	0.16	0.05
6	68.01	1.92	0.08	0.01	6	128.01	2.46	0.14	0.04
6	69.01	2.01	0.03	0.01	6	129.01	2.46	0.09	0.02
6	70.01	2.17	0.08	0.17	6	130.01	2.28	0.02	0.02
6	72.01	2.58	0.10	0.00	6	131.01	2.64	0.00	0.11
6	74.01	2.01	0.01	0.04	6	132.01	2.40	0.08	0.16
6	75.01	2.10	0.02	0.11	6	133.01	2.05	0.10	0.01
6	79.01	2.73	0.03	0.07	6	135.01	2.46	0.06	0.16
6	80.01	2.74	0.17	0.00	6	136.01	2.05	0.06	0.00
6	81.01	2.46	0.06	0.01	6	137.01	2.05	0.04	0.00
6	82.01	2.46	0.01	0.01	6	138.01	2.05	0.08	0.00
6	83.01	2.46	0.00	0.02	6	139.01	2.05	0.07	0.00
6	84.01	2.46	0.02	0.00	6	140.01	2.05	0.07	0.00
6	85.01	2.46	0.00	0.01	6	141.01	2.05	0.08	0.00
6	86.01	2.42	0.01	0.00	6	142.01	1.97	0.27	0.04
6	87.01	2.46	0.01	0.01	6	143.01	2.05	0.11	0.01
6	88.01	2.39	0.00	0.01	6	144.01	2.24	0.12	0.09
6	89.01	2.39	0.01	0.00	6	145.01	2.02	0.17	0.02
6	90.01	2.32	0.01	0.00	6	146.01	1.88	0.26	0.01
6	91.01	2.37	0.01	0.00	6	147.01	1.88	0.26	0.01
6	92.01	2.37	0.00	0.00	6	148.01	1.88	0.31	0.02
6	93.01	2.31	0.04	0.06	6	149.01	1.81	0.19	0.00
6	94.01	2.58	0.03	0.01	6	150.01	1.88	0.09	0.01
6	95.01	2.39	0.01	0.04	6	151.01	1.85	0.22	0.00
6	96.01	2.20	0.01	0.00	6	152.01	1.88	0.09	0.01
6	97.01	2.20	0.02	0.00	6	153.01	1.88	0.21	0.00
6	99.01	2.20	0.03	0.01	6	154.01	2.06	0.01	0.02
6	100.01	2.20	0.27	0.19	6	155.01	2.19	0.01	0.00
6	101.01	1.74	0.32	0.00	6	156.01	2.19	0.00	0.01
6	102.01	1.97	0.10	0.00	6	159.01	2.19	0.00	0.00
6	106.01	1.97	0.27	0.71	6	160.01	1.85	0.02	0.09
6	107.01	1.82	0.03	0.41	6	161.01	1.82	0.00	0.24
6	108.01	2.40	0.00	0.01	6	162.01	2.31	0.00	0.01
6	109.01	2.28	0.01	0.01	6	163.01	2.31	0.01	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	164.01	2.04	0.02	0.16	6	214.01	3.04	0.23	0.08
6	165.01	2.44	0.01	0.00	6	215.01	3.04	0.46	0.01
6	166.01	1.87	0.01	0.29	6	216.01	3.04	0.45	0.01
6	167.01	2.41	0.00	0.03	6	217.01	3.04	0.44	0.01
6	168.01	2.41	0.00	0.02	6	218.01	3.04	0.48	0.00
6	169.01	2.41	0.00	0.02	6	219.01	3.04	0.41	0.01
6	170.01	2.41	0.02	0.06	6	220.01	3.04	0.48	0.00
6	171.01	2.41	0.02	0.06	6	221.01	3.04	0.67	0.00
6	172.01	2.41	0.02	0.06	6	222.01	3.04	0.43	0.01
6	173.01	2.41	0.02	0.07	6	223.01	3.04	0.66	0.00
6	174.01	2.41	0.04	0.10	6	224.01	3.04	0.63	0.00
6	175.01	2.41	0.01	0.04	6	225.01	3.04	0.66	0.00
6	176.01	2.41	0.01	0.06	6	226.01	2.90	0.93	0.12
6	177.01	2.41	0.01	0.05	6	227.01	3.25	0.91	0.00
6	178.01	2.41	0.01	0.04	6	228.01	3.08	0.85	0.02
6	179.01	2.41	0.01	0.04	6	229.01	3.21	0.92	0.00
6	180.01	2.41	0.00	0.03	6	230.01	3.21	0.97	0.00
6	181.01	2.41	0.01	0.04	6	231.01	3.21	0.79	0.00
6	182.01	2.41	0.00	0.03	6	232.01	3.21	0.68	0.01
6	183.01	2.37	0.00	0.02	6	233.01	3.21	0.43	0.07
6	184.01	2.23	0.00	0.00	6	234.01	3.21	0.01	0.71
6	185.01	2.23	0.00	0.00	6	235.01	3.21	0.00	0.77
6	186.01	2.23	0.03	0.01	6	236.01	3.21	0.01	0.71
6	187.01	2.23	0.04	0.02	6	237.01	3.21	0.00	0.80
6	188.01	2.23	0.04	0.02	6	238.01	3.21	0.00	0.82
6	189.01	2.23	0.04	0.02	6	239.01	3.21	0.00	0.83
6	190.01	2.23	0.03	0.01	6	240.01	3.21	0.00	0.83
6	191.01	2.23	0.00	0.00	6	241.01	3.21	0.00	0.86
6	192.01	2.23	0.01	0.00	6	242.01	3.21	0.01	1.08
6	193.01	2.23	0.01	0.03	6	243.01	3.21	0.00	0.83
6	194.01	2.23	0.00	0.01	6	244.01	3.21	0.00	0.78
6	195.01	2.23	0.00	0.00	6	245.01	3.21	0.00	0.82
6	196.01	2.23	0.00	0.00	6	246.01	3.21	0.00	0.87
6	197.01	2.23	0.00	0.00	6	247.01	3.21	0.00	0.82
6	198.01	2.23	0.01	0.00	6	248.01	3.21	0.00	0.83
6	199.01	2.23	0.00	0.00	6	249.01	3.21	0.00	0.82
6	200.01	2.23	0.00	0.00	6	250.01	3.21	0.00	0.76
6	201.01	2.23	0.00	0.00	6	251.01	3.21	0.01	0.64
6	202.01	2.23	0.00	0.00	6	252.01	3.21	0.00	0.78
6	203.01	2.23	0.00	0.00	6	253.01	3.21	0.00	0.79
6	204.01	2.23	0.00	0.00	6	254.01	3.21	0.00	0.81
6	205.01	2.23	0.01	0.03	6	255.01	3.21	0.00	0.87
6	206.01	2.23	0.00	0.01	6	256.01	3.21	0.00	0.75
6	207.01	2.23	0.00	0.00	6	257.01	3.21	0.01	0.98
6	208.01	2.23	0.70	0.80	6	258.01	3.21	0.00	0.83
6	209.01	2.23	0.60	0.69	6	259.01	3.21	0.00	0.80
6	210.01	2.23	0.65	0.74	6	260.01	3.21	0.00	0.86
6	211.01	2.23	0.59	0.68	6	261.01	3.21	0.00	0.89
6	212.01	2.23	0.57	0.67	6	262.01	3.21	0.00	0.83
6	213.01	2.23	0.48	0.56	6	263.01	3.21	0.00	0.89

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	264.01	3.21	0.00	0.78	6	314.01	2.92	0.30	0.01
6	265.01	3.21	0.01	0.66	6	315.01	2.45	0.03	0.00
6	266.01	3.21	0.01	0.67	6	316.01	2.46	0.02	0.00
6	267.01	3.21	0.02	0.60	6	317.01	2.40	0.01	0.00
6	268.01	3.21	0.01	0.64	6	318.01	2.58	0.10	0.00
6	269.01	3.21	0.02	0.58	6	319.01	2.57	0.02	0.02
6	270.01	3.21	0.08	0.41	6	320.01	2.38	0.08	0.03
6	271.01	3.21	0.10	0.36	6	321.01	2.46	0.06	0.01
6	272.01	3.21	0.12	0.33	6	322.01	2.54	0.01	0.02
6	273.01	3.21	0.14	0.30	6	323.01	2.54	0.03	0.01
6	274.01	3.21	0.11	0.35	6	324.01	2.54	0.03	0.00
6	275.01	3.30	0.12	0.44	6	325.01	2.54	0.04	0.00
6	276.01	3.11	0.08	0.29	6	326.01	2.54	0.04	0.00
6	277.01	2.64	0.10	0.00	6	327.01	2.54	0.05	0.00
6	278.01	2.58	0.06	0.00	6	328.01	2.54	0.05	0.00
6	279.01	2.64	0.12	0.00	6	329.01	2.54	0.03	0.00
6	280.01	2.58	0.03	0.01	6	330.01	2.54	0.05	0.00
6	281.01	2.64	0.09	0.00	6	331.01	2.54	0.04	0.00
6	282.01	2.64	0.12	0.00	6	332.01	2.54	0.01	0.02
6	283.01	2.58	0.02	0.02	6	333.01	2.54	0.00	0.04
6	284.01	2.58	0.02	0.02	6	334.01	2.54	0.02	0.01
6	285.01	2.64	0.10	0.00	6	335.01	2.54	0.02	0.01
6	286.01	2.58	0.01	0.04	6	336.01	2.54	0.02	0.01
6	287.01	3.17	0.00	0.72	6	337.01	2.54	0.01	0.03
6	288.01	2.32	0.01	0.00	6	338.01	2.54	0.01	0.02
6	289.01	2.32	0.01	0.00	6	339.01	2.54	0.01	0.03
6	290.01	2.32	0.00	0.00	6	340.01	2.54	0.01	0.02
6	291.01	2.32	0.00	0.00	6	341.01	2.54	0.01	0.12
6	292.01	2.32	0.00	0.00	6	342.01	2.54	0.00	0.09
6	293.01	2.32	0.00	0.00	6	343.01	2.54	0.00	0.09
6	294.01	2.32	0.00	0.00	6	344.01	2.54	0.00	0.09
6	295.01	2.32	0.00	0.00	6	345.01	2.54	0.01	0.03
6	296.01	2.32	0.01	0.02	6	346.01	2.54	0.00	0.08
6	297.01	2.32	0.00	0.00	6	347.01	2.64	0.00	0.18
6	298.01	2.32	0.01	0.01	6	348.01	2.22	0.02	0.01
6	299.01	2.32	0.00	0.00	6	349.01	2.22	0.04	0.01
6	300.01	2.32	0.00	0.00	6	350.01	2.41	0.05	0.12
6	301.01	2.18	0.00	0.01	6	351.01	2.06	0.07	0.00
6	302.01	2.26	0.00	0.00	6	352.01	2.06	0.09	0.00
6	303.01	2.26	0.04	0.02	6	353.01	2.06	0.06	0.00
6	304.01	2.26	0.02	0.01	6	354.01	2.04	0.05	0.00
6	305.01	2.92	0.24	0.02	6	355.01	2.06	0.11	0.01
6	306.01	2.26	0.01	0.00	6	356.01	2.06	0.10	0.01
6	307.01	2.20	0.00	0.00	6	357.01	2.22	0.00	0.00
6	308.01	2.25	0.05	0.07	6	358.01	2.04	0.06	0.00
6	309.01	2.60	0.03	0.02	6	359.01	2.22	0.01	0.00
6	310.01	2.40	0.00	0.00	6	360.01	2.04	0.05	0.00
6	311.01	2.46	0.40	0.21	6	361.01	2.22	0.02	0.00
6	312.01	2.92	0.31	0.01	6	362.01	2.04	0.01	0.02
6	313.01	2.92	0.30	0.01	6	363.01	2.50	0.02	0.11

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	364.01	2.04	0.02	0.01	6	414.01	1.97	0.03	0.02
6	365.01	2.04	0.01	0.02	6	415.01	2.13	0.04	0.00
6	366.01	2.04	0.03	0.01	6	416.01	2.07	0.30	0.59
6	367.01	2.04	0.01	0.02	6	417.01	2.84	0.28	0.00
6	368.01	2.04	0.03	0.00	6	418.01	2.84	0.05	0.11
6	369.01	2.04	0.03	0.00	6	419.01	2.84	0.09	0.06
6	370.01	2.04	0.03	0.01	6	420.01	2.84	0.06	0.09
6	371.01	2.04	0.03	0.01	6	421.01	2.84	0.03	0.14
6	372.01	2.04	0.02	0.01	6	422.01	2.84	0.03	0.14
6	373.01	2.04	0.06	0.00	6	423.01	2.84	0.04	0.13
6	374.01	2.04	0.03	0.00	6	424.01	2.84	0.02	0.16
6	375.01	2.04	0.06	0.00	6	425.01	2.84	0.03	0.14
6	376.01	2.04	0.04	0.00	6	426.01	2.23	0.34	0.41
6	377.01	2.04	0.07	0.00	6	427.01	2.88	0.36	0.00
6	378.01	2.04	0.10	0.00	6	428.01	2.84	0.00	0.27
6	379.01	2.04	0.05	0.00	6	429.01	2.84	0.03	0.14
6	380.01	2.04	0.09	0.00	6	430.01	2.84	0.00	0.24
6	381.01	2.04	0.10	0.01	6	431.01	2.84	0.00	0.23
6	382.01	2.04	0.08	0.00	6	432.01	2.87	0.00	0.26
6	383.01	1.56	0.21	0.07	6	433.01	2.36	0.01	0.00
6	384.01	2.09	0.30	0.12	6	434.01	2.36	0.00	0.00
6	385.01	1.74	0.28	0.00	6	435.01	2.29	0.00	0.00
6	386.01	1.55	0.12	0.15	6	436.01	2.84	0.00	0.24
6	387.01	1.94	0.12	0.00	6	437.01	2.67	0.00	0.15
6	388.01	1.94	0.09	0.00	6	438.01	2.72	0.09	0.02
6	389.01	2.62	0.09	0.00	6	439.01	2.59	0.01	0.04
6	390.01	1.94	0.00	0.08	6	440.01	2.47	0.09	0.02
6	391.01	1.94	0.01	0.05	6	441.01	2.59	0.03	0.02
6	392.01	1.84	0.11	0.60	6	442.01	2.59	0.02	0.02
6	393.01	2.62	0.02	0.04	6	443.01	2.59	0.06	0.00
6	394.01	2.62	0.07	0.00	6	444.01	2.59	0.07	0.00
6	395.01	2.62	0.08	0.00	6	445.01	2.47	0.09	0.01
6	396.01	2.62	0.06	0.01	6	446.01	2.59	0.05	0.00
6	397.01	2.62	0.06	0.01	6	447.01	2.59	0.07	0.00
6	398.01	2.62	0.01	0.05	6	448.01	2.59	0.07	0.00
6	399.01	1.66	0.00	0.32	6	449.01	2.59	0.08	0.00
6	400.01	2.22	0.01	0.00	6	450.01	2.59	0.08	0.00
6	401.01	2.22	0.01	0.00	6	451.01	2.59	0.02	0.02
6	402.01	2.22	0.00	0.00	6	452.01	2.59	0.02	0.03
6	403.01	2.22	0.04	0.02	6	453.01	2.59	0.09	0.00
6	404.01	2.05	0.35	0.12	6	454.01	2.59	0.07	0.00
6	405.01	2.34	0.17	0.21	6	455.01	2.59	0.25	0.04
6	406.01	2.16	0.26	0.14	6	456.01	2.52	0.44	0.19
6	407.01	1.78	0.23	0.00	6	457.01	2.59	0.25	0.04
6	408.01	1.78	0.24	0.00	6	458.01	2.95	0.68	0.03
6	409.01	1.82	0.26	0.00	6	459.01	2.95	0.99	0.11
6	410.01	1.69	0.46	0.01	6	460.01	2.95	0.68	0.03
6	411.01	1.51	0.52	0.00	6	461.01	2.95	0.64	0.02
6	412.01	1.56	0.03	0.32	6	462.01	3.03	0.54	0.00
6	413.01	2.13	0.03	0.00	6	463.01	2.84	0.76	0.11

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	464.01	3.16	0.54	0.02	6	62.02	1.02	0.21	0.66
6	465.01	3.02	0.54	0.00	6	63.02	1.84	0.31	0.01
6	466.01	3.02	0.54	0.00	6	64.02	1.81	0.32	0.01
6	467.01	2.79	0.42	0.02	6	65.02	1.72	0.32	0.00
6	468.01	3.07	0.86	0.02	6	66.02	1.72	0.31	0.00
6	469.01	3.22	0.79	0.00	6	68.02	1.89	0.26	0.01
6	470.01	3.22	0.74	0.00	6	69.02	1.78	0.25	0.00
6	471.01	2.94	0.34	0.00	6	70.02	2.03	0.12	0.01
6	472.01	2.94	0.37	0.00	6	72.02	1.94	0.13	0.00
6	473.01	2.94	0.24	0.02	6	74.02	1.92	0.19	0.00
6	474.01	3.22	0.75	0.00	6	75.02	1.84	0.22	0.00
6	475.01	3.22	0.54	0.04	6	81.02	2.02	0.15	0.01
6	476.01	2.94	0.09	0.12	6	82.02	1.90	0.12	0.00
6	477.01	3.22	0.65	0.01	6	83.02	2.07	0.11	0.01
6	478.01	3.22	0.59	0.02	6	87.02	1.98	0.22	0.03
6	479.01	2.94	0.05	0.76	6	88.02	1.78	0.22	0.00
6	480.01	2.94	0.03	0.70	6	90.02	2.02	0.06	0.00
6	481.01	3.06	0.58	0.00	6	91.02	1.84	0.18	0.00
6	482.01	2.87	0.27	0.00	6	92.02	1.87	0.16	0.00
6	483.01	3.05	0.91	0.04	6	94.02	1.90	0.76	0.23
6	484.01	3.05	0.69	0.00	6	95.02	1.56	0.49	0.00
6	485.01	2.90	0.68	0.04	6	96.02	1.59	0.57	0.00
6	486.01	3.05	0.83	0.02	6	97.02	1.59	0.50	0.00
6	487.01	3.11	0.67	0.00	6	99.02	1.59	0.40	0.00
6	488.01	3.11	0.72	0.00	6	100.02	1.64	0.26	0.02
6	489.01	3.11	0.79	0.00	6	101.02	1.78	0.27	0.00
6	490.01	3.02	4.11	1.69	6	102.02	1.78	0.27	0.00
6	491.01	3.11	4.17	1.48	6	106.02	1.99	0.04	0.01
6	492.01	4.32	4.11	0.00	6	108.02	1.73	0.18	0.02
6	493.01	4.43	4.14	0.01	6	109.02	1.86	0.11	0.01
6	494.01	4.13	3.59	0.00	6	110.02	1.86	0.11	0.01
6	495.01	4.16	3.20	0.01	6	111.02	1.86	0.11	0.01
6	496.01	4.08	2.94	0.01	6	113.02	1.73	0.20	0.01
6	497.01	4.31	3.50	0.02	6	114.02	1.86	0.08	0.02
6	498.01	2.82	0.11	0.04	6	115.02	1.86	0.11	0.01
6	499.01	4.16	3.52	0.00	6	116.02	1.73	0.16	0.02
6	500.01	4.23	3.19	0.02	6	117.02	1.86	0.14	0.00
6	501.01	4.08	3.42	0.00	6	118.02	1.91	0.10	0.00
6	502.01	4.08	3.71	0.02	6	119.02	1.86	0.13	0.00
6	503.01	4.08	3.60	0.01	6	120.02	1.88	0.12	0.00
6	504.01	4.08	3.84	0.03	6	121.02	1.92	0.10	0.00
6	505.01	3.80	1.43	0.10	6	122.02	1.98	0.09	0.00
6	506.01	4.16	3.36	0.00	6	123.02	1.88	0.16	0.00
6	507.01	4.12	2.61	0.05	6	124.02	1.98	0.10	0.00
6	508.01	3.80	0.75	0.41	6	125.02	1.94	0.14	0.00
6	509.01	2.98	0.56	0.00	6	126.02	1.98	0.10	0.00
6	510.01	3.95	0.47	0.95	6	128.02	1.91	0.12	0.00
6	511.01	3.02	2.28	0.61	6	129.02	1.80	0.12	0.02
6	512.01	2.39	0.03	0.08	6	130.02	1.94	0.12	0.00
6	513.01	1.89	1.14	0.44	6	131.02	1.94	0.06	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	135.02	1.95	0.02	0.04	6	198.02	2.59	0.04	0.01
6	138.02	2.14	0.01	0.00	6	199.02	2.59	0.04	0.01
6	140.02	2.25	0.01	0.00	6	200.02	2.76	0.05	0.07
6	141.02	2.30	0.00	0.00	6	201.02	2.53	0.02	0.01
6	142.02	2.24	0.00	0.00	6	202.02	2.60	0.03	0.02
6	143.02	2.24	0.00	0.00	6	203.02	2.47	0.05	0.00
6	144.02	2.24	0.00	0.00	6	204.02	2.47	0.03	0.00
6	145.02	2.24	0.00	0.00	6	208.02	2.61	0.13	0.00
6	146.02	2.24	0.00	0.00	6	209.02	2.65	0.13	0.00
6	147.02	2.24	0.00	0.00	6	211.02	2.84	0.25	0.00
6	148.02	2.14	0.03	0.00	6	212.02	2.56	0.30	0.07
6	149.02	2.10	0.06	0.00	6	213.02	2.57	0.03	0.01
6	150.02	2.28	0.01	0.01	6	214.02	2.83	0.36	0.00
6	151.02	2.15	0.01	0.00	6	215.02	3.00	0.19	0.07
6	153.02	2.14	0.03	0.00	6	216.02	2.75	0.09	0.03
6	155.02	2.39	0.01	0.00	6	219.02	2.58	0.17	0.02
6	156.02	2.40	0.01	0.00	6	220.02	2.58	0.14	0.01
6	159.02	2.40	0.01	0.00	6	222.02	2.58	0.19	0.02
6	160.02	2.20	0.00	0.00	6	223.02	2.94	0.41	0.00
6	163.02	2.36	0.00	0.00	6	224.02	2.84	0.21	0.01
6	165.02	2.34	0.01	0.00	6	225.02	2.77	0.16	0.01
6	166.02	2.55	0.02	0.02	6	228.02	2.79	0.36	0.01
6	169.02	2.51	0.04	0.00	6	229.02	2.89	0.31	0.00
6	171.02	2.57	0.08	0.00	6	230.02	2.89	0.33	0.00
6	172.02	2.57	0.08	0.00	6	231.02	2.89	0.37	0.00
6	173.02	2.57	0.11	0.00	6	232.02	2.89	0.36	0.00
6	174.02	2.57	0.12	0.00	6	233.02	2.89	0.47	0.01
6	175.02	2.57	0.11	0.00	6	234.02	2.89	1.12	0.21
6	176.02	2.57	0.09	0.00	6	235.02	2.89	1.15	0.23
6	177.02	2.57	0.11	0.00	6	236.02	2.89	1.11	0.21
6	178.02	2.57	0.10	0.00	6	237.02	2.89	1.22	0.26
6	179.02	2.57	0.08	0.00	6	238.02	2.89	1.21	0.25
6	180.02	2.57	0.09	0.00	6	239.02	2.80	0.74	0.12
6	181.02	2.57	0.09	0.00	6	240.02	3.04	1.22	0.13
6	182.02	2.57	0.09	0.00	6	241.02	3.15	0.70	0.00
6	183.02	2.60	0.09	0.00	6	242.02	2.86	1.13	0.24
6	184.02	2.59	0.08	0.00	6	243.02	3.40	1.15	0.00
6	185.02	2.59	0.08	0.00	6	244.02	3.47	0.84	0.07
6	186.02	2.59	0.13	0.00	6	245.02	3.29	0.79	0.01
6	187.02	2.59	0.15	0.01	6	246.02	3.49	0.78	0.10
6	188.02	2.59	0.11	0.00	6	247.02	2.96	1.51	0.32
6	189.02	2.59	0.10	0.00	6	248.02	3.17	0.69	0.00
6	190.02	2.59	0.09	0.00	6	249.02	3.17	0.64	0.01
6	191.02	2.59	0.08	0.00	6	250.02	3.17	0.79	0.00
6	192.02	2.59	0.09	0.00	6	251.02	3.17	0.58	0.02
6	193.02	2.59	0.07	0.00	6	252.02	3.17	0.61	0.01
6	194.02	2.59	0.08	0.00	6	253.02	3.17	0.61	0.01
6	195.02	2.59	0.04	0.01	6	254.02	3.17	0.64	0.01
6	196.02	2.59	0.05	0.01	6	255.02	3.24	0.70	0.01
6	197.02	2.59	0.04	0.01	6	256.02	3.26	0.36	0.14

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	257.02	3.46	0.68	0.12	6	307.02	2.46	0.04	0.00
6	258.02	3.54	0.91	0.09	6	308.02	2.69	0.04	0.04
6	259.02	3.21	0.83	0.00	6	309.02	2.34	0.00	0.00
6	260.02	3.35	0.85	0.02	6	310.02	2.60	0.02	0.03
6	261.02	3.20	0.85	0.00	6	311.02	2.64	0.16	0.00
6	262.02	3.20	0.77	0.00	6	312.02	2.69	0.07	0.02
6	263.02	3.20	0.89	0.00	6	313.02	2.69	0.17	0.00
6	264.02	3.20	0.79	0.00	6	314.02	2.69	0.15	0.00
6	265.02	3.20	0.82	0.00	6	315.02	2.43	0.04	0.00
6	266.02	3.20	0.82	0.00	6	316.02	2.37	0.02	0.00
6	267.02	3.20	0.73	0.00	6	317.02	2.42	0.01	0.00
6	268.02	3.20	0.82	0.00	6	318.02	2.62	0.05	0.01
6	269.02	3.20	0.75	0.00	6	319.02	2.47	0.05	0.00
6	270.02	3.20	0.82	0.00	6	320.02	2.51	0.06	0.00
6	271.02	3.20	0.73	0.00	6	321.02	2.50	0.04	0.00
6	272.02	3.20	0.73	0.00	6	322.02	2.50	0.08	0.00
6	273.02	3.20	0.75	0.00	6	323.02	2.50	0.08	0.00
6	274.02	3.20	0.74	0.00	6	324.02	2.50	0.08	0.00
6	275.02	3.20	0.77	0.00	6	325.02	2.50	0.06	0.00
6	276.02	3.20	0.74	0.00	6	326.02	2.50	0.07	0.00
6	277.02	3.20	0.80	0.00	6	327.02	2.50	0.07	0.00
6	278.02	3.20	0.80	0.00	6	328.02	2.50	0.07	0.00
6	279.02	3.09	0.77	0.01	6	329.02	2.50	0.08	0.00
6	280.02	3.29	0.85	0.01	6	330.02	2.50	0.08	0.00
6	281.02	3.17	0.75	0.00	6	331.02	2.50	0.08	0.01
6	282.02	3.17	0.74	0.00	6	332.02	2.50	0.10	0.01
6	283.02	3.21	0.83	0.00	6	333.02	2.50	0.11	0.01
6	284.02	3.21	0.84	0.00	6	334.02	2.50	0.09	0.01
6	285.02	3.17	0.38	0.07	6	335.02	2.50	0.10	0.01
6	286.02	3.21	0.84	0.00	6	336.02	2.50	0.07	0.00
6	287.02	3.14	1.05	0.03	6	337.02	2.50	0.09	0.01
6	288.02	3.25	0.62	0.03	6	338.02	2.50	0.10	0.01
6	289.02	3.05	0.53	0.00	6	339.02	2.50	0.09	0.01
6	290.02	3.02	0.53	0.00	6	340.02	2.50	0.10	0.01
6	291.02	3.22	0.60	0.03	6	341.02	2.38	0.03	0.01
6	292.02	2.92	0.02	0.57	6	342.02	2.50	0.10	0.01
6	293.02	2.93	0.52	0.01	6	343.02	2.50	0.10	0.01
6	294.02	3.00	0.42	0.00	6	344.02	2.50	0.09	0.01
6	295.02	3.13	0.89	0.01	6	345.02	2.50	0.06	0.00
6	296.02	2.87	0.04	0.15	6	346.02	2.64	0.09	0.00
6	297.02	2.94	0.25	0.02	6	347.02	2.60	0.14	0.00
6	298.02	2.38	0.04	0.01	6	348.02	2.65	0.19	0.01
6	299.02	2.66	1.80	0.93	6	349.02	2.55	0.23	0.05
6	300.02	2.48	0.03	0.00	6	350.02	2.38	0.05	0.02
6	301.02	2.48	0.03	0.00	6	351.02	2.56	0.08	0.00
6	302.02	2.48	0.02	0.00	6	352.02	2.38	0.07	0.03
6	303.02	2.48	0.00	0.03	6	353.02	2.56	0.07	0.00
6	304.02	2.48	0.02	0.00	6	354.02	2.56	0.06	0.00
6	305.02	2.69	0.03	0.05	6	355.02	2.56	0.08	0.00
6	306.02	2.48	0.02	0.00	6	356.02	2.56	0.07	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	357.02	2.77	0.12	0.02	6	407.02	1.52	0.67	0.00
6	358.02	2.56	0.07	0.00	6	408.02	1.52	0.59	0.00
6	359.02	2.77	0.17	0.00	6	409.02	1.66	0.25	0.02
6	360.02	2.77	0.12	0.02	6	410.02	1.53	0.35	0.03
6	361.02	2.77	0.15	0.01	6	411.02	1.64	0.24	0.02
6	362.02	2.77	0.11	0.02	6	412.02	1.73	0.01	0.22
6	363.02	2.77	0.15	0.01	6	413.02	2.19	0.01	0.00
6	364.02	2.55	0.04	0.00	6	414.02	2.19	0.02	0.00
6	365.02	2.50	0.07	0.00	6	415.02	2.19	0.01	0.00
6	366.02	2.55	0.04	0.00	6	416.02	2.19	0.01	0.00
6	367.02	2.55	0.08	0.00	6	417.02	2.19	0.02	0.00
6	368.02	2.55	0.09	0.00	6	418.02	2.19	0.01	0.00
6	369.02	2.55	0.09	0.00	6	419.02	2.19	0.01	0.00
6	370.02	2.55	0.09	0.00	6	420.02	2.19	0.01	0.00
6	371.02	2.55	0.07	0.00	6	421.02	2.04	0.01	0.02
6	372.02	2.55	0.04	0.00	6	422.02	2.21	0.01	0.00
6	373.02	2.55	0.09	0.00	6	423.02	2.30	0.01	0.01
6	374.02	2.55	0.03	0.01	6	424.02	2.17	0.01	0.00
6	375.02	2.43	0.00	0.02	6	425.02	2.21	0.01	0.00
6	376.02	2.69	0.03	0.05	6	426.02	2.16	0.34	0.51
6	377.02	2.66	0.10	0.00	6	427.02	2.87	0.31	0.00
6	378.02	2.46	0.03	0.11	6	428.02	2.11	0.01	0.00
6	379.02	2.63	0.00	0.08	6	429.02	2.21	0.01	0.00
6	380.02	2.51	0.00	0.07	6	430.02	1.97	0.02	0.03
6	381.02	2.16	0.01	0.00	6	431.02	2.14	0.02	0.00
6	382.02	2.21	0.02	0.00	6	432.02	2.14	0.03	0.00
6	383.02	2.34	0.01	0.00	6	433.02	2.14	0.01	0.00
6	384.02	2.04	0.00	0.06	6	434.02	2.14	0.00	0.01
6	385.02	2.28	0.01	0.01	6	435.02	2.29	0.00	0.00
6	386.02	2.14	0.00	0.02	6	436.02	2.23	0.00	0.00
6	387.02	2.35	0.00	0.00	6	437.02	2.29	0.00	0.00
6	388.02	2.10	0.04	0.00	6	438.02	2.02	0.03	0.19
6	389.02	2.37	0.00	0.00	6	439.02	2.11	0.26	0.48
6	390.02	2.10	0.06	0.00	6	440.02	2.24	0.27	0.32
6	391.02	2.10	0.06	0.00	6	441.02	2.80	0.22	0.00
6	392.02	2.32	0.19	0.16	6	442.02	2.75	0.23	0.00
6	393.02	2.03	0.04	0.00	6	443.02	2.77	0.26	0.00
6	394.02	2.73	0.10	0.01	6	444.02	2.77	0.20	0.00
6	395.02	2.14	0.02	0.00	6	445.02	2.77	0.22	0.00
6	396.02	2.16	0.01	0.00	6	446.02	2.77	0.22	0.00
6	397.02	2.23	0.07	0.04	6	447.02	2.77	0.21	0.00
6	398.02	2.03	0.13	0.01	6	448.02	2.77	0.23	0.00
6	399.02	1.96	0.34	0.07	6	449.02	2.77	0.24	0.00
6	400.02	1.64	0.36	0.00	6	450.02	2.77	0.25	0.00
6	401.02	1.69	0.36	0.00	6	451.02	2.77	0.33	0.01
6	402.02	1.62	0.38	0.00	6	452.02	2.77	0.33	0.01
6	403.02	1.59	0.62	0.01	6	453.02	2.85	0.31	0.00
6	404.02	1.59	0.48	0.00	6	454.02	2.60	0.23	0.03
6	405.02	1.46	0.40	0.04	6	455.02	2.84	0.25	0.00
6	406.02	1.60	0.52	0.00	6	456.02	2.65	0.26	0.02

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	457.02	2.77	0.16	0.01	6	507.02	2.60	0.17	0.01
6	458.02	2.80	0.31	0.00	6	508.02	2.51	0.37	0.15
6	459.02	2.80	0.15	0.02	6	509.02	2.71	0.58	0.12
6	460.02	2.80	0.28	0.00	6	510.02	3.05	0.44	0.01
6	461.02	2.80	0.28	0.00	6	511.02	2.66	0.55	0.14
6	462.02	2.68	0.27	0.02	6	512.02	3.25	0.08	1.56
6	463.02	2.70	0.29	0.02	6	65.03	0.99	0.52	0.34
6	464.02	2.83	0.32	0.00	6	66.03	1.57	0.49	0.00
6	465.02	2.81	0.25	0.00	6	94.03	1.99	0.59	0.21
6	466.02	2.81	0.23	0.00	6	95.03	1.52	0.57	0.00
6	467.02	2.81	0.23	0.00	6	96.03	1.52	0.56	0.00
6	468.02	2.81	0.20	0.00	6	97.03	1.57	0.63	0.01
6	469.02	2.81	0.22	0.00	6	99.03	1.50	0.70	0.00
6	470.02	2.81	0.19	0.01	6	106.03	1.59	0.12	0.12
6	471.02	2.81	0.04	0.10	6	108.03	1.62	0.43	0.00
6	472.02	2.81	0.15	0.02	6	109.03	1.64	0.46	0.00
6	473.02	2.62	0.11	0.43	6	110.03	1.60	0.47	0.00
6	474.02	2.81	0.17	0.01	6	111.03	1.60	0.45	0.00
6	475.02	2.81	0.12	0.03	6	113.03	1.76	0.28	0.00
6	476.02	1.96	0.04	0.02	6	114.03	1.64	0.46	0.00
6	477.02	2.81	0.10	0.04	6	116.03	1.76	0.29	0.00
6	478.02	2.86	0.12	0.05	6	117.03	1.84	0.10	0.02
6	479.02	1.96	0.00	0.15	6	118.03	1.87	0.23	0.00
6	480.02	1.96	0.01	0.19	6	119.03	1.89	0.18	0.00
6	481.02	2.64	0.15	0.00	6	120.03	1.76	0.28	0.00
6	482.02	1.96	0.00	0.14	6	123.03	1.82	0.21	0.00
6	483.02	2.64	0.24	0.02	6	125.03	1.78	0.33	0.00
6	484.02	2.64	0.24	0.02	6	128.03	1.92	0.22	0.01
6	485.02	2.64	0.35	0.06	6	129.03	1.86	0.26	0.01
6	486.02	2.64	0.29	0.04	6	130.03	1.78	0.33	0.00
6	487.02	2.64	0.31	0.04	6	131.03	1.78	0.31	0.00
6	488.02	2.70	0.26	0.01	6	135.03	1.76	0.29	0.00
6	489.02	2.80	0.19	0.00	6	138.03	1.75	0.25	0.00
6	490.02	2.62	0.10	0.00	6	140.03	1.75	0.22	0.00
6	491.02	2.70	0.11	0.01	6	141.03	1.75	0.24	0.00
6	492.02	2.62	0.08	0.00	6	143.03	1.71	0.26	0.00
6	493.02	2.62	0.10	0.00	6	144.03	1.78	0.29	0.00
6	494.02	2.62	0.14	0.00	6	145.03	1.78	0.23	0.00
6	495.02	2.69	0.15	0.00	6	146.03	1.78	0.21	0.00
6	496.02	2.68	0.13	0.00	6	148.03	1.78	0.08	0.05
6	497.02	2.44	0.13	0.04	6	149.03	1.70	0.12	0.06
6	498.02	2.88	1.62	0.46	6	150.03	1.95	0.00	0.09
6	499.02	2.65	0.09	0.00	6	151.03	2.26	0.01	0.00
6	500.02	2.54	0.10	0.00	6	153.03	1.78	0.06	0.07
6	501.02	2.60	0.10	0.00	6	155.03	2.26	0.00	0.00
6	502.02	2.60	0.08	0.00	6	156.03	2.26	0.00	0.00
6	503.02	2.60	0.11	0.00	6	159.03	2.26	0.00	0.00
6	504.02	2.60	0.07	0.00	6	160.03	1.86	0.02	0.09
6	505.02	2.34	0.10	0.07	6	165.03	1.76	0.04	0.11
6	506.02	2.60	0.11	0.00	6	166.03	2.10	0.05	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	169.03	2.21	0.20	0.13	6	231.03	2.24	0.00	0.00
6	171.03	1.84	0.22	0.00	6	232.03	2.24	0.00	0.00
6	172.03	1.82	0.19	0.00	6	233.03	2.24	0.00	0.00
6	173.03	1.82	0.20	0.00	6	234.03	2.37	0.00	0.01
6	174.03	1.82	0.20	0.00	6	235.03	2.18	0.01	0.00
6	175.03	1.82	0.22	0.00	6	236.03	2.25	0.00	0.00
6	176.03	1.76	0.21	0.01	6	237.03	2.22	0.00	0.00
6	177.03	1.83	0.25	0.00	6	238.03	2.25	0.01	0.00
6	178.03	1.83	0.32	0.01	6	239.03	2.25	0.01	0.01
6	179.03	1.98	0.12	0.00	6	240.03	2.25	0.01	0.00
6	180.03	1.94	0.15	0.00	6	241.03	2.25	0.00	0.00
6	181.03	1.83	0.28	0.01	6	242.03	2.25	0.00	0.00
6	182.03	1.94	0.16	0.00	6	243.03	2.25	0.01	0.00
6	183.03	1.83	0.20	0.00	6	244.03	2.25	0.00	0.01
6	184.03	1.84	0.21	0.00	6	245.03	2.25	0.01	0.02
6	185.03	1.84	0.20	0.00	6	246.03	2.25	0.01	0.03
6	186.03	1.84	0.20	0.00	6	247.03	2.25	0.00	0.00
6	187.03	1.84	0.20	0.00	6	248.03	2.25	0.04	0.06
6	188.03	1.84	0.18	0.00	6	249.03	2.25	0.04	0.06
6	189.03	1.84	0.16	0.00	6	250.03	2.25	0.02	0.03
6	190.03	1.84	0.15	0.00	6	251.03	2.25	0.06	0.09
6	191.03	1.83	0.20	0.00	6	252.03	2.25	0.05	0.07
6	192.03	1.84	0.23	0.00	6	253.03	2.19	0.05	0.10
6	193.03	1.84	0.19	0.00	6	254.03	2.25	0.07	0.09
6	194.03	1.80	0.34	0.01	6	255.03	2.56	0.07	0.00
6	195.03	2.07	0.10	0.01	6	256.03	2.56	0.09	0.00
6	196.03	1.83	0.18	0.00	6	257.03	2.32	0.07	0.06
6	197.03	1.86	0.16	0.00	6	258.03	2.50	0.05	0.00
6	198.03	1.86	0.15	0.00	6	259.03	2.50	0.05	0.00
6	199.03	1.86	0.17	0.00	6	260.03	2.50	0.05	0.00
6	200.03	1.86	0.18	0.00	6	261.03	2.50	0.07	0.00
6	201.03	1.86	0.21	0.00	6	262.03	2.56	0.12	0.01
6	202.03	1.86	0.23	0.00	6	263.03	2.26	0.07	0.09
6	203.03	1.86	0.21	0.00	6	264.03	2.55	0.10	0.00
6	204.03	1.86	0.21	0.00	6	265.03	2.55	0.04	0.00
6	211.03	1.99	0.12	0.00	6	266.03	2.55	0.07	0.00
6	212.03	1.94	0.07	0.01	6	267.03	2.55	0.06	0.00
6	213.03	1.88	0.06	0.03	6	268.03	2.55	0.05	0.00
6	214.03	1.94	0.09	0.00	6	269.03	2.55	0.06	0.00
6	215.03	2.12	0.00	0.01	6	270.03	2.55	0.04	0.00
6	216.03	2.22	0.00	0.00	6	271.03	2.55	0.05	0.00
6	219.03	1.93	0.00	0.09	6	272.03	2.55	0.05	0.00
6	220.03	2.05	0.01	0.02	6	273.03	2.55	0.06	0.00
6	222.03	2.23	0.00	0.00	6	274.03	2.55	0.06	0.00
6	223.03	2.22	0.00	0.00	6	275.03	2.55	0.06	0.00
6	224.03	2.23	0.00	0.00	6	276.03	2.55	0.06	0.00
6	225.03	2.20	0.00	0.00	6	277.03	2.55	0.06	0.00
6	228.03	2.24	0.00	0.00	6	278.03	2.55	0.05	0.00
6	229.03	2.24	0.00	0.00	6	279.03	2.66	0.07	0.01
6	230.03	2.24	0.00	0.00	6	280.03	2.48	0.05	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	281.03	2.55	0.08	0.00	6	332.03	2.54	0.07	0.00
6	282.03	2.51	0.08	0.00	6	333.03	2.54	0.07	0.00
6	283.03	2.51	0.06	0.00	6	334.03	2.54	0.06	0.00
6	284.03	2.51	0.07	0.00	6	335.03	2.54	0.07	0.00
6	285.03	2.70	0.30	0.02	6	336.03	2.54	0.08	0.00
6	287.03	2.46	0.09	0.02	6	337.03	2.54	0.08	0.00
6	288.03	2.84	0.22	0.01	6	338.03	2.54	0.11	0.01
6	289.03	2.49	0.00	0.03	6	339.03	2.54	0.08	0.00
6	290.03	2.33	0.00	0.00	6	340.03	2.54	0.10	0.00
6	291.03	2.33	0.00	0.00	6	341.03	2.30	0.00	0.00
6	292.03	2.73	0.74	0.18	6	342.03	2.54	0.09	0.00
6	293.03	2.33	0.01	0.00	6	343.03	2.54	0.11	0.01
6	294.03	2.73	0.33	0.02	6	344.03	2.54	0.09	0.00
6	295.03	2.63	0.19	0.01	6	345.03	2.54	0.10	0.01
6	296.03	2.73	0.72	0.17	6	346.03	2.54	0.07	0.00
6	297.03	2.73	0.46	0.06	6	347.03	2.54	0.10	0.01
6	298.03	2.73	0.72	0.16	6	348.03	2.47	0.01	0.01
6	299.03	2.84	0.27	0.00	6	349.03	2.49	0.01	0.01
6	300.03	2.73	0.71	0.16	6	350.03	2.43	0.08	0.02
6	301.03	2.73	0.69	0.15	6	351.03	2.57	0.03	0.01
6	302.03	2.73	0.75	0.18	6	352.03	2.57	0.05	0.00
6	303.03	2.73	0.38	0.03	6	353.03	2.57	0.04	0.01
6	304.03	2.73	0.71	0.16	6	354.03	2.42	0.04	0.01
6	305.03	2.80	0.47	0.03	6	355.03	2.57	0.06	0.00
6	306.03	2.73	0.60	0.11	6	356.03	2.57	0.05	0.00
6	307.03	2.73	0.63	0.12	6	357.03	2.27	0.02	0.03
6	308.03	2.80	0.41	0.02	6	358.03	2.32	0.01	0.01
6	309.03	2.73	0.10	0.02	6	359.03	2.44	0.02	0.00
6	310.03	2.80	0.09	0.05	6	360.03	2.36	0.04	0.02
6	311.03	2.46	0.26	0.11	6	361.03	2.44	0.02	0.00
6	312.03	2.80	0.40	0.01	6	362.03	2.61	0.04	0.01
6	313.03	2.80	0.26	0.00	6	363.03	2.44	0.02	0.00
6	314.03	2.80	0.31	0.00	6	364.03	2.60	0.02	0.02
6	315.03	2.73	0.41	0.04	6	365.03	2.46	0.25	0.45
6	316.03	2.73	0.51	0.07	6	366.03	2.04	0.28	0.08
6	317.03	2.73	0.50	0.07	6	367.03	2.45	0.01	0.06
6	318.03	2.47	0.06	0.01	6	368.03	2.30	0.02	0.03
6	319.03	2.67	0.25	0.01	6	369.03	2.05	0.06	0.00
6	320.03	2.54	0.04	0.00	6	370.03	2.33	0.02	0.03
6	321.03	2.79	0.08	0.05	6	371.03	2.18	0.07	0.03
6	322.03	2.69	0.23	0.01	6	372.03	1.89	0.11	0.01
6	323.03	2.68	0.11	0.00	6	373.03	1.95	0.16	0.00
6	324.03	2.54	0.15	0.02	6	374.03	1.89	0.10	0.01
6	325.03	2.78	0.10	0.03	6	375.03	1.84	0.11	0.02
6	326.03	2.58	0.06	0.00	6	376.03	1.89	0.09	0.01
6	327.03	2.54	0.06	0.00	6	377.03	1.89	0.15	0.00
6	328.03	2.66	0.06	0.02	6	378.03	2.14	0.01	0.00
6	329.03	2.54	0.07	0.00	6	379.03	1.85	0.13	0.01
6	330.03	2.54	0.07	0.00	6	380.03	1.94	0.08	0.01
6	331.03	2.54	0.07	0.00	6	381.03	1.89	0.18	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	382.03	2.16	0.05	0.01	6	432.03	2.22	0.00	0.00
6	383.03	1.77	0.23	0.00	6	433.03	2.07	0.00	0.03
6	384.03	1.95	0.22	0.02	6	434.03	2.23	0.01	0.00
6	385.03	1.98	0.24	0.03	6	435.03	2.21	0.03	0.01
6	386.03	1.75	0.33	0.00	6	436.03	2.26	0.00	0.00
6	387.03	1.66	0.36	0.00	6	437.03	2.29	0.00	0.00
6	388.03	1.36	0.74	0.00	6	438.03	2.75	0.24	0.00
6	389.03	1.73	0.70	0.07	6	439.03	2.75	0.14	0.01
6	390.03	1.43	0.60	0.01	6	440.03	2.14	0.21	0.37
6	391.03	1.37	0.74	0.00	6	441.03	2.75	0.16	0.00
6	392.03	2.14	0.08	0.19	6	442.03	2.70	0.17	0.00
6	393.03	1.52	0.28	0.06	6	443.03	2.70	0.11	0.01
6	394.03	2.01	0.06	0.00	6	444.03	2.70	0.21	0.00
6	395.03	1.69	0.45	0.01	6	445.03	2.70	0.17	0.00
6	396.03	1.62	0.92	0.08	6	446.03	2.70	0.13	0.00
6	397.03	1.30	0.79	0.01	6	447.03	2.70	0.15	0.00
6	398.03	1.43	0.66	0.00	6	448.03	2.70	0.13	0.00
6	399.03	1.43	0.25	0.13	6	449.03	2.70	0.12	0.00
6	400.03	1.76	0.20	0.01	6	450.03	2.70	0.10	0.01
6	401.03	1.84	0.19	0.00	6	451.03	2.70	0.07	0.02
6	402.03	1.71	0.18	0.02	6	452.03	2.70	0.05	0.04
6	403.03	1.71	0.06	0.11	6	453.03	2.60	0.03	0.02
6	404.03	1.81	0.00	0.21	6	454.03	2.72	0.09	0.02
6	405.03	2.00	0.00	0.07	6	455.03	2.47	0.06	0.00
6	406.03	2.23	0.00	0.00	6	456.03	2.47	0.07	0.01
6	407.03	2.23	0.01	0.00	6	457.03	2.59	0.13	0.00
6	408.03	2.23	0.00	0.00	6	458.03	2.57	0.07	0.00
6	409.03	2.23	0.01	0.00	6	459.03	2.81	0.12	0.03
6	410.03	2.23	0.00	0.00	6	460.03	2.65	0.10	0.00
6	411.03	2.23	0.01	0.00	6	461.03	2.60	0.10	0.00
6	412.03	2.17	0.03	0.00	6	462.03	2.50	0.05	0.00
6	413.03	2.12	0.02	0.00	6	463.03	2.53	0.05	0.00
6	414.03	2.12	0.01	0.00	6	464.03	2.50	0.03	0.00
6	415.03	2.12	0.02	0.00	6	465.03	2.50	0.05	0.00
6	416.03	2.23	0.00	0.00	6	466.03	2.50	0.06	0.00
6	417.03	2.23	0.00	0.00	6	467.03	2.50	0.09	0.01
6	418.03	2.08	0.00	0.03	6	468.03	2.50	0.06	0.00
6	419.03	2.23	0.00	0.00	6	469.03	2.50	0.06	0.00
6	420.03	2.26	0.00	0.00	6	470.03	2.50	0.07	0.00
6	421.03	2.26	0.00	0.00	6	471.03	2.50	0.05	0.00
6	422.03	2.26	0.00	0.00	6	472.03	2.50	0.06	0.00
6	423.03	2.26	0.00	0.00	6	473.03	2.50	0.15	0.03
6	424.03	2.26	0.00	0.00	6	474.03	2.50	0.08	0.01
6	425.03	2.26	0.00	0.00	6	475.03	2.50	0.05	0.00
6	426.03	2.02	0.35	0.73	6	476.03	2.50	0.15	0.03
6	427.03	2.02	0.35	0.75	6	477.03	2.50	0.11	0.02
6	428.03	2.26	0.00	0.00	6	478.03	2.50	0.08	0.01
6	429.03	2.26	0.00	0.00	6	479.03	2.55	0.23	0.05
6	430.03	2.25	0.00	0.00	6	480.03	2.77	0.16	0.01
6	431.03	2.29	0.00	0.00	6	481.03	2.50	0.06	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	482.03	2.77	0.21	0.00	6	131.04	1.42	0.81	0.00
6	483.03	2.50	0.14	0.03	6	140.04	1.41	0.55	0.02
6	484.03	2.50	0.09	0.01	6	141.04	1.55	0.60	0.00
6	485.03	2.50	0.20	0.06	6	143.04	1.55	0.53	0.00
6	486.03	2.50	0.20	0.06	6	144.04	1.55	0.46	0.00
6	487.03	2.35	0.12	0.08	6	145.04	1.55	0.49	0.00
6	488.03	2.63	0.16	0.00	6	146.04	1.57	0.48	0.00
6	489.03	2.63	0.13	0.00	6	148.04	1.60	0.46	0.00
6	490.03	2.84	0.30	0.00	6	151.04	1.59	0.73	0.02
6	491.03	2.37	0.30	0.22	6	153.04	1.60	0.48	0.00
6	492.03	2.84	0.31	0.00	6	160.04	1.55	0.63	0.00
6	493.03	2.84	0.32	0.00	6	165.04	1.63	0.59	0.01
6	494.03	2.84	0.32	0.00	6	166.04	1.52	0.53	0.00
6	495.03	2.84	0.35	0.00	6	169.04	1.53	0.17	0.12
6	496.03	2.84	0.31	0.00	6	171.04	1.86	0.43	0.05
6	497.03	2.84	0.36	0.00	6	173.04	1.63	0.35	0.00
6	498.03	2.53	0.02	0.01	6	174.04	1.66	0.41	0.00
6	499.03	2.84	0.33	0.00	6	175.04	1.65	0.39	0.00
6	500.03	2.84	0.32	0.00	6	176.04	1.65	0.39	0.00
6	501.03	2.84	0.29	0.00	6	177.04	1.70	0.33	0.00
6	502.03	2.84	0.32	0.00	6	178.04	1.69	0.45	0.01
6	503.03	2.84	0.28	0.00	6	179.04	1.88	0.02	0.08
6	504.03	2.84	0.31	0.00	6	180.04	1.83	0.16	0.00
6	505.03	2.74	0.16	0.00	6	181.04	1.57	0.44	0.00
6	506.03	2.84	0.27	0.00	6	182.04	1.72	0.34	0.00
6	507.03	2.75	0.20	0.00	6	183.04	1.81	0.28	0.00
6	508.03	2.74	0.17	0.00	6	184.04	1.78	0.37	0.01
6	509.03	2.67	0.14	0.00	6	185.04	1.60	0.38	0.01
6	510.03	2.66	0.11	0.00	6	186.04	1.62	0.41	0.00
6	511.03	2.74	0.21	0.00	6	187.04	1.65	0.42	0.00
6	512.03	2.22	0.05	0.02	6	188.04	1.65	0.38	0.00
6	94.04	2.01	0.73	0.33	6	189.04	1.65	0.39	0.00
6	95.04	2.22	0.65	0.54	6	190.04	1.65	0.43	0.00
6	96.04	2.05	0.67	0.34	6	191.04	1.57	0.41	0.01
6	97.04	1.54	0.63	0.00	6	192.04	1.65	0.31	0.01
6	106.04	1.04	0.09	0.92	6	193.04	1.83	0.30	0.01
6	108.04	1.48	0.46	0.02	6	194.04	1.67	0.24	0.02
6	109.04	1.61	0.44	0.00	6	195.04	1.74	0.18	0.02
6	110.04	1.77	0.43	0.02	6	196.04	1.80	0.19	0.00
6	111.04	1.64	0.47	0.00	6	197.04	1.80	0.20	0.00
6	113.04	1.61	0.59	0.01	6	198.04	1.80	0.25	0.00
6	114.04	1.65	0.37	0.00	6	199.04	1.80	0.18	0.00
6	116.04	1.84	0.39	0.03	6	200.04	1.80	0.16	0.01
6	118.04	1.67	0.29	0.01	6	201.04	1.80	0.20	0.00
6	120.04	1.66	1.09	0.17	6	202.04	1.98	0.16	0.01
6	123.04	1.23	1.04	0.00	6	203.04	1.74	0.19	0.01
6	125.04	1.25	1.03	0.00	6	204.04	1.88	0.18	0.00
6	128.04	1.30	1.12	0.00	6	211.04	1.88	0.13	0.00
6	129.04	1.28	1.03	0.00	6	212.04	1.85	0.18	0.00
6	130.04	1.40	0.75	0.00	6	213.04	1.85	0.18	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	214.04	1.85	0.18	0.00	6	269.04	2.05	0.03	0.00
6	215.04	1.88	0.11	0.01	6	270.04	2.05	0.02	0.01
6	216.04	1.88	0.13	0.00	6	271.04	2.05	0.02	0.01
6	219.04	1.94	0.16	0.00	6	272.04	2.05	0.02	0.01
6	220.04	1.94	0.15	0.00	6	273.04	2.05	0.03	0.01
6	222.04	1.94	0.17	0.00	6	274.04	2.05	0.02	0.01
6	223.04	1.83	0.12	0.01	6	275.04	2.05	0.03	0.00
6	224.04	1.94	0.16	0.00	6	276.04	2.05	0.02	0.01
6	225.04	1.94	0.09	0.00	6	277.04	2.05	0.03	0.01
6	228.04	1.94	0.11	0.00	6	278.04	2.05	0.02	0.01
6	229.04	1.94	0.08	0.00	6	279.04	2.05	0.02	0.01
6	230.04	1.94	0.09	0.00	6	280.04	2.05	0.02	0.01
6	231.04	1.94	0.07	0.01	6	281.04	2.05	0.02	0.01
6	232.04	1.94	0.07	0.01	6	282.04	2.05	0.02	0.01
6	233.04	1.94	0.07	0.01	6	283.04	2.05	0.02	0.01
6	234.04	1.89	0.09	0.01	6	284.04	2.05	0.03	0.01
6	235.04	2.12	0.05	0.00	6	285.04	2.05	0.03	0.00
6	236.04	2.07	0.06	0.00	6	287.04	2.05	0.06	0.00
6	237.04	1.99	0.09	0.00	6	288.04	2.05	0.06	0.00
6	238.04	1.97	0.06	0.01	6	289.04	2.01	0.11	0.00
6	239.04	2.04	0.03	0.01	6	290.04	2.01	0.11	0.00
6	240.04	2.04	0.04	0.00	6	291.04	1.92	0.11	0.00
6	241.04	2.04	0.04	0.00	6	292.04	2.12	0.08	0.01
6	242.04	2.04	0.05	0.00	6	293.04	1.96	0.19	0.01
6	243.04	2.04	0.05	0.00	6	294.04	2.01	0.07	0.00
6	244.04	2.04	0.05	0.00	6	295.04	1.94	0.08	0.00
6	245.04	2.04	0.05	0.00	6	296.04	2.01	0.08	0.00
6	246.04	2.04	0.06	0.00	6	297.04	2.01	0.07	0.00
6	247.04	2.04	0.05	0.00	6	298.04	1.92	0.07	0.01
6	248.04	2.04	0.07	0.00	6	299.04	2.05	0.07	0.00
6	249.04	2.04	0.06	0.00	6	300.04	2.02	0.09	0.00
6	250.04	2.04	0.06	0.00	6	301.04	2.02	0.08	0.00
6	251.04	2.04	0.07	0.00	6	302.04	2.02	0.06	0.00
6	252.04	2.15	0.06	0.01	6	303.04	2.23	0.00	0.01
6	253.04	2.05	0.06	0.00	6	304.04	2.02	0.05	0.00
6	254.04	1.96	0.09	0.00	6	305.04	1.95	0.06	0.01
6	255.04	1.99	0.08	0.00	6	306.04	2.02	0.02	0.02
6	256.04	1.99	0.08	0.00	6	307.04	2.08	0.00	0.03
6	257.04	1.99	0.07	0.00	6	308.04	2.04	0.02	0.01
6	258.04	2.05	0.06	0.00	6	309.04	2.11	0.04	0.00
6	259.04	2.06	0.06	0.00	6	310.04	2.21	0.03	0.01
6	260.04	2.05	0.06	0.00	6	311.04	2.18	0.02	0.06
6	261.04	2.05	0.05	0.00	6	312.04	2.43	0.01	0.00
6	262.04	2.05	0.06	0.00	6	313.04	2.43	0.01	0.00
6	263.04	2.05	0.05	0.00	6	314.04	2.43	0.01	0.00
6	264.04	2.05	0.05	0.00	6	315.04	1.97	0.00	0.10
6	265.04	2.05	0.02	0.01	6	316.04	2.24	0.01	0.00
6	266.04	2.05	0.04	0.00	6	317.04	2.22	0.00	0.00
6	267.04	2.05	0.03	0.00	6	318.04	2.09	0.11	0.02
6	268.04	2.05	0.03	0.01	6	319.04	2.09	0.05	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	320.04	1.96	0.11	0.00	6	370.04	1.97	0.52	0.16
6	321.04	1.96	0.13	0.00	6	371.04	1.87	0.50	0.08
6	322.04	2.07	0.08	0.00	6	372.04	1.51	0.61	0.00
6	323.04	1.92	0.06	0.02	6	373.04	1.51	0.60	0.00
6	324.04	2.16	0.05	0.01	6	374.04	1.49	0.89	0.02
6	325.04	1.96	0.05	0.01	6	375.04	1.63	0.35	0.01
6	326.04	2.07	0.06	0.00	6	376.04	1.35	0.76	0.01
6	327.04	2.07	0.04	0.00	6	377.04	1.35	0.84	0.00
6	328.04	2.07	0.06	0.00	6	378.04	1.34	0.67	0.02
6	329.04	2.07	0.04	0.00	6	379.04	1.47	0.59	0.00
6	330.04	2.07	0.06	0.00	6	380.04	1.45	0.65	0.00
6	331.04	2.05	0.05	0.00	6	381.04	1.26	1.06	0.00
6	332.04	2.04	0.06	0.00	6	382.04	1.36	1.05	0.01
6	333.04	2.04	0.05	0.00	6	383.04	1.56	0.46	0.00
6	334.04	2.04	0.07	0.00	6	384.04	1.25	0.78	0.02
6	335.04	2.16	0.06	0.01	6	386.04	1.38	0.28	0.15
6	336.04	1.92	0.14	0.00	6	387.04	1.58	0.52	0.00
6	337.04	1.91	0.14	0.00	6	388.04	1.79	0.01	0.17
6	338.04	2.21	0.06	0.03	6	389.04	1.73	0.31	0.00
6	339.04	1.91	0.13	0.00	6	390.04	2.12	0.02	0.00
6	340.04	2.05	0.05	0.00	6	391.04	1.98	0.07	0.00
6	341.04	1.87	0.07	0.02	6	392.04	1.76	0.10	0.73
6	342.04	2.05	0.05	0.00	6	393.04	1.68	0.18	0.03
6	343.04	2.04	0.06	0.00	6	394.04	1.43	0.75	0.00
6	344.04	2.04	0.05	0.00	6	395.04	1.85	0.10	0.01
6	345.04	2.04	0.06	0.00	6	396.04	1.86	0.12	0.01
6	346.04	2.21	0.04	0.01	6	397.04	1.81	0.09	0.03
6	347.04	1.94	0.18	0.01	6	398.04	1.97	0.04	0.01
6	348.04	2.17	0.10	0.04	6	399.04	2.09	0.02	0.01
6	349.04	1.97	0.05	0.01	6	400.04	2.09	0.02	0.00
6	350.04	2.01	0.01	0.04	6	401.04	2.09	0.03	0.00
6	351.04	2.02	0.09	0.00	6	402.04	2.09	0.03	0.00
6	352.04	2.04	0.01	0.02	6	403.04	2.09	0.02	0.00
6	353.04	2.02	0.09	0.00	6	404.04	2.09	0.01	0.01
6	354.04	1.87	1.19	0.46	6	405.04	2.09	0.00	0.02
6	355.04	2.02	0.09	0.00	6	406.04	2.09	0.00	0.02
6	356.04	2.02	0.03	0.01	6	407.04	2.20	0.00	0.00
6	357.04	2.19	0.00	0.02	6	408.04	1.97	0.01	0.04
6	358.04	2.20	0.02	0.00	6	409.04	2.09	0.00	0.04
6	359.04	2.19	0.00	0.02	6	410.04	2.17	0.01	0.00
6	360.04	1.87	0.07	0.03	6	411.04	2.26	0.00	0.00
6	361.04	2.19	0.00	0.01	6	412.04	2.03	0.00	0.06
6	362.04	2.11	0.01	0.01	6	413.04	2.29	0.00	0.00
6	363.04	2.19	0.00	0.01	6	414.04	2.29	0.00	0.00
6	364.04	2.28	0.06	0.06	6	415.04	2.29	0.00	0.00
6	365.04	1.54	0.64	0.00	6	416.04	2.29	0.00	0.00
6	366.04	1.43	0.63	0.00	6	417.04	2.29	0.00	0.00
6	367.04	1.88	0.89	0.28	6	418.04	2.29	0.00	0.00
6	368.04	2.27	0.46	0.44	6	419.04	2.29	0.00	0.00
6	369.04	1.73	0.51	0.02	6	420.04	2.29	0.00	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	421.04	2.29	0.00	0.00	6	473.04	2.87	0.33	0.00
6	422.04	2.29	0.00	0.00	6	474.04	3.02	0.59	0.00
6	423.04	2.29	0.00	0.00	6	475.04	3.02	0.69	0.01
6	424.04	2.29	0.00	0.00	6	476.04	3.05	0.58	0.00
6	425.04	2.29	0.00	0.00	6	477.04	3.02	0.65	0.01
6	426.04	2.00	0.24	0.61	6	478.04	3.02	0.64	0.01
6	427.04	2.78	0.27	0.00	6	479.04	2.87	0.30	0.00
6	428.04	2.29	0.00	0.00	6	480.04	2.87	0.36	0.00
6	429.04	2.29	0.00	0.00	6	481.04	2.95	0.65	0.02
6	430.04	2.22	0.00	0.00	6	482.04	2.87	0.36	0.00
6	431.04	2.22	0.00	0.00	6	483.04	3.16	0.58	0.01
6	432.04	2.22	0.00	0.02	6	484.04	2.99	0.34	0.01
6	433.04	2.21	0.00	0.01	6	485.04	3.05	0.59	0.00
6	434.04	2.27	0.00	0.00	6	486.04	2.87	0.34	0.00
6	435.04	2.30	0.00	0.00	6	487.04	3.05	0.60	0.00
6	436.04	2.29	0.01	0.01	6	488.04	3.05	0.59	0.00
6	437.04	2.17	0.00	0.00	6	489.04	3.05	0.58	0.00
6	438.04	2.47	0.10	0.02	6	490.04	2.92	0.36	0.00
6	439.04	2.76	0.26	0.00	6	491.04	3.02	0.39	0.01
6	440.04	2.16	0.09	0.19	6	492.04	2.92	0.38	0.00
6	441.04	2.56	0.23	0.05	6	493.04	2.92	0.39	0.00
6	442.04	2.77	0.20	0.00	6	494.04	2.92	0.36	0.00
6	443.04	2.77	0.22	0.00	6	495.04	2.92	0.34	0.00
6	445.04	2.82	0.24	0.00	6	496.04	2.92	0.38	0.00
6	446.04	2.78	0.27	0.00	6	497.04	2.92	0.28	0.01
6	447.04	2.78	0.25	0.00	6	498.04	2.08	0.02	0.11
6	448.04	2.78	0.29	0.00	6	499.04	2.92	0.33	0.00
6	449.04	2.78	0.30	0.00	6	500.04	2.92	0.35	0.00
6	450.04	2.78	0.30	0.00	6	501.04	2.92	0.34	0.00
6	451.04	2.78	0.36	0.01	6	502.04	2.92	0.15	0.06
6	452.04	2.78	0.45	0.03	6	503.04	2.92	0.16	0.05
6	453.04	2.89	0.45	0.01	6	504.04	2.92	0.14	0.06
6	454.04	2.64	0.30	0.04	6	505.04	2.18	0.01	0.00
6	455.04	2.96	0.40	0.00	6	506.04	2.92	0.15	0.06
6	456.04	2.75	0.40	0.03	6	507.04	2.69	0.25	0.01
6	457.04	2.83	0.28	0.00	6	508.04	2.21	0.01	0.00
6	458.04	2.92	0.40	0.00	6	509.04	2.08	0.01	0.01
6	459.04	2.92	0.35	0.00	6	510.04	2.17	0.00	0.01
6	460.04	2.92	0.39	0.00	6	511.04	2.71	0.00	0.18
6	461.04	2.92	0.38	0.00	6	512.04	2.46	0.08	0.20
6	462.04	3.05	0.56	0.00	6	514.04	2.21	0.17	0.23
6	463.04	2.80	0.47	0.03	6	120.05	1.03	1.27	0.02
6	465.04	3.04	0.51	0.00	6	125.05	1.45	0.96	0.02
6	466.04	3.04	0.63	0.00	6	129.05	1.20	0.97	0.01
6	467.04	3.02	0.41	0.01	6	131.05	1.31	0.92	0.00
6	468.04	2.97	0.53	0.00	6	140.05	1.31	0.99	0.00
6	469.04	3.02	0.54	0.00	6	141.05	1.37	0.92	0.00
6	470.04	3.02	0.63	0.00	6	143.05	1.33	0.90	0.00
6	471.04	3.02	0.66	0.01	6	144.05	1.33	0.96	0.00
6	472.04	3.02	0.62	0.00	6	145.05	1.34	1.06	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	146.05	1.30	1.01	0.00	6	239.05	2.13	0.03	0.00
6	148.05	1.28	0.99	0.00	6	240.05	2.13	0.04	0.00
6	153.05	1.32	1.02	0.00	6	241.05	2.13	0.03	0.00
6	169.05	1.30	0.42	0.12	6	242.05	2.13	0.05	0.00
6	171.05	1.36	0.84	0.00	6	243.05	2.13	0.03	0.00
6	173.05	1.39	0.83	0.00	6	244.05	2.13	0.02	0.00
6	174.05	1.35	0.83	0.00	6	245.05	2.13	0.03	0.00
6	175.05	1.39	0.79	0.00	6	246.05	2.25	0.03	0.02
6	176.05	1.40	0.81	0.00	6	247.05	2.13	0.03	0.00
6	177.05	1.40	0.77	0.00	6	248.05	2.11	0.03	0.00
6	178.05	1.41	0.64	0.01	6	249.05	2.11	0.03	0.00
6	179.05	1.65	0.87	0.09	6	250.05	2.08	0.07	0.00
6	180.05	1.57	0.67	0.01	6	251.05	2.03	0.07	0.00
6	181.05	1.49	0.62	0.00	6	252.05	2.15	0.04	0.00
6	182.05	1.42	0.74	0.00	6	253.05	2.09	0.03	0.00
6	184.05	1.48	1.01	0.04	6	254.05	2.09	0.04	0.00
6	185.05	1.71	0.84	0.11	6	255.05	2.09	0.05	0.00
6	186.05	1.51	0.67	0.00	6	256.05	2.09	0.06	0.00
6	187.05	1.47	0.66	0.00	6	257.05	2.09	0.07	0.00
6	188.05	1.48	0.68	0.00	6	258.05	2.09	0.04	0.00
6	189.05	1.48	0.65	0.00	6	259.05	2.09	0.03	0.00
6	190.05	1.48	0.65	0.00	6	260.05	2.09	0.03	0.00
6	191.05	1.50	0.50	0.01	6	261.05	2.26	0.04	0.03
6	192.05	1.71	0.44	0.01	6	262.05	2.01	0.14	0.01
6	194.05	1.63	0.39	0.00	6	263.05	2.09	0.04	0.00
6	196.05	1.63	0.40	0.00	6	264.05	2.08	0.09	0.01
6	197.05	1.63	0.37	0.00	6	265.05	1.99	0.06	0.00
6	198.05	1.82	0.29	0.00	6	266.05	1.99	0.06	0.00
6	199.05	1.58	0.45	0.00	6	267.05	1.99	0.09	0.00
6	200.05	1.62	0.42	0.00	6	268.05	1.99	0.09	0.00
6	201.05	1.75	0.25	0.00	6	269.05	1.99	0.09	0.00
6	202.05	1.67	0.29	0.01	6	270.05	1.99	0.09	0.00
6	203.05	1.75	0.35	0.00	6	271.05	1.99	0.09	0.00
6	211.05	1.90	0.29	0.02	6	272.05	1.99	0.08	0.00
6	212.05	1.76	0.27	0.00	6	273.05	1.99	0.09	0.00
6	213.05	1.79	0.22	0.00	6	274.05	1.99	0.08	0.00
6	214.05	1.88	0.25	0.01	6	275.05	1.98	0.08	0.00
6	219.05	1.85	0.17	0.00	6	276.05	2.00	0.11	0.00
6	220.05	1.80	0.19	0.00	6	277.05	2.00	0.08	0.00
6	222.05	1.85	0.13	0.01	6	278.05	2.00	0.09	0.00
6	223.05	1.93	0.14	0.00	6	279.05	2.00	0.09	0.00
6	224.05	1.85	0.12	0.01	6	280.05	2.00	0.11	0.00
6	231.05	2.13	0.03	0.00	6	281.05	2.00	0.09	0.00
6	232.05	1.97	0.02	0.03	6	282.05	2.00	0.08	0.00
6	233.05	2.13	0.01	0.00	6	283.05	2.00	0.10	0.00
6	234.05	2.24	0.01	0.00	6	284.05	2.00	0.10	0.00
6	235.05	2.10	0.03	0.00	6	285.05	1.98	0.60	0.22
6	236.05	2.10	0.03	0.00	6	287.05	1.52	0.63	0.00
6	237.05	2.20	0.01	0.00	6	288.05	1.45	0.69	0.00
6	238.05	2.17	0.03	0.00	6	289.05	1.87	0.18	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	290.05	1.87	0.21	0.00	6	343.05	1.82	0.17	0.00
6	292.05	1.87	0.21	0.00	6	344.05	1.88	0.19	0.00
6	293.05	2.09	0.06	0.00	6	345.05	1.88	0.19	0.00
6	294.05	1.48	0.18	0.15	6	346.05	1.88	0.17	0.00
6	295.05	1.83	0.14	0.01	6	347.05	1.67	0.37	0.00
6	296.05	1.80	0.20	0.00	6	348.05	1.90	0.38	0.05
6	297.05	1.87	0.24	0.00	6	349.05	1.67	0.42	0.00
6	298.05	1.80	0.20	0.00	6	350.05	1.81	0.35	0.01
6	300.05	1.84	0.17	0.00	6	351.05	1.67	0.24	0.02
6	301.05	1.85	0.15	0.00	6	352.05	1.59	0.41	0.00
6	302.05	1.90	0.18	0.00	6	353.05	1.55	0.35	0.02
6	303.05	1.75	0.22	0.01	6	354.05	1.52	1.45	0.19
6	304.05	1.90	0.19	0.00	6	355.05	1.71	0.36	0.00
6	305.05	1.82	0.17	0.00	6	356.05	1.97	0.26	0.03
6	306.05	1.89	0.21	0.00	6	357.05	1.88	0.12	0.00
6	307.05	1.81	0.22	0.00	6	358.05	1.78	0.47	0.03
6	308.05	2.03	0.17	0.02	6	359.05	1.69	0.14	0.05
6	309.05	1.48	0.70	0.00	6	360.05	2.00	0.16	0.01
6	310.05	1.67	0.50	0.01	6	361.05	1.82	0.09	0.03
6	312.05	1.90	0.20	0.00	6	362.05	1.68	0.32	0.00
6	313.05	2.04	0.10	0.00	6	363.05	1.99	0.10	0.00
6	314.05	1.98	0.11	0.00	6	364.05	1.35	0.60	0.03
6	315.05	1.80	0.46	0.04	6	365.05	1.73	0.36	0.00
6	316.05	1.58	0.34	0.02	6	366.05	1.71	0.35	0.00
6	317.05	1.70	0.38	0.00	6	367.05	1.52	0.64	0.00
6	318.05	1.80	0.04	0.09	6	368.05	1.92	0.18	0.00
6	319.05	1.77	0.11	0.04	6	369.05	1.73	0.28	0.00
6	320.05	1.80	0.07	0.05	6	370.05	1.76	0.32	0.00
6	321.05	1.88	0.16	0.00	6	371.05	1.52	0.34	0.03
6	322.05	1.48	0.22	0.12	6	372.05	1.71	0.27	0.00
6	323.05	1.88	0.16	0.00	6	373.05	1.71	0.24	0.01
6	324.05	1.59	0.17	0.08	6	374.05	1.80	0.34	0.01
6	325.05	1.88	0.19	0.00	6	375.05	1.67	0.23	0.02
6	326.05	1.88	0.20	0.00	6	376.05	1.66	0.41	0.00
6	327.05	1.88	0.20	0.00	6	377.05	1.56	0.42	0.01
6	328.05	1.88	0.20	0.00	6	378.05	1.84	0.08	0.03
6	329.05	1.88	0.22	0.00	6	379.05	1.56	0.14	0.13
6	330.05	1.81	0.19	0.00	6	380.05	1.79	0.00	0.25
6	331.05	1.87	0.23	0.00	6	381.05	1.88	0.06	0.02
6	332.05	1.81	0.22	0.00	6	382.05	1.60	0.10	0.14
6	333.05	1.81	0.23	0.00	6	383.05	2.17	0.04	0.10
6	334.05	1.81	0.17	0.00	6	384.05	2.17	0.03	0.08
6	335.05	1.81	0.16	0.01	6	386.05	1.83	0.06	0.04
6	336.05	1.81	0.16	0.01	6	387.05	2.46	0.03	0.00
6	337.05	1.94	0.16	0.00	6	388.05	2.46	0.02	0.00
6	338.05	1.81	0.16	0.01	6	389.05	2.46	0.02	0.00
6	339.05	1.89	0.16	0.00	6	390.05	2.29	0.00	0.00
6	340.05	1.73	0.17	0.02	6	391.05	2.29	0.00	0.00
6	341.05	1.67	0.35	0.00	6	392.05	1.80	0.00	0.19
6	342.05	1.87	0.17	0.00	6	393.05	1.93	0.00	0.13

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	394.05	1.56	0.18	0.09	6	445.05	2.72	0.16	0.00
6	395.05	2.09	0.03	0.14	6	446.05	2.72	0.24	0.00
6	396.05	2.29	0.00	0.00	6	447.05	2.72	0.21	0.00
6	397.05	2.29	0.00	0.00	6	448.05	2.72	0.22	0.00
6	398.05	2.39	0.00	0.00	6	449.05	2.72	0.22	0.00
6	399.05	2.19	0.00	0.01	6	450.05	2.72	0.24	0.00
6	400.05	2.27	0.01	0.00	6	451.05	2.72	0.21	0.00
6	401.05	2.27	0.01	0.00	6	452.05	2.72	0.25	0.01
6	402.05	2.27	0.01	0.01	6	453.05	2.72	0.29	0.01
6	403.05	2.27	0.02	0.01	6	454.05	2.72	0.30	0.01
6	404.05	2.34	0.01	0.00	6	455.05	2.68	0.24	0.01
6	405.05	2.34	0.01	0.00	6	456.05	2.86	0.32	0.00
6	406.05	2.34	0.00	0.01	6	457.05	2.64	0.19	0.01
6	407.05	2.23	0.00	0.00	6	458.05	2.85	0.31	0.00
6	408.05	2.39	0.00	0.02	6	459.05	2.72	0.21	0.00
6	409.05	2.34	0.00	0.01	6	460.05	2.75	0.31	0.01
6	410.05	2.25	0.00	0.00	6	461.05	2.85	0.30	0.00
6	411.05	2.24	0.00	0.00	6	462.05	2.80	0.17	0.01
6	412.05	2.26	0.00	0.00	6	463.05	2.78	0.32	0.01
6	413.05	2.31	0.00	0.00	6	465.05	2.71	0.16	0.00
6	414.05	2.31	0.00	0.00	6	466.05	2.53	0.07	0.00
6	415.05	2.31	0.00	0.00	6	467.05	2.68	0.22	0.01
6	416.05	2.31	0.00	0.00	6	468.05	2.88	0.21	0.02
6	417.05	2.31	0.00	0.00	6	469.05	2.76	0.14	0.01
6	418.05	2.31	0.00	0.00	6	470.05	2.76	0.08	0.03
6	419.05	2.31	0.00	0.00	6	471.05	2.76	0.13	0.01
6	420.05	2.31	0.00	0.00	6	472.05	2.76	0.08	0.04
6	421.05	2.31	0.00	0.00	6	473.05	2.69	0.21	0.00
6	422.05	2.31	0.00	0.00	6	474.05	2.76	0.08	0.04
6	423.05	2.31	0.00	0.00	6	475.05	2.76	0.08	0.04
6	424.05	2.31	0.01	0.01	6	476.05	2.69	0.19	0.00
6	425.05	2.31	0.00	0.01	6	477.05	2.76	0.10	0.02
6	426.05	2.04	1.03	1.59	6	478.05	2.76	0.16	0.01
6	427.05	3.30	1.00	0.00	6	479.05	2.69	0.23	0.01
6	428.05	2.25	0.08	0.06	6	480.05	2.69	0.24	0.01
6	429.05	2.21	0.08	0.04	6	481.05	2.65	0.16	0.00
6	430.05	2.20	0.02	0.04	6	482.05	2.69	0.16	0.00
6	431.05	1.83	0.06	0.04	6	483.05	2.69	0.17	0.00
6	432.05	2.42	0.04	0.01	6	484.05	2.69	0.19	0.00
6	433.05	2.18	0.08	0.16	6	485.05	2.69	0.17	0.00
6	434.05	2.15	0.03	0.10	6	486.05	2.69	0.21	0.00
6	435.05	1.88	0.06	0.03	6	487.05	2.69	0.19	0.00
6	436.05	2.45	0.00	0.05	6	488.05	2.69	0.15	0.00
6	437.05	1.88	0.11	0.01	6	489.05	2.69	0.15	0.00
6	438.05	1.95	0.27	0.73	6	490.05	2.85	0.19	0.02
6	439.05	2.18	1.52	1.81	6	491.05	2.55	0.11	0.00
6	440.05	1.80	0.27	1.02	6	492.05	2.63	0.17	0.01
6	441.05	2.78	0.19	0.00	6	493.05	2.71	0.14	0.00
6	442.05	2.73	0.25	0.00	6	494.05	2.71	0.16	0.00
6	443.05	2.68	0.18	0.00	6	495.05	2.67	0.15	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	496.05	2.68	0.17	0.00	6	237.06	1.91	0.14	0.00
6	497.05	2.68	0.20	0.00	6	238.06	2.05	0.05	0.00
6	498.05	2.00	1.19	1.90	6	239.06	2.08	0.08	0.01
6	499.05	2.68	0.19	0.00	6	240.06	2.12	0.04	0.00
6	500.05	2.68	0.19	0.00	6	241.06	2.25	0.11	0.08
6	501.05	2.45	0.09	0.02	6	242.06	1.96	0.16	0.01
6	502.05	2.60	0.21	0.02	6	243.06	2.08	0.09	0.01
6	503.05	2.83	0.46	0.02	6	244.06	2.04	0.16	0.03
6	504.05	2.75	0.19	0.00	6	245.06	2.23	0.14	0.09
6	505.05	2.98	0.37	1.70	6	246.06	1.92	0.13	0.00
6	506.05	2.75	0.22	0.00	6	247.06	2.08	0.08	0.00
6	507.05	2.75	0.24	0.00	6	248.06	1.92	0.10	0.00
6	508.05	1.68	0.33	0.00	6	249.06	1.92	0.11	0.00
6	509.05	1.55	0.33	0.03	6	250.06	1.88	0.22	0.00
6	510.05	1.71	0.30	0.00	6	251.06	2.10	0.21	0.07
6	511.05	2.57	0.82	0.40	6	252.06	1.83	0.20	0.00
6	512.05	2.70	0.04	0.38	6	253.06	1.98	0.18	0.01
6	514.05	1.57	0.46	1.94	6	254.06	1.77	0.28	0.00
6	143.06	1.04	1.61	0.00	6	255.06	1.76	0.45	0.02
6	144.06	1.05	1.64	0.00	6	256.06	1.76	0.61	0.06
6	145.06	1.03	1.51	0.00	6	257.06	1.76	0.40	0.01
6	148.06	1.09	1.38	0.00	6	258.06	2.02	0.19	0.03
6	171.06	1.42	0.87	0.00	6	259.06	1.86	0.17	0.00
6	173.06	1.38	0.97	0.01	6	260.06	1.86	0.16	0.00
6	174.06	1.29	1.03	0.00	6	261.06	1.86	0.26	0.01
6	175.06	1.29	1.03	0.00	6	263.06	1.86	0.23	0.00
6	176.06	1.31	1.09	0.00	6	264.06	1.83	0.33	0.01
6	177.06	1.29	1.13	0.00	6	265.06	1.71	0.41	0.00
6	178.06	1.35	0.97	0.00	6	266.06	1.71	0.35	0.00
6	179.06	1.17	0.79	0.05	6	267.06	1.71	0.33	0.00
6	180.06	1.33	1.00	0.00	6	268.06	1.71	0.38	0.00
6	186.06	1.33	0.90	0.00	6	270.06	1.65	0.44	0.00
6	187.06	1.38	0.89	0.00	6	272.06	1.94	0.25	0.02
6	189.06	1.37	0.80	0.00	6	273.06	1.73	0.45	0.01
6	196.06	1.36	0.37	0.10	6	274.06	1.62	0.38	0.00
6	197.06	1.64	0.27	0.02	6	275.06	1.61	0.39	0.00
6	199.06	1.53	0.30	0.05	6	276.06	1.67	0.49	0.01
6	200.06	1.88	0.19	0.00	6	277.06	1.67	0.44	0.00
6	211.06	2.01	0.16	0.01	6	278.06	1.67	0.53	0.01
6	212.06	1.89	0.12	0.00	6	279.06	1.67	0.54	0.01
6	213.06	1.86	0.19	0.00	6	280.06	1.67	0.62	0.03
6	214.06	1.89	0.18	0.00	6	281.06	1.67	0.53	0.01
6	219.06	1.95	0.16	0.00	6	282.06	1.67	0.79	0.07
6	220.06	2.07	0.08	0.00	6	283.06	1.67	0.57	0.02
6	222.06	1.89	0.17	0.00	6	284.06	1.40	0.84	0.00
6	223.06	1.89	0.15	0.00	6	285.06	1.47	0.63	0.00
6	231.06	2.04	0.10	0.01	6	287.06	1.55	0.57	0.00
6	232.06	1.86	0.15	0.00	6	288.06	1.52	0.50	0.00
6	233.06	1.91	0.14	0.00	6	289.06	1.99	0.34	0.08
6	234.06	1.91	0.13	0.00	6	292.06	1.75	0.41	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	293.06	1.65	0.47	0.00	6	345.06	1.66	0.37	0.00
6	294.06	1.53	0.59	0.00	6	346.06	1.66	0.37	0.00
6	295.06	1.88	0.12	0.00	6	347.06	1.78	0.41	0.02
6	296.06	1.61	0.39	0.00	6	348.06	1.78	0.66	0.09
6	297.06	1.58	0.42	0.00	6	349.06	1.88	0.18	0.00
6	298.06	1.67	0.40	0.00	6	350.06	1.74	0.26	0.00
6	300.06	1.67	0.42	0.00	6	351.06	1.56	0.61	0.00
6	301.06	1.67	0.43	0.00	6	352.06	1.78	0.40	0.02
6	302.06	1.67	0.40	0.00	6	353.06	1.69	0.30	0.00
6	303.06	1.67	0.46	0.00	6	354.06	2.11	0.00	0.05
6	304.06	1.67	0.37	0.00	6	355.06	1.54	0.46	0.00
6	305.06	1.89	0.27	0.01	6	356.06	1.74	0.32	0.00
6	306.06	1.60	0.38	0.01	6	357.06	1.67	0.22	0.02
6	307.06	1.61	0.48	0.00	6	358.06	1.29	0.56	0.06
6	308.06	1.77	0.30	0.00	6	359.06	1.98	0.21	0.02
6	309.06	1.64	0.64	0.02	6	360.06	1.60	0.66	0.01
6	310.06	1.72	0.33	0.00	6	361.06	1.83	0.20	0.00
6	312.06	1.67	0.37	0.00	6	362.06	1.46	0.74	0.00
6	313.06	1.67	0.41	0.00	6	363.06	1.83	0.19	0.00
6	314.06	1.67	0.42	0.00	6	364.06	1.34	0.29	0.17
6	315.06	1.61	0.31	0.02	6	365.06	2.15	0.00	0.03
6	316.06	1.66	0.46	0.00	6	366.06	2.51	0.07	0.00
6	317.06	1.61	0.55	0.00	6	367.06	2.28	0.02	0.03
6	318.06	2.10	0.04	0.00	6	368.06	1.70	0.02	0.20
6	319.06	2.08	0.13	0.02	6	369.06	2.36	0.02	0.00
6	320.06	2.08	0.08	0.01	6	370.06	2.12	0.00	0.03
6	321.06	1.74	0.31	0.00	6	371.06	2.33	0.00	0.00
6	322.06	1.95	0.21	0.01	6	372.06	2.34	0.00	0.00
6	323.06	1.98	0.18	0.01	6	373.06	2.30	0.00	0.00
6	324.06	1.75	0.24	0.00	6	374.06	2.35	0.00	0.00
6	325.06	1.80	0.26	0.00	6	375.06	2.27	0.00	0.01
6	326.06	1.78	0.26	0.00	6	376.06	2.35	0.00	0.00
6	327.06	1.78	0.33	0.00	6	377.06	2.35	0.00	0.01
6	328.06	1.78	0.24	0.00	6	378.06	2.50	0.16	0.04
6	329.06	1.77	0.33	0.00	6	379.06	2.69	0.13	0.00
6	330.06	1.72	0.29	0.00	6	380.06	2.48	0.95	0.62
6	331.06	1.75	0.29	0.00	6	381.06	2.35	0.02	0.00
6	332.06	1.68	0.43	0.00	6	382.06	2.35	0.02	0.01
6	333.06	1.74	0.34	0.00	6	383.06	2.69	0.14	0.00
6	334.06	1.94	0.30	0.04	6	384.06	2.69	0.13	0.00
6	335.06	1.60	0.48	0.00	6	386.06	2.69	0.08	0.01
6	336.06	1.59	0.54	0.00	6	387.06	2.69	0.07	0.02
6	337.06	1.59	0.53	0.00	6	388.06	2.69	0.08	0.01
6	338.06	1.89	0.29	0.02	6	389.06	2.69	0.14	0.00
6	339.06	1.60	0.37	0.01	6	390.06	2.69	0.07	0.02
6	340.06	1.75	0.24	0.00	6	391.06	2.69	0.07	0.02
6	341.06	1.81	0.54	0.07	6	392.06	1.64	0.00	0.49
6	342.06	1.75	0.27	0.00	6	393.06	2.35	0.05	0.03
6	343.06	1.72	0.40	0.00	6	394.06	2.35	0.02	0.00
6	344.06	1.66	0.38	0.00	6	395.06	2.69	0.13	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	396.06	2.69	0.07	0.02	6	448.06	2.71	0.16	0.00
6	397.06	2.35	0.04	0.02	6	449.06	2.71	0.17	0.00
6	398.06	2.35	0.07	0.04	6	450.06	2.71	0.17	0.00
6	399.06	2.56	0.07	0.00	6	451.06	2.71	0.19	0.00
6	400.06	2.74	0.09	0.02	6	452.06	2.71	0.14	0.00
6	401.06	2.55	0.08	0.00	6	453.06	2.71	0.14	0.00
6	402.06	2.55	0.09	0.00	6	454.06	2.71	0.14	0.00
6	403.06	2.55	0.10	0.00	6	455.06	2.61	0.01	0.19
6	404.06	2.57	0.07	0.00	6	456.06	2.85	0.20	0.01
6	405.06	2.44	0.05	0.01	6	457.06	2.58	0.14	0.45
6	406.06	2.55	0.08	0.00	6	458.06	2.86	0.13	0.05
6	407.06	2.55	0.05	0.00	6	459.06	2.66	0.46	1.11
6	408.06	2.55	0.09	0.00	6	460.06	1.76	0.14	0.03
6	409.06	2.55	0.07	0.00	6	461.06	1.75	0.32	1.24
6	410.06	2.45	0.06	0.01	6	462.06	1.57	0.26	0.04
6	411.06	2.64	0.07	0.01	6	463.06	1.40	0.35	0.09
6	412.06	2.54	0.04	0.00	6	464.06	1.76	0.31	0.00
6	413.06	2.54	0.05	0.00	6	465.06	1.68	0.23	0.02
6	414.06	2.54	0.03	0.01	6	466.06	1.81	0.22	0.00
6	415.06	2.54	0.03	0.01	6	467.06	1.95	0.15	0.00
6	416.06	2.56	0.06	0.00	6	468.06	1.91	0.12	0.00
6	417.06	2.56	0.06	0.00	6	469.06	1.72	0.19	0.02
6	418.06	2.56	0.06	0.00	6	470.06	1.86	0.10	0.01
6	419.06	2.56	0.06	0.00	6	471.06	2.01	0.11	0.00
6	420.06	2.56	0.07	0.00	6	472.06	1.86	0.06	0.03
6	421.06	2.56	0.07	0.00	6	473.06	2.22	0.01	0.00
6	422.06	2.56	0.09	0.00	6	474.06	1.86	0.09	0.02
6	423.06	2.55	0.07	0.00	6	476.06	1.97	0.08	0.00
6	424.06	2.45	0.05	0.00	6	477.06	1.91	0.03	0.04
6	425.06	2.56	0.12	0.01	6	478.06	2.26	0.03	0.02
6	426.06	2.55	0.23	0.05	6	479.06	2.17	0.03	0.00
6	427.06	2.77	0.23	0.00	6	480.06	2.08	0.07	0.00
6	428.06	2.45	0.00	0.03	6	481.06	2.06	0.05	0.00
6	429.06	2.47	0.00	0.03	6	482.06	2.08	0.04	0.00
6	431.06	2.67	0.17	0.00	6	483.06	2.01	0.04	0.01
6	432.06	2.46	0.01	0.01	6	484.06	2.09	0.01	0.01
6	433.06	2.67	0.07	0.02	6	485.06	2.09	0.04	0.00
6	434.06	2.67	0.16	0.00	6	486.06	2.09	0.01	0.01
6	435.06	2.55	0.17	0.02	6	487.06	2.01	0.07	0.00
6	436.06	2.72	0.17	0.00	6	488.06	2.03	0.04	0.00
6	437.06	2.45	0.01	0.01	6	489.06	2.08	0.04	0.00
6	438.06	2.64	0.11	0.00	6	490.06	2.08	0.02	0.00
6	439.06	2.89	0.19	0.03	6	491.06	2.04	0.06	0.00
6	440.06	2.57	0.12	0.00	6	492.06	2.31	0.02	0.03
6	441.06	2.51	0.14	0.02	6	493.06	2.13	0.04	0.00
6	442.06	2.66	0.14	0.00	6	494.06	2.08	0.03	0.00
6	443.06	2.53	0.18	0.03	6	495.06	2.13	0.03	0.00
6	445.06	2.71	0.20	0.00	6	496.06	2.13	0.03	0.00
6	446.06	2.71	0.16	0.00	6	497.06	2.13	0.03	0.00
6	447.06	2.71	0.16	0.00	6	498.06	1.72	0.02	0.18

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	499.06	2.13	0.03	0.00	6	250.07	1.62	0.46	0.00
6	500.06	2.13	0.02	0.00	6	251.07	1.62	0.44	0.00
6	501.06	2.12	0.04	0.00	6	252.07	1.62	0.47	0.00
6	502.06	2.05	0.14	0.02	6	253.07	1.58	0.62	0.01
6	503.06	2.09	0.03	0.00	6	254.07	1.50	0.70	0.00
6	504.06	1.87	0.31	0.02	6	255.07	1.50	0.51	0.01
6	505.06	2.03	0.38	0.12	6	256.07	1.63	0.33	0.01
6	506.06	1.68	0.32	0.00	6	257.07	1.50	0.56	0.00
6	507.06	1.72	0.31	0.00	6	258.07	1.83	0.35	0.02
6	508.06	1.68	0.38	0.00	6	259.07	1.70	0.44	0.01
6	509.06	1.59	0.33	0.02	6	260.07	1.70	0.38	0.00
6	510.06	1.72	0.31	0.00	6	261.07	1.74	0.26	0.00
6	511.06	2.01	0.02	0.02	6	263.07	1.68	0.36	0.00
6	512.06	1.78	0.07	0.06	6	264.07	1.66	0.36	0.00
6	514.06	1.57	0.11	0.14	6	265.07	1.90	0.22	0.01
6	143.07	1.04	1.71	0.00	6	266.07	1.73	0.33	0.00
6	144.07	1.06	1.74	0.01	6	267.07	1.67	0.37	0.00
6	145.07	1.00	1.78	0.00	6	268.07	1.91	0.26	0.02
6	171.07	1.29	1.02	0.00	6	270.07	1.76	0.31	0.00
6	174.07	1.32	0.97	0.00	6	272.07	1.70	0.28	0.00
6	175.07	1.35	1.38	0.06	6	273.07	1.96	0.11	0.00
6	176.07	1.17	1.29	0.00	6	274.07	1.75	0.19	0.01
6	177.07	1.25	1.30	0.01	6	275.07	1.74	0.17	0.02
6	178.07	1.15	1.06	0.01	6	276.07	1.91	0.17	0.00
6	179.07	1.03	1.10	0.04	6	277.07	1.88	0.20	0.00
6	180.07	1.28	0.94	0.00	6	279.07	1.82	0.15	0.01
6	186.07	1.20	0.72	0.06	6	281.07	2.09	0.07	0.00
6	187.07	1.46	0.70	0.00	6	282.07	1.85	0.05	0.04
6	189.07	1.48	0.61	0.00	6	283.07	2.08	0.00	0.05
6	211.07	1.65	0.34	0.00	6	284.07	2.03	0.07	0.00
6	212.07	1.70	0.46	0.01	6	285.07	2.02	0.06	0.26
6	213.07	1.91	0.37	0.05	6	287.07	2.48	0.02	0.00
6	214.07	1.69	0.57	0.02	6	288.07	2.73	0.10	0.01
6	223.07	1.70	0.42	0.00	6	289.07	2.52	0.02	0.01
6	231.07	1.76	0.27	0.00	6	292.07	2.55	0.06	0.00
6	232.07	1.77	0.32	0.00	6	293.07	2.52	0.09	0.29
6	233.07	1.77	0.30	0.00	6	294.07	2.74	0.12	0.01
6	234.07	1.77	0.27	0.00	6	295.07	2.42	0.04	0.00
6	237.07	1.77	0.30	0.00	6	296.07	2.65	0.06	0.01
6	238.07	1.77	0.26	0.00	6	297.07	2.54	0.07	0.00
6	239.07	1.68	0.36	0.00	6	298.07	2.54	0.07	0.00
6	241.07	1.65	0.67	0.03	6	300.07	2.54	0.08	0.00
6	242.07	1.84	0.43	0.04	6	301.07	2.54	0.08	0.00
6	243.07	1.68	0.29	0.01	6	302.07	2.54	0.07	0.00
6	244.07	1.85	0.33	0.02	6	303.07	2.38	0.06	0.03
6	245.07	1.47	0.53	0.01	6	304.07	2.54	0.04	0.00
6	246.07	1.69	0.44	0.00	6	305.07	2.45	0.03	0.00
6	247.07	1.94	0.37	0.07	6	306.07	2.41	0.03	0.00
6	248.07	1.62	0.48	0.00	6	307.07	2.45	0.06	0.01
6	249.07	1.62	0.44	0.00	6	308.07	2.45	0.03	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	309.07	2.98	0.43	0.00	6	363.07	3.47	1.22	0.01
6	310.07	2.62	0.31	0.05	6	365.07	11.60	89.98	0.03
6	313.07	1.98	0.09	0.00	6	366.07	3.70	1.80	0.00
6	314.07	1.98	0.08	0.00	6	367.07	3.70	1.90	0.00
6	315.07	2.55	0.15	0.02	6	368.07	3.46	1.98	0.06
6	316.07	2.62	0.25	0.03	6	369.07	3.69	4.51	0.53
6	317.07	2.77	0.32	0.01	6	370.07	.		
6	318.07	2.60	0.11	0.00	6	371.07	3.69	3.32	0.18
6	319.07	2.62	0.17	0.01	6	372.07	4.24	1.20	0.73
6	320.07	2.58	0.20	0.03	6	373.07	4.01	0.95	0.55
6	321.07	2.98	0.56	0.00	6	374.07	3.71	1.10	0.14
6	322.07	2.84	0.44	0.01	6	375.07	4.01	2.03	0.09
6	323.07	2.98	0.43	0.00	6	376.07	3.71	1.10	0.14
6	324.07	2.76	0.48	0.05	6	377.07	4.07	1.28	0.42
6	325.07	2.98	0.53	0.00	6	378.07	3.54	3.17	0.28
6	326.07	2.98	0.58	0.00	6	379.07	4.19	3.39	0.00
6	327.07	2.98	0.68	0.02	6	381.07	3.71	0.24	0.88
6	328.07	2.98	0.57	0.00	6	382.07	3.71	0.24	0.88
6	329.07	2.89	0.62	0.03	6	383.07	4.24	3.16	0.03
6	330.07	3.22	0.95	0.00	6	384.07	4.07	3.27	0.00
6	331.07	3.02	0.78	0.02	6	386.07	4.07	0.28	1.56
6	332.07	3.20	0.97	0.01	6	387.07	4.07	0.52	1.11
6	333.07	3.14	0.45	0.03	6	388.07	4.07	1.24	0.44
6	334.07	3.03	0.83	0.03	6	389.07	4.07	1.50	0.30
6	335.07	2.96	0.54	0.00	6	390.07	4.07	0.31	1.50
6	336.07	2.96	0.59	0.01	6	391.07	4.08	0.28	1.60
6	337.07	2.96	0.57	0.01	6	392.07	3.47	1.57	0.01
6	339.07	3.38	0.93	0.02	6	393.07	3.71	0.23	0.89
6	340.07	3.38	1.18	0.00	6	394.07	3.71	1.00	0.18
6	341.07	3.47	0.83	0.07	6	395.07	4.07	2.71	0.02
6	342.07	3.38	0.89	0.02	6	396.07	4.07	0.25	1.63
6	343.07	3.38	0.96	0.01	6	397.07	2.82	0.23	0.00
6	344.07	3.30	0.79	0.01	6	398.07	2.82	0.24	0.00
6	345.07	2.96	0.41	0.00	6	399.07	2.82	0.24	0.00
6	346.07	2.96	0.41	0.00	6	400.07	2.82	0.26	0.00
6	347.07	2.96	0.57	0.01	6	401.07	2.91	0.29	0.01
6	348.07	2.96	0.73	0.03	6	402.07	2.83	0.26	0.00
6	349.07	3.47	1.21	0.01	6	403.07	2.83	0.32	0.00
6	350.07	2.96	0.49	0.00	6	404.07	2.71	0.19	0.00
6	351.07	3.10	0.52	0.01	6	405.07	2.82	0.22	0.00
6	352.07	2.96	0.56	0.01	6	406.07	2.72	0.26	0.01
6	353.07	3.47	1.26	0.00	6	407.07	2.81	0.26	0.00
6	354.07	3.70	1.79	0.00	6	408.07	2.81	0.20	0.01
6	355.07	3.39	1.20	0.00	6	409.07	2.82	0.27	0.00
6	356.07	2.96	0.63	0.02	6	410.07	2.81	0.15	0.02
6	357.07	3.38	1.39	0.01	6	411.07	2.81	0.18	0.01
6	359.07	3.47	1.38	0.00	6	412.07	2.68	0.14	0.00
6	360.07	3.39	1.84	0.06	6	413.07	2.81	0.13	0.03
6	361.07	3.47	1.28	0.00	6	414.07	2.65	0.18	0.00
6	362.07	3.07	1.50	0.20	6	415.07	2.65	0.08	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	416.07	2.82	0.15	0.02	6	470.07	2.65	0.10	0.00
6	417.07	2.63	0.06	0.01	6	471.07	2.84	0.96	0.18
6	418.07	2.53	0.04	0.00	6	472.07	2.65	0.11	0.00
6	419.07	2.53	0.04	0.00	6	473.07	2.61	0.14	0.00
6	420.07	2.63	0.01	0.05	6	474.07	2.65	0.10	0.00
6	421.07	2.45	0.02	0.00	6	476.07	2.61	0.13	0.00
6	422.07	2.45	0.00	0.04	6	477.07	2.65	0.10	0.00
6	423.07	2.69	0.03	0.06	6	478.07	2.65	0.11	0.00
6	424.07	2.21	0.00	0.01	6	479.07	2.61	0.10	0.00
6	425.07	2.24	0.00	0.00	6	480.07	2.61	0.08	0.00
6	428.07	2.40	0.02	0.00	6	481.07	2.62	0.10	0.00
6	429.07	2.16	0.05	0.01	6	482.07	2.61	0.02	0.03
6	431.07	2.40	0.03	0.00	6	483.07	2.61	0.09	0.00
6	432.07	2.39	0.17	0.10	6	484.07	2.61	0.10	0.00
6	433.07	2.20	0.00	0.02	6	485.07	2.61	0.08	0.00
6	434.07	2.21	0.02	0.00	6	486.07	2.61	0.13	0.00
6	435.07	2.46	0.00	0.03	6	487.07	2.61	0.07	0.00
6	436.07	2.41	0.06	0.01	6	488.07	2.61	0.05	0.01
6	437.07	2.21	0.00	0.02	6	489.07	2.61	0.04	0.02
6	438.07	2.92	0.43	0.00	6	490.07	2.61	0.03	0.02
6	439.07	2.43	0.05	0.01	6	491.07	2.61	0.03	0.03
6	440.07	2.36	0.40	0.32	6	492.07	2.61	0.03	0.02
6	441.07	2.25	0.14	0.16	6	493.07	2.61	0.01	0.04
6	442.07	2.66	0.06	0.02	6	494.07	2.61	0.03	0.02
6	443.07	2.78	0.16	0.01	6	495.07	2.61	0.03	0.02
6	445.07	2.63	0.16	0.00	6	496.07	2.61	0.02	0.03
6	446.07	2.69	0.19	0.00	6	497.07	2.61	0.02	0.03
6	447.07	2.69	0.18	0.00	6	498.07	1.92	0.06	0.02
6	448.07	2.69	0.15	0.00	6	499.07	2.61	0.02	0.04
6	449.07	2.69	0.19	0.00	6	500.07	2.61	0.02	0.03
6	450.07	2.69	0.01	0.24	6	501.07	2.41	0.01	0.00
6	451.07	2.18	0.05	0.01	6	502.07	2.35	0.00	0.01
6	452.07	2.05	0.10	0.01	6	503.07	2.49	0.03	0.00
6	453.07	1.97	0.11	0.00	6	504.07	2.26	0.19	0.17
6	454.07	2.11	0.01	0.00	6	505.07	1.51	0.26	0.07
6	455.07	2.12	0.00	0.03	6	506.07	1.76	0.50	0.03
6	456.07	1.86	0.08	0.02	6	507.07	1.58	0.57	0.00
6	457.07	2.01	0.03	0.22	6	508.07	1.78	0.24	0.00
6	458.07	1.92	0.03	0.04	6	509.07	1.78	0.25	0.00
6	459.07	2.63	0.64	0.21	6	510.07	1.78	0.34	0.00
6	460.07	2.66	0.19	0.00	6	511.07	2.10	0.00	0.04
6	461.07	2.31	0.29	0.27	6	512.07	1.62	0.05	0.20
6	462.07	2.61	0.17	0.01	6	514.07	1.63	2.86	5.53
6	463.07	2.44	0.17	0.07	6	516.07	2.64	2.51	1.52
6	464.07	2.70	0.10	0.01	6	517.07	2.90	0.45	0.00
6	465.07	2.70	0.16	0.00	6	518.07	1.70	0.50	0.01
6	466.07	2.70	0.15	0.00	6	277.08	1.03	0.89	0.10
6	467.07	2.70	0.14	0.00	6	284.08	1.44	0.98	0.02
6	468.07	2.70	0.17	0.00	6	285.08	1.37	0.72	0.01
6	469.07	2.66	0.13	0.00	6	287.08	1.41	0.74	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	288.08	1.66	0.74	0.05	6	402.08	3.76	1.84	0.01
6	289.08	1.50	0.41	0.02	6	403.08	3.65	1.69	0.00
6	292.08	1.68	0.43	0.00	6	406.08	3.65	1.71	0.00
6	294.08	1.70	0.43	0.00	6	407.08	3.63	1.37	0.03
6	296.08	1.65	0.49	0.00	6	408.08	3.65	1.77	0.00
6	297.08	1.65	0.44	0.00	6	409.08	3.65	1.66	0.00
6	298.08	1.56	0.65	0.01	6	410.08	3.84	1.97	0.02
6	300.08	1.82	0.52	0.06	6	411.08	3.79	1.72	0.04
6	303.08	1.84	0.19	0.00	6	412.08	3.66	1.73	0.00
6	305.08	1.76	0.22	0.00	6	413.08	3.61	1.27	0.04
6	307.08	1.82	0.26	0.00	6	414.08	3.43	1.08	0.01
6	308.08	2.07	0.14	0.03	6	415.08	3.14	0.36	0.06
6	315.08	1.85	0.19	0.00	6	417.08	3.35	0.75	0.04
6	316.08	1.85	0.18	0.00	6	418.08	3.33	1.23	0.00
6	323.08	1.99	0.08	0.00	6	419.08	3.16	0.78	0.00
6	325.08	2.14	0.03	0.00	6	420.08	2.76	0.37	0.02
6	327.08	2.27	0.02	0.01	6	421.08	3.28	1.00	0.00
6	333.08	2.39	0.00	0.01	6	422.08	2.71	0.31	0.02
6	334.08	2.29	0.00	0.00	6	423.08	3.12	0.99	0.03
6	341.08	2.70	0.04	0.04	6	424.08	2.77	0.18	0.00
6	344.08	2.40	0.08	0.03	6	425.08	2.77	0.26	0.00
6	345.08	2.70	0.07	0.02	6	428.08	2.99	0.67	0.01
6	346.08	2.56	0.07	0.00	6	429.08	3.05	0.56	0.00
6	348.08	2.91	0.15	0.05	6	432.08	3.03	0.36	0.02
6	349.08	2.69	0.07	0.02	6	433.08	3.07	0.44	0.02
6	350.08	2.69	0.10	0.01	6	434.08	2.82	0.58	0.05
6	352.08	2.74	0.18	0.00	6	435.08	3.05	0.38	0.02
6	354.08	2.92	0.42	0.00	6	436.08	2.77	0.28	0.00
6	367.08	2.98	0.42	0.00	6	437.08	3.11	0.64	0.00
6	368.08	2.84	0.45	0.01	6	438.08	3.24	0.93	0.00
6	372.08	3.12	0.79	0.00	6	439.08	3.07	0.92	0.03
6	373.08	3.12	0.87	0.01	6	440.08	2.95	0.90	0.09
6	374.08	3.32	1.09	0.00	6	441.08	2.87	0.18	0.02
6	375.08	3.05	0.70	0.01	6	442.08	2.66	0.12	0.00
6	376.08	3.12	1.07	0.04	6	443.08	2.72	0.23	0.00
6	377.08	3.33	1.06	0.00	6	445.08	2.86	0.23	0.01
6	378.08	2.96	0.46	0.00	6	446.08	2.94	2.19	0.70
6	379.08	2.96	0.48	0.00	6	447.08	2.71	1.92	0.93
6	381.08	3.44	1.78	0.03	6	448.08	2.79	0.23	0.00
6	382.08	3.28	1.62	0.08	6	449.08	3.67	0.25	0.78
6	388.08	3.31	0.91	0.00	6	450.08	2.76	0.54	0.07
6	389.08	3.11	0.89	0.02	6	451.08	2.78	0.68	0.11
6	391.08	3.61	1.77	0.00	6	452.08	3.11	0.69	0.00
6	393.08	3.73	1.75	0.01	6	453.08	3.11	0.69	0.00
6	394.08	3.48	1.11	0.02	6	454.08	3.11	0.62	0.00
6	396.08	3.65	1.73	0.00	6	455.08	3.11	0.77	0.00
6	397.08	3.61	1.83	0.00	6	456.08	3.11	0.81	0.01
6	399.08	3.74	1.80	0.01	6	457.08	3.11	0.70	0.00
6	400.08	3.63	1.82	0.00	6	458.08	3.11	0.80	0.00
6	401.08	3.63	1.86	0.00	6	459.08	3.11	0.85	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	460.08	3.11	0.74	0.00	6	284.09	1.27	1.37	0.02
6	461.08	2.96	0.97	0.10	6	296.09	1.56	0.39	0.01
6	462.08	3.12	0.68	0.00	6	298.09	1.41	1.07	0.02
6	463.08	3.03	0.69	0.01	6	316.09	1.27	1.18	0.00
6	464.08	3.12	0.74	0.00	6	323.09	1.21	1.00	0.01
6	465.08	3.22	0.71	0.01	6	341.09	1.72	0.42	0.01
6	466.08	3.24	0.82	0.00	6	348.09	1.68	0.84	0.09
6	469.08	3.20	0.80	0.00	6	349.09	1.25	0.55	0.09
6	470.08	3.12	0.77	0.00	6	354.09	1.65	0.50	0.00
6	471.08	3.20	0.79	0.00	6	367.09	1.86	0.38	0.03
6	472.08	3.36	0.98	0.01	6	368.09	1.58	0.37	0.01
6	473.08	2.94	0.40	0.00	6	372.09	1.68	0.37	0.00
6	474.08	3.17	0.75	0.00	6	373.09	1.68	0.37	0.00
6	476.08	2.97	0.40	0.00	6	374.09	1.65	0.41	0.00
6	477.08	3.17	0.72	0.00	6	375.09	1.68	0.37	0.00
6	478.08	3.14	0.57	0.01	6	376.09	1.65	0.39	0.00
6	479.08	2.92	0.42	0.00	6	377.09	1.65	0.39	0.00
6	481.08	3.00	0.45	0.00	6	378.09	1.68	0.40	0.00
6	482.08	3.00	0.54	0.00	6	379.09	1.68	0.38	0.00
6	483.08	2.87	0.36	0.00	6	381.09	1.50	0.56	0.00
6	484.08	2.96	0.44	0.00	6	382.09	1.50	0.54	0.00
6	485.08	2.89	0.37	0.00	6	388.09	1.50	0.58	0.00
6	486.08	3.11	0.42	0.03	6	389.09	1.65	0.40	0.00
6	487.08	2.92	0.47	0.00	6	391.09	1.40	0.80	0.00
6	488.08	2.92	0.49	0.00	6	393.09	1.50	0.79	0.01
6	489.08	3.04	0.51	0.00	6	394.09	1.60	0.62	0.01
6	490.08	3.00	0.59	0.00	6	396.09	1.54	0.65	0.00
6	491.08	3.00	0.58	0.00	6	397.09	1.40	0.83	0.00
6	492.08	3.00	0.58	0.00	6	403.09	1.97	0.13	0.00
6	493.08	3.21	0.56	0.03	6	406.09	1.41	0.10	0.31
6	494.08	2.91	0.46	0.00	6	407.09	1.85	0.20	0.00
6	495.08	3.01	0.51	0.00	6	408.09	1.91	0.20	0.00
6	496.08	3.01	0.53	0.00	6	409.09	2.01	0.16	0.01
6	497.08	3.01	0.50	0.00	6	410.09	1.84	0.24	0.00
6	498.08	.			6	411.09	1.84	0.18	0.00
6	499.08	3.01	0.45	0.00	6	412.09	1.81	0.37	0.02
6	500.08	3.01	0.36	0.01	6	413.09	1.67	0.05	0.16
6	501.08	2.76	0.49	1.36	6	414.09	2.01	0.00	0.06
6	502.08	1.94	0.65	1.34	6	415.09	2.27	0.01	0.00
6	503.08	3.01	0.38	0.01	6	417.09	2.61	0.04	0.28
6	504.08	1.57	0.43	0.00	6	418.09	2.25	0.35	0.31
6	505.08	1.56	0.06	0.23	6	419.09	2.30	0.11	0.12
6	506.08	1.61	0.42	0.00	6	420.09	2.22	0.00	0.00
6	507.08	1.64	0.39	0.00	6	421.09	1.92	0.17	0.00
6	508.08	2.04	0.06	0.00	6	422.09	2.68	0.08	0.01
6	511.08	1.72	0.96	2.39	6	423.09	2.00	0.14	0.01
6	514.08	1.87	0.18	0.00	6	424.09	2.46	0.00	0.02
6	516.08	2.98	1.40	0.25	6	425.09	2.43	0.02	0.00
6	517.08	3.11	0.66	0.00	6	428.09	2.43	0.01	0.00
6	277.09	1.08	0.83	0.09	6	429.09	2.36	0.05	0.08

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	432.09	2.26	0.02	0.03	6	490.09	3.09	0.56	0.00
6	433.09	2.43	0.03	0.00	6	491.09	3.04	0.54	0.00
6	434.09	2.43	0.01	0.00	6	492.09	3.04	0.56	0.00
6	435.09	2.08	0.07	0.00	6	493.09	3.04	0.65	0.00
6	436.09	2.68	0.06	0.02	6	494.09	3.08	0.81	0.01
6	437.09	2.43	0.02	0.00	6	495.09	3.04	0.66	0.00
6	438.09	2.68	0.07	0.02	6	496.09	3.16	0.68	0.00
6	439.09	1.93	0.00	0.12	6	497.09	3.08	0.75	0.01
6	440.09	2.36	0.16	0.10	6	498.09	2.23	0.00	0.01
6	441.09	2.06	0.04	0.19	6	499.09	3.12	0.96	0.02
6	442.09	2.08	0.10	0.27	6	500.09	3.12	0.98	0.03
6	443.09	2.18	0.10	0.17	6	501.09	2.67	2.09	3.32
6	445.09	2.60	0.12	0.00	6	502.09	2.96	0.38	0.00
6	446.09	2.22	0.01	0.00	6	503.09	3.00	0.73	0.02
6	447.09	2.17	0.00	0.02	6	504.09	0.89	0.55	0.43
6	448.09	2.60	0.08	0.00	6	505.09	1.57	0.18	0.09
6	449.09	2.60	0.08	0.00	6	506.09	1.53	0.42	0.01
6	450.09	2.60	0.07	0.00	6	507.09	1.64	0.47	0.00
6	451.09	2.60	0.06	0.01	6	508.09	1.87	0.18	0.00
6	452.09	2.60	0.04	0.01	6	511.09	3.26	1.22	0.02
6	453.09	2.60	0.04	0.01	6	514.09	1.71	0.05	0.12
6	454.09	2.60	0.09	0.00	6	516.09	2.49	0.31	0.12
6	455.09	2.60	0.05	0.01	6	517.09	2.83	0.19	0.01
6	456.09	2.60	0.06	0.00	6	284.10	1.04	2.73	0.16
6	457.09	2.52	0.06	0.00	6	316.10	0.69	1.64	0.10
6	458.09	2.60	0.04	0.01	6	341.10	1.32	1.14	0.01
6	459.09	2.60	0.06	0.00	6	348.10	1.26	1.10	0.00
6	460.09	2.60	0.05	0.01	6	349.10	1.03	2.31	0.07
6	461.09	2.50	0.02	0.01	6	354.10	1.44	0.95	0.02
6	462.09	2.67	0.16	0.00	6	372.10	1.28	1.06	0.00
6	463.09	2.56	0.15	0.01	6	373.10	1.31	1.05	0.00
6	464.09	2.67	0.18	0.00	6	374.10	1.21	1.16	0.00
6	465.09	2.67	0.21	0.01	6	375.10	0.79	1.01	0.24
6	469.09	2.64	0.12	0.00	6	376.10	1.24	1.15	0.00
6	470.09	2.69	0.12	0.00	6	377.10	1.26	1.20	0.00
6	471.09	2.70	0.17	0.00	6	381.10	1.17	0.67	0.09
6	472.09	2.88	0.23	0.01	6	382.10	1.44	0.60	0.01
6	474.09	2.64	0.15	0.00	6	388.10	1.45	0.49	0.02
6	476.09	3.22	1.01	0.01	6	389.10	1.27	1.11	0.00
6	477.09	2.64	0.19	0.01	6	391.10	1.68	0.25	0.01
6	478.09	2.64	0.42	0.09	6	393.10	1.61	0.45	0.00
6	481.09	2.64	0.79	0.29	6	394.10	1.17	0.73	0.07
6	482.09	3.27	0.63	0.04	6	396.10	1.40	0.75	0.00
6	483.09	2.64	0.87	0.34	6	406.10	1.45	0.38	0.05
6	484.09	2.64	0.80	0.30	6	407.10	1.38	1.09	0.02
6	485.09	2.74	0.86	0.23	6	408.10	1.46	0.68	0.00
6	486.09	2.64	0.81	0.30	6	409.10	1.72	0.71	0.07
6	487.09	3.22	0.89	0.00	6	410.10	1.49	0.72	0.00
6	488.09	3.31	0.85	0.01	6	411.10	1.46	0.90	0.01
6	489.09	3.20	0.72	0.00	6	415.10	2.35	0.02	0.04

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	417.10	1.24	0.14	0.47	6	481.10	2.94	0.05	0.18
6	418.10	1.94	0.12	0.00	6	482.10	2.58	0.16	0.01
6	419.10	1.95	0.12	0.00	6	483.10	2.94	0.05	0.18
6	420.10	2.32	0.00	0.00	6	484.10	2.94	0.05	0.18
6	422.10	2.34	0.00	0.01	6	485.10	3.13	0.06	0.35
6	424.10	2.14	0.00	0.01	6	486.10	2.94	0.07	0.16
6	425.10	2.34	0.04	0.06	6	487.10	2.54	0.08	0.00
6	428.10	2.34	0.00	0.00	6	488.10	2.94	0.10	0.11
6	429.10	2.65	0.11	0.00	6	489.10	2.47	0.13	0.03
6	432.10	2.22	0.00	0.01	6	490.10	2.83	0.47	0.02
6	433.10	2.46	0.02	0.00	6	491.10	2.98	0.52	0.00
6	434.10	2.46	0.06	0.00	6	492.10	2.98	0.47	0.00
6	435.10	2.67	0.14	0.00	6	493.10	2.98	0.33	0.01
6	436.10	2.63	0.06	0.01	6	494.10	2.69	0.17	0.00
6	437.10	2.40	0.01	0.04	6	495.10	2.83	0.23	0.00
6	438.10	2.60	0.00	0.08	6	496.10	2.77	0.24	0.00
6	439.10	1.99	0.01	0.15	6	497.10	2.69	0.07	0.02
6	440.10	2.12	0.07	0.19	6	498.10	2.22	0.12	0.17
6	441.10	2.67	0.20	0.00	6	499.10	2.65	0.05	0.02
6	442.10	2.70	0.18	0.00	6	500.10	2.53	0.00	0.04
6	443.10	2.67	0.21	0.01	6	502.10	1.97	0.05	0.01
6	445.10	2.69	0.20	0.00	6	503.10	2.34	0.01	0.02
6	446.10	2.58	0.03	0.02	6	504.10	2.11	0.50	0.28
6	447.10	2.46	0.02	0.00	6	505.10	1.63	0.06	0.17
6	448.10	2.76	0.29	0.00	6	506.10	1.56	0.33	0.03
6	449.10	2.94	0.60	0.02	6	507.10	1.72	0.30	0.00
6	450.10	2.83	0.30	0.00	6	508.10	2.05	0.08	0.00
6	451.10	2.83	0.27	0.00	6	511.10	2.34	0.00	0.00
6	452.10	2.83	0.32	0.00	6	514.10	1.73	0.05	0.12
6	453.10	2.83	0.23	0.00	6	516.10	2.58	0.24	0.04
6	454.10	2.83	0.33	0.00	6	517.10	2.81	0.30	0.00
6	455.10	2.83	0.08	0.07	6	519.10	1.21	0.74	0.04
6	456.10	2.83	0.37	0.01	6	284.11	1.04	2.46	0.10
6	457.10	2.49	0.13	0.02	6	316.11	0.77	2.03	0.01
6	458.10	2.83	0.30	0.00	6	341.11	1.42	1.03	0.02
6	459.10	2.83	0.17	0.01	6	348.11	1.23	1.60	0.04
6	460.10	2.56	0.09	0.00	6	349.11	1.23	1.54	0.03
6	461.10	2.74	0.23	0.00	6	354.11	1.43	1.39	0.11
6	462.10	2.61	0.41	0.10	6	372.11	1.27	1.18	0.00
6	463.10	2.80	0.36	0.01	6	373.11	1.43	1.14	0.05
6	464.10	2.78	0.29	0.00	6	374.11	1.43	1.01	0.02
6	465.10	2.94	0.22	0.03	6	375.11	0.90	1.18	0.09
6	469.10	2.76	0.42	0.03	6	376.11	1.30	1.20	0.01
6	470.10	2.94	0.42	0.00	6	377.11	1.37	1.09	0.02
6	471.10	2.69	0.39	0.05	6	381.11	1.25	1.06	0.00
6	472.10	2.95	0.72	0.03	6	382.11	1.25	1.00	0.00
6	474.10	2.94	0.39	0.00	6	389.11	1.23	1.05	0.00
6	476.10	2.91	0.01	0.25	6	396.11	1.33	1.38	0.05
6	477.10	2.94	0.38	0.00	6	406.11	1.13	1.75	0.03
6	478.10	2.94	0.05	0.18	6	407.11	1.10	0.07	0.87

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
6	409.11	1.37	0.64	0.01	6	503.11	2.75	1.07	2.24
6	415.11	2.32	0.03	0.04	6	504.11	1.66	0.45	0.00
6	417.11	1.10	0.03	1.01	6	506.11	1.59	0.39	0.00
6	418.11	1.30	0.02	1.27	6	507.11	1.66	0.44	0.00
6	419.11	2.42	0.01	0.00	6	514.11	1.52	0.16	0.13
6	420.11	1.26	0.00	1.19	6	515.11	1.72	0.50	0.02
6	429.11	3.16	0.53	0.02	6	519.11	1.28	1.04	0.00
6	434.11	2.49	0.21	0.07	6	389.12	1.00	1.07	0.07
6	440.11	1.30	0.03	1.34	6	415.12	1.28	1.65	0.08
6	441.11	2.98	0.44	0.00	6	452.12	1.04	0.47	0.32
6	442.11	2.85	0.42	0.01	6	453.12	1.61	0.37	0.01
6	443.11	3.05	0.48	0.00	6	455.12	1.87	0.19	0.00
6	445.11	3.01	0.40	0.01	6	459.12	1.75	0.31	0.00
6	450.11	3.11	0.50	0.01	6	460.12	1.88	0.17	0.00
6	451.11	3.03	0.47	0.00	6	465.12	1.87	0.15	0.00
6	452.11	3.11	0.68	0.00	6	469.12	1.85	0.68	0.15
6	453.11	3.11	0.73	0.00	6	470.12	1.47	0.71	0.00
6	455.11	3.08	0.77	0.01	6	474.12	1.49	0.68	0.00
6	459.11	3.09	0.80	0.01	6	477.12	1.48	0.60	0.00
6	460.11	3.33	1.03	0.00	6	483.12	1.48	0.21	0.12
6	461.11	2.92	0.37	0.00	6	484.12	1.37	0.23	0.20
6	462.11	3.28	1.64	0.08	6	485.12	1.76	0.13	0.03
6	463.11	3.36	1.78	0.07	6	486.12	1.73	0.01	0.19
6	464.11	3.62	1.87	0.00	6	487.12	1.54	0.18	0.11
6	465.11	3.70	1.50	0.03	6	488.12	1.86	0.29	0.01
6	469.11	3.53	1.14	0.03	6	489.12	2.04	0.15	0.02
6	470.11	3.36	1.25	0.00	6	502.12	1.82	0.29	0.00
6	474.11	3.36	1.29	0.00	6	514.12	1.60	0.24	0.04
6	476.11	3.73	1.85	0.01	7	1.01	1.04	1.05	0.05
6	477.11	3.37	1.19	0.00	7	2.01	1.08	0.39	0.34
6	478.11	3.33	1.25	0.01	7	3.01	0.99	1.90	0.01
6	481.11	3.60	1.82	0.00	7	4.01	1.49	1.48	0.17
6	482.11	3.56	1.57	0.00	7	5.01	1.52	0.79	0.01
6	483.11	3.47	1.36	0.00	7	6.01	1.74	0.57	0.04
6	484.11	3.39	1.40	0.01	7	7.01	1.02	0.60	0.24
6	485.11	3.48	1.42	0.00	7	8.01	1.53	0.35	0.03
6	486.11	3.47	1.33	0.00	7	9.01	1.70	0.42	0.00
6	487.11	3.48	1.51	0.00	7	10.01	1.70	0.35	0.00
6	488.11	3.49	1.60	0.00	7	11.01	1.70	0.33	0.00
6	489.11	3.56	1.63	0.00	7	12.01	1.84	0.45	0.05
6	490.11	3.56	1.56	0.00	7	16.01	1.59	0.23	0.05
6	491.11	3.56	1.53	0.00	7	17.01	1.87	0.04	0.05
6	492.11	3.56	1.57	0.00	7	18.01	1.66	0.12	0.08
6	493.11	3.50	0.49	0.26	7	19.01	1.95	0.13	0.00
6	494.11	3.72	0.75	0.32	7	20.01	1.95	0.15	0.00
6	495.11	3.57	0.49	0.34	7	23.01	1.88	0.52	0.09
6	496.11	3.01	0.37	0.01	7	24.01	1.57	0.35	0.02
6	497.11	2.90	0.36	0.00	7	25.01	1.57	0.48	0.00
6	498.11	2.78	0.53	0.05	7	27.01	1.74	0.32	0.00
6	502.11	1.26	0.36	0.19	7	28.01	1.74	0.43	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	30.01	1.67	0.51	0.01	7	80.01	1.83	0.34	0.01
7	31.01	1.83	0.35	0.02	7	81.01	1.83	0.38	0.02
7	32.01	1.57	0.59	0.00	7	82.01	1.83	0.19	0.00
7	33.01	1.62	0.62	0.01	7	83.01	1.83	0.28	0.01
7	34.01	1.57	0.67	0.01	7	84.01	1.83	0.17	0.00
7	35.01	1.57	0.59	0.00	7	85.01	1.87	0.27	0.01
7	36.01	1.57	0.56	0.00	7	86.01	1.87	0.18	0.00
7	37.01	1.57	0.60	0.00	7	87.01	1.87	0.26	0.01
7	38.01	1.58	0.57	0.00	7	88.01	2.00	0.10	0.00
7	39.01	1.53	0.58	0.00	7	89.01	1.97	0.12	0.00
7	40.01	1.48	1.51	0.18	7	90.01	1.81	0.24	0.00
7	41.01	1.91	0.65	0.19	7	91.01	1.97	0.13	0.00
7	42.01	1.49	0.99	0.04	7	92.01	1.80	0.25	0.00
7	43.01	1.30	0.91	0.00	7	93.01	1.80	0.29	0.00
7	44.01	1.48	0.45	0.02	7	94.01	1.80	0.28	0.00
7	45.01	1.48	0.44	0.02	7	95.01	1.97	0.07	0.00
7	46.01	1.30	0.83	0.01	7	96.01	1.80	0.27	0.00
7	47.01	1.62	0.47	0.00	7	97.01	1.80	0.32	0.01
7	48.01	1.62	0.45	0.00	7	98.01	1.80	0.30	0.00
7	49.01	1.58	0.45	0.00	7	99.01	1.97	0.18	0.01
7	50.01	1.62	0.42	0.00	7	100.01	1.97	0.20	0.02
7	51.01	1.62	0.61	0.01	7	101.01	1.97	0.12	0.00
7	52.01	1.62	0.27	0.02	7	102.01	1.80	0.26	0.00
7	53.01	1.62	0.51	0.00	7	103.01	1.97	0.13	0.00
7	54.01	1.62	0.35	0.01	7	104.01	1.80	0.26	0.00
7	55.01	1.62	0.34	0.01	7	105.01	1.97	0.16	0.01
7	56.01	1.62	0.25	0.03	7	106.01	1.80	0.30	0.00
7	57.01	1.62	0.28	0.02	7	107.01	1.83	0.28	0.00
7	58.01	1.62	0.34	0.01	7	108.01	1.97	0.18	0.01
7	59.01	1.62	0.33	0.01	7	109.01	1.85	0.26	0.01
7	60.01	1.62	0.32	0.01	7	110.01	1.78	0.28	0.00
7	61.01	1.62	0.34	0.01	7	111.01	1.97	0.14	0.00
7	62.01	1.62	0.25	0.03	7	112.01	1.67	0.29	0.01
7	63.01	1.62	0.25	0.03	7	113.01	1.71	0.45	0.01
7	64.01	1.62	0.33	0.01	7	114.01	1.62	0.38	0.00
7	65.01	1.62	0.30	0.01	7	115.01	1.82	0.39	0.02
7	66.01	1.62	0.30	0.01	7	116.01	1.60	0.50	0.00
7	67.01	1.62	0.28	0.02	7	117.01	1.67	0.24	0.02
7	68.01	1.62	0.30	0.02	7	118.01	1.59	0.52	0.00
7	69.01	1.62	0.23	0.04	7	119.01	1.59	0.48	0.00
7	70.01	1.62	0.27	0.02	7	120.01	1.86	0.11	0.01
7	71.01	1.83	0.25	0.00	7	121.01	1.59	0.38	0.01
7	72.01	1.66	0.21	0.03	7	122.01	1.95	0.15	0.00
7	73.01	1.83	0.24	0.00	7	123.01	1.59	0.34	0.01
7	74.01	1.83	0.28	0.00	7	124.01	1.95	0.12	0.00
7	75.01	1.83	0.30	0.01	7	125.01	1.95	0.08	0.00
7	76.01	1.83	0.28	0.01	7	126.01	1.95	0.04	0.02
7	77.01	1.83	0.27	0.00	7	127.01	1.95	0.06	0.01
7	78.01	1.83	0.32	0.01	7	128.01	1.95	0.06	0.01
7	79.01	1.83	0.33	0.01	7	129.01	1.95	0.04	0.02

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	130.01	1.95	0.02	0.04	7	181.01	2.13	0.12	0.03
7	131.01	1.59	0.21	0.06	7	182.01	2.13	0.12	0.03
7	132.01	1.59	0.22	0.06	7	183.01	2.49	0.02	0.00
7	133.01	1.95	0.02	0.04	7	184.01	2.49	0.02	0.00
7	134.01	1.59	0.25	0.04	7	185.01	2.49	0.03	0.00
7	135.01	1.95	0.02	0.03	7	186.01	2.49	0.04	0.00
7	136.01	1.95	0.03	0.03	7	187.01	2.13	0.06	0.01
7	137.01	1.95	0.04	0.02	7	188.01	2.13	0.04	0.00
7	138.01	1.95	0.03	0.03	7	189.01	2.49	0.06	0.00
7	139.01	1.95	0.01	0.05	7	190.01	2.49	0.05	0.00
7	140.01	1.59	0.42	0.00	7	191.01	2.07	0.00	0.04
7	141.01	1.95	0.01	0.06	7	192.01	2.49	0.05	0.00
7	142.01	1.59	0.36	0.01	7	193.01	2.33	0.01	0.00
7	143.01	1.59	0.30	0.03	7	194.01	2.07	0.00	0.07
7	144.01	1.59	0.09	0.16	7	195.01	2.46	0.02	0.00
7	145.01	1.95	0.02	0.04	7	196.01	2.46	0.02	0.00
7	146.01	1.69	0.03	0.19	7	197.01	2.49	0.03	0.00
7	147.01	2.10	0.00	0.02	7	198.01	2.46	0.00	0.01
7	148.01	2.23	0.08	0.05	7	199.01	2.20	0.03	0.07
7	149.01	2.23	0.01	0.00	7	200.01	2.46	0.01	0.01
7	150.01	2.23	0.01	0.00	7	201.01	2.46	0.01	0.01
7	151.01	2.23	0.00	0.00	7	202.01	2.46	0.00	0.01
7	152.01	2.23	0.01	0.00	7	203.01	2.46	0.00	0.03
7	153.01	2.23	0.01	0.00	7	204.01	2.46	0.00	0.03
7	154.01	2.23	0.01	0.00	7	205.01	2.46	0.00	0.04
7	155.01	2.26	0.01	0.01	7	206.01	2.44	0.01	0.00
7	156.01	2.18	0.01	0.00	7	207.01	2.33	0.02	0.01
7	157.01	2.18	0.01	0.00	7	208.01	2.40	0.00	0.00
7	158.01	2.18	0.01	0.00	7	209.01	2.31	0.01	0.01
7	159.01	2.18	0.00	0.00	7	210.01	2.40	0.01	0.00
7	160.01	2.18	0.00	0.00	7	211.01	2.40	0.04	0.01
7	161.01	2.18	0.01	0.00	7	212.01	2.47	0.03	0.00
7	162.01	2.18	0.00	0.00	7	213.01	2.33	0.03	0.02
7	163.01	2.18	0.01	0.00	7	214.01	2.30	0.01	0.01
7	164.01	2.18	0.00	0.00	7	215.01	2.40	0.01	0.00
7	165.01	2.18	0.00	0.00	7	216.01	2.40	0.00	0.01
7	166.01	2.18	0.00	0.01	7	217.01	2.40	0.00	0.01
7	167.01	2.18	0.02	0.00	7	218.01	2.40	0.00	0.00
7	168.01	2.18	0.00	0.01	7	219.01	2.40	0.00	0.01
7	169.01	1.99	0.03	0.02	7	220.01	2.40	0.00	0.00
7	171.01	2.13	0.03	0.00	7	221.01	2.40	0.01	0.00
7	172.01	2.38	0.04	0.01	7	222.01	2.40	0.00	0.00
7	173.01	2.13	0.18	0.07	7	223.01	2.40	0.00	0.01
7	174.01	2.49	0.03	0.00	7	224.01	2.40	0.00	0.01
7	175.01	2.13	0.15	0.05	7	225.01	2.37	0.00	0.02
7	176.01	2.13	0.12	0.03	7	226.01	2.22	0.00	0.00
7	177.01	2.49	0.03	0.00	7	227.01	2.22	0.00	0.00
7	178.01	2.49	0.03	0.00	7	228.01	2.22	0.00	0.00
7	179.01	2.49	0.02	0.00	7	229.01	2.22	0.01	0.00
7	180.01	2.49	0.02	0.01	7	230.01	2.22	0.01	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	231.01	2.39	0.00	0.03	7	281.01	2.37	0.00	0.00
7	232.01	2.14	0.02	0.00	7	282.01	2.15	0.03	0.00
7	233.01	2.22	0.02	0.01	7	283.01	2.15	0.04	0.00
7	234.01	2.05	0.05	0.00	7	284.01	2.15	0.04	0.00
7	235.01	2.05	0.06	0.00	7	285.01	2.37	0.00	0.01
7	236.01	2.13	0.00	0.05	7	286.01	2.37	0.00	0.02
7	237.01	2.36	0.03	0.01	7	287.01	2.37	0.00	0.01
7	238.01	2.35	0.00	0.00	7	288.01	2.27	0.00	0.00
7	239.01	2.35	0.00	0.00	7	289.01	2.08	0.00	0.04
7	240.01	2.35	0.00	0.00	7	290.01	2.38	0.00	0.00
7	241.01	2.35	0.00	0.00	7	291.01	2.27	0.45	0.42
7	242.01	2.35	0.00	0.01	7	292.01	2.27	0.05	0.04
7	243.01	2.35	0.01	0.02	7	293.01	2.35	0.00	0.01
7	244.01	2.21	0.00	0.00	7	294.01	2.35	0.00	0.00
7	245.01	2.22	0.00	0.00	7	295.01	2.35	0.00	0.01
7	246.01	2.35	0.01	0.02	7	296.01	2.13	0.01	0.00
7	247.01	2.49	0.02	0.00	7	297.01	2.27	0.00	0.00
7	248.01	2.22	0.00	0.00	7	298.01	2.21	0.43	0.33
7	249.01	2.44	0.01	0.00	7	299.01	2.27	0.00	0.00
7	250.01	2.22	0.03	0.01	7	300.01	2.26	0.00	0.00
7	251.01	2.44	0.01	0.00	7	301.01	1.59	0.28	0.03
7	252.01	2.44	0.01	0.00	7	302.01	1.84	0.01	0.27
7	253.01	2.31	0.01	0.01	7	303.01	.		
7	254.01	2.44	0.01	0.00	7	304.01	1.63	0.09	0.13
7	255.01	2.44	0.01	0.00	7	305.01	1.74	0.01	0.20
7	256.01	2.41	0.00	0.01	7	306.01	2.14	0.01	0.00
7	257.01	2.41	0.01	0.00	7	307.01	2.19	0.01	0.00
7	258.01	2.41	0.00	0.01	7	308.01	2.05	0.04	0.00
7	259.01	2.41	0.00	0.02	7	309.01	2.05	0.06	0.24
7	260.01	2.41	0.00	0.01	7	310.01	2.54	0.06	0.00
7	261.01	2.41	0.00	0.02	7	311.01	2.39	0.00	0.02
7	262.01	2.41	0.00	0.00	7	312.01	2.04	0.29	0.61
7	263.01	2.41	0.00	0.01	7	313.01	2.30	0.88	0.86
7	264.01	2.41	0.00	0.02	7	314.01	2.54	0.03	0.01
7	265.01	2.41	0.00	0.01	7	315.01	2.54	0.03	0.01
7	266.01	2.41	0.00	0.02	7	316.01	2.54	0.05	0.00
7	267.01	2.41	0.00	0.01	7	317.01	3.23	0.62	0.02
7	268.01	2.41	0.00	0.01	7	318.01	2.54	0.06	0.00
7	269.01	2.41	0.00	0.01	7	319.01	2.54	0.01	0.02
7	270.01	2.15	0.01	0.00	7	320.01	3.23	0.45	0.07
7	271.01	2.41	0.00	0.01	7	321.01	2.54	0.07	0.00
7	272.01	2.41	0.00	0.01	7	322.01	3.23	0.23	0.21
7	273.01	2.32	0.02	0.03	7	323.01	3.23	0.41	0.09
7	274.01	2.37	0.02	0.00	7	324.01	2.11	0.12	0.27
7	275.01	2.33	0.01	0.00	7	325.01	2.64	0.29	0.04
7	276.01	2.15	0.01	0.00	7	326.01	2.64	0.39	0.08
7	277.01	2.15	0.01	0.00	7	327.01	2.64	0.27	0.03
7	278.01	2.37	0.00	0.01	7	328.01	2.64	0.33	0.05
7	279.01	2.37	0.00	0.00	7	329.01	2.64	0.19	0.01
7	280.01	2.37	0.00	0.01	7	330.01	2.64	0.31	0.04

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	331.01	2.64	0.19	0.01	7	381.01	2.27	0.00	0.00
7	332.01	2.64	0.14	0.00	7	382.01	2.27	0.01	0.00
7	333.01	3.23	0.52	0.05	7	383.01	2.27	0.00	0.00
7	334.01	3.23	0.32	0.14	7	384.01	2.27	0.00	0.00
7	335.01	2.64	0.06	0.01	7	385.01	2.19	0.00	0.00
7	336.01	3.23	0.25	0.19	7	386.01	2.27	0.01	0.01
7	337.01	3.23	0.35	0.12	7	387.01	2.37	0.00	0.00
7	338.01	3.23	0.46	0.07	7	388.01	2.24	0.01	0.00
7	339.01	2.64	0.37	0.07	7	389.01	2.35	0.00	0.00
7	340.01	2.64	0.28	0.03	7	390.01	2.29	0.00	0.00
7	341.01	2.64	0.09	0.00	7	391.01	2.22	0.00	0.01
7	342.01	2.64	0.09	0.00	7	392.01	2.29	0.00	0.00
7	343.01	2.31	2.77	2.72	7	393.01	2.29	0.00	0.00
7	344.01	3.95	2.43	0.01	7	394.01	2.29	0.00	0.00
7	345.01	2.64	0.06	0.01	7	395.01	2.29	0.00	0.00
7	346.01	2.64	0.21	0.01	7	396.01	2.29	0.01	0.01
7	347.01	2.64	0.01	0.06	7	397.01	2.29	0.01	0.01
7	348.01	2.64	0.12	0.00	7	398.01	2.29	0.01	0.01
7	349.01	2.64	0.02	0.04	7	399.01	2.29	0.00	0.00
7	350.01	2.64	0.14	0.00	7	400.01	2.29	0.02	0.02
7	351.01	2.52	0.00	0.04	7	401.01	2.29	0.01	0.01
7	352.01	2.64	0.09	0.00	7	402.01	2.29	0.01	0.01
7	353.01	2.32	0.01	0.00	7	403.01	2.29	0.01	0.01
7	354.01	2.64	0.06	0.01	7	404.01	2.29	0.00	0.00
7	355.01	2.32	0.03	0.04	7	405.01	2.30	0.00	0.00
7	356.01	2.32	0.07	0.09	7	406.01	2.25	0.00	0.00
7	357.01	2.64	0.07	0.01	7	407.01	2.29	0.00	0.00
7	358.01	2.32	0.08	0.10	7	408.01	2.23	0.00	0.00
7	359.01	2.64	0.05	0.02	7	409.01	2.29	0.00	0.00
7	360.01	2.64	0.05	0.02	7	410.01	2.29	0.02	0.02
7	361.01	2.32	0.14	0.16	7	411.01	2.29	0.02	0.02
7	362.01	2.64	0.03	0.03	7	412.01	2.29	0.01	0.01
7	363.01	2.32	0.15	0.18	7	413.01	2.29	0.02	0.02
7	364.01	2.32	0.08	0.10	7	414.01	2.29	0.03	0.03
7	365.01	2.79	0.03	0.11	7	415.01	2.29	0.02	0.02
7	366.01	2.27	0.00	0.00	7	416.01	2.29	0.03	0.03
7	367.01	2.46	0.07	0.01	7	417.01	2.29	0.04	0.04
7	368.01	2.46	0.05	0.00	7	418.01	2.29	0.02	0.02
7	369.01	2.46	0.04	0.00	7	419.01	2.29	0.02	0.02
7	370.01	2.46	0.02	0.00	7	420.01	2.29	0.01	0.01
7	371.01	2.46	0.00	0.02	7	421.01	2.29	0.02	0.02
7	372.01	2.27	0.00	0.00	7	422.01	2.29	0.01	0.01
7	373.01	2.46	0.03	0.00	7	423.01	2.29	0.03	0.03
7	374.01	2.46	0.01	0.01	7	424.01	2.29	0.04	0.04
7	375.01	2.46	0.00	0.04	7	425.01	2.29	0.06	0.06
7	376.01	2.61	0.00	0.12	7	426.01	2.29	0.04	0.04
7	377.01	2.27	0.00	0.00	7	427.01	2.29	0.04	0.04
7	378.01	2.25	0.00	0.00	7	428.01	2.29	0.08	0.08
7	379.01	2.27	0.00	0.00	7	429.01	2.19	0.13	0.06
7	380.01	2.27	0.00	0.00	7	430.01	2.40	0.04	0.10

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	431.01	2.16	0.07	0.02	7	481.01	1.91	0.09	0.01
7	432.01	2.03	0.08	0.00	7	482.01	1.99	0.14	0.01
7	433.01	2.03	0.06	0.00	7	483.01	1.99	0.09	0.00
7	434.01	2.03	0.04	0.00	7	484.01	1.99	0.08	0.00
7	435.01	2.03	0.09	0.00	7	485.01	1.99	0.13	0.00
7	436.01	2.03	0.02	0.01	7	486.01	1.99	0.08	0.00
7	437.01	2.03	0.04	0.00	7	487.01	1.99	0.09	0.00
7	438.01	2.03	0.06	0.00	7	488.01	1.99	0.07	0.00
7	439.01	2.03	0.03	0.01	7	489.01	1.99	0.08	0.00
7	440.01	2.03	0.05	0.00	7	490.01	1.99	0.06	0.00
7	441.01	2.03	0.07	0.00	7	491.01	1.99	0.07	0.00
7	442.01	2.03	0.04	0.00	7	492.01	1.99	0.05	0.01
7	443.01	2.03	0.05	0.00	7	493.01	1.99	0.07	0.00
7	444.01	1.83	0.05	0.05	7	494.01	1.76	0.11	0.04
7	445.01	2.03	0.04	0.00	7	495.01	2.11	0.02	0.00
7	446.01	2.06	0.05	0.00	7	496.01	2.09	0.03	0.00
7	447.01	2.03	0.01	0.03	7	497.01	1.92	0.02	0.05
7	448.01	2.06	0.05	0.00	7	498.01	2.15	0.02	0.00
7	449.01	2.14	0.01	0.00	7	499.01	2.09	0.06	0.00
7	450.01	2.18	0.00	0.01	7	500.01	2.09	0.01	0.01
7	451.01	2.06	0.03	0.00	7	501.01	2.13	0.04	0.00
7	452.01	2.18	0.00	0.01	7	502.01	2.09	0.08	0.01
7	453.01	2.18	0.00	0.00	7	503.01	2.17	0.02	0.00
7	454.01	2.06	0.05	0.00	7	504.01	1.94	0.08	0.01
7	455.01	2.18	0.01	0.00	7	505.01	2.15	0.01	0.00
7	456.01	2.20	0.06	0.02	7	506.01	2.01	0.06	0.00
7	457.01	2.18	0.01	0.00	7	507.01	2.02	0.03	0.01
7	458.01	2.20	0.05	0.02	7	508.01	2.12	0.03	0.00
7	459.01	2.04	0.05	0.00	7	509.01	2.12	0.02	0.00
7	460.01	1.99	0.01	0.04	7	510.01	2.12	0.05	0.00
7	461.01	2.20	0.01	0.00	7	511.01	2.12	0.03	0.00
7	462.01	2.06	0.35	0.13	7	512.01	2.12	0.03	0.00
7	463.01	2.20	0.01	0.00	7	513.01	2.12	0.04	0.00
7	464.01	2.17	0.02	0.00	7	514.01	1.94	0.07	0.01
7	465.01	2.22	0.01	0.00	7	515.01	2.21	0.02	0.01
7	466.01	2.31	0.01	0.01	7	516.01	2.10	0.04	0.00
7	467.01	2.21	0.00	0.00	7	517.01	2.09	0.07	0.01
7	468.01	2.21	0.01	0.00	7	518.01	2.09	0.05	0.00
7	469.01	2.24	0.08	0.05	7	519.01	2.09	0.03	0.00
7	470.01	2.01	0.08	0.00	7	520.01	2.09	0.12	0.02
7	471.01	2.01	0.06	0.00	7	521.01	2.09	0.12	0.02
7	472.01	2.01	0.06	0.00	7	522.01	2.09	0.02	0.00
7	473.01	2.01	0.05	0.00	7	523.01	1.97	0.11	0.00
7	474.01	2.01	0.05	0.00	7	524.01	1.95	0.08	0.00
7	475.01	2.01	0.08	0.00	7	525.01	1.95	0.11	0.00
7	476.01	2.01	0.05	0.00	7	526.01	1.95	0.15	0.00
7	477.01	2.01	0.07	0.00	7	527.01	2.18	0.03	0.00
7	478.01	2.01	0.12	0.00	7	528.01	2.11	0.01	0.01
7	479.01	2.01	0.05	0.00	7	529.01	2.11	0.00	0.01
7	480.01	1.99	0.09	0.00	7	530.01	1.95	0.09	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	531.01	2.11	0.00	0.02	7	581.01	2.16	0.05	0.01
7	532.01	1.95	0.15	0.00	7	582.01	2.16	0.05	0.01
7	533.01	2.11	0.00	0.02	7	583.01	2.16	0.07	0.02
7	534.01	2.11	0.00	0.02	7	584.01	2.16	0.06	0.01
7	535.01	2.01	0.01	0.03	7	585.01	2.16	0.06	0.01
7	536.01	2.11	0.03	0.00	7	586.01	2.16	0.06	0.01
7	537.01	2.19	0.01	0.00	7	587.01	2.16	0.07	0.02
7	538.01	2.19	0.01	0.00	7	588.01	2.16	0.09	0.03
7	539.01	2.19	0.01	0.00	7	589.01	2.16	0.06	0.01
7	540.01	2.18	0.01	0.00	7	590.01	2.16	0.08	0.02
7	541.01	2.18	0.01	0.00	7	591.01	2.16	0.09	0.03
7	542.01	2.18	0.01	0.00	7	592.01	2.16	0.08	0.02
7	543.01	2.18	0.01	0.00	7	593.01	2.16	0.06	0.01
7	544.01	2.18	0.01	0.00	7	594.01	2.16	0.08	0.02
7	545.01	2.18	0.01	0.00	7	595.01	2.16	0.07	0.02
7	546.01	2.18	0.01	0.00	7	596.01	2.16	0.06	0.01
7	547.01	2.18	0.02	0.00	7	597.01	2.16	0.07	0.02
7	548.01	2.18	0.02	0.00	7	598.01	2.16	0.11	0.04
7	549.01	2.18	0.01	0.00	7	599.01	2.16	0.07	0.02
7	550.01	2.18	0.01	0.00	7	600.01	2.02	0.09	0.00
7	551.01	2.18	0.03	0.00	7	601.01	2.01	0.07	0.00
7	552.01	2.18	0.01	0.00	7	602.01	2.02	0.08	0.00
7	553.01	2.18	0.03	0.01	7	603.01	2.02	0.10	0.00
7	554.01	2.18	0.02	0.00	7	604.01	2.02	0.09	0.00
7	555.01	2.18	0.03	0.01	7	605.01	2.02	0.07	0.00
7	556.01	2.18	0.04	0.01	7	606.01	2.02	0.08	0.00
7	557.01	2.18	0.01	0.00	7	607.01	2.02	0.07	0.00
7	558.01	2.18	0.01	0.00	7	608.01	2.02	0.07	0.00
7	559.01	2.18	0.02	0.00	7	609.01	2.02	0.09	0.00
7	560.01	2.18	0.03	0.00	7	610.01	2.02	0.13	0.01
7	561.01	2.18	0.03	0.00	7	611.01	2.02	0.08	0.00
7	562.01	2.18	0.04	0.01	7	612.01	2.02	0.09	0.00
7	563.01	2.18	0.05	0.01	7	613.01	2.02	0.07	0.00
7	564.01	2.23	0.00	0.00	7	614.01	2.02	0.10	0.00
7	565.01	2.17	0.00	0.00	7	615.01	2.02	0.11	0.00
7	566.01	2.23	0.00	0.00	7	616.01	2.02	0.08	0.00
7	567.01	2.23	0.00	0.00	7	617.01	2.02	0.10	0.00
7	568.01	2.23	0.00	0.00	7	618.01	2.02	0.09	0.00
7	569.01	2.23	0.00	0.00	7	619.01	2.02	0.04	0.00
7	570.01	2.23	0.01	0.00	7	620.01	2.02	0.03	0.01
7	571.01	2.23	0.00	0.00	7	621.01	2.02	0.04	0.00
7	572.01	2.23	0.01	0.00	7	622.01	2.02	0.06	0.00
7	573.01	2.23	0.00	0.00	7	623.01	2.02	0.08	0.00
7	574.01	2.13	0.02	0.00	7	624.01	2.02	0.05	0.00
7	575.01	2.16	0.01	0.00	7	625.01	2.02	0.05	0.00
7	576.01	2.16	0.08	0.02	7	626.01	2.02	0.02	0.02
7	577.01	2.16	0.03	0.00	7	627.01	2.02	0.03	0.01
7	578.01	2.16	0.05	0.01	7	628.01	1.92	0.03	0.03
7	579.01	2.16	0.06	0.01	7	629.01	2.04	0.03	0.01
7	580.01	2.16	0.05	0.01	7	630.01	2.11	0.03	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	631.01	1.97	0.02	0.03	7	37.02	1.30	1.00	0.00
7	632.01	2.14	0.03	0.00	7	38.02	1.33	1.09	0.01
7	633.01	2.14	0.03	0.00	7	39.02	1.21	1.38	0.01
7	634.01	2.14	0.00	0.01	7	40.02	1.21	0.97	0.01
7	635.01	2.14	0.03	0.00	7	41.02	1.69	0.52	0.01
7	636.01	2.04	0.04	0.00	7	42.02	1.67	0.48	0.00
7	637.01	2.09	0.15	0.04	7	43.02	1.63	0.81	0.06
7	638.01	2.09	0.07	0.00	7	45.02	1.42	0.39	0.06
7	639.01	2.09	0.09	0.01	7	46.02	1.87	0.41	0.05
7	640.01	2.09	0.05	0.00	7	47.02	1.39	0.75	0.00
7	641.01	2.03	0.08	0.00	7	48.02	1.65	0.57	0.01
7	642.01	1.96	0.07	0.01	7	52.02	1.89	0.43	0.06
7	643.01	2.03	0.09	0.00	7	53.02	1.83	0.32	0.01
7	644.01	1.83	0.66	0.12	7	54.02	1.68	0.38	0.00
7	645.01	1.91	0.17	0.00	7	55.02	1.75	0.37	0.00
7	646.01	1.30	0.06	0.56	7	56.02	1.88	0.23	0.00
7	647.01	2.03	0.11	0.01	7	57.02	1.68	0.37	0.00
7	648.01	0.99	1.25	0.03	7	58.02	1.68	0.35	0.00
7	649.01	1.37	1.14	0.02	7	59.02	1.68	0.34	0.00
7	650.01	1.11	1.34	0.00	7	60.02	1.68	0.35	0.00
7	651.01	1.02	1.36	0.01	7	61.02	1.68	0.36	0.00
7	652.01	1.07	0.44	0.31	7	62.02	1.68	0.37	0.00
7	653.01	1.62	0.43	0.00	7	63.02	1.68	0.36	0.00
7	654.01	1.62	0.49	0.00	7	64.02	1.68	0.32	0.00
7	655.01	1.48	0.57	0.00	7	65.02	1.68	0.37	0.00
7	656.01	1.43	2.71	0.62	7	67.02	1.86	0.28	0.01
7	657.01	1.40	0.45	0.05	7	68.02	1.63	0.34	0.01
7	658.01	0.58	1.26	0.34	7	69.02	1.76	0.26	0.00
7	659.01	1.02	1.33	0.01	7	70.02	1.71	0.36	0.00
7	661.01	0.92	0.57	0.37	7	71.02	1.76	0.36	0.01
7	662.01	1.53	0.35	0.03	7	72.02	1.71	0.40	0.00
7	663.01	1.44	1.35	0.10	7	73.02	1.76	0.38	0.01
7	664.01	0.86	1.37	0.07	7	74.02	1.68	0.43	0.00
7	665.01	1.48	0.35	0.05	7	77.02	1.58	0.47	0.00
7	3.02	0.99	1.91	0.01	7	78.02	1.60	0.46	0.00
7	4.02	0.94	2.67	0.08	7	79.02	1.78	0.16	0.01
7	18.02	0.76	0.76	0.44	7	80.02	1.60	0.43	0.00
7	19.02	1.47	0.89	0.01	7	81.02	1.60	0.41	0.00
7	20.02	1.41	1.21	0.05	7	84.02	1.81	0.10	0.03
7	23.02	1.34	1.25	0.03	7	86.02	1.98	0.11	0.00
7	24.02	1.27	0.96	0.00	7	87.02	1.78	0.06	0.06
7	25.02	1.17	1.21	0.00	7	88.02	2.04	0.07	0.00
7	28.02	1.21	0.95	0.01	7	89.02	2.23	0.08	0.06
7	30.02	1.21	1.11	0.00	7	90.02	1.98	0.20	0.02
7	31.02	1.37	1.15	0.02	7	91.02	2.00	0.11	0.00
7	32.02	1.43	0.94	0.01	7	92.02	1.85	0.18	0.00
7	33.02	1.22	1.11	0.00	7	93.02	1.85	0.15	0.00
7	34.02	1.27	0.98	0.00	7	94.02	1.85	0.17	0.00
7	35.02	1.30	1.03	0.00	7	95.02	2.00	0.11	0.00
7	36.02	1.30	1.04	0.00	7	96.02	1.85	0.17	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	97.02	1.85	0.21	0.00	7	160.02	2.46	0.02	0.00
7	98.02	1.85	0.15	0.00	7	161.02	2.46	0.02	0.00
7	99.02	2.00	0.09	0.00	7	162.02	2.39	0.00	0.01
7	100.02	2.00	0.08	0.00	7	163.02	2.46	0.01	0.00
7	101.02	2.00	0.07	0.00	7	164.02	2.39	0.00	0.01
7	102.02	2.15	0.08	0.02	7	165.02	2.62	0.04	0.02
7	104.02	1.93	0.12	0.00	7	166.02	2.48	0.03	0.00
7	105.02	2.20	0.03	0.01	7	167.02	2.31	0.00	0.00
7	106.02	1.95	0.09	0.00	7	168.02	2.48	0.03	0.00
7	107.02	1.95	0.11	0.00	7	169.02	2.31	0.00	0.00
7	109.02	1.95	0.11	0.00	7	171.02	2.31	0.00	0.01
7	110.02	2.14	0.08	0.02	7	173.02	2.31	0.00	0.00
7	111.02	2.19	0.02	0.00	7	175.02	2.31	0.00	0.00
7	112.02	2.01	0.04	0.01	7	176.02	2.31	0.00	0.00
7	116.02	2.13	0.06	0.16	7	177.02	2.64	0.13	0.00
7	117.02	2.17	0.05	0.11	7	178.02	2.64	0.12	0.00
7	118.02	2.27	0.00	0.00	7	179.02	2.64	0.14	0.00
7	119.02	1.89	0.00	0.15	7	180.02	2.64	0.12	0.00
7	121.02	2.27	0.02	0.02	7	181.02	2.31	0.00	0.01
7	123.02	2.27	0.02	0.02	7	182.02	2.31	0.02	0.03
7	124.02	2.13	0.07	0.19	7	183.02	2.64	0.11	0.00
7	126.02	2.57	0.03	0.02	7	184.02	2.64	0.10	0.00
7	127.02	2.17	0.02	0.07	7	185.02	2.64	0.09	0.00
7	128.02	2.44	0.01	0.00	7	186.02	2.64	0.09	0.00
7	129.02	2.05	0.02	0.14	7	187.02	2.31	0.02	0.03
7	130.02	2.45	0.03	0.00	7	188.02	2.31	0.02	0.03
7	131.02	2.44	0.00	0.01	7	191.02	2.76	0.19	0.00
7	132.02	2.36	0.01	0.00	7	192.02	2.61	0.22	0.02
7	133.02	2.45	0.02	0.00	7	193.02	2.31	0.01	0.01
7	134.02	2.33	0.00	0.01	7	194.02	2.31	0.00	0.01
7	139.02	2.56	0.08	0.00	7	195.02	2.31	0.01	0.01
7	140.02	2.27	0.06	0.05	7	196.02	2.76	0.27	0.00
7	141.02	2.57	0.08	0.00	7	197.02	2.76	0.25	0.00
7	142.02	2.29	0.00	0.00	7	198.02	2.31	0.00	0.00
7	143.02	2.33	0.00	0.00	7	199.02	2.76	0.25	0.00
7	144.02	2.57	0.06	0.00	7	200.02	2.76	0.32	0.01
7	145.02	2.57	0.07	0.00	7	201.02	2.76	0.31	0.01
7	146.02	2.57	0.04	0.01	7	202.02	2.76	0.30	0.01
7	148.02	2.56	0.04	0.00	7	203.02	2.76	0.33	0.01
7	149.02	2.49	0.08	0.00	7	204.02	2.44	0.20	0.09
7	150.02	2.56	0.06	0.00	7	205.02	2.74	0.14	0.01
7	151.02	2.56	0.06	0.00	7	207.02	2.74	0.07	0.03
7	152.02	2.56	0.06	0.00	7	208.02	2.67	0.14	0.00
7	153.02	2.59	0.04	0.01	7	209.02	2.84	0.14	0.03
7	154.02	2.49	0.04	0.00	7	210.02	2.67	0.14	0.00
7	155.02	2.38	0.03	0.01	7	211.02	2.67	0.09	0.01
7	156.02	2.46	0.03	0.00	7	212.02	2.67	0.11	0.00
7	157.02	2.46	0.03	0.00	7	213.02	2.67	0.11	0.00
7	158.02	2.46	0.02	0.00	7	214.02	2.57	0.09	0.00
7	159.02	2.46	0.02	0.00	7	215.02	2.78	0.15	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	216.02	2.57	0.15	0.01	7	269.02	2.80	0.22	0.00
7	217.02	2.82	0.16	0.02	7	270.02	2.68	0.05	0.03
7	218.02	2.67	0.15	0.00	7	272.02	2.71	0.16	0.00
7	219.02	2.69	0.19	0.00	7	273.02	2.68	0.04	0.03
7	220.02	2.78	0.17	0.01	7	274.02	2.85	0.27	0.00
7	221.02	2.67	0.09	0.01	7	275.02	2.95	0.32	0.01
7	222.02	2.67	0.09	0.01	7	276.02	2.68	0.04	0.03
7	223.02	2.85	0.21	0.01	7	277.02	2.68	0.04	0.03
7	224.02	2.75	0.19	0.00	7	278.02	2.85	0.23	0.01
7	225.02	2.59	0.14	0.01	7	279.02	2.85	0.22	0.01
7	226.02	2.81	0.20	0.01	7	280.02	2.85	0.25	0.00
7	227.02	2.66	0.10	0.00	7	281.02	2.85	0.26	0.00
7	228.02	2.73	0.17	0.00	7	282.02	2.50	0.01	0.02
7	229.02	2.66	0.12	0.00	7	283.02	2.50	0.01	0.02
7	230.02	2.73	0.18	0.00	7	284.02	2.50	0.00	0.03
7	231.02	2.66	0.08	0.01	7	285.02	2.72	0.12	0.01
7	232.02	2.73	0.13	0.01	7	286.02	2.65	0.19	0.00
7	233.02	2.73	0.13	0.01	7	287.02	2.76	0.13	0.01
7	234.02	2.66	0.19	0.00	7	288.02	2.50	0.00	0.07
7	235.02	2.66	0.19	0.00	7	289.02	2.50	0.00	0.06
7	236.02	2.81	0.22	0.00	7	290.02	2.65	0.08	0.01
7	240.02	2.84	0.40	0.01	7	291.02	2.52	0.09	0.28
7	241.02	2.66	0.32	0.04	7	292.02	2.54	0.19	0.47
7	242.02	2.66	0.28	0.02	7	293.02	2.65	0.05	0.02
7	243.02	2.66	0.23	0.01	7	294.02	2.65	0.07	0.01
7	244.02	2.66	0.19	0.00	7	295.02	2.65	0.04	0.02
7	245.02	2.66	0.19	0.00	7	296.02	2.65	0.02	0.04
7	246.02	2.92	0.57	0.01	7	297.02	2.65	0.04	0.02
7	247.02	2.92	0.37	0.00	7	298.02	2.52	0.15	0.03
7	248.02	2.66	0.19	0.00	7	299.02	2.65	0.02	0.05
7	249.02	2.92	0.41	0.00	7	300.02	2.65	0.00	0.10
7	250.02	2.66	0.23	0.01	7	301.02	2.68	0.16	0.00
7	251.02	2.92	0.34	0.00	7	302.02	2.61	0.10	0.00
7	252.02	2.92	0.38	0.00	7	303.02	2.65	0.09	0.00
7	253.02	2.69	0.31	0.03	7	304.02	2.48	0.09	0.01
7	254.02	2.92	0.38	0.00	7	305.02	2.76	0.14	0.01
7	255.02	2.92	0.41	0.00	7	306.02	2.58	0.07	0.00
7	256.02	2.85	0.24	0.00	7	307.02	2.58	0.09	0.00
7	257.02	2.85	0.26	0.00	7	308.02	2.58	0.08	0.00
7	258.02	3.04	0.26	0.06	7	309.02	2.58	0.06	0.00
7	259.02	2.76	0.21	0.00	7	310.02	2.58	0.04	0.01
7	260.02	2.75	0.17	0.00	7	311.02	2.65	0.05	0.02
7	261.02	2.75	0.17	0.00	7	312.02	2.67	0.08	0.01
7	262.02	2.85	0.22	0.01	7	313.02	2.67	0.13	0.00
7	263.02	2.75	0.19	0.00	7	314.02	2.58	0.05	0.00
7	264.02	2.75	0.16	0.01	7	315.02	2.58	0.06	0.00
7	265.02	2.75	0.19	0.00	7	316.02	2.58	0.06	0.00
7	266.02	2.65	0.16	0.00	7	317.02	2.67	0.12	0.00
7	267.02	2.95	0.22	0.04	7	318.02	2.58	0.07	0.00
7	268.02	2.76	0.16	0.00	7	319.02	2.58	0.12	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	320.02	2.67	0.14	0.00	7	370.02	2.65	0.14	0.00
7	321.02	2.54	0.06	0.00	7	371.02	2.81	0.19	0.01
7	322.02	2.67	0.19	0.00	7	372.02	2.54	0.10	0.00
7	323.02	2.67	0.14	0.00	7	373.02	2.65	0.14	0.00
7	324.02	2.54	0.06	0.00	7	374.02	2.65	0.18	0.00
7	325.02	2.54	0.06	0.00	7	375.02	2.73	0.22	0.00
7	326.02	2.54	0.04	0.00	7	376.02	2.73	0.22	0.00
7	327.02	2.48	0.01	0.01	7	377.02	2.73	0.17	0.00
7	328.02	2.67	0.03	0.04	7	378.02	2.73	0.16	0.00
7	329.02	2.59	0.04	0.01	7	379.02	2.81	0.15	0.02
7	330.02	2.50	0.03	0.00	7	380.02	2.64	0.13	0.00
7	331.02	2.47	0.06	0.00	7	381.02	2.65	0.12	0.00
7	332.02	2.47	0.05	0.00	7	382.02	2.65	0.14	0.00
7	333.02	2.67	0.13	0.00	7	383.02	2.65	0.12	0.00
7	334.02	2.67	0.15	0.00	7	384.02	2.50	0.10	0.01
7	335.02	2.47	0.07	0.01	7	385.02	2.60	0.06	0.01
7	336.02	2.67	0.18	0.00	7	386.02	2.78	0.16	0.01
7	337.02	2.67	0.21	0.01	7	387.02	2.69	0.17	0.00
7	338.02	2.67	0.18	0.00	7	388.02	2.60	0.06	0.00
7	339.02	2.43	0.02	0.00	7	389.02	2.69	0.15	0.00
7	340.02	2.45	0.02	0.00	7	390.02	2.60	0.05	0.01
7	341.02	2.47	0.08	0.01	7	391.02	2.69	0.12	0.00
7	342.02	2.38	0.07	0.03	7	392.02	2.60	0.06	0.00
7	343.02	2.76	0.42	0.03	7	393.02	2.69	0.12	0.00
7	344.02	2.93	0.42	0.00	7	394.02	2.69	0.12	0.00
7	345.02	2.55	0.03	0.01	7	395.02	2.69	0.13	0.00
7	346.02	2.55	0.03	0.01	7	396.02	2.60	0.07	0.00
7	347.02	2.55	0.04	0.00	7	397.02	2.60	0.09	0.00
7	348.02	2.47	0.04	0.00	7	398.02	2.60	0.05	0.01
7	349.02	2.55	0.04	0.00	7	399.02	2.69	0.13	0.00
7	350.02	2.47	0.05	0.00	7	400.02	2.60	0.04	0.01
7	351.02	2.62	0.06	0.01	7	401.02	2.69	0.13	0.00
7	352.02	2.47	0.08	0.01	7	402.02	2.69	0.10	0.01
7	353.02	2.43	0.05	0.01	7	403.02	2.69	0.11	0.00
7	354.02	2.59	0.09	0.00	7	404.02	2.60	0.02	0.03
7	355.02	2.65	0.13	0.00	7	405.02	2.69	0.09	0.01
7	356.02	2.65	0.14	0.00	7	406.02	2.69	0.08	0.01
7	357.02	2.58	0.09	0.00	7	407.02	2.79	0.15	0.01
7	358.02	2.65	0.12	0.00	7	408.02	2.58	0.10	0.00
7	359.02	2.58	0.10	0.00	7	409.02	2.62	0.09	0.00
7	360.02	2.58	0.10	0.00	7	410.02	2.59	0.09	0.00
7	361.02	2.48	0.11	0.02	7	411.02	2.59	0.07	0.00
7	362.02	2.58	0.11	0.00	7	412.02	2.59	0.08	0.00
7	363.02	2.61	0.10	0.00	7	413.02	2.59	0.07	0.00
7	364.02	2.61	0.06	0.01	7	414.02	2.59	0.06	0.00
7	365.02	2.49	0.11	0.02	7	415.02	2.59	0.05	0.01
7	366.02	2.73	0.18	0.00	7	416.02	2.59	0.05	0.01
7	367.02	2.62	0.11	0.00	7	417.02	2.59	0.02	0.02
7	368.02	2.82	0.12	0.03	7	418.02	2.59	0.02	0.02
7	369.02	2.64	0.13	0.00	7	419.02	2.59	0.03	0.02

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	420.02	2.59	0.01	0.03	7	470.02	2.42	0.05	0.01
7	421.02	2.59	0.02	0.03	7	471.02	2.42	0.03	0.00
7	422.02	2.59	0.01	0.04	7	472.02	2.45	0.05	0.00
7	423.02	2.59	0.01	0.04	7	473.02	2.45	0.02	0.00
7	424.02	2.59	0.02	0.03	7	474.02	2.39	0.02	0.00
7	425.02	2.59	0.02	0.03	7	475.02	2.50	0.04	0.00
7	426.02	2.59	0.02	0.02	7	476.02	2.42	0.02	0.00
7	427.02	2.46	0.01	0.01	7	477.02	2.50	0.04	0.00
7	428.02	2.65	0.03	0.04	7	478.02	2.50	0.08	0.00
7	429.02	2.46	0.04	0.00	7	479.02	2.42	0.02	0.00
7	430.02	2.38	0.01	0.00	7	480.02	2.45	0.04	0.00
7	431.02	2.38	0.01	0.00	7	481.02	2.41	0.03	0.00
7	432.02	2.46	0.04	0.00	7	482.02	2.45	0.03	0.00
7	433.02	2.38	0.00	0.00	7	483.02	2.45	0.03	0.00
7	434.02	2.46	0.03	0.00	7	484.02	2.45	0.03	0.00
7	435.02	2.38	0.00	0.02	7	485.02	2.45	0.03	0.00
7	436.02	2.46	0.03	0.00	7	486.02	2.45	0.04	0.00
7	437.02	2.46	0.03	0.00	7	487.02	2.31	0.03	0.02
7	438.02	2.38	0.00	0.02	7	488.02	2.55	0.04	0.00
7	439.02	2.46	0.03	0.00	7	489.02	2.45	0.01	0.00
7	440.02	2.61	0.01	0.06	7	490.02	2.50	0.03	0.00
7	441.02	2.38	0.00	0.02	7	491.02	2.45	0.01	0.00
7	442.02	2.71	0.06	0.03	7	492.02	2.50	0.03	0.00
7	443.02	2.38	0.00	0.02	7	493.02	2.45	0.00	0.05
7	444.02	2.38	0.01	0.03	7	494.02	2.45	0.01	0.05
7	445.02	2.38	0.00	0.03	7	495.02	2.50	0.02	0.01
7	446.02	2.38	0.02	0.05	7	496.02	2.39	0.01	0.00
7	447.02	2.53	0.07	0.00	7	497.02	2.50	0.01	0.01
7	448.02	2.38	0.01	0.04	7	498.02	2.45	0.00	0.01
7	449.02	2.53	0.08	0.00	7	499.02	2.39	0.01	0.00
7	450.02	2.53	0.08	0.00	7	500.02	2.39	0.01	0.00
7	451.02	2.38	0.01	0.05	7	501.02	2.41	0.01	0.00
7	452.02	2.53	0.08	0.00	7	502.02	2.39	0.01	0.00
7	453.02	2.53	0.07	0.00	7	503.02	2.39	0.01	0.00
7	454.02	2.38	0.01	0.05	7	504.02	2.39	0.01	0.00
7	455.02	2.53	0.08	0.00	7	505.02	2.39	0.01	0.00
7	456.02	2.38	0.01	0.04	7	506.02	2.39	0.01	0.00
7	457.02	2.53	0.08	0.00	7	507.02	2.39	0.01	0.00
7	458.02	2.38	0.02	0.05	7	508.02	2.39	0.00	0.00
7	459.02	2.38	0.01	0.03	7	509.02	2.39	0.01	0.00
7	460.02	2.53	0.07	0.00	7	510.02	2.39	0.00	0.00
7	461.02	2.53	0.06	0.00	7	511.02	2.39	0.01	0.00
7	462.02	2.24	0.00	0.01	7	512.02	2.39	0.00	0.01
7	463.02	2.53	0.06	0.00	7	513.02	2.39	0.01	0.00
7	464.02	2.53	0.07	0.00	7	514.02	2.45	0.00	0.01
7	465.02	2.53	0.06	0.00	7	515.02	2.15	0.02	0.00
7	466.02	2.53	0.05	0.00	7	516.02	2.14	0.01	0.00
7	467.02	2.53	0.01	0.02	7	517.02	2.35	0.00	0.00
7	468.02	2.44	0.01	0.00	7	518.02	2.14	0.03	0.00
7	469.02	2.38	0.02	0.00	7	519.02	2.22	0.04	0.02

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	520.02	2.10	0.05	0.00	7	570.02	2.36	0.01	0.00
7	521.02	2.10	0.06	0.00	7	571.02	2.36	0.00	0.00
7	522.02	2.10	0.09	0.01	7	572.02	2.36	0.01	0.00
7	523.02	2.10	0.07	0.01	7	573.02	2.17	0.00	0.02
7	524.02	2.10	0.05	0.00	7	574.02	2.37	0.03	0.01
7	525.02	2.10	0.05	0.00	7	575.02	2.24	0.00	0.01
7	526.02	2.10	0.09	0.01	7	576.02	2.46	0.03	0.00
7	527.02	2.49	0.13	0.03	7	577.02	2.46	0.04	0.00
7	528.02	2.65	0.12	0.00	7	578.02	2.32	0.03	0.02
7	529.02	2.65	0.06	0.01	7	579.02	2.46	0.03	0.00
7	530.02	2.59	0.07	0.00	7	580.02	2.19	0.03	0.07
7	531.02	2.65	0.08	0.01	7	581.02	2.46	0.02	0.00
7	532.02	1.98	0.07	0.00	7	582.02	2.46	0.01	0.00
7	533.02	2.65	0.08	0.01	7	583.02	2.46	0.01	0.00
7	534.02	2.43	0.09	0.03	7	584.02	2.46	0.01	0.01
7	535.02	2.47	0.06	0.01	7	585.02	2.46	0.01	0.00
7	536.02	2.59	0.07	0.00	7	586.02	2.46	0.02	0.00
7	537.02	2.54	0.06	0.00	7	587.02	2.28	0.00	0.00
7	538.02	2.54	0.02	0.01	7	588.02	2.14	0.01	0.00
7	539.02	2.54	0.03	0.01	7	589.02	2.57	0.01	0.03
7	540.02	2.34	0.00	0.00	7	590.02	2.39	0.01	0.00
7	541.02	2.37	0.00	0.00	7	591.02	2.51	0.00	0.04
7	542.02	2.34	0.00	0.00	7	592.02	2.34	0.00	0.01
7	543.02	2.34	0.00	0.00	7	593.02	2.23	0.00	0.00
7	544.02	2.40	0.00	0.01	7	594.02	2.23	0.00	0.00
7	545.02	2.16	0.00	0.01	7	595.02	2.23	0.00	0.00
7	546.02	2.27	0.00	0.00	7	596.02	2.23	0.01	0.00
7	547.02	2.31	0.00	0.00	7	597.02	2.23	0.00	0.00
7	548.02	2.27	0.00	0.00	7	598.02	2.29	0.00	0.00
7	549.02	2.33	0.00	0.00	7	599.02	2.01	0.01	0.03
7	550.02	2.33	0.00	0.01	7	600.02	2.32	0.00	0.00
7	551.02	2.33	0.00	0.00	7	601.02	1.91	0.00	0.17
7	552.02	2.33	0.00	0.00	7	602.02	2.32	0.00	0.00
7	553.02	2.33	0.00	0.00	7	603.02	2.32	0.00	0.00
7	554.02	2.33	0.00	0.00	7	604.02	2.32	0.00	0.00
7	555.02	2.33	0.00	0.01	7	605.02	2.32	0.00	0.00
7	556.02	2.33	0.01	0.02	7	606.02	2.32	0.00	0.00
7	557.02	2.33	0.00	0.01	7	607.02	2.32	0.00	0.00
7	558.02	2.33	0.00	0.01	7	608.02	2.32	0.00	0.00
7	559.02	2.33	0.00	0.00	7	609.02	2.32	0.00	0.00
7	560.02	2.33	0.00	0.01	7	610.02	2.32	0.00	0.00
7	561.02	2.33	0.00	0.01	7	611.02	2.32	0.00	0.00
7	562.02	2.33	0.00	0.00	7	612.02	2.32	0.00	0.00
7	563.02	2.33	0.00	0.00	7	613.02	2.32	0.00	0.00
7	564.02	2.36	0.01	0.00	7	614.02	2.32	0.00	0.00
7	565.02	2.30	0.00	0.00	7	615.02	2.32	0.00	0.00
7	566.02	2.36	0.01	0.00	7	616.02	2.32	0.00	0.00
7	567.02	2.36	0.01	0.00	7	617.02	2.27	0.00	0.00
7	568.02	2.36	0.01	0.00	7	618.02	1.99	0.00	0.08
7	569.02	2.36	0.01	0.00	7	619.02	2.32	0.00	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	620.02	2.42	0.00	0.01	7	36.03	1.03	1.75	0.00
7	621.02	2.32	0.00	0.00	7	37.03	1.30	1.64	0.09
7	622.02	2.21	0.00	0.01	7	38.03	1.03	1.65	0.00
7	623.02	2.33	0.00	0.00	7	43.03	1.06	0.75	0.13
7	624.02	2.33	0.00	0.00	7	47.03	1.44	0.67	0.00
7	625.02	2.33	0.00	0.00	7	48.03	1.62	0.46	0.00
7	626.02	2.33	0.00	0.00	7	58.03	1.74	0.30	0.00
7	627.02	2.33	0.00	0.00	7	59.03	1.78	0.28	0.00
7	628.02	2.33	0.00	0.00	7	60.03	1.91	0.26	0.02
7	629.02	2.33	0.00	0.00	7	61.03	1.78	0.26	0.00
7	630.02	2.33	0.00	0.00	7	63.03	1.76	0.39	0.01
7	631.02	2.33	0.00	0.00	7	64.03	1.96	0.29	0.04
7	632.02	2.33	0.00	0.00	7	65.03	1.78	0.30	0.00
7	633.02	2.33	0.00	0.00	7	67.03	1.78	0.39	0.01
7	634.02	2.33	0.00	0.01	7	68.03	1.66	0.42	0.00
7	635.02	2.33	0.00	0.00	7	69.03	1.66	0.39	0.00
7	636.02	2.22	0.00	0.01	7	70.03	1.66	0.41	0.00
7	637.02	2.18	0.00	0.02	7	71.03	1.66	0.34	0.00
7	638.02	2.34	0.00	0.00	7	72.03	1.61	0.66	0.02
7	639.02	2.34	0.00	0.00	7	73.03	1.48	0.51	0.01
7	640.02	2.25	0.00	0.00	7	74.03	1.90	0.31	0.03
7	641.02	2.27	0.00	0.00	7	77.03	1.62	0.36	0.00
7	642.02	2.11	0.00	0.02	7	78.03	1.81	0.22	0.00
7	643.02	2.27	0.01	0.00	7	80.03	1.82	0.25	0.00
7	644.02	1.80	1.33	0.44	7	90.03	1.62	0.17	0.07
7	645.02	1.96	0.11	0.00	7	91.03	1.85	0.07	0.03
7	646.02	1.97	0.06	0.01	7	92.03	1.88	0.17	0.00
7	647.02	1.95	0.02	0.04	7	93.03	1.80	0.25	0.00
7	648.02	0.96	1.40	0.02	7	94.03	1.82	0.24	0.00
7	649.02	1.13	1.47	0.00	7	95.03	1.67	0.22	0.02
7	650.02	1.01	1.40	0.01	7	96.03	1.80	0.24	0.00
7	651.02	1.01	1.07	0.06	7	97.03	1.87	0.09	0.01
7	652.02	1.19	0.66	0.08	7	98.03	1.80	0.14	0.01
7	653.02	1.48	0.66	0.00	7	104.03	1.84	0.04	0.06
7	654.02	1.48	0.63	0.00	7	106.03	1.88	0.04	0.04
7	655.02	1.35	0.61	0.03	7	107.03	2.08	0.04	0.00
7	656.02	1.62	2.27	0.70	7	109.03	2.08	0.07	0.00
7	657.02	1.33	0.22	0.24	7	110.03	2.48	0.00	0.02
7	658.02	0.71	1.45	0.14	7	111.03	2.10	0.04	0.14
7	659.02	0.94	1.42	0.02	7	112.03	2.48	0.00	0.03
7	661.02	1.00	0.71	0.20	7	116.03	2.48	0.06	0.00
7	662.02	1.45	0.70	0.00	7	117.03	2.48	0.05	0.00
7	663.02	1.36	1.13	0.02	7	118.03	1.94	0.01	0.20
7	664.02	1.30	1.39	0.03	7	119.03	1.81	0.05	0.07
7	4.03	0.99	1.77	0.00	7	123.03	2.55	0.10	0.00
7	18.03	1.04	0.98	0.07	7	124.03	2.48	0.06	0.00
7	19.03	1.08	0.88	0.07	7	127.03	2.08	0.00	0.07
7	25.03	1.37	1.44	0.08	7	129.03	2.37	0.01	0.03
7	32.03	1.12	0.87	0.06	7	130.03	2.55	0.05	0.00
7	35.03	1.42	1.01	0.02	7	133.03	2.52	0.06	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	134.03	2.53	0.01	0.03	7	205.03	2.90	0.43	0.00
7	140.03	2.34	0.00	0.01	7	208.03	3.06	0.59	0.00
7	141.03	2.64	0.13	0.00	7	209.03	3.01	0.59	0.00
7	142.03	2.59	0.02	0.03	7	211.03	3.18	0.73	0.00
7	143.03	2.81	0.16	0.01	7	212.03	3.14	0.69	0.00
7	144.03	2.84	0.12	0.04	7	213.03	3.14	0.71	0.00
7	145.03	2.88	0.05	0.13	7	216.03	3.33	1.01	0.00
7	149.03	2.87	0.11	0.06	7	217.03	3.27	1.09	0.00
7	151.03	2.80	0.18	0.01	7	218.03	3.33	1.00	0.00
7	152.03	2.75	0.11	0.02	7	219.03	3.33	1.01	0.00
7	153.03	2.53	0.12	0.01	7	220.03	3.28	0.92	0.00
7	154.03	2.64	0.14	0.00	7	221.03	3.25	0.85	0.00
7	157.03	2.76	0.41	0.03	7	222.03	3.25	0.72	0.01
7	158.03	2.93	0.39	0.00	7	224.03	3.52	1.41	0.00
7	159.03	2.93	0.42	0.00	7	225.03	3.25	0.83	0.00
7	160.03	2.93	0.37	0.00	7	226.03	3.48	1.47	0.00
7	161.03	2.93	0.43	0.00	7	227.03	3.25	0.84	0.00
7	162.03	2.92	0.42	0.00	7	228.03	3.48	1.49	0.00
7	163.03	2.93	0.43	0.00	7	229.03	3.48	1.36	0.00
7	164.03	3.05	0.41	0.01	7	230.03	3.48	1.48	0.00
7	165.03	2.93	0.49	0.00	7	231.03	3.25	0.78	0.01
7	167.03	3.05	0.19	0.11	7	232.03	3.48	1.36	0.00
7	169.03	2.72	0.18	0.00	7	233.03	3.48	1.35	0.00
7	171.03	2.72	0.18	0.00	7	234.03	3.33	0.91	0.01
7	173.03	2.72	0.19	0.00	7	235.03	3.25	0.96	0.00
7	175.03	2.72	0.20	0.00	7	236.03	3.48	1.41	0.00
7	176.03	3.15	0.30	0.10	7	240.03	3.24	1.06	0.01
7	177.03	3.09	0.75	0.00	7	241.03	3.24	0.97	0.00
7	178.03	3.35	0.75	0.04	7	242.03	3.24	1.02	0.00
7	179.03	3.15	0.65	0.00	7	243.03	3.24	0.74	0.01
7	180.03	3.15	0.52	0.02	7	244.03	3.13	0.59	0.00
7	181.03	2.72	0.26	0.01	7	245.03	3.06	0.45	0.01
7	182.03	2.72	0.35	0.03	7	246.03	3.24	1.06	0.01
7	183.03	3.15	0.38	0.06	7	247.03	3.24	1.03	0.00
7	184.03	3.15	0.38	0.06	7	248.03	3.06	0.38	0.02
7	185.03	3.15	0.38	0.06	7	249.03	3.24	0.81	0.00
7	186.03	3.15	0.40	0.05	7	250.03	3.06	0.39	0.02
7	187.03	3.03	0.32	0.03	7	251.03	3.39	0.66	0.08
7	188.03	3.13	0.35	0.06	7	252.03	3.10	0.64	0.00
7	193.03	2.88	0.35	0.00	7	253.03	3.10	0.64	0.00
7	194.03	2.88	0.39	0.00	7	254.03	3.10	0.68	0.00
7	195.03	2.88	0.27	0.00	7	255.03	3.10	0.62	0.00
7	196.03	3.34	0.70	0.04	7	256.03	3.06	0.43	0.01
7	197.03	3.32	0.54	0.08	7	257.03	3.10	0.62	0.00
7	199.03	3.03	0.38	0.01	7	258.03	3.25	0.60	0.03
7	200.03	2.88	0.36	0.00	7	259.03	3.07	0.45	0.01
7	201.03	2.88	0.35	0.00	7	260.03	3.07	0.44	0.01
7	202.03	2.88	0.36	0.00	7	261.03	3.07	0.49	0.01
7	203.03	2.88	0.34	0.00	7	262.03	3.07	0.58	0.00
7	204.03	3.01	0.37	0.01	7	263.03	3.07	0.50	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	264.03	3.07	0.48	0.01	7	316.03	3.16	0.25	0.14
7	265.03	3.07	0.50	0.01	7	317.03	3.19	0.90	0.00
7	266.03	3.07	0.48	0.01	7	318.03	3.16	0.22	0.17
7	267.03	3.07	0.54	0.00	7	319.03	3.16	0.21	0.17
7	268.03	3.07	0.38	0.03	7	320.03	3.19	0.89	0.00
7	269.03	3.07	0.47	0.01	7	321.03	3.16	0.16	0.23
7	270.03	3.07	0.74	0.01	7	322.03	3.19	0.75	0.00
7	272.03	3.07	0.41	0.02	7	323.03	3.19	0.85	0.00
7	273.03	3.07	0.70	0.00	7	324.03	3.16	0.13	0.27
7	274.03	3.07	0.58	0.00	7	325.03	3.16	0.03	0.47
7	275.03	3.07	0.54	0.00	7	326.03	3.16	0.04	0.45
7	276.03	2.98	0.59	0.01	7	327.03	3.19	1.00	0.01
7	277.03	3.00	0.58	0.00	7	328.03	3.19	1.22	0.04
7	278.03	3.07	0.68	0.00	7	329.03	3.16	0.07	0.37
7	279.03	3.07	0.66	0.00	7	330.03	3.16	0.04	0.45
7	280.03	3.15	0.69	0.00	7	331.03	3.16	0.03	0.47
7	281.03	3.07	0.57	0.00	7	332.03	3.16	0.02	0.54
7	282.03	3.18	0.95	0.01	7	333.03	3.19	0.95	0.01
7	283.03	3.08	0.89	0.02	7	334.03	3.19	0.91	0.00
7	284.03	3.23	0.83	0.00	7	335.03	3.16	0.01	0.62
7	285.03	3.14	0.93	0.01	7	336.03	3.19	0.90	0.00
7	286.03	3.11	0.79	0.01	7	337.03	3.19	0.65	0.01
7	287.03	3.26	0.92	0.00	7	338.03	3.19	0.39	0.08
7	288.03	3.23	0.98	0.00	7	339.03	3.19	0.92	0.00
7	289.03	3.23	0.98	0.00	7	340.03	3.19	0.93	0.00
7	290.03	3.32	1.05	0.00	7	341.03	3.16	0.00	0.68
7	291.03	3.41	1.10	0.01	7	342.03	3.16	0.00	0.72
7	292.03	3.64	1.26	0.05	7	343.03	3.47	1.14	0.01
7	293.03	3.32	1.15	0.00	7	344.03	3.38	0.96	0.01
7	294.03	3.32	1.12	0.00	7	345.03	3.16	0.01	0.59
7	295.03	3.32	1.14	0.00	7	346.03	3.19	0.92	0.00
7	296.03	3.47	1.34	0.00	7	347.03	3.16	0.02	0.56
7	297.03	3.33	1.38	0.02	7	348.03	3.19	0.95	0.01
7	298.03	3.27	0.83	0.00	7	349.03	3.16	0.01	0.59
7	299.03	3.47	1.33	0.00	7	350.03	3.19	0.89	0.00
7	300.03	3.41	1.20	0.00	7	351.03	3.16	0.00	0.65
7	301.03	3.43	0.84	0.05	7	352.03	3.19	0.89	0.00
7	302.03	3.21	0.88	0.00	7	353.03	3.16	0.00	0.66
7	303.03	3.18	1.05	0.02	7	354.03	3.19	0.81	0.00
7	304.03	3.21	0.82	0.00	7	355.03	3.16	0.00	0.67
7	305.03	3.21	0.91	0.00	7	356.03	3.16	0.01	0.64
7	306.03	3.16	0.73	0.00	7	357.03	3.19	0.75	0.00
7	307.03	3.12	0.76	0.00	7	358.03	3.16	0.00	0.69
7	308.03	3.16	0.75	0.00	7	359.03	3.19	0.74	0.00
7	309.03	3.16	0.71	0.00	7	360.03	3.19	0.70	0.00
7	310.03	3.16	0.59	0.01	7	361.03	3.05	0.10	0.19
7	312.03	3.19	0.92	0.00	7	362.03	3.19	0.61	0.01
7	313.03	3.36	0.82	0.03	7	363.03	2.61	0.03	0.02
7	314.03	3.16	0.31	0.10	7	364.03	2.61	0.04	0.02
7	315.03	3.16	0.29	0.11	7	365.03	3.19	0.59	0.02

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	366.03	3.19	0.25	0.16	7	416.03	2.65	0.23	0.02
7	367.03	3.19	0.53	0.03	7	417.03	2.65	0.27	0.03
7	368.03	3.19	0.52	0.03	7	418.03	2.65	0.25	0.02
7	369.03	3.19	0.50	0.04	7	419.03	2.65	0.25	0.02
7	370.03	3.19	0.47	0.05	7	420.03	2.54	0.16	0.02
7	371.03	3.19	0.46	0.05	7	421.03	2.78	0.26	0.00
7	372.03	3.11	0.00	0.57	7	422.03	2.69	0.19	0.00
7	373.03	3.19	0.46	0.05	7	423.03	2.80	0.26	0.00
7	374.03	3.19	0.45	0.06	7	424.03	2.62	0.26	0.03
7	375.03	3.19	0.43	0.06	7	425.03	2.80	0.26	0.00
7	376.03	3.19	0.42	0.06	7	426.03	2.80	0.25	0.00
7	377.03	3.19	0.26	0.15	7	427.03	2.80	0.22	0.00
7	378.03	3.13	0.01	0.53	7	428.03	2.80	0.23	0.00
7	379.03	3.33	0.11	0.50	7	429.03	2.80	0.22	0.00
7	380.03	3.30	1.30	0.02	7	430.03	2.80	0.23	0.00
7	381.03	3.06	0.01	0.42	7	431.03	2.80	0.20	0.00
7	382.03	3.38	0.08	0.64	7	432.03	2.80	0.22	0.00
7	383.03	3.15	0.04	0.42	7	433.03	2.54	0.17	0.02
7	384.03	2.50	0.05	0.00	7	434.03	2.80	0.22	0.00
7	385.03	2.50	0.10	0.01	7	435.03	2.85	0.28	0.00
7	386.03	2.50	0.06	0.00	7	436.03	2.93	0.22	0.03
7	387.03	2.50	0.05	0.00	7	437.03	2.80	0.22	0.00
7	388.03	2.50	0.11	0.02	7	438.03	2.80	0.23	0.00
7	389.03	2.50	0.07	0.00	7	439.03	2.71	0.23	0.00
7	390.03	2.50	0.09	0.01	7	440.03	2.80	0.25	0.00
7	391.03	2.50	0.09	0.01	7	441.03	2.80	0.23	0.00
7	392.03	2.50	0.08	0.01	7	442.03	2.75	0.26	0.00
7	393.03	2.50	0.09	0.01	7	443.03	2.80	0.19	0.01
7	394.03	2.50	0.13	0.02	7	444.03	2.80	0.21	0.00
7	395.03	2.50	0.12	0.02	7	445.03	2.80	0.20	0.00
7	396.03	2.57	0.09	0.00	7	446.03	2.80	0.22	0.00
7	397.03	2.37	0.08	0.04	7	447.03	2.80	0.24	0.00
7	398.03	2.57	0.07	0.00	7	448.03	2.80	0.21	0.00
7	399.03	2.66	0.15	0.00	7	449.03	2.80	0.25	0.00
7	400.03	2.65	0.11	0.00	7	450.03	2.80	0.21	0.00
7	401.03	2.68	0.15	0.00	7	451.03	2.80	0.22	0.00
7	402.03	2.68	0.13	0.00	7	452.03	2.80	0.21	0.00
7	403.03	2.47	0.13	0.03	7	453.03	2.80	0.21	0.00
7	404.03	2.65	0.10	0.00	7	454.03	2.80	0.21	0.00
7	405.03	2.65	0.16	0.00	7	455.03	2.80	0.21	0.00
7	406.03	2.65	0.10	0.00	7	456.03	2.80	0.23	0.00
7	407.03	2.65	0.08	0.01	7	457.03	2.80	0.22	0.00
7	408.03	2.65	0.10	0.00	7	458.03	2.80	0.21	0.00
7	409.03	2.65	0.12	0.00	7	459.03	2.80	0.16	0.01
7	410.03	2.65	0.14	0.00	7	460.03	2.80	0.21	0.00
7	411.03	2.65	0.15	0.00	7	461.03	2.80	0.21	0.00
7	412.03	2.65	0.13	0.00	7	462.03	2.80	0.18	0.01
7	413.03	2.65	0.15	0.00	7	463.03	2.80	0.19	0.01
7	414.03	2.65	0.18	0.00	7	464.03	2.80	0.19	0.01
7	415.03	2.65	0.20	0.01	7	465.03	2.80	0.20	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	466.03	2.80	0.18	0.01	7	516.03	2.40	0.00	0.02
7	467.03	2.80	0.15	0.01	7	517.03	2.39	0.01	0.00
7	468.03	2.80	0.19	0.01	7	518.03	2.37	0.10	0.06
7	469.03	2.80	0.15	0.02	7	519.03	2.37	0.00	0.00
7	470.03	2.80	0.17	0.01	7	520.03	2.34	0.00	0.00
7	471.03	2.80	0.13	0.02	7	521.03	2.34	0.00	0.00
7	472.03	2.80	0.18	0.01	7	522.03	2.34	0.00	0.00
7	473.03	2.80	0.13	0.02	7	523.03	2.34	0.00	0.00
7	474.03	2.80	0.14	0.02	7	524.03	2.34	0.00	0.00
7	475.03	2.80	0.15	0.01	7	525.03	2.34	0.00	0.00
7	476.03	2.99	0.15	0.10	7	526.03	2.47	0.04	0.00
7	477.03	2.66	0.05	0.02	7	527.03	2.63	0.20	0.01
7	478.03	2.66	0.06	0.02	7	528.03	2.74	0.18	0.00
7	479.03	2.89	0.16	0.04	7	529.03	2.74	0.06	0.04
7	480.03	2.66	0.10	0.00	7	530.03	2.74	0.04	0.06
7	481.03	2.92	0.12	0.08	7	531.03	2.74	0.04	0.06
7	482.03	2.60	0.10	0.00	7	532.03	2.46	0.04	0.00
7	483.03	2.78	0.10	0.03	7	533.03	2.74	0.04	0.07
7	484.03	2.60	0.09	0.00	7	534.03	2.74	0.04	0.07
7	485.03	2.60	0.10	0.00	7	535.03	2.74	0.04	0.07
7	486.03	2.60	0.09	0.00	7	536.03	2.74	0.04	0.07
7	487.03	2.60	0.10	0.00	7	537.03	2.74	0.04	0.06
7	488.03	2.60	0.08	0.00	7	538.03	2.49	0.05	0.00
7	489.03	2.60	0.09	0.00	7	539.03	2.49	0.04	0.00
7	490.03	2.60	0.08	0.00	7	540.03	2.49	0.04	0.00
7	491.03	2.60	0.05	0.01	7	541.03	2.46	0.04	0.00
7	492.03	2.60	0.10	0.00	7	542.03	2.49	0.04	0.00
7	493.03	2.60	0.11	0.00	7	543.03	2.49	0.05	0.00
7	494.03	2.60	0.08	0.00	7	544.03	2.49	0.05	0.00
7	495.03	2.60	0.11	0.00	7	545.03	2.49	0.05	0.00
7	496.03	2.75	0.10	0.02	7	546.03	2.49	0.05	0.00
7	497.03	2.60	0.12	0.00	7	547.03	2.49	0.05	0.00
7	498.03	2.60	0.14	0.00	7	548.03	2.49	0.03	0.00
7	499.03	2.46	0.06	0.01	7	549.03	2.49	0.05	0.00
7	500.03	2.61	0.09	0.00	7	550.03	2.49	0.05	0.00
7	501.03	2.60	0.13	0.00	7	551.03	2.49	0.05	0.00
7	502.03	2.54	0.05	0.00	7	552.03	2.49	0.05	0.00
7	503.03	2.56	0.05	0.00	7	553.03	2.49	0.04	0.00
7	504.03	2.52	0.06	0.00	7	554.03	2.49	0.03	0.00
7	505.03	2.52	0.06	0.00	7	555.03	2.49	0.07	0.00
7	506.03	2.52	0.06	0.00	7	556.03	2.39	0.06	0.02
7	507.03	2.52	0.06	0.00	7	557.03	2.49	0.04	0.00
7	508.03	2.52	0.05	0.00	7	558.03	2.40	0.04	0.01
7	509.03	2.52	0.05	0.00	7	559.03	2.60	0.11	0.00
7	510.03	2.52	0.05	0.00	7	560.03	2.54	0.07	0.00
7	511.03	2.52	0.05	0.00	7	561.03	2.54	0.07	0.00
7	512.03	2.52	0.03	0.00	7	562.03	2.54	0.07	0.00
7	513.03	2.52	0.05	0.00	7	563.03	2.54	0.06	0.00
7	514.03	2.52	0.02	0.01	7	564.03	2.50	0.05	0.00
7	515.03	2.40	0.00	0.01	7	565.03	2.49	0.05	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	566.03	2.50	0.04	0.00	7	616.03	2.38	0.02	0.00
7	567.03	2.50	0.06	0.00	7	617.03	2.42	0.01	0.00
7	568.03	2.50	0.05	0.00	7	618.03	2.42	0.01	0.00
7	569.03	2.50	0.08	0.01	7	619.03	2.42	0.02	0.00
7	570.03	2.50	0.06	0.00	7	620.03	2.33	0.02	0.01
7	571.03	2.30	0.01	0.01	7	621.03	2.42	0.02	0.00
7	572.03	2.55	0.10	0.00	7	622.03	2.42	0.02	0.00
7	573.03	2.37	0.02	0.00	7	623.03	2.42	0.03	0.00
7	574.03	2.61	0.09	0.00	7	624.03	2.42	0.04	0.00
7	575.03	2.37	0.01	0.00	7	625.03	2.42	0.04	0.00
7	576.03	2.61	0.07	0.00	7	626.03	2.42	0.04	0.01
7	577.03	2.61	0.07	0.00	7	627.03	2.42	0.04	0.01
7	578.03	2.37	0.02	0.00	7	628.03	2.42	0.04	0.00
7	579.03	2.61	0.05	0.01	7	629.03	2.42	0.05	0.01
7	580.03	2.61	0.04	0.01	7	630.03	2.42	0.05	0.01
7	581.03	2.61	0.05	0.01	7	631.03	2.42	0.06	0.01
7	582.03	2.61	0.06	0.01	7	632.03	2.42	0.05	0.01
7	583.03	2.37	0.00	0.00	7	633.03	2.42	0.05	0.01
7	584.03	2.37	0.00	0.00	7	634.03	2.42	0.04	0.01
7	585.03	2.61	0.06	0.01	7	635.03	2.42	0.04	0.01
7	586.03	2.37	0.00	0.00	7	636.03	2.29	0.05	0.05
7	587.03	2.54	0.04	0.00	7	637.03	2.30	0.07	0.06
7	588.03	2.57	0.04	0.01	7	638.03	2.48	0.06	0.00
7	589.03	2.37	0.06	0.03	7	639.03	2.42	0.02	0.00
7	590.03	2.44	0.06	0.01	7	640.03	2.30	0.03	0.03
7	591.03	2.44	0.08	0.02	7	641.03	2.32	0.00	0.00
7	592.03	2.50	0.03	0.00	7	642.03	2.30	0.00	0.00
7	593.03	2.50	0.04	0.00	7	643.03	2.03	0.03	0.01
7	594.03	2.50	0.03	0.00	7	644.03	1.95	1.44	0.75
7	595.03	2.50	0.04	0.00	7	645.03	2.18	0.13	0.06
7	596.03	2.50	0.02	0.00	7	646.03	2.17	0.14	0.06
7	597.03	2.50	0.03	0.00	7	647.03	1.66	0.75	0.06
7	598.03	2.50	0.01	0.01	7	648.03	0.97	1.26	0.04
7	599.03	2.50	0.05	0.00	7	649.03	1.09	1.44	0.00
7	600.03	2.50	0.02	0.00	7	650.03	1.02	1.37	0.01
7	601.03	2.50	0.02	0.00	7	651.03	1.06	1.22	0.01
7	602.03	2.50	0.02	0.00	7	652.03	1.12	0.51	0.20
7	603.03	2.50	0.02	0.00	7	653.03	1.57	0.50	0.00
7	604.03	2.50	0.01	0.01	7	654.03	1.57	0.50	0.00
7	605.03	2.50	0.02	0.00	7	655.03	1.43	0.55	0.01
7	606.03	2.50	0.01	0.01	7	656.03	1.59	2.27	0.65
7	607.03	2.50	0.04	0.00	7	657.03	1.41	0.25	0.15
7	608.03	2.55	0.04	0.00	7	658.03	0.71	1.35	0.17
7	609.03	2.33	0.00	0.00	7	659.03	0.98	1.24	0.04
7	610.03	2.34	0.01	0.00	7	661.03	1.07	0.68	0.15
7	611.03	2.50	0.02	0.00	7	662.03	1.46	0.66	0.00
7	612.03	2.41	0.01	0.00	7	663.03	1.38	1.28	0.05
7	613.03	2.26	0.01	0.01	7	664.03	1.23	1.34	0.01
7	614.03	2.43	0.01	0.00	7	25.04	1.04	1.44	0.00
7	615.03	2.37	0.01	0.00	7	36.04	0.97	1.95	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	37.04	1.15	1.95	0.06	7	171.04	2.49	0.09	0.01
7	47.04	0.97	1.33	0.03	7	173.04	2.59	0.11	0.00
7	48.04	1.14	1.29	0.00	7	175.04	2.59	0.12	0.00
7	58.04	1.14	1.30	0.00	7	176.04	2.59	0.11	0.00
7	61.04	1.18	1.07	0.01	7	180.04	2.29	0.05	0.05
7	63.04	1.31	0.74	0.01	7	181.04	2.55	0.06	0.00
7	65.04	1.44	0.99	0.02	7	182.04	2.54	0.06	0.00
7	67.04	1.33	0.66	0.02	7	183.04	2.52	0.10	0.01
7	68.04	1.47	0.76	0.00	7	184.04	2.75	0.12	0.01
7	69.04	1.53	0.67	0.00	7	186.04	2.75	0.09	0.03
7	70.04	1.47	0.68	0.00	7	187.04	2.67	0.15	0.00
7	71.04	1.47	0.67	0.00	7	188.04	2.54	0.05	0.00
7	72.04	1.49	0.68	0.00	7	193.04	2.53	0.02	0.01
7	77.04	1.41	0.85	0.00	7	194.04	2.54	0.00	0.04
7	78.04	1.48	0.78	0.00	7	195.04	2.76	0.24	0.00
7	90.04	1.53	0.57	0.00	7	196.04	2.59	0.12	0.00
7	91.04	1.47	0.59	0.00	7	197.04	2.59	0.09	0.00
7	92.04	1.71	0.54	0.02	7	199.04	2.79	0.15	0.01
7	93.04	1.41	0.77	0.00	7	200.04	2.67	0.20	0.00
7	94.04	1.41	0.80	0.00	7	201.04	2.67	0.22	0.01
7	95.04	1.63	0.77	0.05	7	202.04	2.78	0.22	0.00
7	96.04	1.75	0.37	0.00	7	203.04	2.76	0.21	0.00
7	97.04	1.70	0.54	0.02	7	204.04	2.62	0.14	0.00
7	98.04	1.72	0.29	0.00	7	205.04	2.66	0.14	0.00
7	107.04	1.45	0.98	0.02	7	208.04	2.66	0.16	0.00
7	109.04	1.51	0.84	0.02	7	209.04	2.66	0.16	0.00
7	116.04	1.26	0.96	0.00	7	211.04	2.66	0.18	0.00
7	117.04	1.51	1.06	0.06	7	212.04	2.66	0.23	0.01
7	119.04	1.83	0.25	0.00	7	213.04	2.66	0.20	0.01
7	127.04	1.79	0.28	0.00	7	216.04	2.66	0.25	0.02
7	130.04	1.78	0.22	0.00	7	217.04	2.66	0.21	0.01
7	133.04	1.83	0.22	0.00	7	220.04	2.62	0.28	0.04
7	134.04	2.13	0.02	0.00	7	221.04	2.82	0.33	0.00
7	140.04	1.92	0.19	0.00	7	222.04	2.95	0.42	0.00
7	141.04	1.59	0.18	0.08	7	224.04	2.86	0.40	0.00
7	151.04	2.02	0.03	0.01	7	225.04	2.90	0.40	0.00
7	152.04	2.13	0.02	0.00	7	226.04	2.92	0.39	0.00
7	153.04	2.13	0.01	0.00	7	227.04	2.92	0.41	0.00
7	154.04	2.13	0.01	0.00	7	228.04	2.92	0.43	0.00
7	157.04	2.08	0.05	0.00	7	229.04	2.95	0.49	0.00
7	158.04	2.28	0.01	0.01	7	230.04	2.70	0.44	0.07
7	159.04	2.19	0.01	0.00	7	231.04	2.98	0.51	0.00
7	160.04	2.07	0.02	0.00	7	232.04	3.09	0.52	0.01
7	161.04	2.19	0.01	0.00	7	233.04	3.01	0.55	0.00
7	162.04	2.07	0.01	0.01	7	234.04	2.98	0.58	0.00
7	163.04	2.07	0.02	0.01	7	235.04	2.98	0.51	0.00
7	164.04	2.32	0.00	0.00	7	236.04	2.97	0.48	0.00
7	165.04	2.19	0.01	0.00	7	241.04	2.95	0.55	0.01
7	167.04	2.52	0.05	0.00	7	242.04	3.03	0.56	0.00
7	169.04	2.36	0.06	0.03	7	243.04	3.03	0.86	0.04

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	244.04	3.43	1.17	0.00	7	299.04	3.61	1.26	0.04
7	245.04	3.43	1.39	0.00	7	300.04	3.61	1.35	0.03
7	246.04	3.16	0.68	0.00	7	301.04	3.99	3.13	0.00
7	247.04	3.11	0.84	0.01	7	302.04	3.71	2.40	0.02
7	248.04	3.36	1.22	0.00	7	303.04	3.75	2.16	0.00
7	249.04	3.11	1.04	0.04	7	304.04	3.84	2.21	0.00
7	250.04	3.42	1.42	0.00	7	305.04	3.84	2.10	0.01
7	251.04	3.04	1.29	0.15	7	306.04	3.84	2.24	0.00
7	252.04	3.43	1.31	0.00	7	307.04	3.84	2.16	0.01
7	253.04	3.66	1.36	0.04	7	308.04	3.76	2.22	0.00
7	254.04	3.43	1.26	0.00	7	309.04	3.78	2.44	0.01
7	255.04	3.43	1.33	0.00	7	310.04	3.78	1.70	0.03
7	256.04	3.48	1.49	0.00	7	312.04	3.84	2.14	0.01
7	257.04	3.48	1.29	0.00	7	313.04	3.84	2.31	0.00
7	258.04	3.48	1.40	0.00	7	314.04	3.78	2.34	0.00
7	259.04	3.48	1.54	0.00	7	315.04	3.78	2.25	0.00
7	260.04	3.48	1.71	0.01	7	316.04	3.78	2.14	0.00
7	261.04	3.48	1.74	0.02	7	317.04	3.84	2.12	0.01
7	262.04	3.48	1.53	0.00	7	318.04	3.78	2.16	0.00
7	263.04	3.48	1.67	0.01	7	319.04	3.78	1.93	0.01
7	264.04	3.48	1.73	0.01	7	320.04	4.00	2.67	0.01
7	265.04	3.48	1.67	0.01	7	321.04	3.78	1.62	0.05
7	266.04	3.48	1.65	0.01	7	322.04	3.92	2.91	0.01
7	267.04	3.48	1.66	0.01	7	323.04	3.92	2.74	0.00
7	268.04	3.34	1.52	0.03	7	324.04	3.75	1.80	0.01
7	270.04	3.75	2.04	0.00	7	325.04	3.63	1.74	0.00
7	272.04	3.69	2.20	0.01	7	326.04	3.63	1.39	0.03
7	273.04	3.43	2.13	0.10	7	327.04	3.92	3.04	0.01
7	276.04	3.75	2.37	0.01	7	328.04	3.92	3.22	0.03
7	277.04	3.75	2.42	0.01	7	329.04	3.63	1.41	0.02
7	278.04	3.75	2.23	0.00	7	330.04	3.63	1.46	0.02
7	279.04	3.75	2.24	0.00	7	331.04	3.63	1.44	0.02
7	280.04	3.75	2.20	0.00	7	332.04	3.63	1.53	0.01
7	281.04	3.68	3.10	0.14	7	334.04	3.92	2.68	0.00
7	282.04	3.75	2.42	0.01	7	335.04	3.63	1.70	0.00
7	283.04	3.75	2.16	0.00	7	336.04	3.92	2.71	0.00
7	284.04	3.75	2.16	0.00	7	337.04	3.92	3.01	0.01
7	285.04	3.75	2.20	0.00	7	338.04	3.92	3.45	0.05
7	286.04	3.75	2.16	0.00	7	339.04	3.84	2.37	0.00
7	287.04	3.75	2.16	0.00	7	340.04	3.92	3.09	0.02
7	288.04	3.61	1.61	0.00	7	341.04	3.63	1.70	0.00
7	289.04	3.67	0.73	0.28	7	342.04	3.63	1.80	0.00
7	290.04	3.75	2.06	0.00	7	343.04	3.89	2.90	0.01
7	292.04	3.61	1.29	0.03	7	344.04	3.99	3.27	0.01
7	293.04	3.75	1.76	0.02	7	345.04	3.63	1.81	0.00
7	294.04	3.75	1.99	0.00	7	346.04	4.01	3.29	0.01
7	295.04	3.93	1.75	0.10	7	347.04	3.63	1.77	0.00
7	296.04	3.61	1.55	0.01	7	348.04	4.10	3.19	0.00
7	297.04	3.61	1.48	0.01	7	349.04	3.63	1.58	0.01
7	298.04	3.99	3.42	0.02	7	350.04	4.10	2.98	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	351.04	3.63	1.47	0.02	7	401.04	3.67	0.81	0.23
7	352.04	4.10	2.93	0.01	7	402.04	3.67	0.80	0.24
7	353.04	3.63	1.47	0.02	7	403.04	3.67	0.78	0.25
7	354.04	4.10	3.00	0.01	7	404.04	3.67	0.81	0.23
7	355.04	3.63	1.37	0.03	7	405.04	3.67	0.86	0.20
7	356.04	3.63	1.19	0.06	7	406.04	3.77	0.80	0.35
7	357.04	4.10	3.04	0.00	7	407.04	3.18	0.63	0.01
7	358.04	3.63	0.79	0.20	7	408.04	3.18	0.74	0.00
7	359.04	4.10	2.77	0.02	7	409.04	3.18	0.58	0.02
7	360.04	4.10	2.60	0.04	7	410.04	3.18	0.53	0.03
7	361.04	4.10	2.49	0.06	7	411.04	3.18	0.52	0.03
7	362.04	4.10	2.60	0.04	7	412.04	3.18	0.47	0.04
7	363.04	4.10	2.45	0.06	7	413.04	3.18	0.46	0.05
7	364.04	4.10	2.59	0.04	7	414.04	3.18	0.43	0.06
7	365.04	4.10	2.52	0.05	7	415.04	3.18	0.39	0.07
7	366.04	4.10	2.49	0.06	7	416.04	3.18	0.32	0.11
7	367.04	4.10	2.46	0.06	7	417.04	3.18	0.27	0.14
7	368.04	4.10	2.54	0.05	7	418.04	3.18	0.26	0.15
7	369.04	4.10	2.56	0.05	7	419.04	3.18	0.28	0.13
7	370.04	4.10	2.59	0.04	7	420.04	3.30	0.35	0.17
7	371.04	4.10	2.63	0.04	7	421.04	3.13	0.24	0.12
7	372.04	3.73	1.62	0.03	7	422.04	2.88	0.32	0.00
7	373.04	4.10	2.55	0.05	7	423.04	2.78	0.24	0.00
7	374.04	4.10	2.65	0.04	7	424.04	3.17	0.25	0.15
7	375.04	4.10	2.68	0.03	7	425.04	2.79	0.23	0.00
7	376.04	4.10	2.67	0.03	7	426.04	2.79	0.27	0.00
7	377.04	4.10	2.46	0.06	7	427.04	2.79	0.11	0.03
7	378.04	3.89	2.42	0.00	7	428.04	2.79	0.26	0.00
7	379.04	3.81	2.57	0.01	7	429.04	2.79	0.06	0.06
7	380.04	4.10	2.58	0.04	7	430.04	2.79	0.08	0.05
7	381.04	3.93	1.91	0.07	7	431.04	2.79	0.09	0.04
7	382.04	3.74	2.35	0.01	7	432.04	2.79	0.07	0.06
7	383.04	3.56	1.64	0.00	7	433.04	2.79	0.07	0.06
7	384.04	3.56	1.36	0.01	7	434.04	2.79	0.05	0.07
7	385.04	3.56	0.72	0.18	7	435.04	2.79	0.05	0.07
7	386.04	3.67	1.86	0.00	7	436.04	2.79	0.05	0.07
7	387.04	3.67	1.85	0.00	7	437.04	2.79	0.04	0.08
7	388.04	3.56	0.59	0.25	7	438.04	2.72	0.10	0.01
7	389.04	3.67	1.31	0.06	7	439.04	2.79	0.04	0.08
7	390.04	3.56	0.54	0.29	7	440.04	2.88	0.09	0.08
7	391.04	3.67	1.24	0.07	7	441.04	2.61	0.07	0.00
7	392.04	3.56	0.52	0.31	7	442.04	2.74	0.06	0.05
7	393.04	3.67	1.05	0.13	7	443.04	2.69	0.11	0.01
7	394.04	3.67	0.98	0.15	7	444.04	2.62	0.12	0.00
7	395.04	3.67	0.99	0.15	7	445.04	2.62	0.11	0.00
7	396.04	3.56	0.46	0.35	7	446.04	2.62	0.11	0.00
7	397.04	3.56	0.51	0.31	7	447.04	2.61	0.08	0.00
7	398.04	3.56	0.42	0.39	7	448.04	2.62	0.09	0.00
7	399.04	3.67	0.89	0.19	7	449.04	2.61	0.08	0.00
7	400.04	3.56	0.36	0.45	7	450.04	2.58	0.03	0.02

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	451.04	2.50	0.05	0.00	7	503.04	2.71	0.17	0.00
7	452.04	2.46	0.04	0.00	7	504.04	2.71	0.17	0.00
7	453.04	2.46	0.04	0.00	7	505.04	2.71	0.16	0.00
7	454.04	2.50	0.05	0.00	7	506.04	2.71	0.18	0.00
7	455.04	2.46	0.04	0.00	7	507.04	2.71	0.15	0.00
7	456.04	2.50	0.05	0.00	7	508.04	2.71	0.20	0.00
7	457.04	2.46	0.03	0.00	7	509.04	2.71	0.11	0.01
7	458.04	2.38	0.00	0.02	7	510.04	2.71	0.20	0.00
7	459.04	2.65	0.02	0.05	7	511.04	2.71	0.12	0.01
7	460.04	2.46	0.03	0.00	7	512.04	2.82	0.19	0.01
7	461.04	2.60	0.04	0.01	7	513.04	2.56	0.07	0.00
7	462.04	2.51	0.00	0.03	7	514.04	2.56	0.09	0.00
7	463.04	2.50	0.05	0.00	7	515.04	2.59	0.12	0.00
7	464.04	2.50	0.04	0.00	7	516.04	2.59	0.11	0.00
7	465.04	2.50	0.04	0.00	7	517.04	2.59	0.11	0.00
7	466.04	2.49	0.05	0.00	7	518.04	2.73	0.22	0.00
7	467.04	2.62	0.00	0.07	7	519.04	2.59	0.10	0.00
7	468.04	2.23	0.00	0.01	7	520.04	2.59	0.09	0.00
7	470.04	2.34	0.00	0.00	7	521.04	2.59	0.10	0.00
7	472.04	2.20	0.01	0.03	7	522.04	2.59	0.11	0.00
7	473.04	2.39	0.08	0.03	7	523.04	2.59	0.10	0.00
7	474.04	2.58	0.07	0.00	7	524.04	2.59	0.00	0.07
7	475.04	2.37	0.01	0.00	7	525.04	2.59	0.00	0.06
7	476.04	2.34	0.06	0.03	7	526.04	3.05	0.53	0.00
7	477.04	2.52	0.04	0.00	7	527.04	2.83	0.20	0.01
7	478.04	2.52	0.06	0.00	7	528.04	2.73	0.22	0.00
7	479.04	2.48	0.05	0.00	7	530.04	3.05	0.53	0.00
7	480.04	2.52	0.05	0.00	7	531.04	2.78	0.58	0.07
7	481.04	2.52	0.04	0.00	7	532.04	2.66	0.40	0.07
7	482.04	2.52	0.06	0.00	7	533.04	3.05	0.52	0.00
7	483.04	2.52	0.05	0.00	7	534.04	3.05	0.51	0.00
7	484.04	2.52	0.05	0.00	7	535.04	3.05	0.53	0.00
7	485.04	2.52	0.05	0.00	7	536.04	3.05	0.53	0.00
7	486.04	2.52	0.06	0.00	7	537.04	3.05	0.53	0.00
7	487.04	2.40	0.03	0.00	7	538.04	3.05	0.53	0.00
7	488.04	2.64	0.06	0.01	7	539.04	3.05	0.49	0.00
7	489.04	2.46	0.04	0.00	7	540.04	2.92	0.42	0.00
7	490.04	2.54	0.07	0.00	7	541.04	2.85	0.42	0.01
7	491.04	2.46	0.06	0.00	7	542.04	2.87	0.40	0.00
7	492.04	2.54	0.07	0.00	7	543.04	2.92	0.39	0.00
7	493.04	2.52	0.06	0.00	7	544.04	2.92	0.37	0.00
7	494.04	2.52	0.10	0.01	7	545.04	2.92	0.40	0.00
7	495.04	2.54	0.07	0.00	7	546.04	2.92	0.35	0.00
7	496.04	2.47	0.05	0.00	7	547.04	2.92	0.37	0.00
7	497.04	2.49	0.05	0.00	7	548.04	2.92	0.45	0.00
7	498.04	2.52	0.06	0.00	7	549.04	2.92	0.31	0.00
7	499.04	2.65	0.15	0.00	7	550.04	2.86	0.34	0.00
7	500.04	2.67	0.20	0.00	7	551.04	3.00	0.40	0.01
7	501.04	2.52	0.06	0.00	7	552.04	2.87	0.12	0.06
7	502.04	2.47	0.18	0.06	7	553.04	2.92	0.38	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	554.04	2.92	0.35	0.00	7	604.04	2.61	0.12	0.00
7	555.04	2.87	0.14	0.04	7	605.04	2.60	0.11	0.00
7	556.04	2.68	0.04	0.03	7	606.04	2.60	0.11	0.00
7	557.04	2.92	0.30	0.01	7	607.04	2.63	0.10	0.00
7	558.04	2.92	0.29	0.01	7	608.04	2.44	0.08	0.02
7	559.04	2.87	0.14	0.04	7	609.04	2.66	0.18	0.00
7	560.04	2.95	0.31	0.01	7	610.04	2.72	0.17	0.00
7	561.04	2.50	0.15	0.03	7	611.04	2.58	0.14	0.01
7	562.04	2.84	0.35	0.00	7	612.04	2.55	0.16	0.02
7	563.04	2.83	0.12	0.04	7	613.04	2.70	0.11	0.01
7	564.04	2.66	0.13	0.00	7	614.04	2.70	0.16	0.00
7	565.04	2.59	0.14	0.01	7	615.04	2.70	0.11	0.01
7	566.04	2.66	0.12	0.00	7	616.04	2.70	0.15	0.00
7	567.04	2.66	0.10	0.00	7	617.04	2.68	0.11	0.00
7	568.04	2.66	0.11	0.00	7	618.04	2.39	0.12	0.06
7	569.04	2.66	0.11	0.00	7	619.04	2.83	0.15	0.03
7	570.04	2.66	0.11	0.00	7	620.04	2.70	0.16	0.00
7	571.04	2.60	0.09	0.00	7	621.04	2.64	0.15	0.00
7	572.04	2.55	0.11	0.01	7	622.04	2.68	0.14	0.00
7	573.04	2.60	0.10	0.00	7	623.04	2.68	0.15	0.00
7	574.04	2.56	0.09	0.00	7	624.04	2.68	0.15	0.00
7	575.04	2.60	0.08	0.00	7	625.04	2.68	0.13	0.00
7	576.04	2.60	0.11	0.00	7	626.04	2.68	0.13	0.00
7	577.04	2.60	0.11	0.00	7	627.04	2.36	0.01	0.00
7	578.04	2.60	0.07	0.00	7	628.04	2.81	0.18	0.01
7	579.04	2.60	0.08	0.00	7	629.04	2.71	0.16	0.00
7	580.04	2.60	0.09	0.00	7	630.04	2.63	0.07	0.00
7	581.04	2.60	0.09	0.00	7	631.04	2.56	0.05	0.00
7	582.04	2.60	0.08	0.00	7	632.04	2.56	0.06	0.00
7	583.04	2.60	0.06	0.00	7	634.04	2.58	0.11	0.00
7	584.04	2.60	0.11	0.00	7	635.04	2.62	0.12	0.00
7	585.04	2.60	0.08	0.00	7	636.04	2.54	0.12	0.01
7	586.04	2.60	0.10	0.00	7	637.04	2.64	0.08	0.00
7	587.04	2.67	0.04	0.03	7	638.04	2.45	0.10	0.03
7	588.04	2.56	0.25	0.05	7	639.04	2.35	0.10	0.06
7	589.04	2.60	0.07	0.00	7	640.04	2.60	0.07	0.00
7	590.04	2.43	0.01	0.00	7	641.04	2.53	0.03	0.01
7	591.04	2.66	0.10	0.00	7	642.04	2.71	0.58	0.12
7	592.04	2.60	0.13	0.00	7	643.04	2.28	0.71	0.70
7	593.04	2.43	0.11	0.04	7	644.04	1.09	1.43	0.00
7	594.04	2.65	0.12	0.00	7	645.04	1.15	0.23	0.44
7	595.04	2.52	0.13	0.02	7	646.04	1.50	0.22	0.11
7	596.04	2.65	0.14	0.00	7	647.04	1.27	1.21	0.01
7	597.04	2.65	0.11	0.00	7	648.04	0.81	1.43	0.08
7	598.04	2.65	0.14	0.00	7	649.04	1.09	1.19	0.01
7	599.04	2.65	0.18	0.00	7	650.04	1.12	1.35	0.00
7	600.04	2.47	0.10	0.02	7	651.04	1.00	1.45	0.01
7	601.04	2.65	0.11	0.00	7	652.04	1.03	0.72	0.17
7	602.04	2.65	0.12	0.00	7	653.04	1.44	0.70	0.00
7	603.04	2.68	0.11	0.00	7	654.04	1.44	0.67	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	655.04	1.31	0.72	0.02	7	248.05	2.25	0.00	0.00
7	656.04	1.32	2.36	0.32	7	249.05	2.18	0.01	0.00
7	657.04	1.31	0.63	0.03	7	250.05	2.44	0.01	0.00
7	658.04	0.69	1.35	0.20	7	252.05	2.26	0.00	0.00
7	659.04	0.98	1.41	0.01	7	254.05	2.39	0.00	0.02
7	661.04	1.00	0.73	0.19	7	255.05	2.17	0.00	0.02
7	662.04	1.44	0.71	0.00	7	256.05	2.42	0.04	0.00
7	663.04	1.35	1.27	0.04	7	258.05	2.42	0.02	0.00
7	664.04	1.24	1.41	0.02	7	260.05	2.49	0.04	0.00
7	666.04	1.04	2.33	7.68	7	261.05	2.43	0.02	0.00
7	667.04	3.81	2.13	0.00	7	262.05	2.63	0.04	0.02
7	93.05	1.05	2.00	0.03	7	264.05	2.43	0.02	0.00
7	94.05	1.11	1.56	0.01	7	265.05	2.68	0.15	0.00
7	95.05	0.98	1.45	0.01	7	266.05	2.65	0.19	0.01
7	107.05	0.88	1.93	0.00	7	267.05	2.65	0.17	0.00
7	130.05	1.27	0.31	0.22	7	268.05	2.63	0.25	0.03
7	133.05	1.74	0.31	0.00	7	270.05	2.79	0.32	0.00
7	160.05	0.92	0.56	0.38	7	273.05	2.79	0.29	0.00
7	162.05	1.53	0.55	0.00	7	276.05	2.85	0.23	0.01
7	163.05	1.55	0.59	0.00	7	277.05	2.76	0.25	0.00
7	169.05	1.53	0.54	0.00	7	278.05	2.79	0.26	0.00
7	171.05	1.56	0.50	0.00	7	280.05	2.91	0.38	0.00
7	173.05	1.54	0.51	0.00	7	282.05	2.76	0.17	0.00
7	182.05	1.62	0.11	0.11	7	283.05	2.76	0.27	0.00
7	188.05	1.73	0.37	0.00	7	284.05	2.76	0.32	0.01
7	193.05	1.73	0.30	0.00	7	285.05	3.00	0.44	0.00
7	194.05	1.87	0.31	0.02	7	287.05	2.95	0.43	0.00
7	200.05	1.99	0.19	0.02	7	288.05	2.91	0.41	0.00
7	201.05	1.85	0.18	0.00	7	290.05	2.98	0.55	0.00
7	202.05	2.10	0.19	0.06	7	293.05	2.98	0.61	0.01
7	203.05	1.86	0.16	0.00	7	294.05	2.98	0.54	0.00
7	204.05	1.73	0.30	0.00	7	295.05	2.91	0.40	0.00
7	208.05	1.87	0.20	0.00	7	296.05	2.93	0.35	0.00
7	209.05	1.87	0.17	0.00	7	297.05	2.92	0.31	0.00
7	212.05	1.90	0.15	0.00	7	298.05	3.04	0.42	0.01
7	213.05	1.88	0.16	0.00	7	299.05	3.01	0.49	0.00
7	220.05	2.04	0.06	0.00	7	300.05	3.14	0.67	0.00
7	221.05	2.14	0.07	0.01	7	301.05	2.99	0.43	0.00
7	222.05	2.13	0.04	0.00	7	302.05	3.00	0.60	0.00
7	225.05	2.04	0.06	0.00	7	303.05	3.09	0.48	0.01
7	226.05	1.93	0.06	0.01	7	304.05	3.06	0.81	0.02
7	227.05	2.04	0.05	0.00	7	305.05	3.06	0.78	0.01
7	229.05	2.08	0.08	0.01	7	306.05	3.21	0.79	0.00
7	241.05	2.11	0.03	0.00	7	307.05	3.04	0.84	0.03
7	242.05	2.18	0.03	0.00	7	308.05	3.21	0.79	0.00
7	243.05	2.18	0.02	0.00	7	309.05	3.21	0.80	0.00
7	244.05	2.08	0.09	0.01	7	310.05	3.57	1.57	0.00
7	245.05	2.12	0.03	0.00	7	312.05	3.29	1.07	0.00
7	246.05	2.27	0.05	0.06	7	313.05	3.33	1.28	0.01
7	247.05	2.15	0.01	0.00	7	314.05	3.38	1.08	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	315.05	3.33	1.15	0.00	7	372.05	3.77	2.20	0.00
7	316.05	3.33	1.42	0.02	7	373.05	4.41	3.47	0.06
7	317.05	3.32	1.08	0.00	7	374.05	4.41	3.41	0.07
7	318.05	3.33	1.54	0.04	7	375.05	4.41	3.33	0.09
7	319.05	3.33	1.75	0.08	7	376.05	4.41	3.38	0.08
7	320.05	3.32	1.05	0.00	7	377.05	4.05	3.01	0.00
7	321.05	3.33	1.73	0.08	7	378.05	3.72	2.19	0.00
7	322.05	3.42	1.25	0.00	7	379.05	4.19	2.04	0.23
7	323.05	3.32	1.12	0.00	7	380.05	4.41	3.44	0.07
7	324.05	3.33	1.80	0.09	7	381.05	3.87	2.18	0.01
7	325.05	3.33	1.98	0.14	7	382.05	3.72	2.35	0.01
7	326.05	3.33	2.40	0.26	7	383.05	3.77	2.24	0.00
7	328.05	3.50	1.67	0.01	7	384.05	3.77	2.46	0.01
7	329.05	3.33	2.00	0.14	7	385.05	3.88	3.51	0.08
7	330.05	3.33	1.99	0.14	7	386.05	3.77	2.16	0.00
7	331.05	3.33	2.07	0.16	7	387.05	3.77	2.17	0.00
7	332.05	3.33	2.08	0.16	7	388.05	4.08	3.75	0.02
7	334.05	3.32	1.21	0.00	7	389.05	3.77	2.84	0.04
7	335.05	3.33	2.07	0.16	7	390.05	4.08	3.63	0.01
7	336.05	3.13	1.28	0.09	7	391.05	3.73	2.88	0.07
7	337.05	3.45	1.26	0.00	7	392.05	4.08	3.24	0.00
7	338.05	3.58	1.47	0.01	7	393.05	3.77	3.20	0.10
7	339.05	3.33	2.02	0.15	7	394.05	4.08	3.19	0.00
7	340.05	3.57	1.77	0.00	7	395.05	4.08	3.22	0.00
7	341.05	3.33	2.03	0.15	7	396.05	3.99	2.33	0.03
7	342.05	3.33	1.69	0.07	7	397.05	3.97	2.28	0.03
7	343.05	2.91	0.39	0.00	7	398.05	3.82	2.46	0.00
7	344.05	2.91	0.37	0.00	7	399.05	4.08	3.17	0.00
7	345.05	3.33	0.65	0.05	7	400.05	3.82	2.40	0.00
7	346.05	3.62	1.83	0.00	7	401.05	4.08	3.20	0.00
7	347.05	3.33	0.66	0.05	7	402.05	4.31	2.77	0.13
7	349.05	3.33	0.70	0.04	7	403.05	.		
7	350.05	3.61	2.24	0.03	7	404.05	3.94	2.81	0.00
7	351.05	3.40	3.10	0.42	7	405.05	4.27	2.74	0.11
7	352.05	3.78	2.33	0.00	7	406.05	3.94	2.84	0.00
7	353.05	3.89	1.02	0.36	7	407.05	3.96	2.70	0.00
7	354.05	3.78	2.42	0.00	7	408.05	4.12	2.78	0.03
7	355.05	3.30	1.09	0.00	7	409.05	3.96	2.60	0.00
7	356.05	3.30	1.29	0.02	7	410.05	3.96	2.69	0.00
7	358.05	3.30	1.95	0.15	7	411.05	3.96	2.71	0.00
7	361.05	4.41	3.49	0.06	7	412.05	3.96	2.65	0.00
7	362.05	3.56	4.48	0.72	7	413.05	3.96	2.52	0.01
7	363.05	4.05	1.76	0.19	7	414.05	3.96	2.59	0.00
7	365.05	4.41	4.49	0.00	7	415.05	3.96	2.61	0.00
7	366.05	4.20	3.11	0.02	7	416.05	3.96	2.75	0.00
7	367.05	4.41	4.74	0.00	7	417.05	3.96	2.79	0.00
7	368.05	4.41	3.61	0.05	7	418.05	3.96	2.72	0.00
7	369.05	4.41	3.63	0.05	7	419.05	3.96	2.71	0.00
7	370.05	4.41	3.54	0.06	7	420.05	3.96	2.65	0.00
7	371.05	4.41	3.35	0.08	7	421.05	3.96	2.72	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	422.05	3.96	2.33	0.02	7	474.05	3.17	0.80	0.00
7	423.05	3.96	2.67	0.00	7	475.05	3.17	0.74	0.00
7	424.05	3.96	2.43	0.01	7	476.05	3.17	0.86	0.00
7	425.05	3.96	2.21	0.03	7	477.05	3.15	0.79	0.00
7	426.05	3.96	2.19	0.04	7	478.05	3.45	0.94	0.03
7	427.05	4.06	2.73	0.01	7	479.05	2.98	0.95	0.08
7	428.05	3.89	1.98	0.04	7	480.05	3.27	0.82	0.01
7	429.05	3.70	2.70	0.06	7	481.05	3.20	0.77	0.00
7	430.05	3.94	2.89	0.00	7	482.05	3.20	0.77	0.00
7	431.05	3.94	2.89	0.00	7	483.05	3.20	0.79	0.00
7	432.05	3.70	2.69	0.05	7	484.05	3.20	0.76	0.00
7	433.05	3.94	3.17	0.02	7	485.05	3.20	0.71	0.00
7	434.05	3.70	2.78	0.07	7	486.05	3.20	0.72	0.00
7	435.05	3.78	2.19	0.00	7	487.05	3.20	0.69	0.01
7	436.05	3.70	2.57	0.04	7	488.05	3.20	0.67	0.01
7	437.05	3.97	2.23	0.04	7	489.05	3.20	0.63	0.01
7	438.05	3.78	2.14	0.00	7	490.05	3.20	0.64	0.01
7	439.05	3.78	2.16	0.00	7	491.05	3.20	0.49	0.04
7	440.05	3.78	2.16	0.00	7	492.05	3.20	0.57	0.02
7	441.05	3.78	2.04	0.00	7	493.05	3.08	0.04	0.34
7	442.05	3.78	2.05	0.00	7	494.05	3.12	0.08	0.30
7	443.05	3.69	0.94	0.19	7	495.05	3.20	0.59	0.02
7	444.05	3.26	0.57	0.05	7	496.05	2.57	0.05	0.00
7	445.05	3.26	0.69	0.02	7	497.05	3.20	0.58	0.02
7	446.05	3.26	0.54	0.05	7	498.05	3.28	0.45	0.10
7	447.05	3.78	2.13	0.00	7	499.05	2.43	0.03	0.00
7	448.05	3.26	0.58	0.04	7	500.05	2.66	0.06	0.02
7	449.05	3.78	2.08	0.00	7	501.05	2.56	0.07	0.00
7	450.05	3.93	2.21	0.02	7	502.05	2.52	0.04	0.00
7	451.05	3.26	0.59	0.04	7	503.05	2.52	0.04	0.00
7	452.05	3.78	1.75	0.03	7	504.05	2.52	0.04	0.00
7	453.05	3.78	1.68	0.04	7	505.05	2.52	0.04	0.00
7	454.05	3.26	0.56	0.05	7	506.05	2.52	0.04	0.00
7	455.05	3.78	1.38	0.10	7	507.05	2.42	0.01	0.00
7	456.05	3.26	0.54	0.05	7	508.05	2.62	0.02	0.03
7	457.05	3.78	1.10	0.19	7	509.05	2.46	0.01	0.01
7	458.05	3.24	0.77	0.00	7	510.05	2.47	0.03	0.00
7	459.05	3.16	0.90	0.01	7	511.05	2.34	0.00	0.00
7	460.05	3.78	1.07	0.21	7	512.05	2.31	0.00	0.00
7	461.05	3.78	1.01	0.23	7	513.05	2.31	0.00	0.00
7	462.05	3.15	0.62	0.01	7	514.05	2.31	0.00	0.00
7	463.05	3.78	1.03	0.22	7	515.05	2.31	0.02	0.03
7	464.05	3.78	0.88	0.30	7	516.05	2.38	0.01	0.03
7	465.05	3.78	1.00	0.24	7	517.05	2.31	0.00	0.00
7	466.05	3.60	1.01	0.10	7	518.05	2.57	0.07	0.00
7	467.05	3.12	0.64	0.00	7	519.05	2.32	0.00	0.00
7	468.05	3.33	0.74	0.03	7	520.05	2.27	0.00	0.00
7	470.05	3.31	1.13	0.00	7	521.05	2.27	0.01	0.01
7	472.05	3.18	0.77	0.00	7	522.05	2.29	0.01	0.01
7	473.05	3.17	0.84	0.00	7	523.05	2.17	0.00	0.02

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	524.05	2.26	0.01	0.00	7	575.05	2.19	0.00	0.00
7	525.05	2.27	0.00	0.00	7	576.05	2.52	0.01	0.02
7	526.05	2.59	0.02	0.03	7	577.05	2.42	0.01	0.00
7	527.05	2.59	0.08	0.00	7	578.05	2.46	0.03	0.00
7	528.05	2.57	0.07	0.00	7	579.05	2.52	0.04	0.00
7	530.05	2.59	0.07	0.00	7	580.05	2.33	0.07	0.04
7	531.05	2.57	0.07	0.00	7	581.05	2.45	0.04	0.00
7	532.05	2.46	0.01	0.00	7	582.05	2.55	0.04	0.00
7	533.05	2.57	0.09	0.00	7	583.05	2.39	0.03	0.00
7	534.05	2.53	0.09	0.00	7	584.05	2.41	0.01	0.00
7	535.05	2.59	0.03	0.02	7	585.05	2.49	0.04	0.00
7	536.05	2.59	0.05	0.01	7	586.05	2.27	0.01	0.01
7	537.05	2.59	0.02	0.03	7	587.05	2.39	0.02	0.00
7	538.05	2.53	0.01	0.01	7	588.05	2.39	0.03	0.01
7	539.05	2.41	0.02	0.00	7	589.05	2.39	0.03	0.00
7	540.05	2.57	0.00	0.07	7	590.05	2.39	0.04	0.01
7	541.05	2.39	0.00	0.00	7	591.05	2.39	0.03	0.01
7	542.05	2.27	0.00	0.00	7	592.05	2.39	0.01	0.00
7	543.05	2.27	0.00	0.00	7	593.05	2.39	0.02	0.00
7	544.05	2.27	0.00	0.00	7	594.05	2.39	0.02	0.00
7	545.05	2.27	0.00	0.00	7	595.05	2.39	0.03	0.00
7	546.05	2.27	0.00	0.00	7	596.05	2.24	0.03	0.04
7	547.05	2.27	0.00	0.00	7	597.05	2.48	0.07	0.01
7	548.05	2.27	0.00	0.00	7	598.05	2.44	0.07	0.01
7	549.05	2.27	0.00	0.00	7	599.05	2.20	0.02	0.05
7	550.05	2.27	0.00	0.00	7	600.05	2.49	0.04	0.00
7	551.05	2.27	0.00	0.00	7	601.05	2.10	0.04	0.15
7	552.05	2.37	0.03	0.01	7	602.05	2.49	0.04	0.00
7	553.05	2.22	0.00	0.00	7	603.05	2.49	0.04	0.00
7	554.05	2.16	0.00	0.01	7	604.05	2.34	0.00	0.01
7	555.05	2.18	0.01	0.00	7	605.05	2.49	0.05	0.00
7	556.05	2.43	0.02	0.00	7	606.05	2.27	0.00	0.00
7	557.05	2.21	0.00	0.01	7	607.05	2.54	0.06	0.00
7	558.05	2.43	0.00	0.01	7	608.05	2.53	0.05	0.00
7	559.05	2.13	0.08	0.01	7	609.05	2.27	0.00	0.00
7	560.05	2.42	0.00	0.01	7	610.05	2.27	0.00	0.00
7	561.05	2.13	0.00	0.04	7	611.05	2.40	0.00	0.00
7	562.05	2.35	0.00	0.00	7	612.05	2.36	0.00	0.00
7	563.05	2.30	0.01	0.00	7	613.05	2.38	0.03	0.00
7	564.05	2.37	0.01	0.00	7	614.05	2.21	0.00	0.00
7	565.05	2.34	0.01	0.00	7	615.05	2.45	0.03	0.00
7	566.05	2.37	0.01	0.00	7	616.05	2.22	0.00	0.00
7	567.05	2.37	0.01	0.00	7	617.05	2.32	0.00	0.01
7	568.05	2.36	0.01	0.00	7	618.05	2.32	0.00	0.01
7	569.05	2.37	0.01	0.00	7	619.05	2.32	0.00	0.00
7	570.05	2.37	0.01	0.00	7	620.05	2.32	0.00	0.00
7	571.05	2.42	0.02	0.00	7	621.05	2.32	0.01	0.01
7	572.05	2.37	0.01	0.00	7	622.05	2.25	0.03	0.02
7	573.05	2.26	0.01	0.01	7	623.05	2.12	0.02	0.00
7	574.05	2.28	0.02	0.02	7	624.05	2.05	0.06	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	625.05	2.04	0.06	0.00	7	226.06	1.98	0.24	0.03
7	626.05	1.83	0.23	0.00	7	242.06	1.92	0.77	0.26
7	627.05	1.97	0.08	0.00	7	243.06	2.14	0.49	0.30
7	628.05	2.19	0.04	0.01	7	244.06	1.57	0.35	0.02
7	629.05	2.02	0.04	0.00	7	252.06	1.95	0.69	0.24
7	630.05	1.98	0.08	0.00	7	255.06	1.43	0.74	0.00
7	631.05	1.92	0.14	0.00	7	270.06	1.39	0.09	0.36
7	632.05	1.91	0.15	0.00	7	273.06	1.27	0.09	0.51
7	634.05	1.91	0.24	0.01	7	276.06	1.96	0.18	0.01
7	635.05	1.91	0.16	0.00	7	277.06	1.96	0.15	0.00
7	636.05	1.83	0.25	0.00	7	278.06	1.59	0.02	0.31
7	637.05	1.79	0.23	0.00	7	280.06	2.01	0.11	0.00
7	638.05	1.79	0.21	0.00	7	282.06	2.07	0.07	0.00
7	639.05	1.65	0.35	0.00	7	285.06	1.96	0.11	0.00
7	640.05	1.62	0.30	0.01	7	287.06	1.96	0.11	0.00
7	641.05	1.65	0.48	0.00	7	288.06	1.91	0.15	0.60
7	642.05	1.70	0.30	0.00	7	296.06	2.16	0.18	0.31
7	643.05	1.50	0.59	0.00	7	298.06	1.96	0.01	0.20
7	645.05	1.59	0.28	0.03	7	299.06	2.72	0.22	0.00
7	646.05	1.11	0.30	0.40	7	300.06	2.72	0.22	0.00
7	647.05	1.34	1.67	0.12	7	301.06	2.40	0.07	0.03
7	648.05	0.96	1.32	0.03	7	302.06	2.13	0.16	0.32
7	649.05	1.01	1.33	0.02	7	306.06	2.96	0.12	0.10
7	650.05	1.06	1.41	0.00	7	307.06	2.81	0.32	0.00
7	651.05	1.04	1.30	0.01	7	308.06	2.95	0.06	0.18
7	655.05	1.05	1.29	0.01	7	309.06	3.20	0.12	0.32
7	656.05	1.23	2.40	0.24	7	310.06	3.17	0.44	0.04
7	657.05	1.05	0.79	0.12	7	315.06	2.87	0.30	0.00
7	658.05	0.67	1.45	0.17	7	318.06	2.94	0.26	0.02
7	659.05	0.94	1.44	0.02	7	319.06	2.80	0.29	0.00
7	661.05	0.99	0.70	0.21	7	320.06	3.01	0.52	0.00
7	662.05	1.45	0.81	0.00	7	321.06	3.26	0.62	0.03
7	663.05	1.37	1.31	0.05	7	323.06	3.20	0.41	0.08
7	664.05	1.22	1.52	0.03	7	324.06	3.52	0.95	0.07
7	666.05	4.07	2.42	0.05	7	325.06	3.26	0.90	0.00
7	667.05	3.85	2.34	0.00	7	326.06	3.46	0.74	0.10
7	93.06	0.98	2.21	0.03	7	328.06	3.15	0.50	0.02
7	95.06	0.98	1.88	0.00	7	329.06	3.25	0.75	0.01
7	162.06	1.30	1.32	0.02	7	330.06	3.16	0.79	0.00
7	163.06	0.91	1.17	0.09	7	331.06	3.16	0.74	0.00
7	169.06	1.12	1.09	0.01	7	332.06	3.16	0.79	0.00
7	171.06	1.24	1.12	0.00	7	335.06	3.16	0.83	0.00
7	173.06	1.18	1.05	0.01	7	336.06	3.20	0.86	0.00
7	200.06	1.31	0.67	0.03	7	337.06	3.20	1.23	0.04
7	201.06	1.47	0.68	0.00	7	338.06	2.98	1.10	0.12
7	212.06	2.04	0.11	0.01	7	339.06	2.94	0.54	0.01
7	213.06	1.48	0.06	0.31	7	340.06	3.17	0.82	0.00
7	220.06	2.21	0.20	0.14	7	341.06	3.11	2.50	0.57
7	221.06	2.04	0.19	0.03	7	342.06	3.28	1.88	0.15
7	225.06	1.88	0.11	0.01	7	343.06	2.24	0.61	0.69

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	344.06	2.19	0.65	0.82	7	421.06	4.62	2.91	0.40
7	345.06	3.75	2.32	0.00	7	422.06	4.62	2.99	0.37
7	347.06	3.81	1.94	0.02	7	423.06	4.62	2.94	0.38
7	349.06	3.94	3.30	0.03	7	424.06	4.62	2.92	0.39
7	351.06	4.03	3.07	0.00	7	425.06	4.62	3.16	0.31
7	352.06	3.14	1.18	0.05	7	426.06	4.62	3.10	0.33
7	353.06	3.67	1.55	0.02	7	427.06	4.53	2.69	0.37
7	355.06	3.71	1.59	0.02	7	428.06	4.73	3.44	0.34
7	356.06	3.93	2.67	0.00	7	429.06	4.14	3.01	0.01
7	358.06	3.90	2.43	0.00	7	430.06	3.93	2.53	0.00
7	361.06	3.82	3.01	0.04	7	431.06	3.93	1.29	0.25
7	363.06	3.91	4.84	0.34	7	433.06	3.93	1.11	0.35
7	366.06	4.03	3.06	0.00	7	435.06	3.93	1.88	0.07
7	370.06	3.26	2.29	0.29	7	436.06	4.74	3.91	0.22
7	372.06	3.85	2.66	0.01	7	437.06	4.27	3.30	0.03
7	373.06	3.80	2.31	0.00	7	438.06	3.92	2.35	0.01
7	375.06	3.26	2.91	0.54	7	439.06	4.27	3.32	0.02
7	378.06	3.99	5.56	0.44	7	440.06	4.59	2.64	0.45
7	379.06	4.49	4.68	0.00	7	441.06	4.02	2.62	0.01
7	383.06	3.92	2.71	0.00	7	442.06	4.08	3.27	0.00
7	384.06	4.01	3.61	0.03	7	443.06	4.29	4.17	0.00
7	385.06	4.03	1.95	0.12	7	444.06	4.15	4.96	0.14
7	388.06	3.68	2.01	0.00	7	445.06	4.29	4.65	0.02
7	390.06	3.68	2.23	0.01	7	446.06	4.52	5.01	0.00
7	391.06	4.32	2.90	0.11	7	448.06	4.52	3.44	0.14
7	392.06	3.68	2.63	0.05	7	451.06	4.52	3.10	0.22
7	393.06	3.99	2.74	0.00	7	452.06	4.00	4.01	0.09
7	394.06	3.99	2.50	0.02	7	453.06	4.29	4.11	0.00
7	395.06	3.99	2.50	0.01	7	454.06	4.08	3.00	0.00
7	396.06	3.68	3.17	0.15	7	455.06	4.29	4.66	0.02
7	397.06	3.68	3.58	0.25	7	456.06	4.08	2.93	0.01
7	398.06	3.68	3.19	0.15	7	457.06	4.29	5.15	0.07
7	400.06	3.68	3.16	0.15	7	458.06	4.08	3.30	0.00
7	401.06	4.36	3.15	0.09	7	459.06	4.08	3.19	0.00
7	402.06	4.06	3.76	0.03	7	460.06	4.46	5.28	0.02
7	403.06	3.10	0.98	0.03	7	461.06	4.59	5.29	0.00
7	404.06	4.06	4.08	0.06	7	462.06	4.08	2.28	0.08
7	405.06	4.06	4.12	0.07	7	463.06	4.59	5.19	0.00
7	406.06	4.06	4.11	0.06	7	464.06	4.59	3.51	0.18
7	409.06	4.35	5.04	0.03	7	465.06	4.59	4.11	0.07
7	410.06	4.53	4.91	0.00	7	466.06	4.31	3.20	0.05
7	411.06	4.21	4.71	0.06	7	467.06	4.08	3.22	0.00
7	412.06	4.46	4.78	0.00	7	468.06	4.08	3.44	0.00
7	413.06	4.46	4.88	0.00	7	470.06	4.08	3.62	0.01
7	415.06	4.59	5.45	0.00	7	472.06	4.08	2.19	0.10
7	416.06	4.62	5.45	0.00	7	473.06	4.08	2.62	0.03
7	417.06	4.62	5.63	0.00	7	475.06	3.70	1.63	0.02
7	418.06	4.62	5.49	0.00	7	476.06	4.22	2.36	0.16
7	419.06	4.62	4.35	0.06	7	477.06	3.70	1.78	0.01
7	420.06	4.62	2.62	0.51	7	478.06	3.70	1.86	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	479.06	3.80	1.99	0.01	7	532.06	3.44	1.34	0.00
7	480.06	3.72	1.77	0.01	7	533.06	4.02	1.89	0.12
7	481.06	3.62	1.78	0.00	7	534.06	4.02	1.94	0.11
7	482.06	3.50	1.76	0.01	7	535.06	4.02	1.79	0.15
7	483.06	3.62	1.80	0.00	7	536.06	4.02	1.93	0.11
7	484.06	3.72	1.90	0.00	7	537.06	4.02	1.87	0.13
7	485.06	3.62	1.90	0.00	7	538.06	4.02	1.93	0.11
7	486.06	3.67	2.01	0.00	7	539.06	4.02	1.91	0.12
7	487.06	3.74	2.12	0.00	7	540.06	3.35	1.09	0.00
7	488.06	3.62	2.11	0.02	7	541.06	3.47	1.12	0.01
7	489.06	3.74	2.17	0.00	7	542.06	3.35	0.93	0.01
7	490.06	3.74	2.15	0.00	7	543.06	3.35	0.91	0.01
7	491.06	3.74	2.27	0.00	7	544.06	3.35	0.90	0.01
7	492.06	3.74	2.36	0.01	7	545.06	3.35	0.86	0.02
7	493.06	3.74	3.22	0.12	7	546.06	3.35	0.85	0.02
7	494.06	3.74	3.23	0.12	7	547.06	3.35	0.90	0.01
7	495.06	3.74	2.23	0.00	7	548.06	3.35	0.92	0.01
7	496.06	3.74	1.73	0.02	7	549.06	3.35	0.90	0.01
7	497.06	3.74	2.33	0.01	7	550.06	3.35	0.96	0.01
7	498.06	3.74	2.50	0.02	7	551.06	3.35	0.97	0.00
7	499.06	3.74	1.70	0.02	7	552.06	3.24	0.92	0.00
7	500.06	3.74	1.73	0.02	7	553.06	3.10	0.91	0.02
7	501.06	3.74	2.21	0.00	7	554.06	3.24	0.92	0.00
7	502.06	3.74	1.70	0.02	7	555.06	3.10	0.03	0.43
7	503.06	3.56	1.65	0.00	7	556.06	3.21	0.09	0.39
7	504.06	3.71	1.62	0.02	7	557.06	3.24	0.06	0.50
7	505.06	3.56	1.56	0.00	7	558.06	3.24	0.06	0.50
7	506.06	3.56	1.59	0.00	7	559.06	2.39	0.00	0.01
7	507.06	3.70	1.84	0.00	7	560.06	3.24	0.07	0.47
7	508.06	3.46	1.67	0.02	7	561.06	2.59	0.06	0.00
7	509.06	3.58	1.58	0.00	7	562.06	3.40	0.10	0.65
7	510.06	3.58	1.64	0.00	7	563.06	2.91	0.07	0.13
7	511.06	3.58	0.97	0.09	7	564.06	2.60	0.10	0.00
7	512.06	3.58	0.93	0.11	7	565.06	2.54	0.09	0.00
7	513.06	3.58	0.83	0.15	7	566.06	2.60	0.09	0.00
7	514.06	3.58	0.93	0.10	7	567.06	2.60	0.09	0.00
7	515.06	3.58	1.18	0.04	7	568.06	2.47	0.11	0.02
7	516.06	4.02	1.91	0.12	7	569.06	2.62	0.10	0.00
7	517.06	3.58	1.02	0.08	7	570.06	2.62	0.08	0.00
7	518.06	3.67	2.98	0.12	7	571.06	2.49	0.07	0.00
7	519.06	3.58	1.24	0.03	7	572.06	2.60	0.09	0.00
7	520.06	3.58	1.25	0.03	7	573.06	2.49	0.04	0.00
7	521.06	3.58	1.07	0.07	7	574.06	2.43	0.04	0.00
7	522.06	4.02	1.50	0.25	7	575.06	2.49	0.07	0.00
7	523.06	4.02	1.80	0.15	7	576.06	2.49	0.05	0.00
7	524.06	3.35	0.98	0.00	7	577.06	2.49	0.04	0.00
7	525.06	3.35	1.00	0.00	7	578.06	2.49	0.06	0.00
7	526.06	4.02	1.93	0.11	7	579.06	2.49	0.04	0.00
7	530.06	4.02	1.89	0.12	7	580.06	2.49	0.06	0.00
7	531.06	4.02	2.91	0.00	7	581.06	2.49	0.05	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	582.06	2.49	0.05	0.00	7	634.06	2.65	0.92	0.36
7	583.06	2.49	0.04	0.00	7	635.06	2.35	0.03	0.02
7	584.06	2.49	0.04	0.00	7	636.06	2.41	0.07	0.02
7	585.06	2.49	0.04	0.00	7	637.06	2.56	0.08	0.00
7	586.06	2.49	0.04	0.00	7	638.06	2.56	0.06	0.00
7	587.06	2.33	0.01	0.00	7	639.06	2.44	0.11	0.04
7	588.06	2.22	0.00	0.01	7	640.06	2.32	0.04	0.05
7	589.06	2.49	0.04	0.00	7	641.06	2.77	2.94	1.52
7	590.06	2.43	0.01	0.00	7	642.06	2.39	0.11	0.05
7	591.06	2.58	0.02	0.02	7	643.06	2.44	0.00	0.01
7	592.06	2.34	0.00	0.00	7	645.06	2.43	0.17	0.07
7	593.06	2.59	0.02	0.02	7	646.06	2.42	0.22	0.11
7	594.06	2.30	0.00	0.00	7	647.06	2.09	1.59	1.14
7	595.06	2.44	0.02	0.00	7	648.06	1.24	1.14	0.00
7	596.06	2.30	0.01	0.01	7	649.06	1.03	1.31	0.01
7	597.06	2.44	0.03	0.00	7	650.06	1.07	1.09	0.03
7	598.06	2.44	0.03	0.00	7	651.06	.		
7	599.06	2.44	0.03	0.00	7	655.06	1.13	1.74	0.03
7	600.06	2.59	0.06	0.00	7	656.06	1.33	2.56	0.41
7	601.06	2.44	0.03	0.00	7	657.06	0.89	0.62	0.38
7	603.06	2.56	0.09	0.00	7	658.06	0.63	1.44	0.21
7	604.06	2.28	0.02	0.02	7	659.06	0.99	1.60	0.00
7	605.06	2.49	0.00	0.02	7	661.06	0.93	0.65	0.30
7	606.06	2.15	0.11	0.03	7	662.06	1.48	0.55	0.00
7	607.06	2.42	0.00	0.00	7	663.06	1.39	1.26	0.05
7	608.06	2.36	0.00	0.00	7	664.06	1.24	1.45	0.02
7	609.06	2.15	0.02	0.00	7	666.06	4.03	4.26	0.10
7	610.06	2.25	0.02	0.03	7	667.06	4.35	3.92	0.01
7	611.06	2.21	0.06	0.11	7	670.06	.		
7	612.06	1.95	0.10	0.00	7	671.06	7.02	21.99	0.00
7	613.06	2.19	0.01	0.00	7	672.06	.		
7	614.06	1.98	0.03	0.02	7	93.07	1.17	1.99	0.08
7	615.06	2.22	0.08	0.13	7	95.07	0.98	1.37	0.02
7	616.06	2.58	0.06	0.00	7	200.07	0.91	0.89	0.19
7	617.06	1.80	0.08	0.04	7	201.07	1.35	0.70	0.01
7	618.06	2.00	0.07	0.00	7	221.07	1.36	1.63	0.12
7	619.06	2.00	0.05	0.00	7	242.07	1.26	0.61	0.06
7	620.06	2.12	0.09	0.01	7	243.07	0.99	0.83	0.15
7	621.06	2.16	0.22	0.37	7	244.07	1.05	0.63	0.20
7	622.06	2.13	0.36	0.58	7	252.07	1.43	0.56	0.01
7	623.06	1.97	0.30	0.76	7	255.07	1.53	0.60	0.00
7	624.06	2.67	0.34	0.04	7	270.07	1.34	1.23	0.03
7	625.06	2.87	0.33	0.00	7	273.07	1.50	0.59	0.00
7	626.06	2.47	0.00	0.02	7	276.07	1.58	0.50	0.00
7	627.06	2.33	0.01	0.01	7	277.07	1.58	0.52	0.00
7	628.06	2.83	0.12	0.04	7	278.07	1.44	0.67	0.00
7	629.06	2.52	0.14	0.02	7	280.07	1.42	1.26	0.07
7	630.06	2.84	0.15	0.02	7	282.07	1.78	0.46	0.03
7	631.06	2.48	0.06	0.00	7	285.07	1.69	0.54	0.02
7	632.06	2.54	0.09	0.00	7	287.07	1.56	0.49	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	288.07	1.47	0.72	0.00	7	375.07	1.91	0.08	0.01
7	298.07	1.61	0.49	0.00	7	378.07	1.95	0.05	0.01
7	299.07	1.74	0.39	0.01	7	379.07	1.97	0.04	0.01
7	300.07	1.67	0.38	0.00	7	383.07	2.70	0.15	0.00
7	301.07	1.81	0.36	0.01	7	384.07	2.05	0.17	0.42
7	302.07	1.69	0.37	0.00	7	385.07	2.70	0.51	0.09
7	306.07	1.69	0.39	0.00	7	390.07	2.83	0.86	0.15
7	307.07	1.59	0.46	0.00	7	391.07	2.70	0.37	0.04
7	308.07	1.90	0.20	0.00	7	392.07	3.33	1.00	0.00
7	309.07	1.61	0.29	0.02	7	393.07	2.70	0.43	0.06
7	310.07	1.54	0.46	0.00	7	396.07	3.38	1.53	0.02
7	315.07	1.99	0.32	0.07	7	397.07	3.40	1.18	0.00
7	318.07	1.82	0.29	0.00	7	398.07	3.39	1.26	0.00
7	319.07	1.76	0.26	0.00	7	400.07	3.66	1.68	0.01
7	320.07	1.69	0.36	0.00	7	403.07	1.68	0.48	0.01
7	321.07	1.78	0.26	0.00	7	406.07	.		
7	323.07	1.68	0.40	0.00	7	409.07	3.52	1.56	0.00
7	324.07	2.01	0.20	0.03	7	410.07	3.68	1.88	0.00
7	325.07	1.84	0.16	0.00	7	411.07	3.56	1.69	0.00
7	326.07	1.91	0.14	0.00	7	412.07	3.59	1.75	0.00
7	328.07	1.74	0.24	0.00	7	413.07	3.59	1.81	0.00
7	329.07	1.86	0.15	0.00	7	415.07	3.59	1.82	0.00
7	330.07	1.91	0.11	0.00	7	416.07	3.59	1.85	0.00
7	331.07	1.91	0.08	0.01	7	417.07	3.59	1.86	0.00
7	332.07	1.91	0.07	0.01	7	418.07	3.59	2.05	0.02
7	335.07	1.91	0.07	0.02	7	419.07	3.59	2.85	0.15
7	336.07	1.71	0.37	0.00	7	420.07	3.59	4.43	0.65
7	337.07	1.68	0.34	0.00	7	421.07	3.59	4.43	0.65
7	338.07	1.72	0.35	0.00	7	422.07	3.51	4.23	0.69
7	339.07	1.84	0.22	0.00	7	423.07	3.59	4.54	0.69
7	340.07	1.80	0.23	0.00	7	424.07	3.81	4.82	0.46
7	341.07	1.91	0.07	0.01	7	425.07	4.51	4.75	0.00
7	342.07	2.12	0.04	0.00	7	426.07	3.61	4.93	0.81
7	343.07	1.74	0.20	1.00	7	427.07	4.51	5.59	0.02
7	344.07	1.70	0.54	1.77	7	428.07	4.51	4.86	0.00
7	345.07	2.20	0.00	0.02	7	429.07	4.51	5.45	0.01
7	347.07	2.34	0.03	0.01	7	430.07	4.51	5.77	0.03
7	349.07	2.09	0.01	0.01	7	431.07	4.59	8.27	0.33
7	351.07	2.12	0.03	0.00	7	433.07	5.16	8.71	0.01
7	352.07	1.72	0.28	0.00	7	435.07	5.16	8.68	0.00
7	353.07	2.34	0.16	0.12	7	436.07	4.51	5.62	0.02
7	355.07	2.00	0.15	0.45	7	437.07	4.50	7.07	0.21
7	356.07	2.09	0.08	0.23	7	438.07	4.51	7.75	0.32
7	358.07	2.09	0.13	0.32	7	439.07	4.95	7.13	0.00
7	361.07	2.08	0.03	0.00	7	440.07	4.95	7.30	0.00
7	363.07	2.12	0.03	0.00	7	441.07	5.07	7.57	0.00
7	366.07	2.12	0.03	0.00	7	442.07	4.95	7.35	0.00
7	370.07	1.84	0.13	0.01	7	443.07	5.00	4.81	0.27
7	372.07	2.27	0.24	0.26	7	444.07	4.49	4.84	0.00
7	373.07	1.91	0.12	0.00	7	445.07	5.08	4.86	0.35

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	446.07	4.49	4.93	0.00	7	502.07	4.07	2.93	0.01
7	448.07	4.49	6.66	0.14	7	503.07	3.98	2.76	0.00
7	451.07	4.49	7.35	0.26	7	504.07	3.73	2.86	0.06
7	452.07	5.07	7.80	0.00	7	505.07	3.98	2.91	0.00
7	453.07	5.07	7.43	0.00	7	506.07	3.98	2.76	0.00
7	454.07	4.49	6.86	0.17	7	507.07	3.98	2.91	0.00
7	455.07	5.31	5.27	0.52	7	508.07	3.98	2.86	0.00
7	456.07	4.44	7.03	0.25	7	509.07	4.09	3.19	0.00
7	457.07	4.49	4.91	0.00	7	510.07	3.98	2.98	0.00
7	458.07	4.52	7.13	0.20	7	511.07	4.08	4.36	0.09
7	459.07	4.71	7.50	0.10	7	512.07	4.08	4.55	0.12
7	460.07	4.49	4.73	0.00	7	513.07	4.08	4.58	0.12
7	461.07	4.49	4.94	0.00	7	514.07	4.08	4.43	0.10
7	462.07	4.96	9.46	0.16	7	515.07	3.69	1.85	0.00
7	463.07	4.49	5.05	0.00	7	516.07	4.03	3.09	0.00
7	464.07	4.49	7.63	0.31	7	517.07	3.96	1.87	0.09
7	465.07	4.49	6.38	0.10	7	518.07	3.98	2.91	0.00
7	466.07	4.49	7.41	0.27	7	519.07	3.69	1.91	0.00
7	467.07	4.96	7.59	0.01	7	520.07	3.78	2.12	0.00
7	468.07	4.96	7.40	0.00	7	521.07	3.81	2.28	0.00
7	470.07	4.96	7.24	0.00	7	522.07	3.61	1.97	0.01
7	472.07	4.96	9.95	0.23	7	523.07	3.61	1.82	0.00
7	473.07	4.96	9.17	0.13	7	524.07	3.74	1.85	0.01
7	475.07	5.34	7.68	0.08	7	525.07	3.74	2.16	0.00
7	476.07	4.96	9.78	0.21	7	526.07	3.69	1.88	0.00
7	477.07	5.06	7.48	0.00	7	530.07	3.97	4.08	0.11
7	478.07	5.66	8.74	0.17	7	531.07	3.89	2.83	0.01
7	479.07	4.61	10.31	0.79	7	532.07	3.55	1.77	0.00
7	480.07	5.25	8.40	0.00	7	533.07	3.97	4.17	0.13
7	481.07	5.52	8.11	0.15	7	534.07	3.97	4.15	0.13
7	482.07	5.21	8.14	0.00	7	535.07	4.23	2.96	0.05
7	483.07	5.14	8.01	0.00	7	536.07	3.97	4.13	0.12
7	484.07	5.09	7.93	0.00	7	537.07	4.04	1.96	0.12
7	485.07	5.14	8.21	0.00	7	538.07	3.69	1.93	0.00
7	486.07	5.10	7.94	0.00	7	539.07	3.57	1.74	0.00
7	487.07	5.14	8.13	0.00	7	540.07	3.74	2.13	0.00
7	488.07	5.10	7.85	0.00	7	541.07	3.48	2.12	0.07
7	489.07	5.14	8.18	0.00	7	542.07	3.74	2.08	0.00
7	490.07	5.10	7.90	0.00	7	543.07	3.74	2.15	0.00
7	491.07	5.14	8.20	0.00	7	544.07	3.74	2.11	0.00
7	492.07	5.10	7.88	0.00	7	545.07	3.74	2.19	0.00
7	493.07	5.05	3.35	0.86	7	546.07	3.74	2.24	0.00
7	494.07	5.26	3.88	1.01	7	547.07	3.74	2.12	0.00
7	495.07	5.10	7.73	0.00	7	548.07	3.74	2.11	0.00
7	496.07	3.97	2.37	0.02	7	549.07	3.74	2.19	0.00
7	497.07	5.10	7.58	0.00	7	550.07	3.74	2.14	0.00
7	498.07	5.10	3.53	0.87	7	551.07	3.74	2.10	0.00
7	499.07	3.94	2.88	0.00	7	552.07	3.74	2.37	0.01
7	500.07	5.13	2.85	1.32	7	553.07	3.74	2.33	0.01
7	501.07	5.29	6.62	0.19	7	554.07	3.74	2.39	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	555.07	4.59	5.21	0.00	7	606.07	2.21	0.00	0.02
7	556.07	4.59	2.40	0.57	7	607.07	2.21	0.01	0.00
7	557.07	3.74	5.03	0.62	7	608.07	2.21	0.01	0.00
7	558.07	3.70	5.09	0.71	7	609.07	2.21	0.00	0.02
7	559.07	3.63	0.96	0.13	7	610.07	3.27	0.11	0.43
7	560.07	3.87	5.67	0.64	7	611.07	3.70	0.96	0.18
7	561.07	4.59	2.36	0.59	7	612.07	2.21	0.00	0.01
7	562.07	3.77	5.30	0.68	7	613.07	2.21	0.00	0.02
7	563.07	4.30	2.31	0.25	7	614.07	2.21	0.00	0.01
7	564.07	3.75	2.07	0.00	7	615.07	3.27	0.10	0.43
7	565.07	4.20	2.13	0.20	7	616.07	3.27	0.10	0.45
7	566.07	3.75	2.06	0.00	7	617.07	3.41	0.00	1.37
7	567.07	3.75	2.08	0.00	7	618.07	3.32	0.01	1.31
7	568.07	3.75	2.16	0.00	7	619.07	3.27	0.09	0.46
7	569.07	3.70	1.99	0.00	7	620.07	2.21	0.02	0.04
7	570.07	3.83	2.00	0.02	7	621.07	3.27	0.08	0.49
7	571.07	3.42	2.10	0.10	7	622.07	3.27	0.06	0.54
7	572.07	3.46	1.90	0.04	7	623.07	3.27	0.07	0.51
7	573.07	3.59	1.70	0.00	7	624.07	3.27	0.07	0.51
7	574.07	3.64	1.68	0.00	7	625.07	3.27	0.08	0.49
7	575.07	3.59	1.71	0.00	7	626.07	3.41	0.07	0.74
7	576.07	3.59	1.70	0.00	7	627.07	2.66	0.08	0.01
7	577.07	3.59	1.76	0.00	7	628.07	3.27	0.19	0.30
7	578.07	3.59	1.72	0.00	7	629.07	3.27	0.19	0.30
7	579.07	3.59	1.72	0.00	7	630.07	2.66	0.12	0.00
7	580.07	3.59	1.69	0.00	7	631.07	2.53	0.06	0.00
7	581.07	3.59	1.71	0.00	7	632.07	2.53	0.06	0.00
7	582.07	3.59	1.73	0.00	7	634.07	3.85	0.14	1.41
7	583.07	3.71	1.70	0.01	7	635.07	2.53	0.05	0.00
7	584.07	3.60	1.64	0.00	7	636.07	2.39	0.05	0.01
7	585.07	3.59	1.46	0.01	7	637.07	2.51	0.05	0.00
7	586.07	3.86	2.01	0.02	7	638.07	2.48	0.03	0.00
7	587.07	3.59	0.52	0.34	7	639.07	2.38	0.02	0.00
7	588.07	3.59	0.52	0.34	7	640.07	1.69	0.18	0.03
7	589.07	3.95	2.06	0.05	7	641.07	2.53	0.05	0.00
7	590.07	3.59	0.49	0.36	7	642.07	2.30	0.02	0.02
7	591.07	3.59	0.50	0.36	7	643.07	1.39	0.81	0.00
7	592.07	3.45	0.13	0.65	7	645.07	1.52	0.63	0.00
7	593.07	3.59	0.54	0.33	7	646.07	1.66	0.59	0.02
7	594.07	2.65	0.15	0.00	7	647.07	0.97	1.53	0.01
7	595.07	3.59	0.54	0.33	7	648.07	2.31	0.77	0.81
7	596.07	2.65	0.20	0.01	7	649.07	2.42	0.95	1.22
7	597.07	3.71	0.57	0.44	7	650.07	2.67	0.01	0.07
7	598.07	3.66	0.55	0.40	7	651.07	2.18	0.22	0.13
7	599.07	3.03	0.56	0.00	7	655.07	1.29	2.15	0.21
7	600.07	2.65	0.13	0.00	7	656.07	.		
7	601.07	3.03	0.55	0.00	7	657.07	0.75	0.39	0.84
7	603.07	3.03	0.50	0.00	7	658.07	1.52	1.67	0.27
7	604.07	2.21	0.00	0.01	7	659.07	0.86	1.60	0.03
7	605.07	3.38	0.01	1.37	7	661.07	0.93	0.61	0.33

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	662.07	1.51	0.62	0.00	7	352.08	2.05	0.04	0.00
7	663.07	1.42	1.25	0.06	7	353.08	1.89	0.07	0.02
7	664.07	1.25	1.40	0.02	7	355.08	2.01	0.12	0.01
7	666.07	2.09	0.01	0.09	7	358.08	2.11	0.03	0.00
7	667.07	2.09	0.04	0.17	7	361.08	2.03	0.03	0.01
7	672.07	3.54	0.06	1.02	7	363.08	2.03	0.03	0.01
7	674.07	1.75	0.26	1.10	7	366.08	2.03	0.03	0.01
7	675.07	1.36	0.09	1.52	7	370.08	2.15	0.01	0.00
7	221.08	0.96	1.72	0.00	7	372.08	2.03	0.07	0.00
7	242.08	1.09	0.65	0.16	7	373.08	2.15	0.05	0.01
7	243.08	1.48	0.72	0.00	7	375.08	2.05	0.07	0.00
7	244.08	1.53	0.95	0.05	7	378.08	2.07	0.07	0.00
7	252.08	1.32	0.98	0.00	7	379.08	2.11	0.08	0.01
7	255.08	1.31	1.01	0.00	7	383.08	1.93	0.13	0.00
7	273.08	1.25	1.16	0.00	7	384.08	1.93	0.13	0.00
7	278.08	1.23	1.09	0.00	7	385.08	2.31	0.00	0.00
7	280.08	1.24	0.76	0.03	7	391.08	2.08	0.00	0.05
7	285.08	1.24	1.12	0.00	7	392.08	1.87	0.05	0.04
7	287.08	1.23	1.11	0.00	7	393.08	2.31	0.00	0.00
7	298.08	1.69	0.39	0.00	7	396.08	2.31	0.00	0.00
7	301.08	1.44	0.36	0.06	7	397.08	2.11	0.00	0.04
7	302.08	1.69	0.39	0.00	7	403.08	2.01	0.14	0.01
7	306.08	1.84	0.15	0.00	7	406.08	1.32	0.98	0.00
7	307.08	1.83	0.28	0.00	7	409.08	1.97	0.00	0.12
7	308.08	1.84	0.17	0.00	7	410.08	2.32	0.00	0.01
7	309.08	1.84	0.18	0.00	7	411.08	2.48	0.01	0.01
7	310.08	1.84	0.17	0.00	7	412.08	2.39	0.01	0.00
7	315.08	1.74	0.08	0.07	7	413.08	2.39	0.01	0.00
7	318.08	1.80	0.15	0.01	7	415.08	2.39	0.01	0.00
7	319.08	1.90	0.15	0.00	7	416.08	2.39	0.02	0.00
7	321.08	1.75	0.06	0.08	7	417.08	2.39	0.02	0.00
7	323.08	1.90	0.20	0.00	7	418.08	2.39	0.03	0.00
7	324.08	2.04	0.02	0.01	7	419.08	2.39	0.02	0.00
7	325.08	2.15	0.01	0.00	7	420.08	2.39	0.05	0.01
7	326.08	1.77	0.06	0.08	7	421.08	2.39	0.02	0.00
7	328.08	1.84	0.16	0.00	7	422.08	2.58	0.07	0.00
7	329.08	2.05	0.06	0.00	7	423.08	2.39	0.02	0.00
7	330.08	2.05	0.08	0.00	7	424.08	2.36	0.02	0.01
7	331.08	2.05	0.07	0.00	7	425.08	2.42	0.03	0.00
7	332.08	2.05	0.06	0.00	7	426.08	2.42	0.02	0.00
7	335.08	2.05	0.04	0.00	7	427.08	2.35	0.00	0.00
7	338.08	1.84	0.15	0.00	7	428.08	2.42	0.03	0.00
7	339.08	2.01	0.05	0.00	7	429.08	2.59	0.04	0.01
7	340.08	1.84	0.16	0.00	7	430.08	2.34	0.01	0.00
7	341.08	2.05	0.10	0.01	7	431.08	2.34	0.01	0.00
7	342.08	2.03	0.03	0.01	7	433.08	2.36	0.02	0.00
7	345.08	2.23	0.03	0.01	7	435.08	2.46	0.02	0.00
7	347.08	2.10	0.06	0.00	7	436.08	2.48	0.03	0.00
7	349.08	1.94	0.13	0.00	7	437.08	2.48	0.04	0.00
7	351.08	2.03	0.03	0.01	7	438.08	2.46	0.04	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	439.08	2.64	0.04	0.02	7	500.08	4.72	10.43	0.64
7	440.08	2.46	0.03	0.00	7	501.08	3.88	6.01	0.74
7	441.08	2.41	0.02	0.00	7	502.08	4.72	10.43	0.64
7	442.08	2.48	0.03	0.00	7	503.08	5.59	11.05	0.00
7	443.08	2.44	0.49	0.30	7	504.08	4.82	10.92	0.60
7	444.08	2.34	0.51	0.45	7	505.08	5.59	10.69	0.00
7	445.08	2.42	0.49	0.32	7	506.08	5.59	11.15	0.00
7	446.08	3.00	0.44	0.00	7	507.08	5.59	9.61	0.04
7	448.08	3.00	0.50	0.00	7	508.08	5.59	9.47	0.05
7	451.08	3.00	0.57	0.00	7	509.08	5.18	5.14	0.39
7	452.08	2.46	0.05	0.00	7	510.08	5.68	8.35	0.25
7	454.08	2.43	0.82	0.59	7	511.08	5.18	5.21	0.37
7	455.08	2.65	0.72	0.24	7	512.08	5.70	5.21	1.27
7	456.08	3.16	0.69	0.00	7	513.08	4.35	4.58	0.01
7	457.08	2.55	0.81	0.40	7	514.08	4.21	4.15	0.01
7	458.08	3.33	1.07	0.00	7	515.08	4.74	7.42	0.08
7	459.08	3.20	0.89	0.00	7	517.08	4.33	7.85	0.59
7	460.08	3.19	0.81	0.00	7	518.08	5.50	3.68	1.66
7	461.08	3.19	0.77	0.00	7	519.08	4.84	7.54	0.04
7	462.08	3.42	1.14	0.00	7	520.08	5.35	9.31	0.00
7	463.08	3.19	0.75	0.00	7	521.08	5.12	8.25	0.00
7	464.08	3.19	0.68	0.00	7	522.08	5.42	8.80	0.03
7	465.08	3.19	0.78	0.00	7	523.08	4.99	8.78	0.07
7	466.08	3.19	0.75	0.00	7	524.08	4.65	5.55	0.00
7	467.08	3.24	0.79	0.00	7	525.08	5.33	5.59	0.46
7	468.08	3.32	1.02	0.00	7	530.08	4.42	4.09	0.01
7	470.08	3.12	0.75	0.00	7	531.08	4.21	3.81	0.00
7	472.08	.			7	532.08	4.98	9.59	0.16
7	473.08	3.18	0.64	0.01	7	533.08	4.21	3.93	0.00
7	475.08	3.62	2.14	0.02	7	534.08	5.57	4.35	1.41
7	477.08	3.42	2.20	0.13	7	535.08	4.42	7.06	0.27
7	478.08	3.62	1.77	0.00	7	536.08	4.49	4.87	0.00
7	479.08	3.29	1.05	0.00	7	537.08	4.95	8.80	0.10
7	482.08	3.88	2.50	0.00	7	538.08	5.05	9.34	0.09
7	483.08	3.93	2.54	0.00	7	539.08	5.35	9.34	0.00
7	484.08	3.88	2.54	0.00	7	540.08	5.39	5.74	0.49
7	485.08	3.88	2.45	0.00	7	541.08	5.39	5.72	0.50
7	486.08	3.88	2.49	0.00	7	542.08	4.65	5.47	0.00
7	487.08	3.88	2.50	0.00	7	543.08	4.67	5.35	0.00
7	488.08	3.88	2.55	0.00	7	544.08	4.60	5.34	0.00
7	489.08	3.88	2.36	0.00	7	545.08	4.60	5.27	0.00
7	490.08	3.88	2.43	0.00	7	546.08	4.45	5.31	0.02
7	491.08	3.88	2.46	0.00	7	547.08	4.72	28.48	8.43
7	492.08	3.88	2.36	0.00	7	548.08	7.63	26.93	0.02
7	493.08	4.42	5.91	0.09	7	549.08	4.59	5.45	0.00
7	494.08	3.69	5.75	0.99	7	550.08	4.73	6.46	0.01
7	495.08	3.88	2.50	0.00	7	551.08	4.54	4.45	0.02
7	497.08	3.88	2.61	0.00	7	552.08	4.73	5.81	0.00
7	498.08	3.88	5.66	0.62	7	553.08	4.40	2.25	0.37
7	499.08	4.72	10.43	0.64	7	555.08	5.01	6.24	0.05

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	556.08	4.56	6.06	0.04	7	607.08	4.00	5.15	0.31
7	557.08	4.50	2.47	0.41	7	608.08	3.86	2.13	0.01
7	558.08	3.86	2.46	0.00	7	609.08	3.86	1.56	0.10
7	559.08	4.73	11.44	0.88	7	610.08	4.00	5.43	0.38
7	560.08	4.69	7.41	0.10	7	611.08	4.00	2.99	0.00
7	561.08	4.73	5.72	0.00	7	612.08	3.59	1.78	0.00
7	562.08	3.86	2.54	0.00	7	613.08	3.86	1.70	0.07
7	563.08	4.69	5.80	0.00	7	614.08	3.59	1.60	0.00
7	564.08	4.57	4.09	0.07	7	615.08	4.00	5.08	0.29
7	565.08	4.46	5.20	0.01	7	616.08	4.11	4.83	0.14
7	566.08	4.57	4.00	0.08	7	617.08	3.98	2.33	0.03
7	567.08	4.57	3.87	0.10	7	618.08	3.74	2.10	0.00
7	568.08	4.57	3.76	0.12	7	619.08	4.60	2.73	0.43
7	569.08	4.27	3.71	0.00	7	620.08	3.59	1.61	0.00
7	570.08	4.60	3.93	0.11	7	621.08	4.11	5.57	0.29
7	571.08	4.05	3.87	0.04	7	622.08	4.65	5.15	0.01
7	572.08	4.27	3.79	0.00	7	623.08	4.14	5.33	0.21
7	573.08	4.15	1.47	0.42	7	624.08	4.60	3.56	0.18
7	574.08	4.00	3.45	0.02	7	625.08	4.60	3.14	0.29
7	575.08	4.02	1.41	0.29	7	626.08	3.82	2.35	0.00
7	576.08	4.15	1.49	0.40	7	627.08	3.82	2.31	0.00
7	577.08	4.15	1.45	0.43	7	628.08	4.60	2.74	0.42
7	578.08	4.15	1.41	0.45	7	629.08	3.85	1.77	0.05
7	579.08	4.15	1.46	0.42	7	630.08	4.20	2.46	0.12
7	580.08	4.15	1.41	0.45	7	631.08	3.83	2.24	0.00
7	581.08	4.27	1.43	0.62	7	632.08	3.83	2.25	0.00
7	582.08	3.49	1.32	0.00	7	634.08	4.08	2.79	0.01
7	583.08	3.45	1.31	0.00	7	635.08	3.83	2.55	0.00
7	584.08	3.45	1.22	0.00	7	636.08	3.58	2.58	0.10
7	585.08	4.13	1.35	0.46	7	637.08	3.90	2.67	0.00
7	586.08	3.48	1.05	0.03	7	638.08	3.60	2.38	0.05
7	587.08	3.34	2.16	0.18	7	639.08	3.23	0.95	0.00
7	588.08	3.20	2.18	0.32	7	640.08	3.37	0.18	2.27
7	589.08	3.49	1.42	0.00	7	641.08	3.83	2.31	0.00
7	590.08	.			7	642.08	3.55	1.41	0.01
7	591.08	3.56	2.83	0.17	7	643.08	1.46	0.61	0.00
7	592.08	4.00	2.87	0.00	7	645.08	1.59	0.53	0.00
7	593.08	3.57	3.00	0.20	7	646.08	2.93	0.44	1.70
7	594.08	4.00	2.93	0.00	7	647.08	2.01	1.21	0.67
7	595.08	4.02	2.92	0.00	7	648.08	1.24	1.11	0.00
7	596.08	4.00	2.99	0.00	7	649.08	1.24	1.09	0.00
7	597.08	3.43	2.93	0.33	7	650.08	1.20	1.23	0.00
7	598.08	3.77	2.94	0.06	7	651.08	2.90	0.34	1.43
7	599.08	4.00	2.81	0.00	7	656.08	2.20	1.19	1.00
7	600.08	4.00	3.18	0.00	7	657.08	1.13	0.66	0.12
7	601.08	4.00	2.75	0.00	7	658.08	1.35	1.53	0.09
7	603.08	4.00	2.75	0.00	7	659.08	0.91	1.72	0.00
7	604.08	3.75	1.55	0.05	7	661.08	0.89	0.64	0.36
7	605.08	4.00	5.47	0.39	7	662.08	1.49	0.61	0.00
7	606.08	3.85	1.96	0.02	7	663.08	1.40	1.30	0.06

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	664.08	1.22	1.06	0.00	7	485.09	2.13	0.07	0.01
7	672.08	3.56	2.37	0.07	7	486.09	2.33	0.00	0.00
7	674.08	1.47	0.02	0.89	7	487.09	2.23	0.03	0.02
7	675.08	2.55	0.01	0.02	7	488.09	2.33	0.00	0.00
7	252.09	0.95	1.59	0.01	7	489.09	2.21	0.02	0.01
7	255.09	0.96	1.52	0.01	7	490.09	2.47	0.00	0.02
7	353.09	2.22	0.01	0.00	7	491.09	2.14	0.01	0.01
7	355.09	2.29	0.00	0.00	7	492.09	2.33	0.00	0.00
7	358.09	1.07	0.00	1.34	7	493.09	2.33	0.00	0.00
7	383.09	2.09	0.22	0.07	7	494.09	2.33	0.00	0.00
7	384.09	2.29	0.05	0.05	7	497.09	2.47	0.00	0.01
7	392.09	1.96	0.08	0.00	7	498.09	2.34	0.00	0.00
7	406.09	0.95	1.37	0.03	7	499.09	2.32	0.01	0.01
7	418.09	2.16	0.07	0.16	7	500.09	2.33	0.01	0.00
7	420.09	2.51	0.05	0.00	7	501.09	2.33	0.00	0.00
7	421.09	2.62	0.05	0.01	7	502.09	2.39	0.01	0.00
7	422.09	2.52	0.02	0.01	7	503.09	2.39	0.01	0.00
7	423.09	2.51	0.04	0.00	7	504.09	2.39	0.01	0.00
7	424.09	2.44	0.04	0.00	7	505.09	2.39	0.02	0.00
7	425.09	2.46	0.02	0.00	7	506.09	2.39	0.01	0.00
7	426.09	2.48	0.03	0.00	7	507.09	2.34	0.08	0.06
7	427.09	2.16	0.09	0.03	7	508.09	2.49	0.16	0.04
7	428.09	2.50	0.02	0.12	7	509.09	3.33	1.12	0.00
7	429.09	2.16	0.01	0.00	7	510.09	2.69	0.34	0.04
7	430.09	1.94	0.16	0.00	7	511.09	3.27	0.77	0.01
7	431.09	2.09	0.08	0.01	7	512.09	3.50	1.30	0.00
7	433.09	2.09	0.08	0.01	7	513.09	3.34	1.09	0.00
7	435.09	1.98	0.14	0.01	7	514.09	3.15	0.60	0.01
7	438.09	1.98	0.12	0.00	7	515.09	3.09	0.62	0.00
7	440.09	1.98	0.12	0.00	7	517.09	3.24	0.64	0.02
7	442.09	2.07	0.09	0.01	7	518.09	3.30	1.21	0.01
7	443.09	1.79	0.27	0.00	7	519.09	3.09	0.64	0.00
7	444.09	1.71	0.12	0.05	7	520.09	3.09	0.61	0.00
7	446.09	1.75	0.07	0.08	7	524.09	4.16	3.67	0.00
7	448.09	2.03	0.06	0.00	7	525.09	3.83	3.50	0.11
7	451.09	2.15	0.04	0.00	7	530.09	3.34	1.16	0.00
7	452.09	2.00	0.15	0.01	7	531.09	3.42	1.10	0.01
7	454.09	2.08	0.03	0.00	7	532.09	3.05	0.82	0.02
7	456.09	2.24	0.01	0.00	7	533.09	3.34	1.09	0.00
7	457.09	1.90	0.25	0.01	7	534.09	3.34	1.11	0.00
7	464.09	2.03	0.07	0.00	7	535.09	3.34	0.91	0.01
7	465.09	1.92	0.06	0.02	7	536.09	3.34	1.17	0.00
7	470.09	2.24	0.00	0.00	7	537.09	3.41	0.87	0.03
7	475.09	2.29	0.00	0.00	7	538.09	3.22	0.86	0.00
7	477.09	2.29	0.00	0.00	7	539.09	3.09	0.61	0.00
7	478.09	2.29	0.00	0.00	7	540.09	3.12	3.39	1.01
7	479.09	2.36	0.00	0.01	7	541.09	3.34	3.32	0.60
7	482.09	2.21	0.03	0.01	7	542.09	4.16	3.61	0.00
7	483.09	2.29	0.00	0.00	7	543.09	3.98	3.60	0.04
7	484.09	2.42	0.00	0.01	7	544.09	4.12	3.61	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	545.09	4.35	3.80	0.01	7	603.09	4.56	5.37	0.00
7	546.09	4.26	3.66	0.00	7	604.09	4.43	5.33	0.03
7	547.09	2.43	1.09	0.82	7	605.09	3.75	1.90	0.01
7	548.09	3.50	1.19	0.01	7	606.09	4.76	6.37	0.00
7	552.09	4.30	3.68	0.01	7	607.09	4.47	3.45	0.10
7	553.09	4.30	7.30	0.47	7	608.09	4.68	5.54	0.00
7	555.09	4.10	3.66	0.01	7	609.09	4.81	5.98	0.01
7	556.09	4.07	3.68	0.02	7	610.09	4.47	3.47	0.10
7	557.09	4.99	7.56	0.00	7	611.09	4.69	4.76	0.05
7	558.09	4.99	7.57	0.00	7	612.09	4.65	3.83	0.17
7	559.09	4.31	7.19	0.44	7	613.09	4.65	5.83	0.00
7	560.09	4.32	3.98	0.00	7	614.09	4.25	3.77	0.00
7	561.09	4.21	3.75	0.00	7	615.09	4.47	3.09	0.18
7	563.09	4.35	5.67	0.11	7	616.09	4.47	3.26	0.14
7	564.09	5.29	10.77	0.08	7	617.09	4.44	4.37	0.00
7	565.09	4.62	9.02	0.45	7	618.09	4.18	4.61	0.07
7	566.09	5.29	10.87	0.09	7	621.09	3.75	2.37	0.01
7	567.09	4.18	11.02	2.03	7	622.09	4.32	3.03	0.08
7	568.09	5.64	10.92	0.00	7	626.09	4.44	4.64	0.00
7	569.09	5.50	10.58	0.00	7	627.09	4.44	4.49	0.00
7	570.09	5.64	10.33	0.02	7	630.09	4.41	4.90	0.01
7	571.09	5.50	7.62	0.21	7	631.09	4.44	2.58	0.29
7	572.09	5.50	10.63	0.00	7	632.09	4.44	3.30	0.11
7	573.09	4.82	9.94	0.39	7	634.09	4.34	6.77	0.31
7	574.09	5.14	6.38	0.11	7	635.09	4.40	1.00	1.24
7	575.09	4.89	10.05	0.32	7	636.09	3.26	0.99	0.00
7	576.09	4.82	9.99	0.40	7	637.09	3.28	0.98	0.00
7	577.09	4.82	9.89	0.38	7	638.09	3.04	1.23	0.13
7	578.09	4.82	9.94	0.39	7	639.09	3.26	0.57	2.98
7	579.09	4.82	9.92	0.39	7	640.09	.		
7	580.09	4.82	9.94	0.39	7	641.09	4.44	1.56	0.81
7	582.09	5.63	10.36	0.01	7	642.09	3.15	1.50	0.13
7	583.09	5.49	10.41	0.00	7	643.09	2.03	0.65	0.30
7	584.09	5.49	10.26	0.00	7	645.09	1.83	0.01	0.12
7	585.09	5.49	10.47	0.00	7	646.09	2.30	0.06	0.06
7	586.09	5.52	10.23	0.00	7	647.09	1.31	1.68	0.10
7	587.09	4.57	3.89	0.10	7	648.09	1.17	1.31	0.00
7	588.09	5.31	11.21	0.11	7	649.09	1.16	1.26	0.00
7	590.09	4.20	5.57	0.20	7	650.09	1.12	1.42	0.00
7	591.09	5.51	8.67	0.08	7	651.09	2.34	0.08	0.05
7	592.09	4.64	5.16	0.01	7	656.09	0.91	1.37	0.05
7	593.09	5.23	6.05	0.23	7	657.09	1.06	0.89	0.08
7	594.09	4.56	5.09	0.00	7	659.09	1.18	1.91	0.08
7	595.09	5.22	5.68	0.29	7	661.09	0.83	0.51	0.56
7	596.09	4.56	5.01	0.00	7	662.09	1.57	0.54	0.00
7	597.09	4.86	5.72	0.03	7	663.09	1.48	1.26	0.10
7	598.09	4.68	5.75	0.00	7	664.09	1.24	1.17	0.00
7	599.09	4.68	5.89	0.00	7	672.09	4.44	4.51	0.00
7	600.09	4.44	2.12	0.48	7	674.09	1.34	0.01	1.13
7	601.09	4.68	6.04	0.00	7	675.09	1.82	0.24	0.93

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	678.09	2.58	0.13	0.01	7	497.10	1.73	0.38	0.00
7	679.09	5.37	9.65	0.00	7	498.10	1.67	0.40	0.00
7	681.09	1.51	0.08	1.12	7	499.10	1.64	0.39	0.00
7	252.10	0.86	2.08	0.00	7	500.10	1.65	0.34	0.00
7	255.10	0.90	1.99	0.00	7	501.10	1.67	0.44	0.00
7	353.10	1.76	0.26	0.00	7	502.10	1.66	0.40	0.00
7	358.10	0.88	0.23	0.87	7	503.10	1.66	0.36	0.00
7	383.10	1.53	1.68	0.29	7	504.10	1.66	0.35	0.00
7	384.10	1.71	0.59	0.04	7	505.10	1.66	0.35	0.00
7	406.10	0.95	2.03	0.01	7	506.10	1.66	0.40	0.00
7	422.10	1.04	0.84	0.11	7	507.10	1.66	0.40	0.00
7	424.10	1.37	0.92	0.00	7	508.10	1.66	0.41	0.00
7	425.10	1.42	0.85	0.00	7	509.10	1.58	0.33	0.02
7	426.10	1.40	0.76	0.00	7	510.10	1.66	0.41	0.00
7	427.10	1.56	0.74	0.02	7	511.10	1.98	0.07	0.00
7	428.10	1.43	0.54	0.01	7	512.10	1.72	0.30	0.00
7	429.10	1.56	0.55	0.00	7	513.10	1.92	0.22	0.01
7	430.10	1.49	0.64	0.00	7	514.10	1.90	0.20	0.00
7	431.10	1.36	0.63	0.02	7	515.10	1.84	0.18	0.00
7	433.10	1.49	0.66	0.00	7	517.10	1.84	0.17	0.00
7	438.10	1.53	0.49	0.00	7	518.10	1.83	0.09	0.02
7	440.10	.			7	519.10	1.84	0.18	0.00
7	443.10	1.70	0.49	0.01	7	520.10	1.84	0.16	0.00
7	444.10	1.80	0.31	0.01	7	524.10	1.93	0.13	0.00
7	446.10	1.40	0.45	0.05	7	525.10	1.99	0.13	0.00
7	448.10	1.58	0.39	0.01	7	530.10	1.94	0.20	0.01
7	451.10	1.67	0.43	0.00	7	531.10	1.70	0.13	0.05
7	452.10	1.56	0.51	0.00	7	532.10	2.01	0.14	0.01
7	454.10	1.69	0.43	0.00	7	533.10	1.92	0.18	0.00
7	456.10	1.69	0.48	0.01	7	534.10	1.92	0.21	0.01
7	457.10	1.55	0.36	0.02	7	535.10	1.83	0.18	0.00
7	464.10	1.78	0.25	0.00	7	537.10	1.82	0.15	0.01
7	465.10	1.48	0.55	0.00	7	538.10	1.90	0.14	0.00
7	470.10	1.59	0.47	0.00	7	539.10	1.84	0.16	0.00
7	475.10	1.49	0.59	0.00	7	542.10	1.93	0.12	0.00
7	477.10	1.72	0.35	0.00	7	543.10	1.93	0.12	0.00
7	478.10	1.61	0.64	0.02	7	544.10	1.93	0.19	0.00
7	479.10	1.54	0.48	0.00	7	545.10	1.93	0.14	0.00
7	482.10	1.66	0.55	0.01	7	546.10	1.93	0.19	0.01
7	484.10	1.64	0.45	0.00	7	552.10	2.07	0.09	0.01
7	485.10	1.47	0.77	0.00	7	553.10	2.00	0.09	0.00
7	486.10	1.86	0.42	0.05	7	555.10	2.11	0.16	0.05
7	487.10	1.74	0.50	0.03	7	556.10	1.90	0.03	0.05
7	488.10	1.64	0.48	0.00	7	559.10	1.74	0.31	0.00
7	489.10	1.48	0.89	0.02	7	561.10	2.23	0.00	0.00
7	490.10	1.55	0.54	0.00	7	563.10	2.02	0.01	0.03
7	491.10	1.35	0.89	0.00	7	564.10	2.27	0.00	0.00
7	492.10	1.58	0.47	0.00	7	565.10	2.08	0.00	0.04
7	493.10	1.68	0.41	0.00	7	566.10	2.27	0.01	0.01
7	494.10	1.56	0.42	0.01	7	567.10	2.02	0.00	0.08

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	569.10	2.14	0.00	0.01	7	630.10	4.01	4.61	0.19
7	571.10	2.26	0.16	0.19	7	631.10	3.89	4.47	0.26
7	572.10	2.44	0.02	0.00	7	632.10	3.89	3.85	0.13
7	573.10	3.08	0.66	0.00	7	634.10	3.93	3.13	0.02
7	574.10	2.58	0.62	0.25	7	635.10	4.57	5.96	0.03
7	575.10	3.08	0.66	0.00	7	636.10	4.25	4.56	0.03
7	576.10	3.08	0.66	0.00	7	637.10	4.43	3.83	0.03
7	577.10	3.08	0.65	0.00	7	638.10	4.08	2.07	0.13
7	578.10	3.08	0.58	0.00	7	639.10	1.99	1.16	0.61
7	579.10	3.08	0.65	0.00	7	640.10	3.48	0.05	1.97
7	580.10	3.08	0.64	0.00	7	641.10	3.83	5.19	0.55
7	582.10	3.08	0.66	0.00	7	642.10	1.95	0.01	0.05
7	583.10	3.10	0.70	0.00	7	643.10	1.35	0.62	0.02
7	584.10	3.10	0.70	0.00	7	645.10	1.56	0.53	0.00
7	585.10	3.10	0.66	0.00	7	646.10	1.16	0.74	0.07
7	586.10	3.10	0.60	0.00	7	647.10	1.33	1.78	0.14
7	587.10	3.62	1.62	0.00	7	648.10	0.82	1.59	0.04
7	588.10	2.87	0.68	0.06	7	649.10	1.19	1.49	0.01
7	590.10	1.76	0.39	0.01	7	650.10	1.08	1.31	0.00
7	591.10	3.29	1.22	0.01	7	651.10	2.19	0.83	0.65
7	592.10	3.56	1.72	0.00	7	656.10	0.83	1.45	0.07
7	593.10	3.10	1.69	0.24	7	657.10	0.94	0.85	0.18
7	594.10	3.56	1.71	0.00	7	659.10	1.20	1.85	0.08
7	595.10	3.59	1.90	0.01	7	661.10	0.85	0.65	0.41
7	596.10	3.47	1.09	0.02	7	662.10	1.48	0.67	0.00
7	597.10	3.59	1.70	0.00	7	663.10	1.39	1.50	0.11
7	598.10	3.59	1.75	0.00	7	664.10	1.15	1.63	0.02
7	599.10	3.59	1.77	0.00	7	672.10	3.96	2.57	0.00
7	600.10	3.84	2.38	0.00	7	674.10	15.07	163.08	0.00
7	601.10	3.59	1.74	0.00	7	675.10	.		
7	603.10	3.56	1.77	0.00	7	677.10	1.56	0.75	0.02
7	604.10	3.88	2.75	0.00	7	678.10	.		
7	605.10	3.83	2.49	0.00	7	679.10	3.10	0.62	0.00
7	606.10	3.87	2.63	0.00	7	680.10	3.10	0.75	0.00
7	607.10	3.86	2.67	0.00	7	681.10	1.21	0.01	1.40
7	608.10	3.83	2.54	0.00	7	427.11	1.02	0.74	0.17
7	609.10	3.87	2.64	0.00	7	430.11	1.68	0.61	0.03
7	610.10	3.56	2.48	0.09	7	431.11	1.26	0.77	0.02
7	611.10	3.75	1.59	0.04	7	433.11	1.44	0.71	0.00
7	612.10	3.68	3.00	0.11	7	438.11	1.48	0.63	0.00
7	613.10	3.72	1.66	0.02	7	443.11	1.66	0.52	0.01
7	614.10	4.02	3.31	0.01	7	444.11	1.65	0.40	0.00
7	615.10	3.83	2.53	0.00	7	446.11	1.66	0.58	0.02
7	616.10	3.83	2.74	0.01	7	448.11	1.67	0.68	0.04
7	617.10	3.91	1.28	0.24	7	451.11	1.46	0.65	0.00
7	618.10	3.59	1.04	0.08	7	452.11	1.47	0.75	0.00
7	621.10	3.96	2.53	0.01	7	454.11	1.50	0.69	0.00
7	622.10	3.63	2.49	0.06	7	457.11	1.33	0.65	0.02
7	626.10	3.68	1.14	0.11	7	464.11	1.49	0.40	0.03
7	627.10	3.92	1.24	0.27	7	465.11	1.66	0.49	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	470.11	1.40	0.77	0.00	7	565.11	1.86	0.04	0.38
7	484.11	1.47	0.74	0.00	7	566.11	1.82	0.16	0.00
7	485.11	1.52	0.92	0.04	7	567.11	1.61	0.09	0.14
7	488.11	1.48	0.64	0.00	7	571.11	1.68	0.51	0.01
7	489.11	1.53	0.59	0.00	7	572.11	1.73	0.38	0.00
7	490.11	1.51	0.55	0.00	7	573.11	1.55	0.49	0.00
7	491.11	1.52	0.55	0.00	7	574.11	1.59	0.55	0.00
7	492.11	1.68	0.49	0.01	7	575.11	1.55	0.48	0.00
7	493.11	1.75	0.29	0.00	7	576.11	1.55	0.54	0.00
7	494.11	1.75	0.28	0.00	7	577.11	1.55	0.52	0.00
7	497.11	1.59	0.53	0.00	7	578.11	1.55	0.51	0.00
7	498.11	1.74	0.29	0.00	7	579.11	1.55	0.48	0.00
7	499.11	1.56	0.59	0.00	7	580.11	1.55	0.47	0.00
7	500.11	1.62	0.54	0.00	7	583.11	1.60	0.43	0.00
7	503.11	1.72	0.42	0.01	7	584.11	1.60	0.44	0.00
7	504.11	1.64	0.52	0.00	7	585.11	1.67	0.48	0.01
7	505.11	1.64	0.51	0.00	7	586.11	1.60	0.42	0.00
7	506.11	1.64	0.50	0.00	7	587.11	1.79	0.24	0.00
7	507.11	1.64	0.51	0.00	7	588.11	1.38	0.85	0.00
7	508.11	1.64	0.50	0.00	7	590.11	1.82	0.85	0.21
7	509.11	1.67	0.79	0.07	7	592.11	1.80	0.27	0.00
7	510.11	1.64	0.54	0.01	7	593.11	1.99	0.25	0.04
7	511.11	1.42	0.95	0.01	7	594.11	1.79	0.34	0.01
7	512.11	1.46	0.91	0.02	7	595.11	1.60	0.23	0.04
7	513.11	1.46	0.94	0.02	7	596.11	1.76	0.46	0.02
7	514.11	1.46	0.40	0.04	7	597.11	1.81	0.25	0.00
7	515.11	1.76	0.23	0.00	7	598.11	1.78	0.27	0.00
7	517.11	1.77	0.25	0.00	7	599.11	1.78	0.27	0.00
7	518.11	1.63	0.68	0.03	7	600.11	1.74	0.24	0.00
7	519.11	1.76	0.24	0.00	7	601.11	1.78	0.25	0.00
7	520.11	1.55	0.28	0.05	7	603.11	1.80	0.28	0.00
7	524.11	1.91	0.16	0.00	7	604.11	1.79	0.30	0.00
7	525.11	1.86	0.14	0.00	7	605.11	2.02	0.07	0.00
7	533.11	1.49	0.58	0.00	7	608.11	2.04	0.08	0.00
7	534.11	1.53	0.67	0.00	7	609.11	2.04	0.17	0.02
7	535.11	1.76	0.35	0.00	7	610.11	2.05	0.14	0.02
7	537.11	1.70	0.37	0.00	7	611.11	1.70	0.20	0.02
7	538.11	1.70	0.36	0.00	7	612.11	1.60	0.39	0.00
7	539.11	1.76	0.27	0.00	7	613.11	1.79	0.30	0.00
7	542.11	1.91	0.16	0.00	7	614.11	1.92	0.25	0.02
7	543.11	1.96	0.37	0.08	7	615.11	2.05	0.05	0.00
7	544.11	1.60	0.46	0.00	7	616.11	1.84	0.08	0.03
7	545.11	1.68	0.47	0.01	7	617.11	2.17	0.04	0.01
7	546.11	1.61	0.50	0.00	7	618.11	2.17	0.02	0.00
7	555.11	1.85	0.00	0.23	7	621.11	2.00	0.15	0.01
7	556.11	2.16	0.17	0.08	7	622.11	1.90	0.15	0.00
7	559.11	1.78	0.01	0.16	7	626.11	2.15	0.05	0.01
7	561.11	1.95	0.36	0.07	7	627.11	2.06	0.07	0.00
7	563.11	2.02	0.12	0.01	7	631.11	2.17	0.02	0.00
7	564.11	1.57	0.22	0.07	7	632.11	2.04	0.01	0.02

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	634.11	1.82	0.25	0.00	7	545.12	1.69	0.40	0.00
7	635.11	2.06	0.12	0.01	7	546.12	1.77	0.34	0.00
7	636.11	1.86	0.04	0.05	7	559.12	1.65	0.21	0.03
7	637.11	2.08	0.00	0.03	7	566.12	1.83	0.23	0.00
7	639.11	1.79	0.86	0.18	7	567.12	1.81	0.23	0.00
7	640.11	1.83	1.33	0.48	7	571.12	1.81	0.59	0.08
7	641.11	2.06	0.06	0.00	7	573.12	1.55	0.51	0.00
7	642.11	2.45	0.50	0.75	7	574.12	1.51	0.55	0.00
7	643.11	1.04	0.89	0.10	7	575.12	1.55	0.49	0.00
7	647.11	1.18	1.61	0.03	7	576.12	1.55	0.51	0.00
7	648.11	0.83	1.59	0.04	7	577.12	1.55	0.53	0.00
7	649.11	1.03	1.77	0.00	7	578.12	1.55	0.47	0.00
7	651.11	1.90	1.44	0.66	7	579.12	1.55	0.50	0.00
7	657.11	0.94	0.76	0.23	7	580.12	1.55	0.49	0.00
7	659.11	1.29	1.81	0.12	7	583.12	1.29	0.81	0.01
7	661.11	0.86	0.55	0.47	7	584.12	1.46	0.99	0.03
7	662.11	1.55	0.67	0.01	7	585.12	1.45	0.73	0.00
7	663.11	1.41	1.56	0.14	7	586.12	1.55	0.70	0.01
7	664.11	1.12	0.08	2.10	7	588.12	1.09	0.43	0.29
7	672.11	2.42	0.00	0.03	7	592.12	1.72	0.23	0.01
7	674.11	1.76	0.01	0.41	7	593.12	1.51	0.21	0.11
7	675.11	2.10	0.04	0.16	7	594.12	1.72	0.51	0.02
7	679.11	1.57	0.40	0.01	7	595.12	1.50	0.32	0.05
7	680.11	1.59	0.48	0.00	7	596.12	1.94	0.16	0.00
7	681.11	2.45	0.07	0.01	7	597.12	1.34	0.32	0.15
7	443.12	1.92	0.33	0.04	7	598.12	1.75	0.32	0.00
7	444.12	1.04	0.26	0.55	7	599.12	1.61	0.36	0.01
7	457.12	1.78	0.28	0.00	7	600.12	1.94	0.17	0.00
7	465.12	1.63	0.58	0.01	7	601.12	1.71	0.26	0.00
7	470.12	1.57	0.98	0.07	7	603.12	1.81	0.22	0.00
7	485.12	1.36	0.98	0.00	7	604.12	1.71	0.52	0.02
7	489.12	1.50	0.48	0.01	7	605.12	1.94	0.15	0.00
7	491.12	1.26	1.11	0.00	7	608.12	1.98	0.23	0.03
7	493.12	1.40	0.89	0.00	7	609.12	1.72	0.57	0.03
7	494.12	1.34	0.84	0.00	7	610.12	1.94	0.12	0.00
7	499.12	1.35	1.20	0.02	7	611.12	2.21	0.12	0.07
7	500.12	1.54	0.83	0.03	7	612.12	2.24	0.00	0.00
7	505.12	1.36	0.98	0.00	7	613.12	1.85	0.00	0.21
7	506.12	1.30	0.95	0.00	7	614.12	2.32	0.00	0.01
7	509.12	1.22	1.03	0.00	7	615.12	1.83	0.12	0.01
7	511.12	1.28	1.01	0.00	7	616.12	1.94	0.13	0.00
7	512.12	1.28	0.94	0.00	7	617.12	1.70	0.86	0.12
7	513.12	1.29	0.53	0.07	7	618.12	2.02	0.53	0.21
7	518.12	1.31	1.19	0.01	7	626.12	1.47	0.80	0.01
7	524.12	1.75	0.27	0.00	7	627.12	1.74	0.67	0.07
7	525.12	1.56	0.29	0.04	7	631.12	1.83	0.21	0.00
7	533.12	.			7	632.12	2.09	0.23	0.08
7	534.12	3.33	1.21	0.00	7	634.12	1.99	0.07	0.00
7	542.12	1.75	0.30	0.00	7	635.12	1.47	1.08	0.05
7	544.12	1.98	0.30	0.06	7	636.12	1.18	1.21	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
7	637.12	1.19	1.20	0.00	7	609.13	1.27	0.32	0.21
7	639.12	2.19	1.85	1.60	7	610.13	1.89	0.20	0.00
7	647.12	0.80	1.50	0.07	7	611.13	1.87	0.19	0.00
7	648.12	1.16	1.27	0.00	7	612.13	1.80	1.02	0.27
7	649.12	1.12	1.28	0.00	7	614.13	1.80	0.25	0.00
7	657.12	1.06	0.56	0.23	7	615.13	1.74	0.23	0.00
7	659.12	1.36	1.74	0.15	7	616.13	1.88	0.17	0.00
7	661.12	.			7	631.13	1.20	1.17	0.00
7	662.12	3.83	2.66	0.01	7	632.13	1.21	1.16	0.00
7	663.12	0.93	1.59	0.01	7	636.13	1.14	1.23	0.00
7	674.12	2.34	0.00	0.00	7	637.13	1.18	1.21	0.00
7	675.12	2.18	0.01	0.05	7	639.13	1.96	2.18	1.32
7	679.12	1.58	0.48	0.00	7	647.13	0.70	1.63	0.10
7	680.12	1.21	0.91	0.02	7	659.13	0.88	1.68	0.01
7	681.12	1.19	0.00	1.32	7	663.13	0.95	1.81	0.00
7	512.13	1.33	1.06	0.01	7	664.13	1.05	0.03	1.14
7	518.13	1.00	1.24	0.03	7	679.13	1.48	0.67	0.00
7	524.13	1.48	0.66	0.00	7	680.13	1.90	0.14	0.00
7	525.13	1.21	0.66	0.07	7	681.13	1.19	0.04	0.82
7	542.13	1.52	0.71	0.00	8	1	1.04	2.47	0.10
7	544.13	1.50	0.45	0.01	8	2	0.86	1.12	0.14
7	545.13	1.62	0.46	0.00	8	3	1.33	1.09	0.01
7	546.13	1.59	0.37	0.01	8	4	1.34	1.18	0.02
7	559.13	1.67	0.37	0.00	8	5	1.30	1.18	0.01
7	566.13	1.67	0.32	0.00	8	6	1.30	0.99	0.00
7	567.13	1.73	0.25	0.00	8	7	1.38	1.00	0.01
7	571.13	1.73	0.48	0.02	8	8	1.34	1.01	0.00
7	573.13	1.43	0.64	0.00	8	9	1.33	1.00	0.00
7	574.13	1.63	0.52	0.00	8	10	1.33	0.97	0.00
7	575.13	1.51	0.64	0.00	8	11	1.34	1.08	0.01
7	576.13	1.54	0.55	0.00	8	12	1.29	1.30	0.02
7	577.13	1.61	0.56	0.00	8	13	1.24	1.33	0.01
7	578.13	1.74	0.51	0.03	8	15	1.20	1.14	0.00
7	579.13	1.55	0.62	0.00	8	17	1.32	1.44	0.05
7	580.13	1.50	0.62	0.00	8	18	1.16	1.46	0.01
7	585.13	1.40	0.70	0.00	8	19	1.10	1.54	0.00
7	586.13	1.36	0.65	0.02	8	20	1.06	1.77	0.01
7	588.13	1.77	0.35	0.00	8	21	1.06	1.66	0.00
7	592.13	1.77	0.16	0.02	8	22	1.06	1.75	0.01
7	593.13	1.62	0.15	0.08	8	23	0.96	1.77	0.00
7	594.13	1.85	0.30	0.01	8	24	1.03	1.78	0.01
7	595.13	1.93	0.13	0.00	8	25	1.03	1.84	0.01
7	597.13	2.35	0.12	0.16	8	26	0.97	1.95	0.01
7	598.13	1.88	0.18	0.00	8	27	0.96	1.95	0.00
7	599.13	1.85	0.19	0.00	8	28	0.89	1.94	0.00
7	600.13	1.82	0.95	0.26	8	29	0.89	1.97	0.00
7	601.13	1.67	0.19	0.04	8	30	0.96	1.97	0.01
7	603.13	1.89	0.17	0.00	8	31	1.00	1.91	0.01
7	604.13	1.87	0.24	0.00	8	32	0.94	1.90	0.00
7	605.13	1.87	0.16	0.00	8	33	0.94	1.90	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	34	0.91	1.93	0.00	8	84	1.30	1.03	0.00
8	35	0.99	1.84	0.00	8	85	1.33	1.11	0.01
8	36	1.05	1.81	0.01	8	86	1.24	1.14	0.00
8	37	1.02	1.79	0.00	8	87	1.24	1.19	0.00
8	38	0.95	1.83	0.00	8	88	1.28	1.29	0.02
8	39	1.07	1.81	0.02	8	89	1.15	1.28	0.00
8	40	0.95	1.82	0.00	8	90	1.15	1.32	0.00
8	41	0.99	1.77	0.00	8	91	1.21	1.36	0.01
8	42	1.02	0.89	0.10	8	93	1.13	1.16	0.01
8	43	1.42	0.85	0.00	8	94	1.21	1.15	0.00
8	44	1.37	0.92	0.00	8	95	1.21	1.21	0.00
8	45	1.35	0.91	0.00	8	96	1.23	1.21	0.00
8	46	1.34	0.89	0.00	8	97	1.28	1.28	0.01
8	47	1.34	0.92	0.00	8	98	1.25	1.35	0.02
8	48	1.42	0.93	0.01	8	99	1.18	1.34	0.00
8	49	1.40	0.92	0.00	8	100	1.18	1.24	0.00
8	50	1.36	0.93	0.00	8	101	1.27	1.26	0.01
8	51	1.41	1.01	0.01	8	102	1.16	1.30	0.00
8	52	1.36	1.01	0.01	8	103	1.21	1.39	0.01
8	53	1.28	1.01	0.00	8	104	1.16	1.43	0.00
8	54	1.37	1.00	0.01	8	105	1.09	1.51	0.00
8	55	1.32	0.99	0.00	8	106	1.09	1.55	0.00
8	56	1.29	1.03	0.00	8	107	1.15	1.45	0.00
8	57	1.36	0.99	0.00	8	109	1.18	1.37	0.00
8	58	1.32	1.04	0.00	8	110	1.12	1.37	0.00
8	59	1.31	0.94	0.00	8	111	1.12	1.40	0.00
8	60	1.40	0.99	0.01	8	112	1.09	1.43	0.00
8	61	1.32	1.00	0.00	8	113	1.10	1.44	0.00
8	62	1.27	1.05	0.00	8	114	1.14	1.48	0.00
8	63	1.33	1.12	0.01	8	115	1.07	1.53	0.00
8	64	1.23	1.03	0.00	8	116	1.17	1.44	0.01
8	65	1.32	1.03	0.00	8	117	1.14	1.39	0.00
8	66	1.27	1.08	0.00	8	118	1.16	1.28	0.00
8	67	1.30	1.10	0.00	8	119	1.16	1.29	0.00
8	68	1.24	1.09	0.00	8	120	1.16	1.35	0.00
8	69	1.28	1.19	0.01	8	121	1.16	1.38	0.00
8	70	1.29	1.11	0.00	8	122	1.15	1.44	0.00
8	71	1.24	1.16	0.00	8	123	1.19	1.34	0.00
8	72	1.21	1.18	0.00	8	124	1.23	1.27	0.00
8	73	1.29	1.15	0.01	8	125	1.16	1.26	0.00
8	74	1.23	1.24	0.00	8	126	1.16	1.27	0.00
8	75	1.23	1.20	0.00	8	127	1.25	1.28	0.01
8	76	1.20	1.22	0.00	8	128	1.16	1.30	0.00
8	77	1.24	1.25	0.00	8	129	1.15	1.37	0.00
8	78	1.17	1.31	0.00	8	130	1.19	1.22	0.00
8	79	1.26	1.30	0.01	8	131	1.18	1.20	0.00
8	80	1.20	1.28	0.00	8	132	1.18	1.23	0.00
8	81	1.14	1.34	0.00	8	133	1.23	1.25	0.00
8	82	1.22	1.27	0.00	8	134	1.21	1.17	0.00
8	83	1.26	0.98	0.00	8	135	1.21	1.25	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	136	1.29	1.21	0.01	8	186	1.26	1.21	0.01
8	137	1.26	1.15	0.00	8	187	1.19	1.26	0.00
8	138	1.22	1.19	0.00	8	188	1.22	1.21	0.00
8	139	1.22	1.24	0.00	8	189	1.26	1.25	0.01
8	140	1.31	1.24	0.02	8	190	1.20	1.20	0.00
8	141	1.13	1.34	0.00	8	191	1.14	1.26	0.00
8	142	1.13	1.26	0.00	8	192	1.25	1.25	0.01
8	143	1.23	1.27	0.00	8	193	1.22	1.27	0.00
8	144	1.25	1.17	0.00	8	194	1.16	1.28	0.00
8	145	1.21	1.19	0.00	8	195	1.24	1.28	0.01
8	146	1.21	1.22	0.00	8	196	1.23	1.31	0.01
8	147	1.26	1.28	0.01	8	197	1.19	1.34	0.00
8	148	1.16	1.30	0.00	8	198	1.18	1.35	0.00
8	149	1.19	1.31	0.00	8	199	1.13	1.41	0.00
8	150	1.15	1.33	0.00	8	200	1.20	1.41	0.01
8	151	1.19	1.29	0.00	8	201	1.13	1.39	0.00
8	152	1.15	1.34	0.00	8	202	1.11	1.43	0.00
8	153	1.15	1.33	0.00	8	203	1.19	1.39	0.01
8	154	1.19	1.34	0.00	8	204	1.16	1.26	0.00
8	155	1.13	1.32	0.00	8	205	1.24	1.23	0.00
8	156	1.18	1.04	0.01	8	206	1.18	1.27	0.00
8	157	1.27	1.05	0.00	8	207	1.23	1.15	0.00
8	158	1.27	1.09	0.00	8	208	1.22	0.98	0.01
8	159	1.36	1.06	0.01	8	209	1.16	1.06	0.01
8	160	1.26	1.08	0.00	8	210	1.33	0.97	0.00
8	161	1.26	1.11	0.00	8	211	1.30	1.01	0.00
8	162	1.25	1.12	0.00	8	212	1.30	0.97	0.00
8	163	1.23	1.15	0.00	8	213	1.30	1.01	0.00
8	164	1.32	1.16	0.01	8	214	1.30	1.03	0.00
8	165	1.21	1.21	0.00	8	215	1.30	1.06	0.00
8	166	1.21	1.24	0.00	8	216	1.33	1.09	0.01
8	167	1.24	1.26	0.01	8	217	1.23	1.11	0.00
8	168	1.19	1.20	0.00	8	218	1.22	1.11	0.00
8	169	1.20	1.20	0.00	8	219	1.24	1.15	0.00
8	170	1.19	1.25	0.00	8	220	1.31	1.23	0.02
8	171	1.17	1.32	0.00	8	221	1.14	1.24	0.00
8	172	1.22	1.34	0.01	8	222	1.25	1.21	0.00
8	173	1.17	1.25	0.00	8	223	1.26	1.14	0.00
8	174	1.17	1.20	0.00	8	224	1.22	1.19	0.00
8	175	1.17	1.24	0.00	8	225	1.20	1.18	0.00
8	176	1.25	1.20	0.00	8	226	1.28	1.09	0.00
8	177	1.19	1.23	0.00	8	227	1.13	1.06	0.02
8	178	1.19	1.21	0.00	8	228	1.29	1.02	0.00
8	179	1.19	1.19	0.00	8	229	1.28	1.06	0.00
8	180	1.19	1.20	0.00	8	230	1.28	1.09	0.00
8	181	1.15	1.22	0.00	8	231	1.28	1.12	0.00
8	182	1.29	1.23	0.01	8	232	1.20	1.15	0.00
8	183	1.18	1.26	0.00	8	233	1.16	1.15	0.00
8	184	1.24	1.26	0.00	8	234	1.21	1.16	0.00
8	185	1.25	1.24	0.00	8	235	1.20	1.18	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	237	1.19	1.24	0.00	8	63.01	1.16	1.32	0.00
8	238	1.17	1.96	0.08	8	64.01	1.14	1.34	0.00
8	239	0.86	2.15	0.00	8	65.01	1.14	1.43	0.00
8	240	0.82	2.19	0.00	8	66.01	1.13	1.46	0.00
8	241	0.75	1.50	0.10	8	67.01	1.08	1.40	0.00
8	243	0.97	2.29	0.04	8	68.01	1.08	1.42	0.00
8	244	0.71	2.23	0.01	8	69.01	1.14	1.12	0.01
8	245	0.72	1.99	0.02	8	70.01	1.23	1.09	0.00
8	248	0.76	0.69	0.49	8	71.01	1.23	1.09	0.00
8	17.01	1.08	1.70	0.01	8	72.01	1.32	1.07	0.00
8	18.01	1.06	2.07	0.04	8	73.01	1.34	1.13	0.01
8	19.01	0.94	2.21	0.02	8	74.01	1.27	1.11	0.00
8	20.01	0.90	2.52	0.04	8	75.01	1.25	1.08	0.00
8	23.01	0.73	1.90	0.03	8	76.01	1.25	1.08	0.00
8	25.01	0.94	1.69	0.00	8	77.01	1.28	1.06	0.00
8	26.01	0.99	1.54	0.00	8	78.01	1.26	1.05	0.00
8	27.01	1.05	0.80	0.12	8	79.01	1.26	1.01	0.00
8	28.01	1.42	0.84	0.00	8	80.01	1.30	0.97	0.00
8	29.01	1.42	0.81	0.00	8	81.01	1.28	0.94	0.00
8	30.01	1.41	0.83	0.00	8	82.01	1.32	0.91	0.00
8	31.01	1.45	0.85	0.01	8	83.01	1.40	0.90	0.00
8	32.01	1.44	0.83	0.00	8	84.01	1.34	0.88	0.00
8	33.01	1.45	0.83	0.01	8	85.01	1.37	0.85	0.00
8	34.01	1.38	0.82	0.00	8	86.01	1.37	0.82	0.00
8	35.01	1.42	0.90	0.01	8	87.01	1.37	0.78	0.00
8	36.01	1.34	0.91	0.00	8	88.01	1.40	0.74	0.00
8	37.01	1.34	0.93	0.00	8	89.01	1.43	0.79	0.00
8	39.01	1.42	0.81	0.00	8	90.01	1.44	0.82	0.00
8	40.01	1.47	0.84	0.01	8	91.01	1.39	0.80	0.00
8	42.01	1.45	0.68	0.00	8	93.01	1.39	0.86	0.00
8	43.01	1.53	0.63	0.00	8	94.01	1.39	0.86	0.00
8	44.01	1.49	0.60	0.00	8	95.01	1.42	0.89	0.01
8	45.01	1.49	0.60	0.00	8	96.01	1.34	0.86	0.00
8	46.01	1.49	0.62	0.00	8	97.01	1.34	0.83	0.00
8	47.01	1.49	0.63	0.00	8	98.01	1.42	0.78	0.00
8	48.01	1.56	0.73	0.02	8	99.01	1.40	0.76	0.00
8	49.01	1.47	0.96	0.03	8	100.01	1.38	0.82	0.00
8	50.01	1.34	1.30	0.04	8	101.01	1.38	0.80	0.00
8	51.01	1.17	1.21	0.00	8	102.01	1.40	0.80	0.00
8	52.01	1.27	1.18	0.01	8	103.01	1.40	0.73	0.00
8	53.01	1.20	1.14	0.00	8	104.01	1.43	0.69	0.00
8	54.01	1.20	1.15	0.00	8	105.01	1.43	0.65	0.00
8	55.01	1.24	1.15	0.00	8	106.01	1.43	0.66	0.00
8	56.01	1.22	1.14	0.00	8	107.01	1.46	0.68	0.00
8	57.01	1.30	1.24	0.01	8	109.01	1.47	0.62	0.00
8	58.01	1.26	1.23	0.01	8	110.01	1.50	0.60	0.00
8	59.01	1.27	1.23	0.01	8	111.01	1.50	0.61	0.00
8	60.01	1.27	1.22	0.01	8	112.01	1.50	0.63	0.00
8	61.01	1.22	1.32	0.01	8	113.01	1.50	0.63	0.00
8	62.01	1.18	1.41	0.01	8	114.01	1.51	0.62	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	115.01	1.50	0.62	0.00	8	165.01	1.55	0.58	0.00
8	116.01	1.56	0.61	0.00	8	166.01	1.55	0.56	0.00
8	117.01	1.51	0.59	0.00	8	167.01	1.54	0.57	0.00
8	118.01	1.52	0.59	0.00	8	168.01	1.53	0.50	0.00
8	119.01	1.52	0.59	0.00	8	169.01	1.53	0.53	0.00
8	120.01	1.52	0.59	0.00	8	170.01	1.49	0.53	0.00
8	121.01	1.52	0.57	0.00	8	171.01	1.56	0.51	0.00
8	122.01	1.53	0.65	0.00	8	172.01	1.56	0.54	0.00
8	123.01	1.47	0.65	0.00	8	173.01	1.56	0.56	0.00
8	124.01	1.49	0.66	0.00	8	174.01	1.56	0.59	0.00
8	125.01	1.49	0.66	0.00	8	175.01	1.56	0.58	0.00
8	126.01	1.49	0.65	0.00	8	176.01	1.56	0.59	0.00
8	127.01	1.47	0.66	0.00	8	177.01	1.56	0.59	0.00
8	128.01	1.48	0.65	0.00	8	178.01	1.56	0.64	0.01
8	129.01	1.45	0.62	0.00	8	179.01	1.56	0.66	0.01
8	130.01	1.50	0.59	0.00	8	180.01	1.56	0.64	0.00
8	131.01	1.50	0.61	0.00	8	181.01	1.56	0.65	0.01
8	132.01	1.50	0.59	0.00	8	182.01	1.48	0.64	0.00
8	133.01	1.50	0.55	0.00	8	183.01	1.48	0.64	0.00
8	134.01	1.46	0.62	0.00	8	184.01	1.48	0.65	0.00
8	135.01	1.50	0.58	0.00	8	185.01	1.48	0.64	0.00
8	136.01	1.50	0.59	0.00	8	186.01	1.48	0.63	0.00
8	137.01	1.55	0.60	0.00	8	187.01	1.48	0.63	0.00
8	138.01	1.52	0.59	0.00	8	188.01	1.49	0.62	0.00
8	139.01	1.52	0.55	0.00	8	189.01	1.55	0.59	0.00
8	140.01	1.52	0.54	0.00	8	190.01	1.52	0.62	0.00
8	141.01	1.53	0.49	0.00	8	191.01	1.58	0.59	0.00
8	142.01	1.59	0.53	0.00	8	192.01	1.52	0.59	0.00
8	143.01	1.59	0.51	0.00	8	193.01	1.52	0.59	0.00
8	144.01	1.65	0.50	0.00	8	194.01	1.52	0.61	0.00
8	145.01	1.59	0.51	0.00	8	195.01	1.52	0.60	0.00
8	146.01	1.59	0.48	0.00	8	196.01	1.52	0.58	0.00
8	147.01	1.59	0.46	0.00	8	197.01	1.47	0.56	0.01
8	148.01	1.59	0.50	0.00	8	198.01	1.48	0.57	0.00
8	149.01	1.59	0.50	0.00	8	199.01	1.53	0.53	0.00
8	150.01	1.59	0.52	0.00	8	200.01	1.49	0.52	0.01
8	151.01	1.59	0.48	0.00	8	201.01	1.57	0.55	0.00
8	152.01	1.59	0.49	0.00	8	202.01	1.57	0.55	0.00
8	153.01	1.59	0.48	0.00	8	203.01	1.57	0.59	0.00
8	154.01	1.59	0.48	0.00	8	204.01	1.57	0.59	0.00
8	155.01	1.59	0.47	0.00	8	205.01	1.57	0.61	0.00
8	156.01	1.59	0.52	0.00	8	206.01	1.53	0.61	0.00
8	157.01	1.59	0.55	0.00	8	207.01	1.51	0.60	0.00
8	158.01	1.59	0.54	0.00	8	208.01	1.51	0.58	0.00
8	159.01	1.64	0.55	0.01	8	209.01	1.51	0.58	0.00
8	160.01	1.55	0.53	0.00	8	210.01	1.46	0.54	0.01
8	161.01	1.55	0.52	0.00	8	211.01	1.50	0.58	0.00
8	162.01	1.55	0.47	0.00	8	212.01	1.53	0.55	0.00
8	163.01	1.55	0.48	0.00	8	213.01	1.53	0.56	0.00
8	164.01	1.55	0.44	0.01	8	214.01	1.53	0.58	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	215.01	1.53	0.55	0.00	8	47.02	1.47	0.66	0.00
8	216.01	1.53	0.62	0.00	8	48.02	1.47	0.52	0.01
8	217.01	1.53	0.59	0.00	8	49.02	1.53	0.37	0.02
8	218.01	1.53	0.59	0.00	8	50.02	1.68	0.21	0.03
8	219.01	1.53	0.57	0.00	8	51.02	1.87	0.18	0.00
8	220.01	1.58	0.52	0.00	8	52.02	1.88	0.25	0.01
8	221.01	1.57	0.50	0.00	8	53.02	1.79	0.29	0.00
8	222.01	1.57	0.49	0.00	8	54.02	1.79	0.29	0.00
8	223.01	1.57	0.47	0.00	8	55.02	1.77	0.29	0.00
8	224.01	1.57	0.42	0.00	8	56.02	1.75	0.28	0.00
8	225.01	1.57	0.45	0.00	8	57.02	1.78	0.22	0.00
8	226.01	1.50	0.46	0.01	8	58.02	1.85	0.21	0.00
8	227.01	1.61	0.46	0.00	8	59.02	1.86	0.20	0.00
8	228.01	1.61	0.46	0.00	8	60.02	1.88	0.19	0.00
8	229.01	1.61	0.44	0.00	8	61.02	1.83	0.14	0.01
8	230.01	1.61	0.42	0.00	8	62.02	1.80	0.22	0.00
8	231.01	1.54	0.40	0.02	8	63.02	2.29	0.07	0.07
8	232.01	1.66	0.39	0.00	8	64.02	2.03	0.07	0.00
8	233.01	1.66	0.41	0.00	8	65.02	1.95	0.10	0.00
8	234.01	1.62	0.41	0.00	8	66.02	1.89	0.09	0.01
8	235.01	1.65	0.41	0.00	8	69.02	2.39	0.96	0.78
8	237.01	1.56	1.02	0.08	8	70.02	2.23	1.14	1.27
8	238.01	1.21	2.13	0.15	8	71.02	2.03	0.00	0.04
8	239.01	0.81	2.00	0.00	8	72.02	2.23	0.01	0.00
8	240.01	0.87	1.99	0.00	8	73.02	2.20	0.01	0.00
8	241.01	0.80	1.57	0.06	8	74.02	2.20	0.01	0.00
8	243.01	0.95	2.80	0.11	8	75.02	2.12	0.02	0.00
8	244.01	0.61	2.78	0.00	8	76.02	2.16	0.02	0.00
8	248.01	0.56	2.70	0.01	8	77.02	2.16	0.02	0.00
8	17.02	1.08	1.81	0.02	8	78.02	2.16	0.03	0.00
8	18.02	1.02	2.59	0.12	8	79.02	2.16	0.05	0.01
8	19.02	0.78	2.58	0.01	8	80.02	2.12	0.04	0.00
8	20.02	0.79	2.32	0.00	8	81.02	2.08	0.03	0.00
8	23.02	0.86	2.35	0.01	8	82.02	2.08	0.03	0.00
8	25.02	0.85	2.31	0.01	8	83.02	2.10	0.31	0.14
8	26.02	0.81	2.71	0.03	8	84.02	1.73	0.89	0.15
8	29.02	0.74	2.37	0.00	8	85.02	1.72	0.96	0.17
8	32.02	0.88	2.04	0.00	8	86.02	1.31	0.95	0.00
8	33.02	0.92	2.19	0.01	8	87.02	1.31	0.94	0.00
8	34.02	0.81	2.12	0.00	8	88.02	1.35	0.94	0.00
8	35.02	0.90	1.97	0.00	8	89.02	1.32	0.94	0.00
8	36.02	0.93	1.97	0.00	8	90.02	1.36	0.96	0.00
8	37.02	0.93	1.89	0.00	8	91.02	1.31	0.97	0.00
8	39.02	0.96	1.91	0.00	8	93.02	1.31	1.01	0.00
8	40.02	1.03	1.86	0.01	8	94.02	1.31	1.05	0.00
8	42.02	1.04	0.75	0.15	8	95.02	1.34	0.99	0.00
8	43.02	1.42	0.69	0.00	8	96.02	1.33	1.08	0.01
8	44.02	1.46	0.68	0.00	8	97.02	1.25	1.08	0.00
8	45.02	1.47	0.73	0.00	8	98.02	1.34	1.08	0.01
8	46.02	1.47	0.69	0.00	8	99.02	1.25	1.07	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	100.02	1.34	1.02	0.00	8	151.02	1.40	0.86	0.00
8	101.02	1.31	1.01	0.00	8	152.02	1.36	0.90	0.00
8	102.02	1.36	0.98	0.00	8	153.02	1.36	0.88	0.00
8	103.02	1.33	0.97	0.00	8	154.02	1.36	0.89	0.00
8	104.02	1.30	0.97	0.00	8	155.02	1.34	0.90	0.00
8	105.02	1.30	0.98	0.00	8	156.02	1.34	0.86	0.00
8	106.02	1.32	0.98	0.00	8	157.02	1.36	0.92	0.00
8	107.02	1.38	1.10	0.02	8	158.02	1.35	0.89	0.00
8	109.02	1.32	1.09	0.01	8	159.02	1.42	0.91	0.01
8	110.02	1.25	1.06	0.00	8	160.02	1.33	0.93	0.00
8	111.02	1.25	1.06	0.00	8	161.02	1.33	0.95	0.00
8	112.02	1.25	1.03	0.00	8	162.02	1.33	0.98	0.00
8	113.02	1.25	1.04	0.00	8	163.02	1.33	1.03	0.00
8	114.02	1.28	1.06	0.00	8	164.02	1.33	1.03	0.00
8	115.02	1.26	1.06	0.00	8	165.02	1.32	0.80	0.01
8	116.02	1.34	1.04	0.00	8	166.02	1.39	0.74	0.00
8	117.02	1.27	1.06	0.00	8	167.02	1.40	0.82	0.00
8	118.02	1.30	1.10	0.00	8	168.02	1.38	0.83	0.00
8	119.02	1.24	1.07	0.00	8	169.02	1.38	0.82	0.00
8	120.02	1.24	1.05	0.00	8	170.02	1.36	0.80	0.00
8	121.02	1.24	1.04	0.00	8	171.02	1.39	0.82	0.00
8	122.02	1.27	0.87	0.01	8	172.02	1.35	0.79	0.00
8	123.02	1.43	0.99	0.02	8	173.02	1.40	0.77	0.00
8	124.02	1.29	0.83	0.01	8	174.02	1.40	0.76	0.00
8	125.02	1.29	0.85	0.01	8	175.02	1.40	0.76	0.00
8	126.02	1.29	0.84	0.01	8	176.02	1.40	0.77	0.00
8	127.02	1.38	0.83	0.00	8	177.02	1.40	0.78	0.00
8	128.02	1.38	0.86	0.00	8	178.02	1.40	0.76	0.00
8	129.02	1.41	0.86	0.00	8	179.02	1.40	0.76	0.00
8	130.02	1.36	0.87	0.00	8	180.02	1.40	0.77	0.00
8	131.02	1.36	0.85	0.00	8	181.02	1.40	0.77	0.00
8	132.02	1.36	0.86	0.00	8	182.02	1.40	0.76	0.00
8	133.02	1.37	0.91	0.00	8	183.02	1.40	0.74	0.00
8	134.02	1.36	0.80	0.00	8	184.02	1.40	0.73	0.00
8	135.02	1.37	0.82	0.00	8	185.02	1.40	0.74	0.00
8	136.02	1.38	0.86	0.00	8	186.02	1.40	0.75	0.00
8	137.02	1.41	0.87	0.00	8	187.02	1.40	0.73	0.00
8	138.02	1.36	0.85	0.00	8	188.02	1.39	0.72	0.00
8	139.02	1.35	0.90	0.00	8	189.02	1.44	0.73	0.00
8	140.02	1.34	0.86	0.00	8	190.02	1.44	0.70	0.00
8	141.02	1.34	0.92	0.00	8	191.02	1.44	0.71	0.00
8	142.02	1.34	0.93	0.00	8	192.02	1.44	0.70	0.00
8	143.02	1.34	0.90	0.00	8	193.02	1.40	0.68	0.00
8	144.02	1.42	0.94	0.01	8	194.02	1.47	0.67	0.00
8	145.02	1.32	0.89	0.00	8	195.02	1.47	0.65	0.00
8	146.02	1.33	0.92	0.00	8	196.02	1.47	0.66	0.00
8	147.02	1.33	0.91	0.00	8	197.02	1.49	0.65	0.00
8	148.02	1.33	0.84	0.00	8	198.02	1.50	0.63	0.00
8	149.02	1.33	0.80	0.00	8	199.02	1.50	0.64	0.00
8	150.02	1.34	0.78	0.00	8	200.02	1.54	0.66	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	201.02	1.48	0.64	0.00	8	37.03	1.05	1.98	0.03
8	202.02	1.48	0.64	0.00	8	39.03	1.01	1.99	0.02
8	203.02	1.46	0.60	0.00	8	40.03	1.00	2.07	0.02
8	204.02	1.52	0.61	0.00	8	44.03	0.90	1.49	0.03
8	205.02	1.52	0.60	0.00	8	47.03	1.09	1.16	0.01
8	206.02	1.52	0.58	0.00	8	48.03	1.21	1.16	0.00
8	207.02	1.53	0.62	0.00	8	51.03	1.27	0.94	0.00
8	208.02	1.53	0.62	0.00	8	54.03	1.34	0.77	0.01
8	209.02	1.67	0.58	0.02	8	59.03	1.48	0.34	0.05
8	210.02	1.55	0.68	0.01	8	60.03	1.70	0.34	0.00
8	211.02	1.48	0.66	0.00	8	63.03	1.71	0.25	0.01
8	212.02	1.48	0.69	0.00	8	64.03	1.79	0.24	0.00
8	213.02	1.48	0.67	0.00	8	65.03	1.95	0.15	0.00
8	214.02	1.44	0.61	0.00	8	69.03	1.28	1.04	0.00
8	215.02	1.51	0.63	0.00	8	70.03	1.37	1.02	0.01
8	216.02	1.51	0.55	0.00	8	71.03	2.06	0.09	0.00
8	217.02	1.43	0.58	0.01	8	72.03	2.00	0.08	0.00
8	218.02	1.53	0.60	0.00	8	73.03	2.00	0.06	0.00
8	219.02	1.53	0.56	0.00	8	74.03	2.00	0.06	0.00
8	220.02	1.58	0.57	0.00	8	75.03	2.00	0.04	0.01
8	221.02	1.54	0.56	0.00	8	76.03	2.00	0.04	0.01
8	222.02	1.49	0.55	0.00	8	77.03	2.00	0.04	0.01
8	223.02	1.51	0.57	0.00	8	78.03	2.00	0.03	0.02
8	224.02	1.54	0.61	0.00	8	79.03	2.00	0.01	0.03
8	225.02	1.54	0.59	0.00	8	80.03	2.01	0.02	0.02
8	226.02	1.48	0.56	0.00	8	82.03	2.33	0.01	0.01
8	227.02	1.54	0.55	0.00	8	83.03	2.22	0.10	0.15
8	228.02	1.48	0.62	0.00	8	84.03	2.22	0.51	0.62
8	229.02	1.41	0.64	0.01	8	85.03	2.18	0.61	0.79
8	230.02	1.49	0.62	0.00	8	86.03	2.42	0.74	0.54
8	231.02	1.48	0.64	0.00	8	87.03	2.27	0.67	0.71
8	232.02	1.49	0.63	0.00	8	88.03	3.11	0.70	0.00
8	233.02	1.49	0.56	0.00	8	89.03	3.11	0.78	0.00
8	234.02	1.49	0.56	0.00	8	90.03	3.11	0.82	0.01
8	235.02	1.49	0.50	0.01	8	91.03	3.11	0.83	0.01
8	237.02	1.41	1.62	0.15	8	93.03	3.11	0.96	0.03
8	238.02	0.98	2.15	0.02	8	94.03	3.11	0.98	0.03
8	239.02	0.80	1.86	0.01	8	95.03	3.11	1.01	0.04
8	240.02	0.93	1.94	0.00	8	96.03	2.98	1.05	0.12
8	243.02	0.84	2.79	0.05	8	97.03	3.31	1.00	0.00
8	244.02	0.62	2.80	0.00	8	98.03	3.30	0.84	0.01
8	248.02	0.56	2.99	0.00	8	99.03	3.47	1.10	0.02
8	18.03	1.04	2.76	0.17	8	100.03	3.22	1.08	0.01
8	19.03	0.74	2.53	0.00	8	101.03	3.23	1.01	0.00
8	20.03	0.80	2.25	0.00	8	102.03	3.30	1.02	0.00
8	23.03	0.88	2.18	0.00	8	103.03	3.30	0.96	0.00
8	25.03	0.90	2.24	0.01	8	104.03	3.30	0.19	0.33
8	26.03	0.84	2.22	0.00	8	105.03	3.30	0.16	0.37
8	35.03	0.89	1.54	0.02	8	106.03	3.16	0.14	0.24
8	36.03	1.16	1.71	0.03	8	107.03	2.63	0.17	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	109.03	2.70	0.18	0.00	8	163.03	1.22	1.01	0.00
8	110.03	2.70	0.17	0.00	8	164.03	1.22	1.04	0.00
8	111.03	2.70	0.16	0.00	8	165.03	1.25	1.04	0.00
8	113.03	2.86	0.22	0.01	8	166.03	1.27	1.06	0.00
8	114.03	2.66	0.24	0.01	8	167.03	1.25	0.90	0.01
8	115.03	2.77	0.23	0.00	8	168.03	1.34	0.90	0.00
8	116.03	2.72	0.22	0.00	8	169.03	1.35	0.93	0.00
8	117.03	2.80	0.05	0.09	8	170.03	1.31	0.97	0.00
8	118.03	2.55	0.06	0.00	8	171.03	1.30	0.95	0.00
8	119.03	2.54	0.06	0.00	8	172.03	1.35	0.99	0.00
8	120.03	2.54	0.06	0.00	8	173.03	1.29	1.01	0.00
8	121.03	2.54	0.07	0.00	8	174.03	1.29	1.00	0.00
8	122.03	2.46	0.06	0.01	8	175.03	1.29	1.01	0.00
8	123.03	2.51	1.26	1.80	8	176.03	1.29	1.01	0.00
8	124.03	1.17	1.44	0.01	8	177.03	1.28	1.02	0.00
8	125.03	1.17	1.39	0.00	8	178.03	1.28	1.03	0.00
8	126.03	1.17	1.41	0.00	8	179.03	1.28	1.06	0.00
8	127.03	1.26	1.41	0.03	8	180.03	1.28	1.08	0.00
8	128.03	1.10	1.40	0.00	8	181.03	1.28	1.06	0.00
8	130.03	.			8	182.03	1.28	1.07	0.00
8	132.03	1.11	1.12	0.01	8	183.03	1.28	1.10	0.00
8	133.03	1.27	1.06	0.00	8	184.03	1.28	1.09	0.00
8	134.03	1.25	1.09	0.00	8	185.03	1.28	1.08	0.00
8	135.03	1.24	1.23	0.00	8	186.03	1.28	1.07	0.00
8	136.03	1.18	1.17	0.00	8	187.03	1.28	1.06	0.00
8	137.03	1.26	1.17	0.00	8	188.03	1.31	1.04	0.00
8	138.03	1.21	1.18	0.00	8	189.03	1.27	1.08	0.00
8	139.03	1.25	1.16	0.00	8	190.03	1.27	1.09	0.00
8	140.03	1.22	1.18	0.00	8	191.03	1.27	1.07	0.00
8	141.03	1.20	1.17	0.00	8	192.03	1.27	1.06	0.00
8	142.03	1.20	1.11	0.00	8	193.03	1.31	1.09	0.00
8	143.03	1.20	1.17	0.00	8	194.03	1.25	1.07	0.00
8	144.03	1.20	1.16	0.00	8	195.03	1.25	1.11	0.00
8	145.03	1.20	1.20	0.00	8	196.03	1.25	1.09	0.00
8	146.03	1.23	1.17	0.00	8	197.03	1.25	1.11	0.00
8	147.03	1.21	1.16	0.00	8	198.03	1.29	1.13	0.00
8	148.03	1.21	1.17	0.00	8	199.03	1.23	1.15	0.00
8	149.03	1.21	1.20	0.00	8	200.03	1.29	1.10	0.00
8	150.03	1.23	1.11	0.00	8	201.03	1.24	1.09	0.00
8	151.03	1.27	1.04	0.00	8	202.03	1.24	1.04	0.00
8	152.03	1.27	1.02	0.00	8	203.03	1.30	1.10	0.00
8	153.03	1.27	1.02	0.00	8	204.03	1.21	1.08	0.00
8	154.03	1.29	1.05	0.00	8	205.03	1.25	1.05	0.00
8	155.03	1.26	1.05	0.00	8	206.03	1.25	1.01	0.00
8	156.03	1.29	1.07	0.00	8	207.03	1.22	0.93	0.01
8	158.03	1.28	1.20	0.01	8	208.03	1.32	0.91	0.00
8	159.03	1.28	1.15	0.00	8	209.03	1.32	0.99	0.00
8	160.03	1.22	1.12	0.00	8	210.03	1.39	1.02	0.01
8	161.03	1.22	1.09	0.00	8	211.03	1.31	0.98	0.00
8	162.03	1.22	1.08	0.00	8	212.03	1.30	1.02	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	213.03	1.30	1.00	0.00	8	110.04	1.62	0.00	0.44
8	214.03	1.33	1.00	0.00	8	111.04	2.31	0.00	0.01
8	215.03	1.29	1.01	0.00	8	114.04	2.39	0.00	0.02
8	216.03	1.26	1.09	0.00	8	115.04	2.27	0.00	0.00
8	217.03	1.28	1.09	0.00	8	116.04	2.27	0.01	0.00
8	218.03	1.24	1.02	0.00	8	117.04	2.48	0.35	0.16
8	219.03	1.24	1.06	0.00	8	118.04	2.21	0.06	0.11
8	220.03	1.32	0.96	0.00	8	119.04	2.54	0.05	0.00
8	221.03	1.31	0.96	0.00	8	121.04	2.54	0.03	0.01
8	222.03	1.37	1.00	0.01	8	122.04	2.75	0.10	0.02
8	223.03	1.35	0.98	0.00	8	123.04	2.58	2.72	1.85
8	224.03	1.30	0.96	0.00	8	124.04	3.94	2.91	0.00
8	225.03	1.30	0.95	0.00	8	125.04	3.94	2.81	0.00
8	226.03	1.37	1.10	0.02	8	126.04	3.94	2.78	0.00
8	227.03	1.24	1.07	0.00	8	127.04	3.94	2.94	0.00
8	228.03	1.27	1.04	0.00	8	128.04	3.99	2.75	0.00
8	229.03	1.24	1.06	0.00	8	132.04	3.95	2.69	0.00
8	230.03	1.26	1.09	0.00	8	133.04	3.80	2.44	0.00
8	231.03	1.27	1.08	0.00	8	134.04	3.75	2.40	0.01
8	232.03	1.25	1.07	0.00	8	135.04	3.99	3.23	0.01
8	234.03	1.23	0.97	0.01	8	136.04	3.87	2.89	0.01
8	235.03	1.30	1.04	0.00	8	137.04	3.99	2.88	0.00
8	237.03	1.24	1.45	0.02	8	138.04	3.99	2.86	0.00
8	238.03	1.04	2.26	0.06	8	139.04	3.79	2.90	0.04
8	239.03	0.77	1.92	0.02	8	140.04	3.84	2.90	0.02
8	240.03	0.90	1.88	0.00	8	141.04	3.99	2.93	0.00
8	243.03	.			8	142.04	3.99	2.76	0.00
8	244.03	.			8	143.04	3.99	2.74	0.00
8	75.04	0.99	1.22	0.04	8	144.04	3.99	2.75	0.00
8	80.04	1.23	0.99	0.00	8	145.04	3.99	2.75	0.00
8	83.04	1.47	0.86	0.01	8	147.04	4.12	2.75	0.03
8	88.04	1.50	0.50	0.01	8	148.04	3.95	0.81	0.58
8	89.04	1.57	0.61	0.00	8	149.04	3.95	0.76	0.62
8	90.04	1.79	0.46	0.03	8	150.04	3.95	0.71	0.67
8	91.04	1.64	0.52	0.01	8	151.04	3.95	0.73	0.65
8	93.04	1.57	0.59	0.00	8	152.04	3.95	0.72	0.65
8	94.04	1.57	0.59	0.00	8	153.04	3.95	0.69	0.69
8	95.04	1.60	0.64	0.01	8	154.04	3.74	0.69	0.38
8	97.04	1.55	0.49	0.00	8	155.04	3.12	0.63	0.00
8	98.04	1.64	0.48	0.00	8	159.04	3.04	1.09	0.09
8	99.04	1.56	0.53	0.00	8	160.04	3.33	0.77	0.03
8	100.04	2.02	0.42	0.15	8	161.04	3.33	0.81	0.02
8	101.04	1.60	0.47	0.00	8	162.04	3.33	0.71	0.04
8	102.04	1.60	0.48	0.00	8	163.04	3.35	0.61	0.08
8	103.04	1.60	0.40	0.00	8	164.04	3.07	0.59	0.00
8	104.04	1.60	0.00	0.39	8	165.04	3.09	0.59	0.00
8	105.04	1.60	0.00	0.41	8	166.04	3.06	0.55	0.00
8	106.04	1.60	0.00	0.44	8	167.04	2.99	0.54	0.00
8	107.04	1.60	0.00	0.43	8	168.04	3.47	0.67	0.13
8	109.04	1.82	0.00	0.25	8	169.04	2.92	0.35	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	170.04	2.72	0.68	1.58	8	223.04	1.31	0.97	0.00
8	171.04	1.46	0.68	0.00	8	224.04	1.31	0.98	0.00
8	172.04	1.45	0.66	0.00	8	225.04	1.31	0.99	0.00
8	173.04	1.49	0.64	0.00	8	226.04	1.37	0.86	0.00
8	174.04	1.49	0.67	0.00	8	227.04	1.36	0.93	0.00
8	175.04	1.49	0.65	0.00	8	228.04	1.38	0.91	0.00
8	176.04	1.54	0.63	0.00	8	229.04	1.33	0.94	0.00
8	177.04	1.49	0.63	0.00	8	230.04	1.33	0.95	0.00
8	178.04	1.49	0.61	0.00	8	231.04	1.33	0.94	0.00
8	179.04	1.49	0.59	0.00	8	232.04	1.33	0.89	0.00
8	180.04	1.49	0.58	0.00	8	234.04	1.32	0.96	0.00
8	181.04	1.49	0.59	0.00	8	235.04	1.31	0.93	0.00
8	182.04	1.49	0.58	0.00	8	237.04	1.25	1.43	0.02
8	183.04	1.49	0.56	0.00	8	238.04	1.05	2.39	0.09
8	184.04	1.49	0.58	0.00	8	239.04	0.73	1.88	0.03
8	185.04	1.49	0.60	0.00	8	240.04	0.92	1.82	0.00
8	186.04	1.50	0.63	0.00	8	244.04	0.79	2.25	0.00
8	187.04	1.50	0.59	0.00	8	246.04	.		
8	188.04	1.52	0.68	0.00	8	251.04	0.67	2.16	0.02
8	189.04	1.46	0.64	0.00	8	253.04	0.75	2.91	0.03
8	190.04	1.46	0.62	0.00	8	254.04	0.53	2.84	0.01
8	191.04	1.46	0.63	0.00	8	123.05	1.07	0.67	0.16
8	192.04	1.46	0.62	0.00	8	124.05	1.47	0.69	0.00
8	193.04	1.49	0.70	0.00	8	125.05	1.47	0.66	0.00
8	194.04	1.45	0.72	0.00	8	127.05	1.60	0.70	0.02
8	195.04	1.46	1.10	0.05	8	132.05	1.45	0.73	0.00
8	196.04	1.24	1.08	0.00	8	133.05	1.65	0.44	0.00
8	197.04	1.24	1.09	0.00	8	134.05	1.48	0.69	0.00
8	198.04	1.24	1.08	0.00	8	135.05	1.82	0.40	0.03
8	199.04	1.25	1.05	0.00	8	136.05	1.51	0.72	0.00
8	200.04	1.33	1.10	0.01	8	139.05	1.59	0.66	0.01
8	201.04	1.24	1.09	0.00	8	140.05	1.52	0.70	0.00
8	202.04	1.24	1.11	0.00	8	141.05	1.45	0.71	0.00
8	203.04	1.30	1.07	0.00	8	142.05	1.45	0.71	0.00
8	204.04	1.29	1.07	0.00	8	143.05	1.46	0.68	0.00
8	205.04	1.27	1.08	0.00	8	144.05	1.50	0.72	0.00
8	206.04	1.23	1.09	0.00	8	145.05	1.44	0.67	0.00
8	207.04	1.29	1.13	0.00	8	147.05	1.44	0.60	0.01
8	210.04	1.30	1.03	0.00	8	148.05	1.44	0.00	0.71
8	211.04	1.27	1.04	0.00	8	151.05	1.42	0.01	0.91
8	212.04	1.27	1.06	0.00	8	152.05	1.64	0.02	0.62
8	213.04	1.27	1.03	0.00	8	154.05	1.42	0.27	0.12
8	214.04	1.27	1.06	0.00	8	155.05	1.84	0.04	0.42
8	215.04	1.27	1.06	0.00	8	159.05	1.47	0.01	0.55
8	216.04	1.30	1.05	0.00	8	160.05	2.25	0.00	0.00
8	217.04	1.29	1.01	0.00	8	161.05	2.27	0.00	0.00
8	218.04	1.29	1.03	0.00	8	162.05	2.27	0.00	0.00
8	219.04	1.29	1.04	0.00	8	163.05	2.26	0.00	0.00
8	220.04	1.36	1.08	0.01	8	164.05	2.29	0.00	0.00
8	222.04	1.32	0.99	0.00	8	165.05	2.24	0.00	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	166.05	2.30	0.00	0.00	8	220.05	1.43	0.81	0.00
8	167.05	2.29	0.00	0.00	8	222.05	1.45	0.75	0.00
8	168.05	2.23	0.00	0.00	8	223.05	1.42	0.76	0.00
8	169.05	2.31	0.05	0.04	8	224.05	1.42	0.76	0.00
8	170.05	2.31	2.70	2.63	8	225.05	1.42	0.75	0.00
8	171.05	2.31	2.74	2.66	8	226.05	1.48	0.73	0.00
8	172.05	2.26	2.74	2.82	8	227.05	1.44	0.75	0.00
8	173.05	3.74	2.74	0.04	8	228.05	1.45	0.76	0.00
8	174.05	3.94	2.65	0.00	8	229.05	1.42	0.74	0.00
8	176.05	3.92	2.50	0.00	8	230.05	1.42	0.77	0.00
8	177.05	4.18	3.08	0.02	8	231.05	1.42	0.78	0.00
8	178.05	4.04	3.02	0.00	8	232.05	1.38	0.90	0.00
8	179.05	3.98	2.85	0.00	8	234.05	1.33	0.84	0.00
8	181.05	4.12	3.09	0.01	8	235.05	1.35	0.95	0.00
8	182.05	4.05	3.12	0.00	8	237.05	1.25	1.59	0.05
8	183.05	4.05	3.13	0.00	8	238.05	0.99	2.21	0.03
8	184.05	4.05	3.16	0.00	8	239.05	0.74	1.80	0.04
8	185.05	4.08	3.17	0.00	8	240.05	0.86	1.85	0.01
8	186.05	3.90	3.24	0.04	8	247.05	0.80	2.11	0.00
8	187.05	4.09	3.18	0.00	8	253.05	0.72	2.65	0.00
8	188.05	3.87	3.33	0.06	8	254.05	0.38	2.69	0.07
8	189.05	4.11	3.31	0.00	8	132.06	1.08	1.78	0.01
8	190.05	4.11	3.30	0.00	8	139.06	1.03	1.70	0.00
8	191.05	4.11	3.33	0.00	8	140.06	1.09	1.67	0.01
8	192.05	4.11	3.23	0.00	8	141.06	1.00	1.66	0.00
8	193.05	3.90	1.41	0.18	8	142.06	1.00	1.65	0.00
8	194.05	3.48	1.37	0.00	8	143.06	1.06	1.69	0.00
8	195.05	3.33	1.84	0.10	8	144.06	1.10	1.58	0.00
8	196.05	3.65	1.77	0.00	8	145.06	1.03	1.62	0.00
8	197.05	3.65	1.82	0.00	8	147.06	1.08	1.79	0.02
8	198.05	3.65	1.91	0.00	8	148.06	0.97	1.83	0.00
8	199.05	3.46	1.84	0.04	8	151.06	0.83	2.13	0.00
8	200.05	3.65	1.79	0.00	8	152.06	0.96	2.13	0.02
8	201.05	3.65	0.88	0.17	8	159.06	0.95	1.47	0.02
8	202.05	3.65	0.85	0.19	8	160.06	1.17	1.35	0.00
8	203.05	3.65	0.89	0.17	8	161.06	1.13	1.38	0.00
8	204.05	3.65	0.88	0.18	8	162.06	1.13	1.36	0.00
8	205.05	3.65	0.83	0.20	8	163.06	1.15	1.24	0.00
8	206.05	3.42	0.78	0.06	8	164.06	1.18	1.31	0.00
8	207.05	3.14	0.73	0.00	8	165.06	1.17	1.39	0.00
8	210.05	3.05	0.78	0.02	8	166.06	1.11	1.31	0.00
8	211.05	3.18	0.03	0.51	8	170.06	1.16	0.79	0.06
8	212.05	3.18	0.78	3.12	8	171.06	1.40	0.81	0.00
8	213.05	3.18	0.88	3.33	8	172.06	1.43	0.79	0.00
8	214.05	3.18	0.85	3.30	8	173.06	1.42	0.78	0.00
8	215.05	1.37	0.86	0.00	8	174.06	1.41	0.77	0.00
8	216.05	1.37	0.81	0.00	8	176.06	1.41	0.75	0.00
8	217.05	1.37	0.82	0.00	8	177.06	1.41	0.79	0.00
8	218.05	1.37	0.79	0.00	8	178.06	1.41	0.77	0.00
8	219.05	1.37	0.83	0.00	8	179.06	1.40	0.82	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	181.06	1.60	0.68	0.02	8	235.06	2.96	0.14	1.08
8	182.06	1.42	0.74	0.00	8	237.06	1.80	1.48	0.53
8	183.06	1.43	0.74	0.00	8	239.06	1.03	1.88	0.01
8	184.06	1.43	0.77	0.00	8	240.06	0.85	1.83	0.01
8	185.06	1.49	0.74	0.00	8	247.06	0.85	2.26	0.00
8	186.06	1.43	0.73	0.00	8	253.06	0.67	2.84	0.00
8	187.06	1.43	0.74	0.00	8	254.06	0.55	2.94	0.00
8	188.06	1.44	0.72	0.00	8	147.07	1.03	1.28	0.02
8	189.06	1.44	0.71	0.00	8	148.07	1.17	1.27	0.00
8	190.06	1.44	0.72	0.00	8	159.07	1.26	1.70	0.07
8	191.06	1.44	0.77	0.00	8	162.07	1.13	1.41	0.00
8	192.06	1.44	0.76	0.00	8	164.07	1.16	1.16	0.00
8	193.06	1.44	0.04	0.41	8	171.07	1.22	0.82	0.03
8	194.06	1.42	0.03	0.46	8	172.07	1.43	0.83	0.00
8	195.06	2.10	0.03	0.00	8	182.07	1.41	0.39	0.06
8	196.06	2.11	0.03	0.00	8	183.07	1.67	0.45	0.00
8	197.06	2.11	0.03	0.00	8	184.07	1.63	0.45	0.00
8	198.06	2.11	0.04	0.00	8	186.07	1.67	0.91	0.11
8	199.06	2.06	0.04	0.00	8	187.07	1.36	0.95	0.00
8	200.06	2.09	0.03	0.00	8	191.07	1.34	0.53	0.05
8	201.06	2.09	0.05	0.17	8	192.07	1.61	0.51	0.00
8	202.06	2.09	0.04	0.16	8	193.07	1.61	0.57	0.01
8	203.06	2.09	0.04	0.15	8	194.07	1.54	0.55	0.00
8	204.06	2.09	0.04	0.15	8	197.07	1.58	0.38	0.01
8	205.06	2.09	0.05	0.17	8	198.07	1.71	0.36	0.00
8	206.06	2.09	0.06	0.20	8	204.07	1.72	0.24	0.01
8	207.06	2.06	0.08	0.26	8	206.07	1.86	0.18	0.00
8	210.06	2.53	0.11	0.01	8	207.07	1.71	0.37	0.00
8	211.06	2.62	1.07	0.50	8	210.07	2.29	0.15	0.15
8	212.06	3.35	4.61	1.18	8	211.07	1.75	0.37	0.01
8	213.06	4.47	4.63	0.00	8	212.07	1.90	0.30	0.03
8	214.06	4.19	4.45	0.04	8	213.07	1.73	0.40	0.00
8	215.06	4.40	4.57	0.00	8	214.07	1.70	0.41	0.00
8	216.06	4.40	4.66	0.00	8	215.07	1.65	0.43	0.00
8	217.06	4.40	4.62	0.00	8	216.07	1.68	0.59	0.02
8	218.06	4.40	4.57	0.00	8	217.07	1.55	0.69	0.01
8	219.06	4.40	4.58	0.00	8	218.07	1.46	0.75	0.00
8	220.06	4.20	4.01	0.01	8	219.07	1.45	1.49	0.14
8	222.06	4.31	3.81	0.00	8	220.07	0.89	1.88	0.00
8	223.06	4.26	3.62	0.00	8	222.07	1.49	1.18	0.08
8	224.06	4.19	3.61	0.00	8	223.07	1.15	1.54	0.01
8	225.06	4.19	3.63	0.00	8	224.07	1.05	1.52	0.00
8	226.06	4.20	3.51	0.00	8	225.07	1.05	1.51	0.00
8	227.06	4.16	3.30	0.00	8	226.07	1.14	1.72	0.03
8	228.06	3.94	1.64	0.13	8	227.07	0.98	1.56	0.00
8	229.06	3.54	1.67	0.00	8	228.07	1.03	0.56	0.26
8	230.06	3.62	1.65	0.00	8	229.07	1.49	0.65	0.00
8	231.06	3.58	1.56	0.00	8	231.07	1.47	2.26	0.47
8	232.06	3.30	1.30	0.02	8	232.07	0.79	2.07	0.00
8	234.06	3.46	0.65	0.13	8	237.07	0.83	1.62	0.04

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
8	239.07	0.98	1.69	0.00	8	227.09	1.03	1.57	0.00
8	240.07	0.99	1.72	0.00	8	228.09	1.08	1.42	0.00
8	247.07	0.90	1.99	0.00	8	229.09	1.09	2.42	0.13
8	253.07	0.80	0.52	0.59	8	237.09	0.72	1.74	0.06
8	254.07	1.34	0.59	0.03	8	239.09	0.94	1.73	0.00
8	257.07	.			8	240.09	0.90	1.76	0.00
8	258.07	.			8	253.09	0.88	2.92	0.09
8	171.08	0.99	2.71	0.12	8	254.09	0.48	2.82	0.02
8	172.08	0.74	2.74	0.01	9	10	1.04	2.49	0.11
8	182.08	0.74	2.66	0.01	9	11	0.71	2.49	0.00
8	183.08	0.76	2.60	0.01	9	12	0.77	2.43	0.00
8	184.08	0.77	2.56	0.01	9	13	0.73	2.44	0.00
8	193.08	0.74	1.77	0.05	9	14	0.77	2.46	0.00
8	194.08	0.98	1.80	0.00	9	16	0.82	2.29	0.00
8	197.08	0.97	1.80	0.00	9	18	0.87	2.13	0.00
8	198.08	1.01	1.89	0.01	9	19	0.91	2.13	0.01
8	204.08	0.98	1.58	0.00	9	20	0.83	2.12	0.00
8	207.08	1.09	1.90	0.03	9	26	0.87	1.68	0.02
8	211.08	0.99	1.87	0.00	9	27	0.99	1.85	0.00
8	212.08	0.93	1.84	0.00	9	30	1.37	1.30	0.05
8	214.08	0.98	1.48	0.01	9	31	1.03	1.59	0.00
8	215.08	1.07	1.52	0.00	9	35	1.06	1.49	0.00
8	216.08	1.12	2.01	0.06	9	36	1.07	1.48	0.00
8	217.08	0.93	1.94	0.00	9	37	1.17	1.48	0.01
8	218.08	0.91	1.86	0.00	9	38	1.07	1.50	0.00
8	219.08	0.98	2.21	0.03	9	39	1.10	1.52	0.00
8	220.08	0.99	1.82	0.00	9	40	0.93	1.62	0.01
8	222.08	0.91	1.99	0.00	9	41	1.31	1.45	0.05
8	223.08	1.03	1.70	0.00	9	42	1.09	1.49	0.00
8	224.08	0.99	1.69	0.00	9	46	1.11	1.34	0.00
8	225.08	0.99	1.63	0.00	9	47	1.13	1.32	0.00
8	226.08	1.08	1.43	0.00	9	48	1.00	1.50	0.00
8	227.08	1.10	1.40	0.00	9	49	1.57	1.42	0.23
8	228.08	1.09	1.38	0.00	9	50	1.19	1.52	0.02
8	229.08	1.11	1.93	0.04	9	51	1.11	1.58	0.01
8	231.08	0.89	2.71	0.06	9	52	1.09	1.55	0.00
8	232.08	0.66	2.46	0.00	9	53	1.05	1.54	0.00
8	237.08	0.71	1.70	0.08	9	54	1.05	1.53	0.00
8	239.08	0.95	2.08	0.01	9	55	1.05	1.55	0.00
8	240.08	0.80	2.10	0.00	9	57	1.10	1.49	0.00
8	247.08	.			9	59	1.08	1.40	0.00
8	253.08	0.76	2.99	0.04	9	60	1.10	1.40	0.00
8	254.08	0.51	2.79	0.01	9	61	1.10	1.41	0.00
8	182.09	1.04	2.44	0.10	9	65	1.21	1.20	0.00
8	183.09	0.73	2.42	0.00	9	66	1.29	1.21	0.01
8	184.09	0.73	2.40	0.00	9	67	1.28	1.18	0.01
8	207.09	0.79	1.84	0.02	9	68	1.21	1.17	0.00
8	219.09	0.99	2.35	0.06	9	69	1.21	1.16	0.00
8	220.09	0.87	1.92	0.00	9	70	1.21	1.17	0.00
8	226.09	1.01	1.58	0.00	9	71	1.27	1.13	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	72	1.23	1.15	0.00	9	125	1.22	1.16	0.00
9	73	1.19	1.28	0.00	9	126	1.32	1.19	0.01
9	74	1.40	1.12	0.03	9	127	1.20	1.18	0.00
9	75	1.23	1.12	0.00	9	128	1.20	1.20	0.00
9	77	1.26	1.16	0.00	9	129	1.20	1.17	0.00
9	78	1.25	1.17	0.00	9	130	1.02	1.22	0.03
9	80	1.25	1.10	0.00	9	131	1.42	1.10	0.03
9	81	1.24	1.12	0.00	9	133	1.29	1.08	0.00
9	82	1.24	1.13	0.00	9	134	1.24	1.12	0.00
9	83	1.31	1.13	0.01	9	135	1.23	1.10	0.00
9	84	1.26	1.11	0.00	9	136	1.23	1.11	0.00
9	85	1.22	1.11	0.00	9	137	1.23	1.10	0.00
9	86	1.33	1.17	0.01	9	138	1.20	1.10	0.00
9	87	1.21	1.18	0.00	9	139	1.24	1.10	0.00
9	88	1.21	1.19	0.00	9	140	1.23	1.16	0.00
9	89	1.19	1.20	0.00	9	141	1.18	1.18	0.00
9	90	1.22	1.21	0.00	9	142	1.30	1.19	0.01
9	91	1.22	1.22	0.00	9	143	1.18	1.06	0.01
9	93	1.20	1.12	0.00	9	144	1.26	1.01	0.00
9	94	1.28	1.12	0.00	9	145	1.26	1.05	0.00
9	95	1.33	1.11	0.01	9	146	1.26	1.07	0.00
9	96	1.24	1.09	0.00	9	147	1.31	1.08	0.00
9	97	1.24	1.11	0.00	9	148	1.25	1.10	0.00
9	98	1.24	1.15	0.00	9	149	1.25	1.09	0.00
9	99	1.24	1.13	0.00	9	150	1.25	1.11	0.00
9	100	1.24	1.15	0.00	9	151	1.23	1.05	0.00
9	101	1.24	1.16	0.00	9	152	1.26	1.07	0.00
9	102	1.24	1.17	0.00	9	153	1.26	1.10	0.00
9	103	1.24	1.21	0.00	9	154	1.26	1.09	0.00
9	104	1.24	1.21	0.00	9	155	1.26	1.12	0.00
9	105	1.23	1.25	0.00	9	156	1.47	1.17	0.07
9	106	1.17	1.25	0.00	9	157	1.21	1.20	0.00
9	107	1.24	1.20	0.00	9	158	1.17	1.24	0.00
9	108	1.19	1.21	0.00	9	159	1.27	1.24	0.01
9	109	1.19	1.23	0.00	9	160	1.25	1.24	0.00
9	110	1.02	1.24	0.02	9	161	1.25	1.21	0.00
9	111	1.35	1.13	0.01	9	162	1.16	1.24	0.00
9	112	1.23	1.21	0.00	9	163	1.17	1.28	0.00
9	113	1.19	1.18	0.00	9	164	1.17	1.32	0.00
9	114	1.28	1.19	0.01	9	165	1.14	1.33	0.00
9	115	1.30	1.19	0.01	9	166	1.17	1.25	0.00
9	116	1.20	1.21	0.00	9	167	1.17	1.24	0.00
9	117	1.24	1.20	0.00	9	168	1.18	1.25	0.00
9	118	1.19	1.22	0.00	9	169	1.17	1.27	0.00
9	119	1.19	1.24	0.00	9	170	1.09	1.30	0.00
9	120	1.28	1.24	0.01	9	171	1.29	1.25	0.01
9	121	1.18	1.23	0.00	9	172	1.14	1.29	0.00
9	122	1.21	1.19	0.00	9	173	1.24	1.26	0.01
9	123	1.20	1.21	0.00	9	174	1.14	1.26	0.00
9	124	1.23	1.14	0.00	9	175	1.23	1.19	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	176	1.20	1.21	0.00	9	226	1.20	1.21	0.00
9	177	1.19	1.24	0.00	9	227	1.20	1.20	0.00
9	178	1.19	1.25	0.00	9	228	1.20	1.23	0.00
9	179	1.18	1.28	0.00	9	229	1.20	1.25	0.00
9	180	1.21	1.23	0.00	9	230	1.20	1.27	0.00
9	181	1.18	1.21	0.00	9	231	1.20	1.29	0.00
9	182	1.18	1.21	0.00	9	232	1.20	1.29	0.00
9	183	1.18	1.22	0.00	9	233	1.15	1.31	0.00
9	184	1.18	1.23	0.00	9	234	1.19	1.34	0.00
9	185	1.18	1.25	0.00	9	235	1.18	1.31	0.00
9	186	1.18	1.28	0.00	9	236	1.19	1.28	0.00
9	187	1.17	1.28	0.00	9	237	1.16	1.31	0.00
9	188	1.16	1.24	0.00	9	238	1.16	1.28	0.00
9	189	1.18	1.22	0.00	9	239	1.16	1.30	0.00
9	190	1.18	1.22	0.00	9	240	1.15	1.28	0.00
9	191	1.18	1.22	0.00	9	241	1.25	1.31	0.01
9	192	1.23	1.18	0.00	9	242	1.24	1.25	0.00
9	193	1.20	1.20	0.00	9	243	1.22	1.27	0.00
9	194	1.20	1.22	0.00	9	244	1.16	1.29	0.00
9	195	1.20	1.18	0.00	9	245	1.14	1.28	0.00
9	196	1.20	1.21	0.00	9	246	1.16	1.27	0.00
9	197	1.20	1.24	0.00	9	247	1.16	1.30	0.00
9	198	1.18	1.27	0.00	9	248	1.16	1.32	0.00
9	199	1.12	1.27	0.00	9	249	1.16	1.35	0.00
9	200	1.16	1.29	0.00	9	250	1.14	1.34	0.00
9	201	1.15	1.30	0.00	9	251	1.08	1.37	0.00
9	202	1.15	1.30	0.00	9	252	1.12	1.39	0.00
9	203	1.16	1.27	0.00	9	253	1.14	1.37	0.00
9	204	1.16	1.29	0.00	9	254	1.12	1.38	0.00
9	205	1.15	1.30	0.00	9	255	1.11	1.40	0.00
9	206	1.15	1.29	0.00	9	256	0.97	1.43	0.02
9	207	1.16	1.28	0.00	9	257	1.21	1.35	0.01
9	208	1.16	1.20	0.00	9	258	1.08	1.38	0.00
9	209	1.19	1.21	0.00	9	259	1.15	1.37	0.00
9	210	1.19	1.23	0.00	9	260	1.12	1.38	0.00
9	211	1.19	1.22	0.00	9	261	0.91	1.35	0.05
9	212	1.19	1.22	0.00	9	262	1.13	1.36	0.00
9	213	1.18	1.23	0.00	9	263	1.26	1.17	0.00
9	214	1.18	1.24	0.00	9	264	1.01	1.34	0.02
9	215	1.18	1.27	0.00	9	265	1.13	1.32	0.00
9	216	1.23	1.31	0.01	9	266	1.13	1.35	0.00
9	217	1.14	1.30	0.00	9	267	1.13	1.39	0.00
9	218	1.14	1.30	0.00	9	268	1.13	1.35	0.00
9	219	1.16	1.31	0.00	9	269	1.12	1.37	0.00
9	220	1.21	1.31	0.00	9	270	1.12	1.38	0.00
9	221	1.15	1.32	0.00	9	271	1.16	1.40	0.00
9	222	1.15	1.33	0.00	9	272	1.11	1.41	0.00
9	223	1.14	1.34	0.00	9	273	1.15	1.41	0.00
9	224	1.22	1.19	0.00	9	274	1.10	1.41	0.00
9	225	1.20	1.19	0.00	9	275	1.15	1.46	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	276	1.12	1.43	0.00	9	326	1.17	1.33	0.00
9	277	1.17	1.36	0.00	9	327	1.17	1.33	0.00
9	278	1.14	1.29	0.00	9	328	1.17	1.24	0.00
9	279	1.23	1.10	0.00	9	329	1.17	1.27	0.00
9	280	1.24	1.12	0.00	9	330	1.17	1.30	0.00
9	281	1.24	1.16	0.00	9	331	1.17	1.31	0.00
9	282	1.22	1.19	0.00	9	332	1.20	1.29	0.00
9	283	1.25	1.19	0.00	9	333	1.15	1.28	0.00
9	284	1.20	1.20	0.00	9	334	1.19	1.27	0.00
9	285	1.20	1.15	0.00	9	335	1.16	1.28	0.00
9	286	1.20	1.19	0.00	9	336	1.16	1.30	0.00
9	287	1.20	1.19	0.00	9	337	1.19	1.31	0.00
9	288	1.19	1.17	0.00	9	338	1.15	1.26	0.00
9	289	1.21	1.19	0.00	9	339	1.20	1.29	0.00
9	290	1.28	1.21	0.01	9	340	1.17	1.30	0.00
9	291	1.19	1.23	0.00	9	341	1.15	1.34	0.00
9	292	1.19	1.23	0.00	9	342	1.15	1.30	0.00
9	293	1.20	1.22	0.00	9	343	1.13	1.18	0.00
9	294	1.18	1.23	0.00	9	344	1.20	1.21	0.00
9	295	1.18	1.21	0.00	9	345	1.20	1.20	0.00
9	296	1.23	1.21	0.00	9	346	1.20	1.23	0.00
9	297	1.19	1.20	0.00	9	347	1.05	1.24	0.02
9	298	1.19	1.22	0.00	9	348	1.03	1.41	0.00
9	299	1.21	1.21	0.00	9	349	0.66	1.79	0.08
9	300	1.21	1.24	0.00	9	350	0.95	1.72	0.00
9	301	1.18	1.23	0.00	9	351	1.50	0.31	0.06
9	302	1.18	1.22	0.00	9	352	1.11	0.34	0.35
9	303	1.18	1.24	0.00	9	353	1.55	1.44	0.21
9	304	1.18	1.28	0.00	9	51.01	1.07	1.47	0.00
9	305	1.18	1.28	0.00	9	52.01	1.08	1.50	0.00
9	306	1.16	1.29	0.00	9	53.01	1.08	1.49	0.00
9	307	1.16	1.31	0.00	9	59.01	1.11	1.17	0.01
9	308	1.23	1.31	0.01	9	60.01	1.21	1.19	0.00
9	309	1.14	1.32	0.00	9	65.01	1.26	1.07	0.00
9	310	1.14	1.34	0.00	9	66.01	1.26	1.05	0.00
9	311	1.14	1.33	0.00	9	67.01	1.26	1.09	0.00
9	312	1.14	1.36	0.00	9	70.01	1.30	0.95	0.00
9	313	1.13	1.28	0.00	9	71.01	1.31	1.22	0.02
9	314	1.14	1.24	0.00	9	72.01	1.18	1.20	0.00
9	315	1.17	1.27	0.00	9	73.01	1.22	1.10	0.00
9	316	1.21	1.29	0.00	9	75.01	1.20	1.14	0.00
9	317	1.15	1.29	0.00	9	77.01	1.22	1.05	0.00
9	318	1.15	1.28	0.00	9	78.01	1.22	1.03	0.00
9	319	1.15	1.28	0.00	9	80.01	1.22	1.02	0.00
9	320	1.15	1.25	0.00	9	81.01	1.22	0.97	0.01
9	321	1.24	1.25	0.00	9	82.01	1.22	0.97	0.01
9	322	1.17	1.27	0.00	9	84.01	1.28	0.85	0.01
9	323	1.17	1.29	0.00	9	85.01	1.39	0.84	0.00
9	324	1.17	1.30	0.00	9	86.01	1.40	0.78	0.00
9	325	1.17	1.36	0.00	9	87.01	1.40	0.75	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	93.01	1.46	0.32	0.07	9	149.01	1.67	0.45	0.00
9	94.01	1.74	0.31	0.00	9	150.01	1.67	0.44	0.00
9	95.01	1.73	0.26	0.00	9	151.01	1.67	0.46	0.00
9	96.01	1.75	0.29	0.00	9	152.01	1.67	0.44	0.00
9	97.01	1.75	0.26	0.00	9	153.01	1.67	0.41	0.00
9	98.01	1.80	0.24	0.00	9	154.01	1.67	0.41	0.00
9	99.01	1.80	0.27	0.00	9	155.01	1.67	0.41	0.00
9	100.01	1.80	0.25	0.00	9	156.01	1.67	0.40	0.00
9	101.01	1.80	0.25	0.00	9	157.01	1.67	0.39	0.00
9	102.01	1.80	0.26	0.00	9	158.01	1.67	0.38	0.00
9	103.01	1.80	0.25	0.00	9	159.01	1.67	0.37	0.00
9	104.01	1.80	0.24	0.00	9	160.01	1.67	0.37	0.00
9	105.01	1.74	0.24	0.00	9	161.01	1.67	0.35	0.00
9	106.01	1.80	0.25	0.00	9	162.01	1.68	0.36	0.00
9	109.01	1.85	0.13	0.00	9	163.01	1.72	0.34	0.00
9	110.01	1.87	0.18	0.00	9	164.01	1.71	0.31	0.00
9	111.01	1.91	0.13	0.00	9	165.01	1.71	0.32	0.00
9	112.01	1.87	0.21	0.00	9	166.01	1.71	0.29	0.00
9	113.01	1.87	0.23	0.00	9	167.01	1.71	0.31	0.00
9	114.01	1.87	0.22	0.00	9	168.01	1.71	0.31	0.00
9	115.01	1.87	0.23	0.00	9	169.01	1.71	0.32	0.00
9	116.01	1.87	0.23	0.00	9	170.01	1.71	0.35	0.00
9	117.01	1.87	0.19	0.00	9	171.01	1.71	0.29	0.00
9	118.01	1.87	0.19	0.00	9	172.01	1.71	0.39	0.00
9	119.01	1.87	0.18	0.00	9	173.01	1.71	0.40	0.00
9	120.01	1.87	0.19	0.00	9	174.01	1.71	0.40	0.00
9	121.01	1.87	0.19	0.00	9	175.01	1.72	0.41	0.00
9	122.01	1.87	0.18	0.00	9	176.01	1.67	0.42	0.00
9	123.01	1.87	0.18	0.00	9	177.01	1.64	0.42	0.00
9	124.01	1.94	0.20	0.01	9	178.01	1.64	0.38	0.00
9	125.01	1.84	0.20	0.00	9	179.01	1.64	0.34	0.00
9	126.01	1.89	0.18	0.00	9	180.01	1.65	0.34	0.00
9	127.01	1.89	0.26	0.01	9	181.01	1.71	0.33	0.00
9	130.01	1.86	0.17	0.00	9	182.01	1.71	0.35	0.00
9	131.01	1.82	0.19	0.00	9	183.01	1.71	0.34	0.00
9	133.01	1.86	0.38	0.03	9	184.01	1.71	0.35	0.00
9	134.01	1.86	0.36	0.03	9	185.01	1.71	0.36	0.00
9	135.01	1.86	0.40	0.04	9	186.01	1.64	0.40	0.00
9	136.01	1.86	0.41	0.04	9	187.01	1.85	0.26	0.00
9	137.01	1.86	0.41	0.04	9	188.01	1.69	0.37	0.00
9	138.01	1.86	0.41	0.04	9	189.01	1.68	0.35	0.00
9	140.01	1.83	0.27	0.00	9	190.01	1.68	0.37	0.00
9	141.01	1.77	0.25	0.00	9	191.01	1.68	0.39	0.00
9	142.01	1.77	0.25	0.00	9	192.01	1.68	0.43	0.00
9	143.01	1.77	0.29	0.00	9	193.01	1.68	0.45	0.00
9	144.01	1.77	0.29	0.00	9	194.01	1.68	0.40	0.00
9	145.01	1.77	0.28	0.00	9	195.01	1.68	0.43	0.00
9	146.01	1.77	0.35	0.01	9	196.01	1.68	0.42	0.00
9	147.01	1.79	0.38	0.01	9	197.01	1.67	0.50	0.01
9	148.01	1.67	0.44	0.00	9	198.01	1.54	0.52	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	199.01	1.57	0.54	0.00	9	249.01	1.31	0.96	0.00
9	200.01	1.58	0.55	0.00	9	250.01	1.31	0.99	0.00
9	201.01	1.55	0.59	0.00	9	251.01	1.29	1.01	0.00
9	202.01	1.55	0.59	0.00	9	252.01	1.29	1.00	0.00
9	203.01	1.55	0.61	0.00	9	253.01	1.34	0.98	0.00
9	204.01	1.55	0.60	0.00	9	254.01	1.30	1.00	0.00
9	205.01	1.55	0.61	0.00	9	255.01	1.26	0.94	0.00
9	206.01	1.55	0.59	0.00	9	256.01	1.32	0.92	0.00
9	207.01	1.56	0.75	0.02	9	257.01	1.32	0.94	0.00
9	208.01	1.40	0.76	0.00	9	258.01	1.32	0.94	0.00
9	209.01	1.42	0.78	0.00	9	259.01	1.32	0.95	0.00
9	210.01	1.42	0.78	0.00	9	260.01	1.32	0.94	0.00
9	211.01	1.42	0.80	0.00	9	261.01	1.32	0.96	0.00
9	212.01	1.42	0.80	0.00	9	262.01	1.32	0.98	0.00
9	213.01	1.42	0.83	0.00	9	263.01	1.32	0.95	0.00
9	214.01	1.42	0.86	0.00	9	264.01	1.32	1.02	0.00
9	215.01	1.42	0.87	0.00	9	265.01	1.32	0.99	0.00
9	216.01	1.44	0.81	0.00	9	266.01	1.32	1.01	0.00
9	217.01	1.39	0.88	0.00	9	267.01	1.32	0.95	0.00
9	218.01	1.39	0.90	0.00	9	268.01	1.32	1.00	0.00
9	219.01	1.39	0.89	0.00	9	269.01	1.32	1.03	0.00
9	220.01	1.39	0.91	0.00	9	270.01	1.32	1.04	0.00
9	221.01	1.39	0.91	0.00	9	271.01	1.32	1.04	0.00
9	222.01	1.41	0.92	0.01	9	272.01	1.32	1.07	0.00
9	223.01	1.33	0.92	0.00	9	273.01	1.32	1.08	0.00
9	224.01	1.40	0.90	0.00	9	274.01	1.32	1.11	0.01
9	225.01	1.34	0.90	0.00	9	275.01	1.34	1.05	0.01
9	226.01	1.34	0.92	0.00	9	276.01	1.27	1.05	0.00
9	227.01	1.34	0.94	0.00	9	277.01	1.27	1.02	0.00
9	228.01	1.34	0.95	0.00	9	278.01	1.27	1.06	0.00
9	229.01	1.34	0.95	0.00	9	279.01	1.33	0.94	0.00
9	230.01	1.34	0.96	0.00	9	280.01	1.32	0.94	0.00
9	231.01	1.34	0.97	0.00	9	281.01	1.32	0.92	0.00
9	232.01	1.37	0.98	0.01	9	282.01	1.30	0.92	0.00
9	233.01	1.30	1.00	0.00	9	283.01	1.33	0.95	0.00
9	234.01	1.32	0.97	0.00	9	284.01	1.33	0.93	0.00
9	235.01	1.33	0.94	0.00	9	285.01	1.33	0.92	0.00
9	236.01	1.35	0.95	0.00	9	286.01	1.33	0.91	0.00
9	237.01	1.32	0.93	0.00	9	287.01	1.33	0.94	0.00
9	238.01	1.32	1.00	0.00	9	288.01	1.33	0.93	0.00
9	239.01	1.32	0.99	0.00	9	289.01	1.33	0.93	0.00
9	240.01	1.29	1.09	0.00	9	290.01	1.33	0.92	0.00
9	241.01	1.33	1.01	0.00	9	291.01	1.33	0.90	0.00
9	242.01	1.37	0.96	0.00	9	292.01	1.32	0.88	0.00
9	243.01	1.31	0.96	0.00	9	293.01	1.35	0.89	0.00
9	244.01	1.31	0.98	0.00	9	294.01	1.35	0.90	0.00
9	245.01	1.28	0.96	0.00	9	295.01	1.35	0.88	0.00
9	246.01	1.31	0.93	0.00	9	296.01	1.35	0.87	0.00
9	247.01	1.31	0.92	0.00	9	297.01	1.35	0.88	0.00
9	248.01	1.31	0.93	0.00	9	298.01	1.35	0.89	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	299.01	1.35	0.90	0.00	9	349.01	0.86	2.07	0.00
9	300.01	1.35	0.90	0.00	9	350.01	1.77	2.05	0.82
9	301.01	1.35	0.92	0.00	9	351.01	0.79	0.21	1.07
9	302.01	1.35	0.88	0.00	9	352.01	1.83	0.13	0.01
9	303.01	1.35	0.89	0.00	9	353.01	0.78	1.56	0.07
9	304.01	1.35	0.87	0.00	9	355.01	0.95	2.84	0.12
9	305.01	1.33	0.86	0.00	9	356.01	0.60	2.83	0.00
9	306.01	1.36	0.88	0.00	9	65.02	1.08	1.69	0.01
9	307.01	1.36	0.88	0.00	9	66.02	0.99	1.75	0.00
9	308.01	1.36	0.87	0.00	9	70.02	1.06	1.61	0.00
9	309.01	1.36	0.87	0.00	9	71.02	1.05	2.27	0.07
9	310.01	1.36	0.87	0.00	9	72.02	0.78	2.32	0.00
9	311.01	1.36	0.89	0.00	9	75.02	0.82	2.25	0.00
9	312.01	1.36	0.90	0.00	9	77.02	0.96	2.17	0.02
9	313.01	1.29	0.99	0.00	9	81.02	0.96	1.85	0.00
9	314.01	1.29	1.00	0.00	9	82.02	0.93	1.83	0.00
9	315.01	1.29	0.99	0.00	9	86.02	1.05	2.02	0.03
9	316.01	1.29	1.02	0.00	9	87.02	0.87	2.03	0.00
9	317.01	1.29	1.01	0.00	9	94.02	1.00	1.88	0.01
9	318.01	1.29	0.99	0.00	9	95.02	0.92	1.87	0.00
9	319.01	1.29	0.95	0.00	9	96.02	0.94	1.91	0.00
9	320.01	1.29	0.97	0.00	9	100.02	0.94	1.45	0.02
9	321.01	1.29	0.95	0.00	9	101.02	1.08	1.41	0.00
9	322.01	1.29	0.92	0.00	9	102.02	1.08	1.35	0.00
9	323.01	1.29	0.92	0.00	9	103.02	1.08	1.29	0.00
9	324.01	1.29	0.92	0.00	9	104.02	1.08	1.31	0.00
9	325.01	1.22	0.88	0.02	9	105.02	1.08	1.32	0.00
9	326.01	1.35	0.90	0.00	9	106.02	1.08	1.30	0.00
9	327.01	1.35	0.92	0.00	9	110.02	1.23	0.99	0.00
9	328.01	1.35	0.95	0.00	9	111.02	1.23	1.12	0.00
9	329.01	1.35	0.95	0.00	9	113.02	1.20	0.93	0.01
9	330.01	1.35	0.95	0.00	9	114.02	1.48	0.74	0.00
9	331.01	1.35	0.96	0.00	9	115.02	1.27	0.75	0.02
9	332.01	1.35	0.99	0.00	9	116.02	1.42	0.75	0.00
9	333.01	1.35	0.98	0.00	9	117.02	1.42	0.77	0.00
9	334.01	1.37	1.01	0.01	9	118.02	1.42	0.76	0.00
9	335.01	1.28	1.05	0.00	9	119.02	1.42	0.77	0.00
9	336.01	1.28	0.97	0.00	9	120.02	1.42	0.77	0.00
9	337.01	1.28	0.97	0.00	9	121.02	1.42	0.76	0.00
9	338.01	1.28	0.99	0.00	9	122.02	1.42	0.78	0.00
9	339.01	1.28	1.00	0.00	9	123.02	1.42	0.80	0.00
9	340.01	1.29	1.01	0.00	9	124.02	1.44	0.75	0.00
9	341.01	1.29	1.01	0.00	9	125.02	1.43	0.72	0.00
9	342.01	1.29	1.07	0.00	9	126.02	1.50	0.83	0.02
9	343.01	1.29	1.08	0.00	9	127.02	1.40	0.67	0.01
9	344.01	1.19	1.09	0.00	9	130.02	1.49	0.63	0.00
9	345.01	1.24	1.03	0.00	9	131.02	1.91	0.42	0.07
9	346.01	1.24	1.04	0.00	9	133.02	1.50	0.36	0.04
9	347.01	1.17	1.06	0.01	9	134.02	1.50	0.35	0.04
9	348.01	1.16	2.56	0.22	9	135.02	1.50	0.30	0.06

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	136.02	1.50	0.29	0.07	9	191.02	1.64	0.48	0.00
9	137.02	1.50	0.27	0.07	9	192.02	1.64	0.43	0.00
9	140.02	1.66	0.23	0.02	9	193.02	1.64	0.40	0.00
9	142.02	1.93	0.17	0.00	9	194.02	1.57	0.42	0.00
9	143.02	1.88	0.14	0.00	9	195.02	1.79	0.38	0.01
9	144.02	1.88	0.13	0.00	9	196.02	1.67	0.39	0.00
9	145.02	1.88	0.14	0.00	9	197.02	1.58	0.31	0.02
9	146.02	1.88	0.10	0.01	9	198.02	1.73	0.27	0.00
9	147.02	1.87	0.08	0.02	9	199.02	1.73	0.24	0.00
9	148.02	2.01	0.06	0.00	9	200.02	1.73	0.23	0.01
9	149.02	2.01	0.05	0.00	9	201.02	1.73	0.20	0.01
9	150.02	2.01	0.05	0.00	9	202.02	1.73	0.21	0.01
9	151.02	2.01	0.05	0.00	9	203.02	1.73	0.21	0.01
9	152.02	2.01	0.04	0.01	9	204.02	1.73	0.20	0.01
9	153.02	2.01	0.05	0.00	9	205.02	1.73	0.19	0.01
9	154.02	2.01	0.05	0.00	9	206.02	1.73	0.22	0.01
9	155.02	2.01	0.05	0.00	9	207.02	1.76	0.14	0.02
9	156.02	2.01	0.05	0.00	9	208.02	1.91	0.13	0.00
9	157.02	2.01	0.05	0.00	9	209.02	1.91	0.13	0.00
9	159.02	2.16	0.02	0.00	9	210.02	1.91	0.13	0.00
9	160.02	2.13	0.03	0.00	9	211.02	1.91	0.11	0.00
9	161.02	2.13	0.03	0.00	9	212.02	1.91	0.11	0.00
9	162.02	2.05	0.02	0.01	9	213.02	1.91	0.10	0.00
9	163.02	2.10	0.02	0.00	9	214.02	1.91	0.10	0.00
9	164.02	2.14	0.02	0.00	9	215.02	1.91	0.10	0.00
9	165.02	2.14	0.02	0.00	9	216.02	1.94	0.08	0.00
9	166.02	2.14	0.02	0.00	9	217.02	2.00	0.06	0.00
9	167.02	2.14	0.02	0.00	9	218.02	2.00	0.06	0.00
9	168.02	2.14	0.02	0.00	9	219.02	2.00	0.07	0.00
9	169.02	2.14	0.02	0.00	9	220.02	2.00	0.06	0.00
9	170.02	2.33	0.01	0.02	9	221.02	2.00	0.07	0.00
9	171.02	2.07	0.10	0.01	9	222.02	2.03	0.08	0.00
9	172.02	2.19	0.01	0.00	9	223.02	2.01	0.08	0.00
9	173.02	2.18	0.03	0.00	9	224.02	2.01	0.09	0.00
9	174.02	2.12	0.02	0.00	9	225.02	2.01	0.10	0.00
9	175.02	2.10	0.02	0.00	9	226.02	2.01	0.10	0.00
9	176.02	2.15	0.01	0.00	9	227.02	2.01	0.10	0.00
9	177.02	2.15	0.02	0.00	9	228.02	2.01	0.10	0.00
9	178.02	2.15	0.05	0.01	9	229.02	2.01	0.10	0.00
9	179.02	2.15	0.41	0.25	9	230.02	2.01	0.10	0.00
9	180.02	2.15	0.45	0.28	9	231.02	2.01	0.13	0.01
9	181.02	2.15	0.46	0.28	9	232.02	2.01	0.13	0.01
9	182.02	2.15	0.46	0.28	9	233.02	2.04	0.19	0.03
9	183.02	2.15	0.48	0.30	9	234.02	1.85	0.20	0.00
9	184.02	2.15	0.48	0.31	9	235.02	1.86	0.22	0.00
9	185.02	2.15	0.47	0.29	9	236.02	1.80	0.43	0.03
9	187.02	2.15	0.49	0.31	9	237.02	1.63	0.49	0.00
9	188.02	1.64	0.56	0.01	9	238.02	1.63	0.43	0.00
9	189.02	2.29	0.42	0.42	9	239.02	1.63	0.42	0.00
9	190.02	1.64	0.47	0.00	9	240.02	1.58	0.41	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	241.02	1.65	0.40	0.00	9	291.02	1.39	0.81	0.00
9	242.02	1.65	0.41	0.00	9	292.02	1.37	0.81	0.00
9	243.02	1.65	0.41	0.00	9	293.02	1.39	0.83	0.00
9	244.02	1.65	0.41	0.00	9	294.02	1.34	0.92	0.00
9	245.02	1.52	0.45	0.01	9	295.02	1.33	0.90	0.00
9	246.02	1.79	0.39	0.02	9	296.02	1.33	0.93	0.00
9	247.02	1.64	0.42	0.00	9	297.02	1.33	0.91	0.00
9	248.02	1.64	0.40	0.00	9	298.02	1.33	0.90	0.00
9	249.02	1.64	0.39	0.00	9	299.02	1.33	0.88	0.00
9	250.02	1.64	0.39	0.00	9	300.02	1.33	0.88	0.00
9	251.02	1.63	0.42	0.00	9	301.02	1.33	0.91	0.00
9	252.02	1.64	0.45	0.00	9	302.02	1.33	0.93	0.00
9	253.02	1.64	0.45	0.00	9	303.02	1.33	0.97	0.00
9	254.02	1.64	0.47	0.00	9	304.02	1.33	0.96	0.00
9	255.02	1.58	0.55	0.00	9	305.02	1.24	0.98	0.00
9	256.02	1.55	0.55	0.00	9	306.02	1.30	0.98	0.00
9	257.02	1.55	0.55	0.00	9	307.02	1.30	0.97	0.00
9	258.02	1.55	0.55	0.00	9	308.02	1.30	0.97	0.00
9	259.02	1.55	0.56	0.00	9	309.02	1.30	0.96	0.00
9	260.02	1.55	0.56	0.00	9	310.02	1.30	0.94	0.00
9	261.02	1.55	0.57	0.00	9	311.02	1.30	0.94	0.00
9	262.02	1.55	0.58	0.00	9	312.02	1.30	0.91	0.00
9	263.02	1.55	0.58	0.00	9	313.02	1.32	1.03	0.00
9	264.02	1.42	0.55	0.02	9	314.02	1.28	1.02	0.00
9	265.02	1.65	0.50	0.00	9	315.02	1.28	1.01	0.00
9	266.02	1.50	0.54	0.00	9	316.02	1.21	0.97	0.01
9	267.02	1.56	0.55	0.00	9	317.02	1.30	0.98	0.00
9	268.02	1.56	0.55	0.00	9	318.02	1.30	1.00	0.00
9	269.02	1.56	0.61	0.00	9	319.02	1.30	0.99	0.00
9	270.02	1.51	0.61	0.00	9	320.02	1.30	0.98	0.00
9	271.02	1.48	0.62	0.00	9	321.02	1.30	1.01	0.00
9	272.02	1.50	0.58	0.00	9	322.02	1.30	1.02	0.00
9	273.02	1.50	0.60	0.00	9	323.02	1.30	0.99	0.00
9	274.02	1.50	0.60	0.00	9	324.02	1.30	1.00	0.00
9	275.02	1.47	0.67	0.00	9	325.02	1.36	0.97	0.00
9	276.02	1.47	0.65	0.00	9	326.02	1.30	0.97	0.00
9	277.02	1.46	0.67	0.00	9	327.02	1.30	0.97	0.00
9	278.02	1.43	0.68	0.00	9	328.02	1.30	0.97	0.00
9	279.02	1.42	0.78	0.00	9	329.02	1.30	0.97	0.00
9	280.02	1.41	0.78	0.00	9	330.02	1.30	0.97	0.00
9	281.02	1.39	0.77	0.00	9	331.02	1.30	0.96	0.00
9	282.02	1.38	0.78	0.00	9	332.02	1.30	0.94	0.00
9	283.02	1.40	0.77	0.00	9	333.02	1.30	0.96	0.00
9	284.02	1.40	0.77	0.00	9	334.02	1.32	0.91	0.00
9	285.02	1.40	0.78	0.00	9	335.02	1.33	0.87	0.00
9	286.02	1.40	0.77	0.00	9	336.02	1.33	0.89	0.00
9	287.02	1.40	0.78	0.00	9	337.02	1.33	0.95	0.00
9	288.02	1.33	0.77	0.01	9	338.02	1.27	0.91	0.00
9	289.02	1.41	0.79	0.00	9	339.02	1.25	0.98	0.00
9	290.02	1.37	0.81	0.00	9	340.02	1.31	1.02	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	341.02	1.22	1.04	0.00	9	169.03	2.77	0.19	0.00
9	342.02	1.27	1.06	0.00	9	173.03	2.89	0.43	0.00
9	343.02	1.27	1.04	0.00	9	179.03	3.11	2.09	0.38
9	344.02	1.31	1.07	0.00	9	180.03	3.73	1.70	0.02
9	345.02	1.26	1.07	0.00	9	181.03	3.73	1.74	0.02
9	346.02	1.26	1.07	0.00	9	184.03	3.90	2.07	0.03
9	347.02	1.13	1.08	0.01	9	185.03	3.73	2.10	0.00
9	348.02	0.87	1.29	0.08	9	187.03	3.73	2.01	0.00
9	349.02	0.95	1.80	0.00	9	188.03	3.89	2.28	0.01
9	350.02	1.24	1.79	0.08	9	189.03	3.73	1.52	0.04
9	351.02	1.68	0.07	0.12	9	190.03	3.74	1.30	0.09
9	352.02	2.02	0.13	0.01	9	191.03	3.43	1.10	0.01
9	353.02	0.87	1.20	0.11	9	192.03	3.43	0.98	0.02
9	355.02	1.09	2.41	0.12	9	193.03	3.43	0.77	0.07
9	356.02	0.74	2.45	0.00	9	198.03	3.56	0.79	0.15
9	71.03	1.04	2.17	0.05	9	201.03	3.09	0.88	0.02
9	72.03	0.82	2.17	0.00	9	205.03	3.39	0.09	0.64
9	75.03	0.91	2.19	0.01	9	209.03	2.75	0.26	0.00
9	81.03	0.86	2.11	0.00	9	211.03	2.95	0.31	0.01
9	82.03	0.89	2.13	0.00	9	213.03	3.00	0.38	0.01
9	86.03	0.96	1.98	0.01	9	214.03	2.91	0.39	0.00
9	87.03	0.88	1.97	0.00	9	215.03	2.90	0.38	0.00
9	94.03	1.01	1.97	0.02	9	216.03	2.80	0.38	0.01
9	95.03	0.89	1.99	0.00	9	217.03	2.91	0.37	0.00
9	100.03	0.97	1.83	0.00	9	218.03	2.91	0.41	0.00
9	101.03	0.94	1.87	0.00	9	219.03	2.91	0.43	0.00
9	102.03	0.94	1.89	0.00	9	220.03	2.91	0.43	0.00
9	104.03	1.00	1.81	0.00	9	221.03	2.91	0.45	0.00
9	110.03	1.09	1.49	0.00	9	222.03	2.80	0.42	0.02
9	111.03	0.99	1.49	0.01	9	223.03	2.94	0.41	0.00
9	113.03	1.10	1.38	0.00	9	224.03	2.94	0.38	0.00
9	115.03	1.11	1.39	0.00	9	225.03	2.94	0.32	0.01
9	120.03	1.29	0.98	0.00	9	226.03	2.94	0.11	0.98
9	123.03	1.47	0.70	0.00	9	227.03	2.94	0.37	1.58
9	126.03	1.47	0.40	0.03	9	228.03	2.94	0.39	1.63
9	133.03	1.83	0.25	0.00	9	229.03	2.94	0.40	1.64
9	135.03	1.92	0.18	0.00	9	230.03	2.94	0.41	1.66
9	136.03	1.87	0.17	0.00	9	231.03	2.94	0.39	1.64
9	142.03	2.00	0.10	0.00	9	232.03	2.94	0.37	1.59
9	146.03	2.12	0.02	0.00	9	233.03	2.82	0.34	1.24
9	147.03	2.16	0.02	0.00	9	234.03	1.71	0.32	0.00
9	148.03	2.16	0.02	0.00	9	235.03	1.75	0.30	0.00
9	152.03	2.29	0.00	0.00	9	236.03	1.74	0.16	0.02
9	153.03	2.22	0.00	0.00	9	237.03	1.74	0.12	0.04
9	156.03	2.39	0.00	0.00	9	238.03	1.74	0.15	0.02
9	157.03	2.35	0.00	0.00	9	239.03	1.74	0.17	0.02
9	162.03	2.22	0.02	0.05	9	240.03	1.74	0.15	0.03
9	163.03	2.56	0.11	0.00	9	241.03	1.90	0.16	0.00
9	164.03	2.62	0.11	0.00	9	242.03	1.90	0.17	0.00
9	168.03	2.37	0.19	0.13	9	243.03	1.90	0.17	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	244.03	1.93	0.17	0.00	9	296.03	1.43	0.79	0.00
9	247.03	1.87	0.11	0.01	9	297.03	1.43	0.79	0.00
9	248.03	1.95	0.13	0.00	9	298.03	1.43	0.81	0.00
9	249.03	1.95	0.13	0.00	9	299.03	1.43	0.79	0.00
9	250.03	1.95	0.14	0.00	9	300.03	1.43	0.79	0.00
9	251.03	1.95	0.13	0.00	9	301.03	1.43	0.77	0.00
9	252.03	1.95	0.13	0.00	9	302.03	1.43	0.75	0.00
9	253.03	1.95	0.13	0.00	9	303.03	1.43	0.70	0.00
9	254.03	1.95	0.11	0.00	9	304.03	1.43	0.74	0.00
9	255.03	1.87	0.10	0.01	9	305.03	1.40	0.73	0.00
9	256.03	1.98	0.11	0.00	9	306.03	1.44	0.72	0.00
9	257.03	1.98	0.10	0.00	9	307.03	1.44	0.74	0.00
9	258.03	1.98	0.11	0.00	9	308.03	1.44	0.76	0.00
9	259.03	1.98	0.13	0.00	9	309.03	1.44	0.77	0.00
9	260.03	1.98	0.11	0.00	9	310.03	1.44	0.78	0.00
9	261.03	1.98	0.13	0.00	9	311.03	1.44	0.78	0.00
9	262.03	1.98	0.12	0.00	9	312.03	1.44	0.81	0.00
9	263.03	1.98	0.11	0.00	9	313.03	1.44	0.88	0.01
9	264.03	1.98	0.13	0.00	9	314.03	1.35	0.92	0.00
9	265.03	1.98	0.14	0.00	9	315.03	1.35	0.94	0.00
9	266.03	1.95	0.13	0.00	9	316.03	1.37	0.97	0.00
9	267.03	1.94	0.13	0.00	9	317.03	1.31	0.97	0.00
9	268.03	1.94	0.12	0.00	9	318.03	1.31	0.97	0.00
9	269.03	1.90	0.09	0.01	9	319.03	1.31	1.04	0.00
9	270.03	2.00	0.14	0.01	9	320.03	1.31	1.05	0.00
9	271.03	1.96	0.14	0.00	9	321.03	1.31	1.04	0.00
9	272.03	1.91	0.16	0.00	9	322.03	1.31	1.04	0.00
9	273.03	1.91	0.24	0.01	9	323.03	1.31	1.07	0.00
9	274.03	1.91	0.22	0.01	9	324.03	1.31	1.05	0.00
9	275.03	1.88	0.21	0.00	9	325.03	1.36	1.06	0.01
9	276.03	1.84	0.23	0.00	9	326.03	1.26	1.06	0.00
9	277.03	1.84	0.22	0.00	9	327.03	1.26	1.05	0.00
9	278.03	1.78	0.24	0.00	9	328.03	1.26	1.01	0.00
9	279.03	1.83	0.34	0.02	9	329.03	1.26	1.00	0.00
9	280.03	1.70	0.37	0.00	9	330.03	1.26	1.02	0.00
9	281.03	1.68	0.36	0.00	9	331.03	1.18	1.05	0.01
9	282.03	1.63	0.36	0.00	9	332.03	1.26	1.02	0.00
9	283.03	1.69	0.37	0.00	9	333.03	1.26	1.03	0.00
9	284.03	1.69	0.48	0.01	9	334.03	1.29	1.03	0.00
9	285.03	1.69	0.47	0.01	9	335.03	1.28	1.04	0.00
9	286.03	1.69	0.54	0.02	9	336.03	1.28	1.04	0.00
9	287.03	1.69	0.62	0.04	9	337.03	1.30	0.97	0.00
9	288.03	1.64	0.68	0.03	9	338.03	1.30	1.02	0.00
9	289.03	1.46	0.70	0.00	9	339.03	1.38	0.92	0.00
9	290.03	1.51	0.74	0.01	9	340.03	1.33	0.89	0.00
9	291.03	1.43	0.76	0.00	9	341.03	1.37	0.84	0.00
9	292.03	1.41	0.79	0.00	9	342.03	1.38	0.85	0.00
9	293.03	1.40	0.78	0.00	9	343.03	1.38	0.87	0.00
9	294.03	1.37	0.74	0.00	9	344.03	1.41	0.87	0.00
9	295.03	1.43	0.78	0.00	9	345.03	1.36	0.90	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	346.03	1.36	0.93	0.00	9	228.04	3.54	6.16	1.51
9	347.03	1.27	1.60	0.06	9	229.04	3.54	6.27	1.57
9	348.03	0.95	2.13	0.01	9	230.04	3.54	6.37	1.62
9	349.03	0.97	1.73	0.00	9	231.04	3.54	6.61	1.74
9	350.03	0.85	1.73	0.01	9	232.04	3.54	6.65	1.76
9	353.03	0.89	1.26	0.08	9	233.04	3.59	6.80	1.70
9	355.03	1.02	2.46	0.09	9	234.04	4.90	6.85	0.00
9	356.03	0.72	2.43	0.00	9	235.04	4.93	6.96	0.00
9	71.04	1.04	2.13	0.05	9	236.04	4.93	7.15	0.00
9	72.04	0.90	2.20	0.01	9	237.04	5.01	7.12	0.00
9	75.04	0.90	2.17	0.01	9	238.04	4.97	7.04	0.00
9	81.04	0.82	2.17	0.00	9	239.04	4.96	6.84	0.00
9	82.04	0.91	2.29	0.02	9	240.04	4.56	6.91	0.12
9	94.04	0.91	1.85	0.00	9	241.04	4.95	6.64	0.01
9	95.04	0.93	1.85	0.00	9	242.04	4.87	6.52	0.00
9	100.04	0.93	1.86	0.00	9	243.04	4.87	6.53	0.00
9	101.04	0.93	1.87	0.00	9	244.04	4.57	6.56	0.08
9	102.04	0.93	1.90	0.00	9	247.04	4.85	6.61	0.00
9	110.04	1.03	1.77	0.01	9	248.04	4.85	6.63	0.00
9	111.04	0.96	1.77	0.00	9	249.04	4.85	6.49	0.00
9	115.04	1.11	1.69	0.01	9	250.04	4.85	6.46	0.00
9	126.04	1.11	1.44	0.00	9	251.04	4.85	0.41	3.69
9	135.04	1.24	1.38	0.02	9	252.04	4.85	0.45	3.56
9	142.04	1.26	1.33	0.02	9	253.04	4.85	0.44	3.60
9	147.04	1.31	1.20	0.01	9	254.04	4.85	0.47	3.52
9	148.04	1.26	1.23	0.01	9	255.04	4.85	0.45	3.58
9	152.04	1.24	1.30	0.01	9	256.04	4.85	0.45	3.56
9	153.04	1.18	1.47	0.01	9	257.04	4.85	0.48	3.49
9	162.04	1.14	0.92	0.04	9	258.04	4.85	0.47	3.51
9	168.04	1.33	0.89	0.00	9	259.04	4.79	0.46	3.31
9	169.04	1.32	1.06	0.00	9	260.04	5.01	0.53	3.95
9	180.04	1.29	0.52	0.08	9	261.04	4.98	0.64	3.56
9	181.04	1.57	0.54	0.00	9	262.04	3.09	0.61	0.00
9	188.04	1.55	0.27	0.05	9	264.04	3.09	0.41	2.08
9	189.04	1.78	0.08	0.05	9	265.04	3.09	0.59	0.00
9	190.04	1.59	0.09	0.17	9	266.04	3.09	0.45	2.17
9	191.04	2.00	0.04	0.01	9	267.04	3.09	0.42	2.11
9	192.04	2.02	0.02	0.02	9	268.04	3.09	0.42	2.11
9	201.04	2.07	0.16	0.38	9	269.04	3.09	0.40	2.06
9	211.04	2.86	1.75	0.57	9	270.04	3.09	0.31	1.85
9	215.04	3.78	2.07	0.00	9	271.04	3.09	0.29	1.79
9	216.04	3.73	1.93	0.00	9	272.04	1.75	0.26	0.00
9	217.04	3.73	1.76	0.01	9	273.04	1.75	0.17	0.02
9	221.04	3.90	2.22	0.01	9	274.04	1.75	0.18	0.01
9	222.04	3.81	2.01	0.01	9	275.04	1.74	0.15	0.02
9	223.04	3.71	2.07	0.00	9	276.04	1.91	0.13	0.00
9	224.04	3.75	1.57	0.05	9	277.04	1.95	0.14	0.00
9	225.04	3.54	1.66	0.00	9	278.04	1.91	0.11	0.00
9	226.04	3.54	4.84	0.90	9	279.04	1.91	0.04	0.03
9	227.04	3.54	6.08	1.48	9	280.04	1.91	0.03	0.04

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	281.04	1.88	0.04	0.05	9	331.04	1.64	0.45	0.00
9	282.04	2.00	0.04	0.01	9	332.04	1.58	0.43	0.00
9	283.04	2.10	0.03	0.00	9	333.04	1.64	0.45	0.00
9	284.04	2.10	0.01	0.01	9	334.04	1.64	0.69	0.03
9	285.04	2.10	0.01	0.01	9	335.04	1.64	0.75	0.04
9	286.04	2.09	0.01	0.01	9	336.04	1.64	0.77	0.05
9	287.04	2.20	0.00	0.00	9	337.04	1.64	0.77	0.05
9	288.04	2.20	0.04	0.01	9	338.04	1.64	0.77	0.05
9	289.04	2.20	0.03	0.01	9	339.04	1.64	0.77	0.05
9	290.04	2.20	0.02	0.00	9	340.04	1.61	0.81	0.05
9	291.04	2.20	0.02	0.00	9	341.04	1.39	0.83	0.00
9	292.04	2.14	0.03	0.00	9	342.04	1.39	0.84	0.00
9	293.04	2.12	0.03	0.00	9	343.04	1.39	0.85	0.00
9	294.04	2.12	0.02	0.00	9	344.04	1.42	0.81	0.00
9	295.04	2.12	0.02	0.00	9	345.04	1.39	0.78	0.00
9	296.04	2.12	0.02	0.00	9	346.04	1.39	0.77	0.00
9	297.04	2.12	0.02	0.00	9	347.04	1.30	1.84	0.14
9	298.04	2.12	0.02	0.00	9	348.04	0.86	2.24	0.00
9	299.04	2.12	0.02	0.00	9	349.04	0.93	1.86	0.00
9	300.04	2.12	0.02	0.00	9	350.04	0.82	1.86	0.01
9	301.04	2.12	0.02	0.00	9	353.04	0.84	1.41	0.07
9	302.04	2.12	0.03	0.00	9	355.04	0.96	2.44	0.05
9	303.04	2.12	0.04	0.00	9	356.04	0.62	2.42	0.01
9	304.04	2.12	0.04	0.00	9	226.05	1.08	1.52	0.00
9	305.04	2.12	0.04	0.00	9	227.05	1.05	1.52	0.00
9	306.04	2.12	0.03	0.00	9	228.05	1.05	1.51	0.00
9	307.04	2.12	0.04	0.00	9	229.05	1.05	1.53	0.00
9	308.04	2.12	0.05	0.00	9	230.05	1.05	1.54	0.00
9	309.04	2.12	0.06	0.01	9	232.05	1.19	1.44	0.01
9	310.04	2.12	0.07	0.01	9	235.05	1.18	1.29	0.00
9	311.04	2.12	0.08	0.01	9	236.05	1.20	1.41	0.01
9	312.04	2.12	0.07	0.01	9	241.05	1.20	1.18	0.00
9	313.04	2.06	0.29	0.10	9	242.05	1.25	1.22	0.00
9	314.04	1.75	0.29	0.00	9	243.05	1.19	1.20	0.00
9	315.04	1.75	0.30	0.00	9	247.05	1.33	0.99	0.00
9	316.04	1.74	0.32	0.00	9	248.05	1.30	0.98	0.00
9	317.04	1.73	0.32	0.00	9	249.05	1.33	0.92	0.00
9	318.04	1.73	0.32	0.00	9	251.05	1.38	1.07	3.75
9	319.04	1.73	0.29	0.00	9	252.05	3.32	1.04	0.00
9	320.04	1.73	0.29	0.00	9	256.05	3.06	0.58	0.00
9	321.04	1.73	0.28	0.00	9	257.05	3.35	0.59	0.09
9	322.04	1.73	0.29	0.00	9	259.05	3.49	0.53	0.23
9	323.04	1.75	0.32	0.00	9	260.05	3.01	0.44	0.00
9	324.04	1.75	0.33	0.00	9	261.05	3.09	0.44	0.02
9	325.04	1.76	0.34	0.00	9	262.05	2.95	0.46	0.00
9	326.04	1.70	0.34	0.00	9	264.05	2.95	4.37	2.04
9	327.04	1.70	0.35	0.00	9	265.05	2.95	0.51	0.00
9	328.04	1.70	0.39	0.00	9	266.05	2.95	4.52	2.15
9	329.04	1.70	0.40	0.00	9	267.05	2.95	4.48	2.12
9	330.04	1.70	0.42	0.00	9	268.05	2.95	4.36	2.04

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	269.05	2.95	4.41	2.07	9	321.05	2.12	0.02	0.00
9	270.05	2.95	4.41	2.07	9	322.05	2.02	0.02	0.02
9	271.05	2.83	4.37	2.39	9	323.05	2.15	0.01	0.00
9	272.05	4.38	4.31	0.00	9	324.05	2.15	0.01	0.00
9	275.05	4.14	4.79	0.12	9	325.05	2.13	0.02	0.00
9	276.05	4.22	4.46	0.03	9	326.05	2.14	0.03	0.00
9	277.05	4.18	3.27	0.01	9	327.05	2.14	0.11	0.03
9	278.05	4.02	1.85	0.14	9	328.05	2.14	0.10	0.03
9	279.05	4.49	2.71	0.31	9	329.05	2.14	0.11	0.03
9	280.05	3.93	2.67	0.00	9	330.05	2.14	0.10	0.03
9	281.05	3.87	2.48	0.00	9	331.05	2.03	0.11	0.00
9	282.05	3.78	2.24	0.00	9	332.05	2.47	0.06	0.19
9	283.05	4.05	2.79	0.01	9	333.05	2.15	0.09	0.02
9	284.05	4.02	2.44	0.03	9	334.05	2.00	0.02	0.02
9	285.05	3.81	2.30	0.00	9	335.05	1.98	0.02	0.03
9	286.05	3.66	1.86	0.00	9	336.05	2.16	0.02	0.00
9	287.05	3.65	1.66	0.01	9	337.05	2.12	0.02	0.00
9	288.05	3.65	0.59	0.36	9	338.05	2.14	0.02	0.00
9	289.05	3.65	0.51	0.43	9	339.05	2.16	0.02	0.00
9	290.05	3.65	0.48	0.45	9	340.05	2.09	0.01	0.01
9	291.05	3.65	0.49	0.44	9	341.05	2.20	0.01	0.00
9	292.05	3.48	0.51	0.23	9	342.05	2.20	0.00	0.00
9	293.05	3.01	0.51	0.00	9	343.05	2.20	0.00	0.00
9	294.05	2.98	0.51	0.00	9	344.05	2.18	0.00	0.00
9	295.05	3.00	0.48	0.00	9	345.05	2.23	0.00	0.00
9	296.05	3.00	0.45	0.00	9	346.05	2.23	0.00	0.00
9	297.05	3.00	0.43	0.00	9	347.05	2.07	1.74	1.22
9	298.05	3.00	0.41	0.01	9	348.05	0.90	2.02	0.00
9	299.05	3.00	0.42	0.01	9	349.05	0.91	1.94	0.00
9	300.05	3.01	0.37	0.01	9	350.05	0.89	1.91	0.00
9	301.05	2.90	0.28	0.01	9	353.05	0.87	1.53	0.03
9	302.05	2.90	0.44	1.60	9	355.05	0.96	2.48	0.06
9	303.05	2.90	0.44	1.61	9	356.05	0.60	2.51	0.01
9	304.05	2.90	0.44	1.61	9	226.06	1.08	1.68	0.01
9	305.05	2.90	0.42	1.57	9	227.06	1.03	1.71	0.00
9	306.05	2.90	0.42	1.57	9	228.06	0.98	1.74	0.00
9	307.05	2.90	0.41	1.56	9	229.06	1.05	1.75	0.01
9	308.05	2.90	0.36	1.47	9	241.06	1.08	1.48	0.00
9	309.05	2.90	0.34	1.42	9	242.06	1.17	1.46	0.01
9	310.05	2.90	0.32	1.37	9	243.06	1.13	1.51	0.00
9	311.05	2.90	0.34	1.42	9	247.06	1.11	1.55	0.00
9	312.05	2.91	0.37	1.53	9	248.06	1.11	1.57	0.01
9	313.05	1.68	0.05	0.15	9	249.06	1.09	2.05	0.05
9	314.05	1.68	0.05	0.15	9	256.06	0.87	2.04	0.00
9	315.05	1.68	0.04	0.17	9	257.06	0.88	2.02	0.00
9	316.05	1.66	0.03	0.21	9	261.06	0.98	1.50	0.01
9	317.05	2.12	0.03	0.00	9	262.06	1.06	1.46	0.00
9	318.05	2.12	0.02	0.00	9	264.06	1.06	1.46	0.00
9	319.05	2.12	0.02	0.00	9	265.06	1.06	1.45	0.00
9	320.05	2.12	0.02	0.00	9	266.06	1.08	1.46	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	267.06	1.08	1.49	0.00	9	327.06	2.97	0.71	0.03
9	268.06	1.09	1.50	0.00	9	328.06	2.97	0.66	0.02
9	271.06	1.11	1.54	0.00	9	330.06	3.11	0.84	0.01
9	272.06	1.08	1.56	0.00	9	331.06	3.19	0.83	0.00
9	275.06	1.09	1.64	0.01	9	332.06	3.06	0.81	0.02
9	276.06	1.05	1.76	0.01	9	333.06	3.19	0.77	0.00
9	279.06	1.06	0.99	0.05	9	334.06	3.19	0.76	0.00
9	280.06	1.30	0.97	0.00	9	335.06	3.05	0.64	0.00
9	281.06	1.46	0.81	0.00	9	336.06	3.09	0.61	0.00
9	282.06	1.36	0.76	0.00	9	337.06	3.06	0.63	0.00
9	283.06	1.47	0.81	0.01	9	338.06	2.95	0.63	0.02
9	284.06	1.42	0.74	0.00	9	339.06	3.09	0.60	0.00
9	285.06	1.42	0.66	0.00	9	340.06	2.94	0.45	1.73
9	286.06	1.42	0.38	0.06	9	341.06	1.62	0.48	0.00
9	287.06	1.42	0.25	0.14	9	342.06	1.60	0.49	0.00
9	288.06	1.44	0.03	1.07	9	343.06	1.59	0.51	0.00
9	289.06	2.47	0.06	0.00	9	344.06	1.56	0.51	0.00
9	290.06	2.49	0.04	0.00	9	345.06	1.53	0.59	0.00
9	291.06	2.49	0.04	0.00	9	346.06	1.50	0.57	0.00
9	292.06	2.50	0.04	0.00	9	347.06	1.44	1.75	0.22
9	293.06	2.50	0.05	0.00	9	348.06	0.89	1.90	0.00
9	294.06	2.36	0.05	0.02	9	349.06	0.90	1.92	0.00
9	295.06	2.51	0.06	0.00	9	350.06	0.93	1.93	0.00
9	296.06	2.51	0.07	0.00	9	355.06	0.82	2.62	0.02
9	297.06	2.51	0.08	0.00	9	356.06	0.44	2.64	0.05
9	298.06	2.51	0.09	0.01	9	363.06	0.65	2.43	0.01
9	299.06	2.51	0.10	0.01	9	243.07	1.08	1.42	0.00
9	300.06	2.47	0.13	0.03	9	247.07	1.16	1.42	0.00
9	301.06	2.65	0.20	0.01	9	248.07	1.10	2.26	0.10
9	302.06	2.65	2.67	1.62	9	264.07	0.81	2.18	0.00
9	303.06	2.65	2.72	1.66	9	265.07	0.81	2.18	0.00
9	304.06	2.65	2.75	1.68	9	266.07	0.89	2.16	0.00
9	305.06	2.65	2.66	1.61	9	267.07	0.88	2.14	0.00
9	306.06	2.65	2.60	1.56	9	268.07	0.90	2.15	0.01
9	307.06	2.65	2.63	1.59	9	271.07	0.89	2.07	0.00
9	308.06	2.65	2.64	1.59	9	272.07	0.96	2.11	0.02
9	309.06	2.65	2.62	1.58	9	275.07	0.91	2.09	0.00
9	310.06	2.65	2.62	1.58	9	279.07	0.95	1.24	0.05
9	311.06	2.65	2.63	1.59	9	280.07	1.18	1.25	0.00
9	315.06	2.67	3.49	2.22	9	282.07	1.24	1.14	0.00
9	316.06	3.93	3.53	0.06	9	283.07	1.17	1.12	0.00
9	317.06	4.17	3.52	0.00	9	284.07	1.10	1.44	0.00
9	318.06	4.17	3.49	0.00	9	285.07	1.24	1.41	0.02
9	319.06	4.17	3.44	0.00	9	286.07	1.11	1.59	0.01
9	320.06	4.17	3.49	0.00	9	287.07	1.03	1.62	0.00
9	321.06	4.17	3.49	0.00	9	288.07	1.40	0.81	0.00
9	323.06	4.20	3.67	0.00	9	289.07	1.04	1.49	0.00
9	324.06	4.21	3.56	0.00	9	290.07	1.15	1.42	0.00
9	325.06	4.00	0.46	1.07	9	291.07	1.10	1.43	0.00
9	326.06	2.97	0.45	0.00	9	292.07	1.15	1.45	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
9	294.07	1.20	1.33	0.00	9	248.10	0.99	2.97	0.18
9	295.07	1.14	1.29	0.00	9	264.10	0.64	2.75	0.00
9	296.07	1.14	1.30	0.00	9	265.10	0.67	2.73	0.00
9	297.07	1.14	1.31	0.00	9	283.10	0.73	1.78	0.05
9	298.07	1.14	1.31	0.00	9	284.10	1.00	1.69	0.00
9	299.07	1.14	1.30	0.00	9	285.10	1.07	1.66	0.00
9	300.07	1.17	1.31	0.00	9	292.10	1.02	1.27	0.02
9	301.07	1.15	1.32	0.00	9	296.10	1.25	1.20	0.00
9	302.07	1.15	1.33	0.00	9	297.10	1.19	1.18	0.00
9	303.07	1.15	1.35	0.00	9	301.10	1.25	1.00	0.00
9	304.07	1.14	1.33	0.00	9	302.10	1.29	1.00	0.00
9	305.07	1.14	1.27	0.00	9	303.10	1.29	0.99	0.00
9	306.07	1.14	1.22	0.00	9	304.10	1.29	0.99	0.00
9	307.07	1.14	1.17	0.01	9	305.10	1.34	1.00	0.00
9	308.07	1.14	1.16	0.01	9	306.10	1.29	1.00	0.00
9	309.07	1.14	1.14	0.01	9	307.10	1.32	1.50	0.06
9	310.07	1.14	1.14	0.01	9	310.10	1.11	1.40	0.00
9	311.07	1.14	1.13	0.01	9	311.10	1.10	1.39	0.00
9	315.07	1.17	1.14	0.00	9	316.10	1.15	1.37	0.00
9	316.07	1.24	1.16	0.00	9	317.10	1.12	1.36	0.00
9	317.07	1.21	1.16	0.00	9	318.10	1.14	1.40	0.00
9	318.07	1.21	1.18	0.00	9	321.10	1.19	1.31	0.00
9	319.07	1.21	1.17	0.00	9	331.10	1.12	1.36	0.00
9	320.07	1.21	1.21	0.00	9	332.10	1.16	1.37	0.00
9	321.07	1.21	1.25	0.00	9	334.10	1.15	1.36	0.00
9	323.07	1.21	1.18	0.00	9	335.10	1.16	1.36	0.00
9	324.07	1.17	3.22	0.46	9	336.10	1.12	1.41	0.00
9	325.07	1.62	0.04	0.75	9	337.10	1.16	1.31	0.00
9	326.07	2.49	0.04	0.00	9	338.10	1.15	1.30	0.00
9	327.07	2.49	0.05	0.00	9	340.10	0.96	2.07	0.01
9	328.07	2.49	0.05	0.00	9	344.10	1.20	1.50	0.02
9	331.07	2.56	0.07	0.00	9	345.10	1.07	1.50	0.00
9	332.07	1.31	0.07	1.56	9	346.10	1.10	1.49	0.00
9	334.07	2.66	0.13	0.00	9	347.10	1.01	1.94	0.01
9	335.07	2.66	0.17	0.00	9	349.10	0.87	2.04	0.00
9	336.07	2.70	0.20	0.00	9	350.10	0.92	2.01	0.00
9	337.07	2.69	0.04	0.04	9	363.10	0.79	2.30	0.00
9	338.07	2.49	0.04	0.00	10	2	1.05	2.11	0.04
9	339.07	2.51	0.00	0.08	10	3	0.86	2.20	0.00
9	340.07	2.16	1.05	1.34	10	8	0.89	1.94	0.00
9	341.07	3.17	0.00	0.71	10	9	0.89	1.94	0.00
9	342.07	2.33	0.00	0.00	10	10	0.89	1.94	0.00
9	344.07	2.28	0.37	0.36	10	14	0.95	1.59	0.01
9	345.07	1.59	0.34	0.01	10	15	1.03	1.60	0.00
9	346.07	1.67	0.36	0.00	10	16	1.03	1.57	0.00
9	347.07	1.58	1.85	0.42	10	17	1.03	1.56	0.00
9	348.07	0.86	1.75	0.01	10	19	1.17	1.36	0.00
9	349.07	0.86	2.03	0.00	10	21	1.27	1.25	0.01
9	350.07	0.98	2.04	0.01	10	23	1.31	1.26	0.02
9	363.07	.			10	25	1.29	1.17	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
10	26	1.21	1.17	0.00	10	103	1.96	0.14	0.00
10	28	1.18	1.24	0.00	10	104	1.76	0.00	0.35
10	30	1.33	1.13	0.01	10	105	1.57	0.20	0.07
10	31	1.43	0.99	0.02	10	106	1.72	0.06	0.10
10	32	1.20	1.17	0.00	10	108	1.75	0.08	0.07
10	34	1.21	1.00	0.01	10	109	1.97	0.11	0.00
10	36	1.20	1.04	0.00	10	110	1.96	0.20	0.01
10	37	1.27	0.99	0.00	10	111	1.96	0.21	0.02
10	38	1.48	0.86	0.01	10	113	2.16	0.03	0.00
10	40	1.36	0.93	0.00	10	114	1.98	0.18	0.01
10	41	1.33	0.92	0.00	10	115	2.13	0.02	0.00
10	42	1.33	0.96	0.00	10	117	2.12	0.01	0.00
10	46	1.45	0.73	0.00	10	118	1.85	0.13	0.01
10	48	1.52	0.62	0.00	10	120	1.93	0.13	0.00
10	49	1.60	0.59	0.01	10	121	2.16	0.00	0.01
10	50	1.52	0.62	0.00	10	122	1.96	0.02	0.03
10	52	1.57	0.62	0.00	10	123	2.21	0.00	0.00
10	53	1.68	0.53	0.01	10	124	1.99	0.04	0.01
10	54	1.66	0.47	0.00	10	125	2.21	0.06	0.03
10	55	1.50	0.59	0.00	10	126	1.98	0.11	0.00
10	57	1.52	0.50	0.00	10	127	2.04	0.05	0.00
10	60	1.59	0.50	0.00	10	128	1.95	0.13	0.00
10	61	1.75	0.39	0.01	10	129	2.20	0.09	0.05
10	62	1.63	0.44	0.00	10	130	1.98	0.16	0.01
10	63	1.64	0.48	0.00	10	131	1.89	0.19	0.00
10	64	1.60	0.52	0.00	10	132	1.99	0.09	0.00
10	65	1.60	0.51	0.00	10	133	1.99	0.12	0.00
10	68	1.80	0.25	0.00	10	134	2.04	0.15	0.02
10	69	1.79	0.27	0.00	10	135	1.91	0.14	0.00
10	70	1.76	0.32	0.00	10	136	1.91	0.16	0.00
10	72	1.57	0.39	0.01	10	137	2.11	0.16	0.05
10	74	1.76	0.16	0.02	10	138	1.88	0.26	0.01
10	77	1.56	0.22	0.06	10	139	1.91	0.27	0.02
10	78	1.99	0.11	0.00	10	140	1.77	0.30	0.00
10	79	1.57	0.18	0.08	10	141	1.74	0.33	0.00
10	81	1.56	0.42	0.01	10	142	1.92	0.26	0.02
10	83	1.79	0.05	0.07	10	143	1.71	0.39	0.00
10	84	2.06	0.14	0.02	10	144	1.78	0.39	0.01
10	85	1.46	0.23	0.12	10	145	1.71	0.42	0.00
10	87	1.81	0.25	0.00	10	146	1.78	0.41	0.02
10	89	1.81	0.28	0.00	10	147	1.71	0.48	0.01
10	90	1.79	0.03	0.11	10	148	1.78	0.53	0.05
10	91	1.56	0.07	0.22	10	149	1.60	0.53	0.00
10	93	1.77	0.06	0.07	10	150	1.53	0.60	0.00
10	94	1.60	0.31	0.02	10	151	1.72	0.51	0.02
10	96	2.04	0.10	0.01	10	152	1.60	0.60	0.01
10	99	2.04	0.12	0.01	10	153	1.48	0.75	0.00
10	100	1.79	0.00	0.32	10	154	1.89	0.51	0.10
10	101	1.59	0.16	0.09	10	155	1.53	0.63	0.00
10	102	1.74	0.11	0.05	10	156	1.50	0.64	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
10	157	1.73	0.39	0.00	10	207	1.36	0.90	0.00
10	158	1.67	0.43	0.00	10	208	1.36	0.84	0.00
10	159	1.45	0.49	0.02	10	209	1.34	0.92	0.00
10	160	1.66	0.36	0.00	10	210	1.41	0.92	0.01
10	161	1.51	0.46	0.01	10	211	1.33	0.85	0.00
10	162	1.61	0.47	0.00	10	212	1.33	0.96	0.00
10	163	1.61	0.42	0.00	10	213	1.21	0.95	0.01
10	164	1.61	0.49	0.00	10	214	1.70	0.82	0.10
10	165	1.61	0.59	0.01	10	215	1.32	0.79	0.01
10	166	1.61	0.67	0.02	10	216	1.40	0.81	0.00
10	167	1.61	0.50	0.00	10	217	1.40	0.80	0.00
10	168	1.61	0.60	0.01	10	218	1.46	0.82	0.01
10	169	1.61	0.71	0.03	10	219	1.39	0.82	0.00
10	170	1.61	0.71	0.03	10	220	1.41	0.87	0.00
10	171	1.56	0.77	0.02	10	221	1.36	0.90	0.00
10	172	1.76	0.61	0.06	10	222	1.36	0.92	0.00
10	173	1.41	0.74	0.00	10	223	1.39	0.97	0.01
10	174	1.51	0.75	0.01	10	224	1.31	0.99	0.00
10	175	1.41	0.76	0.00	10	225	1.31	0.96	0.00
10	176	1.41	0.79	0.00	10	226	1.39	0.90	0.00
10	177	1.51	0.74	0.01	10	227	1.34	0.89	0.00
10	178	1.41	0.77	0.00	10	228	1.34	0.89	0.00
10	179	1.51	0.70	0.00	10	229	1.34	0.92	0.00
10	180	1.41	0.72	0.00	10	230	1.34	0.96	0.00
10	181	1.51	0.59	0.00	10	231	1.38	0.99	0.01
10	182	1.41	0.72	0.00	10	232	1.37	1.02	0.01
10	183	1.51	0.63	0.00	10	233	1.21	1.04	0.00
10	184	1.41	0.69	0.00	10	234	1.43	0.96	0.01
10	185	1.41	0.73	0.00	10	235	1.30	1.05	0.00
10	186	1.51	0.60	0.00	10	236	1.27	1.00	0.00
10	187	1.64	0.76	0.05	10	237	1.27	1.02	0.00
10	188	1.42	0.66	0.00	10	238	1.27	0.92	0.00
10	189	1.42	0.73	0.00	10	239	1.27	0.94	0.00
10	190	1.42	0.72	0.00	10	240	1.27	0.90	0.01
10	191	1.42	0.79	0.00	10	241	1.27	0.88	0.01
10	192	1.42	0.81	0.00	10	242	1.27	0.88	0.01
10	193	1.42	0.84	0.00	10	243	1.27	0.94	0.00
10	194	1.42	0.88	0.00	10	244	1.27	0.98	0.00
10	195	1.37	0.82	0.00	10	245	1.27	0.89	0.01
10	196	1.46	0.80	0.00	10	246	1.27	0.96	0.00
10	197	1.38	0.79	0.00	10	247	1.27	0.90	0.01
10	198	1.38	0.84	0.00	10	248	1.31	0.87	0.00
10	199	1.38	0.89	0.00	10	249	1.23	0.98	0.00
10	200	1.38	0.88	0.00	10	250	1.58	0.88	0.05
10	201	1.38	0.89	0.00	10	251	1.36	0.91	0.00
10	202	1.38	0.85	0.00	10	252	1.34	0.96	0.00
10	203	1.38	0.83	0.00	10	253	1.34	0.99	0.00
10	204	1.38	0.83	0.00	10	254	1.34	0.97	0.00
10	205	1.38	0.86	0.00	10	255	1.34	0.98	0.00
10	206	1.49	0.87	0.02	10	256	1.34	0.99	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
10	257	1.33	1.00	0.00	10	308	1.23	1.18	0.00
10	258	1.29	1.02	0.00	10	309	1.23	1.18	0.00
10	259	1.29	1.03	0.00	10	310	1.23	1.24	0.00
10	260	1.32	1.05	0.00	10	311	1.28	1.25	0.01
10	261	1.29	1.08	0.00	10	312	1.21	1.18	0.00
10	262	1.23	1.15	0.00	10	313	1.24	1.10	0.00
10	263	1.26	1.18	0.00	10	314	1.24	1.13	0.00
10	264	1.25	1.26	0.01	10	315	1.32	1.08	0.00
10	265	1.15	1.24	0.00	10	316	1.25	1.08	0.00
10	266	1.27	1.16	0.00	10	317	1.32	1.03	0.00
10	267	1.21	1.24	0.00	10	318	1.27	0.92	0.00
10	268	1.21	1.27	0.00	10	319	1.27	1.00	0.00
10	269	1.21	1.28	0.00	10	320	1.27	0.91	0.00
10	270	1.21	1.31	0.00	10	321	1.54	0.29	0.04
10	271	1.15	1.91	0.06	10	322	1.25	0.95	0.00
10	273	1.22	1.01	0.00	10	323	1.32	0.93	0.00
10	274	1.29	1.05	0.00	10	324	1.32	0.90	0.00
10	275	1.36	0.98	0.00	10	325	1.32	0.93	0.00
10	276	1.30	1.02	0.00	10	326	1.32	0.98	0.00
10	277	1.29	1.05	0.00	10	327	1.32	0.89	0.00
10	278	1.27	1.06	0.00	10	328	1.32	1.01	0.00
10	279	1.28	1.05	0.00	10	331	1.42	0.90	0.01
10	280	1.30	1.04	0.00	10	332	1.44	0.90	0.01
10	281	1.30	1.02	0.00	10	333	1.42	0.84	0.00
10	282	1.24	0.98	0.00	10	334	1.37	0.88	0.00
10	283	1.30	1.06	0.00	10	335	1.37	0.88	0.00
10	284	1.38	1.03	0.01	10	336	1.33	0.79	0.01
10	285	1.29	1.05	0.00	10	337	1.40	0.77	0.00
10	286	1.36	1.00	0.00	10	338	1.40	0.82	0.00
10	287	1.29	0.99	0.00	10	339	1.40	0.82	0.00
10	288	1.29	1.02	0.00	10	340	1.40	0.82	0.00
10	289	1.26	1.03	0.00	10	341	1.40	0.85	0.00
10	290	1.28	1.08	0.00	10	342	1.43	0.77	0.00
10	291	1.28	1.08	0.00	10	343	1.41	0.80	0.00
10	292	1.30	1.12	0.00	10	344	1.41	0.80	0.00
10	293	1.31	1.11	0.01	10	345	1.41	0.76	0.00
10	294	0.99	1.00	0.09	10	346	1.40	0.54	0.02
10	295	1.35	0.90	0.00	10	347	1.56	0.60	0.00
10	296	1.29	0.99	0.00	10	348	1.56	0.62	0.00
10	297	1.34	0.91	0.00	10	349	1.56	0.70	0.01
10	298	1.20	0.95	0.01	10	350	1.56	0.61	0.00
10	299	1.32	0.95	0.00	10	351	1.56	0.69	0.01
10	300	1.32	1.02	0.00	10	352	1.56	0.75	0.02
10	301	1.32	1.07	0.00	10	353	1.56	0.78	0.02
10	302	1.32	1.11	0.01	10	354	1.56	0.70	0.01
10	303	1.28	1.14	0.00	10	355	1.56	0.82	0.03
10	304	1.26	1.18	0.00	10	356	1.56	0.81	0.03
10	305	1.17	1.11	0.00	10	357	1.56	0.81	0.03
10	306	1.23	1.15	0.00	10	358	1.56	0.80	0.03
10	307	1.23	1.17	0.00	10	359	1.56	0.82	0.03

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
10	360	1.56	0.86	0.04	10	410	1.32	0.82	0.00
10	361	1.56	0.79	0.02	10	411	1.38	0.81	0.00
10	362	1.56	0.82	0.03	10	412	1.38	0.84	0.00
10	363	1.56	0.82	0.03	10	413	1.34	0.85	0.00
10	364	1.56	0.85	0.04	10	414	1.36	0.77	0.00
10	365	1.56	0.90	0.05	10	415	1.41	0.73	0.00
10	366	1.65	0.79	0.06	10	416	1.41	0.79	0.00
10	367	1.38	0.99	0.01	10	417	1.41	0.83	0.00
10	368	1.32	0.92	0.00	10	418	1.41	0.88	0.00
10	369	1.53	0.94	0.04	10	419	1.35	0.86	0.00
10	370	1.32	0.91	0.00	10	420	1.33	0.87	0.00
10	371	1.32	0.94	0.00	10	421	1.36	0.92	0.00
10	372	1.32	0.95	0.00	10	422	1.34	0.95	0.00
10	373	1.23	0.98	0.01	10	423	1.30	0.96	0.00
10	374	1.30	0.96	0.00	10	424	1.31	0.96	0.00
10	375	1.66	0.80	0.07	10	425	1.28	1.09	0.00
10	376	1.40	0.89	0.00	10	426	1.25	1.12	0.00
10	377	1.12	0.93	0.04	10	427	1.00	1.24	0.03
10	378	1.24	0.96	0.00	10	428	1.34	0.99	0.00
10	379	1.31	0.99	0.00	10	429	1.19	1.17	0.00
10	380	1.25	0.96	0.00	10	430	1.05	1.80	0.01
10	381	1.31	0.99	0.00	10	431	0.95	1.76	0.00
10	382	1.38	0.96	0.01	10	432	0.82	2.10	0.00
10	383	1.31	1.00	0.00	10	2.01	1.00	2.49	0.08
10	384	1.31	1.00	0.00	10	25.01	0.77	1.70	0.05
10	385	1.31	1.01	0.00	10	26.01	1.01	1.65	0.00
10	386	1.31	1.01	0.00	10	28.01	1.05	1.70	0.00
10	387	1.25	1.00	0.00	10	30.01	1.06	1.60	0.00
10	388	1.29	1.02	0.00	10	46.01	1.01	1.60	0.00
10	389	1.36	0.93	0.00	10	50.01	1.05	1.55	0.00
10	390	1.35	0.81	0.00	10	52.01	1.04	1.63	0.00
10	391	1.39	0.85	0.00	10	54.01	1.21	1.53	0.02
10	392	1.39	0.79	0.00	10	57.01	1.28	1.39	0.03
10	393	1.39	0.83	0.00	10	60.01	1.04	1.27	0.02
10	394	1.39	0.81	0.00	10	63.01	1.24	1.10	0.00
10	395	1.45	0.72	0.00	10	69.01	1.23	1.08	0.00
10	396	1.44	0.71	0.00	10	70.01	1.24	1.04	0.00
10	397	1.44	0.71	0.00	10	72.01	1.48	0.91	0.02
10	398	1.44	0.74	0.00	10	77.01	1.27	0.90	0.00
10	399	1.43	0.80	0.00	10	81.01	1.32	0.46	0.08
10	400	1.40	0.79	0.00	10	87.01	1.33	0.25	0.21
10	401	1.40	0.84	0.00	10	89.01	1.32	0.24	0.22
10	402	1.41	0.80	0.00	10	102.01	1.80	0.10	0.03
10	403	1.39	0.84	0.00	10	103.01	1.80	0.08	0.05
10	404	1.39	0.86	0.00	10	104.01	1.55	0.20	0.09
10	405	1.39	0.93	0.00	10	105.01	2.25	0.01	0.00
10	406	1.39	0.98	0.01	10	108.01	1.55	0.00	0.49
10	407	1.39	1.01	0.01	10	109.01	1.32	0.03	0.64
10	408	1.41	0.99	0.01	10	114.01	1.55	0.04	0.88
10	409	1.31	0.98	0.00	10	117.01	1.50	0.00	0.65

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
10	126.01	1.57	0.32	1.67	10	233.01	4.55	0.00	5.11
10	130.01	1.52	0.50	2.18	10	234.01	4.68	0.07	4.55
10	134.01	1.39	0.63	2.85	10	235.01	2.29	0.00	0.00
10	135.01	3.08	0.66	0.00	10	236.01	2.20	0.16	0.10
10	137.01	3.22	0.78	0.00	10	237.01	2.41	0.02	0.07
10	139.01	3.15	0.97	0.02	10	238.01	1.88	0.50	0.09
10	142.01	3.27	1.02	0.00	10	239.01	2.14	0.13	0.04
10	146.01	3.14	1.52	0.14	10	240.01	1.88	0.22	0.00
10	149.01	3.38	2.61	0.28	10	241.01	2.14	0.14	0.05
10	152.01	3.38	2.98	0.41	10	244.01	2.48	0.13	0.31
10	153.01	3.35	3.12	0.50	10	245.01	1.88	0.31	0.02
10	155.01	3.40	3.63	0.64	10	246.01	2.33	0.41	0.45
10	160.01	3.31	3.48	0.71	10	247.01	1.65	0.39	0.00
10	161.01	4.30	3.72	0.01	10	248.01	1.65	0.42	0.00
10	169.01	4.39	5.47	0.06	10	249.01	1.85	0.43	0.05
10	174.01	4.84	6.47	0.00	10	250.01	1.62	0.58	0.01
10	175.01	4.37	6.53	0.22	10	251.01	1.63	0.43	0.00
10	176.01	4.84	6.45	0.00	10	252.01	1.63	0.41	0.00
10	181.01	4.97	6.97	0.00	10	253.01	1.68	0.40	0.00
10	183.01	4.90	6.99	0.00	10	254.01	1.54	0.57	0.00
10	185.01	4.98	7.44	0.00	10	255.01	1.88	0.47	0.07
10	186.01	5.15	7.56	0.01	10	256.01	1.68	0.54	0.01
10	187.01	5.02	7.53	0.00	10	257.01	1.56	0.47	0.00
10	192.01	4.98	8.50	0.05	10	258.01	1.56	0.51	0.00
10	194.01	4.99	8.80	0.07	10	259.01	1.56	0.51	0.00
10	195.01	5.33	9.73	0.01	10	260.01	1.56	0.53	0.00
10	196.01	5.17	9.92	0.07	10	261.01	1.56	0.56	0.00
10	197.01	4.99	9.06	0.10	10	262.01	1.56	0.54	0.00
10	199.01	5.17	10.33	0.11	10	263.01	1.56	0.53	0.00
10	200.01	4.99	9.62	0.16	10	264.01	1.57	0.52	0.00
10	201.01	5.50	10.20	0.00	10	265.01	1.56	0.52	0.00
10	205.01	5.07	10.33	0.19	10	266.01	1.56	0.51	0.00
10	206.01	5.47	6.81	0.33	10	267.01	1.56	0.49	0.00
10	207.01	5.75	10.17	0.08	10	268.01	1.56	0.49	0.00
10	210.01	5.67	11.76	0.00	10	269.01	1.56	0.52	0.00
10	214.01	5.50	11.98	0.06	10	270.01	1.56	0.47	0.00
10	217.01	5.67	14.11	0.14	10	271.01	1.59	1.52	0.28
10	218.01	5.21	12.74	0.42	10	273.01	1.56	0.46	0.00
10	219.01	5.86	12.18	0.01	10	274.01	1.56	0.46	0.00
10	221.01	6.02	12.80	0.02	10	275.01	1.62	0.44	0.00
10	223.01	5.86	11.97	0.01	10	276.01	1.66	0.43	0.00
10	224.01	6.03	14.00	0.00	10	277.01	1.84	0.43	0.04
10	225.01	5.92	4.95	1.98	10	278.01	1.64	0.42	0.00
10	226.01	4.51	4.20	0.03	10	279.01	1.64	0.41	0.00
10	227.01	4.51	2.22	0.54	10	280.01	1.64	0.42	0.00
10	228.01	4.51	1.84	0.75	10	281.01	1.79	0.11	0.03
10	229.01	4.51	1.31	1.17	10	282.01	1.65	0.40	0.00
10	230.01	4.51	1.13	1.35	10	283.01	1.69	0.41	0.00
10	231.01	4.51	0.05	3.98	10	284.01	1.65	0.41	0.00
10	232.01	4.50	0.00	4.72	10	285.01	1.60	0.50	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
10	286.01	1.65	0.38	0.00	10	338.01	1.64	0.42	0.00
10	287.01	1.88	0.35	0.03	10	339.01	1.62	0.43	0.00
10	288.01	1.70	0.34	0.00	10	340.01	1.79	0.34	0.01
10	289.01	1.54	0.36	0.02	10	341.01	1.66	0.42	0.00
10	290.01	1.70	0.34	0.00	10	342.01	1.64	0.39	0.00
10	291.01	1.70	0.35	0.00	10	343.01	1.64	0.40	0.00
10	292.01	1.70	0.36	0.00	10	344.01	1.51	0.43	0.02
10	293.01	1.69	0.34	0.00	10	345.01	1.51	0.46	0.01
10	294.01	1.62	0.34	0.01	10	346.01	1.79	0.31	0.00
10	295.01	1.70	0.33	0.00	10	347.01	1.61	0.45	0.00
10	296.01	1.70	0.36	0.00	10	348.01	1.62	0.46	0.00
10	297.01	1.70	0.32	0.00	10	349.01	1.61	0.39	0.00
10	298.01	1.55	0.44	0.01	10	350.01	1.81	0.34	0.01
10	299.01	1.88	0.32	0.02	10	351.01	1.66	0.38	0.00
10	300.01	1.73	0.41	0.01	10	352.01	1.66	0.35	0.00
10	301.01	1.65	0.43	0.00	10	353.01	1.66	0.37	0.00
10	302.01	1.65	0.40	0.00	10	354.01	1.66	0.34	0.00
10	303.01	1.58	0.41	0.00	10	355.01	1.66	0.35	0.00
10	304.01	1.65	0.41	0.00	10	356.01	1.66	0.36	0.00
10	305.01	1.65	0.44	0.00	10	357.01	1.69	0.37	0.00
10	306.01	1.65	0.45	0.00	10	358.01	1.69	0.34	0.00
10	307.01	1.65	0.46	0.00	10	359.01	1.69	0.35	0.00
10	308.01	1.65	0.46	0.00	10	360.01	1.69	0.36	0.00
10	309.01	1.65	0.48	0.00	10	361.01	1.69	0.35	0.00
10	310.01	1.65	0.47	0.00	10	362.01	1.69	0.35	0.00
10	311.01	1.65	0.48	0.00	10	363.01	1.69	0.33	0.00
10	312.01	1.65	0.46	0.00	10	364.01	1.69	0.33	0.00
10	313.01	1.61	0.47	0.00	10	365.01	1.69	0.34	0.00
10	314.01	1.61	0.47	0.00	10	366.01	1.69	0.34	0.00
10	315.01	1.65	0.45	0.00	10	367.01	1.69	0.32	0.00
10	316.01	1.66	0.46	0.00	10	368.01	1.69	0.29	0.00
10	317.01	1.59	0.53	0.00	10	369.01	1.69	0.31	0.00
10	318.01	1.76	0.43	0.02	10	370.01	1.69	0.28	0.01
10	319.01	1.64	0.45	0.00	10	371.01	1.69	0.28	0.00
10	320.01	1.62	0.47	0.00	10	372.01	1.69	0.29	0.00
10	321.01	1.62	0.45	0.00	10	373.01	1.69	0.26	0.01
10	322.01	1.62	0.48	0.00	10	374.01	1.69	0.28	0.01
10	323.01	1.62	0.51	0.00	10	375.01	1.69	0.26	0.01
10	324.01	1.62	0.43	0.00	10	376.01	1.69	0.25	0.01
10	325.01	1.84	0.11	0.01	10	377.01	1.69	0.25	0.01
10	326.01	1.49	0.62	0.00	10	378.01	1.69	0.25	0.01
10	327.01	1.64	0.41	0.00	10	379.01	1.69	0.24	0.01
10	328.01	1.80	0.38	0.02	10	380.01	1.61	0.34	0.01
10	331.01	1.68	0.40	0.00	10	381.01	1.71	0.35	0.00
10	332.01	1.65	0.40	0.00	10	382.01	1.72	0.35	0.00
10	333.01	1.65	0.42	0.00	10	383.01	1.70	0.36	0.00
10	334.01	1.65	0.41	0.00	10	384.01	1.70	0.39	0.00
10	335.01	1.65	0.40	0.00	10	385.01	1.70	0.39	0.00
10	336.01	1.59	0.42	0.00	10	386.01	1.70	0.40	0.00
10	337.01	1.64	0.39	0.00	10	387.01	1.70	0.39	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
10	388.01	1.70	0.39	0.00	10	197.02	1.55	0.55	0.00
10	389.01	1.71	0.40	0.00	10	217.02	1.54	0.45	0.01
10	390.01	1.65	0.38	0.00	10	219.02	1.81	0.04	0.07
10	391.01	1.65	0.38	0.00	10	221.02	1.61	0.04	0.24
10	392.01	1.65	0.40	0.00	10	226.02	2.15	2.49	2.96
10	393.01	1.65	0.39	0.00	10	228.02	4.04	5.36	0.32
10	394.01	1.65	0.39	0.00	10	231.02	4.63	12.77	1.52
10	395.01	1.65	0.39	0.00	10	237.02	5.85	17.06	0.33
10	396.01	1.67	0.39	0.00	10	241.02	6.07	20.24	0.51
10	397.01	1.67	0.41	0.00	10	244.02	6.04	21.07	0.71
10	398.01	1.67	0.41	0.00	10	250.02	7.51	25.87	0.02
10	399.01	1.66	0.40	0.00	10	251.02	7.05	25.83	0.10
10	400.01	1.66	0.43	0.00	10	257.02	7.52	28.78	0.02
10	401.01	1.66	0.42	0.00	10	258.02	7.68	28.40	0.00
10	402.01	1.66	0.42	0.00	10	259.02	7.62	28.90	0.00
10	403.01	1.66	0.44	0.00	10	260.02	7.62	29.17	0.01
10	404.01	1.66	0.42	0.00	10	263.02	7.79	30.98	0.00
10	405.01	1.66	0.41	0.00	10	264.02	7.27	31.62	0.41
10	406.01	1.66	0.40	0.00	10	266.02	8.08	32.28	0.01
10	407.01	1.66	0.41	0.00	10	268.02	7.98	33.04	0.00
10	408.01	1.66	0.42	0.00	10	269.02	8.04	33.13	0.00
10	409.01	1.68	0.42	0.00	10	270.02	8.14	34.23	0.00
10	410.01	1.63	0.40	0.00	10	271.02	8.44	37.58	0.00
10	411.01	1.66	0.43	0.00	10	273.02	7.99	33.37	0.01
10	412.01	1.66	0.44	0.00	10	274.02	8.07	34.09	0.00
10	413.01	1.66	0.45	0.00	10	275.02	7.93	32.32	0.00
10	414.01	1.66	0.44	0.00	10	276.02	8.28	34.65	0.01
10	415.01	1.66	0.47	0.00	10	277.02	8.04	33.37	0.00
10	416.01	1.66	0.48	0.00	10	280.02	8.27	37.43	0.02
10	417.01	1.66	0.56	0.01	10	283.02	8.03	35.31	0.04
10	418.01	1.66	0.55	0.01	10	284.02	8.32	38.95	0.04
10	419.01	1.62	0.56	0.01	10	285.02	8.09	38.18	0.15
10	420.01	1.48	0.59	0.00	10	286.02	8.04	37.15	0.12
10	421.01	1.52	0.59	0.00	10	287.02	8.28	39.35	0.08
10	422.01	1.49	0.56	0.00	10	288.02	8.56	39.63	0.00
10	423.01	1.54	0.55	0.00	10	292.02	8.68	40.55	0.00
10	424.01	1.54	0.55	0.00	10	293.02	8.69	41.42	0.00
10	425.01	1.52	0.45	0.01	10	296.02	8.63	38.85	0.01
10	426.01	1.62	0.45	0.00	10	297.02	8.44	37.47	0.00
10	427.01	1.62	0.44	0.00	10	299.02	8.66	41.83	0.01
10	428.01	1.62	0.45	0.00	10	300.02	8.66	43.59	0.05
10	429.01	1.62	0.42	0.00	10	301.02	8.52	41.39	0.04
10	430.01	1.43	2.21	0.39	10	302.02	8.74	41.18	0.00
10	431.01	0.57	2.33	0.04	10	304.02	8.84	42.30	0.00
10	432.01	0.65	2.15	0.03	10	306.02	8.92	44.21	0.00
10	2.02	1.05	2.58	0.13	10	307.02	8.94	43.73	0.00
10	102.02	0.72	1.67	0.08	10	308.02	8.94	44.01	0.00
10	181.02	1.03	0.90	0.10	10	309.02	8.94	44.47	0.00
10	183.02	1.34	0.85	0.00	10	311.02	9.06	44.31	0.01
10	194.02	1.49	0.60	0.00	10	312.02	8.95	44.17	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
10	313.02	8.95	0.94	32.37	10	366.02	1.87	0.19	0.00
10	314.02	8.95	0.09	40.44	10	367.02	1.87	0.14	0.00
10	315.02	8.95	0.05	41.35	10	368.02	1.87	0.19	0.00
10	316.02	9.10	0.04	43.62	10	369.02	1.87	0.16	0.00
10	317.02	2.50	0.04	0.00	10	370.02	1.87	0.22	0.00
10	318.02	8.90	0.01	42.19	10	371.02	1.87	0.22	0.00
10	319.02	2.50	0.02	0.01	10	372.02	1.87	0.22	0.00
10	320.02	2.41	0.00	0.01	10	373.02	1.87	0.23	0.00
10	321.02	9.11	0.02	44.59	10	374.02	1.87	0.22	0.00
10	322.02	8.91	0.08	47.72	10	375.02	1.87	0.23	0.00
10	323.02	2.00	0.28	0.06	10	376.02	1.87	0.23	0.00
10	324.02	9.09	0.03	43.84	10	377.02	1.87	0.29	0.02
10	325.02	8.93	0.01	45.58	10	378.02	1.87	0.22	0.00
10	326.02	2.00	0.18	0.02	10	379.02	1.87	0.26	0.01
10	328.02	9.07	0.04	43.32	10	380.02	1.87	0.26	0.01
10	331.02	2.49	0.05	0.00	10	381.02	1.78	0.25	0.00
10	332.02	2.49	0.04	0.00	10	382.02	1.82	0.26	0.00
10	333.02	2.49	0.04	0.00	10	383.02	1.78	0.26	0.00
10	334.02	2.49	0.01	0.10	10	384.02	1.78	0.24	0.00
10	335.02	2.00	0.08	0.00	10	385.02	1.78	0.23	0.00
10	336.02	2.49	0.04	0.16	10	386.02	1.78	0.24	0.00
10	337.02	2.49	0.01	0.09	10	387.02	1.78	0.23	0.00
10	338.02	2.49	0.04	0.16	10	388.02	1.78	0.20	0.00
10	339.02	2.49	0.04	0.17	10	389.02	1.81	0.21	0.00
10	340.02	2.00	0.06	0.00	10	390.02	1.83	0.23	0.00
10	341.02	8.99	0.06	48.06	10	391.02	1.83	0.23	0.00
10	342.02	2.05	0.07	0.00	10	392.02	1.83	0.22	0.00
10	343.02	2.05	0.09	0.01	10	393.02	1.83	0.21	0.00
10	344.02	2.26	0.06	0.04	10	394.02	1.83	0.22	0.00
10	345.02	2.05	0.04	0.00	10	395.02	1.83	0.21	0.00
10	346.02	2.02	0.11	0.00	10	396.02	1.85	0.23	0.00
10	347.02	2.08	0.05	0.00	10	397.02	1.81	0.22	0.00
10	348.02	2.08	0.06	0.00	10	398.02	1.81	0.22	0.00
10	349.02	2.08	0.07	0.00	10	399.02	1.81	0.21	0.00
10	350.02	2.07	0.04	0.00	10	400.02	1.81	0.21	0.00
10	351.02	2.08	0.08	0.01	10	401.02	1.81	0.22	0.00
10	352.02	2.08	0.09	0.01	10	402.02	1.81	0.21	0.00
10	353.02	2.08	0.09	0.01	10	403.02	1.81	0.21	0.00
10	354.02	2.08	0.11	0.01	10	404.02	1.81	0.22	0.00
10	355.02	2.08	0.09	0.01	10	405.02	1.81	0.21	0.00
10	356.02	2.00	0.10	0.00	10	406.02	1.81	0.19	0.00
10	357.02	1.97	0.10	0.00	10	407.02	1.81	0.19	0.00
10	358.02	1.97	0.10	0.00	10	408.02	1.81	0.19	0.00
10	359.02	1.97	0.11	0.00	10	409.02	1.83	0.19	0.00
10	360.02	2.08	0.09	0.01	10	410.02	1.88	0.20	0.00
10	361.02	1.84	0.11	0.01	10	411.02	1.84	0.20	0.00
10	362.02	1.95	0.18	0.01	10	412.02	1.84	0.21	0.00
10	363.02	1.99	0.11	0.00	10	413.02	1.84	0.19	0.00
10	364.02	1.98	0.18	0.01	10	414.02	1.83	0.22	0.00
10	365.02	1.86	0.18	0.00	10	415.02	1.82	0.20	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
10	416.02	1.82	0.19	0.00	10	390.03	10.95	74.30	0.00
10	417.02	1.82	0.14	0.01	10	391.03	10.66	72.42	0.02
10	418.02	1.82	0.14	0.01	10	392.03	10.91	74.40	0.00
10	419.02	1.72	0.15	0.03	10	393.03	10.75	72.42	0.00
10	422.02	1.84	0.07	0.03	10	394.03	10.80	61.50	0.45
10	423.02	2.03	0.08	0.00	10	395.03	10.80	61.01	0.49
10	424.02	2.03	0.08	0.00	10	396.03	10.80	59.97	0.59
10	425.02	1.93	0.10	0.00	10	397.03	10.80	60.57	0.53
10	426.02	1.98	0.10	0.00	10	398.03	10.80	49.39	2.20
10	427.02	1.98	0.06	0.00	10	399.03	10.84	1.70	52.59
10	428.02	1.98	0.13	0.00	10	400.03	3.59	1.59	0.00
10	429.02	1.98	0.09	0.00	10	401.03	3.59	1.54	0.00
10	430.02	1.63	2.55	0.88	10	402.03	3.59	0.02	2.13
10	431.02	1.94	2.56	1.56	10	403.03	3.59	0.20	3.07
10	432.02	.			10	404.03	3.59	0.21	3.10
10	273.03	1.04	1.13	0.04	10	405.03	3.59	0.21	3.11
10	276.03	1.26	1.22	0.01	10	406.03	3.59	0.23	3.18
10	296.03	1.38	0.81	0.00	10	407.03	3.59	0.21	3.10
10	297.03	1.81	0.64	0.10	10	408.03	3.59	0.21	3.09
10	299.03	1.39	0.88	0.00	10	409.03	3.45	0.20	2.59
10	300.03	1.25	0.81	0.02	10	410.03	1.81	0.20	0.00
10	306.03	1.42	0.75	0.00	10	411.03	1.84	0.20	0.00
10	307.03	1.59	0.67	0.02	10	412.03	1.84	0.18	0.00
10	308.03	1.46	0.77	0.00	10	413.03	1.84	0.19	0.00
10	309.03	1.68	0.65	0.04	10	414.03	1.79	0.16	0.01
10	311.03	1.50	0.59	0.00	10	415.03	1.89	0.16	0.00
10	320.03	1.51	38.52	48.84	10	416.03	1.89	0.14	0.00
10	322.03	1.55	42.69	52.84	10	417.03	1.89	0.14	0.00
10	333.03	1.78	42.58	49.51	10	418.03	1.89	0.13	0.00
10	339.03	8.99	49.71	0.12	10	419.03	1.89	0.14	0.00
10	340.03	9.34	49.32	0.00	10	422.03	1.85	0.14	0.00
10	341.03	9.34	49.39	0.00	10	423.03	1.91	0.15	0.00
10	342.03	9.34	49.05	0.00	10	424.03	1.91	0.16	0.00
10	346.03	9.37	50.40	0.00	10	426.03	2.02	0.11	0.00
10	348.03	9.56	52.18	0.00	10	429.03	2.07	0.06	0.00
10	354.03	9.49	53.58	0.01	11	1	1.08	2.26	0.09
10	356.03	9.69	56.87	0.02	11	2	0.92	2.23	0.02
10	357.03	9.57	54.96	0.02	11	3	0.93	1.99	0.00
10	358.03	9.70	54.95	0.00	11	4	0.88	2.08	0.00
10	360.03	9.68	52.30	0.02	11	5	0.93	2.53	0.05
10	365.03	10.14	59.96	0.01	11	6	0.75	2.56	0.00
10	379.03	9.75	69.07	0.72	11	7	0.78	2.00	0.01
10	381.03	10.66	71.10	0.00	11	8	0.87	2.08	0.00
10	382.03	10.77	70.53	0.01	11	9	0.87	2.12	0.00
10	383.03	10.69	71.04	0.00	11	10	0.87	2.14	0.00
10	384.03	10.65	69.91	0.00	11	11	0.87	2.13	0.00
10	385.03	10.89	71.12	0.03	11	13	0.90	1.77	0.00
10	386.03	10.71	70.71	0.00	11	16	1.00	1.77	0.00
10	388.03	10.94	73.96	0.00	11	17	0.98	2.09	0.02
10	389.03	10.66	71.87	0.01	11	18	0.87	2.02	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
11	19	0.90	1.84	0.00	11	78	1.54	0.67	0.01
11	21	0.93	1.84	0.00	11	79	1.47	0.62	0.00
11	22	1.14	1.48	0.00	11	80	1.47	0.70	0.00
11	23	0.91	1.65	0.01	11	81	1.47	0.64	0.00
11	24	1.07	1.47	0.00	11	82	1.47	0.72	0.00
11	25	0.98	1.65	0.00	11	83	1.47	0.88	0.01
11	26	1.00	1.62	0.00	11	84	1.47	0.84	0.01
11	27	1.00	1.66	0.00	11	85	1.44	0.95	0.02
11	28	1.07	1.81	0.02	11	86	1.32	1.01	0.00
11	29	1.06	1.83	0.02	11	87	1.32	0.86	0.00
11	30	0.94	1.84	0.00	11	88	1.33	1.05	0.00
11	31	1.00	1.87	0.01	11	89	1.23	1.08	0.00
11	32	0.99	1.68	0.00	11	90	1.25	1.10	0.00
11	33	0.99	1.66	0.00	11	91	1.41	0.77	0.00
11	34	1.05	1.60	0.00	11	92	1.41	0.74	0.00
11	35	1.08	1.50	0.00	11	93	1.25	0.96	0.00
11	36	1.11	1.59	0.01	11	94	1.41	0.93	0.01
11	37	1.03	1.52	0.00	11	95	1.31	0.90	0.00
11	38	0.99	1.60	0.00	11	96	1.31	0.96	0.00
11	40	0.99	1.57	0.00	11	97	1.31	0.97	0.00
11	42	1.16	1.24	0.00	11	98	1.31	0.98	0.00
11	43	1.19	1.03	0.01	11	99	1.31	0.96	0.00
11	46	1.17	1.04	0.01	11	100	1.31	0.92	0.00
11	47	0.99	1.12	0.06	11	101	1.31	0.95	0.00
11	48	1.22	1.06	0.00	11	102	1.31	0.92	0.00
11	49	1.05	1.13	0.03	11	103	1.27	0.93	0.00
11	50	1.20	1.10	0.00	11	104	1.32	0.91	0.00
11	51	1.24	1.11	0.00	11	105	1.50	0.80	0.01
11	55	1.19	1.02	0.01	11	106	1.33	0.90	0.00
11	56	1.43	0.64	0.00	11	107	1.33	0.91	0.00
11	58	1.27	0.62	0.05	11	108	1.33	0.88	0.00
11	59	1.28	0.89	0.00	11	109	1.33	0.88	0.00
11	60	1.50	0.62	0.00	11	110	1.33	0.80	0.00
11	61	1.28	0.84	0.01	11	111	1.33	0.84	0.00
11	62	1.50	0.59	0.00	11	112	1.33	0.78	0.01
11	63	1.50	0.69	0.00	11	113	1.33	0.80	0.00
11	64	1.55	0.77	0.02	11	114	1.33	0.77	0.01
11	65	1.41	0.76	0.00	11	115	1.33	0.75	0.01
11	66	1.41	0.73	0.00	11	116	1.33	0.71	0.01
11	67	1.41	0.74	0.00	11	117	1.29	0.77	0.01
11	68	1.38	0.77	0.00	11	118	1.57	0.66	0.01
11	69	1.66	0.68	0.04	11	119	1.34	0.74	0.01
11	70	1.47	0.70	0.00	11	120	1.45	0.70	0.00
11	71	1.45	0.73	0.00	11	121	1.45	0.73	0.00
11	72	1.45	0.74	0.00	11	122	1.45	0.66	0.00
11	73	1.45	0.74	0.00	11	123	1.45	0.70	0.00
11	74	1.45	0.70	0.00	11	124	1.45	0.64	0.00
11	75	1.48	0.71	0.00	11	125	1.45	0.65	0.00
11	76	1.46	0.67	0.00	11	126	1.40	0.68	0.00
11	77	1.49	0.68	0.00	11	127	1.64	0.60	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
11	128	1.48	0.63	0.00	11	179	1.50	0.60	0.00
11	129	1.47	0.65	0.00	11	180	1.51	0.70	0.00
11	130	1.69	0.55	0.02	11	181	1.45	0.69	0.00
11	131	1.53	0.61	0.00	11	182	1.40	0.67	0.00
11	132	1.52	0.44	0.01	11	183	1.47	0.67	0.00
11	133	1.62	0.56	0.01	11	184	1.53	0.60	0.00
11	134	1.62	0.46	0.00	11	185	1.49	0.58	0.00
11	135	1.68	0.37	0.00	11	186	1.53	0.63	0.00
11	136	1.62	0.37	0.00	11	187	1.53	0.69	0.00
11	137	1.68	0.43	0.00	11	188	1.53	0.62	0.00
11	138	1.65	0.40	0.00	11	189	1.51	0.68	0.00
11	139	1.66	0.37	0.00	11	190	1.46	0.63	0.00
11	140	1.66	0.40	0.00	11	191	1.46	0.78	0.00
11	141	1.66	0.40	0.00	11	192	1.46	0.81	0.00
11	142	1.66	0.43	0.00	11	193	1.39	0.76	0.00
11	143	1.66	0.45	0.00	11	194	1.39	0.79	0.00
11	144	1.69	0.49	0.01	11	195	1.39	0.90	0.00
11	145	1.56	0.51	0.00	11	196	1.39	0.88	0.00
11	146	1.55	0.50	0.00	11	197	1.39	0.83	0.00
11	147	1.58	0.48	0.00	11	198	1.41	0.77	0.00
11	148	1.58	0.55	0.00	11	199	1.41	0.79	0.00
11	149	1.59	0.54	0.00	11	200	1.41	0.85	0.00
11	150	1.59	0.58	0.00	11	201	1.41	0.87	0.00
11	151	1.53	0.58	0.00	11	202	1.40	0.83	0.00
11	152	1.50	0.56	0.00	11	203	1.38	0.83	0.00
11	154	1.55	0.52	0.00	11	204	1.38	0.81	0.00
11	155	1.57	0.52	0.00	11	205	1.38	0.80	0.00
11	156	1.57	0.54	0.00	11	206	1.35	0.87	0.00
11	157	1.57	0.52	0.00	11	207	1.52	0.73	0.01
11	158	1.57	0.47	0.00	11	208	1.40	0.81	0.00
11	159	1.57	0.47	0.00	11	209	1.28	0.99	0.00
11	160	1.57	0.52	0.00	11	210	1.60	0.77	0.04
11	161	1.57	0.52	0.00	11	211	1.41	0.70	0.00
11	162	1.57	0.55	0.00	11	212	1.40	0.83	0.00
11	163	1.57	0.56	0.00	11	213	1.46	0.80	0.00
11	164	1.57	0.57	0.00	11	214	1.39	0.87	0.00
11	165	1.57	0.55	0.00	11	215	1.39	0.90	0.00
11	166	1.57	0.60	0.00	11	216	1.39	0.93	0.00
11	167	1.54	0.58	0.00	11	217	1.42	0.91	0.01
11	168	1.51	0.70	0.00	11	218	1.37	0.82	0.00
11	169	1.72	0.61	0.05	11	219	1.41	0.84	0.00
11	170	1.46	0.73	0.00	11	220	1.37	0.86	0.00
11	171	1.44	0.70	0.00	11	221	1.41	0.93	0.01
11	172	1.54	0.68	0.01	11	222	1.32	0.97	0.00
11	173	1.44	0.66	0.00	11	223	1.32	1.00	0.00
11	174	1.37	1.04	0.01	11	224	1.32	1.02	0.00
11	175	1.66	0.64	0.03	11	225	1.36	1.06	0.01
11	176	1.49	0.55	0.00	11	226	1.30	1.06	0.00
11	177	1.40	0.69	0.00	11	227	1.34	0.99	0.00
11	178	1.66	0.55	0.01	11	228	1.29	1.04	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
11	229	1.32	0.95	0.00	11	280	1.35	0.99	0.00
11	230	1.31	0.99	0.00	11	281	1.29	0.99	0.00
11	231	1.32	1.00	0.00	11	282	1.36	1.01	0.01
11	232	1.31	1.02	0.00	11	283	1.49	0.94	0.03
11	233	1.28	1.06	0.00	11	284	1.32	0.93	0.00
11	234	1.36	1.07	0.01	11	285	1.37	0.88	0.00
11	235	1.26	1.11	0.00	11	286	1.35	0.93	0.00
11	236	1.26	1.12	0.00	11	287	1.35	0.95	0.00
11	237	1.26	1.11	0.00	11	288	1.35	0.97	0.00
11	238	1.26	1.13	0.00	11	289	1.35	1.00	0.00
11	239	1.26	1.16	0.00	11	290	1.35	1.02	0.01
11	240	1.28	1.17	0.01	11	291	1.40	1.04	0.02
11	241	1.21	1.06	0.00	11	292	1.29	0.96	0.00
11	242	1.21	1.13	0.00	11	293	1.31	0.98	0.00
11	243	1.21	1.05	0.00	11	294	1.31	1.02	0.00
11	244	1.21	1.09	0.00	11	295	1.33	0.97	0.00
11	245	1.21	1.13	0.00	11	296	1.34	0.99	0.00
11	246	1.14	1.05	0.01	11	297	1.30	1.00	0.00
11	247	1.26	1.02	0.00	11	298	1.38	0.96	0.00
11	248	1.26	1.03	0.00	11	299	1.31	0.94	0.00
11	249	1.26	1.05	0.00	11	300	1.31	0.91	0.00
11	250	1.26	1.06	0.00	11	301	1.31	0.74	0.01
11	251	1.35	1.01	0.00	11	302	1.31	0.74	0.01
11	252	1.31	1.06	0.00	11	303	1.29	0.76	0.02
11	253	1.23	1.15	0.00	11	304	1.42	0.75	0.00
11	254	1.19	1.03	0.01	11	305	1.42	0.77	0.00
11	255	1.28	1.09	0.00	11	306	1.41	0.71	0.00
11	256	1.28	1.09	0.00	11	307	1.43	0.76	0.00
11	257	1.31	1.16	0.01	11	308	1.42	0.68	0.00
11	258	1.23	1.18	0.00	11	309	1.47	0.69	0.00
11	259	1.18	1.18	0.00	11	310	1.53	0.55	0.00
11	260	1.22	1.09	0.00	11	311	1.55	0.59	0.00
11	261	1.24	1.18	0.00	11	312	1.55	0.61	0.00
11	263	1.26	1.04	0.00	11	313	1.53	0.55	0.00
11	264	1.27	1.07	0.00	11	314	1.55	0.57	0.00
11	265	1.27	1.09	0.00	11	315	1.55	0.57	0.00
11	266	1.28	1.07	0.00	11	316	1.55	0.60	0.00
11	267	1.26	1.09	0.00	11	317	1.56	0.56	0.00
11	268	1.26	1.02	0.00	11	318	1.54	0.58	0.00
11	269	1.26	1.05	0.00	11	319	1.60	0.51	0.00
11	270	1.26	1.06	0.00	11	320	1.55	0.57	0.00
11	271	1.26	1.09	0.00	11	321	1.52	0.46	0.01
11	272	1.33	1.08	0.01	11	322	1.61	0.52	0.00
11	273	1.34	1.05	0.01	11	323	1.61	0.53	0.00
11	274	1.27	1.10	0.00	11	324	1.66	0.50	0.01
11	275	1.24	1.01	0.00	11	325	1.58	0.53	0.00
11	276	1.28	1.02	0.00	11	326	1.63	0.49	0.00
11	277	1.28	1.00	0.00	11	327	1.59	0.47	0.00
11	278	1.31	1.02	0.00	11	328	1.59	0.50	0.00
11	279	1.08	1.89	0.03	11	329	1.59	0.53	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
11	330	1.56	0.46	0.00	11	73.01	1.61	0.24	0.04
11	331	1.61	0.48	0.00	11	74.01	1.80	0.30	0.00
11	332	1.61	0.44	0.00	11	75.01	1.78	0.35	0.01
11	333	1.63	0.46	0.00	11	76.01	1.94	0.34	0.06
11	334	1.63	0.49	0.00	11	78.01	1.95	0.17	0.01
11	335	1.63	0.50	0.00	11	83.01	1.76	0.09	0.06
11	336	1.63	0.54	0.01	11	84.01	1.99	0.08	0.00
11	337	1.63	0.53	0.00	11	85.01	2.00	0.09	0.00
11	338	1.54	0.55	0.00	11	86.01	2.00	0.07	0.00
11	339	1.42	1.18	0.05	11	87.01	2.01	0.09	0.00
11	340	1.20	1.34	0.00	11	89.01	1.98	0.02	0.02
11	341	1.15	1.35	0.00	11	90.01	2.13	0.03	0.00
11	342	1.21	1.33	0.01	11	95.01	2.13	0.02	0.00
11	343	1.14	1.34	0.00	11	99.01	2.06	0.03	0.17
11	344	1.16	1.40	0.00	11	100.01	2.13	0.00	0.03
11	345	1.18	1.40	0.00	11	102.01	2.64	0.03	0.03
11	346	1.17	1.48	0.01	11	103.01	2.45	0.04	0.00
11	347	1.13	1.42	0.00	11	104.01	2.48	0.04	0.00
11	348	1.14	1.01	0.02	11	105.01	2.63	0.08	0.00
11	349	1.36	0.97	0.00	11	108.01	2.48	0.04	0.00
11	350	1.35	0.91	0.00	11	109.01	2.48	0.02	0.00
11	351	1.37	0.82	0.00	11	112.01	2.44	0.11	0.03
11	352	1.38	0.88	0.00	11	113.01	2.63	0.21	0.01
11	353	1.38	0.92	0.00	11	114.01	2.44	0.07	0.01
11	354	1.38	0.97	0.01	11	119.01	2.44	0.19	0.08
11	356	1.25	1.13	0.00	11	120.01	2.63	0.33	0.05
11	357	1.23	1.07	0.00	11	121.01	2.52	0.21	0.06
11	358	1.28	1.53	0.05	11	122.01	2.75	0.21	0.00
11	359	1.05	1.64	0.00	11	123.01	2.77	0.20	0.00
11	360	0.97	0.35	0.53	11	125.01	2.77	0.20	0.00
11	361	1.50	0.17	0.14	11	126.01	2.94	0.27	0.02
11	16.01	1.08	2.29	0.09	11	127.01	2.73	0.14	0.00
11	27.01	0.81	1.64	0.04	11	129.01	2.98	0.31	0.02
11	28.01	1.08	1.54	0.00	11	130.01	2.69	0.26	0.01
11	29.01	0.92	1.54	0.02	11	132.01	2.86	0.25	0.01
11	30.01	1.26	1.41	0.03	11	135.01	2.82	0.34	0.00
11	32.01	1.07	1.34	0.00	11	136.01	3.18	0.89	0.00
11	33.01	1.13	1.35	0.00	11	139.01	3.01	0.43	0.00
11	37.01	1.11	1.18	0.01	11	142.01	3.10	0.49	0.01
11	38.01	1.27	1.03	0.00	11	144.01	2.92	0.56	0.01
11	40.01	1.30	1.02	0.00	11	145.01	3.04	0.62	0.00
11	46.01	1.49	0.88	0.02	11	149.01	3.06	0.78	0.01
11	50.01	1.42	0.81	0.00	11	150.01	3.17	0.80	0.00
11	51.01	1.39	0.82	0.00	11	151.01	3.17	0.74	0.00
11	55.01	1.54	0.69	0.01	11	154.01	3.26	0.81	0.01
11	59.01	1.46	0.67	0.00	11	155.01	3.03	0.95	0.05
11	61.01	1.67	0.69	0.05	11	156.01	3.26	0.91	0.00
11	63.01	1.44	0.90	0.01	11	157.01	3.26	0.87	0.00
11	65.01	1.60	0.54	0.00	11	160.01	3.39	1.01	0.01
11	68.01	1.54	0.65	0.00	11	161.01	3.25	0.38	0.12

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
11	162.01	3.49	0.51	0.24	11	223.01	2.16	0.02	0.00
11	163.01	3.26	0.04	0.62	11	224.01	2.16	0.03	0.00
11	164.01	3.54	0.07	0.98	11	225.01	2.12	0.04	0.00
11	168.01	3.49	0.50	0.24	11	226.01	2.09	0.05	0.00
11	169.01	3.27	0.39	0.12	11	227.01	2.10	0.06	0.00
11	170.01	3.24	0.29	0.17	11	228.01	2.05	0.06	0.00
11	175.01	3.44	0.72	0.09	11	229.01	2.01	0.06	0.00
11	176.01	2.83	0.50	0.03	11	230.01	2.05	0.07	0.00
11	177.01	2.83	0.61	0.06	11	231.01	2.01	0.07	0.00
11	178.01	3.14	0.63	0.00	11	232.01	1.99	0.01	0.03
11	179.01	3.34	0.59	0.08	11	233.01	2.17	0.02	0.00
11	180.01	3.00	0.63	0.01	11	234.01	2.21	0.02	0.01
11	181.01	3.25	0.74	0.01	11	235.01	2.14	0.02	0.00
11	182.01	3.07	0.72	0.00	11	236.01	2.14	0.03	0.00
11	184.01	3.11	0.70	0.00	11	237.01	2.14	0.03	0.00
11	185.01	3.29	0.68	0.03	11	238.01	2.14	0.03	0.00
11	187.01	3.35	0.49	0.13	11	239.01	2.14	0.04	0.00
11	188.01	2.99	0.43	0.00	11	240.01	2.13	0.04	0.00
11	189.01	2.99	0.33	0.02	11	241.01	2.13	0.03	0.00
11	190.01	2.99	0.30	0.02	11	242.01	2.13	0.03	0.00
11	191.01	2.99	0.29	0.02	11	243.01	2.13	0.05	0.00
11	192.01	2.99	0.17	0.08	11	244.01	2.13	0.04	0.00
11	193.01	2.99	0.20	0.06	11	245.01	2.13	0.04	0.00
11	194.01	2.99	0.03	0.27	11	246.01	2.13	0.05	0.00
11	195.01	2.99	0.06	0.20	11	247.01	2.13	0.05	0.00
11	196.01	2.99	0.05	0.23	11	248.01	2.13	0.04	0.00
11	197.01	2.99	0.04	0.25	11	249.01	2.13	0.08	0.02
11	199.01	3.15	0.05	0.40	11	250.01	2.13	0.03	0.00
11	200.01	2.52	0.04	0.00	11	251.01	2.13	0.09	0.02
11	202.01	2.52	0.03	0.01	11	252.01	2.09	0.08	0.01
11	203.01	2.45	0.03	0.00	11	253.01	1.86	0.15	0.00
11	204.01	2.45	0.02	0.00	11	254.01	2.40	0.08	0.16
11	205.01	2.45	0.02	0.00	11	255.01	2.04	0.13	0.01
11	206.01	2.67	0.03	0.05	11	256.01	1.96	0.15	0.00
11	207.01	2.36	0.00	0.01	11	257.01	1.90	0.17	0.00
11	208.01	2.45	0.03	0.00	11	258.01	1.88	0.31	0.02
11	209.01	2.51	0.00	0.05	11	259.01	1.75	0.34	0.00
11	210.01	2.48	0.00	0.03	11	260.01	1.68	0.39	0.00
11	211.01	2.21	0.05	0.02	11	261.01	1.68	0.51	0.01
11	212.01	2.29	0.00	0.00	11	263.01	1.56	0.52	0.00
11	213.01	2.34	0.02	0.03	11	264.01	1.57	0.51	0.00
11	214.01	2.15	0.02	0.00	11	265.01	1.61	0.51	0.00
11	215.01	2.15	0.02	0.00	11	266.01	1.58	0.48	0.00
11	216.01	2.15	0.02	0.00	11	267.01	1.58	0.51	0.00
11	217.01	2.15	0.02	0.00	11	268.01	1.58	0.53	0.00
11	218.01	2.12	0.03	0.00	11	269.01	1.58	0.54	0.00
11	219.01	2.09	0.02	0.00	11	270.01	1.58	0.54	0.00
11	220.01	2.14	0.02	0.00	11	271.01	1.58	0.53	0.00
11	221.01	2.11	0.02	0.00	11	272.01	1.58	0.54	0.00
11	222.01	2.16	0.02	0.00	11	273.01	1.64	0.55	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
11	274.01	1.53	0.49	0.00	11	324.01	1.67	0.43	0.00
11	275.01	1.56	0.50	0.00	11	325.01	1.64	0.42	0.00
11	276.01	1.59	0.53	0.00	11	326.01	1.68	0.39	0.00
11	277.01	1.57	0.54	0.00	11	327.01	1.66	0.46	0.00
11	278.01	1.56	0.53	0.00	11	328.01	1.66	0.45	0.00
11	279.01	1.36	2.41	0.39	11	329.01	1.66	0.42	0.00
11	280.01	1.56	0.56	0.00	11	330.01	1.65	0.43	0.00
11	281.01	1.56	0.56	0.00	11	331.01	1.63	0.43	0.00
11	282.01	1.56	0.55	0.00	11	332.01	1.63	0.42	0.00
11	283.01	1.56	0.55	0.00	11	333.01	1.63	0.42	0.00
11	284.01	1.56	0.57	0.00	11	334.01	1.63	0.41	0.00
11	285.01	1.62	0.55	0.00	11	335.01	1.61	0.42	0.00
11	286.01	1.55	0.54	0.00	11	336.01	1.64	0.39	0.00
11	287.01	1.55	0.53	0.00	11	337.01	1.66	0.37	0.00
11	288.01	1.55	0.53	0.00	11	338.01	1.65	0.37	0.00
11	289.01	1.55	0.51	0.00	11	339.01	1.68	0.06	0.14
11	290.01	1.55	0.50	0.00	11	340.01	1.68	0.04	0.16
11	291.01	1.77	0.53	0.04	11	341.01	1.68	0.03	0.18
11	292.01	1.55	0.50	0.00	11	342.01	1.68	0.04	0.17
11	293.01	1.58	0.50	0.00	11	343.01	1.68	0.05	0.15
11	294.01	1.58	0.48	0.00	11	344.01	1.65	0.05	0.17
11	295.01	1.58	0.48	0.00	11	345.01	2.07	0.04	0.00
11	296.01	1.62	0.51	0.00	11	346.01	2.07	0.03	0.00
11	297.01	1.58	0.51	0.00	11	347.01	2.07	0.02	0.00
11	298.01	1.63	0.53	0.01	11	348.01	2.03	0.02	0.01
11	299.01	1.56	0.54	0.00	11	349.01	2.13	0.02	0.00
11	300.01	1.56	0.54	0.00	11	350.01	2.10	0.03	0.00
11	301.01	1.56	0.55	0.00	11	351.01	2.11	0.03	0.00
11	302.01	1.56	0.54	0.00	11	352.01	2.11	0.03	0.00
11	303.01	1.51	0.53	0.00	11	353.01	2.11	0.03	0.00
11	304.01	1.56	0.53	0.00	11	354.01	2.10	0.03	0.00
11	305.01	1.57	0.53	0.00	11	356.01	1.93	0.99	0.40
11	306.01	1.54	0.56	0.00	11	357.01	1.29	1.03	0.00
11	307.01	1.49	0.56	0.00	11	358.01	1.34	1.55	0.09
11	308.01	1.54	0.59	0.00	11	359.01	1.04	1.43	0.00
11	309.01	1.54	0.58	0.00	11	360.01	0.92	0.52	0.42
11	310.01	1.60	0.56	0.00	11	361.01	1.38	2.51	0.46
11	311.01	1.54	0.53	0.00	11	63.02	1.04	1.24	0.02
11	312.01	1.54	0.54	0.00	11	78.02	1.33	1.11	0.01
11	313.01	1.54	0.53	0.00	11	89.02	1.23	0.84	0.02
11	314.01	1.56	0.52	0.00	11	90.02	1.64	0.63	0.02
11	315.01	1.56	0.53	0.00	11	95.02	1.27	0.76	0.02
11	316.01	1.56	0.51	0.00	11	100.02	1.45	0.81	0.00
11	317.01	1.56	0.49	0.00	11	121.02	1.45	0.26	0.11
11	318.01	1.56	0.50	0.00	11	122.02	1.78	0.29	0.00
11	319.01	1.52	0.60	0.00	11	123.02	1.77	0.32	0.00
11	320.01	1.75	0.44	0.01	11	126.02	2.22	0.18	0.12
11	321.01	1.52	0.45	0.01	11	142.02	1.84	0.01	0.13
11	322.01	1.62	0.41	0.00	11	144.02	2.20	0.00	0.00
11	323.01	1.62	0.43	0.00	11	145.02	2.38	0.02	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
11	157.02	2.35	0.09	0.06	11	287.02	3.40	1.35	0.00
11	163.02	2.58	1.41	0.81	11	288.02	3.40	1.31	0.00
11	168.02	2.61	1.25	0.63	11	289.02	3.40	1.41	0.01
11	169.02	2.82	1.49	0.47	11	290.02	3.40	1.27	0.00
11	176.02	2.85	2.04	0.76	11	291.02	3.40	1.13	0.00
11	184.02	3.92	2.59	0.00	11	292.02	3.24	0.64	0.02
11	185.02	2.77	2.64	1.32	11	293.02	3.09	0.42	0.02
11	187.02	3.98	3.36	0.02	11	294.02	3.09	0.40	0.03
11	188.02	4.15	3.38	0.00	11	295.02	2.95	0.00	0.36
11	194.02	4.15	7.07	0.63	11	296.02	2.25	0.01	0.02
11	197.02	4.97	7.52	0.00	11	297.02	2.38	0.02	0.00
11	206.02	5.05	10.07	0.17	11	298.02	2.35	0.01	0.00
11	213.02	5.48	12.98	0.17	11	299.02	2.55	0.03	0.01
11	216.02	5.90	15.78	0.13	11	300.02	2.38	0.02	0.00
11	217.02	6.10	16.84	0.08	11	301.02	2.42	0.03	0.00
11	219.02	5.90	16.85	0.24	11	302.02	2.42	0.03	0.00
11	221.02	6.05	17.70	0.20	11	303.02	2.42	0.04	0.01
11	222.02	6.50	18.04	0.00	11	304.02	2.44	0.03	0.00
11	225.02	6.55	19.83	0.04	11	305.02	2.68	0.08	0.01
11	226.02	6.80	20.01	0.00	11	306.02	2.34	0.03	0.02
11	227.02	6.82	20.14	0.00	11	307.02	2.60	0.08	0.00
11	233.02	6.95	24.44	0.08	11	308.02	2.48	0.04	0.00
11	234.02	6.38	24.72	0.78	11	309.02	2.38	0.01	0.00
11	235.02	7.26	24.93	0.00	11	310.02	2.70	0.10	0.01
11	242.02	7.31	28.28	0.09	11	311.02	2.51	0.03	0.00
11	243.02	7.61	28.26	0.00	11	312.02	2.47	0.05	0.00
11	244.02	7.61	27.95	0.00	11	313.02	2.37	0.04	0.01
11	245.02	7.81	29.12	0.02	11	314.02	2.48	0.04	0.00
11	248.02	7.58	26.63	0.02	11	315.02	2.48	0.02	0.00
11	251.02	7.58	24.89	0.09	11	316.02	2.48	0.28	0.52
11	252.02	7.81	32.32	0.03	11	317.02	2.48	0.37	0.64
11	255.02	7.85	34.37	0.09	11	318.02	2.48	0.39	0.66
11	256.02	7.74	35.10	0.22	11	319.02	2.71	0.31	0.94
11	257.02	8.27	32.76	0.07	11	320.02	2.35	0.40	0.48
11	258.02	7.46	32.06	0.25	11	321.02	2.49	0.42	0.72
11	265.02	7.40	37.74	1.07	11	322.02	1.65	0.50	0.01
11	267.02	8.40	37.50	0.00	11	323.02	1.58	0.53	0.00
11	268.02	8.63	38.14	0.03	11	324.02	1.63	0.54	0.01
11	270.02	8.59	38.13	0.02	11	325.02	1.55	0.56	0.00
11	272.02	8.63	38.40	0.02	11	326.02	1.55	0.58	0.00
11	273.02	8.49	38.24	0.00	11	327.02	1.55	0.59	0.00
11	278.02	7.89	1.21	20.21	11	328.02	1.55	0.60	0.00
11	279.02	2.29	2.56	2.56	11	329.02	1.55	0.61	0.00
11	280.02	3.39	1.22	0.00	11	330.02	1.52	0.60	0.00
11	281.02	3.39	1.24	0.00	11	331.02	1.52	0.62	0.00
11	282.02	3.39	1.21	0.00	11	332.02	1.52	0.63	0.00
11	283.02	3.39	1.20	0.00	11	333.02	1.52	0.65	0.00
11	284.02	3.39	1.15	0.00	11	334.02	1.52	0.66	0.00
11	285.02	3.24	1.24	0.03	11	335.02	1.44	0.69	0.00
11	286.02	3.40	1.33	0.00	11	336.02	1.46	0.71	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
11	337.02	1.48	0.73	0.00	11	326.03	11.13	77.25	0.00
11	338.02	1.43	0.69	0.00	11	327.03	11.05	77.25	0.00
11	339.02	1.46	0.70	0.00	11	332.03	11.08	77.62	0.00
11	340.02	1.46	0.66	0.00	11	333.03	11.28	82.46	0.01
11	341.02	1.46	0.68	0.00	11	334.03	11.37	83.17	0.00
11	342.02	1.46	0.65	0.00	11	337.03	10.25	85.70	1.68
11	343.02	1.46	0.60	0.00	11	338.03	11.38	35.42	9.87
11	344.02	1.45	0.62	0.00	11	342.03	11.80	91.66	0.00
11	345.02	1.50	0.63	0.00	11	344.03	11.39	49.84	4.18
11	346.02	1.50	0.69	0.00	11	345.03	11.94	51.06	6.26
11	347.02	1.50	0.75	0.01	11	346.03	11.36	39.49	7.75
11	348.02	1.46	0.78	0.00	11	347.03	11.72	104.25	0.61
11	349.02	1.40	0.67	0.00	11	348.03	10.63	94.65	1.92
11	350.02	1.44	0.72	0.00	11	349.03	12.02	93.39	0.00
11	351.02	1.44	0.72	0.00	11	350.03	12.05	33.65	15.67
11	352.02	1.44	0.71	0.00	11	351.03	8.12	14.85	3.89
11	356.02	1.31	0.99	0.00	11	352.03	6.16	2.83	4.79
11	357.02	1.29	1.87	0.14	11	356.03	3.62	2.29	8.06
11	358.02	1.12	1.25	0.00	11	357.03	0.78	2.27	0.00
11	359.02	1.63	1.05	0.14	11	358.03	.		
11	360.02	1.58	0.00	0.50	11	359.03	.		
11	361.02	1.13	2.73	0.25	11	361.03	0.66	2.81	0.00
11	362.02	1.71	0.78	0.09					
11	369.02	0.58	0.38	1.20					
11	370.02	1.48	0.36	0.04					
11	371.02	1.54	0.18	0.11					
11	206.03	1.03	2.03	0.03					
11	213.03	0.97	1.98	0.01					
11	221.03	1.03	1.38	0.01					
11	222.03	1.03	1.96	0.02					
11	248.03	0.95	0.72	0.25					
11	251.03	1.59	0.21	0.06					
11	273.03	1.88	0.01	0.10					
11	285.03	2.22	28.90	29.65					
11	288.03	7.84	29.70	0.01					
11	289.03	7.74	29.53	0.00					
11	290.03	7.74	30.26	0.00					
11	293.03	7.72	37.44	0.47					
11	294.03	7.96	38.34	0.27					
11	296.03	7.72	45.64	1.76					
11	297.03	7.99	46.52	1.25					
11	298.03	7.88	46.40	1.49					
11	310.03	9.16	51.40	0.09					
11	311.03	9.60	53.19	0.00					
11	314.03	8.89	54.92	0.66					
11	317.03	9.67	67.82	0.73					
11	318.03	10.10	70.69	0.35					
11	319.03	10.70	71.02	0.00					
11	324.03	9.87	77.52	1.50					
11	325.03	11.15	77.68	0.00					

For the effective normalized descent time versus effective density, the data was divided into 0.5 persons/m^2 segments. The upper value of the segment was defined as being two standard deviations from the mean of that segment. The lower bound was the smallest recorded value in the segment.

Segment Midpoint Density (persons/m^2)	Segment Upper Bound (s/m)	Segment Lower Bound (s/m)
0.38	2.40	0.56
0.63	2.72	0.58
0.88	3.80	0.64
1.13	3.15	0.63
1.38	3.86	0.82
1.63	5.03	0.91
1.88	5.28	0.50
2.13	6.42	1.17
2.38	6.08	1.18
2.63	6.48	0.69
2.88	6.28	1.64
3.13	6.52	1.64

The equations that best fit these points are:
t=1.66*D+1.93 (upper)
t=0.35*D+0.30 (lower)

where:

t=effective normalized descent time (s/m)
D=density (persons/m^2)

The final statistical tests were to calculate the R^2 for the blind data. For the unmodified regression equations, the sum of the squares of the difference between the actual and predicted values was 145.8 and the sum of the square of the difference between the actual and average values was 1239.5. In the table, the predicted value is in s/m.

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	2	0.99	1.94	0.01	12	67	1.87	0.61	0.03
12	5	1.15	1.47	0.01	12	68	1.71	0.66	0.00
12	6	1.30	1.35	0.00	12	69	2.04	0.53	0.08
12	7	1.40	1.62	0.04	12	70	1.71	0.60	0.00
12	8	1.20	1.63	0.00	12	71	1.74	0.61	0.00
12	9	1.24	1.67	0.00	12	72	1.69	0.59	0.00
12	10	1.28	1.30	0.00	12	73	1.69	0.58	0.00
12	11	1.36	0.70	0.08	12	74	1.71	0.60	0.00
12	12	1.64	0.77	0.00	12	75	1.71	0.66	0.00
12	13	1.70	0.82	0.02	12	76	1.72	0.64	0.00
12	14	1.58	0.82	0.00	12	77	1.68	0.64	0.00
12	17	1.54	0.59	0.03	12	78	1.68	0.62	0.00
12	18	1.57	0.07	0.42	12	79	1.68	0.58	0.00
12	23	1.93	0.08	0.07	12	80	1.72	0.59	0.00
12	25	1.60	0.05	0.45	12	81	1.72	0.55	0.00
12	27	2.39	0.02	0.00	12	82	1.72	0.54	0.00
12	29	2.38	0.02	0.00	12	83	1.72	0.61	0.00
12	32	2.33	0.00	0.02	12	84	1.77	0.39	0.01
12	33	2.47	0.00	0.00	12	85	1.80	0.43	0.00
12	34	2.47	0.01	0.01	12	86	1.82	0.52	0.00
12	35	2.52	0.19	0.22	12	87	1.82	0.59	0.01
12	36	2.04	0.22	0.00	12	88	1.77	0.56	0.00
12	37	2.07	0.28	0.02	12	89	1.73	0.55	0.00
12	38	1.94	0.29	0.00	12	90	1.72	0.51	0.00
12	39	1.96	0.31	0.00	12	91	1.76	0.54	0.00
12	41	1.89	0.57	0.03	12	92	1.76	0.58	0.00
12	42	1.76	0.68	0.01	12	93	1.77	0.65	0.01
12	43	1.65	0.81	0.01	12	94	1.67	0.72	0.00
12	44	1.65	0.52	0.01	12	95	1.63	0.79	0.00
12	45	1.65	0.58	0.00	12	96	1.63	0.81	0.00
12	46	1.60	0.57	0.01	12	97	1.63	0.65	0.00
12	47	1.72	0.52	0.00	12	98	1.70	0.45	0.01
12	48	1.72	0.56	0.00	12	99	1.81	0.65	0.02
12	49	1.72	0.60	0.00	12	100	1.81	0.65	0.02
12	50	1.75	0.51	0.00	12	101	1.81	0.70	0.03
12	51	1.79	0.53	0.00	12	102	1.81	0.76	0.04
12	52	1.77	0.53	0.00	12	103	1.81	0.86	0.07
12	53	1.75	0.56	0.00	12	104	1.80	0.95	0.09
12	54	1.75	0.54	0.00	12	105	1.50	0.91	0.00
12	55	1.72	0.54	0.00	12	106	1.56	0.97	0.00
12	56	1.74	0.65	0.01	12	107	1.31	1.03	0.02
12	57	1.71	0.68	0.00	12	108	1.87	1.10	0.19
12	58	1.68	0.68	0.00	12	109	1.48	1.13	0.01
12	59	1.67	0.65	0.00	12	110	1.41	1.07	0.00
12	60	2.02	0.65	0.12	12	111	1.41	1.09	0.00
12	61	1.64	0.69	0.00	12	112	1.41	1.02	0.00
12	62	1.91	0.04	0.13	12	113	1.47	1.07	0.00
12	63	1.61	0.71	0.00	12	114	1.53	0.98	0.00
12	64	1.83	0.80	0.06	12	115	1.49	0.93	0.00
12	66	1.53	0.59	0.03	12	116	1.49	1.06	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	117	1.47	0.99	0.00	12	167	1.53	0.98	0.00
12	118	1.48	1.08	0.00	12	168	1.40	1.04	0.00
12	119	1.48	1.06	0.00	12	169	1.69	0.98	0.04
12	120	1.48	1.09	0.00	12	170	1.46	0.99	0.00
12	121	1.48	1.00	0.00	12	171	1.49	0.88	0.00
12	122	1.48	1.08	0.00	12	172	1.54	0.68	0.01
12	123	1.43	1.03	0.00	12	173	1.65	0.64	0.00
12	124	1.46	0.84	0.01	12	174	1.68	0.66	0.00
12	125	1.55	0.00	0.74	12	175	1.68	0.71	0.00
12	126	2.41	0.02	0.01	12	176	1.66	0.68	0.00
12	127	2.30	0.02	0.00	12	177	1.70	0.67	0.00
12	128	2.34	0.04	0.00	12	178	1.63	0.59	0.01
12	129	2.34	0.07	0.02	12	179	1.71	0.64	0.00
12	130	2.27	0.73	1.14	12	180	1.68	0.63	0.00
12	131	3.33	0.07	1.27	12	181	1.68	0.46	0.01
12	132	3.33	0.08	1.29	12	182	1.68	0.59	0.00
12	133	3.33	0.07	1.26	12	183	1.68	0.65	0.00
12	134	3.20	0.03	0.79	12	184	1.68	0.67	0.00
12	135	2.31	0.05	0.00	12	185	1.68	0.71	0.00
12	136	2.31	0.08	0.01	12	186	1.68	0.78	0.01
12	137	2.20	0.15	0.01	12	187	1.61	0.64	0.01
12	138	2.20	0.06	0.00	12	188	1.68	0.63	0.00
12	139	2.19	0.06	0.00	12	189	1.60	0.59	0.01
12	140	2.22	0.08	0.00	12	190	1.71	0.69	0.00
12	141	2.22	0.05	0.00	12	191	1.71	0.64	0.00
12	142	2.17	0.05	0.01	12	192	1.71	0.72	0.01
12	143	2.24	0.04	0.00	12	193	1.71	0.71	0.01
12	144	2.24	0.07	0.00	12	194	1.71	0.71	0.01
12	145	2.24	0.13	0.02	12	195	1.67	0.72	0.00
12	146	2.24	0.14	0.02	12	196	1.63	0.76	0.00
12	147	2.23	0.17	0.03	12	197	1.66	0.69	0.00
12	148	1.97	0.21	0.00	12	198	1.63	0.75	0.00
12	149	2.25	0.35	0.13	12	199	1.56	0.72	0.00
12	150	2.27	0.20	0.06	12	200	1.63	0.69	0.00
12	151	2.06	0.34	0.03	12	201	1.63	0.64	0.00
12	152	1.91	0.41	0.00	12	202	1.67	0.61	0.00
12	153	1.84	0.47	0.00	12	203	1.67	0.60	0.00
12	154	1.84	0.45	0.00	12	204	1.65	0.64	0.00
12	155	1.84	0.47	0.00	12	205	1.68	0.70	0.00
12	156	1.84	0.66	0.03	12	206	1.68	0.74	0.00
12	157	1.84	0.84	0.08	12	207	1.68	0.75	0.00
12	158	1.78	0.78	0.03	12	208	1.68	0.73	0.00
12	159	1.60	0.79	0.00	12	209	1.64	0.86	0.01
12	160	1.60	0.71	0.00	12	210	1.55	0.80	0.00
12	161	1.64	0.74	0.00	12	211	1.55	0.88	0.00
12	162	1.64	0.81	0.00	12	212	1.55	0.92	0.00
12	163	1.64	0.90	0.01	12	213	1.52	1.04	0.00
12	164	1.64	0.94	0.02	12	214	1.49	1.06	0.00
12	165	1.64	1.08	0.04	12	215	1.45	1.07	0.00
12	166	1.55	0.89	0.00	12	216	1.45	1.07	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	217	1.45	1.11	0.00	12	267	1.53	0.87	0.00
12	218	1.45	1.15	0.00	12	268	1.48	0.94	0.00
12	219	1.45	1.18	0.00	12	269	1.45	0.96	0.00
12	220	1.45	1.20	0.00	12	270	1.47	0.67	0.03
12	221	1.45	1.12	0.00	12	271	1.66	0.68	0.00
12	222	1.45	1.22	0.01	12	272	1.66	0.75	0.00
12	223	1.45	1.32	0.01	12	273	1.66	0.79	0.00
12	224	1.45	1.37	0.02	12	274	1.66	0.88	0.01
12	225	1.45	1.40	0.02	12	275	1.66	0.95	0.02
12	226	1.39	1.34	0.00	12	276	1.66	1.02	0.04
12	227	1.32	1.39	0.00	12	277	1.60	1.20	0.05
12	228	1.32	1.40	0.00	12	278	1.38	1.32	0.00
12	229	1.31	1.37	0.00	12	280	1.23	1.43	0.00
12	230	1.26	1.25	0.01	12	281	0.89	1.95	0.04
12	231	1.36	1.11	0.00	12	282	1.62	0.69	0.00
12	232	1.30	0.92	0.05	12	283	1.06	0.95	0.20
12	233	1.51	0.92	0.00	12	284	1.50	0.98	0.00
12	234	1.51	0.91	0.00	12	285	1.04	1.01	0.18
12	235	1.33	0.92	0.03	12	286	1.30	2.10	0.07
12	236	1.68	0.89	0.02	12	287	1.31	1.30	5.31
12	237	1.52	0.98	0.00	12	288	1.32	1.16	5.01
12	238	1.49	0.90	0.00	12	289	1.09	0.46	4.26
12	239	1.49	0.99	0.00	12	290	0.89	2.00	0.03
12	240	1.49	0.99	0.00	12	291	1.06	2.04	0.00
12	241	1.49	1.01	0.00	12	292	1.06	2.06	0.00
12	242	1.48	1.01	0.00	12	293	0.83	2.18	0.03
12	243	1.47	1.11	0.00	12	294	0.73	2.47	0.03
12	244	1.47	1.12	0.00	12	5.1	1.03	1.24	0.11
12	245	1.47	1.20	0.01	12	7.1	1.44	1.46	0.03
12	246	1.47	1.22	0.01	12	8.1	1.26	1.46	0.00
12	247	1.47	1.17	0.01	12	10.1	1.18	1.21	0.04
12	248	1.47	1.12	0.00	12	23.1	1.64	0.26	0.11
12	249	1.47	1.10	0.00	12	25.1	1.29	0.26	0.47
12	250	1.47	1.11	0.00	12	27.1	1.49	0.25	0.24
12	251	1.47	1.16	0.01	12	32.1	1.41	0.24	0.32
12	252	1.50	0.84	0.00	12	33.1	1.98	0.22	0.00
12	253	1.56	0.84	0.00	12	34.1	2.04	0.58	0.10
12	254	1.56	0.84	0.00	12	35.1	1.75	1.06	0.09
12	255	1.56	0.87	0.00	12	36.1	1.45	0.99	0.00
12	256	1.56	0.90	0.00	12	37.1	1.45	1.22	0.01
12	257	1.56	1.01	0.01	12	38.1	1.45	1.21	0.00
12	258	1.56	1.01	0.01	12	39.1	1.47	1.17	0.00
12	259	1.56	1.10	0.02	12	41.1	1.42	0.61	0.08
12	260	1.56	1.17	0.03	12	42.1	1.73	0.61	0.00
12	261	1.56	1.13	0.02	12	43.1	1.70	0.52	0.00
12	262	1.56	1.12	0.02	12	46.1	1.84	0.49	0.00
12	263	1.51	1.14	0.01	12	47.1	1.78	0.49	0.00
12	264	1.41	1.15	0.00	12	48.1	1.79	0.51	0.00
12	265	1.33	1.05	0.01	12	49.1	1.76	0.50	0.00
12	266	1.40	0.90	0.02	12	50.1	1.76	0.51	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	51.1	1.75	0.51	0.00	12	120.1	2.79	0.00	0.06
12	52.1	1.75	0.52	0.00	12	121.1	2.54	0.01	0.00
12	53.1	2.15	0.53	0.16	12	122.1	2.54	0.00	0.00
12	54.1	2.01	0.56	0.08	12	123.1	2.54	0.00	0.01
12	56.1	1.78	0.30	0.02	12	124.1	2.44	0.00	0.00
12	60.1	1.86	0.09	0.11	12	125.1	2.39	0.04	0.09
12	64.1	2.34	0.00	0.02	12	126.1	2.69	0.07	0.00
12	67.1	2.62	0.02	0.00	12	127.1	2.69	0.05	0.00
12	68.1	2.83	0.00	0.10	12	128.1	2.69	0.07	0.00
12	69.1	2.76	0.04	0.01	12	129.1	2.69	0.07	0.00
12	70.1	2.56	0.02	0.00	12	130.1	2.67	0.07	0.00
12	71.1	2.54	0.04	0.02	12	131.1	2.74	0.07	0.00
12	72.1	2.67	0.04	0.00	12	132.1	2.74	0.08	0.00
12	73.1	2.69	0.03	0.00	12	133.1	2.74	0.08	0.00
12	74.1	2.66	0.04	0.00	12	134.1	2.74	0.09	0.00
12	75.1	2.66	0.04	0.00	12	135.1	2.74	0.07	0.00
12	77.1	2.78	0.11	0.00	12	136.1	2.56	0.08	0.04
12	79.1	2.82	0.17	0.00	12	137.1	2.75	0.07	0.00
12	80.1	2.88	1.54	2.71	12	138.1	2.75	0.08	0.00
12	81.1	2.88	0.15	0.00	12	139.1	2.75	0.09	0.00
12	82.1	2.93	0.17	0.00	12	140.1	2.75	0.07	0.00
12	84.1	2.91	0.27	0.01	12	141.1	2.68	0.00	0.03
12	85.1	2.99	0.28	0.00	12	142.1	2.52	0.00	0.01
12	86.1	3.05	0.31	0.00	12	143.1	2.93	0.11	0.01
12	87.1	3.08	0.32	0.00	12	144.1	2.81	0.15	0.00
12	88.1	3.07	0.32	0.00	12	145.1	2.81	0.12	0.00
12	89.1	3.05	0.33	0.00	12	146.1	2.75	0.05	0.00
12	90.1	2.92	0.28	0.01	12	147.1	2.61	0.07	0.02
12	91.1	3.01	0.27	0.00	12	148.1	2.77	0.02	0.02
12	92.1	3.03	0.27	0.00	12	149.1	2.96	0.25	0.00
12	93.1	2.90	0.29	0.01	12	150.1	2.66	0.11	0.02
12	94.1	3.21	0.29	0.04	12	152.1	2.56	0.13	0.08
12	95.1	3.02	0.31	0.00	12	153.1	2.84	0.11	0.00
12	96.1	3.03	0.03	0.52	12	154.1	2.84	0.11	0.00
12	97.1	3.03	0.02	0.46	12	155.1	2.84	0.12	0.00
12	103.1	3.06	0.10	0.07	12	156.1	2.84	0.19	0.00
12	104.1	2.68	0.12	0.02	12	157.1	2.84	0.22	0.01
12	105.1	2.70	0.13	0.02	12	158.1	2.84	0.17	0.00
12	106.1	2.80	0.15	0.01	12	159.1	2.84	0.17	0.00
12	108.1	3.25	0.33	0.04	12	160.1	2.86	0.17	0.00
12	109.1	2.83	0.35	0.06	12	161.1	2.89	0.19	0.00
12	110.1	3.07	0.31	0.00	12	162.1	2.89	0.16	0.00
12	111.1	3.07	0.10	0.08	12	163.1	2.89	0.17	0.00
12	113.1	3.19	0.19	0.07	12	164.1	2.89	0.20	0.00
12	114.1	2.91	0.16	0.00	12	165.1	2.89	0.19	0.00
12	115.1	2.91	0.16	0.00	12	166.1	2.88	0.19	0.00
12	116.1	2.95	0.10	0.02	12	167.1	2.92	0.20	0.00
12	117.1	2.80	0.01	0.06	12	168.1	2.92	0.19	0.00
12	118.1	2.80	0.00	0.07	12	169.1	2.92	0.17	0.00
12	119.1	2.80	0.01	0.06	12	170.1	2.84	0.17	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	171.1	2.94	0.13	0.01	12	222.1	2.05	0.19	0.00
12	172.1	2.84	0.12	0.00	12	223.1	2.05	0.19	0.00
12	173.1	2.84	0.10	0.00	12	224.1	2.05	0.19	0.00
12	174.1	2.84	0.10	0.00	12	225.1	2.05	0.21	0.00
12	175.1	2.84	0.06	0.01	12	226.1	1.94	0.18	0.01
12	176.1	2.76	0.01	0.03	12	227.1	2.06	0.14	0.00
12	177.1	3.05	0.10	0.07	12	228.1	2.06	0.12	0.01
12	178.1	2.83	0.05	0.02	12	229.1	2.06	0.12	0.01
12	179.1	2.70	0.04	0.00	12	230.1	1.94	0.17	0.01
12	180.1	2.58	0.12	0.06	12	231.1	2.21	0.11	0.01
12	181.1	2.88	0.00	0.16	12	232.1	1.94	0.15	0.02
12	182.1	2.71	0.01	0.02	12	233.1	2.09	0.14	0.00
12	183.1	2.56	0.01	0.00	12	234.1	1.99	0.15	0.01
12	184.1	2.56	0.01	0.00	12	235.1	2.09	0.20	0.00
12	185.1	2.56	0.02	0.00	12	236.1	2.09	0.12	0.00
12	186.1	2.56	0.01	0.00	12	237.1	2.09	0.14	0.00
12	187.1	2.56	0.01	0.00	12	238.1	2.09	0.15	0.00
12	188.1	2.56	0.01	0.00	12	239.1	2.09	0.14	0.00
12	189.1	2.56	0.01	0.00	12	240.1	2.09	0.11	0.00
12	190.1	2.56	0.02	0.00	12	241.1	2.09	0.11	0.00
12	191.1	2.56	0.01	0.00	12	242.1	2.03	0.10	0.02
12	192.1	2.56	0.02	0.00	12	243.1	2.16	0.10	0.00
12	193.1	2.56	0.01	0.00	12	244.1	2.16	0.11	0.00
12	194.1	2.56	0.01	0.00	12	245.1	2.16	0.11	0.00
12	195.1	2.56	0.01	0.00	12	246.1	2.16	0.12	0.00
12	196.1	2.56	0.00	0.00	12	247.1	2.16	0.11	0.00
12	197.1	2.56	0.00	0.00	12	248.1	2.16	0.12	0.00
12	198.1	2.54	0.00	0.00	12	249.1	2.16	0.12	0.00
12	199.1	2.47	0.00	0.00	12	250.1	2.16	0.12	0.00
12	200.1	2.47	0.00	0.00	12	251.1	2.14	0.13	0.00
12	201.1	2.40	0.00	0.00	12	252.1	2.13	0.18	0.01
12	202.1	2.44	0.00	0.00	12	253.1	2.06	0.18	0.00
12	204.1	2.35	0.00	0.01	12	254.1	2.06	0.19	0.00
12	205.1	2.46	0.01	0.00	12	255.1	2.06	0.19	0.00
12	206.1	2.46	0.00	0.00	12	256.1	2.06	0.18	0.00
12	207.1	2.44	0.01	0.00	12	257.1	2.06	0.21	0.00
12	208.1	2.39	0.01	0.00	12	258.1	2.06	0.16	0.00
12	209.1	2.42	0.00	0.00	12	259.1	2.02	0.17	0.00
12	210.1	2.32	0.00	0.01	12	260.1	2.06	0.18	0.00
12	211.1	2.42	0.01	0.00	12	261.1	2.06	0.18	0.00
12	212.1	2.42	0.01	0.00	12	262.1	2.06	0.18	0.00
12	213.1	2.22	0.02	0.02	12	263.1	1.92	0.19	0.02
12	214.1	2.31	0.02	0.00	12	264.1	2.04	0.19	0.00
12	215.1	2.35	0.02	0.00	12	265.1	1.91	0.20	0.02
12	216.1	2.35	0.05	0.01	12	266.1	1.93	0.31	0.00
12	217.1	2.35	0.11	0.04	12	267.1	1.92	0.31	0.00
12	218.1	2.35	0.14	0.06	12	268.1	1.77	0.30	0.03
12	219.1	2.35	0.18	0.08	12	269.1	1.93	0.31	0.00
12	220.1	2.35	0.18	0.09	12	270.1	1.87	0.31	0.00
12	221.1	2.32	0.19	0.08	12	271.1	1.92	0.32	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	272.1	1.92	0.34	0.00	12	89.2	1.73	0.61	0.00
12	273.1	1.92	0.36	0.00	12	90.2	1.71	0.66	0.00
12	274.1	1.91	0.37	0.00	12	91.2	1.66	0.64	0.00
12	275.1	1.87	0.36	0.00	12	95.2	1.82	0.26	0.02
12	276.1	1.84	0.35	0.00	12	96.2	1.98	0.03	0.45
12	277.1	1.77	0.34	0.02	12	97.2	2.65	0.02	0.10
12	278.1	1.89	0.34	0.00	12	103.2	2.27	0.02	0.01
12	280.1	1.51	2.24	0.28	12	104.2	2.35	0.02	0.00
12	281.1	2.01	0.23	0.00	12	105.2	2.35	0.02	0.00
12	282.1	4.90	0.22	8.35	12	108.2	2.33	0.02	0.00
12	283.1	1.81	1.60	0.36	12	109.2	2.34	0.02	0.00
12	284.1	1.21	1.54	0.00	12	110.2	2.37	0.01	0.00
12	285.1	1.10	1.75	0.00	12	111.2	2.40	0.01	0.04
12	286.1	1.01	1.92	0.01	12	113.2	2.60	0.01	0.00
12	287.1	1.78	5.67	9.50	12	114.2	2.74	0.02	0.02
12	288.1	4.44	8.01	0.75	12	115.2	2.61	0.01	0.00
12	289.1	2.01	0.35	1.13	12	119.2	2.65	0.59	0.35
12	290.1	0.95	2.13	0.00	12	120.2	3.06	0.64	0.05
12	291.1	1.02	2.04	0.00	12	121.2	3.27	0.56	0.00
12	292.1	0.80	2.16	0.04	12	122.2	3.27	0.63	0.00
12	293.1	0.87	2.17	0.02	12	123.2	3.24	0.70	0.01
12	294.1	0.87	2.44	0.00	12	124.2	3.10	0.68	0.04
12	300.1	1.45	1.38	0.02	12	125.2	3.71	0.81	0.11
12	301.1	1.45	1.27	0.01	12	126.2	3.49	0.76	0.02
12	27.2	1.08	1.17	0.10	12	128.2	3.29	1.02	0.04
12	28.2	1.42	1.29	0.01	12	130.2	3.39	1.26	0.04
12	37.2	1.32	1.32	0.00	12	131.2	3.60	1.57	0.02
12	38.2	1.32	1.29	0.00	12	132.2	3.60	1.48	0.01
12	39.2	1.35	1.31	0.00	12	133.2	3.60	1.46	0.01
12	47.2	1.36	0.54	0.15	12	134.2	3.60	1.38	0.00
12	48.2	1.69	0.51	0.01	12	135.2	3.60	1.43	0.01
12	49.2	1.82	0.51	0.00	12	137.2	3.60	1.62	0.02
12	60.2	1.75	0.55	0.00	12	138.2	3.55	1.21	0.00
12	64.2	1.73	0.55	0.00	12	139.2	3.83	1.85	0.00
12	67.2	1.76	0.58	0.00	12	140.2	3.64	1.38	0.00
12	68.2	1.74	0.56	0.00	12	141.2	3.66	0.89	0.06
12	69.2	1.76	0.55	0.00	12	142.2	3.66	1.04	0.03
12	71.2	1.76	0.47	0.00	12	143.2	3.65	1.27	0.00
12	72.2	1.93	0.49	0.02	12	144.2	3.65	1.23	0.00
12	73.2	1.81	0.45	0.00	12	145.2	3.69	1.41	0.00
12	74.2	1.80	0.43	0.00	12	146.2	3.48	0.77	0.02
12	75.2	1.83	0.45	0.00	12	147.2	3.24	0.71	0.01
12	77.2	1.80	0.44	0.00	12	148.2	2.82	0.08	0.00
12	79.2	1.79	0.42	0.00	12	149.2	3.20	0.23	0.06
12	82.2	1.80	0.27	0.02	12	150.2	2.95	0.13	0.01
12	84.2	1.99	0.51	0.05	12	152.2	2.76	0.16	0.01
12	85.2	1.72	0.54	0.00	12	153.2	2.91	0.19	0.00
12	86.2	1.72	0.56	0.00	12	155.2	2.91	0.27	0.01
12	87.2	1.71	0.57	0.00	12	156.2	2.91	0.28	0.01
12	88.2	1.73	0.53	0.00	12	157.2	2.91	0.27	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	158.2	2.85	0.34	0.04	12	216.2	2.93	0.15	0.00
12	159.2	3.06	0.27	0.00	12	217.2	2.87	0.15	0.00
12	160.2	3.14	0.07	0.15	12	218.2	2.87	0.18	0.00
12	161.2	2.75	0.06	0.00	12	219.2	2.87	0.20	0.00
12	162.2	2.95	0.06	0.05	12	220.2	2.87	0.18	0.00
12	165.2	2.87	0.14	0.00	12	221.2	2.64	0.18	0.07
12	166.2	2.65	0.10	0.02	12	223.2	2.91	0.26	0.01
12	167.2	2.79	0.10	0.00	12	224.2	3.03	0.21	0.01
12	168.2	2.79	0.15	0.01	12	225.2	2.94	0.20	0.00
12	169.2	2.79	0.15	0.01	12	226.2	2.94	0.17	0.00
12	170.2	2.87	0.14	0.00	12	227.2	2.94	0.15	0.01
12	171.2	2.71	0.16	0.03	12	228.2	2.94	0.14	0.01
12	172.2	2.87	0.17	0.00	12	229.2	2.94	0.13	0.01
12	173.2	2.87	0.19	0.00	12	230.2	3.07	0.17	0.03
12	174.2	2.87	0.20	0.00	12	231.2	2.87	0.06	0.02
12	175.2	2.88	0.10	0.01	12	232.2	2.92	0.09	0.02
12	176.2	2.72	0.00	0.03	12	233.2	2.78	0.09	0.00
12	177.2	2.79	0.13	0.00	12	234.2	2.62	0.08	0.02
12	178.2	2.81	0.18	0.01	12	235.2	2.59	0.06	0.02
12	179.2	2.90	0.21	0.00	12	236.2	2.76	0.07	0.00
12	181.2	2.90	0.41	0.04	12	237.2	2.66	0.03	0.00
12	182.2	2.93	0.34	0.02	12	238.2	2.65	0.01	0.00
12	183.2	3.08	0.32	0.00	12	239.2	2.97	0.15	0.01
12	184.2	3.08	0.26	0.01	12	240.2	2.89	0.08	0.02
12	185.2	2.98	0.34	0.01	12	241.2	2.77	0.03	0.02
12	188.2	3.10	0.53	0.01	12	242.2	2.53	0.01	0.00
12	190.2	3.31	0.47	0.02	12	243.2	2.58	0.00	0.00
12	191.2	3.16	0.54	0.00	12	244.2	2.58	0.00	0.01
12	192.2	3.16	0.51	0.00	12	245.2	2.58	0.00	0.01
12	193.2	3.16	0.59	0.01	12	246.2	2.47	0.00	0.00
12	194.2	3.16	0.51	0.00	12	247.2	2.69	0.00	0.05
12	195.2	3.16	0.48	0.00	12	248.2	2.46	0.00	0.00
12	196.2	3.16	0.47	0.00	12	249.2	2.47	0.00	0.00
12	197.2	3.16	0.44	0.00	12	250.2	2.46	0.00	0.00
12	198.2	2.94	0.50	0.06	12	251.2	2.41	0.00	0.00
12	199.2	3.18	0.51	0.00	12	252.2	2.37	0.00	0.01
12	200.2	3.18	0.51	0.00	12	253.2	2.47	0.00	0.00
12	201.2	3.18	0.37	0.01	12	254.2	2.47	0.00	0.00
12	202.2	3.18	0.11	0.14	12	255.2	2.47	0.00	0.00
12	204.2	3.18	0.13	0.11	12	256.2	2.47	0.00	0.00
12	205.2	2.84	0.19	0.01	12	257.2	2.48	0.00	0.00
12	206.2	2.84	0.19	0.00	12	258.2	2.47	0.01	0.00
12	207.2	2.71	0.19	0.04	12	259.2	2.29	0.01	0.01
12	208.2	2.91	0.22	0.00	12	260.2	2.40	0.01	0.00
12	209.2	2.91	0.21	0.00	12	261.2	2.40	0.07	0.03
12	210.2	2.91	0.14	0.00	12	262.2	2.40	0.11	0.06
12	211.2	2.91	0.21	0.00	12	263.2	2.23	0.16	0.02
12	212.2	2.91	0.22	0.00	12	264.2	2.08	0.17	0.00
12	214.2	2.85	0.34	0.04	12	265.2	1.92	0.16	0.03
12	215.2	3.10	0.52	0.01	12	266.2	2.44	0.10	0.07

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	267.2	2.17	0.10	0.00	12	133.3	2.70	0.05	0.00
12	268.2	2.05	0.14	0.00	12	135.3	2.68	0.11	0.01
12	269.2	2.10	0.11	0.00	12	137.3	2.85	0.17	0.00
12	270.2	2.02	0.11	0.01	12	138.3	2.71	0.19	0.04
12	271.2	2.14	0.13	0.00	12	139.3	2.94	0.14	0.01
12	272.2	1.97	0.30	0.00	12	140.3	2.91	0.24	0.00
12	273.2	2.52	0.12	0.15	12	141.3	3.03	0.46	0.02
12	274.2	2.03	0.13	0.01	12	142.3	3.16	0.53	0.00
12	275.2	2.12	0.15	0.00	12	143.3	2.91	0.32	0.02
12	276.2	1.94	0.13	0.03	12	144.3	2.91	0.38	0.04
12	277.2	1.98	0.23	0.00	12	145.3	2.79	0.42	0.11
12	278.2	1.81	0.40	0.00	12	146.3	3.02	0.87	0.16
12	280.2	1.84	1.17	0.20	12	147.3	3.25	0.89	0.03
12	281.2	1.68	0.62	0.00	12	148.3	3.39	1.76	0.18
12	282.2	1.33	0.63	0.13	12	149.3	3.42	1.67	0.12
12	285.2	1.49	2.17	0.23	12	150.3	3.42	1.80	0.16
12	287.2	2.30	10.48	11.64	12	152.3	3.66	1.68	0.01
12	288.2	2.31	3.10	3.73	12	153.3	3.46	1.67	0.09
12	289.2	1.68	0.64	0.00	12	155.3	3.77	1.69	0.00
12	294.2	0.87	2.87	0.01	12	157.3	3.77	1.97	0.01
12	300.2	1.36	1.43	0.01	12	160.3	3.92	3.77	0.25
12	301.2	1.33	1.33	0.00	12	161.3	4.42	3.81	0.00
12	310.2	1.69	0.76	0.01	12	162.3	4.54	3.96	0.01
12	28.3	0.99	2.97	0.06	12	170.3	5.05	6.44	0.00
12	37.3	1.10	1.87	0.00	12	171.3	4.62	6.62	0.18
12	38.3	1.10	1.89	0.00	12	172.3	5.05	6.34	0.00
12	68.3	1.54	1.34	0.05	12	173.3	5.05	6.27	0.00
12	69.3	1.02	0.82	0.30	12	174.3	5.05	6.30	0.00
12	77.3	1.40	1.10	0.00	12	175.3	5.21	7.52	0.00
12	79.3	1.48	1.06	0.00	12	176.3	4.60	3.18	0.11
12	84.3	1.35	1.68	0.03	12	177.3	5.00	6.22	0.00
12	85.3	1.19	2.10	0.02	12	178.3	5.28	8.26	0.00
12	88.3	1.05	1.77	0.01	12	179.3	5.35	7.08	0.05
12	89.3	1.15	1.80	0.00	12	181.3	5.00	4.89	0.10
12	90.3	1.23	1.77	0.01	12	182.3	4.69	4.43	0.01
12	91.3	1.14	1.72	0.00	12	183.3	5.06	4.51	0.21
12	95.3	1.14	1.74	0.00	12	184.3	4.55	3.93	0.01
12	96.3	1.18	1.67	0.00	12	185.3	4.52	3.67	0.02
12	97.3	1.23	1.11	0.04	12	188.3	4.84	3.54	0.23
12	103.3	1.43	1.08	0.00	12	190.3	4.76	3.64	0.14
12	108.3	1.50	0.88	0.00	12	191.3	4.36	3.74	0.00
12	109.3	1.55	0.94	0.00	12	192.3	4.61	3.42	0.08
12	114.3	1.55	0.49	0.05	12	193.3	4.27	2.24	0.09
12	115.3	1.78	0.45	0.00	12	194.3	4.46	3.49	0.01
12	120.3	1.90	0.36	0.00	12	195.3	4.46	3.91	0.00
12	121.3	1.88	0.36	0.00	12	196.3	4.46	1.82	0.40
12	122.3	1.88	0.24	0.01	12	197.3	4.37	0.05	2.80
12	130.3	2.70	0.02	0.01	12	198.3	2.59	0.02	0.00
12	131.3	1.93	0.05	0.59	12	199.3	2.61	0.04	0.00
12	132.3	2.70	0.01	0.01	12	200.3	2.90	0.03	0.06

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	201.3	2.61	0.09	0.03	12	266.3	2.55	0.15	0.10
12	202.3	2.78	0.28	0.05	12	267.3	3.02	0.23	0.00
12	204.3	3.08	0.27	0.01	12	268.3	2.90	0.25	0.01
12	205.3	3.00	0.27	0.00	12	269.3	2.98	0.21	0.00
12	206.3	2.72	0.18	0.03	12	270.3	2.82	0.20	0.01
12	207.3	2.90	0.19	0.00	12	271.3	2.93	0.22	0.00
12	208.3	2.90	0.18	0.00	12	272.3	3.00	0.32	0.00
12	209.3	2.92	0.17	0.00	12	273.3	2.79	0.27	0.04
12	210.3	2.89	0.27	0.01	12	274.3	3.01	0.27	0.00
12	211.3	2.89	0.18	0.00	12	275.3	3.00	0.28	0.00
12	212.3	3.12	0.20	0.04	12	276.3	2.96	0.03	0.43
12	214.3	2.93	0.14	0.01	12	277.3	2.20	0.00	0.05
12	215.3	2.90	0.20	0.00	12	278.3	2.44	0.22	0.19
12	216.3	2.93	0.49	0.06	12	280.3	1.81	1.96	0.53
12	217.3	2.93	0.64	0.12	12	281.3	2.10	0.12	0.00
12	218.3	2.93	0.63	0.12	12	282.3	1.04	0.14	1.13
12	219.3	2.93	0.66	0.13	12	285.3	1.79	2.24	0.66
12	223.3	3.07	1.05	0.18	12	287.3	2.22	0.00	0.07
12	225.3	3.61	1.26	0.00	12	288.3	2.33	6.57	7.37
12	227.3	3.71	1.57	0.00	12	289.3	2.04	0.26	0.01
12	230.3	3.84	2.04	0.00	12	294.3	0.85	2.92	0.01
12	231.3	3.91	2.20	0.00	12	295.3	0.65	2.72	0.03
12	233.3	4.04	2.52	0.00	12	300.3	1.12	1.40	0.03
12	234.3	4.05	2.58	0.00	12	301.3	1.12	1.89	0.00
12	236.3	4.08	2.66	0.00	12	302.3	0.80	2.01	0.07
12	237.3	4.19	3.04	0.00	12	303.3	1.33	2.00	0.07
12	238.3	4.22	3.32	0.01	12	304.3	1.06	2.00	0.00
12	242.3	4.33	3.96	0.02	12	305.3	1.16	2.33	0.04
12	243.3	4.47	3.80	0.00	12	306.3	1.62	1.49	0.13
12	244.3	4.47	4.93	0.05	12	307.3	1.26	1.48	0.00
12	245.3	4.37	2.33	0.13	12	309.3	4.98	2.03	1.16
12	246.3	4.61	4.55	0.00	12	37.4	1.04	2.46	0.02
12	247.3	4.61	4.45	0.00	12	38.4	0.97	2.50	0.01
12	248.3	4.49	2.54	0.18	12	68.4	0.92	2.24	0.00
12	249.3	4.07	1.21	0.24	12	77.4	1.04	2.29	0.01
12	250.3	4.07	1.57	0.12	12	84.4	1.08	1.60	0.02
12	251.3	4.07	1.23	0.23	12	85.4	1.22	1.32	0.01
12	252.3	3.58	0.26	0.36	12	88.4	1.32	1.13	0.01
12	253.3	3.58	0.25	0.37	12	97.4	1.43	0.53	0.10
12	254.3	3.58	0.26	0.35	12	108.4	1.79	0.20	0.06
12	255.3	3.58	0.28	0.33	12	109.4	2.08	0.19	0.00
12	256.3	3.57	0.24	0.36	12	114.4	2.04	0.18	0.00
12	257.3	2.81	0.18	0.01	12	115.4	2.04	0.21	0.00
12	258.3	2.90	0.02	0.08	12	120.4	2.01	0.25	0.00
12	259.3	2.90	0.01	0.09	12	121.4	1.98	0.27	0.00
12	260.3	2.90	0.02	0.07	12	132.4	2.25	0.00	0.04
12	261.3	2.90	0.09	0.02	12	133.4	2.22	0.03	0.01
12	262.3	2.90	0.13	0.00	12	137.4	2.44	0.00	0.00
12	263.3	2.69	0.15	0.03	12	138.4	2.58	0.01	0.03
12	264.3	2.70	0.11	0.01	12	139.4	2.10	0.00	0.11

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	140.4	2.40	0.01	0.00	12	251.4	4.89	1.67	1.26
12	141.4	2.05	0.11	0.01	12	252.4	3.77	3.49	0.33
12	142.4	2.42	0.10	0.07	12	253.4	3.68	3.53	0.45
12	143.4	2.40	0.01	0.00	12	254.4	3.95	3.42	0.14
12	144.4	2.40	0.01	0.00	12	255.4	4.36	2.82	0.04
12	145.4	2.42	0.08	0.05	12	256.4	4.36	2.68	0.06
12	146.4	2.61	0.13	0.24	12	257.4	4.33	2.93	0.02
12	147.4	2.16	0.11	0.00	12	258.4	3.76	3.73	0.42
12	160.4	2.60	0.28	0.16	12	259.4	4.41	3.88	0.00
12	161.4	3.00	0.29	0.00	12	260.4	4.41	3.19	0.02
12	172.4	2.22	0.65	1.13	12	261.4	4.41	3.09	0.03
12	173.4	3.30	0.69	0.00	12	262.4	4.40	2.95	0.04
12	175.4	3.44	0.77	0.01	12	263.4	3.91	3.18	0.12
12	176.4	4.50	2.93	0.09	12	264.4	4.26	3.42	0.00
12	177.4	3.37	1.29	0.06	12	266.4	4.26	3.54	0.01
12	183.4	3.66	3.88	0.62	12	267.4	4.26	3.64	0.02
12	188.4	4.19	3.95	0.08	12	269.4	4.39	3.91	0.00
12	190.4	4.60	3.84	0.03	12	270.4	4.17	4.05	0.10
12	191.4	4.24	3.97	0.05	12	271.4	4.49	4.10	0.00
12	192.4	4.45	4.12	0.00	12	272.4	4.23	3.52	0.01
12	193.4	4.68	4.66	0.00	12	273.4	4.89	3.90	0.19
12	194.4	4.46	3.61	0.01	12	274.4	4.84	3.87	0.16
12	197.4	4.56	9.51	1.01	12	275.4	4.48	3.81	0.00
12	200.4	5.58	10.74	0.03	12	276.4	4.05	1.93	8.77
12	204.4	5.88	11.89	0.00	12	278.4	1.00	2.64	0.02
12	205.4	5.97	11.77	0.00	12	280.4	0.75	1.78	0.15
12	206.4	5.95	12.30	0.00	12	285.4	0.71	2.53	0.03
12	207.4	5.98	11.65	0.01	12	289.4	1.01	2.71	0.03
12	208.4	5.98	12.79	0.00	12	294.4	0.76	2.84	0.00
12	214.4	6.24	14.76	0.01	12	295.4	0.72	2.72	0.01
12	215.4	6.02	14.17	0.05	12	84.5	1.08	0.91	0.20
12	216.4	6.24	14.93	0.01	12	85.5	1.52	0.79	0.00
12	217.4	6.24	15.04	0.01	12	88.5	1.50	1.10	0.01
12	218.4	6.24	15.16	0.02	12	160.5	1.49	0.46	0.09
12	219.4	6.24	15.10	0.01	12	161.5	1.77	0.70	0.02
12	223.4	6.24	15.13	0.02	12	172.5	2.21	0.39	0.13
12	225.4	6.24	15.52	0.03	12	173.5	1.83	0.58	0.01
12	227.4	6.24	14.87	0.01	12	177.5	1.75	0.99	0.07
12	230.4	6.19	12.93	0.01	12	183.5	1.45	0.97	0.00
12	231.4	6.25	15.10	0.01	12	216.5	1.54	0.10	0.38
12	237.4	6.71	17.12	0.01	12	218.5	2.21	0.23	0.04
12	238.4	6.37	17.94	0.12	12	219.5	2.05	0.21	0.00
12	242.4	6.72	16.85	0.02	12	223.5	1.97	0.18	0.01
12	244.4	6.49	5.28	2.96	12	225.5	2.05	0.16	0.00
12	245.4	5.12	8.03	0.04	12	242.5	2.06	0.07	0.03
12	246.4	6.49	5.50	2.79	12	249.5	3.50	1.85	0.11
12	247.4	5.01	6.18	0.00	12	250.5	3.84	1.64	0.01
12	248.4	5.34	7.93	0.00	12	260.5	3.88	15.86	6.67
12	249.4	5.29	8.44	0.01	12	261.5	6.47	13.46	0.11
12	250.4	5.29	8.05	0.00	12	262.5	6.15	12.09	0.04

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	267.5	5.96	11.70	0.00
12	270.5	5.49	8.76	0.00
12	271.5	5.44	8.86	0.00
12	285.5	4.96	2.34	16.11
12	294.5	0.82	2.53	0.00
12	298.5	2.26	0.32	0.12
12	299.5	1.93	0.97	2.34

For the modified regression equations, the sum of the squares of the difference between the actual and predicted values was 172.4 and the sum of the square of the difference between the actual and average values was 1239.5. In the table, the predicted value is in s/m.

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	2	1.05	1.94	0.00	12	67	2.00	0.61	0.09
12	5	1.21	1.47	0.00	12	68	1.71	0.66	0.00
12	6	1.56	1.35	0.06	12	69	2.16	0.53	0.17
12	7	1.65	1.62	0.20	12	70	1.86	0.60	0.02
12	8	1.20	1.63	0.00	12	71	1.87	0.61	0.03
12	9	1.34	1.67	0.02	12	72	1.69	0.59	0.00
12	10	1.53	1.30	0.04	12	73	1.99	0.58	0.08
12	11	1.64	0.70	0.00	12	74	1.71	0.60	0.00
12	12	1.64	0.77	0.00	12	75	1.71	0.66	0.00
12	13	1.79	0.82	0.05	12	76	2.11	0.64	0.18
12	14	1.86	0.82	0.08	12	77	1.68	0.64	0.00
12	17	1.64	0.59	0.01	12	78	1.68	0.62	0.00
12	18	1.67	0.07	0.30	12	79	1.97	0.58	0.07
12	23	2.01	0.08	0.03	12	80	1.72	0.59	0.00
12	25	1.68	0.05	0.35	12	81	1.72	0.55	0.00
12	27	2.47	0.02	0.02	12	82	1.72	0.54	0.00
12	29	2.48	0.02	0.02	12	83	1.72	0.61	0.00
12	32	2.59	0.00	0.01	12	84	2.03	0.39	0.03
12	33	2.47	0.00	0.00	12	85	1.89	0.43	0.00
12	34	2.47	0.01	0.01	12	86	1.82	0.52	0.00
12	35	2.63	0.19	0.34	12	87	1.82	0.59	0.01
12	36	2.04	0.22	0.00	12	88	1.86	0.56	0.02
12	37	2.17	0.28	0.05	12	89	1.73	0.55	0.00
12	38	1.94	0.29	0.00	12	90	1.88	0.51	0.01
12	39	2.06	0.31	0.02	12	91	1.76	0.54	0.00
12	41	2.01	0.57	0.08	12	92	1.76	0.58	0.00
12	42	1.89	0.68	0.06	12	93	1.94	0.65	0.07
12	43	1.65	0.81	0.01	12	94	1.85	0.72	0.05
12	44	1.65	0.52	0.01	12	95	1.63	0.79	0.00
12	45	1.65	0.58	0.00	12	96	1.63	0.81	0.00
12	46	1.72	0.57	0.00	12	97	1.93	0.65	0.07
12	47	1.72	0.52	0.00	12	98	1.93	0.45	0.01
12	48	1.72	0.56	0.00	12	99	1.81	0.65	0.02
12	49	1.72	0.60	0.00	12	100	1.81	0.65	0.02
12	50	2.06	0.51	0.09	12	101	1.81	0.70	0.03
12	51	2.10	0.53	0.13	12	102	1.81	0.76	0.04
12	52	2.09	0.53	0.12	12	103	1.81	0.86	0.07
12	53	1.75	0.56	0.00	12	104	1.99	0.95	0.23
12	54	1.75	0.54	0.00	12	105	1.86	0.91	0.11
12	55	2.07	0.54	0.10	12	106	1.75	0.97	0.07
12	56	1.74	0.65	0.01	12	107	1.55	1.03	0.01
12	57	2.06	0.68	0.17	12	108	2.02	1.10	0.35
12	58	2.03	0.68	0.14	12	109	1.63	1.13	0.05
12	59	1.83	0.65	0.02	12	110	1.41	1.07	0.00
12	60	2.14	0.65	0.22	12	111	1.78	1.09	0.12
12	61	1.80	0.69	0.02	12	112	1.86	1.02	0.16
12	62	2.06	0.04	0.04	12	113	1.47	1.07	0.00
12	63	1.77	0.71	0.02	12	114	1.83	0.98	0.12
12	64	1.95	0.80	0.14	12	115	1.49	0.93	0.00
12	66	1.69	0.59	0.00	12	116	1.49	1.06	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	117	1.88	0.99	0.16	12	167	1.53	0.98	0.00
12	118	1.48	1.08	0.00	12	168	1.69	1.04	0.05
12	119	1.48	1.06	0.00	12	169	1.97	0.98	0.24
12	120	1.48	1.09	0.00	12	170	1.46	0.99	0.00
12	121	1.48	1.00	0.00	12	171	1.49	0.88	0.00
12	122	1.48	1.08	0.00	12	172	1.85	0.68	0.04
12	123	1.63	1.03	0.03	12	173	1.96	0.64	0.08
12	124	1.83	0.84	0.08	12	174	1.68	0.66	0.00
12	125	1.92	0.00	0.24	12	175	1.68	0.71	0.00
12	126	2.41	0.02	0.01	12	176	2.01	0.68	0.13
12	127	2.56	0.02	0.05	12	177	2.02	0.67	0.13
12	128	2.34	0.04	0.00	12	178	2.03	0.59	0.10
12	129	2.34	0.07	0.02	12	179	1.71	0.64	0.00
12	130	2.61	0.73	0.53	12	180	2.22	0.63	0.29
12	131	3.33	0.07	1.27	12	181	1.68	0.46	0.01
12	132	3.33	0.08	1.29	12	182	1.68	0.59	0.00
12	133	3.33	0.07	1.26	12	183	1.68	0.65	0.00
12	134	3.59	0.03	1.63	12	184	1.68	0.67	0.00
12	135	2.31	0.05	0.00	12	185	1.68	0.71	0.00
12	136	2.57	0.08	0.14	12	186	1.68	0.78	0.01
12	137	2.20	0.15	0.01	12	187	1.99	0.64	0.10
12	138	2.20	0.06	0.00	12	188	1.68	0.63	0.00
12	139	2.50	0.06	0.07	12	189	2.17	0.59	0.21
12	140	2.22	0.08	0.00	12	190	1.71	0.69	0.00
12	141	2.22	0.05	0.00	12	191	1.71	0.64	0.00
12	142	2.49	0.05	0.06	12	192	1.71	0.72	0.01
12	143	2.24	0.04	0.00	12	193	1.71	0.71	0.01
12	144	2.24	0.07	0.00	12	194	1.71	0.71	0.01
12	145	2.24	0.13	0.02	12	195	1.92	0.72	0.08
12	146	2.24	0.14	0.02	12	196	1.63	0.76	0.00
12	147	2.41	0.17	0.12	12	197	2.03	0.69	0.14
12	148	2.18	0.21	0.03	12	198	1.63	0.75	0.00
12	149	2.45	0.35	0.31	12	199	1.84	0.72	0.04
12	150	2.48	0.20	0.20	12	200	1.63	0.69	0.00
12	151	2.37	0.34	0.23	12	201	2.10	0.64	0.19
12	152	2.11	0.41	0.08	12	202	1.67	0.61	0.00
12	153	1.84	0.47	0.00	12	203	1.67	0.60	0.00
12	154	1.84	0.45	0.00	12	204	1.87	0.64	0.04
12	155	1.84	0.47	0.00	12	205	1.68	0.70	0.00
12	156	1.84	0.66	0.03	12	206	1.68	0.74	0.00
12	157	1.84	0.84	0.08	12	207	1.68	0.75	0.00
12	158	2.23	0.78	0.40	12	208	1.68	0.73	0.00
12	159	1.60	0.79	0.00	12	209	1.97	0.86	0.17
12	160	1.90	0.71	0.07	12	210	1.55	0.80	0.00
12	161	1.64	0.74	0.00	12	211	1.55	0.88	0.00
12	162	1.64	0.81	0.00	12	212	1.55	0.92	0.00
12	163	1.64	0.90	0.01	12	213	1.92	1.04	0.21
12	164	1.64	0.94	0.02	12	214	1.89	1.06	0.19
12	165	1.64	1.08	0.04	12	215	1.45	1.07	0.00
12	166	1.84	0.89	0.09	12	216	1.45	1.07	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	217	1.45	1.11	0.00	12	267	1.53	0.87	0.00
12	218	1.45	1.15	0.00	12	268	1.90	0.94	0.16
12	219	1.45	1.18	0.00	12	269	2.00	0.96	0.26
12	220	1.45	1.20	0.00	12	270	1.92	0.67	0.07
12	221	1.45	1.12	0.00	12	271	1.66	0.68	0.00
12	222	1.45	1.22	0.01	12	272	1.66	0.75	0.00
12	223	1.45	1.32	0.01	12	273	1.66	0.79	0.00
12	224	1.45	1.37	0.02	12	274	1.66	0.88	0.01
12	225	1.45	1.40	0.02	12	275	1.66	0.95	0.02
12	226	1.79	1.34	0.22	12	276	1.66	1.02	0.04
12	227	1.32	1.39	0.00	12	277	2.06	1.20	0.46
12	228	1.32	1.40	0.00	12	278	1.38	1.32	0.00
12	229	1.91	1.37	0.36	12	280	1.84	1.43	0.31
12	230	1.50	1.25	0.02	12	281	1.47	1.95	0.15
12	231	1.36	1.11	0.00	12	282	2.21	0.69	0.31
12	232	1.90	0.92	0.15	12	283	1.08	0.95	0.18
12	233	2.04	0.92	0.28	12	284	1.50	0.98	0.00
12	234	2.04	0.91	0.27	12	285	1.12	1.01	0.12
12	235	1.74	0.92	0.05	12	286	1.31	2.10	0.08
12	236	2.03	0.89	0.25	12	287	1.77	1.30	3.41
12	237	1.78	0.98	0.09	12	288	1.76	1.16	3.22
12	238	1.49	0.90	0.00	12	289	1.69	0.46	2.14
12	239	1.49	0.99	0.00	12	290	0.90	2.00	0.03
12	240	1.49	0.99	0.00	12	291	1.06	2.04	0.00
12	241	1.49	1.01	0.00	12	292	1.06	2.06	0.00
12	242	1.87	1.01	0.16	12	293	0.85	2.18	0.02
12	243	1.47	1.11	0.00	12	294	0.81	2.47	0.01
12	244	1.47	1.12	0.00	12	5.1	1.09	1.24	0.08
12	245	1.47	1.20	0.01	12	7.1	1.69	1.46	0.17
12	246	1.47	1.22	0.01	12	8.1	1.32	1.46	0.00
12	247	1.47	1.17	0.01	12	10.1	1.24	1.21	0.02
12	248	1.47	1.12	0.00	12	23.1	1.71	0.26	0.07
12	249	1.47	1.10	0.00	12	25.1	1.35	0.26	0.38
12	250	1.47	1.11	0.00	12	27.1	1.56	0.25	0.17
12	251	1.47	1.16	0.01	12	32.1	1.48	0.24	0.25
12	252	1.94	0.84	0.14	12	33.1	1.98	0.22	0.00
12	253	1.56	0.84	0.00	12	34.1	2.13	0.58	0.17
12	254	1.56	0.84	0.00	12	35.1	2.04	1.06	0.35
12	255	1.56	0.87	0.00	12	36.1	1.45	0.99	0.00
12	256	1.56	0.90	0.00	12	37.1	1.45	1.22	0.01
12	257	1.56	1.01	0.01	12	38.1	1.45	1.21	0.00
12	258	1.56	1.01	0.01	12	39.1	1.74	1.17	0.12
12	259	1.56	1.10	0.02	12	41.1	1.53	0.61	0.03
12	260	1.56	1.17	0.03	12	42.1	2.03	0.61	0.11
12	261	1.56	1.13	0.02	12	43.1	1.70	0.52	0.00
12	262	1.56	1.12	0.02	12	46.1	1.94	0.49	0.03
12	263	1.88	1.14	0.22	12	47.1	1.78	0.49	0.00
12	264	1.41	1.15	0.00	12	48.1	1.90	0.51	0.02
12	265	2.00	1.05	0.30	12	49.1	1.76	0.50	0.00
12	266	1.95	0.90	0.18	12	50.1	1.76	0.51	0.00

Stair	ID	Pred.	Avg. Dif.[2]	Pred. Dif.[2]	Stair	ID	Pred.	Avg. Dif.[2]	Pred. Dif.[2]
12	51.1	1.87	0.51	0.01	12	120.1	2.94	0.00	0.16
12	52.1	1.87	0.52	0.01	12	121.1	2.54	0.01	0.00
12	53.1	2.27	0.53	0.27	12	122.1	2.54	0.00	0.00
12	54.1	2.13	0.56	0.16	12	123.1	2.54	0.00	0.01
12	56.1	1.91	0.30	0.00	12	124.1	2.81	0.00	0.11
12	60.1	1.97	0.09	0.05	12	125.1	2.75	0.04	0.00
12	64.1	2.46	0.00	0.00	12	126.1	2.69	0.07	0.00
12	67.1	2.73	0.02	0.02	12	127.1	2.69	0.05	0.00
12	68.1	2.94	0.00	0.19	12	128.1	2.69	0.07	0.00
12	69.1	2.87	0.04	0.03	12	129.1	2.93	0.07	0.04
12	70.1	2.69	0.02	0.00	12	130.1	3.01	0.07	0.07
12	71.1	2.84	0.04	0.03	12	131.1	2.74	0.07	0.00
12	72.1	2.67	0.04	0.00	12	132.1	2.74	0.08	0.00
12	73.1	2.80	0.03	0.02	12	133.1	2.74	0.08	0.00
12	74.1	2.66	0.04	0.00	12	134.1	2.74	0.09	0.00
12	75.1	2.66	0.04	0.00	12	135.1	2.74	0.07	0.00
12	77.1	2.89	0.11	0.01	12	136.1	2.83	0.08	0.01
12	79.1	2.94	0.17	0.00	12	137.1	2.75	0.07	0.00
12	80.1	2.88	1.54	2.71	12	138.1	2.75	0.08	0.00
12	81.1	2.88	0.15	0.00	12	139.1	2.75	0.09	0.00
12	82.1	3.05	0.17	0.03	12	140.1	2.75	0.07	0.00
12	84.1	3.02	0.27	0.00	12	141.1	2.85	0.00	0.11
12	85.1	3.11	0.28	0.01	12	142.1	2.52	0.00	0.01
12	86.1	3.19	0.31	0.02	12	143.1	3.07	0.11	0.07
12	87.1	3.21	0.32	0.03	12	144.1	2.81	0.15	0.00
12	88.1	3.19	0.32	0.02	12	145.1	2.81	0.12	0.00
12	89.1	3.19	0.33	0.02	12	146.1	2.91	0.05	0.04
12	90.1	3.23	0.28	0.05	12	147.1	2.93	0.07	0.04
12	91.1	3.01	0.27	0.00	12	148.1	2.96	0.02	0.11
12	92.1	3.19	0.27	0.04	12	149.1	3.15	0.25	0.03
12	93.1	3.26	0.29	0.06	12	150.1	2.85	0.11	0.00
12	94.1	3.37	0.29	0.13	12	152.1	2.93	0.13	0.01
12	95.1	3.17	0.31	0.02	12	153.1	2.84	0.11	0.00
12	96.1	3.03	0.03	0.52	12	154.1	2.84	0.11	0.00
12	97.1	3.03	0.02	0.46	12	155.1	2.84	0.12	0.00
12	103.1	3.22	0.10	0.18	12	156.1	2.84	0.19	0.00
12	104.1	3.03	0.12	0.05	12	157.1	2.84	0.22	0.01
12	105.1	3.05	0.13	0.05	12	158.1	2.84	0.17	0.00
12	106.1	2.97	0.15	0.01	12	159.1	2.84	0.17	0.00
12	108.1	3.38	0.33	0.11	12	160.1	3.01	0.17	0.01
12	109.1	2.97	0.35	0.01	12	161.1	2.89	0.19	0.00
12	110.1	3.07	0.31	0.00	12	162.1	2.89	0.16	0.00
12	111.1	3.07	0.10	0.08	12	163.1	2.89	0.17	0.00
12	113.1	3.36	0.19	0.20	12	164.1	2.89	0.20	0.00
12	114.1	2.91	0.16	0.00	12	165.1	2.89	0.19	0.00
12	115.1	2.91	0.16	0.00	12	166.1	3.14	0.19	0.05
12	116.1	3.15	0.10	0.13	12	167.1	2.92	0.20	0.00
12	117.1	2.80	0.01	0.06	12	168.1	2.92	0.19	0.00
12	118.1	2.80	0.00	0.07	12	169.1	2.92	0.17	0.00
12	119.1	2.80	0.01	0.06	12	170.1	2.84	0.17	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	171.1	3.15	0.13	0.09	12	222.1	2.05	0.19	0.00
12	172.1	2.84	0.12	0.00	12	223.1	2.05	0.19	0.00
12	173.1	2.84	0.10	0.00	12	224.1	2.05	0.19	0.00
12	174.1	2.84	0.10	0.00	12	225.1	2.05	0.21	0.00
12	175.1	2.84	0.06	0.01	12	226.1	2.34	0.18	0.08
12	176.1	2.94	0.01	0.14	12	227.1	2.06	0.14	0.00
12	177.1	3.21	0.10	0.18	12	228.1	2.06	0.12	0.01
12	178.1	3.05	0.05	0.12	12	229.1	2.06	0.12	0.01
12	179.1	2.70	0.04	0.00	12	230.1	2.19	0.17	0.02
12	180.1	2.90	0.12	0.01	12	231.1	2.45	0.11	0.10
12	181.1	3.10	0.00	0.39	12	232.1	2.53	0.15	0.20
12	182.1	2.94	0.01	0.14	12	233.1	2.09	0.14	0.00
12	183.1	2.56	0.01	0.00	12	234.1	2.52	0.15	0.18
12	184.1	2.56	0.01	0.00	12	235.1	2.09	0.20	0.00
12	185.1	2.56	0.02	0.00	12	236.1	2.09	0.12	0.00
12	186.1	2.56	0.01	0.00	12	237.1	2.09	0.14	0.00
12	187.1	2.56	0.01	0.00	12	238.1	2.09	0.15	0.00
12	188.1	2.56	0.01	0.00	12	239.1	2.09	0.14	0.00
12	189.1	2.56	0.01	0.00	12	240.1	2.09	0.11	0.00
12	190.1	2.56	0.02	0.00	12	241.1	2.09	0.11	0.00
12	191.1	2.56	0.01	0.00	12	242.1	2.41	0.10	0.06
12	192.1	2.56	0.02	0.00	12	243.1	2.16	0.10	0.00
12	193.1	2.56	0.01	0.00	12	244.1	2.16	0.11	0.00
12	194.1	2.56	0.01	0.00	12	245.1	2.16	0.11	0.00
12	195.1	2.56	0.01	0.00	12	246.1	2.16	0.12	0.00
12	196.1	2.56	0.00	0.00	12	247.1	2.16	0.11	0.00
12	197.1	2.56	0.00	0.00	12	248.1	2.16	0.12	0.00
12	198.1	2.81	0.00	0.11	12	249.1	2.16	0.12	0.00
12	199.1	2.47	0.00	0.00	12	250.1	2.16	0.12	0.00
12	200.1	2.47	0.00	0.00	12	251.1	2.40	0.13	0.08
12	201.1	2.87	0.00	0.19	12	252.1	2.39	0.18	0.11
12	202.1	2.44	0.00	0.00	12	253.1	2.06	0.18	0.00
12	204.1	2.72	0.00	0.07	12	254.1	2.06	0.19	0.00
12	205.1	2.46	0.01	0.00	12	255.1	2.06	0.19	0.00
12	206.1	2.46	0.00	0.00	12	256.1	2.06	0.18	0.00
12	207.1	2.65	0.01	0.07	12	257.1	2.06	0.21	0.00
12	208.1	2.39	0.01	0.00	12	258.1	2.06	0.16	0.00
12	209.1	2.42	0.00	0.00	12	259.1	2.35	0.17	0.09
12	210.1	2.82	0.00	0.16	12	260.1	2.06	0.18	0.00
12	211.1	2.42	0.01	0.00	12	261.1	2.06	0.18	0.00
12	212.1	2.42	0.01	0.00	12	262.1	2.06	0.18	0.00
12	213.1	2.65	0.02	0.09	12	263.1	2.27	0.19	0.05
12	214.1	2.70	0.02	0.12	12	264.1	2.04	0.19	0.00
12	215.1	2.35	0.02	0.00	12	265.1	2.57	0.20	0.29
12	216.1	2.35	0.05	0.01	12	266.1	2.47	0.31	0.30
12	217.1	2.35	0.11	0.04	12	267.1	1.92	0.31	0.00
12	218.1	2.35	0.14	0.06	12	268.1	2.21	0.30	0.08
12	219.1	2.35	0.18	0.08	12	269.1	1.93	0.31	0.00
12	220.1	2.35	0.18	0.09	12	270.1	2.32	0.31	0.15
12	221.1	2.68	0.19	0.40	12	271.1	1.92	0.32	0.00

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	272.1	1.92	0.34	0.00	12	89.2	2.04	0.61	0.12
12	273.1	1.92	0.36	0.00	12	90.2	1.84	0.66	0.03
12	274.1	2.28	0.37	0.17	12	91.2	1.66	0.64	0.00
12	275.1	1.87	0.36	0.00	12	95.2	1.95	0.26	0.00
12	276.1	2.29	0.35	0.16	12	96.2	2.11	0.03	0.29
12	277.1	2.42	0.34	0.28	12	97.2	2.78	0.02	0.19
12	278.1	1.89	0.34	0.00	12	103.2	2.42	0.02	0.00
12	280.1	2.07	2.24	1.20	12	104.2	2.35	0.02	0.00
12	281.1	2.01	0.23	0.00	12	105.2	2.35	0.02	0.00
12	282.1	5.70	0.22	13.61	12	108.2	2.62	0.02	0.09
12	283.1	1.82	1.60	0.37	12	109.2	2.45	0.02	0.02
12	284.1	1.21	1.54	0.00	12	110.2	2.53	0.01	0.03
12	285.1	1.13	1.75	0.00	12	111.2	2.56	0.01	0.00
12	286.1	1.01	1.92	0.01	12	113.2	2.60	0.01	0.00
12	287.1	2.25	5.67	6.78	12	114.2	2.87	0.02	0.07
12	288.1	4.90	8.01	0.16	12	115.2	2.61	0.01	0.00
12	289.1	2.01	0.35	1.13	12	119.2	2.82	0.59	0.18
12	290.1	0.95	2.13	0.00	12	120.2	3.17	0.64	0.01
12	291.1	1.02	2.04	0.00	12	121.2	3.27	0.56	0.00
12	292.1	0.81	2.16	0.04	12	122.2	3.27	0.63	0.00
12	293.1	0.88	2.17	0.02	12	123.2	3.41	0.70	0.01
12	294.1	0.90	2.44	0.00	12	124.2	3.27	0.68	0.00
12	300.1	1.45	1.38	0.02	12	125.2	3.87	0.81	0.24
12	301.1	1.45	1.27	0.01	12	126.2	3.65	0.76	0.09
12	27.2	1.31	1.17	0.01	12	128.2	3.46	1.02	0.00
12	28.2	1.47	1.29	0.02	12	130.2	3.54	1.26	0.00
12	37.2	1.32	1.32	0.00	12	131.2	3.60	1.57	0.02
12	38.2	1.32	1.29	0.00	12	132.2	3.60	1.48	0.01
12	39.2	1.62	1.31	0.08	12	133.2	3.60	1.46	0.01
12	47.2	1.44	0.54	0.09	12	134.2	3.60	1.38	0.00
12	48.2	1.79	0.51	0.00	12	135.2	3.60	1.43	0.01
12	49.2	1.91	0.51	0.02	12	137.2	3.60	1.62	0.02
12	60.2	1.86	0.55	0.02	12	138.2	3.68	1.21	0.01
12	64.2	1.73	0.55	0.00	12	139.2	3.96	1.85	0.01
12	67.2	1.86	0.58	0.02	12	140.2	3.77	1.38	0.01
12	68.2	1.84	0.56	0.01	12	141.2	3.66	0.89	0.06
12	69.2	1.85	0.55	0.01	12	142.2	3.66	1.04	0.03
12	71.2	2.05	0.47	0.07	12	143.2	3.65	1.27	0.00
12	72.2	2.03	0.49	0.06	12	144.2	3.65	1.23	0.00
12	73.2	2.10	0.45	0.09	12	145.2	3.82	1.41	0.03
12	74.2	1.80	0.43	0.00	12	146.2	3.80	0.77	0.20
12	75.2	1.94	0.45	0.02	12	147.2	3.56	0.71	0.06
12	77.2	1.80	0.44	0.00	12	148.2	3.18	0.08	0.17
12	79.2	2.08	0.42	0.06	12	149.2	3.56	0.23	0.36
12	82.2	1.93	0.27	0.00	12	150.2	2.95	0.13	0.01
12	84.2	2.24	0.51	0.22	12	152.2	2.76	0.16	0.01
12	85.2	1.80	0.54	0.00	12	153.2	3.09	0.19	0.03
12	86.2	1.86	0.56	0.02	12	155.2	2.91	0.27	0.01
12	87.2	1.85	0.57	0.02	12	156.2	2.91	0.28	0.01
12	88.2	1.81	0.53	0.00	12	157.2	2.91	0.27	0.01

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	158.2	3.08	0.34	0.00	12	216.2	3.12	0.15	0.07
12	159.2	3.06	0.27	0.00	12	217.2	2.87	0.15	0.00
12	160.2	3.27	0.07	0.28	12	218.2	2.87	0.18	0.00
12	161.2	2.75	0.06	0.00	12	219.2	2.87	0.20	0.00
12	162.2	3.13	0.06	0.16	12	220.2	2.87	0.18	0.00
12	165.2	3.12	0.14	0.07	12	221.2	3.03	0.18	0.01
12	166.2	2.93	0.10	0.02	12	223.2	2.91	0.26	0.01
12	167.2	2.79	0.10	0.00	12	224.2	3.38	0.21	0.20
12	168.2	2.79	0.15	0.01	12	225.2	2.94	0.20	0.00
12	169.2	2.79	0.15	0.01	12	226.2	2.94	0.17	0.00
12	170.2	2.87	0.14	0.00	12	227.2	2.94	0.15	0.01
12	171.2	3.09	0.16	0.05	12	228.2	2.94	0.14	0.01
12	172.2	2.87	0.17	0.00	12	229.2	2.94	0.13	0.01
12	173.2	2.87	0.19	0.00	12	230.2	3.30	0.17	0.17
12	174.2	2.87	0.20	0.00	12	231.2	3.09	0.06	0.13
12	175.2	3.03	0.10	0.06	12	232.2	3.28	0.09	0.25
12	176.2	2.88	0.00	0.11	12	233.2	2.78	0.09	0.00
12	177.2	2.79	0.13	0.00	12	234.2	3.15	0.08	0.15
12	178.2	3.02	0.18	0.01	12	235.2	2.97	0.06	0.06
12	179.2	2.90	0.21	0.00	12	236.2	2.76	0.07	0.00
12	181.2	2.90	0.41	0.04	12	237.2	2.89	0.03	0.06
12	182.2	3.14	0.34	0.01	12	238.2	2.65	0.01	0.00
12	183.2	3.23	0.32	0.03	12	239.2	3.34	0.15	0.22
12	184.2	3.29	0.26	0.09	12	240.2	3.27	0.08	0.26
12	185.2	2.98	0.34	0.01	12	241.2	3.15	0.03	0.26
12	188.2	3.27	0.53	0.00	12	242.2	2.91	0.01	0.11
12	190.2	3.49	0.47	0.11	12	243.2	2.58	0.00	0.00
12	191.2	3.16	0.54	0.00	12	244.2	2.58	0.00	0.01
12	192.2	3.16	0.51	0.00	12	245.2	2.58	0.00	0.01
12	193.2	3.16	0.59	0.01	12	246.2	2.71	0.00	0.06
12	194.2	3.16	0.51	0.00	12	247.2	2.93	0.00	0.22
12	195.2	3.16	0.48	0.00	12	248.2	2.46	0.00	0.00
12	196.2	3.16	0.47	0.00	12	249.2	2.47	0.00	0.00
12	197.2	3.16	0.44	0.00	12	250.2	2.46	0.00	0.00
12	198.2	3.21	0.50	0.00	12	251.2	2.67	0.00	0.05
12	199.2	3.18	0.51	0.00	12	252.2	2.80	0.00	0.11
12	200.2	3.18	0.51	0.00	12	253.2	2.47	0.00	0.00
12	201.2	3.18	0.37	0.01	12	254.2	2.47	0.00	0.00
12	202.2	3.18	0.11	0.14	12	255.2	2.47	0.00	0.00
12	204.2	3.37	0.13	0.28	12	256.2	2.47	0.00	0.00
12	205.2	2.84	0.19	0.01	12	257.2	2.76	0.00	0.08
12	206.2	2.84	0.19	0.00	12	258.2	2.47	0.01	0.00
12	207.2	3.08	0.19	0.03	12	259.2	2.63	0.01	0.05
12	208.2	2.91	0.22	0.00	12	260.2	2.40	0.01	0.00
12	209.2	2.91	0.21	0.00	12	261.2	2.40	0.07	0.03
12	210.2	2.91	0.14	0.00	12	262.2	2.40	0.11	0.06
12	211.2	2.91	0.21	0.00	12	263.2	2.58	0.16	0.24
12	212.2	2.91	0.22	0.00	12	264.2	2.08	0.17	0.00
12	214.2	3.06	0.34	0.00	12	265.2	2.34	0.16	0.07
12	215.2	3.31	0.52	0.01	12	266.2	2.78	0.10	0.37

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	267.2	2.17	0.10	0.00	12	133.3	2.70	0.05	0.00
12	268.2	2.45	0.14	0.12	12	135.3	2.82	0.11	0.00
12	269.2	2.10	0.11	0.00	12	137.3	2.85	0.17	0.00
12	270.2	2.47	0.11	0.11	12	138.3	2.83	0.19	0.01
12	271.2	2.14	0.13	0.00	12	139.3	3.05	0.14	0.04
12	272.2	2.33	0.30	0.16	12	140.3	2.91	0.24	0.00
12	273.2	2.87	0.12	0.55	12	141.3	3.34	0.46	0.04
12	274.2	2.40	0.13	0.08	12	142.3	3.16	0.53	0.00
12	275.2	2.12	0.15	0.00	12	143.3	2.91	0.32	0.02
12	276.2	2.40	0.13	0.08	12	144.3	2.91	0.38	0.04
12	277.2	2.62	0.23	0.39	12	145.3	2.91	0.42	0.04
12	278.2	2.26	0.40	0.18	12	146.3	3.33	0.87	0.01
12	280.2	2.43	1.17	1.08	12	147.3	3.56	0.89	0.02
12	281.2	1.68	0.62	0.00	12	148.3	3.55	1.76	0.07
12	282.2	2.12	0.63	0.19	12	149.3	3.42	1.67	0.12
12	285.2	1.50	2.17	0.25	12	150.3	3.42	1.80	0.16
12	287.2	2.73	10.48	8.91	12	152.3	3.82	1.68	0.00
12	288.2	2.72	3.10	2.30	12	153.3	3.63	1.67	0.02
12	289.2	1.68	0.64	0.00	12	155.3	3.77	1.69	0.00
12	294.2	0.89	2.87	0.01	12	157.3	3.77	1.97	0.01
12	300.2	1.43	1.43	0.02	12	160.3	4.04	3.77	0.15
12	301.2	1.41	1.33	0.01	12	161.3	4.42	3.81	0.00
12	310.2	2.17	0.76	0.32	12	162.3	4.72	3.96	0.06
12	28.3	1.03	2.97	0.08	12	170.3	5.05	6.44	0.00
12	37.3	1.10	1.87	0.00	12	171.3	4.80	6.62	0.06
12	38.3	1.10	1.89	0.00	12	172.3	5.05	6.34	0.00
12	68.3	1.62	1.34	0.09	12	173.3	5.05	6.27	0.00
12	69.3	1.10	0.82	0.22	12	174.3	5.05	6.30	0.00
12	77.3	1.66	1.10	0.05	12	175.3	5.35	7.52	0.02
12	79.3	1.58	1.06	0.02	12	176.3	4.60	3.18	0.11
12	84.3	1.59	1.68	0.17	12	177.3	5.13	6.22	0.03
12	85.3	1.26	2.10	0.05	12	178.3	5.47	8.26	0.01
12	88.3	1.12	1.77	0.00	12	179.3	5.35	7.08	0.05
12	89.3	1.15	1.80	0.00	12	181.3	5.19	4.89	0.25
12	90.3	1.53	1.77	0.15	12	182.3	4.69	4.43	0.01
12	91.3	1.14	1.72	0.00	12	183.3	5.19	4.51	0.35
12	95.3	1.14	1.74	0.00	12	184.3	4.74	3.93	0.08
12	96.3	1.49	1.67	0.09	12	185.3	4.72	3.67	0.11
12	97.3	1.51	1.11	0.01	12	188.3	4.99	3.54	0.39
12	103.3	1.57	1.08	0.02	12	190.3	4.92	3.64	0.28
12	108.3	1.78	0.88	0.06	12	191.3	4.36	3.74	0.00
12	109.3	1.83	0.94	0.11	12	192.3	4.77	3.42	0.19
12	114.3	1.66	0.49	0.01	12	193.3	4.42	2.24	0.20
12	115.3	1.78	0.45	0.00	12	194.3	4.46	3.49	0.01
12	120.3	2.02	0.36	0.02	12	195.3	4.46	3.91	0.00
12	121.3	1.88	0.36	0.00	12	196.3	4.46	1.82	0.40
12	122.3	1.88	0.24	0.01	12	197.3	4.53	0.05	3.38
12	130.3	2.70	0.02	0.01	12	198.3	2.83	0.02	0.05
12	131.3	2.06	0.05	0.41	12	199.3	2.61	0.04	0.00
12	132.3	2.70	0.01	0.01	12	200.3	3.06	0.03	0.16

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	201.3	2.86	0.09	0.01	12	266.3	2.88	0.15	0.00
12	202.3	2.78	0.28	0.05	12	267.3	3.27	0.23	0.10
12	204.3	3.25	0.27	0.07	12	268.3	3.29	0.25	0.10
12	205.3	3.00	0.27	0.00	12	269.3	2.98	0.21	0.00
12	206.3	2.91	0.18	0.00	12	270.3	3.26	0.20	0.11
12	207.3	2.90	0.19	0.00	12	271.3	2.93	0.22	0.00
12	208.3	2.90	0.18	0.00	12	272.3	3.00	0.32	0.00
12	209.3	3.20	0.17	0.09	12	273.3	3.34	0.27	0.11
12	210.3	2.89	0.27	0.01	12	274.3	3.35	0.27	0.12
12	211.3	2.89	0.18	0.00	12	275.3	3.00	0.28	0.00
12	212.3	3.39	0.20	0.22	12	276.3	3.38	0.03	1.15
12	214.3	2.93	0.14	0.01	12	277.3	2.84	0.00	0.17
12	215.3	3.09	0.20	0.02	12	278.3	2.87	0.22	0.75
12	216.3	2.93	0.49	0.06	12	280.3	2.39	1.96	1.73
12	217.3	2.93	0.64	0.12	12	281.3	2.10	0.12	0.00
12	218.3	2.93	0.63	0.12	12	282.3	1.83	0.14	0.07
12	219.3	2.93	0.66	0.13	12	285.3	1.80	2.24	0.68
12	223.3	3.25	1.05	0.06	12	287.3	2.69	0.00	0.04
12	225.3	3.80	1.26	0.04	12	288.3	2.72	6.57	5.36
12	227.3	3.92	1.57	0.03	12	289.3	2.60	0.26	0.40
12	230.3	4.06	2.04	0.02	12	294.3	0.86	2.92	0.01
12	231.3	3.91	2.20	0.00	12	295.3	0.66	2.72	0.03
12	233.3	4.34	2.52	0.08	12	300.3	1.17	1.40	0.01
12	234.3	4.36	2.58	0.08	12	301.3	1.19	1.89	0.01
12	236.3	4.08	2.66	0.00	12	302.3	0.86	2.01	0.04
12	237.3	4.41	3.04	0.03	12	303.3	1.57	2.00	0.26
12	238.3	4.22	3.32	0.01	12	304.3	1.06	2.00	0.00
12	242.3	4.52	3.96	0.00	12	305.3	1.24	2.33	0.08
12	243.3	4.47	3.80	0.00	12	306.3	1.71	1.49	0.20
12	244.3	4.47	4.93	0.05	12	307.3	1.26	1.48	0.00
12	245.3	4.59	2.33	0.35	12	309.3	5.16	2.03	1.58
12	246.3	4.84	4.55	0.05	12	37.4	1.08	2.46	0.03
12	247.3	4.61	4.45	0.00	12	38.4	1.02	2.50	0.01
12	248.3	4.72	2.54	0.42	12	68.4	1.00	2.24	0.00
12	249.3	4.07	1.21	0.24	12	77.4	1.30	2.29	0.11
12	250.3	4.07	1.57	0.12	12	84.4	1.32	1.60	0.01
12	251.3	4.30	1.23	0.51	12	85.4	1.28	1.32	0.00
12	252.3	3.58	0.26	0.36	12	88.4	1.39	1.13	0.00
12	253.3	3.58	0.25	0.37	12	97.4	1.71	0.53	0.00
12	254.3	3.58	0.26	0.35	12	108.4	2.06	0.20	0.00
12	255.3	3.58	0.28	0.33	12	109.4	2.17	0.19	0.02
12	256.3	3.85	0.24	0.78	12	114.4	2.04	0.18	0.00
12	257.3	3.09	0.18	0.04	12	115.4	2.04	0.21	0.00
12	258.3	2.90	0.02	0.08	12	120.4	2.11	0.25	0.02
12	259.3	2.90	0.01	0.09	12	121.4	1.98	0.27	0.00
12	260.3	2.90	0.02	0.07	12	132.4	2.34	0.00	0.01
12	261.3	2.90	0.09	0.02	12	133.4	2.31	0.03	0.00
12	262.3	2.90	0.13	0.00	12	137.4	2.44	0.00	0.00
12	263.3	3.03	0.15	0.03	12	138.4	2.68	0.01	0.08
12	264.3	3.04	0.11	0.05	12	139.4	2.19	0.00	0.06

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}	Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	140.4	2.40	0.01	0.00	12	251.4	5.13	1.67	1.86
12	141.4	2.17	0.11	0.00	12	252.4	3.77	3.49	0.33
12	142.4	2.53	0.10	0.14	12	253.4	3.90	3.53	0.21
12	143.4	2.40	0.01	0.00	12	254.4	4.17	3.42	0.02
12	144.4	2.40	0.01	0.00	12	255.4	4.36	2.82	0.04
12	145.4	2.53	0.08	0.11	12	256.4	4.36	2.68	0.06
12	146.4	2.72	0.13	0.37	12	257.4	4.33	2.93	0.02
12	147.4	2.28	0.11	0.02	12	258.4	4.05	3.73	0.13
12	160.4	2.70	0.28	0.09	12	259.4	4.41	3.88	0.00
12	161.4	3.00	0.29	0.00	12	260.4	4.41	3.19	0.02
12	172.4	2.32	0.65	0.92	12	261.4	4.41	3.09	0.03
12	173.4	3.41	0.69	0.01	12	262.4	4.63	2.95	0.19
12	175.4	3.56	0.77	0.04	12	263.4	4.25	3.18	0.00
12	176.4	4.63	2.93	0.20	12	264.4	4.26	3.42	0.00
12	177.4	3.49	1.29	0.02	12	266.4	4.26	3.54	0.01
12	183.4	3.78	3.88	0.45	12	267.4	4.26	3.64	0.02
12	188.4	4.19	3.95	0.08	12	269.4	4.71	3.91	0.06
12	190.4	4.74	3.84	0.09	12	270.4	4.60	4.05	0.01
12	191.4	4.38	3.97	0.01	12	271.4	4.49	4.10	0.00
12	192.4	4.60	4.12	0.01	12	272.4	4.56	3.52	0.04
12	193.4	4.82	4.66	0.03	12	273.4	5.21	3.90	0.58
12	194.4	4.60	3.61	0.05	12	274.4	5.17	3.87	0.53
12	197.4	4.71	9.51	0.73	12	275.4	4.80	3.81	0.14
12	200.4	5.73	10.74	0.00	12	276.4	4.50	1.93	11.64
12	204.4	6.04	11.89	0.01	12	278.4	1.47	2.64	0.37
12	205.4	6.13	11.77	0.05	12	280.4	1.33	1.78	0.04
12	206.4	6.12	12.30	0.02	12	285.4	0.72	2.53	0.03
12	207.4	5.98	11.65	0.01	12	289.4	1.62	2.71	0.62
12	208.4	5.98	12.79	0.00	12	294.4	0.77	2.84	0.00
12	214.4	6.24	14.76	0.01	12	295.4	0.72	2.72	0.01
12	215.4	6.20	14.17	0.00	12	84.5	1.31	0.91	0.04
12	216.4	6.24	14.93	0.01	12	85.5	1.52	0.79	0.00
12	217.4	6.24	15.04	0.01	12	88.5	1.57	1.10	0.02
12	218.4	6.24	15.16	0.02	12	160.5	1.77	0.46	0.00
12	219.4	6.24	15.10	0.01	12	161.5	1.86	0.70	0.05
12	223.4	6.24	15.13	0.02	12	172.5	2.30	0.39	0.20
12	225.4	6.24	15.52	0.03	12	173.5	2.11	0.58	0.16
12	227.4	6.24	14.87	0.01	12	177.5	2.04	0.99	0.31
12	230.4	6.39	12.93	0.10	12	183.5	1.56	0.97	0.00
12	231.4	6.44	15.10	0.01	12	216.5	1.69	0.10	0.22
12	237.4	6.71	17.12	0.01	12	218.5	2.36	0.23	0.13
12	238.4	6.57	17.94	0.02	12	219.5	2.20	0.21	0.03
12	242.4	6.90	16.85	0.10	12	223.5	2.14	0.18	0.01
12	244.4	6.70	5.28	3.72	12	225.5	2.05	0.16	0.00
12	245.4	5.33	8.03	0.00	12	242.5	2.23	0.07	0.00
12	246.4	6.70	5.50	3.55	12	249.5	3.69	1.85	0.02
12	247.4	5.21	6.18	0.06	12	250.5	3.84	1.64	0.01
12	248.4	5.56	7.93	0.07	12	260.5	4.07	15.86	5.71
12	249.4	5.29	8.44	0.01	12	261.5	6.67	13.46	0.28
12	250.4	5.29	8.05	0.00	12	262.5	6.36	12.09	0.17

Stair	ID	Pred.	Avg. Dif.^{2}	Pred. Dif.^{2}
12	267.5	6.18	11.70	0.08
12	270.5	5.91	8.76	0.23
12	271.5	5.44	8.86	0.00
12	285.5	4.96	2.34	16.12
12	294.5	0.82	2.53	0.00
12	298.5	2.43	0.32	0.26
12	299.5	2.10	0.97	1.85

Appendix D: Travel Distance and Area Comparisons

For the analysis in this appendix, the data from South stair in Building 8 will be used. The reference case will consist of the same assumptions made by Peacock, Hoskins, and Kuligowski (2010). Specifically, the travel distance on the treads is along the slope and the travel distance on the landing is linear (Equation 3.1), and the area is the total landing area. Any other set of assumptions could serve as the reference case because the intent is to demonstrate the importance of knowing the underlying assumptions and the impact of making different assumptions when matching data to equations developed from a different set of assumptions. The mean travel speed for all occupants is 0.51 m/s (S.D. 0.14 m/s). The density is determined based on the number of people on the landing on the higher floor when the occupant entered the landing. The data using these assumptions are shown in Figure D.1.

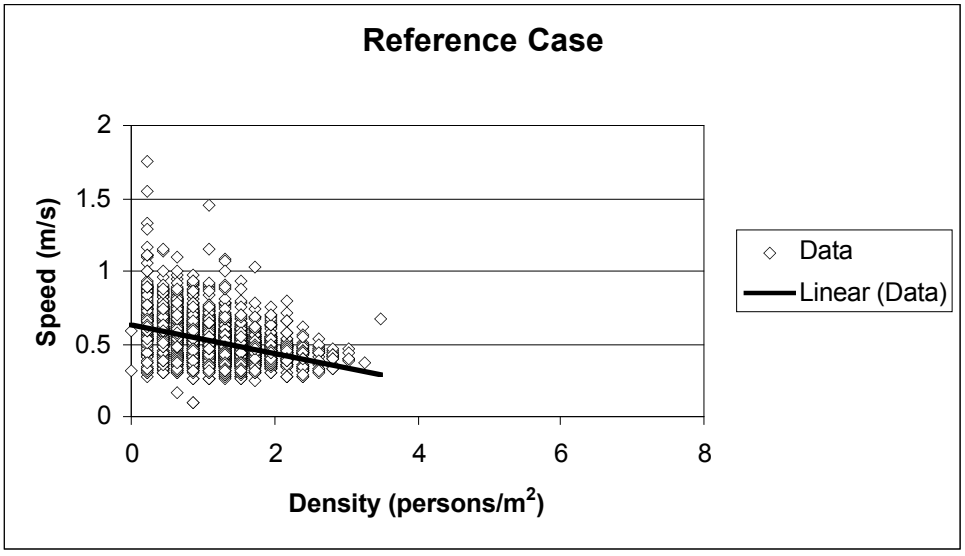

Figure D.1: Reference Case Data

A best-fit regression line, Equation D.1, has an R^2 value of 0.158.

$$s = 0.636 - 0.1013 \cdot D \qquad \text{(D.1)}$$

where:
s= speed (m/s)
D=Density (persons/m^2)

Next, comparisons will be made to data calculated using different assumptions and the reference case regression formula. The intent here is to mimic what could happen in practice: an equation for predicting speed is provided and it is applied to data

calculated using different assumptions. In this analysis, the equation will be deliberately misused to demonstrate that applying an equation developed from one set of assumptions to data collected on another set of assumptions can lead to incorrect results and conclusions. By using the same data (with different measurement methods) for both the reference equation and the data, the entire difference is caused by the change in measurement methods. Four different comparisons will be made:

- The travel distance on the treads changed to the horizontal component.
- The landing area changed to the rectangular area that is centered on the linear travel path.
- The travel distance on the landing changed to being arcs (Equation 3.2).
- Both the travel distance on the landing and the effective area on the landing changed based on arcs (Equation 3.2 and Equation 3.3).

In the different comparisons, "observed" values refer to the data as measured by the assumptions in the given comparison. The "reference" values are the ones that Equation D.1 would predict. This arrangement is analogous to a researcher collecting their own data and then comparing their results to previous work. Because the variable of different data sets is eliminated, the comparisons demonstrate conclusions that could be drawn by the researcher that are the result of differences in measurement methods alone rather than differences in human behavior.

D.1 Comparison 1: Horizontal Travel Distance on Treads

For the first comparison, the travel distance and area on landings are held constant. The travel distance on the treads is reduced to only the horizontal component. This results in an average speed of 0.39 m/s (S.D. 0.11). The data and Equation D.1 are plotted in Figure D.2.

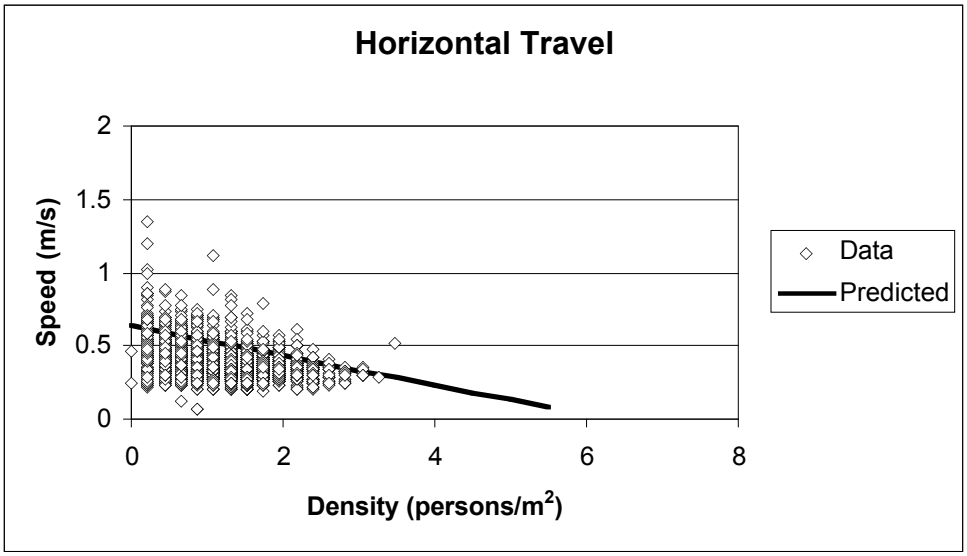

Figure D.2: Horizontal Distance on Treads Case

Using Equation D.1 to predict the speed when the distances on the treads is the horizontal component leads to a less accurate predicted value than simply assuming that all occupants are traveling at the average speed in the observed data. A paired sample t-test found that the speeds calculated by Equation D.1 are significantly over predicting the observed values by a mean of 0.12 m/s (95% confidence interval $0.11<x<0.12$ m/s). In other words, because the speed in the reference case was multiplied by a fraction, the average speed in the observed values is statistically slower.

D.2 Comparison 2: Effective Area on Landing (Linear)

Using an effective area to calculate the density does not change the speeds from the reference case. However the speeds calculated using Equation D.1 will decrease because the density increases as seen in Figure D.3.

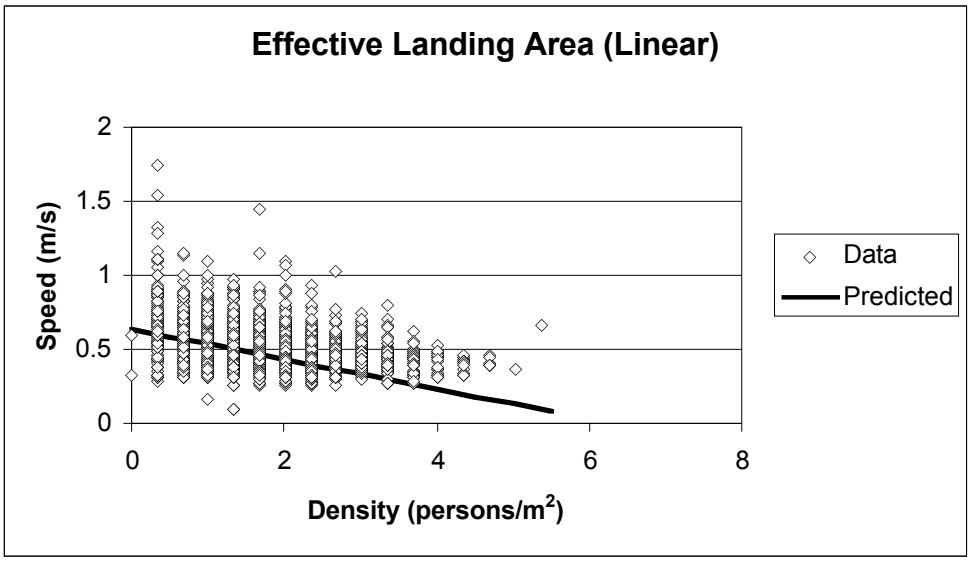

Figure D.3: Effective Landing Area (Linear) Case

A paired sample t-test found the mean difference for the reference values to be significantly under predicting the observed values by 0.069 m/s (95% confidence interval $0.064<x<0.073$ m/s). In other words, because all of the data was shifted to the right in Figure D.3 compared to Figure D.1, the average speed for the observed values is statistically greater than that of the reference values. As with the previous comparison, assuming that all occupants moved at the average observed speed was a better predictor than Equation D.1.

D.3 Comparison 3: Arc Travel Distance on Landing

In this comparison, the paths on the landings are arcs. The landing area is still the total area as used in the reference case. The data are shown in Figure D.4. The mean speed was 0.46 m/s (S.D. 0.13).

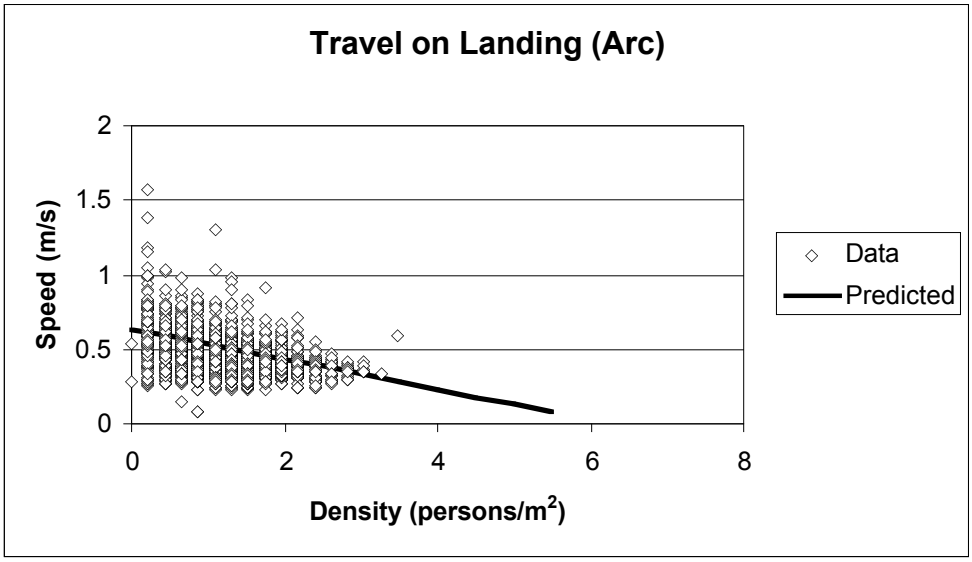

Figure D.4: Arc Travel Length on Landing Case

As was the case with the other comparisons Equation D.1 was less accurate than simply assuming that all occupants traveled at the averaged observed speed. A paired t-test found a significant difference in the results as well. In this comparison, the values calculated using Equation D.1 were greater than the observed values by an average of 0.053 m/s (95% confidence interval $0.049<x<0.057$ m/s). As with the first comparison, a decrease in the travel distance leads to the mean speed decreasing by a statistically significant amount.

Comparison 4: Arc Travel Path on Landing and Effective Area (Arc)

This comparison uses the arc travel distance on the landing and reduces the area on the landing using the same assumptions. The speeds are the same as in the previous comparison, but the density is changed as shown in Figure D.5.

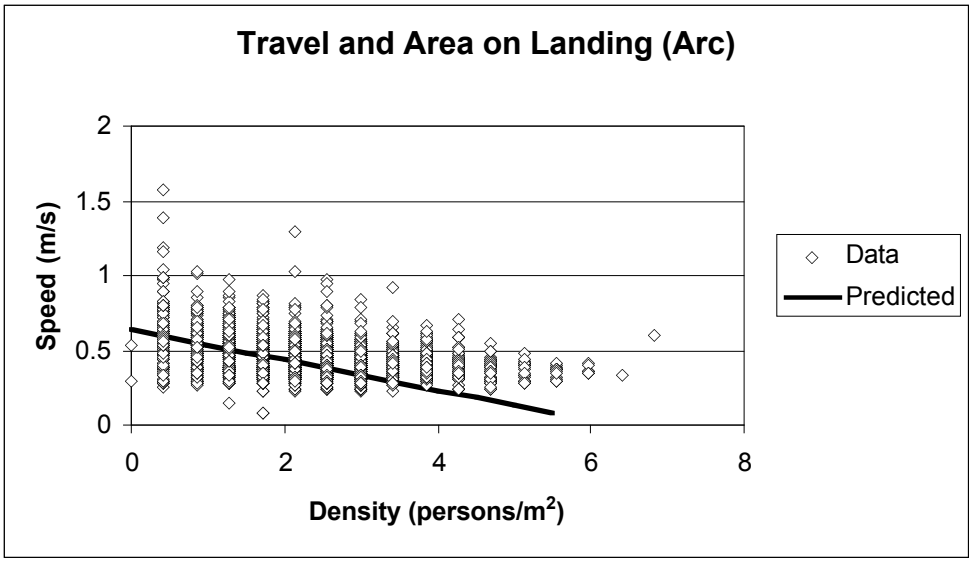

Figure D.5: Arc Length on Landing and Effective Landing Area (Arc) Case

Equation D.1 is a better predictor for this data set than just using the average value (R^2=0.108, approximately two-thirds of the original R^2 value). This is only a result of chance in that the decreasing speeds are approximately countered by the increasing density to give a similar fit to the curve. A paired t-test found the average difference for the reference values was significantly different by 0.019 m/s (95% confidence interval 0.014<x<0.023 m/s). In this comparison, the observed average speed was less than the reference average.

Appendix E: Example of Flow Types

The data for this appendix was from the 4th to 5th floor of the South stair in Building 8. All of the occupants that exited the 5th floor between 180.55 and 576.94 s after the alarm sounded were included in the analysis. This resulted in 288 individuals being considered. Within these times, no individuals entered the stair on the 4th floor and there was always at least one individual on the landing on both the 4th and 5th floors (except for the last individual when leaving the 5th floor). Thus, the flow is considered to be one platoon.

Within this segment of the evacuation, the average descent time was independent of the average number of occupants on the landing when they entered both the 4th and 5th floors (proportional to the density) as can be seen in Figure E.1. The R^2 value is 0.0036, indicating that less than 1% of the variation in descent times can be explained by the average number of people on the landings when that individual entered. Thus, variables other than density are determining what speed occupants are moving at. This is in contrast to the approach indicated in the SFPE Handbook (2008) where speed can be predicted based on density alone. The data are a relatively complete range of potential densities because they varied from individuals nearly in isolation to occupants coming to a complete stop on the stairs.

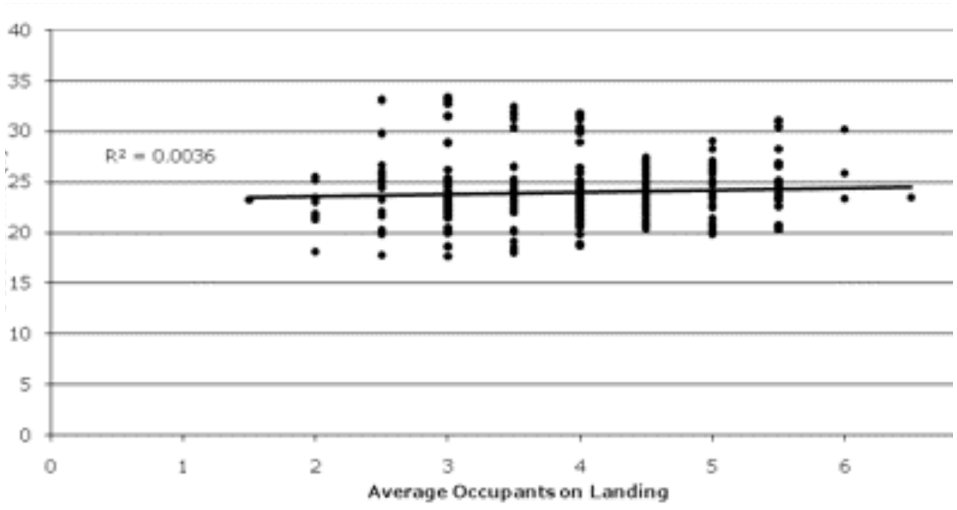

Figure E.1: Descent Time vs. Number of Occupants on Landing

In the raw data, occupants were classified as being on the inner, middle, or outer portion of the stair upon leaving the 5th floor landing and then again for entering the 4th floor landing. For this analysis, while not observed, the probable lane of the occupants between the two floors was desired. The occupants are classified as being in the outer lane, middle, or inner lane based on the lane designation when leaving the 5th floor and entering the 4th floor landings as shown in Table E.1. When possible,

occupants are classified as being in either the inner or outer lane in order to determine how other occupants would be able to pass them. For example, if occupants were recorded as being in the outer lane when leaving the 5th floor and in the middle when entering the 4th floor, they are designated as being in the outer lane. Similarly, if they were in the middle when leaving the 5th floor and the outer lane when entering the 4th floor, they are recorded as being in the outer lane. The inner lane designation is made in a similar manner. Occupants are only classified as being in the middle if (1) they were recorded as only being in the middle on both the 4th and 5th floors or (2) they were recorded as being in the inside lane on one of the two floors and on the outside lane on only the other floor. This exit lane definition led to 46.2% of the individuals as being classified as being in the inner lane, 49.0% being in the outer lane, and 4.8% in the middle.

Table E.1: Lane Assignments

5th Floor	4th Floor	Lane Assigned
Outer	Outer	Outer
Outer	Middle	Outer
Outer	Inner	Middle
Middle	Outer	Outer
Middle	Middle	Middle
Middle	Inner	Inner
Inner	Outer	Middle
Inner	Middle	Inner
Inner	Inner	Inner

Typically (74% of the time), occupants were alternating every other lane either in a staggered file or shoulder-to-shoulder, based only on exit times from the 4th floor[4]. Thus, throughout this segment of the evacuation, both the inner and outer portions of the stairs were considered to be utilized. The position of occupants, with respect to the time since the alarm sounded, is shown in Figure E.2 and Figure E.3[5]. As can be seen in the figures, the occupants were using both sides of the stair (the upper line is occupants in the inner lane and the lower line is occupants in the outer lane) and there were relatively few instances where only occupants on one half of the stair were entering the landing.

[4] Occupants in the middle and those immediately after them were excluded; because no two consecutive individuals were in the middle, including these individuals would have increased the percentage to 76%.

[5] The split between the two figures is used to make the graph more readable and has no other significance.

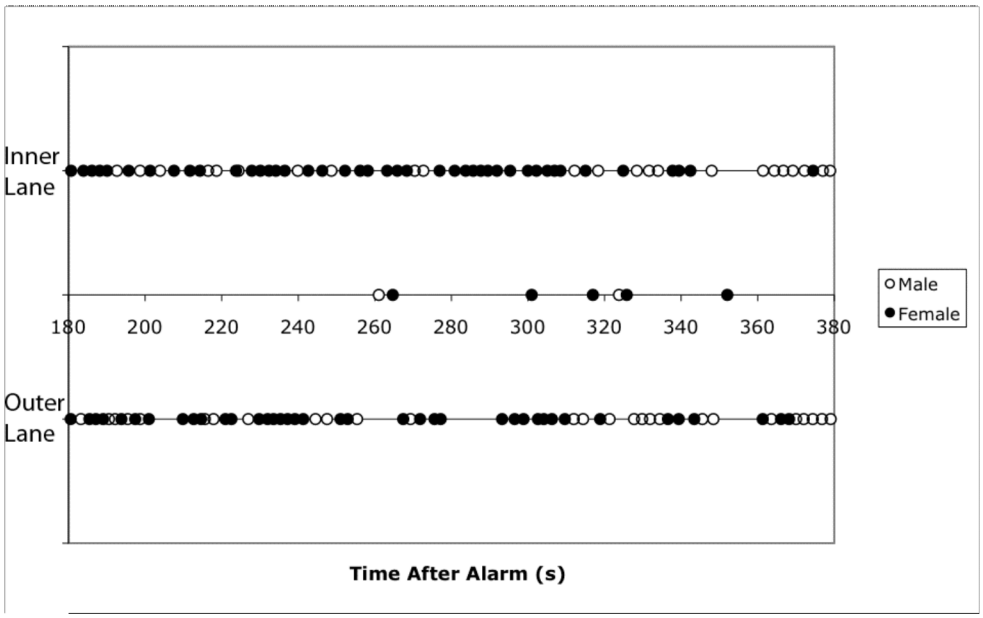

Figure E.2: Exit Lane for First 200s

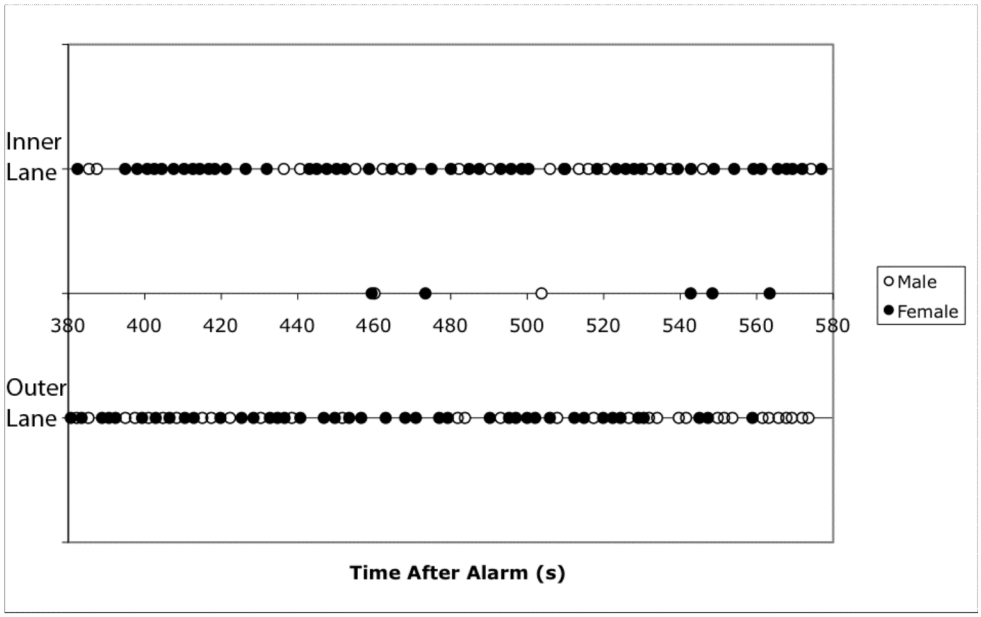

Figure E.3: Exit Lane for Second 200s

For this analysis, groups are defined based on passing behavior and exit lane. In some instances, occupants were passing individuals in the other lane while in other instances no passing behavior was observed. This resulted in different flow types due to this method of defining group behavior.

Two-sided t-tests are performed for each group's descent time. The t-test compares the means from two samples and, based on the sample size and variance, a p-value is then calculated to determine whether the difference in the means is random or reflects a difference in performance.

The null hypothesis in all of the comparisons is that the two groups (usually individuals in the outer lane and individuals in the inner lane or between adjacent groups) had the same average descent time. The alternate hypothesis is that the two times were different. Significance is based on the 95% confidence interval (p-value ≤ 0.05). The smaller that the p-value is, the less likely it is that the two groups are requiring the same amount of time to descend from the 5th floor to the 4th floor.

E.1 Groups Descent Times

The first group consisted of the first twenty-two occupants. Right before this group there had been two individuals, one in each lane, that had allowed individuals to merge from the 4th floor in front of them. Thus, the occupants in both lanes were potentially affected by the merging activity that occurred on the 4th floor. Within this group, every individual in the outer lane that had been followed by an individual in the inner lane on the 5th floor was passed before leaving the landing on the 4th floor. Based on a t-test (results in Table E.2), individuals in the inner lane required statistically less time to descend. One possible explanation for the difference in descent times is that that the merging that had occurred immediately before this point caused more of an effect on the occupants in the outer lane than those in the inner lane. However both lanes had occupants merge into them and the individuals that directly allowed others to enter in front of them were excluded from the analysis. The other possible explanation is that the difference in speeds was due to dynamics unrelated to the previous merging.

Table E.2: Values for Groups Based on Exit Lanes

Group	Number of Occupants Inner/Middle/Outer	Average Time to Descend in s (Standard Deviation) Inner/Outer	p-value
1	10/0/12	23.90 (0.97) / 26.09 (0.87)	$2.6*10^{-5}$
2	8/0/8	20.18 (1.74) / 20.17 (0.95)	0.99
3	5/0/6	19.14 (1.61) / 21.92 (1.31)	0.015
4A	25/3/19	22.70 (1.04) / 23.09 (0.67)	0.25
4B	10/4/12	31.15 (1.14) / 31.80 (1.06)	0.18
4C	17/0/24	23.98 (1.21) / 24.07 (1.14)	0.81
5	6/0/6	26.70 (0.22) / 25.20 (0.73)	0.0030
6	6/0/8	23.16 (0.64) / 23.64 (0.28)	0.13
7A	5/0/4	22.29 (0.67) / 29.17 (0.43)	$4.7*10^{-7}$
7B	Not possible to calculate		
8	14/2/17	24.71 (0.90) / 24.73 (1.11)	0.95
9	6/0/6	20.48 (0.42) / 22.24 (0.62)	$3.2*10^{-4}$
10	10/2/12	21.12 (0.85) / 21.44 (0.76)	0.27
11	8/1/8	20.40 (1.96) / 25.80 (0.81)	$4.2*10^{-5}$

The average time to descend in Table E.2 is shown graphically in Figure E.4.

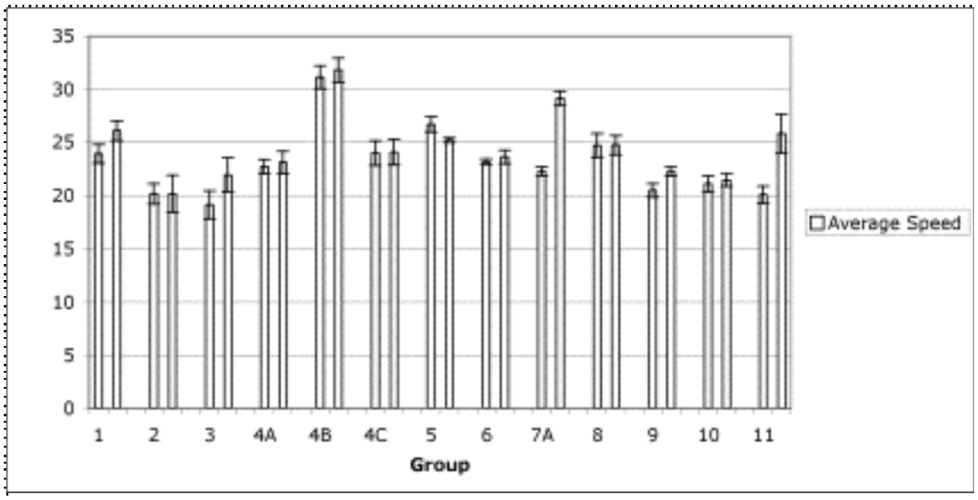

Figure E.4: Time to Descend by Group

The next sixteen occupants (the second group) were split evenly between the two lanes. In no instance within this group did an occupant in the inner lane pass an occupant in the outer lane. As shown in Table E.2, the occupants in the inner and outer lane statistically required the same amount of time to descend from the 5th floor to the 4th floor. Whatever had caused the two lanes to move at different speeds had thus dissipated and any subsequent disparities between the two lanes cannot be attributed to individuals merging into the stairs.

The third group consisted of the next eleven individuals that were split with five being in the inner lane and six being in the outer lane. As had been the case with the first group, all occupants in the outer lane that had been just ahead of an individual in the inner lane on the 5th floor had been passed before leaving the landing on the 4th floor. As shown in Table E.2, the occupants in the inner lane were moving faster, but there were no merging effects as had been a possible explanation with the first group. Thus, some other effect caused the difference in descent times. When the descent times are compared with all individuals from the second group, a t-test for the inner lane gives a p-value of 0.24 and for the outer lane gives a p-value of 0.022. Because $0.24 \geq 0.05$ and $0.022 \leq 0.05$, the hypothesis that the inner lane has the same descent time as the second group cannot be rejected, but the outer lane is requiring more time to descend. Thus, the shift from the second to the third groups was caused by occupants in the outer lane requiring more time to descend from the 5th floor to the 4th floor.

After the third group, the next forty-seven occupants maintained the same order from leaving the 5th floor until leaving the 4th floor with a few exceptions that can be attributed to the two occupants being shoulder-to-shoulder. These occupants comprised the fourth group (part A). From Table E.2, the hypothesis that the occupants in the inner and outer lanes require the same amount of time to descend cannot be rejected. Occupants in the middle had an average descent time of 22.42 s (S.D. 0.49 s) and, using a t-test to compare this value to the average of the rest of the

group, the p-value is 0.25. Again, the hypothesis is not rejected, so everyone in this group is assumed to require the same amount of time to descend. When compared with the occupants in the outer lane of the third group, a t-test gives a p-value of 0.15 and, when compared with the occupants in the inner lane of the third group, the p-value is 0.006. Thus, the hypothesis that the fourth group (part A) requires the same amount of time to descend as the occupants in the outer lane of group 3 failed to be rejected while the occupants in the inner lane of the third group are moving faster. When comparing the second and third groups, the cause of the difference in descent times was that the occupants in the outer lane had slowed down. With this transition of groups, the occupants on the inner lane have slowed to match the occupants on the outer lane.

The fourth group (part B) had no passing. Parts A and B do not represent a change in the flow type. The occupants were forced to come to a stop while on the landing, or before reaching the landing (with the end of Part A, presumably, stopped on the stairs after the 4th floor). With the occupants in part B coming to a complete stop, the descent times are increased, but not due to differences in the groups. The results of a t-test comparing the descent times of occupants in the inner and outer lanes is shown in Table E.2. As was the case with part A, the result is not significant. Occupants in both lanes thus stopped moving for the same basic amount of time and the occupants were unable to pass.

The fourth group continued with part C after the occupants were able to start moving again. As with the distinction between part A and part B, this division is indicative only of the position in the stair (relative to the camera locations) when movement speed was reduced to a standstill and then able to restart and not indicative of any real underlying change. These occupants had been stopped while on the 5th floor landing or before. Like the other parts of the fourth group, the descent times for occupants in both exit lanes (as shown in Table E.2) are not significantly different. The occupants in both lanes are moving together.

Twelve occupants, evenly divided between the two exit lanes, comprised the fifth group. The occupants in the outer lane each passed an occupant in the inner lane as they descended from the 5th to the 4th floor. As shown in Table E.2, this was the only instance where the occupants in the inner lane were moving slower than those that were in the outer lane (and the only instance when the occupants in the two lanes were moving at statistically different speeds and those speeds were both statistically slower than the groups ahead of and behind them). When compared to part C of the fourth group, the p-value from a t-test is 0.008, so the occupants in the outer lane were moving slower than the previous group (and thus the occupants in the inner lane were also moving slower). With both the occupants in the inner and outer lane slowing down, it is possible that some members at the end of the fourth group part C belong with the fifth group in terms of time to descend, but the spacing was not right for passing behavior to be observed over the single observed floor.

The sixth group consisted of the next 14 occupants. No passing behavior was observed and Table E.2 shows that the times for occupants to descend in each lane were not significantly different. When a t-test is used to compare times to descend with the occupants in the outer lane of the fifth group, the p-value is 0.0009, so the sixth group is moving faster than the occupants in the outer lane of the fifth group (and thus also faster than the occupants in the inner lane of that group).

The seventh group (part A) had four individuals in the outer lane being passed by two or three of the five individuals in the inner lane, as compared to the typical single individual passing observed with the other odd number groups. Based on the results shown in Table E.2, individuals in the outer lane required more time to descend. The occupants in the outer lane had the slowest average descent times of all groups except for group four part B.

The seventh group (part B) is similar to part A in that occupants in the inner lane were passing occupants in the outer lane. Within this group, two individuals that were in the outer lane on the 5th floor shifted to the inner lane on the 4th. They were in adjacent positions on the 5th floor, but the trailing occupant passed the leading occupant as well as one other occupant that was in the outer lane. The occupant in the outer lane that was passed had a time to descend of 28.30 s (similar to the outer lane times in part A), the occupant that was trailing on the 5th floor had a time to descend of 23.06 s (similar to the time to descend in part A), and the second occupant that switched lanes had a time to descend of 25.69 s (about half way between the two times). The next individual, able to fill the space vacated by the two lane changers, was in the outer lane and required 23.82 s to descend. Because there were only four occupants and two of them switched lanes at some unknown time between the two floors, it is not possible to determine average times with standard deviations for the different lanes as is done with all of the other groups.

The eighth group consisted of thirty-three individuals. Aside from some individuals that were shoulder-to-shoulder, no passing was observed. However there were two individuals that changed lanes as they descended from the 5th floor to the 4th floor. As shown in Table E.2, the null hypothesis failed to be rejected. Thus, occupants in the inner and outer lanes required the same amount of time to descend from the 5th floor to the 4th floor. To determine if the two individuals that changed lanes were descending in a different amount of time than the rest of the group, a t-test comparing them to the rest of the group gives a p-value of 0.49. Thus, the hypothesis that these times are the same as the rest of the group fails to be rejected. They have statistically similar times to the rest of the eighth group.

Twelve individuals, evenly divided between the two lanes, comprised the ninth group. All of the individuals in the outer lane that had individuals behind them in the inner lane on the 5th floor were passed. From Table E.2, as was the case with the first, third, and seventh (part A) groups, the individuals in the inner lane require less time to descend than those in the outer lane.

The tenth group consisted of twenty-four individuals. As with the other instances of no passing behavior (the other even numbered groups), as shown in Table E.2, the null hypothesis failed to be rejected. Once again, the occupants in the two lanes required the same amount of time to descend. The two individuals in the middle had times to descend of 22.06 s and 20.68 s. Using a t-test to compare these values to the other times in the group, the p-value is 0.93 and the hypothesis that times for these two is the same as the rest of the group also fails to be rejected. When the times of the tenth group are compared to the individuals in the inner and out lanes of the ninth group, the t-tests give respective p-values of 0.0026 and 0.011. Thus, at the 95% confidence level, the times of this group are not similar to, but between, the times of the preceding group. Thus, the occupants in the inner lane are moving slower than the previous occupants in the inner lane, but the occupants in the outer lane are moving faster than the previous occupants in the outer lane.

The eleventh, and final group, consisted of eight individuals in the inner lane, eight individuals in the outer lane and one individual that shifted from the inner to the outer lane. All of the occupants in the outer lane were passed by at least one, usually multiple, individuals in the inner lane. The one occupant that shifted lanes did so before the first individual in the outer lane reached the landing. As shown in Table E.2, occupants in the inner lane were moving faster than occupants in the outer lane. The individual that changed lanes had a time to descend of 18.65 s. Including this individual with the outer lane, the times for each individual were slower than the person ahead. Thus, the speed of this individual is consistent with the other members of the group.

E.2 Flow Types

The selected segment of the evacuation consisted of occupants that were continuously located within the observation area during the drill. As was previously shown, the density was not predictive of the descent times, so other variables accounted for the differences. Groups that formed within the larger flow caused some occupants to require different times than other occupants that were located near them on the 5^{th} floor landing.

Within the continuous flow, two different flow types were identified. These differences were defined in this analysis by the lane individuals were in and passing behavior that occurred between the 5^{th} and 4^{th} floors. However it was not an effect that all occupants experienced equally; the exact relationship appeared to oscillate between the different flow types.

The first flow type is one where the flow in both exit lanes moves in a uniform manner (uniform flow). This type of behavior was observed in the even numbered groups previously discussed. Aside from occupants that walk shoulder-to-shoulder (where the one that is recorded as being in the lead could be constantly changing), all occupants maintain the same order and require the same amount of time to descend from one floor to the next; occupants in either lane are moving together.

This matches the type of behavior around corners (where a landing has two adjacent corners) that Predtechenskii and Milinskii (1978) predicted. For this type of flow, the occupants in the inner lane are traveling a shorter distance than the occupants in the outer lane in the same amount of time. Speeds in the different lanes are adjusted so that the time required in each lane regardless of travel distance is the same.

The second flow type is one where the individuals in the one lane move faster than the ones in the other lane (lane flow). Within lane flow, there are two sub types: when the inner lane moves faster and when the outer lane moves faster.

The inner lane moving faster was seen in the odd numbered groups previously discussed, except for the fifth group. While interactions with merging individuals could have been an issue with the first group, it was not with the subsequent groups. The occupants in the two lanes were moving independently of one another.

This flow type could be caused by the physical geometry of the stairs. The occupants in the inner lane have a shorter distance to travel (less travel distance on the landings), so the two lanes could be moving at the same approximate speed. Another possible explanation is that occupants are self-dividing with faster occupants moving to the inside while the slower occupants move to the outside. In either case, the occupants in this flow type do not feel the need to stay with the person next to them and so continue to move freely.

Lane flow with the outer lane moving faster was seen with the fifth group that was previously discussed. In this case, slower individuals were on the inside as faster individuals were in the outer lane.

The Building 8 Stair S is a sinistral stair, so the inner lane is the right hand lane. Templer (1975) found that slower individuals in the United States tended to stay to the right. This is one possible explanation as to why the occupants in this flow type were located in the inner lane. In a dextral stair, this flow type would only be present if slower individuals do not follow the stay right tendency nor move to the outside (as in the previous flow type), but instead choose to take the shorter path. In the one instance of this flow type, occupants in both lanes were moving slower than both the preceding and subsequent groups. In this example, having the occupants in the inner lane requiring more time than the outer lane was disruptive to the overall flow.

Changes between the types appear to be dependent on the individuals. For example, the second group was a faster moving group where individuals in the outside lane had the same approximate times to descend as individuals in the inside lane of the third group. To transition to the third group, there was an occupant in the outer lane that was moving slower and required more descent time. The transition to the fourth group was completed once an individual on the inside lane moved at the slower speed so as to not pass the outer lane. Also, with occupants in the fourth group coming to a complete stop, transitions to other flow types would have been prevented, potentially

causing more occupants to be included in that group than would have happened in conditions where occupants were able to be continuously moving.

From the data, it is not possible to determine what is causing the transition from one group to another. In some instances, the two lanes are moving independently while in other cases the two lanes are moving together. One possible explanation is that, in reality, the two lanes are always independent and that it is either due to the small area examined (only one floor) or individuals with similar speeds setting the pace for each lane. A second possible explanation is that there are occupants in both lanes that choose to remain together even though one could move faster. This could be caused by the reluctance to pass that previous studies have noted or a relationship between the two occupants that makes them want to stay together during the evacuation.

Beyond what was found in this study, different descent times for individuals in the two lanes could also be caused by variables that were explicitly excluded from this analysis. Specifically, merging individuals could cause occupants in the outside lane to shift inward or stop (to allow the occupants on the floor to descend the stairs). This would have the effect of increasing the number of groups and having an uncontrolled effect on descent times for at least the occupants in the outer lane and, potentially, those in the inner lane as well.

While it was not controlled for, aside from exceptions previously noted, individuals did not change lanes even when the other lane was moving faster. Passing was typically done as one lane passing the other lane rather than individuals weaving through the other occupants. If there was a void in the other lane, caused by the passing of a much slower occupant in the other lane, then occupants could have expand to fill both lanes, but this generally did not happen. For the exceptions where occupants did change lanes in order to pass, it had the potential to be disruptive to the other occupants near them, as happened in the seventh group part B. The effect of dealing with merging individuals is expected to be similar as to what was observed to happen with the individuals that changed lanes to pass.

Glossary

Allow Entering: An occupant located in a platoon in the stair that has an occupant from the floor enter between them and the other occupant that was ahead of them in the platoon.

Available Safe Egress Time (ASET): The amount of time from when the cause of the evacuation has occurred until the conditions become untenable.

Boundary Layer: A gap left between occupants and the wall that is not normally occupied.

Congestion: A first person in a flow unit in the stair that is within three open treads of the previous occupant at the lower floor and is not engaging in passing or being passed behaviors.

Counterflow: When there are people ascending and descending the stairs at the same location at the same time.

Data Point: The values of all variables for a given occupant between two observations.

Density: See Effective Density.

Descent Time: See Effective Normalized Descent Time.

Dextral Stair: A stair that turns to the left while descending.

Effective Density: The number of people per unit of effective area where the effective area is defined based on the observation area and applied boundary layers.

Effective Normalized Descent Time: The amount of time between observations divided by the effective travel distance of a given occupant. It is the inverse of the effective speed.

Effective Speed: The effective travel distance divided by the time between observations. It is the inverse of effective normalized descent time.

Effective Travel Distance: The distance measured along the mean path for an occupant while in the stair from either (1) the floor of origin or (2) the previous observation.

Encumbrance: Something that is being carried.

Exit Lane: A subjective designation as to whether the occupant was on the inner, middle, or outer portion of the stair.

Expected Count: The proportional number of observations expected for a given variable.

First Follower: The second occupant in a flow unit.

First Person in Flow Unit: The first occupant in a flow unit. The flow unit is assigned their characteristics.

Floor of Origin: The floor where the occupant is believed to have entered.

Flow Type: The state of whether the two lanes are moving unified or separately.

Flow Unit: A collection of occupants that are descending together with similar behaviors.

Follower: An occupant that is not the first person in a flow unit.

Free-Flow: An occupant in the stair that is three or more open treads behind the previous occupant at the lower floor and is not engaging in passing or being passed behaviors.

Group: A collection of people that is moving together. They may or may not have a social connection.

Heavy Density: Buildings where the average Level of Service is C or more dense.

Inner Lane: Occupants identified as being on the inner half of the stair when exiting the upper floor and entering the lower floor.

k-Value: A constant used to adjust equations based on different riser heights and tread depths.

Lane Flow: The flow type where multiple occupants in either the inner or outer lane are passing occupants in the other lane.

Light Density: Buildings where the average level of service is at C or less dense.

Merging: Where the flows from the stair and floor mix.

Middle: Occupants identified as being in (1) neither the inner nor outer half of the stair or (2) switching between the inner and out halves of the stair when exiting the upper floor and entering the lower floor.

Mosaic Mode: Videos that are pixilated to distort the view and prohibits viewing of fine details.

Newel: The post around which the stair turns.

Observation: Each time an occupant is seen within the observation area of the cameras.

Observation Area: The combination of treads and landings that are between the enter and exit times recorded in the spreadsheets provided by NIST for a single camera.

Open Treads: A measurement of the spacing between occupants. It is the number of vacant treads between the occupant and the previous occupant.

Outer Lane: Occupants identified as being on the outer half of the stair when exiting the upper floor and entering the lower floor.

Passing: An occupant in the stair that is recorded as being behind an occupant in the upper floor and is then ahead of the occupant on the lower floor, excluding instances of being should-to-shoulder.

Passed: An occupant in the stair that is recorded as being ahead of an occupant in the upper floor and is then behind the occupant on the lower floor, excluding instances of being should-to-shoulder.

Platoon: A continuous string of occupants in the stair.

Pre-Evacuation Time: From the literature: the time from when the occupant is aware of the need to evacuate until (1) they start to move towards an exit, (2) they leave their room of origin, or (3) they are seen in the stair.

Pre-Observation Time: The time from the alarm until the occupant is first observed in the stair.

Previous Flow Unit: The first flow unit preceding the current flow unit that did not engage in passing behavior or was passed.

Queue: A stoppage of the flow where occupants are standing in the stair.

Required Safe Egress Time (RSET): The amount of time an occupant is expected to need to safely evacuate.

Riser: The vertical component from one step to the next.

Security and Floor Wardens: Occupants that are not observed in the stairs until at least 600 s after the alarm.

Shoulder-to-Shoulder: Occupants that are recorded as being within 0.32 s of one another.

Sinistral Stair: A stair that turns to the right while descending.

Speed: See Effective Speed.

Stair: The steps and landings used for vertical egress.

Step: One unit of a stair consisting of a riser and a tread.

Travel Distance: See Effective Travel Distance.

Tread: (1) The horizontal component of a step or (2) a step.

Uniform Flow: The flow type where the occupants in the two lanes are descending together.

Bibliography

Averill, J. D., "Five Grand Challenges in Pedestrian and Evacuation Dynamics", In: Pedestrian and Evacuation Dynamics, 2010 Conference, Peacock, R. D., Kuligowski, E. D., and Averill, J. D. Eds., Springer, New York, 2011. pp. 1-11.

Averill, J. D., Mileti, D. S., Peacock, R. D., Kuligowski, E. D., Groner, N., Proulx, G., Reneke, P. A., and Nelson, H. E., Occupant Behavior, Egress, and Emergency Communication. Federal Building and Fire Safety Investigation of the World Trade Center Disaster, National Institute of Standards and Technology, NIST NCSTAR 1-7, September 2005.

Blair, A. J., The Effect of Stair Width on Occupant Speed and Flow of High Rise Buildings, M.S. Thesis, University of Maryland – College Park, 2010.

Boyce, K. E., Shields, T.J., and Silcock, G. W. H., "Toward the Characterization of Building Occupancies for Fire Safety Engineering: Capabilities of Disabled People Moving Horizontally and on an Incline", Fire Technology, Volume 35, Number I, 1999, pp. 51-67.

Brackston, M. and McDonald, M., “Car-Following: A Historical Review,” Transportation Research Part F: Traffic Psychology and Behaviour, Volume 2, Issue 4, 1999, pp. 181-196.

Bryan, J. L., “Behavioral Response to Fire and Smoke”, In: The SFPE Handbook of Fire Protection Engineering Fourth Edition, DiNenno, P., Ed., National Fire Protection Association, Quincy, MA, 2008.

Bryan, J. L., Smoke as a Determinant of Human Behavior in Fire Situations, University of Maryland, College Park, MD, 1977.

Chertkoff, J. M. and Kushigian, R. H., Don’t Panic: The Psychology of Emergency Egress and Ingress, Praeger Publishers, Westport, CT, 1999.

Daly, P. N., McGrath, F., Annesley, T. J., “Pedestrian Speed/Flow Relationships for Underground Stations”, Traffic Engineering and Control, Volume 32, Number 2, 1991, pp. 75-78.

Fahy, R. F., “Calculation Methods for Egress Prediction”, In: Fire Protection Handbook Twentieth Edition, A. Cote, Ed., National Fire Protection Association, Quincy, MA, 2008.

Francis, R. L. and Saunders, P. B., EVACNET: Prototype Network Optimization Models for Building Evacuation, National Bureau of Standards, NBSIR 79-1593, 1979.

Frantzich, H., “A Model for Performance-Based Design of Escape Routes”, Department of Fire Safety Engineering, Lund Institute of Technology, Lund University, December 1994.

Frantzich, H., “Study of Movement on Stairs during Evacuation Using Video Analysis Techniques”, Department of Fire Safety Engineering, Lund Institute of Technology, Lund University, March 1996.

Fruin, J. J., Designing for Pedestrians: A Level of Service Concept”, Transportation Research Record 355, 1971, pp. 1-15.

Fruin, J. J., Pedestrian Planning and Design, Metropolitan Association of Urban Designers and Environmental Planners, Inc., New York, NY, 1971.

Fujiyama, T. and Tyler, N., “An Explicit Study on Walking Speeds of Pedestrians on Stairs”, Presented at 10th International Conference on Mobility and Transport for Elderly and Disabled People, Hamamatsu, Japan, 2004.

Galbreath, M., “Time of Evacuation by Stairs in High Buildings” National Research Council of Canada, Fire Research Note No. 8, May 1969.

Galea, E. R., Deere, S., Sharp, G., Filippidis, L., and Hulse, L., "Investigating the impact of culture on evacuation behaviour", Proceedings of the 12th International Fire Science & Engineering Conference, Interflam 2010, 5-7th July 2010, University of Nottingham, UK, Volume 1, pp. 879-892.

Galea, E. R., Finney, K. M., Dixon, A. J. P., Siddiqui, A. and Cooney, D. P., "The AASK Database V4.0: Aircraft Accident Statistics and Knowledge: A Database to Record Human Experience of Evacuation in Aviation Accidents", available from Federal Aviation Administration website: http://www.fire.tc.faa.gov/2004Conference/files/evac/E.Galea_AASK_Database.pdf. Last viewed October 2011.

Galea, E. R., Hulse, L., Day, R., Siddiqui, A., and Sharp, G., "The UK WTC 9/11 Evacuation Study: an Overview of the Methodologies Employed and Some Analysis Relating to Fatigue, Stair Travel Speeds and Occupant Response Times", Proceedings of the 4th International Symposium on Human Behaviour in Fire, Robinson College, Cambridge, UK, 2009, pp. 27-40.

Galea, E.R. and Blake, S., Collection and analysis of human behaviour data appearing in the mass media relating to the evacuation of the World Trade Centre towers of 11 September 2001, Office of the Deputy Prime Minister, 2004.

Galea, E.R., Sharp, G., and Lawrence, P.J., "Investigating the Representation of Merging Behavior at the Floor-Stair Interface in Computer Simulations of Multi-Floor Building Evacuations", Journal of Fire Protection Engineering, 18,4, November 2008, pp. 291-316.

Gates, T. J., Noyce, D. A., Bill, A. R., and Van Ee, N., "Recommended Walking Speeds for Pedestrian Clearance Timing Based on Pedestrian Characteristics", Transportation Research Board 85th Annual Meeting Compendium of Papers CD-ROM, November 2005.

Gwynne, S. M. V. and Rosenbaum, E. R., "Employing the Hydraulic Model in Assessing Emergency Movement", In: The SFPE Handbook of Fire Protection Engineering Fourth Edition, DiNenno, P., Ed., National Fire Protection Association, Quincy, MA, 2008.

Hall, E. T., The Hidden Dimension, Double Day & Company, Inc., Garden City, NY, 1966.

Hostikka, S., Paloposki, T., Rinne, T., Saari, J., Korhonen, T., and Heliövaara, S., "Evacuation Experiments in Offices and Public Buildings", VTT, Working Papers 85, 2007.

Hyun-seung, Hwang., Jun-ho, C., and Won-hwa, H., “Calculating and Verifying the Staircase-length for Evacuation Analysis”, In: Pedestrian and Evacuation Dynamics, 2010 Conference, Peacock, R. D., Kuligowski, E. D., and Averill, J. D., Eds., Springer, New York, 2011, pp. 601-610.

Jin, T., “Visibility through Fire Smoke”, Report of Fire Institute of Japan, 42, 1976, pp. 12-18.

Joint Committee, “Fire Grading of Buildings. Part III. Precautions Relating to Personal Safety”, Post-war Building Studies Number 29, 1952, pp. 22-95.

Jones, B. K., Hewitt, J. A., “Leadership and Group Formation in High-Rise Building Evacuation”, Fire Safety Science: Proceedings of the 1st International Symposium, Gaithersburg, Maryland, 1985, pp. 513-522.

Kagawa, M., Kose, S., and Morishita, Y., “Movement of People on Stairs during Fire Evacuation Drill-Japanese Experience in a Highrise Office Building”, Fire Safety Science: Proceedings of the 1st International Symposium, Gaithersburg, Maryland, 1985, pp. 533-540.

Keating, J.P., “The Myth of Panic”, Fire Journal, Volume 76, 1982, pp. 57-61.

Kendik, E., “Designing Escape Routes in Buildings”, Fire Technology, Volume 22, November 1986, pp. 272-294.

Khisty, C. J., “Pedestrian Flow Characteristics on Stairways During Disaster Evacuation”, Transportation Research Record 1047, 1985, pp. 97-102.

Kratchman, J. A., An Investigation on the Effects of Firefighter Counterflow and Human Behavior in a Six-Story Building Evacuation, M.S. Thesis, University of Maryland – College Park, 2007.

Kuligowski, E. D. and Hoskins, B. L., "Analysis of Occupant Behavior", In: Pedestrian and Evacuation Dynamics, 2010 Conference, Peacock, R. D., Kuligowski, E. D., and Averill, J. D., Eds., Springer, New York, 2011. pp. 685-698.

Kuligowski, E. D. and Peacock, R. D., "Building Occupant Egress Data," Report of Test FR 4024, National Institute of Standards and Technology, Gaithersburg, MD, 2010.

Kuligowski, E. D., Peacock, R. D., and Hoskins, B. L., A Review of Building Evacuation Models 2nd Edition, National Institute of Standards and Technology, NIST TN-1680, 2010

Lee, J. Y. S. and Lam, W. H. K, “Variation of Walking Speeds on a Unidirectional Walkway and on a Bidirectional Stairway”, Transportation Research Record 1982, 2006, pp. 122-131.

London Transport Board, “Second Report of the Operational Research Team on the Capacity of Footways”, London Transport Board Research Report No. 95, August 1958.

Melinek, S. J. and Booth, S., “An Analysis of Evacuation Times and the Movement of Crowds in Buildings”, Building Research Establishment, Current Paper 96/75, 1975.

National Bureau of Standards, Design and Construction of Building Exits, National Bureau of Standards, Miscellaneous Publication M151, October 1935.

National Fire Protection Association, Life safety code, National Fire Protection Association, Quincy, MA, 2009.

Nelson, H. E. and MacLennan, H. A., "Emergency movement", In: SFPE Handbook of Fire Protection Engineering, National Fire Protection Association, DiNenno, P..J., Ed., Quincy, MA, 1995, pp. 286-295.

Pauls, J. L. and Jones, B.K., “Building Evacuation: Research Methods and Case Studies”, Fires and Human Behaviour, Cantor, D., Ed., John Wiley & Sons, New York, NY, 1980, pp. 227-249.

Pauls, J. L., “Building Evacuation: Research Findings and Recommendations”, Fires and Human Behaviour, Cantor, D., Ed., John Wiley & Sons, New York, NY, 1980, pp. 251-275.

Pauls, J. L., “Evacuation Drill Held in the BC Hydro Building 26 June 1969”, National Research Council of Canada, Building Research Report 80, 1971.

Pauls, J. L., Fruin, J. J., and Zupan, J. M., Minimum stair-width for evacuation, overtaking movement and counterflow – technical bases and suggestions for the past, present and future”, In: Pedestrian and Evacuation Dynamics 2005, Waldau, N. Gattermann, P., Knoflacher, H., and Schreckenberg M., Eds., Springer-Verlag, Heidelberg, 2007, pp. 57–69.

Pauls, J., “The Movement of People in Buildings and Design Solutions for Means of Egress”, Fire Technology, Volume 20, Issue 1, 1984, pp. 27-47.

Peacock, R. D., Averill, J. D., and Kuligowski, E. D., “Stairwell Evacuations from Buildings: What we Know We Don’t Know”, National Institute of Standards and Technology, NIST Technical Note 1624, 2009.

Peacock, R. D., Hoskins, B. L., and Kuligowski, E. D., "Overall and Local Movement Speeds During Fire Drill Evacuations in Buildings up to 31 Stories", In: Pedestrian and Evacuation Dynamics, 2010 Conference, Peacock, R. D., Kuligowski, E. D., and Averill, J. D., Eds., Springer, New York, 2011, pp. 25-36.

Predtechenskii, V. M. and Milinskii, A. I., Planning for Foot Traffic Flow in Buildings, Translated by Sivaramakrishnan, M. M., Amerind Publishing Co. Prvt. Ltd., New Delhi, India, 1978.

Proulx, G, "Evacuation Time and Movement in Apartment Buildings", Fire Safety Journal, Volume 24, Issue 3, 1995, pp. 229-246.

Proulx, G., "Evacuation Timing", The SFPE Handbook of Fire Protection Engineering Fourth Edition, DiNenno, P., Ed., National Fire Protection Association, Quincy, MA, 2008.

Proulx, G., Bénichou, N., Hum, J. K., Restivo, K. N., "Evaluation of the Effectiveness of Different Photoluminescent Stairwell Installations for the Evacuation of Office Building Occupants", National Research Council of Canada, Research Report 232, 2007.

Proulx, G., Kaufman, A., and Pineau, J., “Evacuation Times and Movement in Office Buildings”, National Research Council of Canada, Internal Report 711, 1996.

Proulx, G., Latour, J. C., Maclaurin, J. W., Pineau, J., Hoffman, L. E., and Laroche, C., “Housing Evacuation of Mixed Ability Occupants in Highrise Buildings”, National Research Council of Canada, Internal Report 706, 1995.

Proulx, G., Tiller, D. K., Kyle, B. R., and Creak, J., “Assessment of Photoluminescent Material During Office Occupant Evacuation”, National Research Council of Canada, Internal Report 774, 1999.

Pushkarev, B. and Zupan, J. M., Urban Space for Pedestrians, MIT Press, Cambridge, MA, 1975.

Robertson, D. I., “TRANSYT Method for Area Traffic Control”, Traffic, Engineering, and Control, Volume 11, Issue 6, 1969, pp. 276-281.

Shields, T. J., Boyce, K. E., and McConnell, N., “The Behaviour and Evacuation Experiences of WTC 9/11 Evacuees with Self-Designated Mobility Impairments”, Fire Safety Journal, Volume 44, 2009, pp. 881-893.

Shields, T. J., Boyce, K. E., Silcock, G. W. H., and Dunne, B., “The Impact of a Wheelchair Bound Evacuee on the Speed and Flow of Evacuees in a Stairway during an Uncontrolled Unannounced Evacuation”, Journal of Applied Fire Science, Volume 7, Number 1, 1997-1998, pp. 29-39.

Sime, J., "Escape Behaviour in Fires and Evacuations", In: Design Against Fire: An Introduction to Fire Safety Engineering Design, Stollard, P. and Johnston, L., Eds., E & FN Spon: An Imprint of Chapman & Hall, London, UK, 1994, pp. 56-87.

Smith, R. A., “Density, Velocity, and Flow Relationships for Closely Packed Crowds”, Safety Science, Volume 18, 1995, pp. 321-327.

Tanaboriboon, Y. and Guyano, J. A., “Analysis of Pedestrian Movements in Bangkok”, Transportation Research Record 1294, 1991, pp. 52-56.

Templer, J. A., Stair Shape and Human Movement, Ph.D. Dissertation, Columbia University, 1975.

Templer, J. A., The Staircase: Studies of Hazards, Falls and Safer Design, The MIT Press, Cambridge, MA, 1992.

Templer, J., Mullet, G. M., Archea, J., and Margulis, S. T., An Analysis of the Behavior of Stair Users, National Bureau of Standards, NBSIR 78-1554, 1978.

Tubbs, J. S. and Meacham, B. J., Egress Design Solutions, John Wiley and Sons, Hoboken, NJ, 2007.

Wright, M. S., Cook, G. K., and Webber, G. M. B., "The Effects of Smoke on People's Walking Speeds Using Overhead Lighting and Wayguidance Provision", Human Behavior in Fire, Proceedings of the 2nd International Symposium, MIT, March 2001.

Ye, J., Chen, X., Yang, C., and Wu, J., "Walking Behavior and Pedestrian Flow Characteristics for Different Types of Walking Facilities", Transportation Research Record 2048, 2008, pp. 43-51.